

# Advanced Interconnect Development at PNNL

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# Presentation Outline

- ▶ Objectives/Approach
- ▶ Background
  - AISI 441
  - Spinel coatings for steel interconnects
- ▶ Results:
  - Performance of MnCo spinel-coated 441
  - Optimization of MnCo spinel coatings
  - Alternative coating compositions
- ▶ Conclusions
- ▶ Future Work
- ▶ Acknowledgements

# Objectives and Approach

## ► Objectives

- Develop cost-effective, optimized materials and fabrication approaches for intermediate temperature alloy-based SOFC interconnects
- Identify, understand, and mitigate degradation processes in alloy-based interconnects

## ► Approach

- Materials and process development
  - Collaboration with ATI Allegheny Ludlum and NETL
  - Emphasis on AISI 441 as alloy substrate
    - ◆ Modified alloys also being evaluated
  - Mn-Co spinel and other coatings for cathode-side protection
- Synthesis of coating materials, Fabrication of coatings
- Characterization of candidate materials
  - Oxidation tests (including dual atmospheres – air vs. fuel)
  - Area-specific resistance (ASR) tests
  - CTE
  - Alloy, scale, and coatings chemistry via XRD, SEM, EDS, TEM, etc.

# Candidate Interconnect Alloy: AISI 441

- ▶ Ferritic stainless steel: Good CTE match to other components; Electrically conductive Cr-based oxide scale
- ▶ Inexpensive - Manufactured via conventional melt metallurgy
  - No vacuum processing required
- ▶ Similar to AISI 430, but additions of Nb and Ti improve high temperature strength and prevent formation of insulating SiO<sub>2</sub> layer at alloy/scale interface
- ▶ Similar to all other FSS, relatively high oxidation rate at SOFC operating temperatures (and volatility of Cr) indicates need for protective coating
- ▶ Also, relatively weak scale adherence (no RE in alloy)

## Typical Analysis:

Designation	Cr	Mn	Ni	C	Al	Si	P	S	Ti	Nb	La
AISI 441	18	0.35	0.30	0.01	0.05	0.34	0.023	0.002	0.22	0.50	
AISI 430	16-18	≤1.0		≤0.12		≤1.0	≤0.04	≤0.03			
Crofer 22 APU	23.0	0.4-0.8		0.030	≤0.02	≤0.02	0.02	0.050	≤0.2		0.04-0.20

Sources: Allegheny Technologies, Inc.; Thyssen Krupp

# Properties of $(\text{Mn}_{0.5}\text{Co}_{0.5})_3\text{O}_4$ Spinel

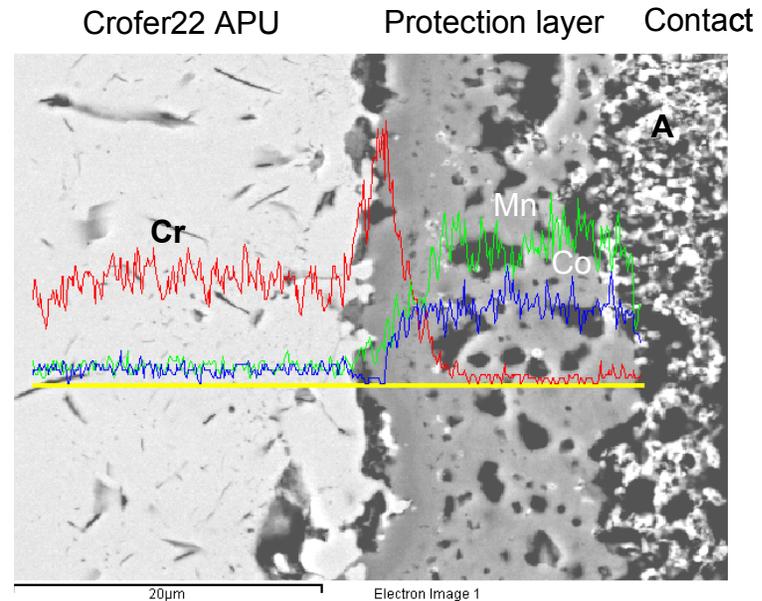
- ▶ High electrical conductivity  
~60 S/cm at 800°C

$$\sigma_{\text{Mn}_{1.5}\text{Co}_{1.5}\text{O}_4} = 10^{3\sim 4} \sigma_{\text{Cr}_2\text{O}_3}$$

- ▶ Good CTE match to FSS and anode-supported cells

$$\text{CTE}_{\text{Mn}_{1.5}\text{Co}_{1.5}\text{O}_4} = 11.5 \times 10^{-6} \text{ K}^{-1}, 20 - 800^\circ \text{ C}$$

- ▶ Chemically compatible with contact pastes, cathodes
- ▶ Cr-free composition
- ▶ Tested with several FSS (Crofer22APU, 430, Ebrite, 441)

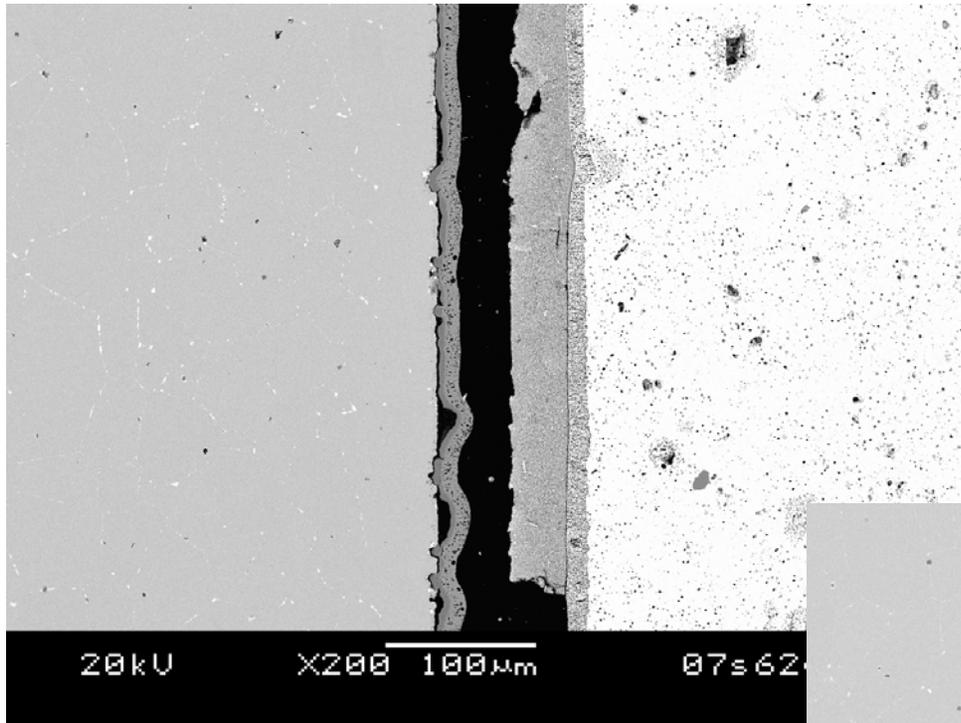


- 6 month thermal cycle test (800°C)
- Negligible Cr transport into coating
- Reduced oxidation rate of alloy

