



UK/US Collaboration in Energy R&D

Advanced Materials Program

FE Materials Conference 27th May 2010

Progress with Phase 2 Tasks

Pittsburgh, 27 May 2010



Approved Phase 2 Tasks



- Steam Oxidation
- Materials for Advanced Boilers and Oxy-combustion Systems
- Gas Turbine Materials Life Assessment and Non-Destructive Evaluation
- Oxide Dispersion Strengthened Alloys

| 1990 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2000 | 2007 | 2000 | 2009 | 2010 | 2011 | 2012 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 |



Phase 2 Task 1 Steam Oxidation



What is the effect of pressure on the steam oxidation of alloys relevant to fossil-fuelled USC steam power plants?

What is the effect of heat flux on steam oxidation and scale exfoliation on alloys relevant to fossilfuelled USC steam power plants?

What is the effect of specimen geometry on the oxidation kinetics, oxide scale morphology and spallation properties?

Is chromia evaporation a concern in USC steam turbines?

What is the agreed-upon standard laboratory test method for steam oxidation testing, and how can its validity be confirmed?

Can a compendium of oxide microstructures provide useful information with respect to predicting component lifetimes and recognizing corrosion mechanisms?

Can existing alloys be modified to be either castable or less expensive, while maintaining acceptable properties?

Partners

- US NETL, University of Pittsburgh, Carpenter Corporation
- UK NPL, Cranfield, Doosan Power Systems
- Integrated work programme developed
- First results Pittsburgh May 2010



Steam Oxidation Participants and Roles



| | Laborat | Laboratory Test | | | Assessment | Standardicad | Maasuramant | Power |
|-----------|---------------------|----------------------|------------------------------|-----------|---------------------------------------|-----------------------------|----------------------------|------------------------|
| | Ambient Pressure | Elevated Pressure | Alloy or Sample Supply | Modelling | of geometry & heat flux effects | Standardised test method | Measurement uncertainty | Industry Experience |
| NPL | | | | | | | | |
| Cranfield | | | | | | | | |
| Doosan | | | | | | | | |
| RWE | | | | | | | | |
| | | | | | | | | |
| NETL | | | | | | | | |
| Carpenter | | | | | | | | |
| UPitt | | | | | | | | |



Steam Oxidation Deliverables



- Review of the effect of pressure and heat flux on the steam oxidation
- Standard test method for steam oxidation testing
- Modified model of scale exfoliation for component lifetime prediction incorporating heat flux
- Reliable oxidation kinetics for candidate alloys including dependence on pressure, and heat flux
- Report on the inter-comparison exercise
- Database of information generated during the collaboration
- Verification of Cr evaporation model with respect to gas velocity
- Completion of ingot modelling (Mar 2011) and provide cast material samples (Jan 2012)
- Completion of alloy modelling and development of matrix of proposed compositions (Mar 2010), and provide material samples of alloys with best predicted performance and most promising data from initial testing (Jan 2012)

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Phase 2 Task 2 Boiler Corrosion



What is the range of anticipated environments in advanced boiler systems? And how does oxy-fired ash differ from ash from air-fired systems?

What is the agreed-upon standard laboratory test method for boiler corrosion testing, and how can its validity be confirmed?

How can we further develop our understanding of the behavior of current and candidate materials for boilers operating under advanced conditions to become better informed for suitable material selection?

What is the performance of candidate coating systems for superheaters and reheaters in advanced boiler systems?

What is the performance of candidate piping systems in oxy-firing boilers for recycle flue gas?

What is the best way to share test results between collaboration partners?

Partners

- US NETL, University of Pittsburgh, REI, ANL
- UK Doosan Power Systems, Cranfield, NPL
- Integrated work programme developed
- First results Pittsburgh May 2010

