

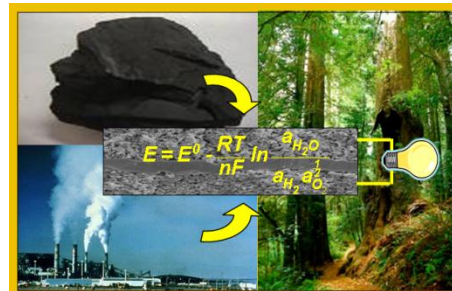
# Progress in Coal Syngas Contaminants Study at West Virginia University

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 West Virginia University

**NIFT**

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- Valuable contributions by Dr. Richard Bajura and the continued support of NRCCE (National Research Center for Coal and Energy) are acknowledged with sincere gratitude.
- The results presented here are the outcomes of the combined efforts of these researchers:

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# Outline

- Introduction
- Objectives
- Methodology
- Characterization of Impurity Effects on SOFC's
- Remedies for Impurity Poisoning
- Modeling
- Conclusions

# Introduction

- Coal syngas contains numerous contaminants and trace elements: As, P, Hg, Cd, Zn, Sb, Pb, Bi, Na, K, Fe etc.
- Small amounts of contaminants (1-5 ppm) cause significant degradation in SOFC performance.
- The effect of some trace elements is not well established.
- It is expensive to completely remove the contaminants, hence Lifetime prediction of the SOFCs exposed to low levels of fuel impurities is critical for design considerations.
- Remedies are needed for contaminant poisoning.

# Objectives

- Characterize degradation mechanisms for coal syngas trace contaminants.
- Develop novel anode materials for improving performance of SOFCs operating on coal-Syngas.
- Predict lifetime and durability of cell and stacks.

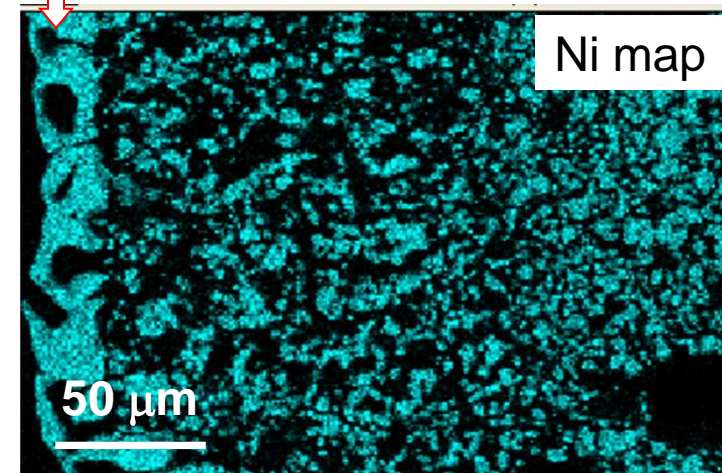
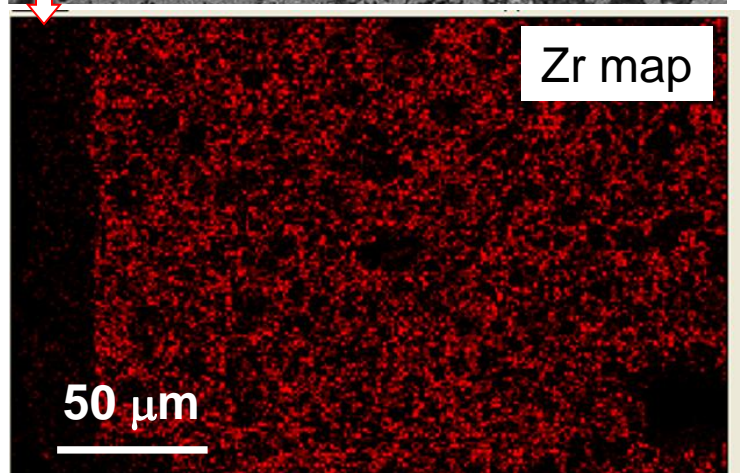
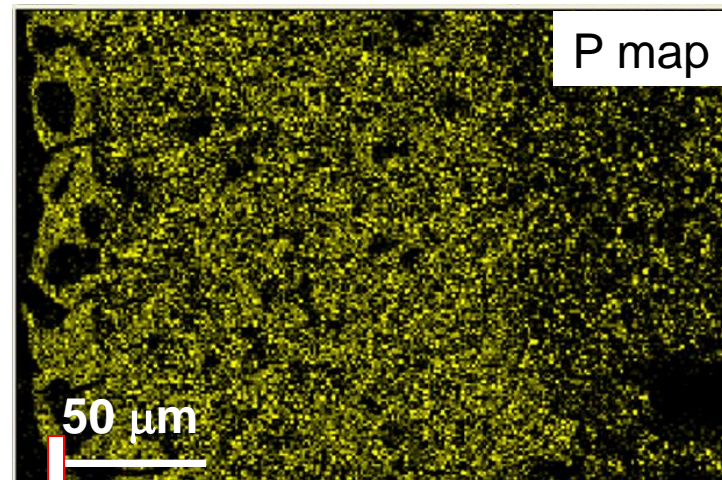
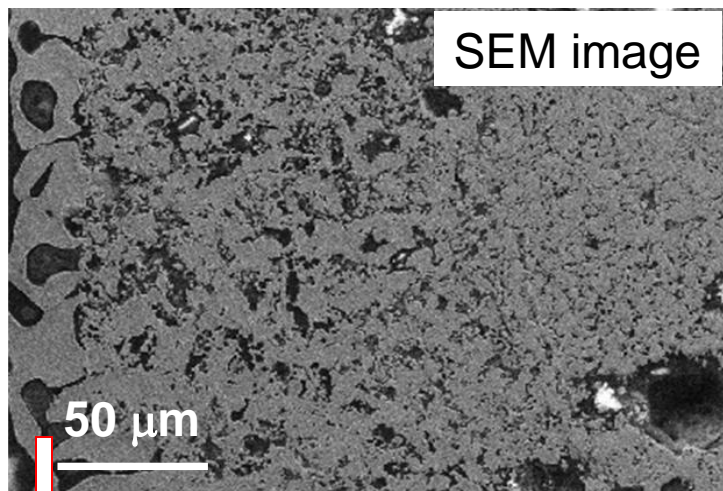
# Methodology

- Multi-scale, multidisciplinary approach.
- In-house cell manufacturing using novel materials and techniques.
- Electrode and cell level testing in simulated syngas with contaminants.
  - SEM, XPS, XRD, TEM, Raman, EDAX
  - EIS, CV, ESEM, MS, Van Der Pauw, In-situ temperature and deformation measurement
- Continuum level modeling for cell and system level performance analysis.
- Phenomenological modeling based on accelerated laboratory tests to predict long term slow degradation rates and lifetime.



# Effect of $\text{PH}_3$ on the Microstructure

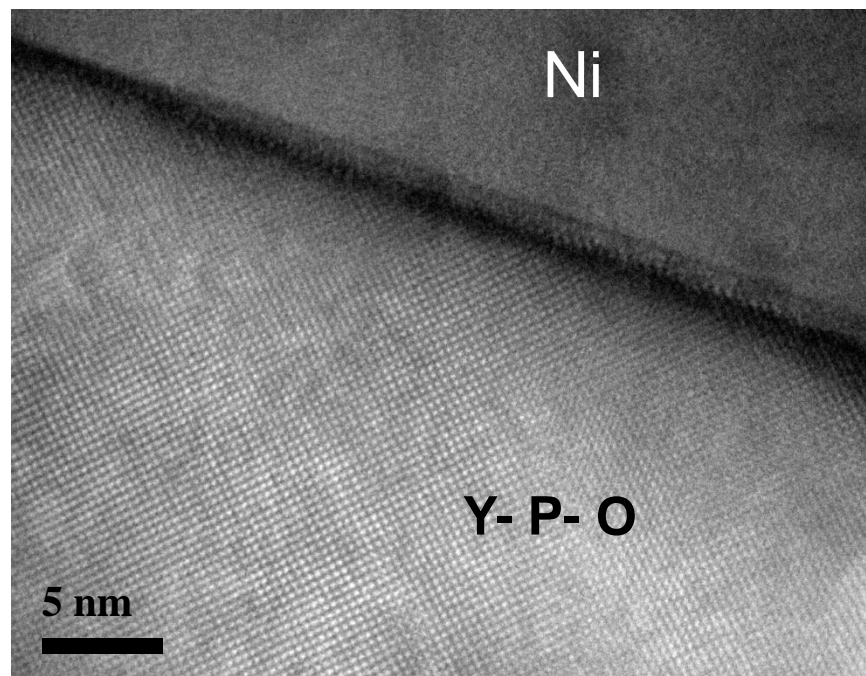
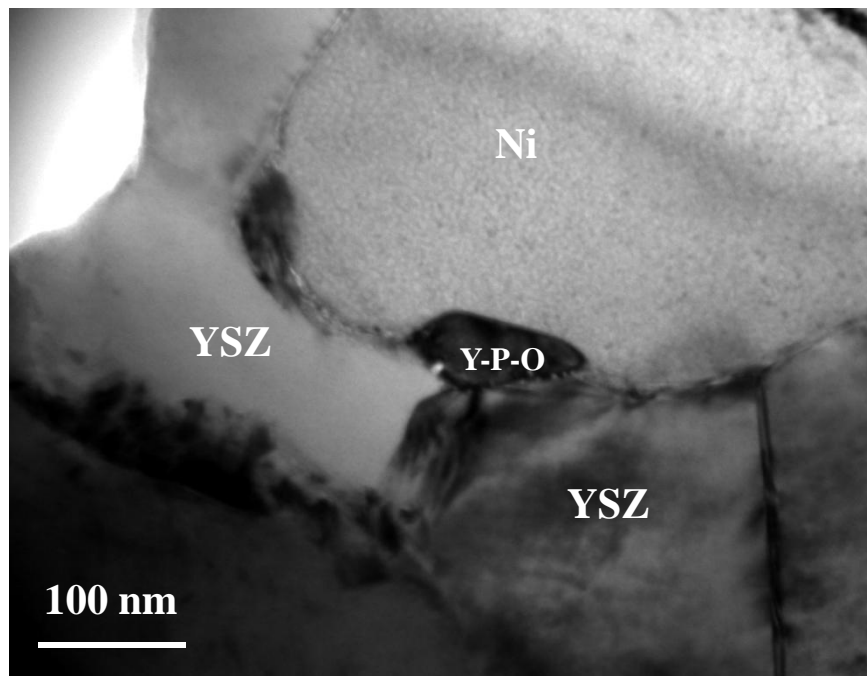
SOFC operated in syngas with 10ppm  $\text{PH}_3$  for 250 h



(I). Formation of Ni-P outer layer

# Effect of $\text{PH}_3$ on the Microstructure (TEM)

SOFC operated in syngas with 10ppm  $\text{PH}_3$  for 100 h

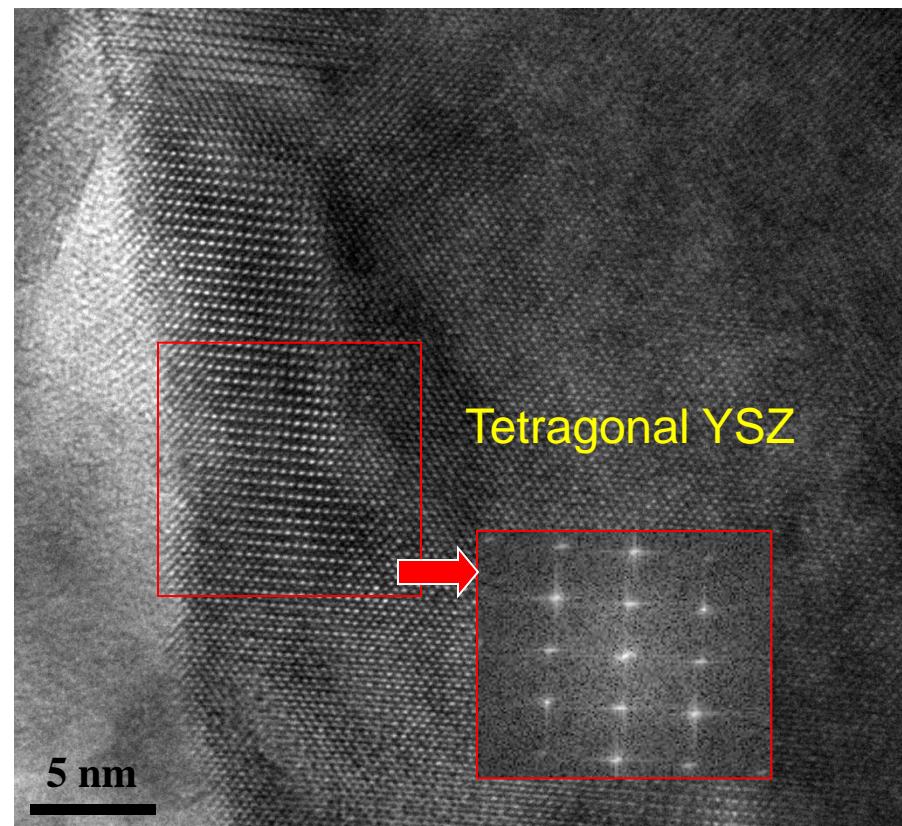
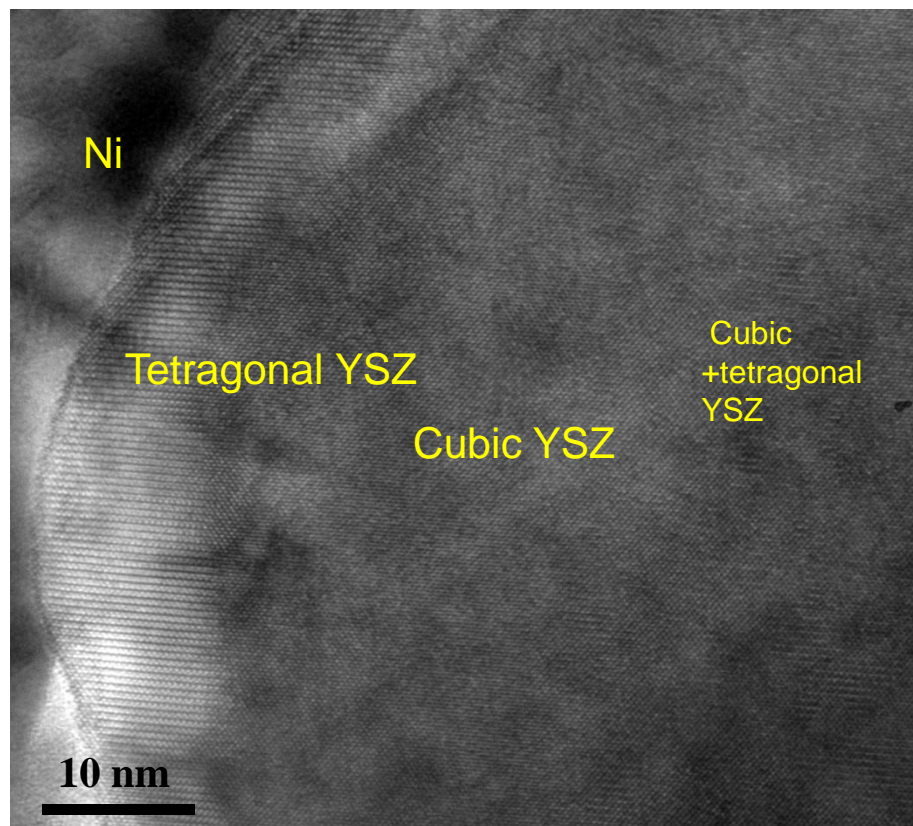