# Ce-modified Mn-Co Spinel

- Rare earth (RE) additions (e.g., Ce, La) to alloys is well-established means of improving scale adherence
- NETL-Albany: Ce surface treatment leads to improved oxidation resistance, lower ASR
- PNNL: Ce-modified Mn-Co spinel coatings improve scale adherence on AISI 441
  - Simple modification – Ce nitrate included in glycine/nitrate precursor
  - Provides
    - ◆ Previously established benefits of MnCo spinel coating (improved oxidation resistance, lower ASR, Cr volatility mitigation)
    - ◆ Benefits of rare earth effect without need for RE additions to alloy

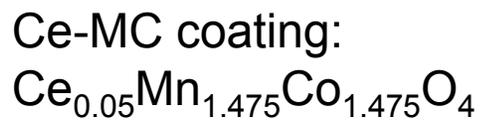
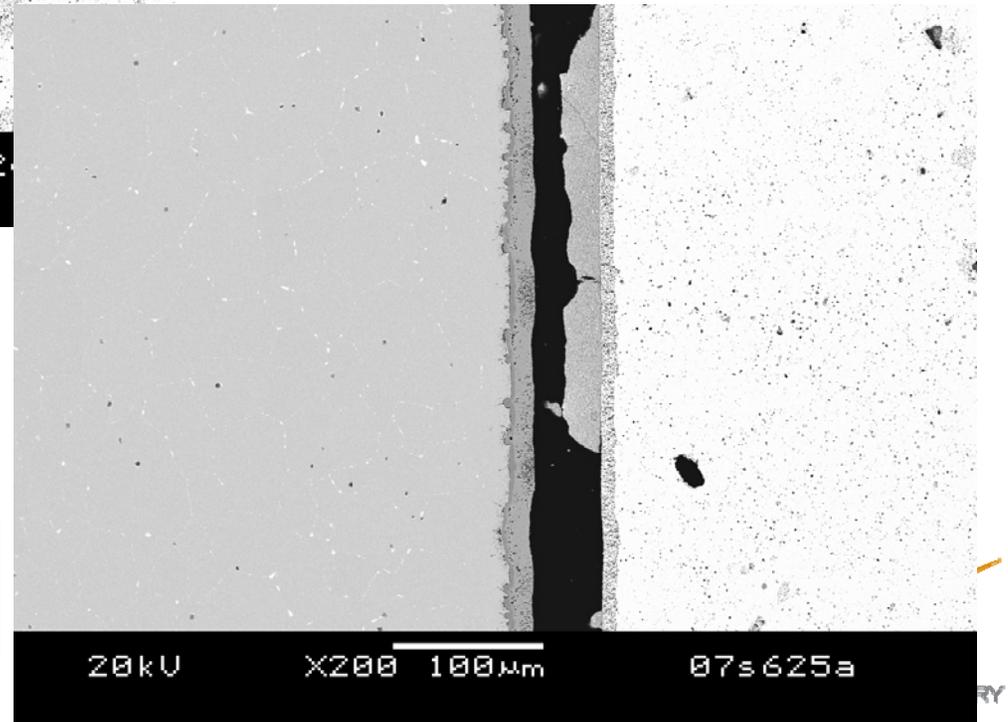
# Improved Scale Adherence with Ce-MC Coatings



