



NATIONAL ENERGY TECHNOLOGY LABORATORY



## Coal Syngas Testing and Evaluation at NETL

*2009 SECA Workshop*

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*Randall Gemmen*

*Kirk Gerdes*

*Greg Hackett*

*Andrew Martinez*



# Goal

Identify the effects of trace coal syngas species on SOFC anodes, and identify the trace material exposure levels that will be acceptable to fuel cell operation.

*Prior to SECA, no data existed to guide developers on how to design coal syngas cleanup systems suitable for SOFC operation.*

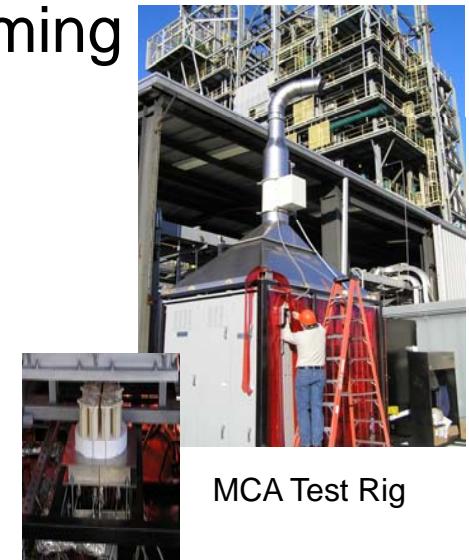
Trace species: <1000ppm (Ref. Speight)

# Possible Effects of Trace Species on SOFC Anode

- **Affect the ability of Ni to promote the electrochemical reactions**
  - Trace species on Ni surface inhibit the adsorption of H<sub>2</sub>, CO, or dissociation of H<sub>2</sub>
- **Affect the ability of YSZ to transport oxygen ion**
  - Formation of secondary zirconia phases
- **Affect the electrical conductivity**
  - Formation of secondary nickel phases such as nickel-phosphide
- **Affect the transport of reactants in/out of electrode**
  - Formation of condensed phases that fill electrode pores