(II). Formation of Y-P-O phase at Ni/YSZ interface



# Effect of $\text{PH}_3$ on the Microstructure (TEM)

SOFC operated in syngas with 10ppm  $\text{PH}_3$  for 100 h



(III). Formation of tetragonal YSZ layer(5-10nm) at Ni/YSZ interface

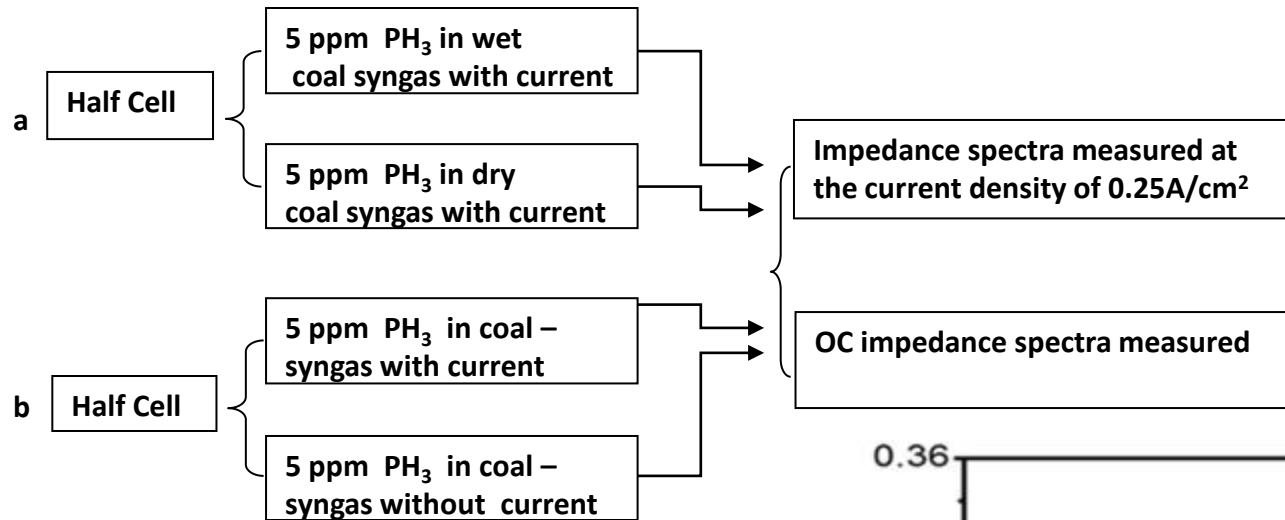
# Effect of $\text{PH}_3$ on the Microstructure

SOFC operated in syngas with 10ppm  $\text{PH}_3$  for over 100 h:

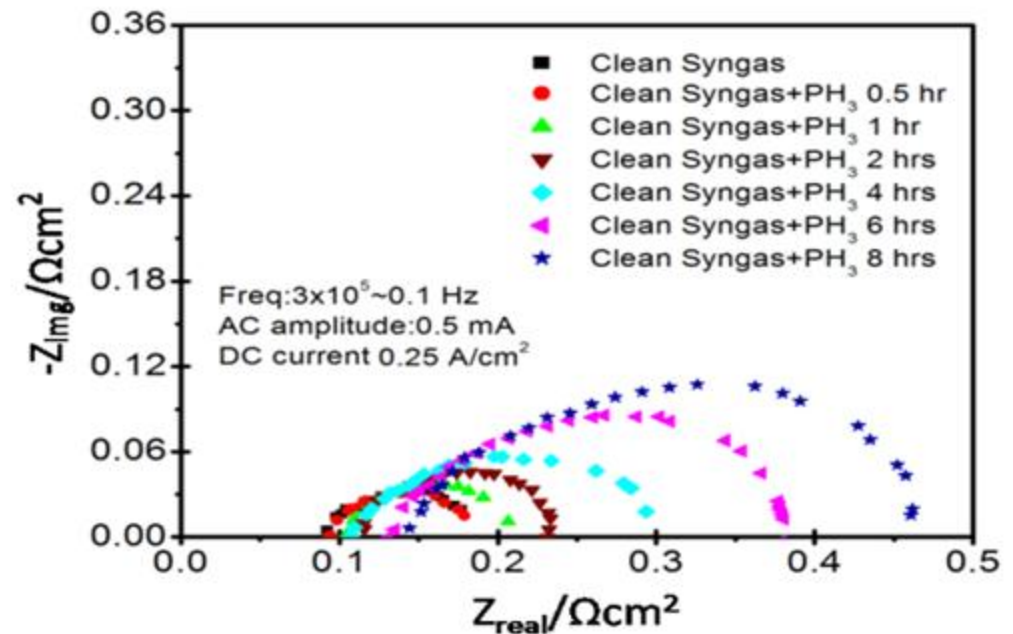
- (I).  $\text{PH}_3$  reacts with Ni and forms a thick layer of Ni-P phase at the outer layer of anode.
- (II).  $\text{PH}_3$  also reacts with YSZ and forms a Y-P-O phase at the interface of Ni/YSZ.
- (III).  $\text{PH}_3$  contamination causes Y deficiency in the YSZ at the Ni/YSZ interface, which consequently forms a tetragonal YSZ interface layer.

***Conclusion:  $\text{PH}_3$  reacts with both Ni and YSZ from the anode of the SOFC.***

# Performance Degradation due to $\text{PH}_3$



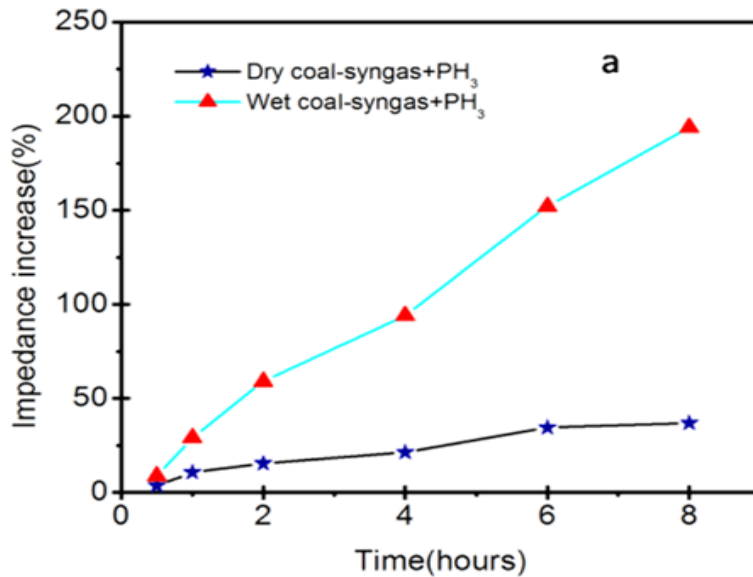
Anode half-cell test: (a) in dry and water containing condition; (b) with and without current loading;  $T = 800^\circ\text{C}$



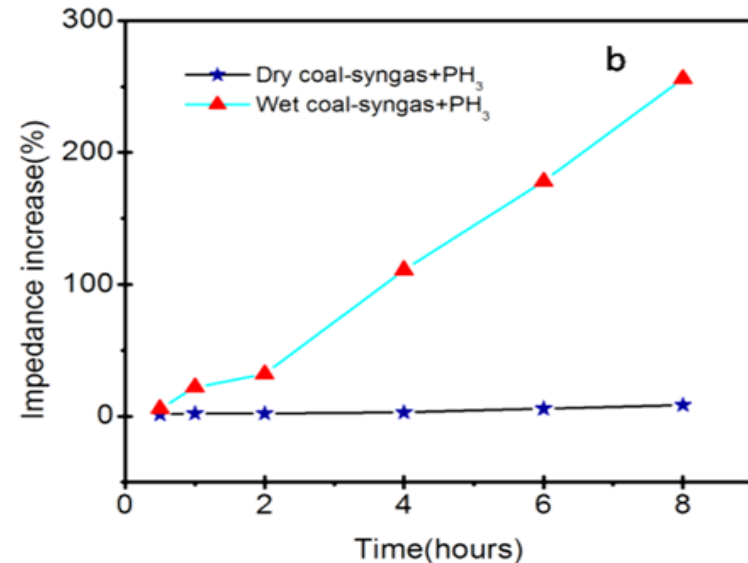
Example impedance spectrum taken from a half cell operated at  $0.25\text{A}/\text{cm}^2$  in wet coal-syngas with 5 ppm  $\text{PH}_3$ .

# Performance Degradation due to $\text{PH}_3$

## Cell operation in dry and wet syngas



a) Impedance with at 0.25 A/cm² bias measured at different times

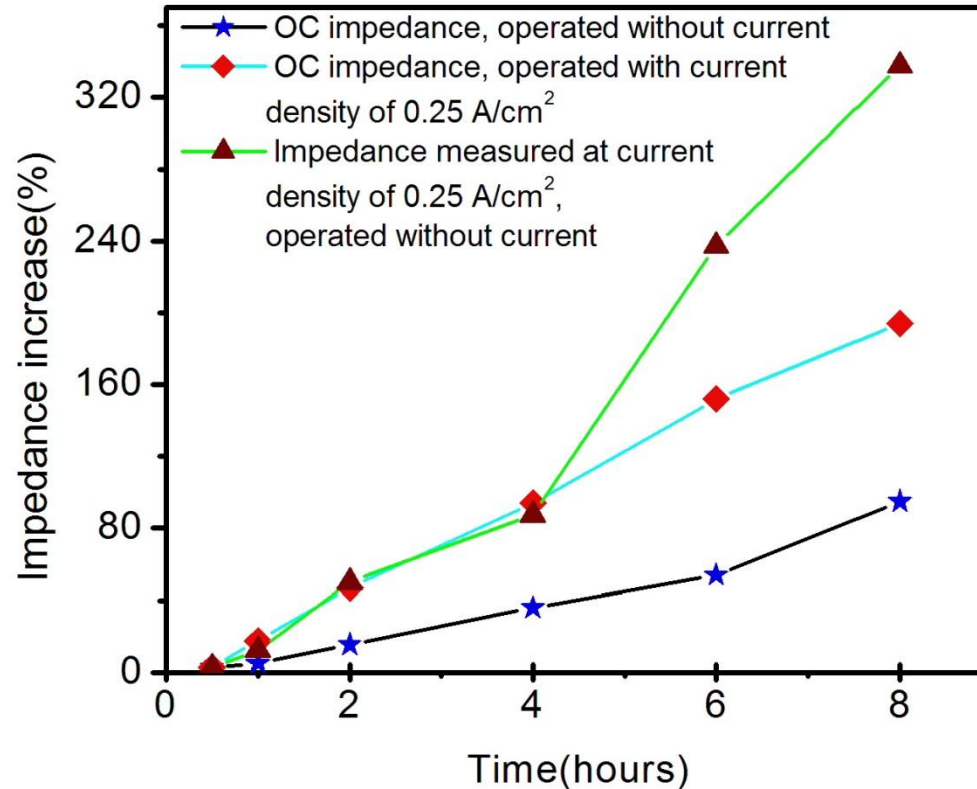


b) OC impedance measured at different times

*The increase in the polarization resistances measured for the cell operated in dry coal-syngas with 5 ppm  $\text{PH}_3$  is ambiguous, while that measured for the cell in wet coal-syngas with 5 ppm  $\text{PH}_3$  is significant.*

# Performance Degradation due to $\text{PH}_3$

## Cell operation with and without current in wet syngas

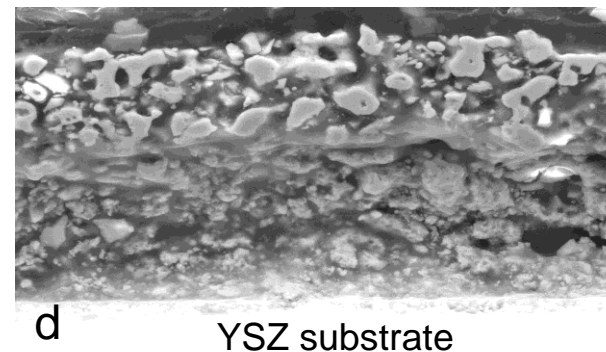
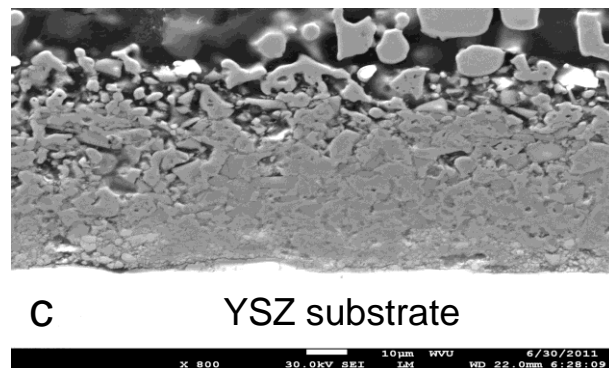
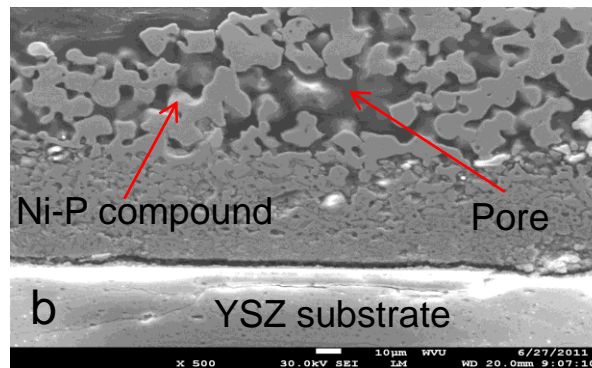
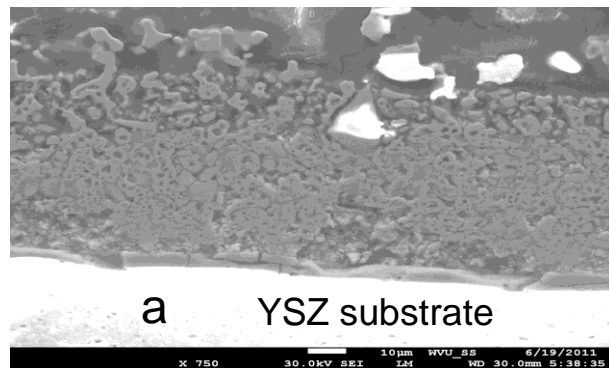


*The increase in activation polarization impedance is larger with current loading than that without current loading.*



# Performance Degradation due to $\text{PH}_3$

## Ni-YSZ anode after being exposed to $\text{PH}_3$ in various conditions

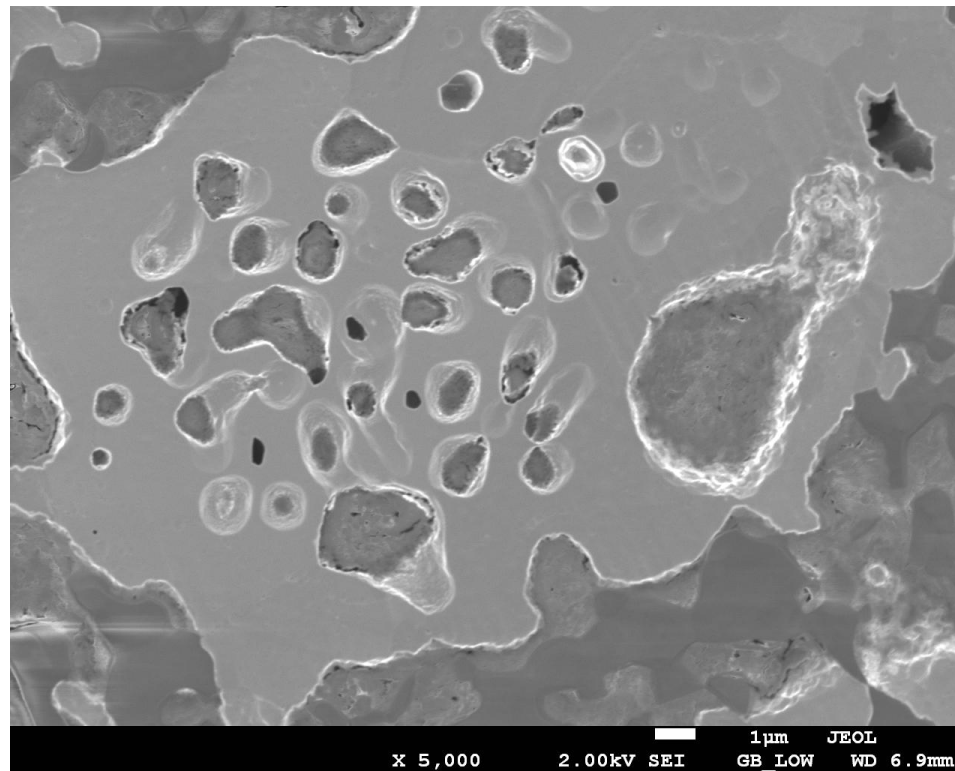


- a. Clean syngas,
- b. 5 ppm  $\text{PH}_3$  for 24 hrs with current density of  $0.25\text{A}/\text{cm}^2$ ,
- c. 5 ppm  $\text{PH}_3$  for 24 hrs without current loading,
- d. 5 ppm  $\text{PH}_3$  for 24 hrs dry syngas

- The half-cell operated with current loading shows (Fig.5b&c) more aggregates to big particles compared to cell w/o current.
- The anode operated with 5 ppm  $\text{PH}_3$  in dry coal syngas exhibits more severe agglomeration compared to wet syngas.