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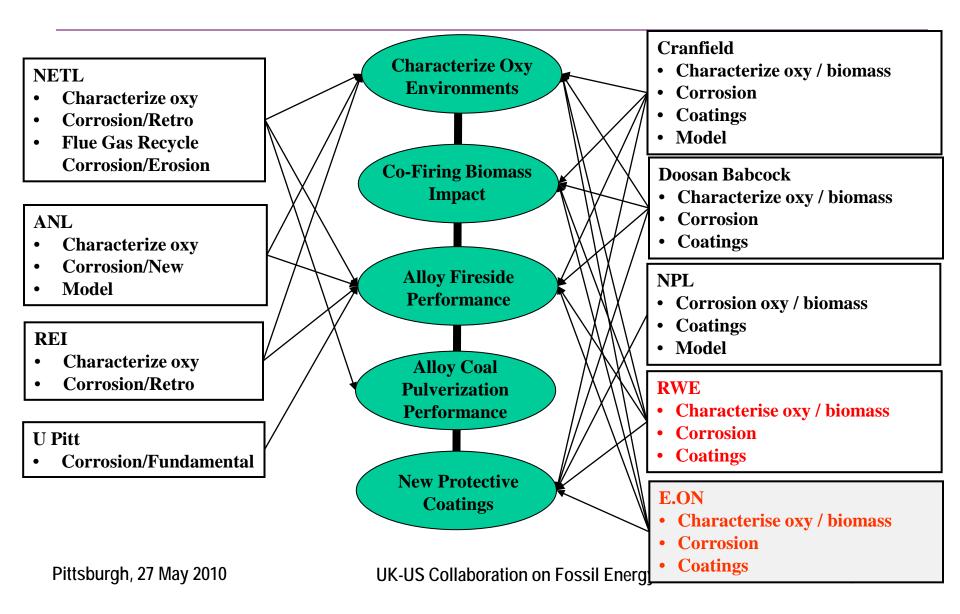
Boiler Corrosion Participants and Role



| | Environment Modeling & | Power Industry | Standardized | Corrosio | on Tests | Coatings | Alloy or Sample | Database | |
|-----------|---------------------------|-------------------|--------------|----------|----------|----------|--------------------|----------|--|
| | Characterization | Experience | Test Method | Lab | Field | Coatings | Supply | Dulubuse | |
| NETL | | | | | | | | | |
| ANL | | | | | | | | | |
| REI | | | | | | | | | |
| UPitt | | | | | | | | | |
| Doosan | | | | | | | | | |
| Cranfield | | | | | | | | | |
| NPL | | | | | | | | | |
| | | | | | | | | | |













- Report on the assessment of environments anticipated in advanced boiler systems.
 - Gas Composition from Process Models
 - Ash Characterization
 - Pilot Scale Testing (deposit compositions, deposition rates, gas compositions)
- Report on the inter-comparison exercise
- Compendium of materials performance data from laboratory and pilot plant exposures of candidate alloys for use in advanced boiler and oxy-fired power systems







- Identification and performance of candidate coating systems for protection of superheaters/reheaters in advanced boiler systems
- Compendium of materials performance data from laboratory exposures for flue gas recycle piping in oxy-fuel boiler systems
- Database of information generated during the collaboration



Phase 2 Task 3 GT Materials Life Assessment & NDE



Task 3: Objectives

Component life prediction

- Access materials performance in multiple simulated environments
- Develop models for deposition/gas phase chemistry along with thermo-kinetics for establishment of corrosion maps
- To use the modified models to predict alloy/coating degradation in specificallydesigned tests
- To identify the fuel/operating conditions and the optimal candidate alloy and coating combinations

Partners:

UK

Cranfield University NPL Siemens Turbomachinery

Non destructive evaluation

- Need to develop rapid and reliable NDE techniques for inspection of gas turbine hot gas path components
- Utilize 2D and 3D NDE technologies to establish their sensitivity and limitations in detecting degradation and delamination in EB-PVD and APS TBCs.
- A multi layered model of thermal diffusivity will be used to develop a methodology for measuring the thermal properties of TBC systems

US

Siemens Energy ANL NETL Pittsburgh ORNL

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Component Life Prediction Activities



Materials Performance Evaluation

- To assess of the passage of contaminants (related to deposition, corrosion and erosion in gas turbines) through the hot gas paths of different IGCC system options; from gasifier through various gas cooling and cleaning options to the gas turbine.
- To identify the fuel/operating conditions and the optimal candidate alloy and coating combinations which are most appropriate to future power systems that use gas turbines fired on wide range of potential fuels.

Component Life Prediction

- To improve models for predicting the fate of trace contaminants within gas turbines (and the effect of fuel composition and turbine operating parameters), including linking deposition / gas phase chemistry models to the latest published versions of models for hot corrosion of alloys/coatings in gas turbines
- To develop a model capable of thermo-kinetic modelling of contaminant flux and extrapolation for high temperatures/high pressures for the establishment of corrosion maps for high temperature metallic and ceramic systems.
- To use the modified models to predict alloy/coating degradation in specifically-designed tests, and for available test cases to validate the model predictions





Develop rapid and reliable NDE techniques for inspection of gas turbine hot gas path components, coated with different types of TBCs.