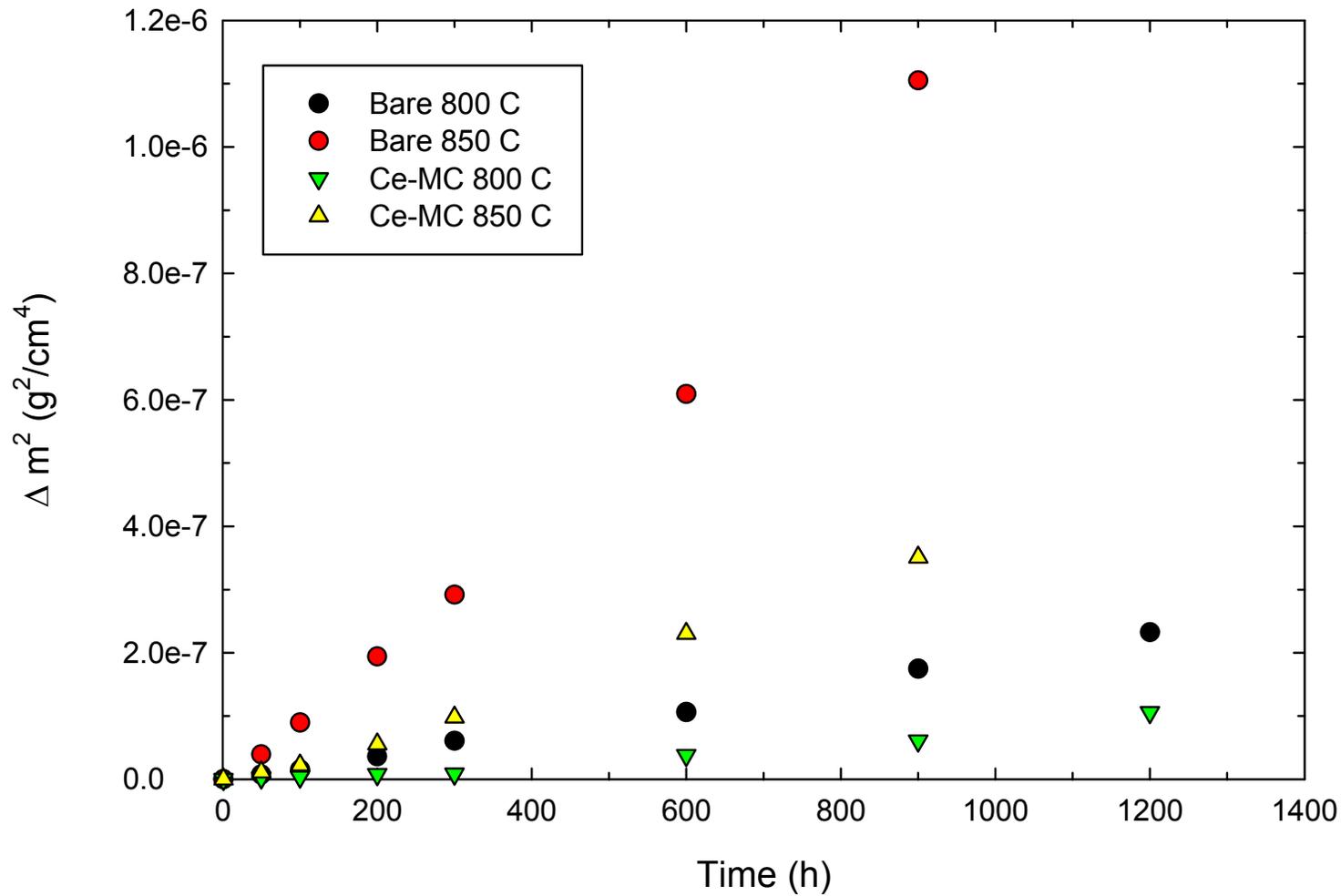
MC coated 441 ↑

After 700 h, 850°C ASR measurement (similar results at 800°C)

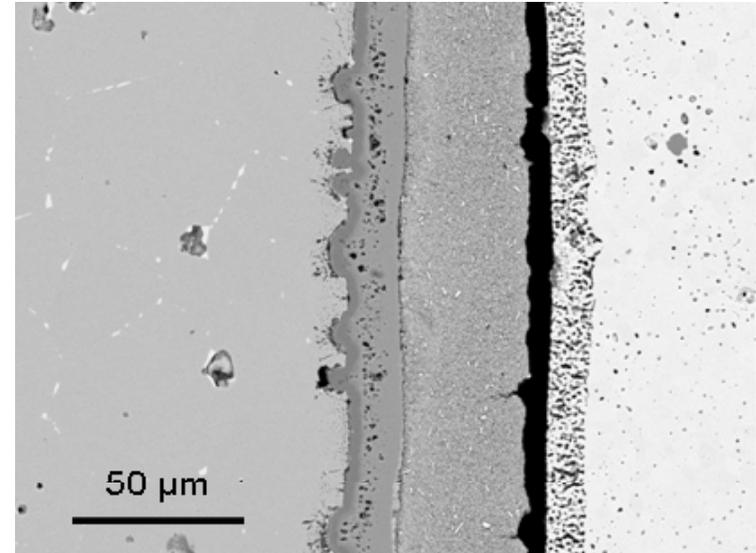
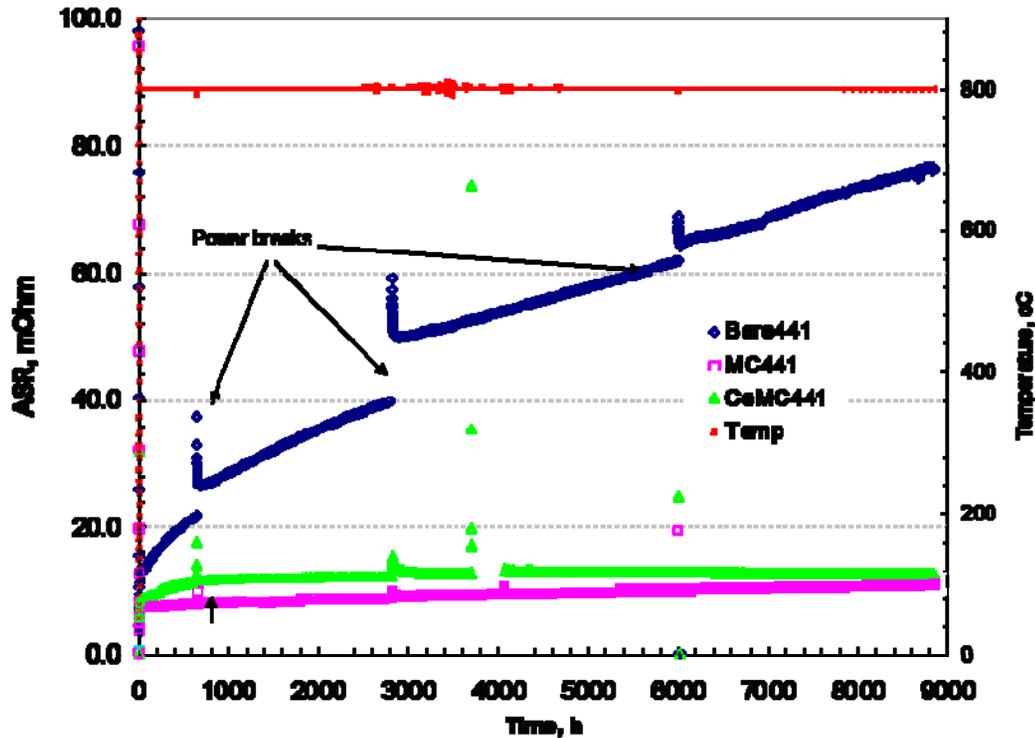
↓ Ce-MC coated 441