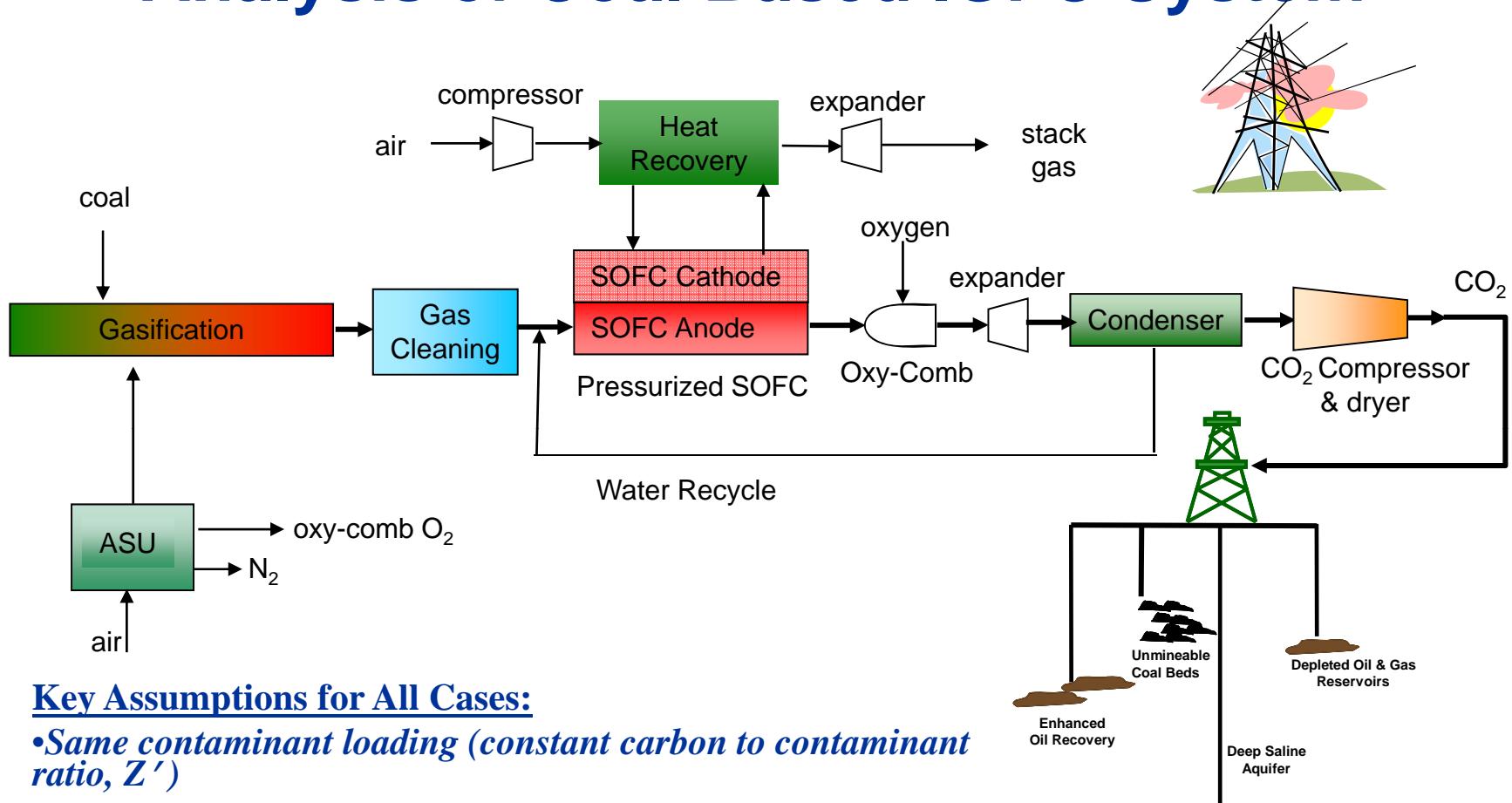
# Outline

- **Analysis**
  - Identify sensitivity of gasification technology on trace species attack
- **Experimental**
  - Individual trace specie evaluations
  - Direct coal syngas testing—next test coming in August.



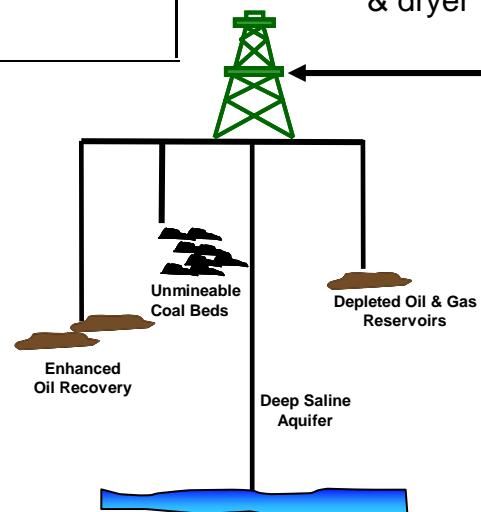
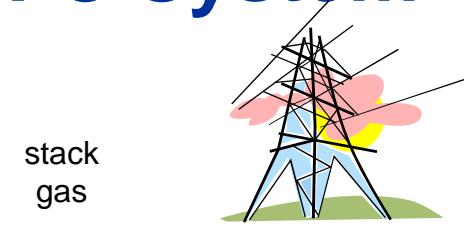
MCA Test Rig

# Analysis of Coal Based IGFC System



## Key Assumptions for All Cases:

- Same contaminant loading (constant carbon to contaminant ratio, Z')
- Same FU (80%)
- Same power, P, from fuel cell stack operated at 80% efficiency
- Different syngas compositions affect stack performance through Nernst Potential (effective cell resistance fixed)
- Carbon deposition control through water addition