- Two optical imaging methods (mid-IR reflectance and polarized optical backscatter) and pulsed thermal-imaging will be evaluated to establish their sensitivity and limitations in detecting degradation and delamination in EB-PVD and APS TBCs.
- 3D NDE technologies, including optical coherence tomography (OCT), confocal microscopy and thermal tomography (developed recently at Argonne), will be investigated for directly imaging the depth variation of the TBC degradation.
- The development of novel thermal barrier coatings (TBCs) with self-diagnostic properties will be continued, focusing on the development of remote luminescence sensing for monitoring the temperature of turbine component materials
- During the course of TBC cyclic testing, a fluorescence technique will be used to monitor the stresses developed in the thermally grown oxide of the TBC system, backed up by a simple thermography system to identify coating delamination locations
- A multi layered model of thermal diffusivity will be used to develop a methodology for measuring the thermal properties of TBC systems



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Boundaries for Environmental Testing

1.540

Below

Water

Tube

Water

Tube

Slag



| | Coal Gasification P | rocess | es | | |
|--------------|------------------------------------|-----------|-------------|---------------|-----------|
| | Process | | HTW | Shell | Texaco |
| | Syngas | | | | |
| | Components | | | | |
| | H2 | %vol | 33.97% | 31.42% | 39.37% |
| | CH4 | %vol | 3.92% | 0.01% | 0.06% |
| | CO | %vol | 43.84% | 63.04% | 45.39% |
| | CO2 | %vol | 16.94% | 1.00% | 13.18% |
| | N2 | %vol | 0.50% | 3.41% | 2.00% |
| | Ar | %vol | 0.00% | 1.10% | 0.00% |
| | C2H6 | %vol | 0.83% | 0.00% | 0.00% |
| | C2H4 | %vol | 0.00% | 0.00% | 0.00% |
| | C3+ | %vol | 0.00% | 0.00% | 0.00% |
| | H2S and COS* | %vol | 0.00% | 0.00% | 0.00% |
| | Total | %vol | 100.00% | 99.98% | 100.00% |
| | * H2S and COS | ppmv | 20 | 20 | 20 |
| | On creating of Characteria | | | | |
| - · | Operating Characteri | Fluidized | Entrain a d | Entrained | |
| Coal | Туре | | Bed | flow | flow |
| | туре | React | Deu | 11000 | 11000 |
| gasification | Number of Gasifiers | ors | 2 | 1 | 1 |
| Susmeation | | | | Dry | |
| feed | | | Dry | Pulverize | |
| feed | Coal feed type | | Crushed | d | Slurry |
| | | | | Lockhop | |
| information | | | Lockhopp | per | |
| | | | er screw | pneumati | |
| | Coal feeding system | | conveyer | с | Pumping |
| | Gasification temp | | | | |
| | (min) | С | | 1,500 | 1,260 |
| | Gasification temp | | | | |
| | (max) | С | 1,000 | 2,000 | 1,540 |
| | Carbon conversion | | 93.00% | 99.50% | 98.50% |
| | | | | Water Wall | Refractor |
| | Conifier lining | | Refractory | | |
| | Gasifier lining Raw gas temp to | | Refractory | refactory | У |
| | IN AW DASTERNO (O | | | | |
| | SGC (min) | с | 850 | 900 | 1,260 |

Raw gas temp to

Radiant SGC design

Convection SGC

Dry particulate

Solid wastes

collection

SGC (max)