# Oxidation Kinetics of AISI 441: Bare vs. Ce-MnCo Spinel Coated

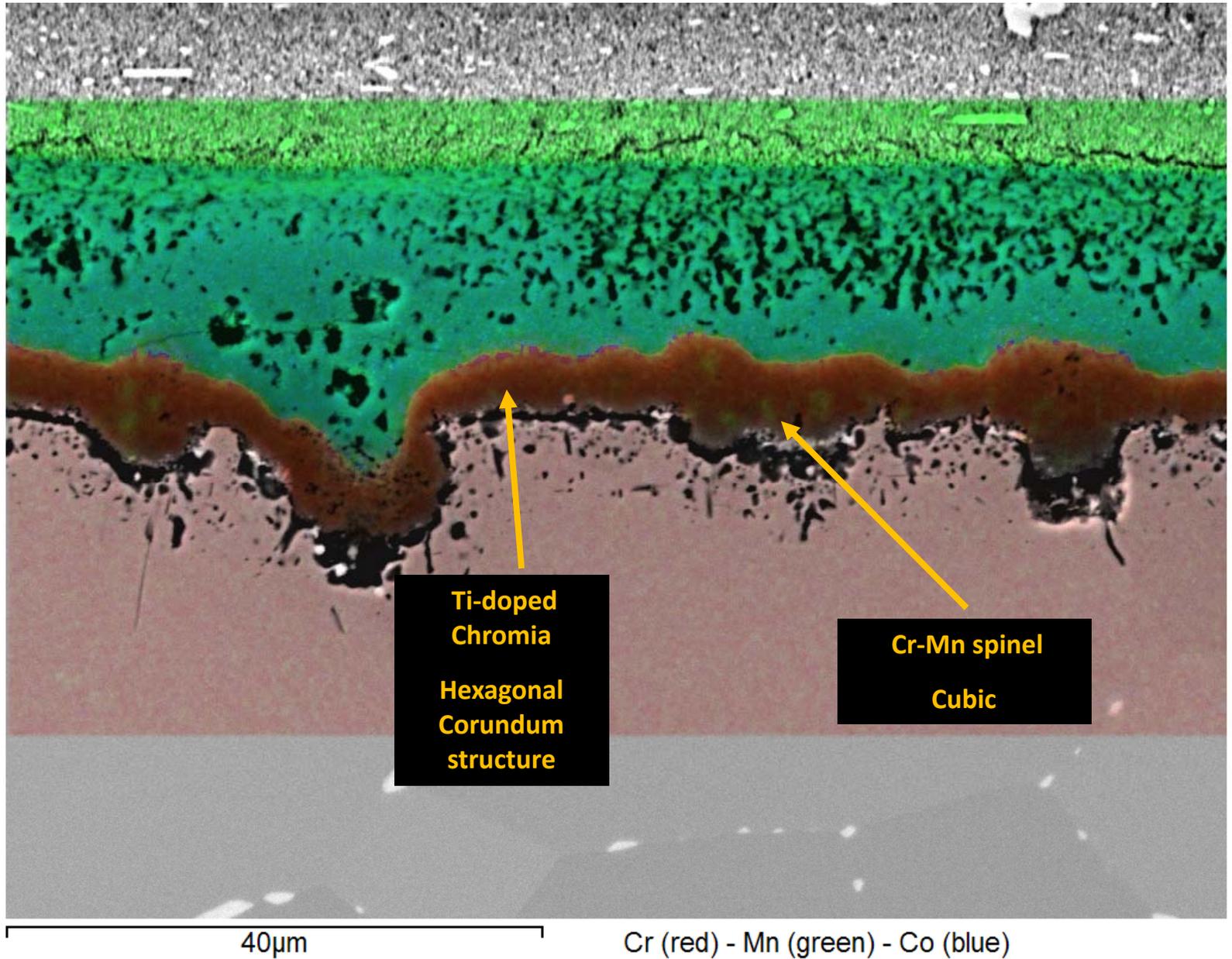


# Electrical Testing of 441

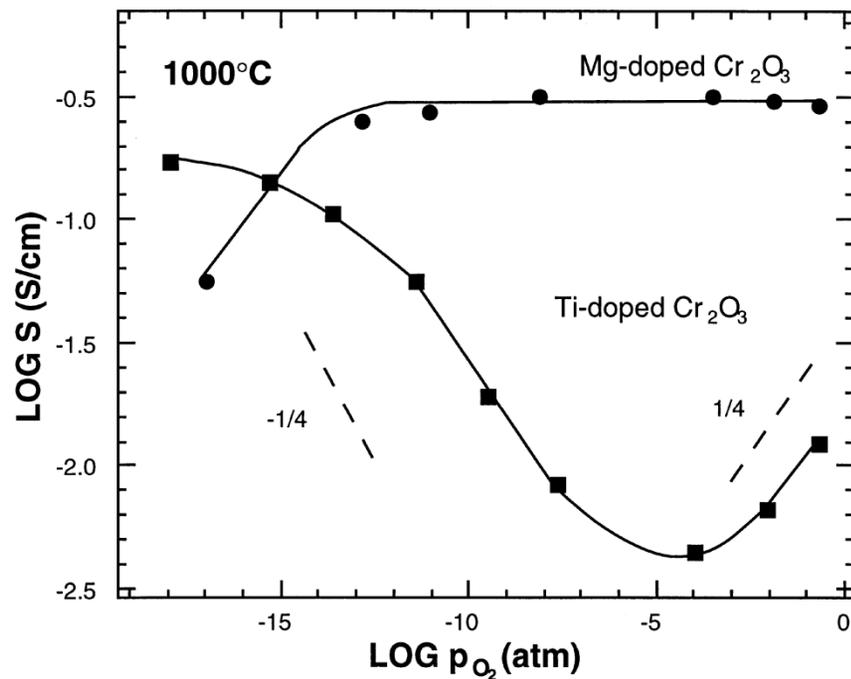
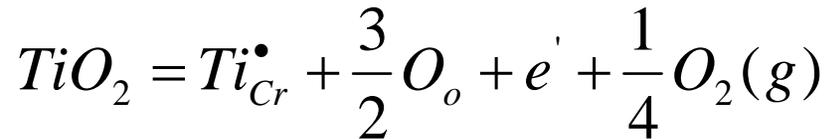


- ❑ Scale growth rates: Bare > MC coated > Ce-MC coated
- ❑ Ce altered interface morphology: smooth scale/metal interface for MC 441, rough interface for Ce-MC 441