# Effect of $\text{PH}_3$ on Microstructure

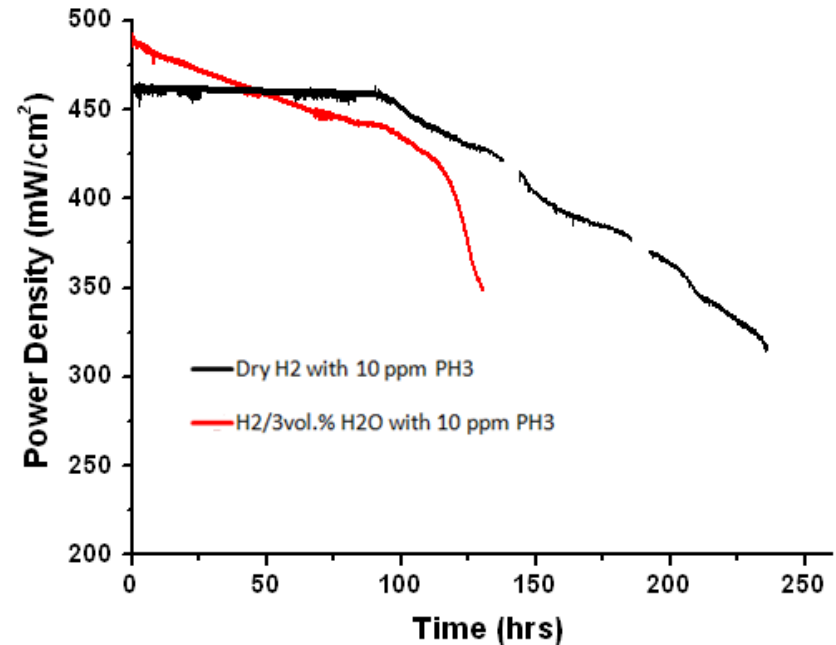
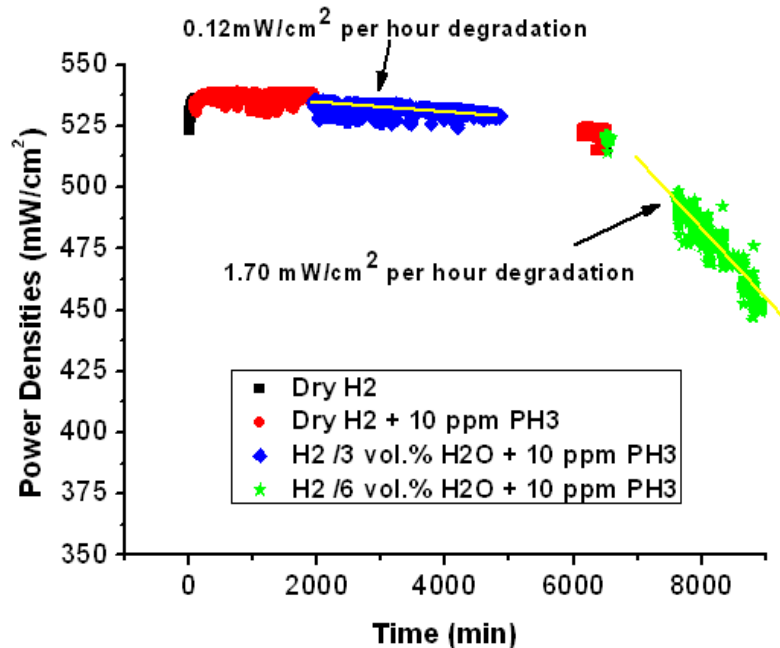
SEM analysis of SOFC anode after exposure to syngas plus 10 ppm phosphine for 250 hrs at  $0.5 \text{ A/cm}^2$ . Sample impregnated with polymer, cut and polished.



*The nickel phase (the lighter gray area in the center) exhibits considerable pitting. Ni, C, P, and O elements detected in the pits.*

# PH3 Effects on SOFC Performance: Fuel Cell

## Dry vs. Wet Conditions

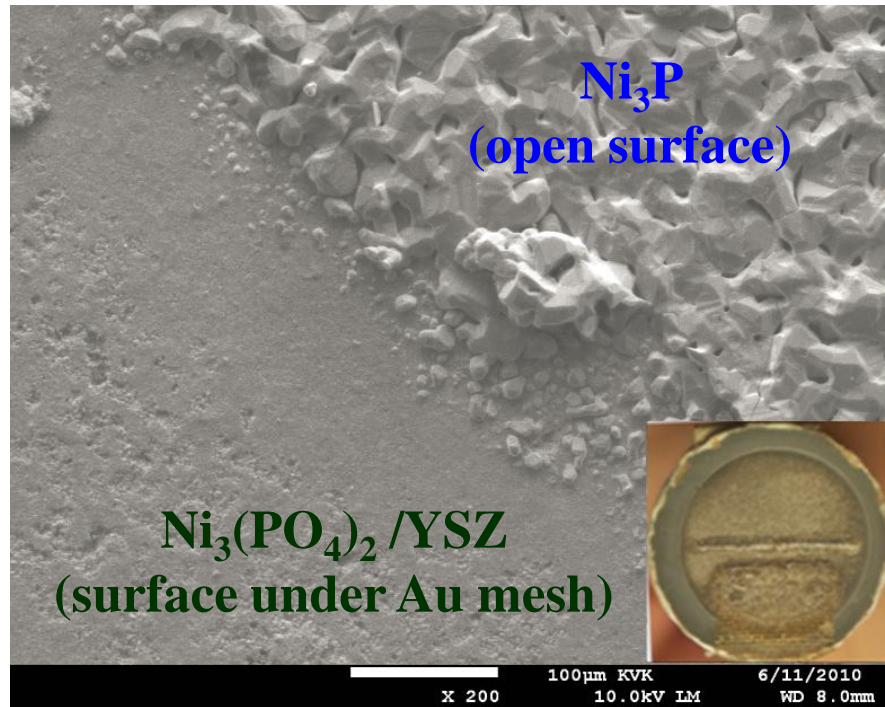


Power density history under dry and wet H<sub>2</sub> + PH<sub>3</sub>

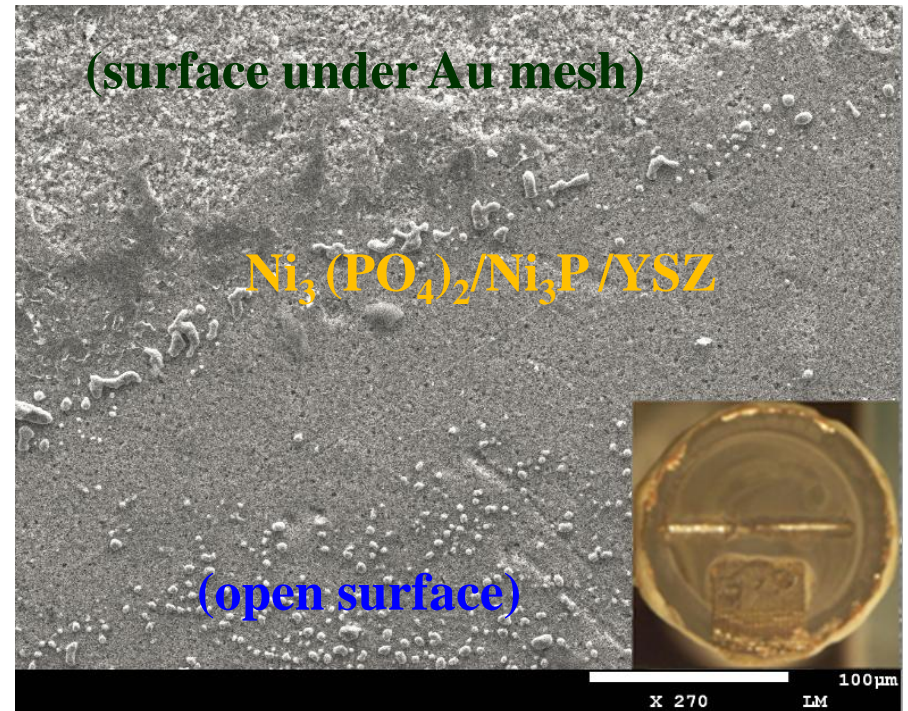
- Cell *degrades immediately* in H<sub>2</sub>+3%H<sub>2</sub>O with 10ppm of PH<sub>3</sub>
- Cell performance *remains stable* in dry H<sub>2</sub>+10ppm of PH<sub>3</sub> for about 4 days and then degrades slowly due to the formation of nickel phosphate
- The rapid failure at the later stage might be caused by substantial internal stresses in the Ni-free YSZ matrix due to the Ni migration and secondary phase stratification.



# Surface Morphology Changes due to $\text{PH}_3$



$\text{PH}_3 + \text{H}_2/3 \text{ vol.}\% \text{H}_2\text{O}$  for 9 days

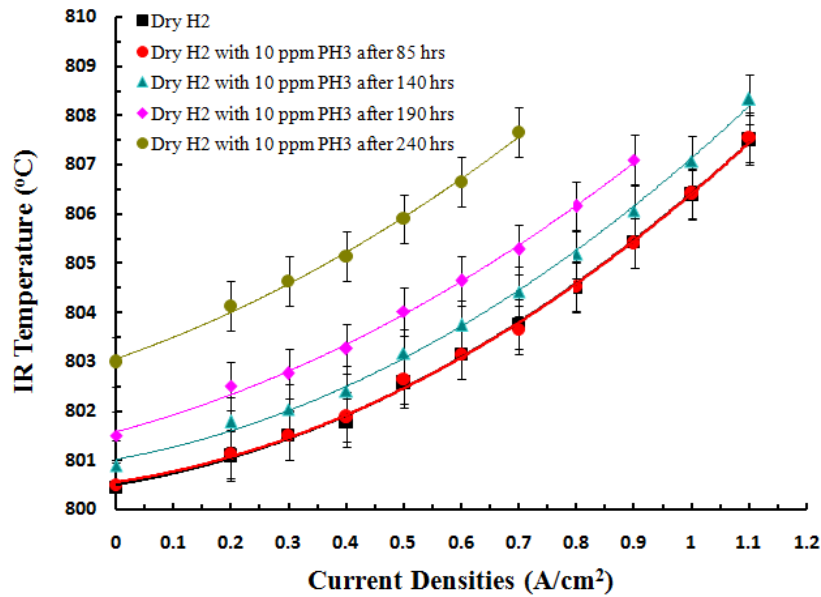


$\text{PH}_3 + \text{dry H}_2$  for 11 days

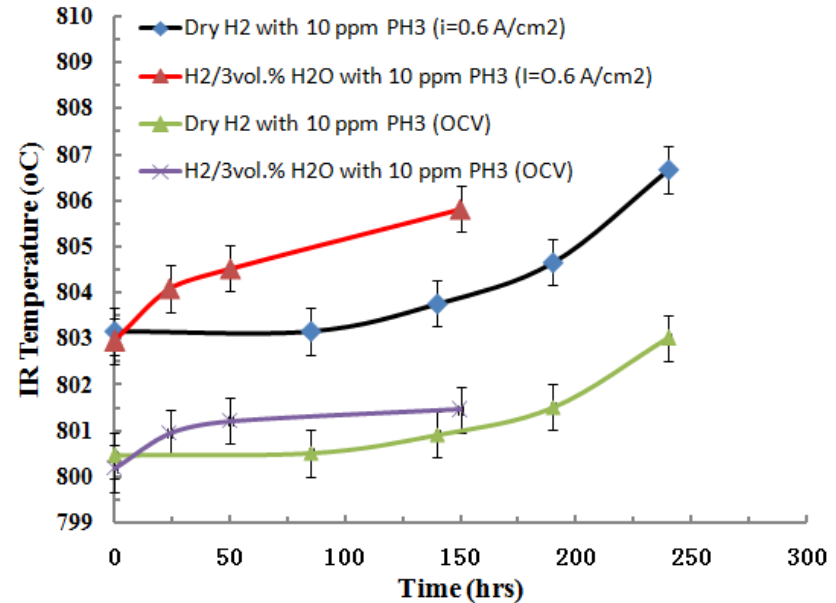
*Steam accelerates the migration of Ni to the surface and reaction with Phosphorous*

# In-Situ Temperature Measurements

## Temperature: Variation due to $\text{PH}_3$ Effects



Surface IR Emission Variation as a function of current density



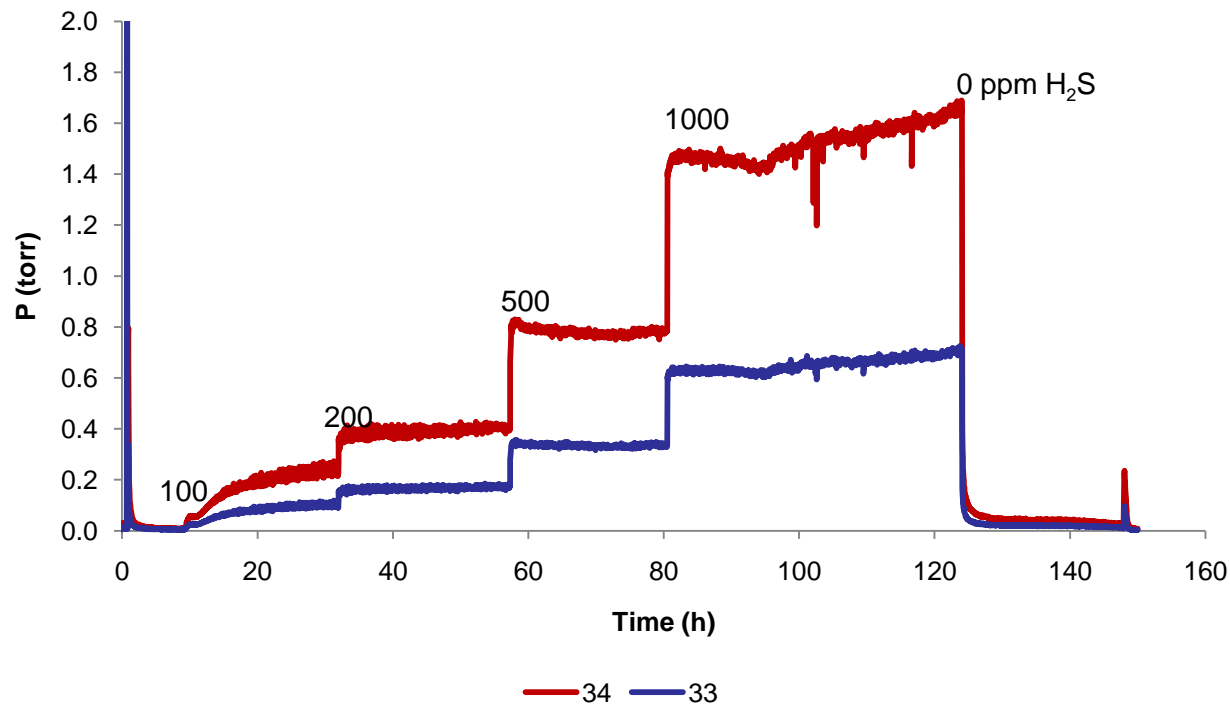
Surface IR Emission Variation under different test conditions

- Analogous to the performance degradation history surface temperature remained stable initially and then increased with the polarization as the cell degraded.
- The button cell exposed to 10 ppm  $\text{PH}_3$  in  $\text{H}_2/3 \text{ vol.}\% \text{H}_2\text{O}$  showed higher surface temperature, which may be attributed to its more severe secondary phase formation and cell electrochemical degradation.
- These results also support model validation efforts.