Radiant SGC location

С

900

Fire tube

cyclone

filler

Ash/Char

900

Above

Water

Tube

Water

Tube

cyclone

filler

Slag

Contaminant analysis

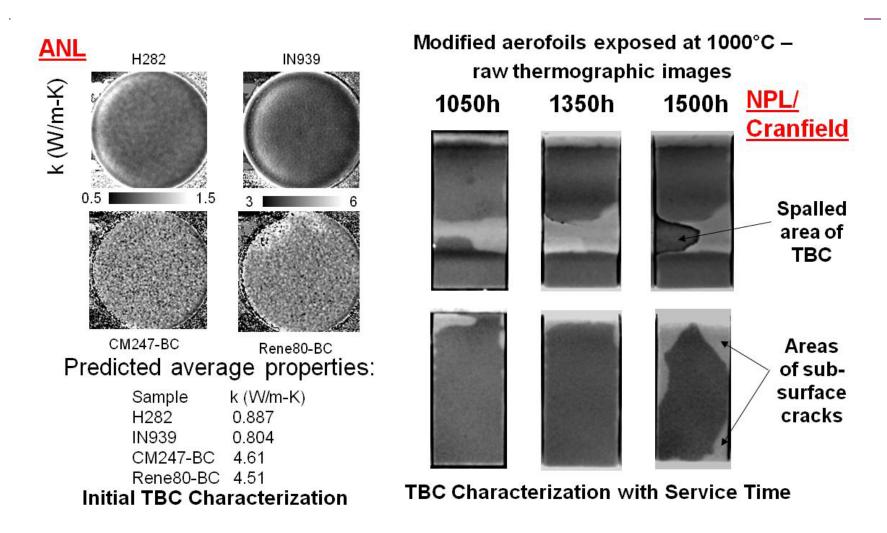
| Fuel type | Company Ref. Fuel | Biogas | Landf | ill gas | Poor quality nat. gas | Pipeline nat. gas | Refinery gases & L | | LPG |
|--|----------------------|------------|--------------|-----------|-----------------------|----------------------|--------------------|---------|-------|
| Net Calorific value (MJ/Kg) | 48.16 | 4 - 10 | 10 - 20 | 20 - 30 | 30 - 40 | 40 - 50 | 50 - 60 | 60 - 70 | 70-80 |
| | Maximum allo | wable conc | entration fr | om ALL so | urces on fuel equiv | alent basis, p | om (mass) | | |
| V | 1.00 | 0.08 | 0.20 | 0.40 | 0.60 | 0.80 | 1.00 | 1.20 | 1.40 |
| Na + K | 0.60 | 0.05 | 0.10 | 0.20 | 0.30 | 0.50 | 0.60 | 0.70 | 0.80 |
| Ca + Mg | 1.00 | 0.10 | 0.20 | 0.40 | 0.60 | 0.80 | 1.00 | 1.20 | 1.40 |
| Pb | 0.50 | 0.04 | 0.10 | 0.20 | 0.30 | 0.40 | 0.50 | 0.60 | 0.70 |
| Zn | 1.00 | 0.10 | 0.20 | 0.40 | 0.60 | 0.80 | 1.00 | 1.20 | 1.40 |
| Hg | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| S | 3000 | 249 | 622 | 1240 | 1860 | 2490 | 3110 | 3730 | 4630 |
| Li | 0.50 | 0.04 | 0.10 | 0.20 | 0.30 | 0.40 | 0.50 | 0.60 | 0.70 |
| SiO2 | 0.04 | 0.003 | 0.008 | 0.016 | 0.024 | 0.032 | 0.042 | 0.05 | 0.058 |
| F+ Cl+ Br+ I | 1.00 | 0.10 | 0.20 | 0.40 | 0.60 | 0.80 | 1.00 | 1.20 | 1.40 |
| Other non- combustibles Incl Ash | 100 | 8 | 20 | 41 | 62 | 83 | 103 | 124 | 145 |

Data being summarized to establish limits for gas compositions and contaminants for **IGCC** environments



NDE Efforts for TBC Characterization







Phase 2 Task 4 ODS Alloys



Aim - To produce a capped tube to header demonstrator as a step towards a single tube heat exchanger

- Improve tube creep properties by a variety of forming means –
 (microstructure modifications achieved in the UK to be creep tested in the US)
- Achieve practical, tested ODS-ODS and ODS-dissimilar metal joints in a number of geometries
- Re-qualify commercial production of ODS alloys
- Investigate the effectiveness of selective laser melting to produce seam welds and layers

Partners

- US UCSD, ORNL, Interface Welding, MER Corp, UNDEERC, Iowa State
- UK Liverpool University, TWI, Cranfield, RWE, Siemens
- Dour Metal
- Integrated work programme developed
- First results Pittsburgh May 2010