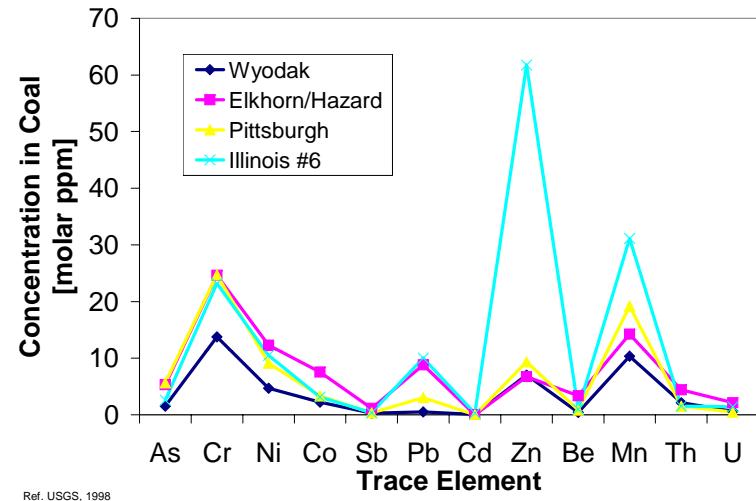


# Trace Metal Contaminants (Coal-Type Dependency)

- USGS analysis of trace elements in coals.
- Different coals have