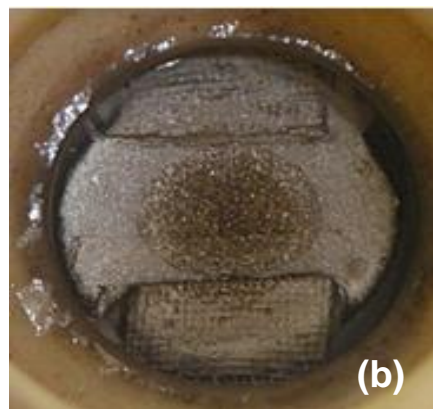
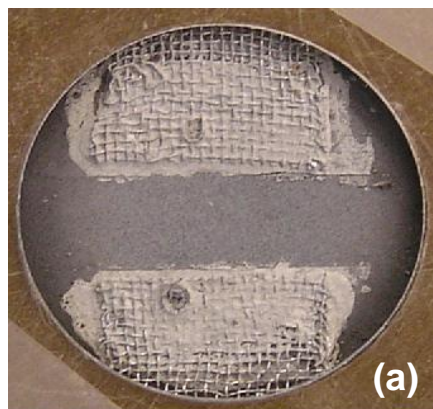
# In-Situ Concentration Measurements

- Monitored inlet and exhaust gas stream with the mass spectrometer.
- Can track concentration changes in  $\text{H}_2\text{S}$  at the 10 – 1000 ppm level.
- Initial slow rise at low concentrations indicates adsorption of  $\text{H}_2\text{S}$  in the system.



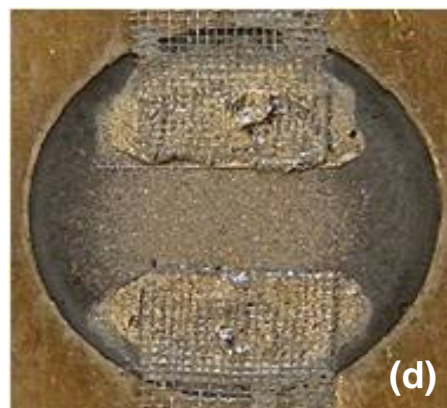
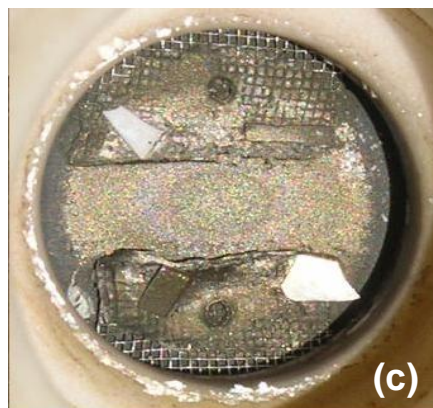
*Mass 34 ( $\text{H}_2\text{S}$ ) and mass 33 ( $\text{HS}$ ) track gas concentrations.*

# Poisoning effect of 10 ppm PH<sub>3</sub> in syngas fuel on Ni-YSZ anode

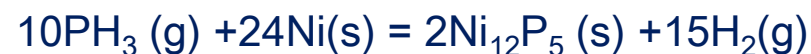


Post-mortem (a) clean syngas; PH<sub>3</sub> poisoned cell anodes at (b) 750°C (c) 800°C and (d) 850°C.

The visible anode diameter is 2 cm. Ni phosphide was produced on the anode surface.

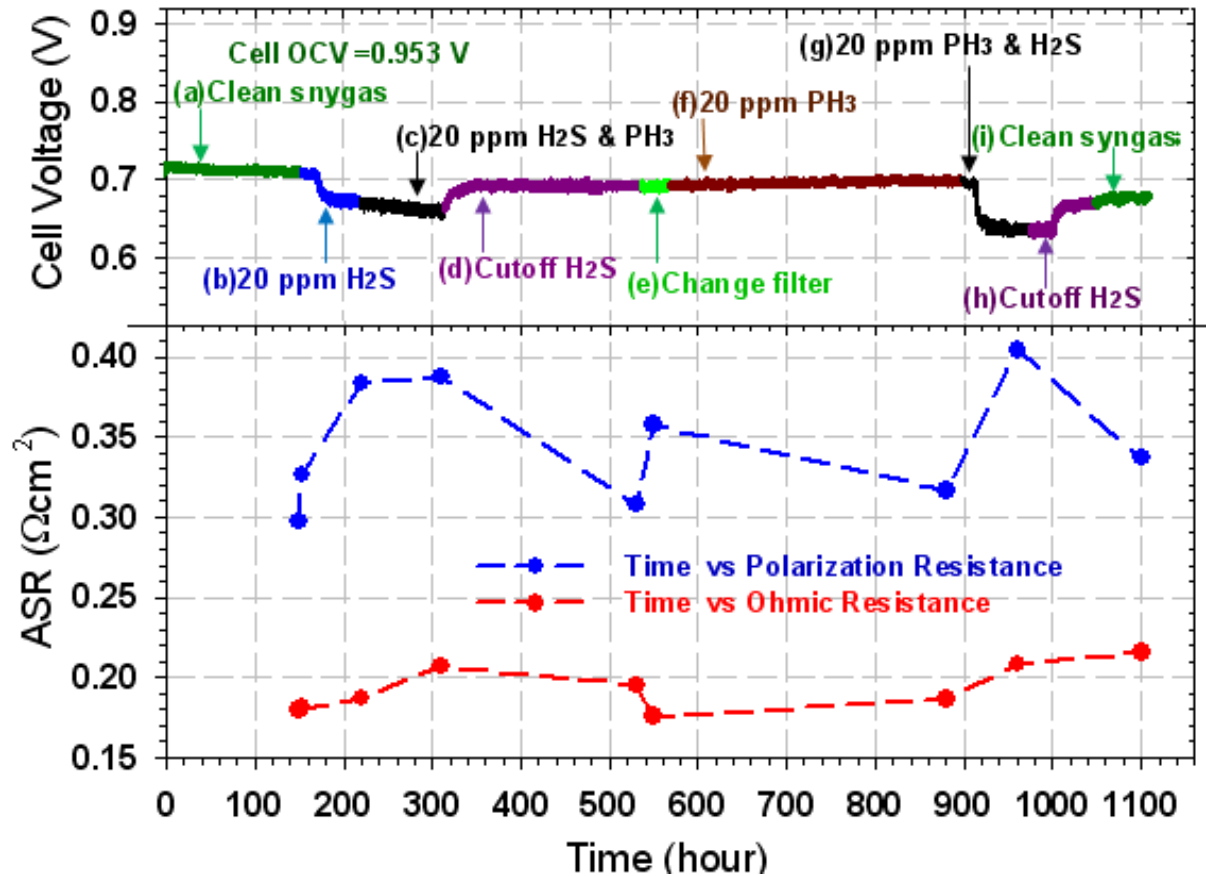


$$\Delta G(1073 \text{ K}) = - 495.07 \text{ kJ/mol}$$



*These experiments indicate that a **nickel-based filter** in front of the cell anode could reduce the PH<sub>3</sub> concentration on the Ni-YSZ anode surface and postpone its degradation.*

# Ni and Ni/Fe Based Pre-filter for both $\text{H}_2\text{S}$ and $\text{PH}_3$



Performance of Ni-YSZ anode supported cell and its area specific resistances (ASR) in syngas with  $\text{PH}_3$  and  $\text{H}_2\text{S}$  impurities. Current load =  $0.5 \text{ A/cm}^2$

1) Does  $\text{H}_2\text{S}$  poison the  $\text{PH}_3$  filter?

Answer: No!

2) Does  $\text{H}_2\text{S}$  poison the cell with the  $\text{PH}_3$  filter?

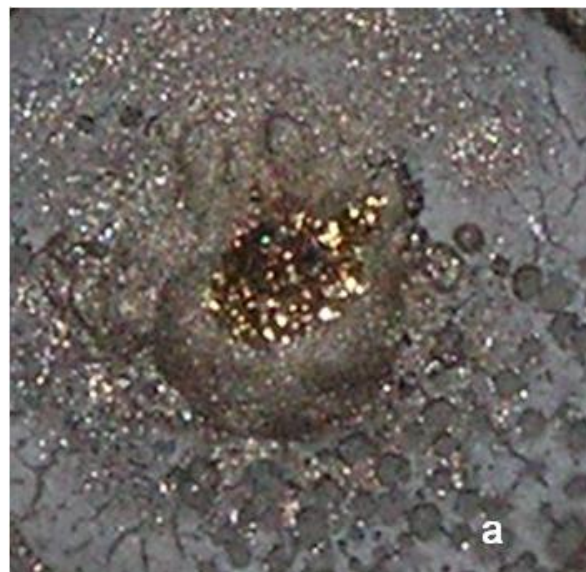
Answer: Yes!

3) *Solution:*

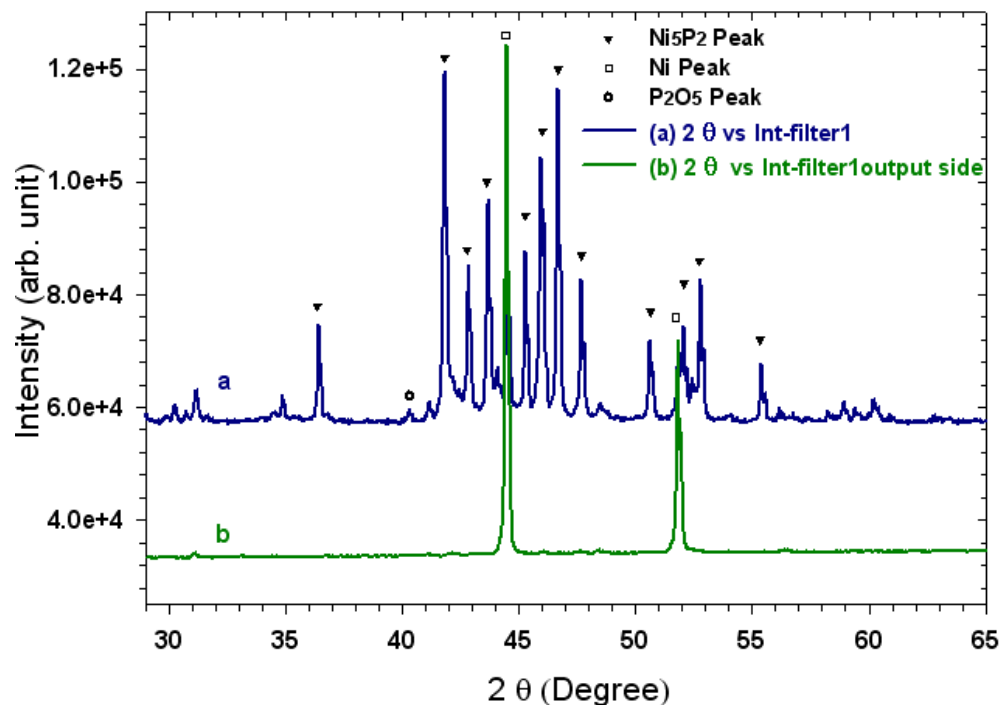
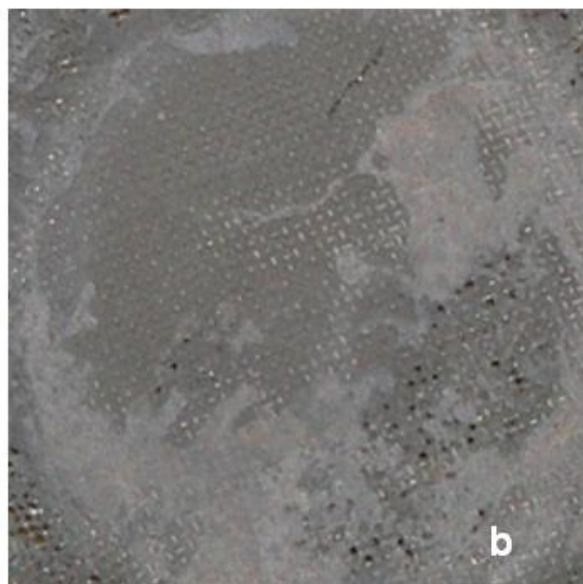
*Develop an  $\text{H}_2\text{S}$  tolerant anode.*

4) *The  $\text{PH}_3$  filter is also expected to remove As and Sb impurities which have the same chemistry as P.*

# Characterization of $\text{PH}_3$ Poisoned Ni Based Pre-filter



(a) A photograph of the front face of the filter which was exposed to syngas with 10 ppm  $\text{PH}_3$  for 200 h and (b) the backside of the same filter.



XRD spectra of the  $\text{PH}_3$  poisoned filter  
(a) exposed surface and (b) backside.