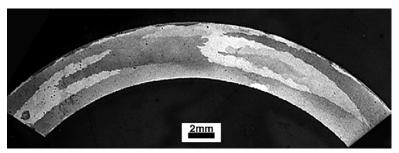


| | Task 1 Alloy Properties | Task 2 Forming | Task 3 Joining | Task 4 SLM | Task 5 Coatings | Task 6 Braze Joints |
|--------------------------|-------------------------------|-------------------|-------------------|---------------|--------------------|---------------------------|
| UCSD | | | | | | |
| ORNL | | | | | | |
| Dour Metal | | | | | | |
| Interface Welding | | | | | | |
| MER Corp | | | | | | |
| UDEERC, ND | | | | | | |
| Iowa State, Iver | | | | | | |
| | | | | | | |
| Liverpool (UK) | | | | | | |
| TWI (UK) | | | | | | |
| Siemens (US) | | | | | | |
| RWE (UK) | | | | | | |
| Cranfield (UK) | | | | | | |



Task 1: ODS Tube Desired structure



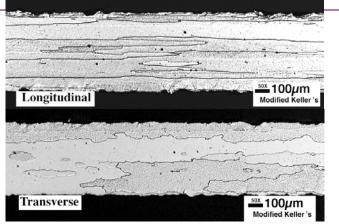


ODM-751, Onion-skin grain structure

In ODS MA956, coarse, secondary recrystallized, grain structure was only possible after extreme cold-working via flow forming.

Flow forming does NOT produce any fibering.

Cold-work achieved via undesirable crosssection reduction. Explore alternates to preserve cross-section



MA956, flow formed grain structure



MA956, starting tube 0.25" thick wall. *flow formed* tube 0.03-0.04"

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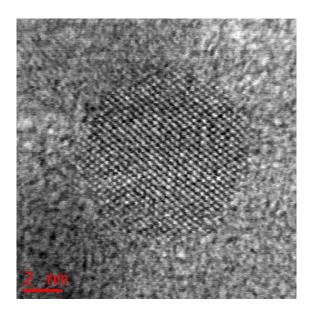


Task 4 ODS Alloys



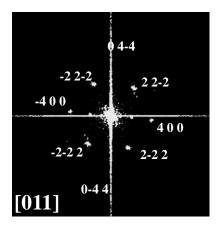
High resolution electron microscopy to determine sequence of oxide dispersion transformations

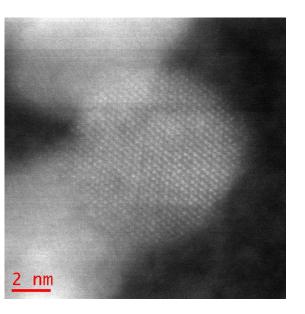
with time and temperature and link with secondary recrystallisation



behaviour.

Cubic -Y₂O₃





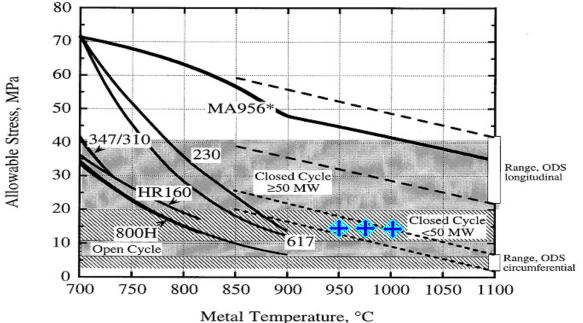


Task 2: Creep Life Assessment for New ODS Alloys



Objective: Establish long term hoop creep property database for ODS alloys

Data plotted upon a minimum of one year exposure at temperature & stress



Current hoop creep metrics for *flow formed* MA956 tubes

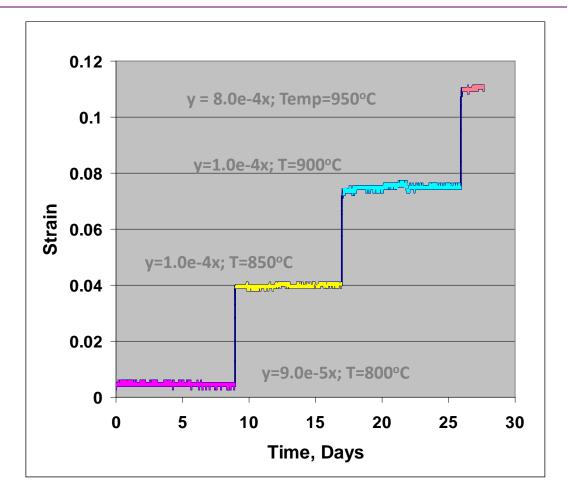
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MA956 Tube Joint Incremental Creep Test







Joint #3, 2ksi Stress, Test in Air, OK

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Phase 2 Next Steps





Workshop –
Pittsburgh, May 2010

• Workshop in the UK in Autumn 2010