different levels of given a given contaminant.

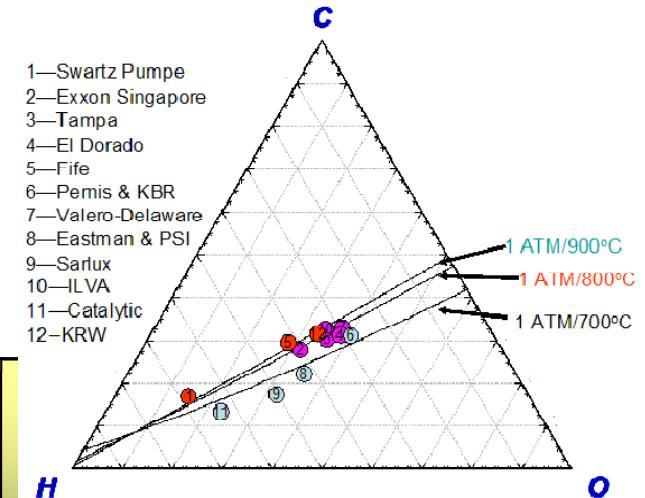
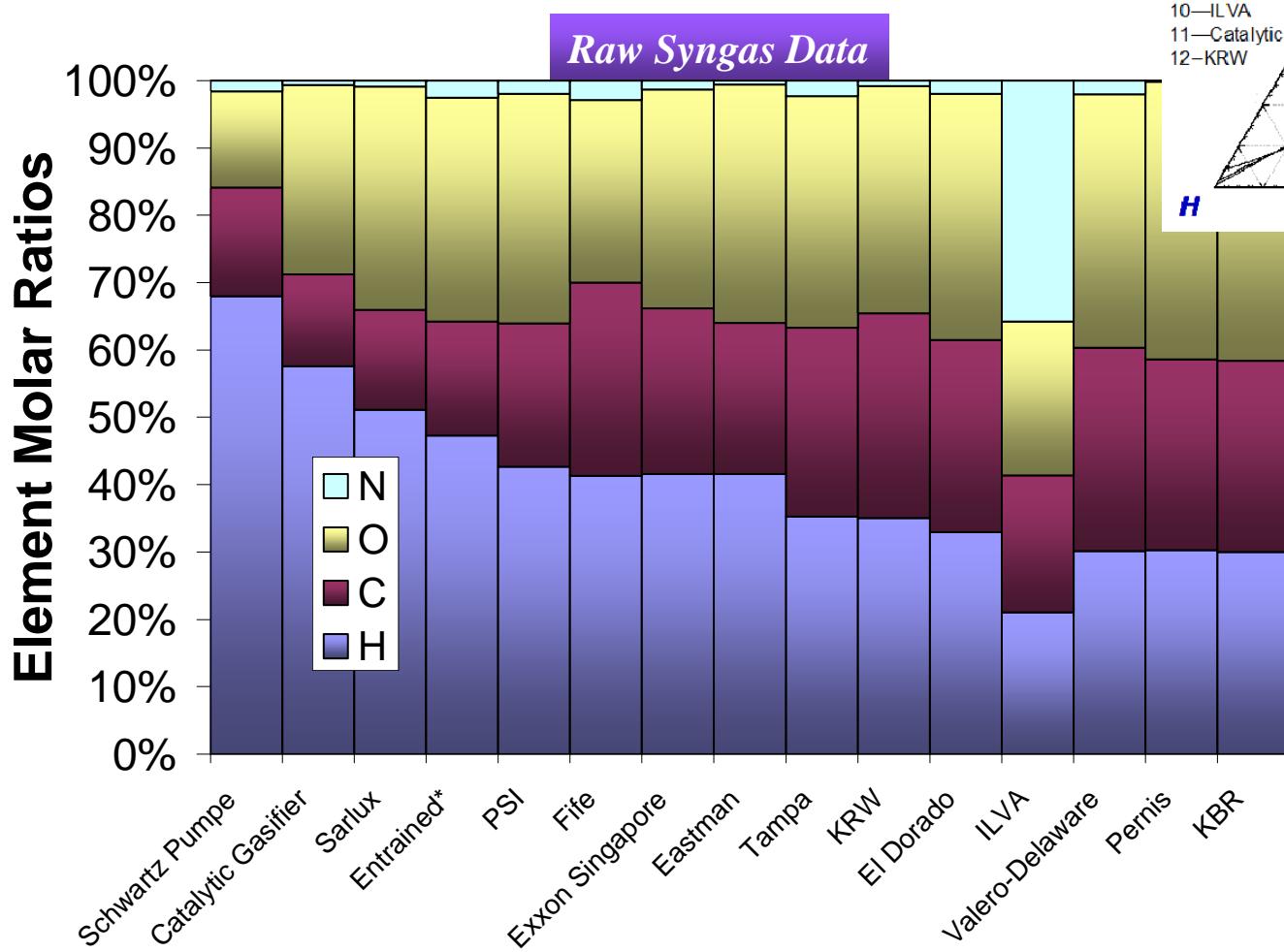
Table 2  
Trace specie concentrations