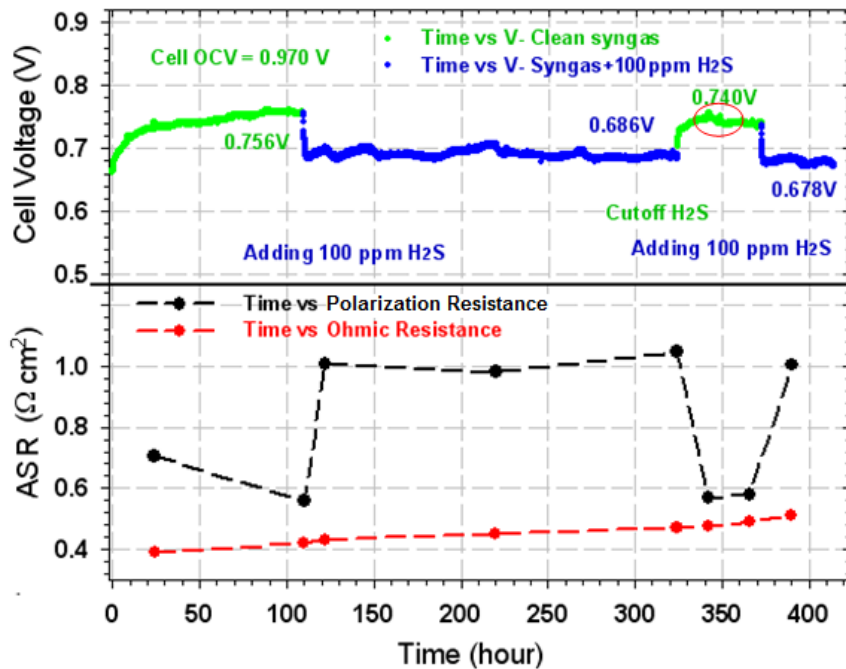
# Sulfur and Tolerant Anodes

- Four strategies were explored for sulfur tolerant anodes
  - Ni-GDC anodes
  - SMM-GDC anodes
  - LDC impregnated Ni-YSZ anodes
  - LaO impregnated Ni-YSZ anodes

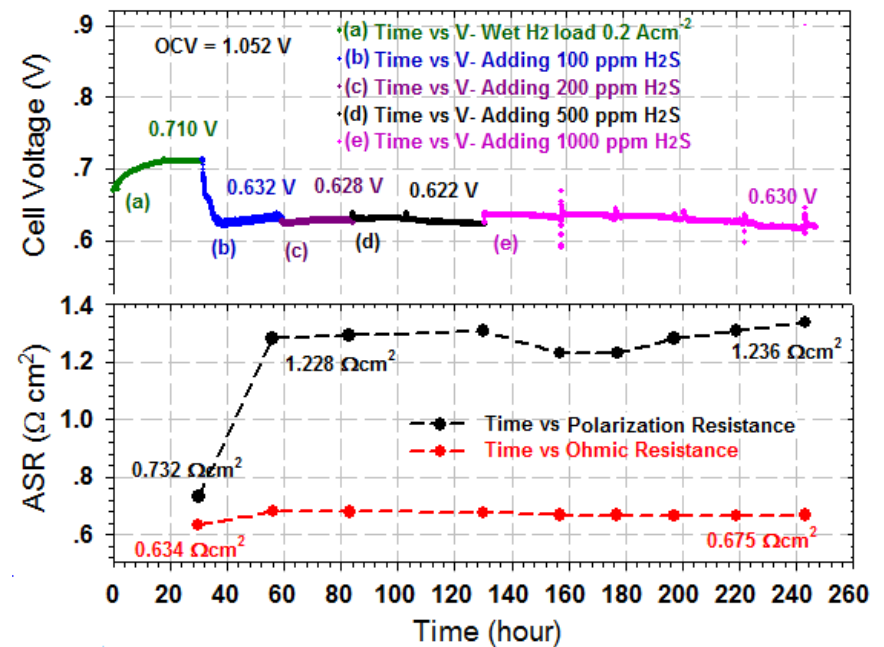


# Sulfur tolerant Ni-GDC anode with a GDC barrier layer-1

*Ni-GDC anodes showed tolerance to up to 1000 ppm H<sub>2</sub>S for over 200 hours.*

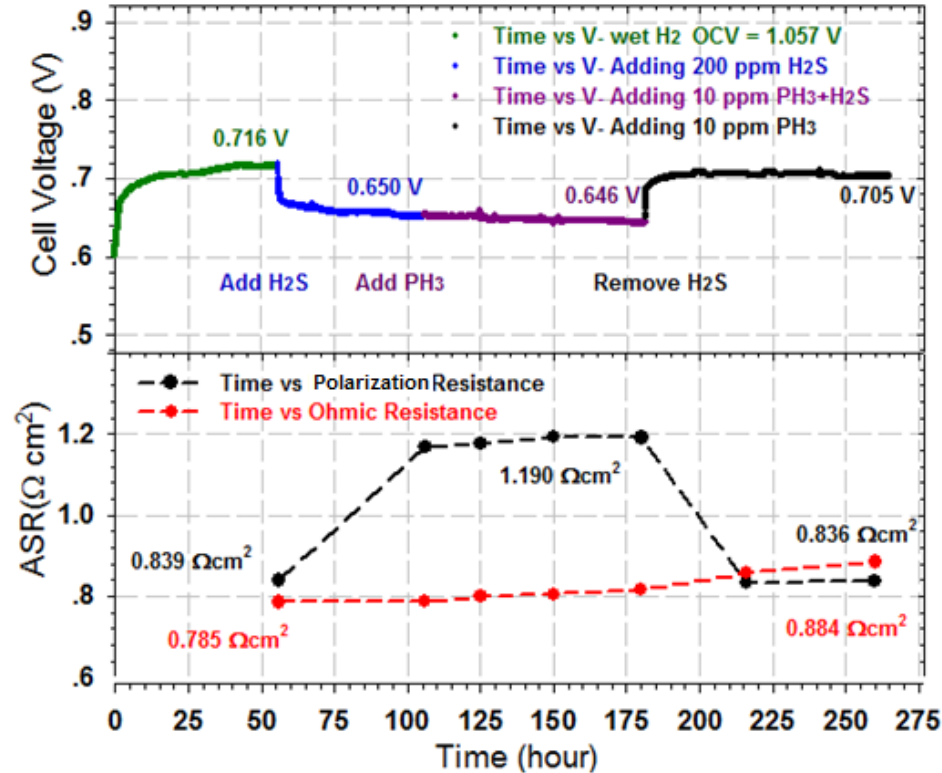


Performance of cell with Ni-GDC and GDC-10 barrier and ASR in clean syngas and syngas with 100 ppm H<sub>2</sub>S.



Performance of cell with Ni-GDC and GDC-20 barrier and its ASR in H<sub>2</sub>+3% H<sub>2</sub>O adding upto 1000 ppm H<sub>2</sub>S.

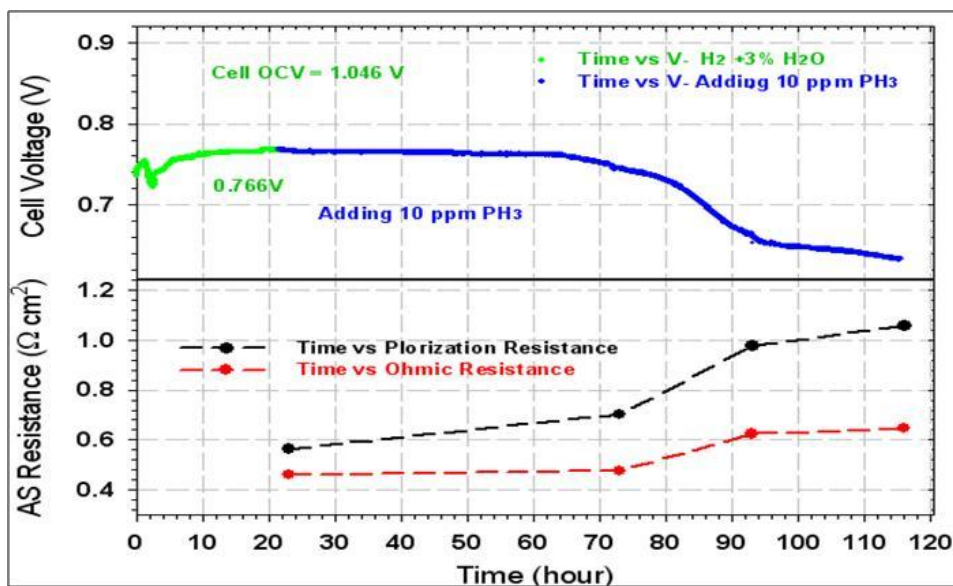
# Combined $\text{H}_2\text{S}$ and $\text{PH}_3$ tolerance test



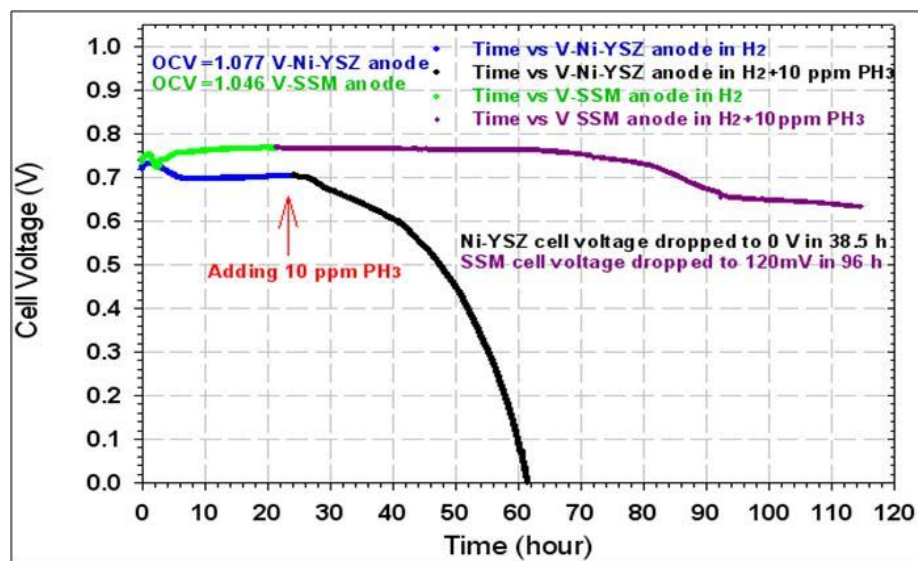
Performance and ASR of the Ni-GDC anode with a GDC barrier:

*Filter  $\text{H}_2\text{S}$  (200 ppm) and  $\text{PH}_3$  (10 ppm) in wet  $\text{H}_2$ . The filter prevented  $\text{PH}_3$  attack and the anode resisted  $\text{H}_2\text{S}$  poisoning.*

# $\text{Sr}_2\text{MgMoO}_{6-\delta}/\text{GDC}$ Anode in $\text{H}_2$ /10 ppm $\text{PH}_3$



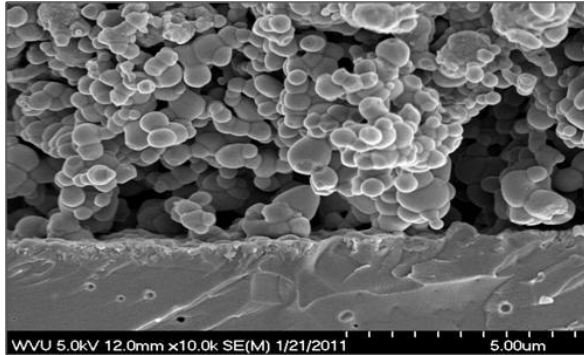
- SMM/GDC anode exhibits better tolerance to  $\text{PH}_3$  than the standard Ni/YSZ anode.
- Decrease in cell performance of almost 46% resulted from this long term exposure.



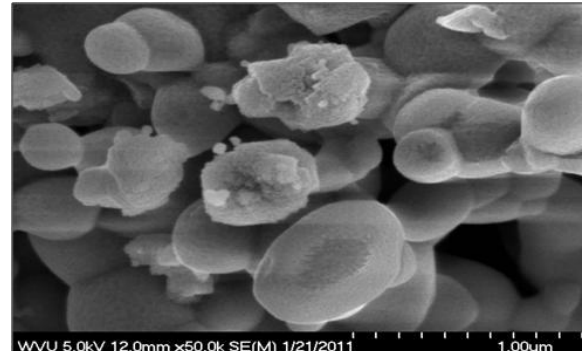
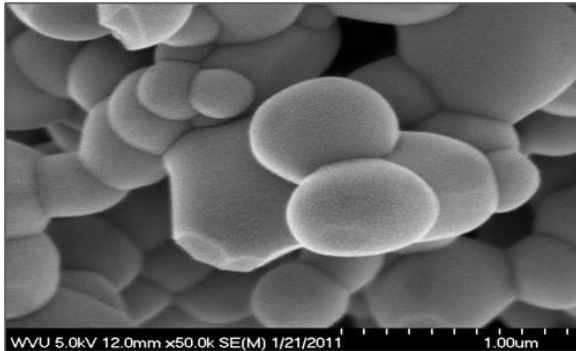
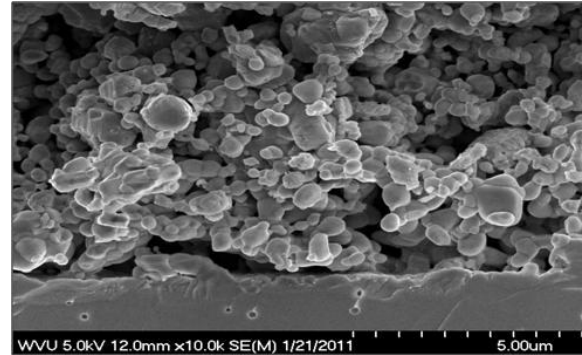
- SMM/GDC composite showed initial tolerance of 10 ppm  $\text{PH}_3$  for upwards of 50 hours before a decrease in potential is observed.

# Post-Mortem Analysis of $\text{Sr}_2\text{MgMoO}_{6-\delta}/\text{GDC}$ Anode-1

$\text{H}_2$

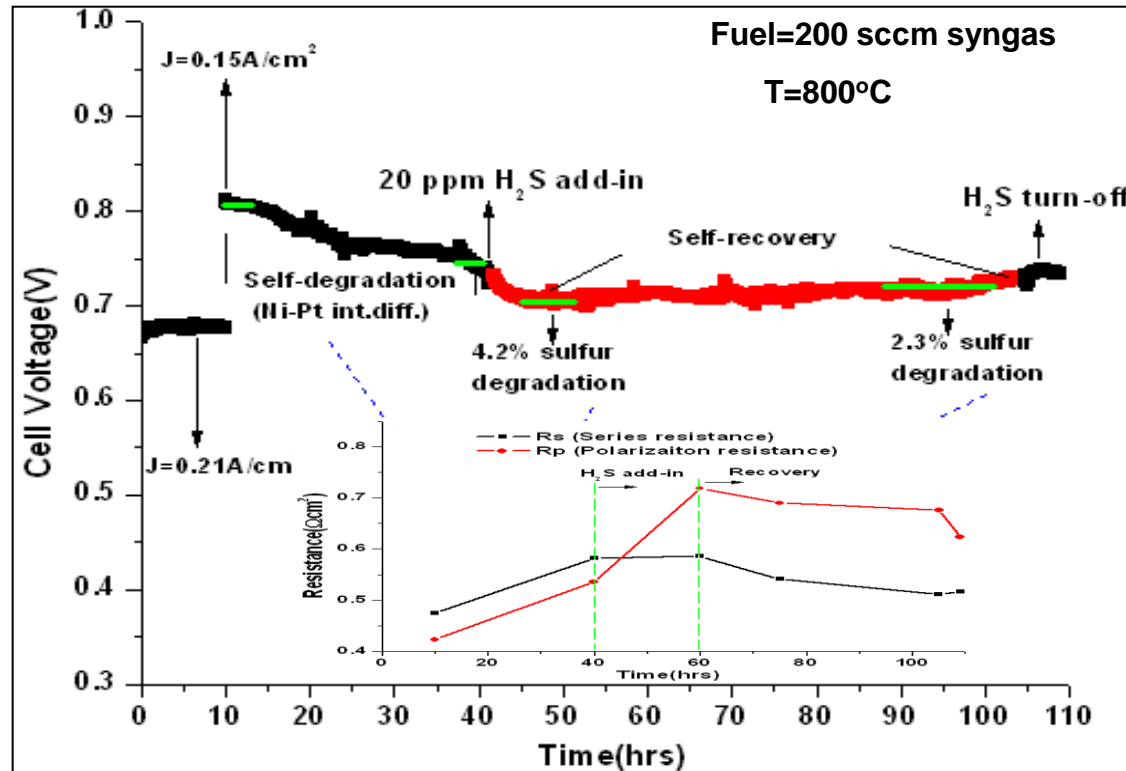


$\text{H}_2$  w/ 10 ppm  $\text{PH}_3$



- *Changes to the microstructure before and after operation in  $\text{PH}_3$  are minimal.*
- *Neither Densification of the electrode nor reaction of phosphorus with the anode or electrolyte constituents are apparent.*
- *The initial test in syngas shows stability for 20 hours which is promising for future studies.*