# SEM/EDS/EBSD Analysis



# Effect of Ti doping on Conductivity of Cr<sub>2</sub>O<sub>3</sub>



Holt & Kofstad, Solid State Ionics 117 (1999) 21

Porous Contact Material

← a<sub>O<sub>2</sub></sub> = ~10<sup>-0.7</sup> atm

Coating

← a<sub>O<sub>2</sub></sub> = ? atm

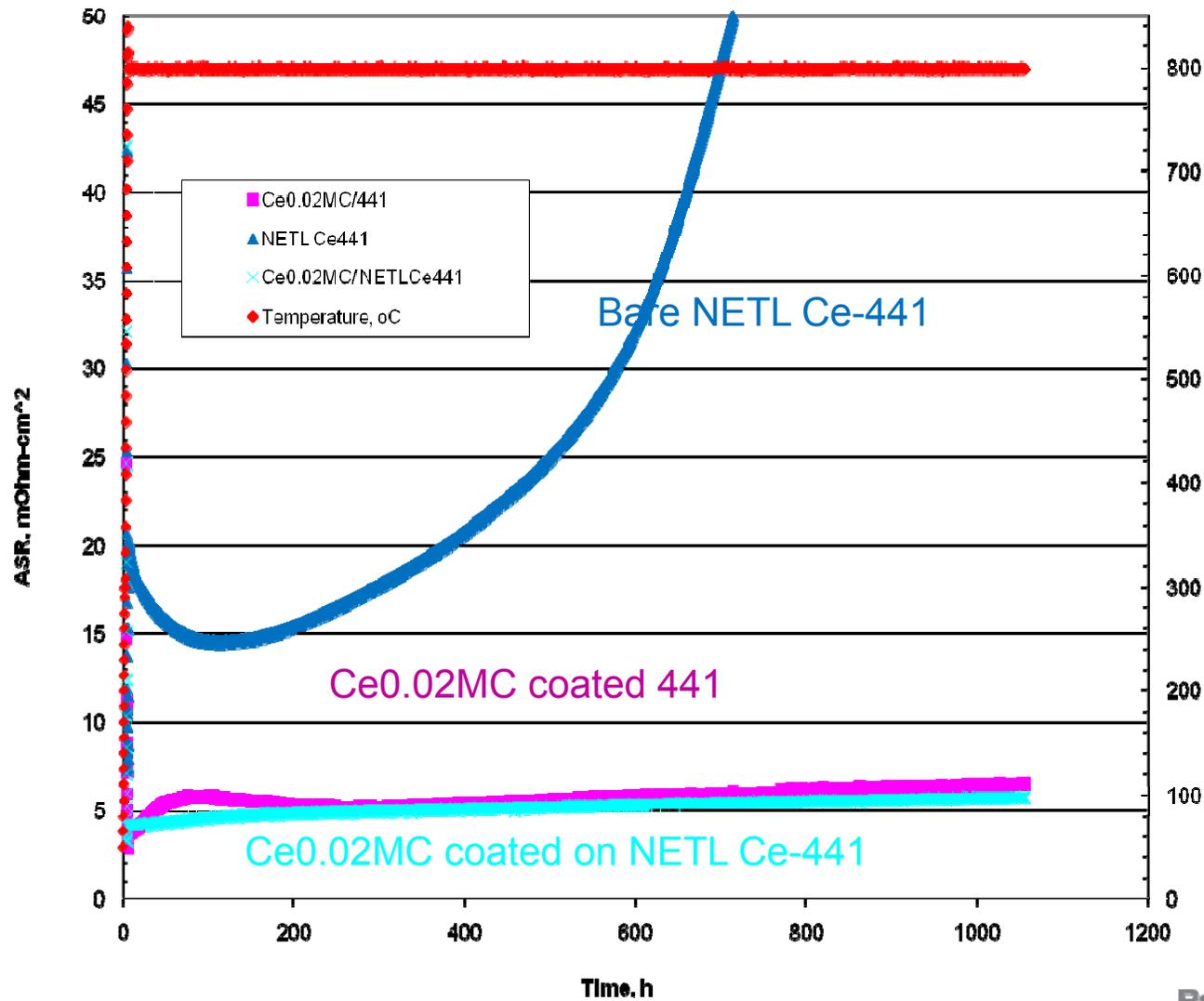
Scale

← a<sub>O<sub>2</sub></sub> = ~10<sup>-28</sup> atm

Alloy

For conductivity of 0.1 S/cm and scale thickness of 6 microns, calculated ASR = 6 mOhm-cm<sup>2</sup>

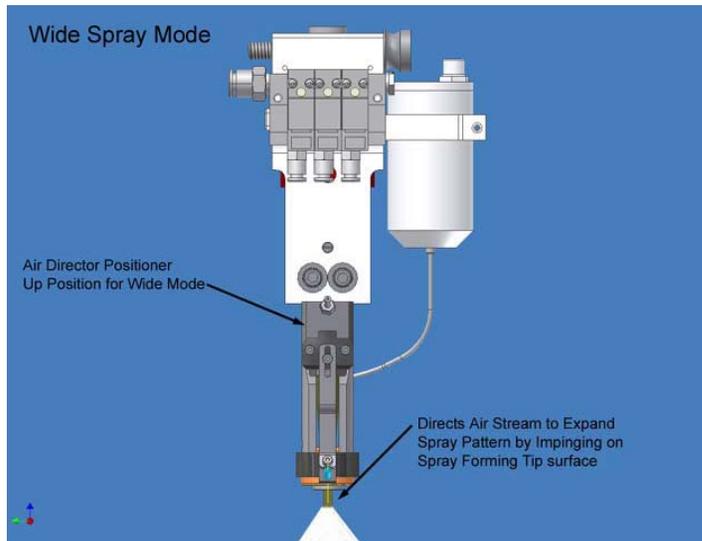
# ASR testing of AISI 441: 0.02Ce-MnCo spinel, NETL-Albany Ce surface treatment



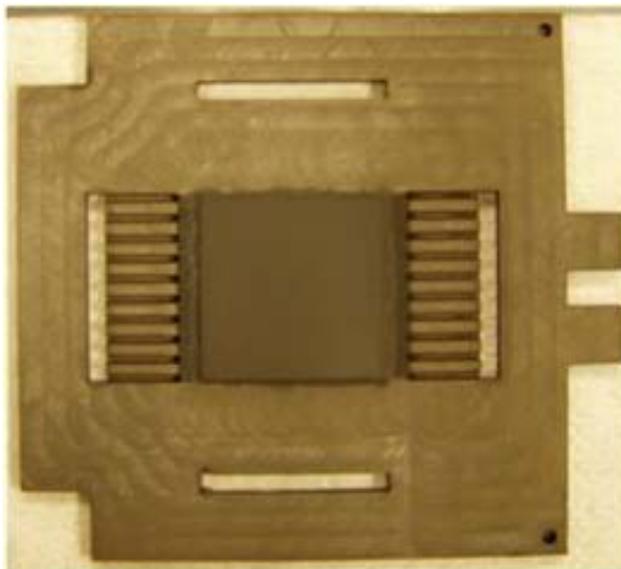
# Optimization of Ce-MnCo spinel coatings

Parameters	Value	Comments
Calcination Temp.	900°C	key parameter
Particle Size	<1mm	attrition -milled
Binder to Powder Ratio	0.6:1	may vary with binder type
Coating Drying Temp.	<60°C	better results with slow drying
Reducing atmosphere	2.7% H <sub>2</sub> , wet	gas passing through a water bubbler
Reducing Temp. and Time	850°C, 4h	at least 650°C
Pre-oxidation Temp.	950°C, 0.5h	match with sealing temperature