Component	Concentration (ppmv)	Volatility class
AsH <sub>3</sub>	0.6	II
HCl	1	III
PH <sub>3</sub>	1.91	II
Sb	0.07	II
Cd	0.011	II
Be	0.025	II
Cr	6	II
Hg	0.025	II
K	512	I
Se	0.15	II
Na	320	I
V	0.025	II
Pb	0.26	II
Zn	9	II

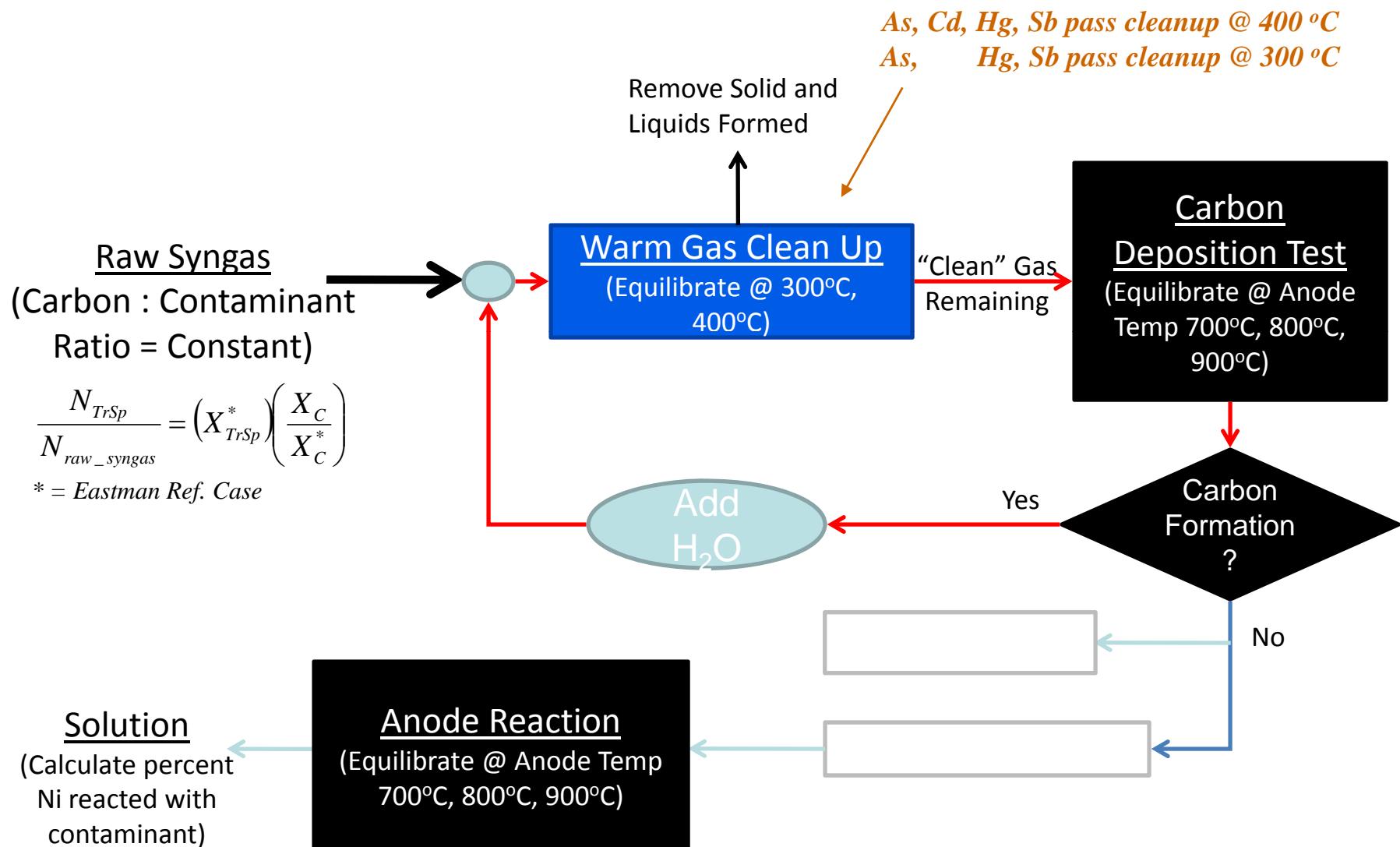


*Contaminant for Eastman Gasifier.  
Other gasifier cases have same trace loadings (by assuming constant Carbon/Contaminant ratio)*

# Gasifier Comparisons



# Computational Procedure



## N<sub>Ni</sub> to N<sub>fuel</sub> Ratio Calculation

$$\left\{ \begin{array}{l} P = A_{cell} i'' V_{cell} N_{cells} \\ N_{cells} A_{cell} i'' = FU \frac{N_{fuel} n_{fuel} F}{t} \\ V_{cell} = V_{Nernst} \eta_{cell} = (V_{Nernst} - V_{act} - i'' R_{ohmic}) \\ A_{cell} = \frac{I}{i''} \\ N_{Ni} = A_{cell} T_{cell} \hat{\rho}_{Ni} N_{cells} \end{array} \right.$$

(Ni to Syngas Molar Ratio at Operating Time 't')

$$\frac{N_{Ni}}{N_{fuel}} = \frac{FU \cdot T_{cell} \cdot n_{fuel} F \cdot R_{ohmic} \cdot \hat{\rho}_{Ni}}{[V_{Nernst} (1 - \eta_{cell}) - V_{act}] \cdot t}$$

Specified :

$\eta_{cell}$  = Cell Efficiency (80%)

$R_{ohmic}$  = Ohmic Resistance (0.1 ohm - cm<sup>2</sup>)

FU = Fuel Utilization (80%)

$V_{act}$  = Activation Loss (0.1 V)

$t$  = time (5000 h)

$\hat{\rho}_{Ni}$  = Electrode Ni Density (0.15 mol/cm<sup>3</sup>)

T<sub>cell</sub> = Anode Thickness (1 mm)