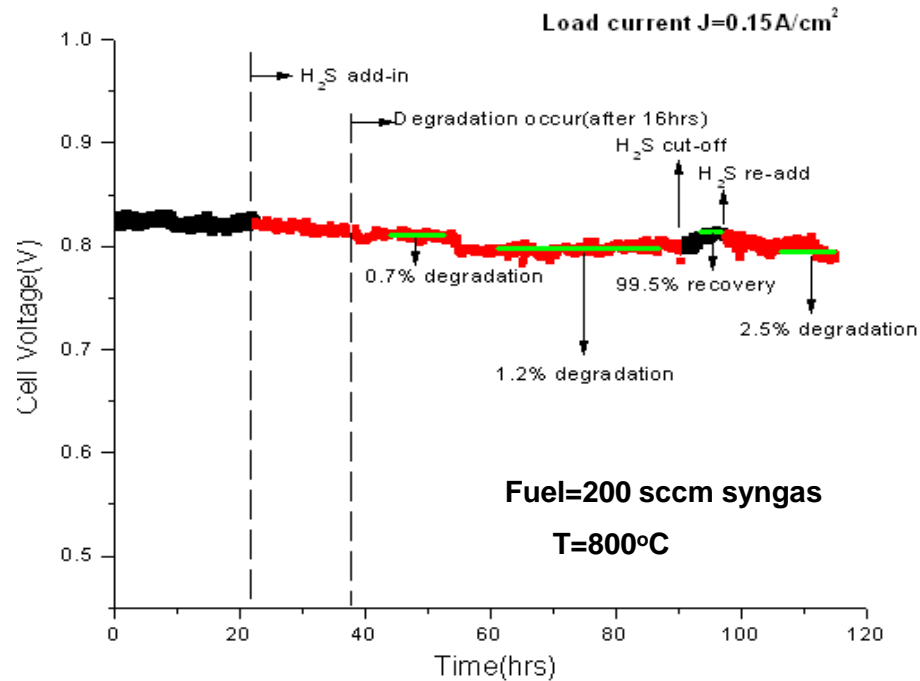
# Sulfur tolerance of LDC impregnated Ni-YSZ anode



- LDC exhibited resistance to  $\text{H}_2\text{S}$  for over 50 hours. The material shows promise for a sulfur tolerant anode

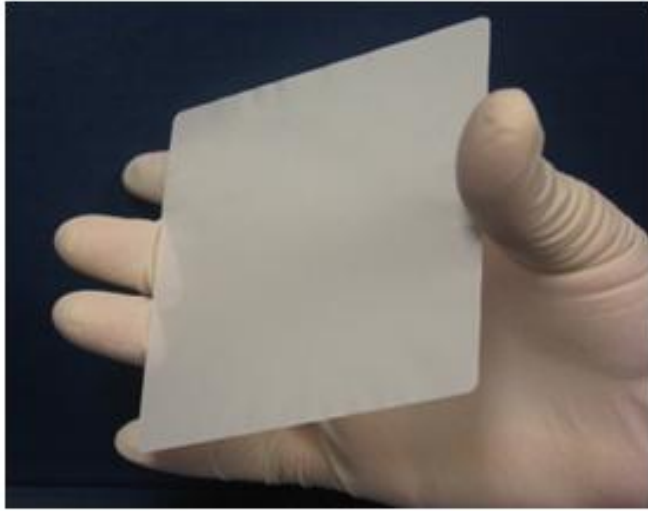


# Improve of sulfur tolerance with La-doped Ni-YSZ anode



*Pure  $\text{La}_2\text{O}_3$ -impregnated Ni anode showed less initial potential drop and slower degradation rate than LDC-impregnated anode*

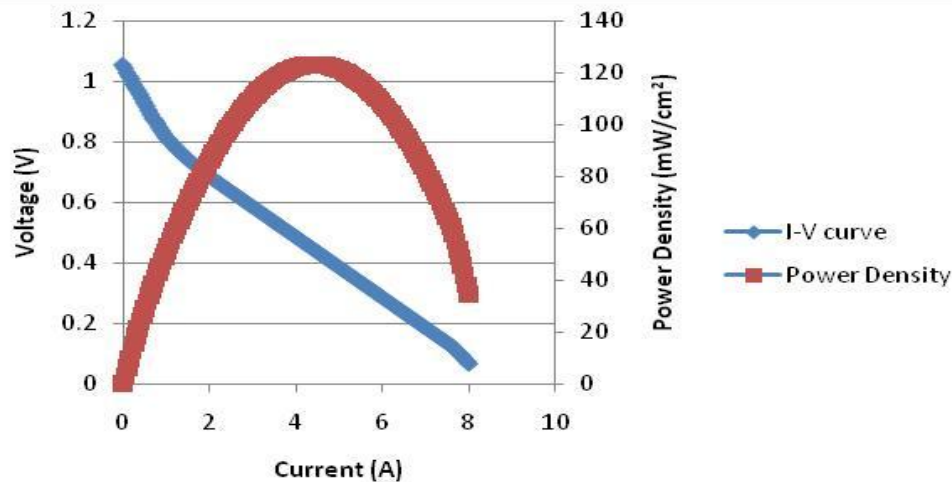
# Testing Planar SOFCs in $H_2S$ and $PH_3$ Laden Fuels



**100 cm<sup>2</sup> electrolyte-supported SOFC fabricated at WVU**



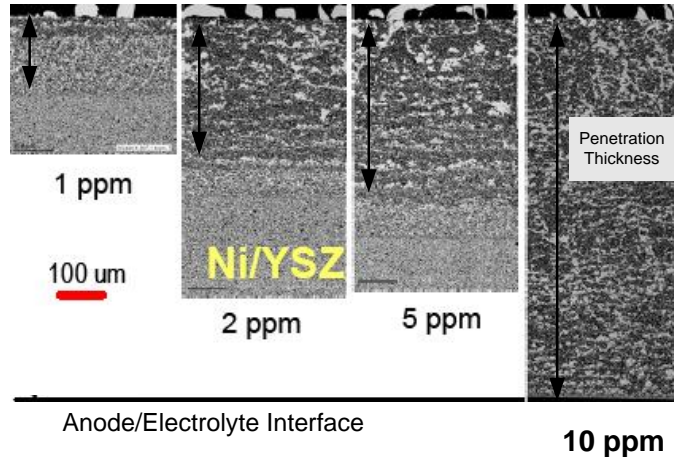
**Ceramic and Haynes 242 Compressive Manifolds for 100 cm<sup>2</sup> Testing**



**Initial test in  $H_2$  fuel at 750 C of a 16 cm<sup>2</sup> planar electrolyte-supported SOFCs fabricated at WVU**

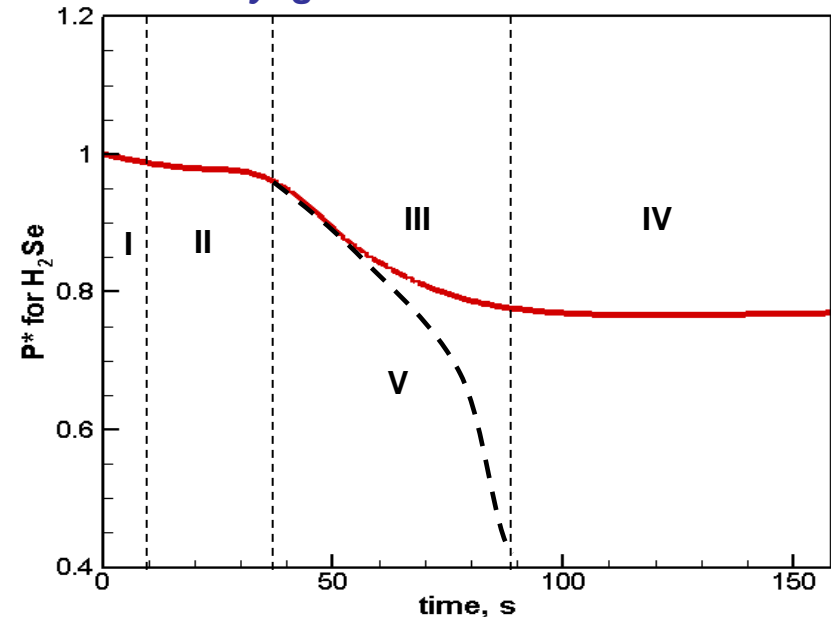
# Contaminant Degradation Model

Penetration thickness after 990 h of exposure to  $PH_3$  in coal syngas (PNNL)



Deposition starts near F/A interface and slowly moves toward the A/E interface

Typical degradation curve for 1 ppm  $H_2Se$  in coal syngas at 700 °C



Four stages of degradation:

- I → Initial performance drop
- II → Intermediate slow degradation
- III → Second fast degradation
- IV → Final slow degradation
- V → Structural failure and/or rapid degradation

Degradation stages correspond to extent of impurity Penetration !



## ★ 1-D Transport Equation for $\theta$ Propagation

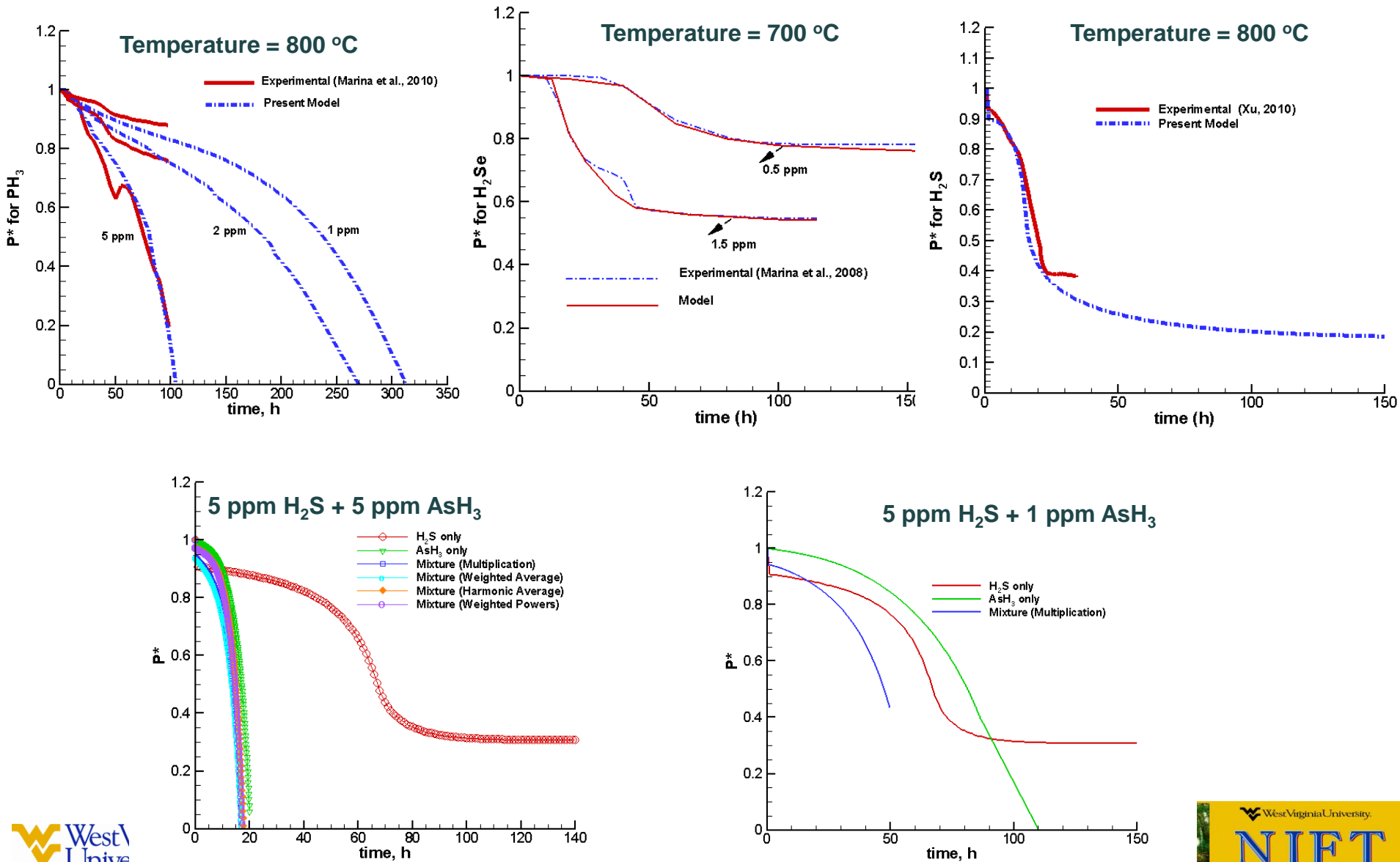
$$\frac{\partial \theta_i}{\partial t} = D_\theta \frac{\partial^2 \theta_i}{\partial z^2} + \omega_{\theta_i}$$

$\theta_i$  : progress variable

$D_\theta$  : transport coefficient

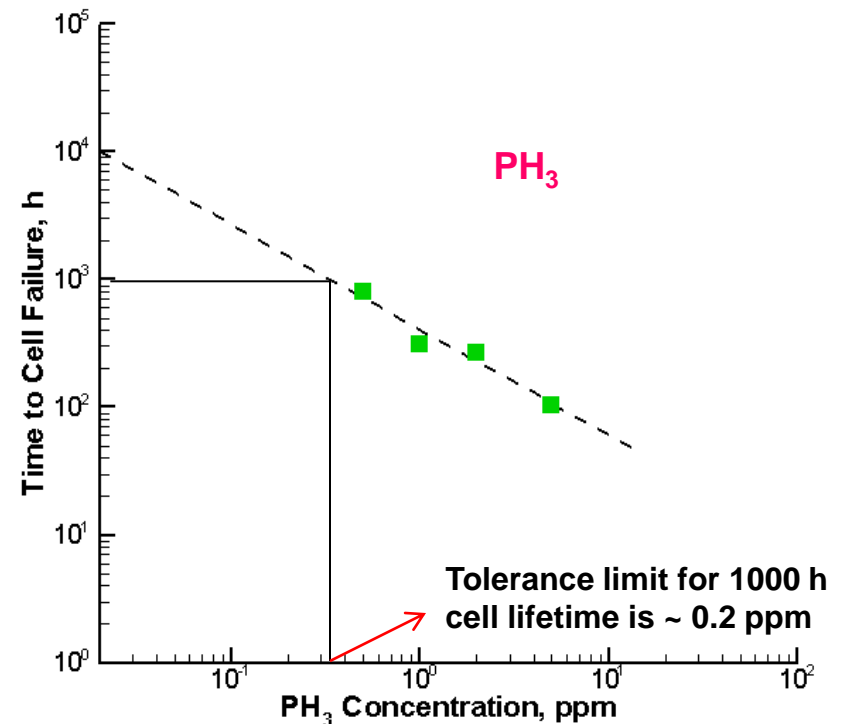
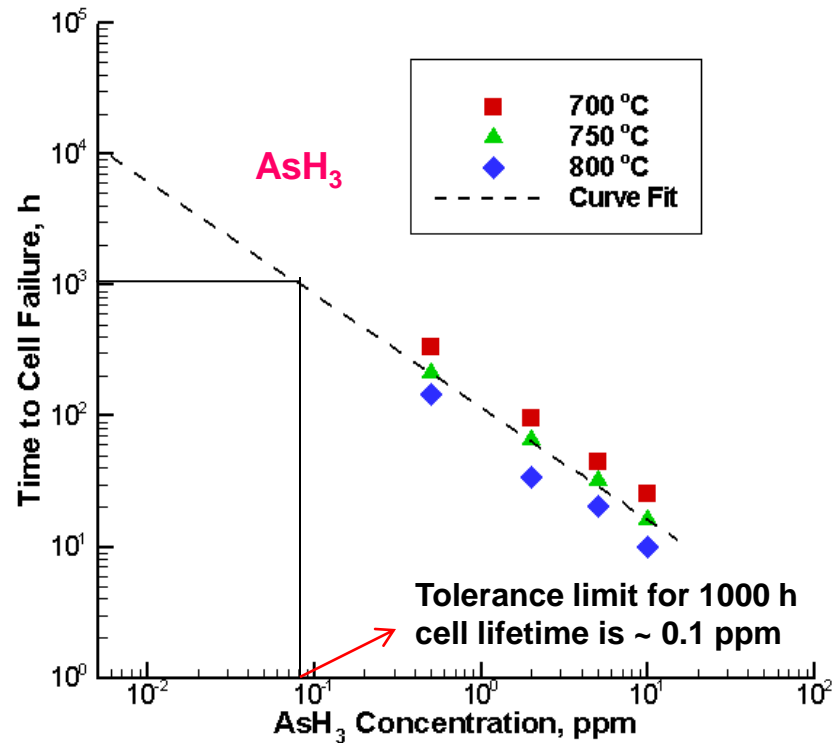
$\omega_{\theta_i}$  : source terms