# Ultrasonic spray-based fabrication of Ce-MnCo spinel coatings: Preliminary Results



Coating speed : 80mm/sec  
Head height : 35mm  
Coating mode : Wide mode  
Ink feeding rate : 1.5ml/sec  
Air flow rate : 50ml/sec



# Ultrasonic spray-based fabrication: Process Optimization

## Design Of Experiment (DOE) Optimization

Taguchi, Grey-Taguchi method and ANOVA (Analysis of Variance)

Points of reference: Coating thickness, pore area per unit area and the amount of material used

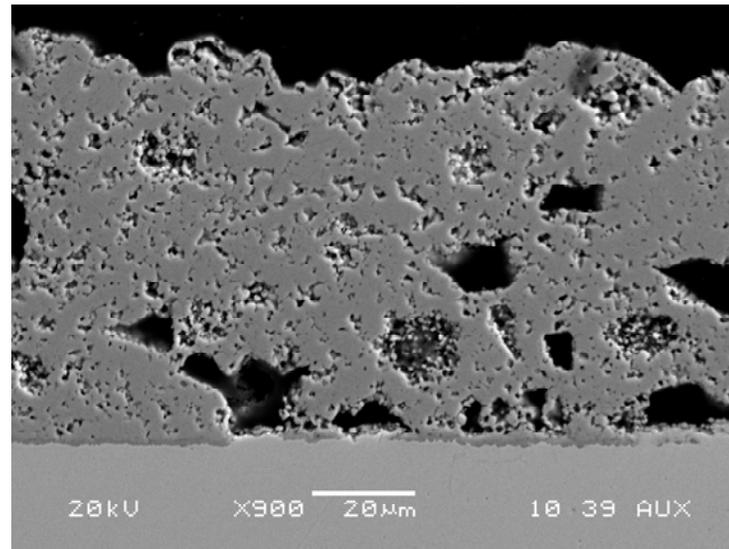
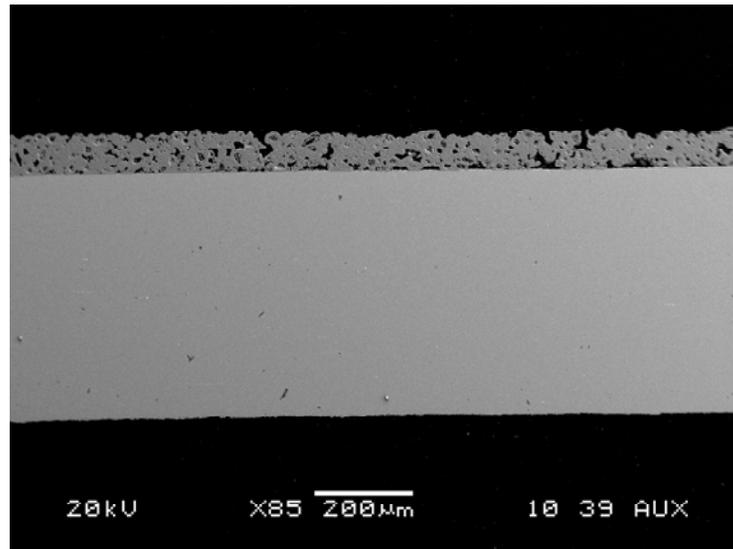
Two different mode : 1. Wide mode  
2. Narrow mode

Factors	level1	level2	level3	level4
Viscosity	37 cP	17 cP	9 cP	5 cP
Coating speed	40mm/sec	60mm/sec	80mm/sec	100mm/sec
Head height	15mm	25mm	35mm	45mm
Ink feeding rate	0.5ml/sec	1ml/sec	1.5ml/sec	2ml/sec
Air flow rate	30ml/sec	40ml/sec	50ml/sec	60ml/sec



# Elimination of Reducing Atmosphere Heat Treatment for MnCo Spinel Coatings

- ▶ Standard fabrication approach requires heat treatment in reducing atmosphere followed by oxidative heat treatment.
- ▶ Use of metallic precursor powders (Mn, Co) eliminates reducing heat treatment, and thus reduces coating cost.
- ▶ Compatible with reactive air aluminization (RAA) of sealing surfaces of the interconnect
- ▶ Preliminary results:



# Solid-State Sintering

## ▶ Conventional Sintering

### ■ Thermodynamics

- Driving Force: Decrease in surface free energy,  $E_S$
- $S_A = 4\pi r^2 N = 3V_m/r$  ;  $E_S = 3\gamma V_m/r$
- Assume  $\gamma = 1 \text{ J/m}^2$ ,  $r = 1\mu\text{m}$ ,  $V_m = 2.5 \times 10^{-5} \text{ m}^3$ :  **$E_S = 75 \text{ J/mole}$** . (Rahaman, "Ceramic Processing and Sintering," Dekker)

### ■ Kinetics

- Diffusion-based process, so thermally activated:  $D \propto \text{Exp}(-E_a/kT)$
- Thermal Energy obtained from furnace
- Assuming  $E_a = 1.5 \text{ eV}$ ,  $D_{1400^\circ\text{C}}/D_{900^\circ} \approx 80$

## ▶ Pressure Sintering

- Driving Force: Externally applied pressure,  $P_a$ , during heating
- Assume 30 MPa pressure:  $W = P_a V_m = \mathbf{750 \text{ J/mole}}$