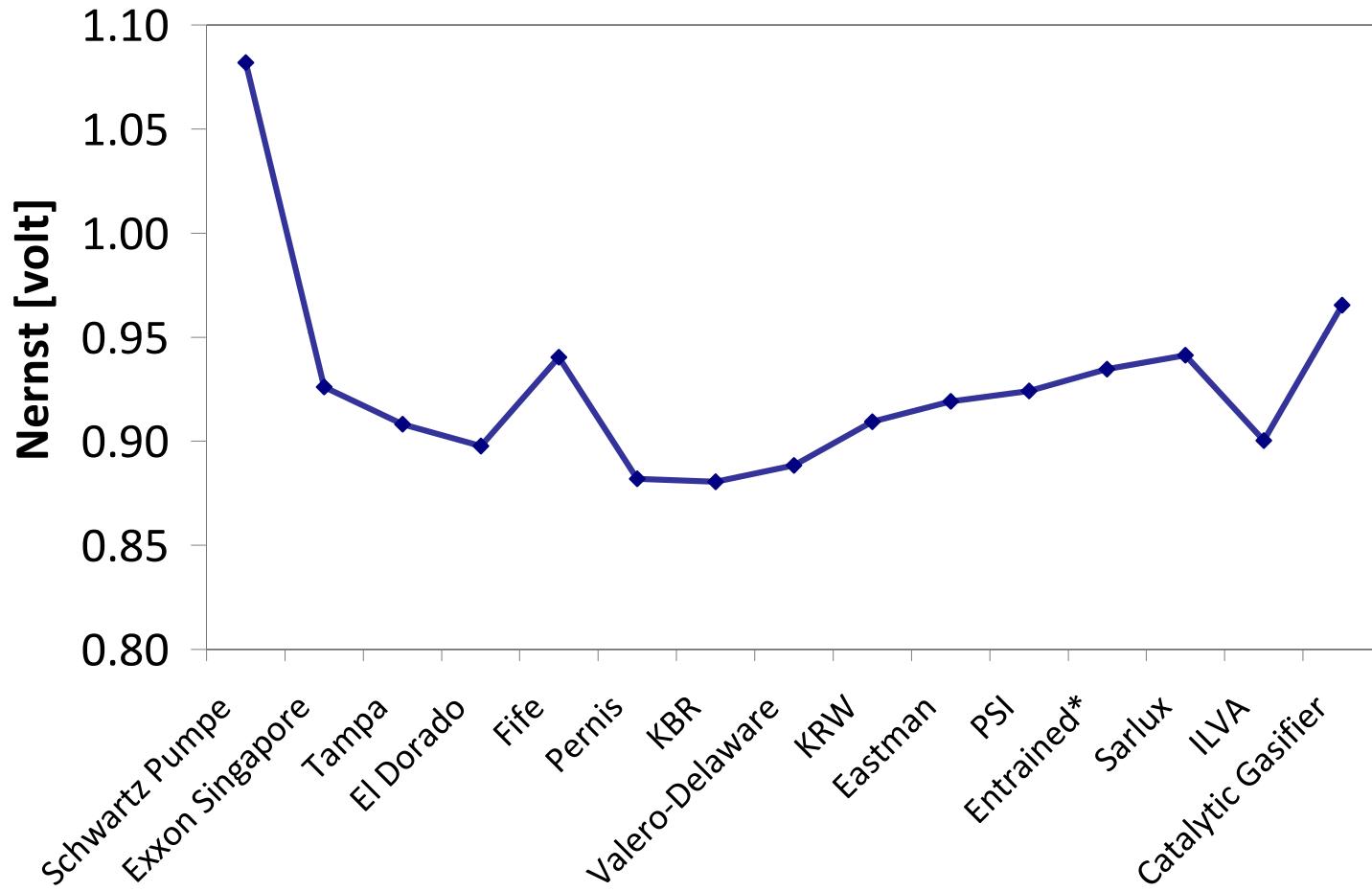
From Syngas Composition :