# Model Predictions



# Modeling: Cell Lifetime and Tolerance Limits

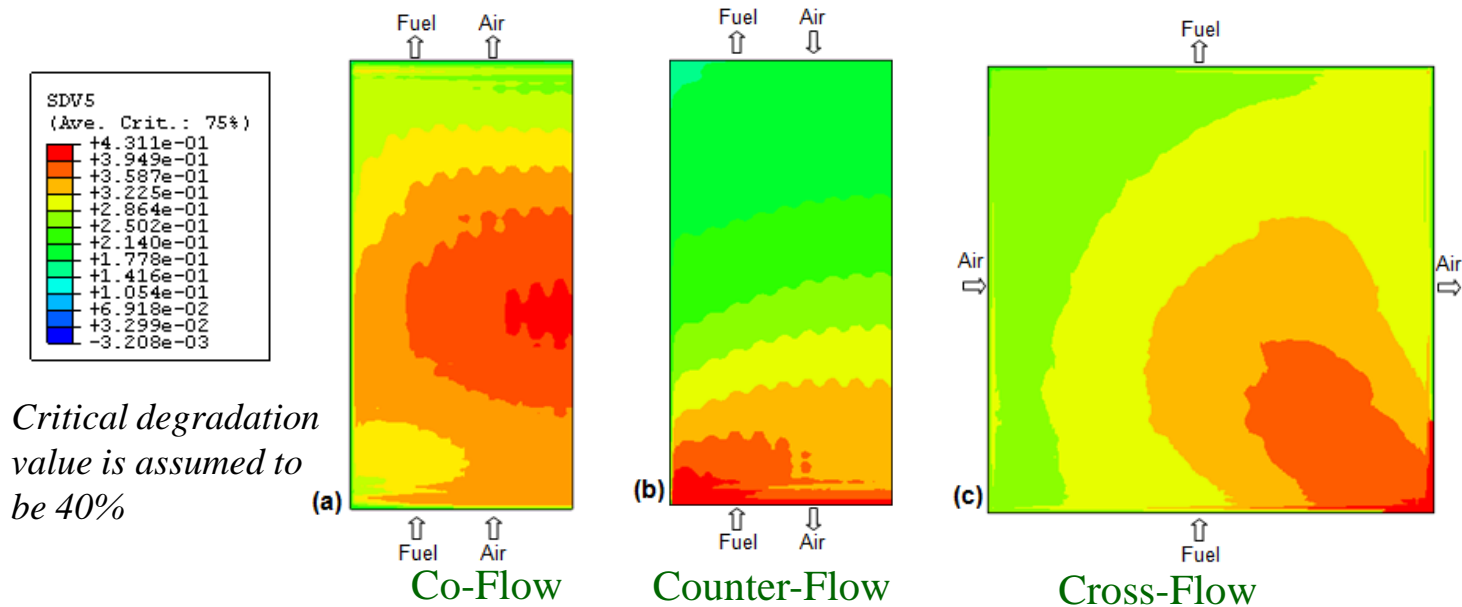
Cell failure is taken as when performance reduces by 60%





# Structural Degradation: Effect of Impurities

## Planar-SOFC Anode Structure Failure Locations



Critical degradation value is assumed to be 40%

Anode structural degradation in anode under 5ppm of  $\text{PH}_3$ , inlet temp.  $800^\circ\text{C}$  and 20 A (a) 19,917 h (b) 16,310 h (c) 1,8450 h

*Co-flow arrangement yields longest anode structural life prediction as compared to the other two configurations under similar operating conditions*

*At low impurity concentrations structural degradation may be more important than electrochemical degradation*

# Conclusions – 1

- TEM characterization revealed new nano-scale phenomena in the SOFC anodes exposed to impurities.
- Determined that 10 ppm  $\text{PH}_3$  in wet  $\text{H}_2$  fuel leads to faster degradation when compared to dry fuel condition.
- Measured surface temperature of button cells under different operating conditions using new in-situ technique.
- A mass spectrometer was used to monitor in-situ forms of impurity species and their concentrations, before and after passing through the furnace.
- Ni and Fe based filters are shown to remove  $\text{PH}_3$  impurity effectively from syngas.
- The mechanism responsible for sulfur tolerance of LDC impregnated anodes was studied and Ni/GDC anode was shown to be a suitable material for syngas contaminated with  $\text{H}_2\text{S}$ .

# Conclusions – 2

- New SMM/GDC anodes were prepared in-house and are shown to be tolerant to  $\text{PH}_3$  in syngas.
- Numerical simulations showed that the co-flow arrangement in a planar SOFC resulted in longest structural life compared to counter-flow and cross-flow arrangements.
- Model results revealed that, at low  $\text{PH}_3$  levels, the anode structural degradation may be as significant as electrochemical degradation.
- A new phenomenological degradation model was developed and used to study cell lifetimes and tolerance limits for impurities.
- The synergistic effects of multiple impurities were simulated including  $\text{H}_2\text{S}$ ,  $\text{AsH}_3$  and  $\text{PH}_3$ .
- The in-house SOFC code was modified to simulate button cells operating on biogas.

# Thank you

# Recent Publications

1. H. Guo, G. Iqbal, and B. S. Kang (2011) "Effects of PH<sub>3</sub> Contaminant on SOFC Performance and Related Anode Surface Temperature Measurements," International Journal of Applied Ceramic Technology, v. 8, p. 68-73.
2. D. Ding, M. Gong, C. Xu, N. Baxter, Y. Li, J. Zondlo, K. Gerdes, X. Liu (2011) "Electrochemical Characteristics of Samaria-Doped Ceria Infiltrated Strontium-Doped LaMnO<sub>3</sub> Cathodes with Varied Thickness for Yttria-Stabilized Zirconia Electrolytes" Journal of Power Sources, v. 196, 2551-2557.
3. C. Xu, J. Zondlo, M. Gong, F. Elizalde-Blancas, X. Liu, I.B. Celik (2010) "Tolerance Tests of H<sub>2</sub>S-laden Biogas Fuel on Solid Oxide Fuel Cells" Journal of Power Sources v.195, p. 4583-4592.
4. C. Xu, J. Zondlo, M. Gong, X.Liu, (2011) "Effects of PH<sub>3</sub> poisoning on a Ni-YSZ anode-supported SOFC under various operation conditions", Journal of Power Sources, v. 196, p. 116-125.
5. Fatma N. Cayan, Suryanarayana R. Pakalapati, Ismail Celik, Chunchuan Xu and John Zondlo (2011) "A Degradation Model for Solid Oxide Fuel Cell Anodes due to Impurities in Coal Syngas: Part I. Theory and Validation", submitted to Fuel Cells.
6. Chunchuan Xu, John Zondlo, Edward Sabolsky, "A prefilter for mitigating PH<sub>3</sub> contamination of a Ni-YSZ anode" Journal of Power Sources, accepted for publication.
7. Huang Guo, Gulfam Iqbal, and Bruce S. Kang, "Investigation of Secondary Phases Formation due to PH<sub>3</sub> Interaction with SOFC Anode," American Society Ceramics Transaction, accepted for publication.
8. Gulfam Iqbal, Raju Pakalapati, Huang Guo, Ismail Celik, and Bruce Kang, "PEN Structure Thermal Stress Analysis for Planar-SOFC Configurations," American Society Ceramics Transaction, accepted for publication.
9. Gulfam Iqbal, and B.S. Kang, "Elastic Brittle Damage Model for Ni-YSZ and Predicted Stress-Strain Relations as a Function of Temperature and Porosity," ASME Journal of Fuel Cell Sciences and Technology, Accepted for publication (2011)
10. F. Elizalde-Blancas, S. R. Pakalapati, F. N. Cayan, C. Xu, I. B. Celik, H. O. Finklea, J. W. Zondlo, "A Computational Model for SOFC Running on Syngas" submitted to Journal of Power Sources.
11. Y. Chen, S. Chen, H. Finklea, X. Song, G. Hackett, K. Gerdes, "Microstructure and chemistry evolution of triple phase boundaries in the anode of solid oxide fuel cells", submitted to Solid State Ionic.



# Supplementary Slides

# Performance Degradation due to $\text{PH}_3$

## Ni-YSZ anode after being exposed to $\text{PH}_3$ in various conditions

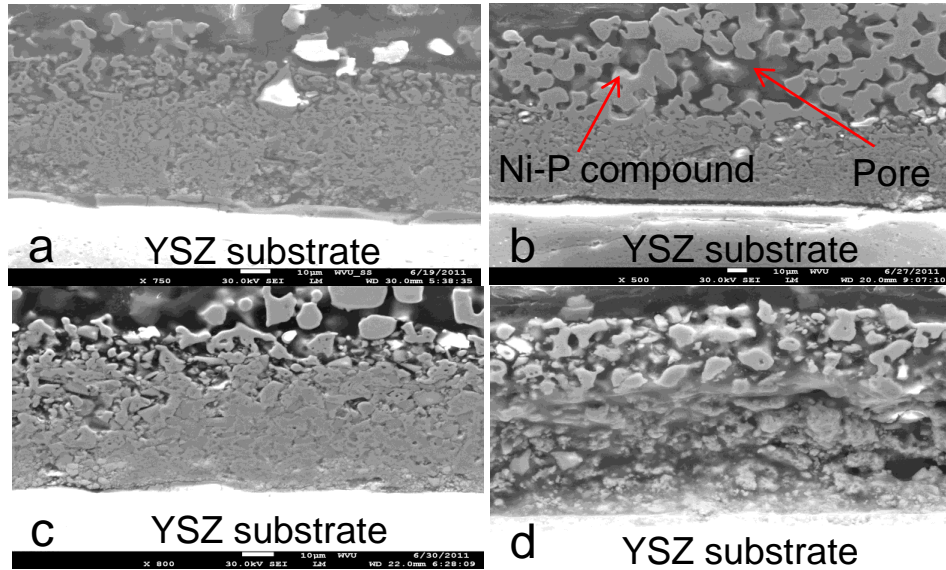


Fig.5. SEM images of the Ni-YSZ working electrode cross section

- a. Clean syngas,
- b. 5 ppm  $\text{PH}_3$  for 24 hrs with current density of  $0.25\text{A}/\text{cm}^2$ ,
- c. 5 ppm  $\text{PH}_3$  for 24 hrs without current loading,
- d. 5 ppm  $\text{PH}_3$  for 24 hrs dry syngas

- The half-cell operated with current loading shows (Fig.5b&c) more aggregates to big particles compared to cell w/o current.
- The anode operated with 5 ppm  $\text{PH}_3$  in dry coal syngas exhibits more severe agglomeration.

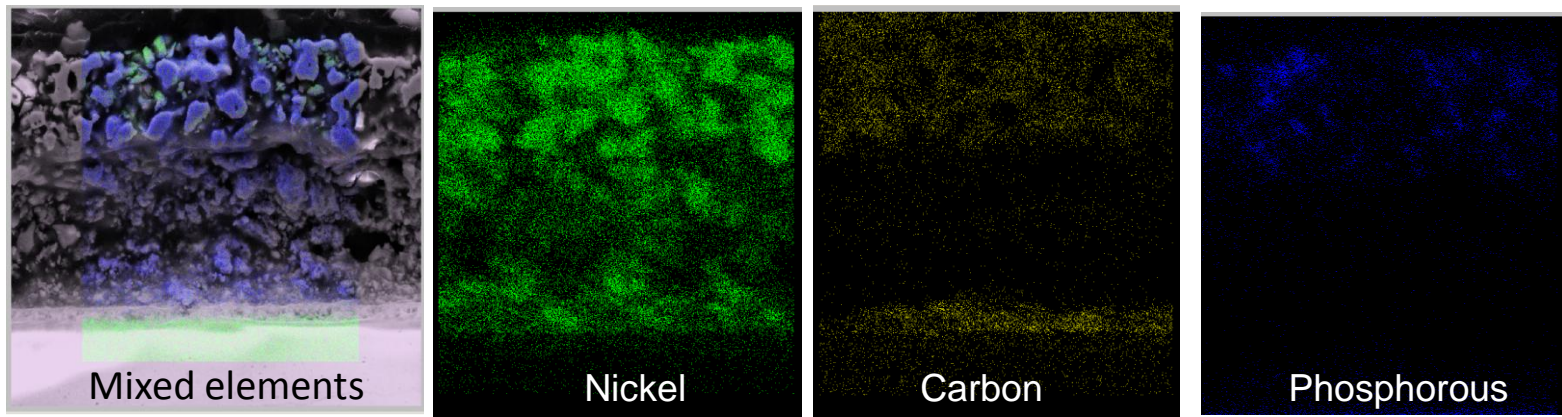
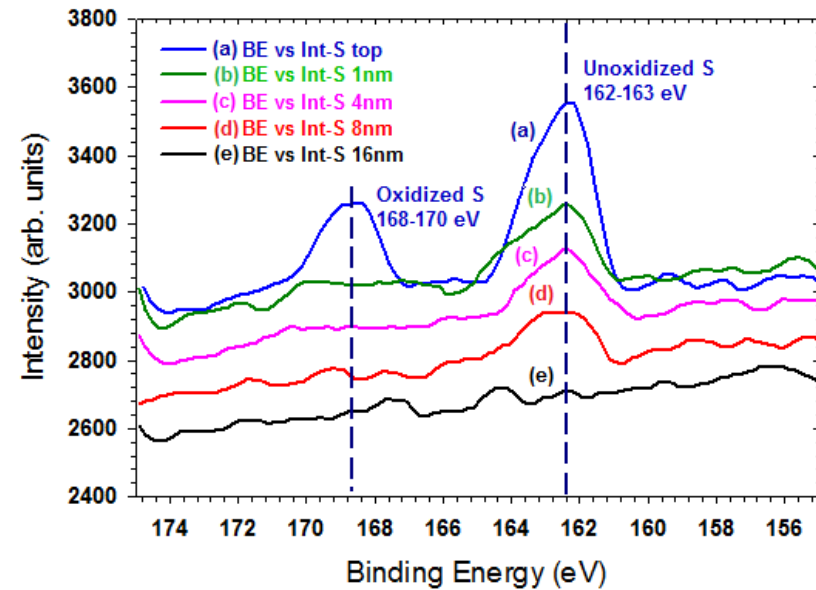


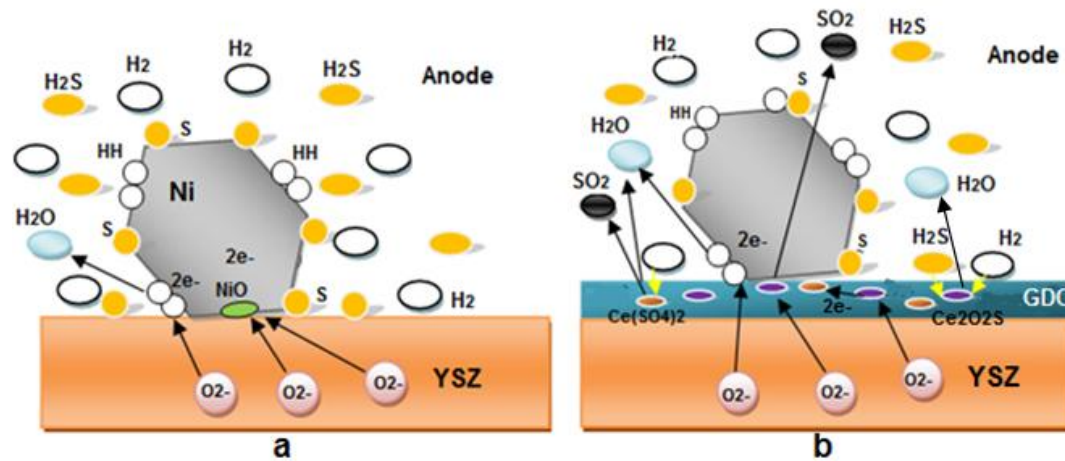
Fig.5. EDS mapping on the cross section of the Ni/YSZ anode after being exposed to 5 ppm  $\text{PH}_3$  for 24 hrs without steam

# Sulfur tolerant Ni-GDC anode with a GDC barrier layer-2



The depth profile of XPS spectra on the Ni surface of the  $\text{H}_2\text{S}$  poisoned cell.