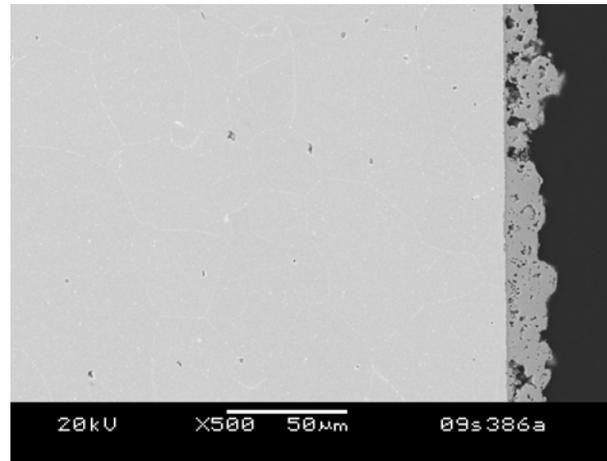
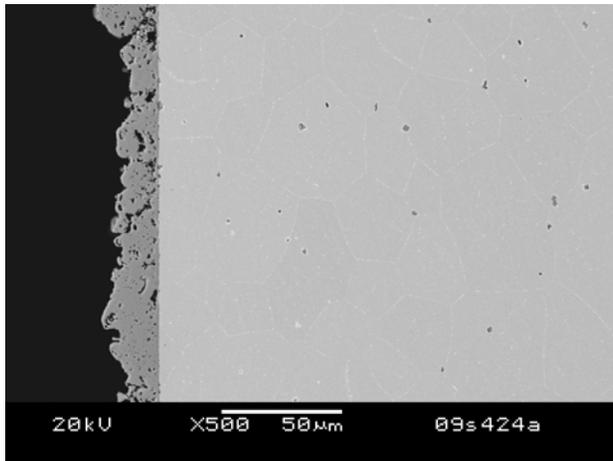
## ▶ Reaction Sintering

- Driving Force provided by decrease in energy accompanying chemical reaction
- Challenges in controlling microstructure due to simultaneous processes (chemical reaction/sintering)

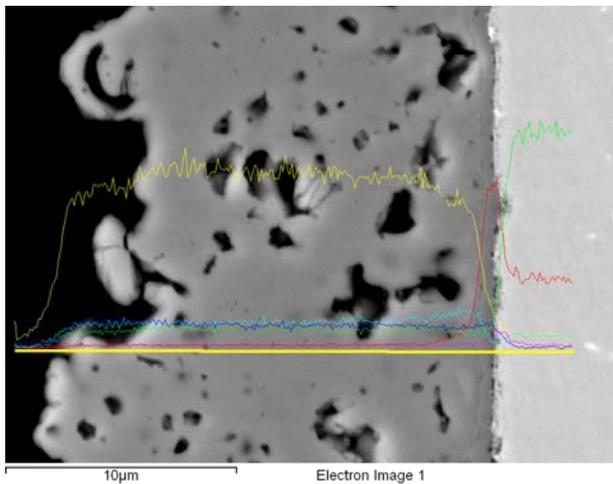
# Reaction-Assisted Sintering of Spinels

- Reaction-Assisted Sintering
  - Both Thermal and Chemical Energy available to enhance densification rate
  - Example (data for MnCo spinel not available):
    - $\text{Co(s)} + 2 \text{FeO(s)} + \text{O}_2(\text{g}) = \text{CoFe}_2\text{O}_4$
    - $\Delta H_r(900^\circ\text{C}) = -547 \text{ kJ/mol}$
    - Adiabatic Temperature:  $\sim 3600^\circ\text{C}$
  - Less advantage with all-oxide precursors:
    - $\text{CoO(s)} + 2 \text{FeO(s)} + 0.5\text{O}_2(\text{g}) = \text{CoFe}_2\text{O}_4$
    - $\Delta H_r(900^\circ\text{C}) = -314 \text{ kJ/mol}$
  - **Greater advantage with all-metallic precursors:**
    - $\text{Co(s)} + 2 \text{Fe(s)} + 2\text{O}_2(\text{g}) = \text{CoFe}_2\text{O}_4$
    - $\Delta H_r(900^\circ\text{C}) = -1077 \text{ kJ/mol}$

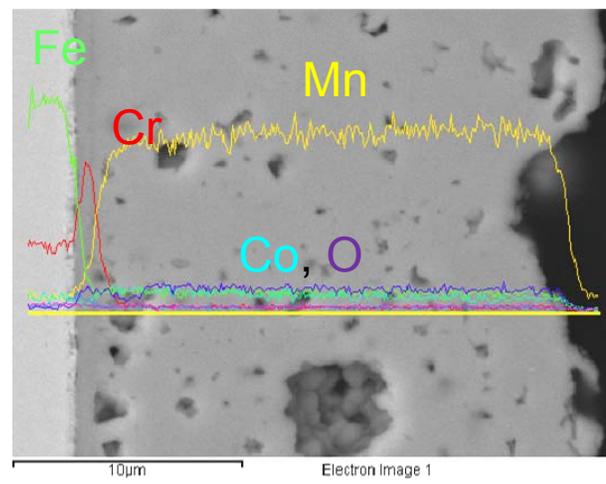
# Alternative Interconnect Coating Compositions



Emphasis on reduction / elimination of Co, to reduce coating cost



Mn4Co1



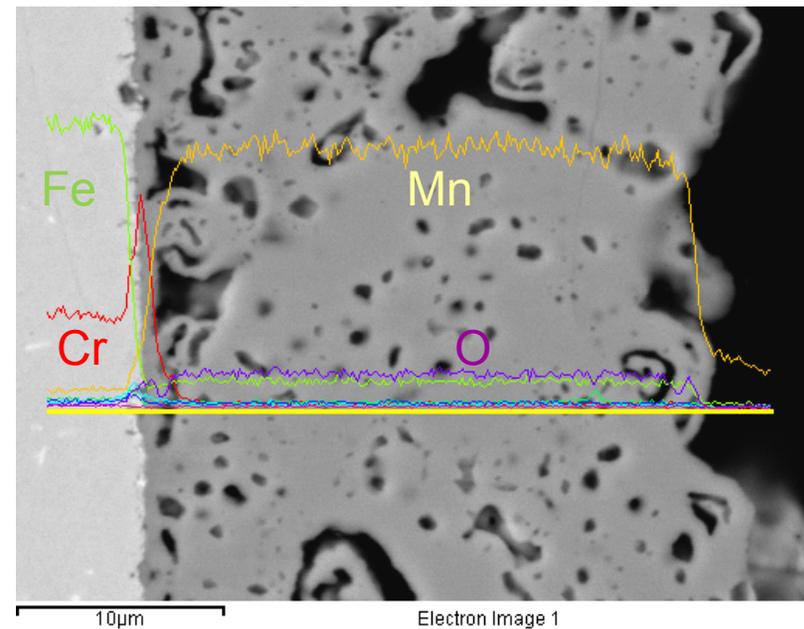
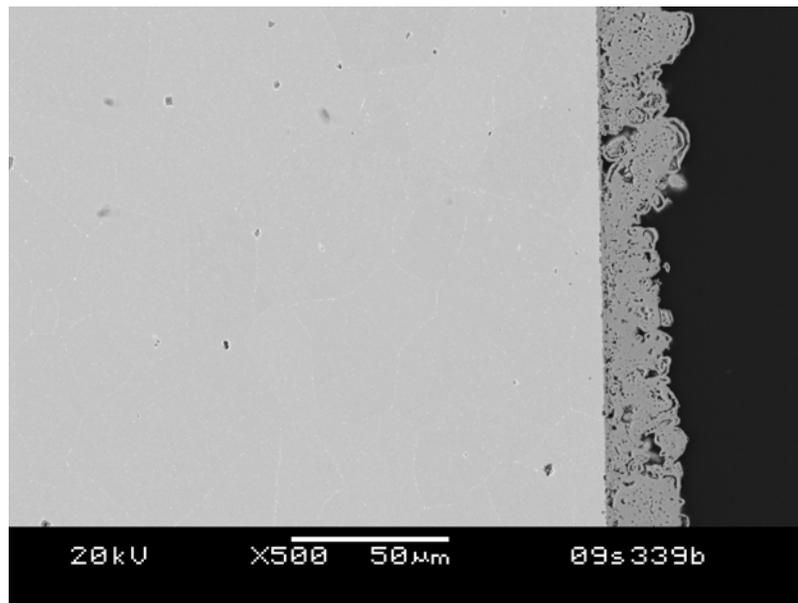
Mn3Co1