$V_{Nernst}$  = Nernst Potential

n<sub>fuel</sub> = Charge Number (electrons/mole of fuel)

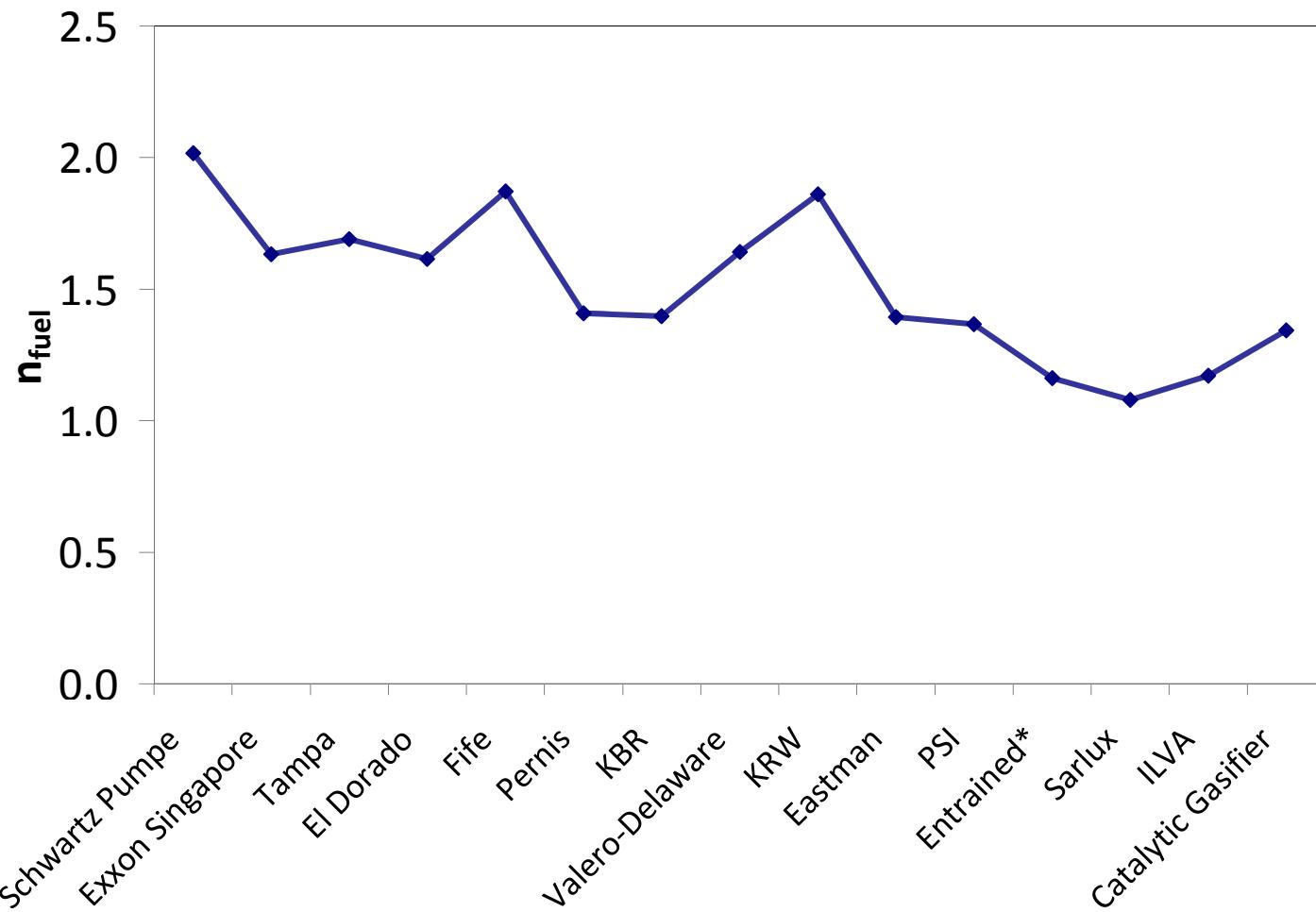
# Cell Inlet Nernst Voltage

(400 deg. C cleanup; 800 deg. C Anode)