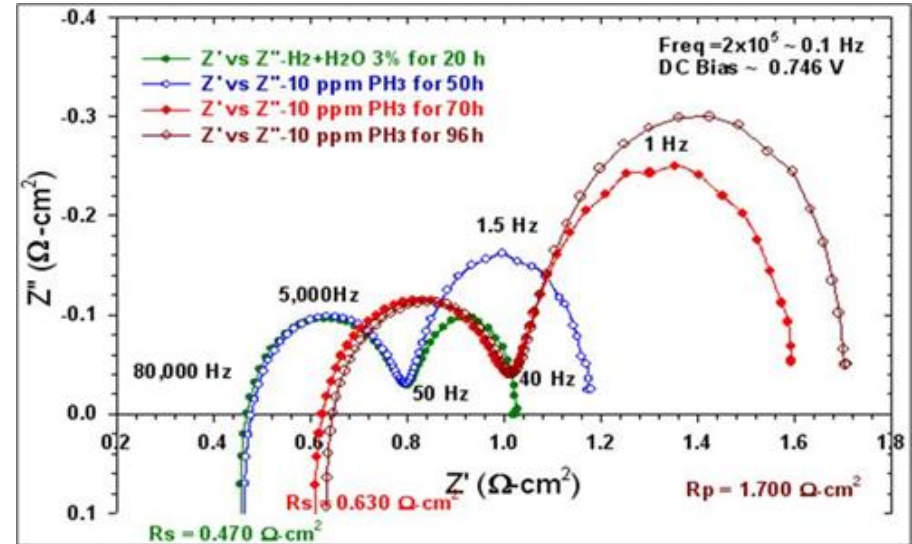
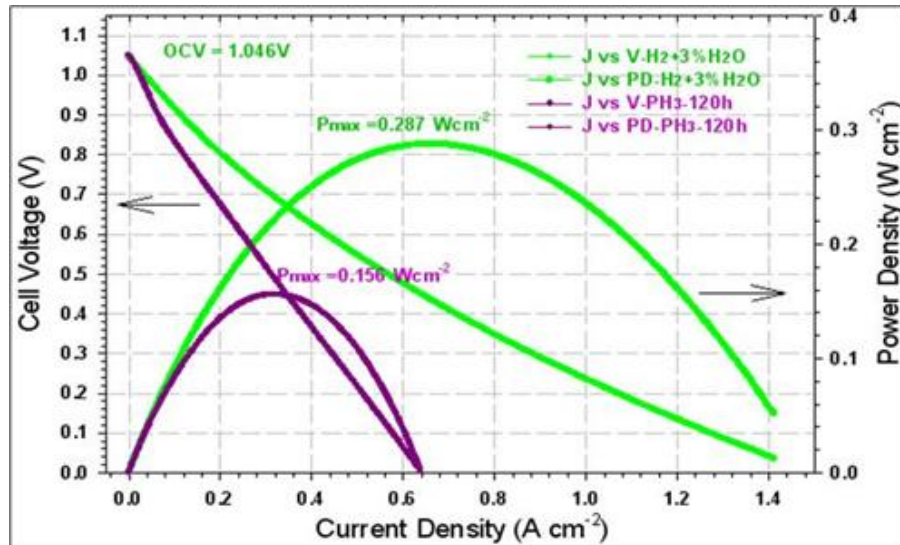
*The oxidized S peak at 169-170 eV is only significant on the top Ni surface. The unoxidized S peak is detectable at 8 nm depth from the Ni surface.*



A conceptualization of the cell anode and electrolyte active interface

- (a) *The Ni is slowly oxidized by  $\text{O}^{2-}$  at the active interface and*
- (b) *The GDC layer is suppressing the  $\text{NiO}$  formation at the active interface.*

# $\text{Sr}_2\text{MgMoO}_{6-\delta}/\text{GDC}$ Anode in $\text{H}_2$ /10 ppm $\text{PH}_3$

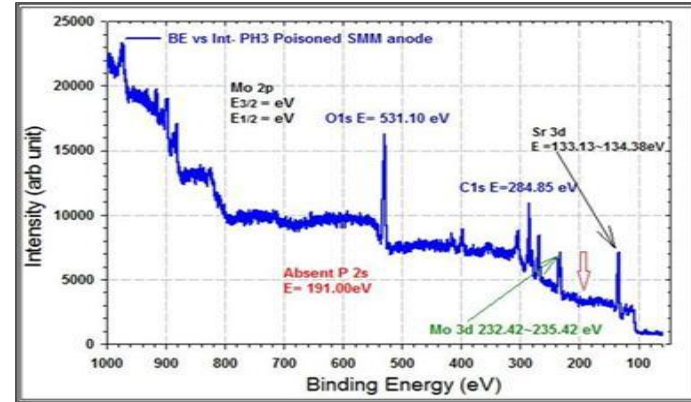
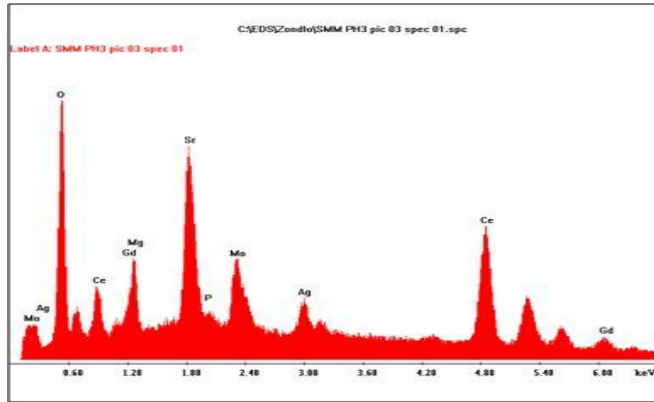


- Results show promise for development of a  $\text{H}_2\text{S}$  and  $\text{PH}_3$  tolerant anode.
- Better understanding of interaction of  $\text{H}_2/\text{PH}_3$  fuel at various loadings is required for further development.

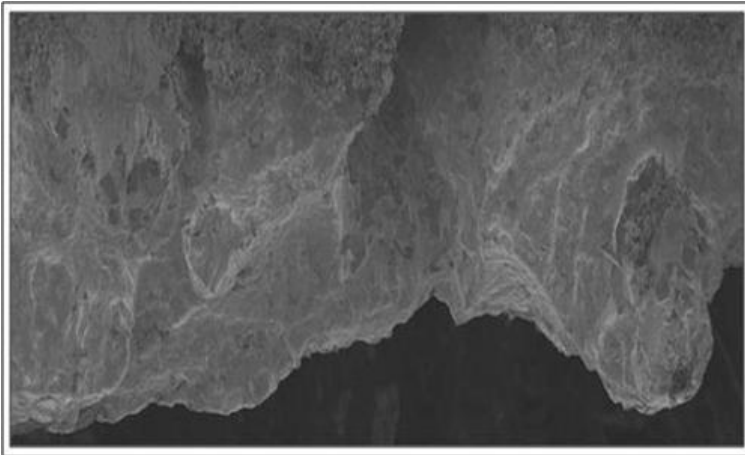
- No change in Ohmic resistance after 50 hours.
- Ohmic and polarization resistance increases after 100 hours.
- Failure of Pt interconnection is one key issue.



# Post-Mortem Analysis of $\text{Sr}_2\text{MgMoO}_{6-\delta}/\text{GDC}$ Anode-2



- EDS analysis detected a slight presence of phosphorus at the interface.



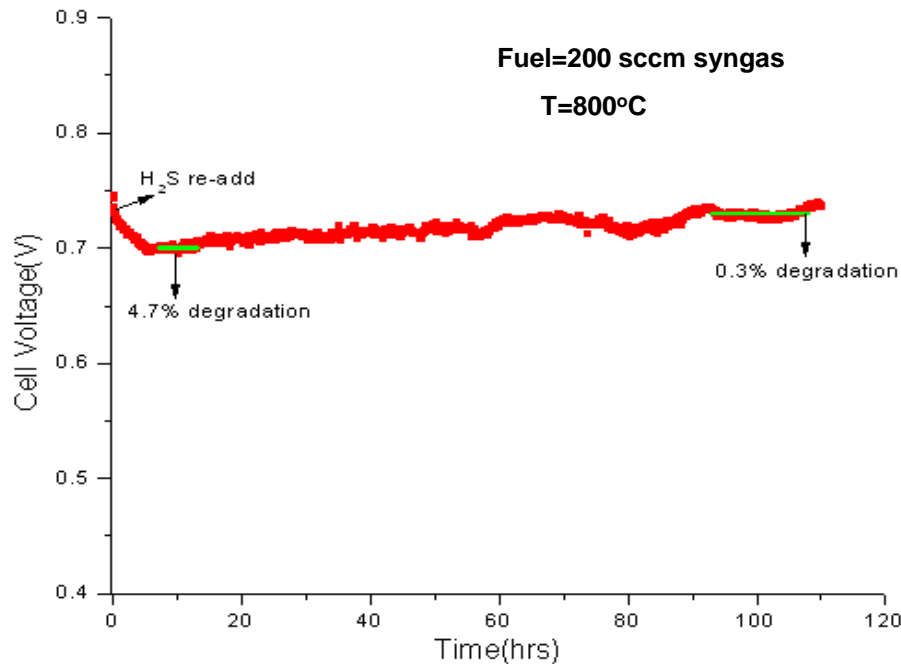
SEM image of the Pt paste

- Pt densification may be the cause for increase in cell polarization.

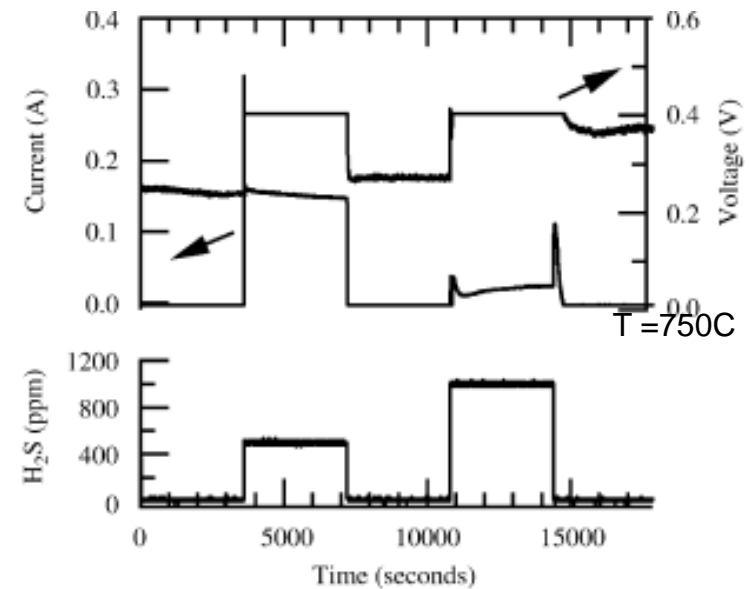


# Recovery of LDC impregnated Ni-YSZ anode

Verification of recovery mechanism with Ni-GDC anode and further sulfur exposure



Our results with LDC impregnation

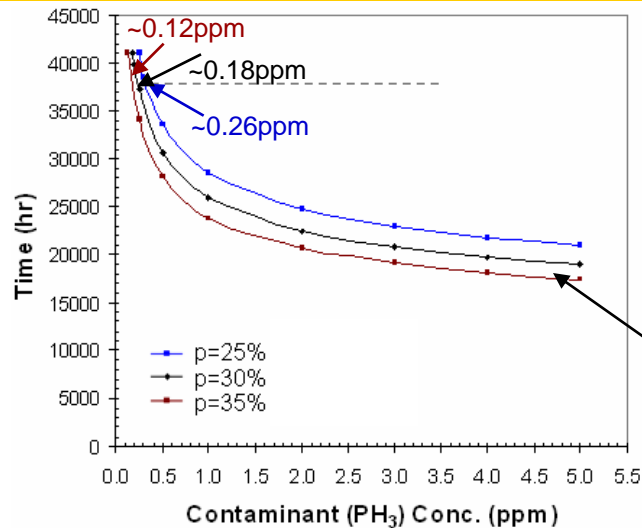


A.Lussier, S.Soffier, J.Dvorak, Y.Idzerda. Int.J.Hydr.Energy, 2008

Literature data with GDC impregnation

# Structural Degradation: Effect of Impurities

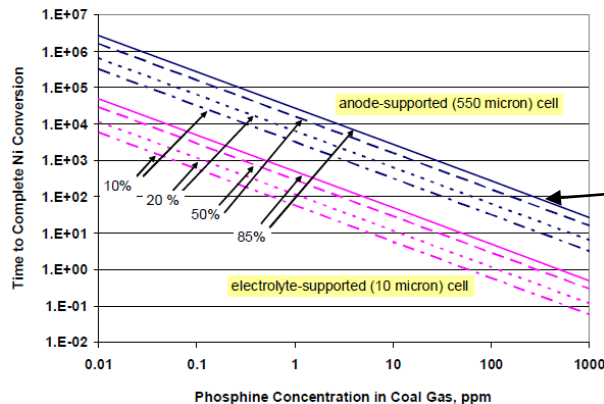
## Anode Structural Life: Electrochemical vs. Structural Degradation



➤ Anode structural life increases exponentially with the decrease in the contaminant concentration

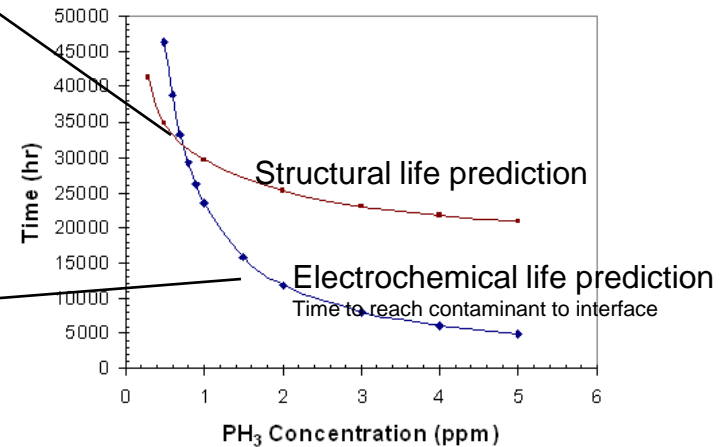
➤ Under lower concentration of contaminant, the anode structural degradation may be significant as compared to electrochemical degradation

Acceptable limit of  $\text{PH}_3$  contaminant for specified anode structural life



Penetration depth of  $\text{PH}_3$  under different concentration<sup>[1]</sup>

[1] O.A. Marina et al. 9th Annual SECA Workshop, August 2008, Pittsburgh, PA



Comparison of predicted anode structural life and time required the contaminant reached the interface