MnCo with reduced Co content



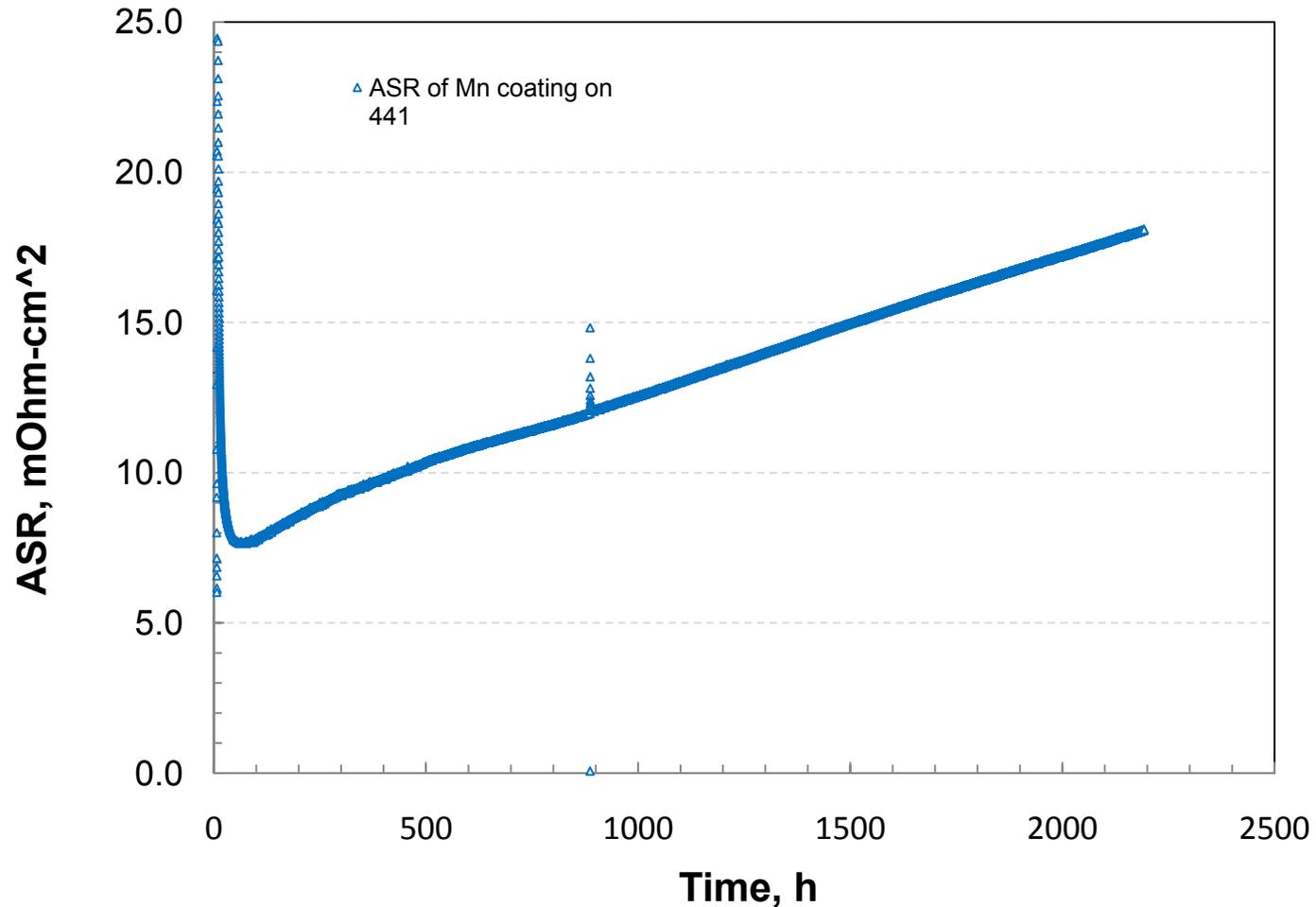
# Alternative Interconnect Coating Compositions

- ▶ Mn only precursor (Cobalt-free)
- ▶ Mn oxide coating prepared from Mn powder:



Heat treatment: 800°C in air for 24 hours

# ASR of Mn Coated 441 at 800°C



- Post-test analysis will be performed to determine cause of ASR increase
- Other compositions are under investigation

# Conclusions

- ▶ AISI 441 exhibits promising alloy chemistry for SOFC interconnect applications
  - Expensive refining processes not required, so cost is reduced
- ▶ Ce-modified MnCo spinel coatings exhibit the benefits of original MnCo coatings, and also provide improved scale adherence and lower scale growth rate
- ▶ Ultrasonic spray-based fabrication process appears promising
  - DOE matrix of optimization trials in progress
- ▶ Cost-reduction approaches are under investigation
  - Elimination of need for preliminary reducing atmosphere heat treatment
  - Reduction or elimination of Co content

## Future Work

- ▶ Evaluate long-term stability and electrical performance of Ce-MC spinel-coated 441 steel, including dual atmosphere (w/ simulated coal gas fuel) and thermal cyclic conditions.
- ▶ Optimize automated ultrasonic spray process for coating of larger, shaped parts.
- ▶ Reduce cost of protective coatings through elimination of reducing heat treatment and/or minimization or elimination of Co content

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