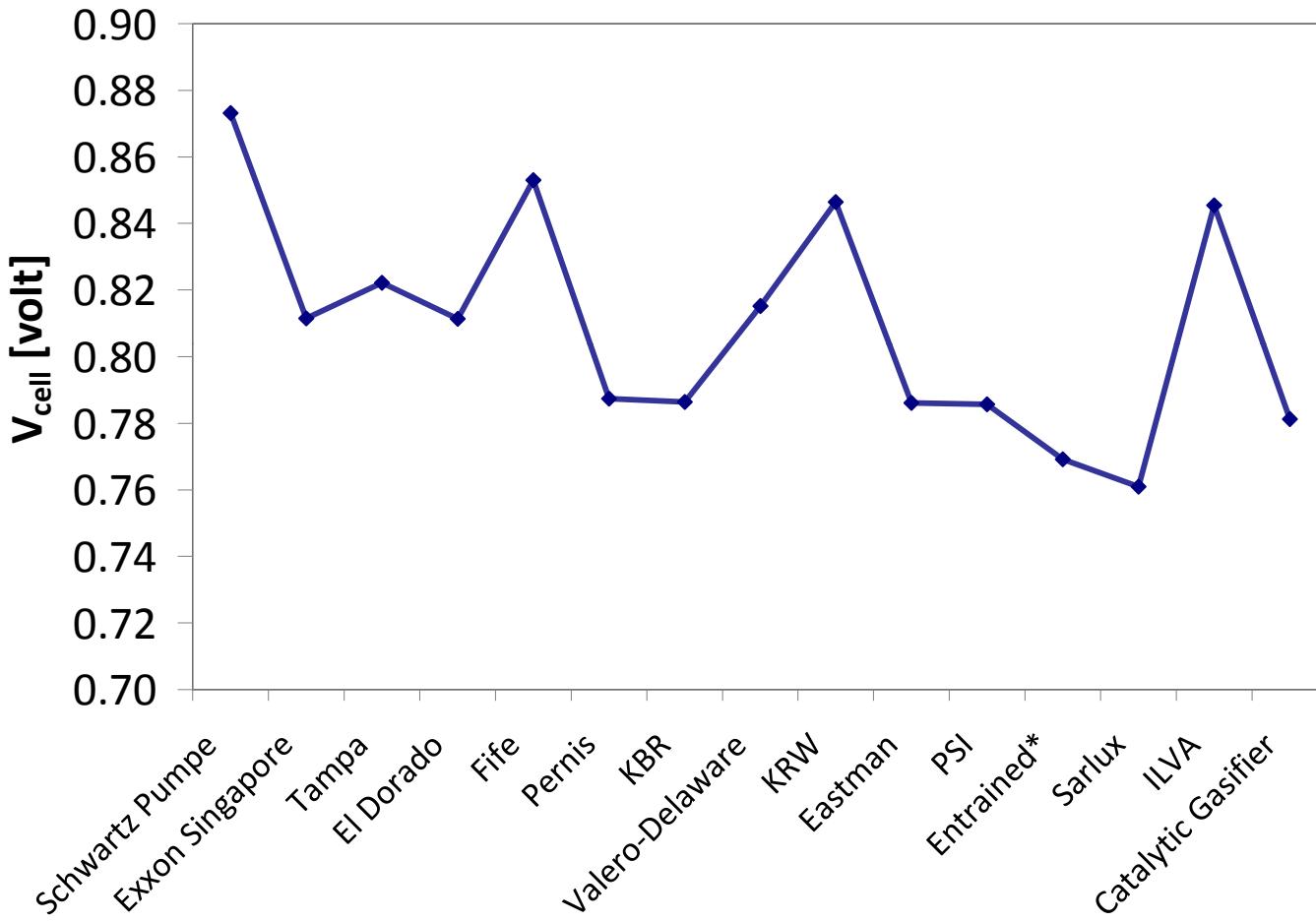
# Charge Number

(400 deg. C cleanup; 800 deg. C Anode)



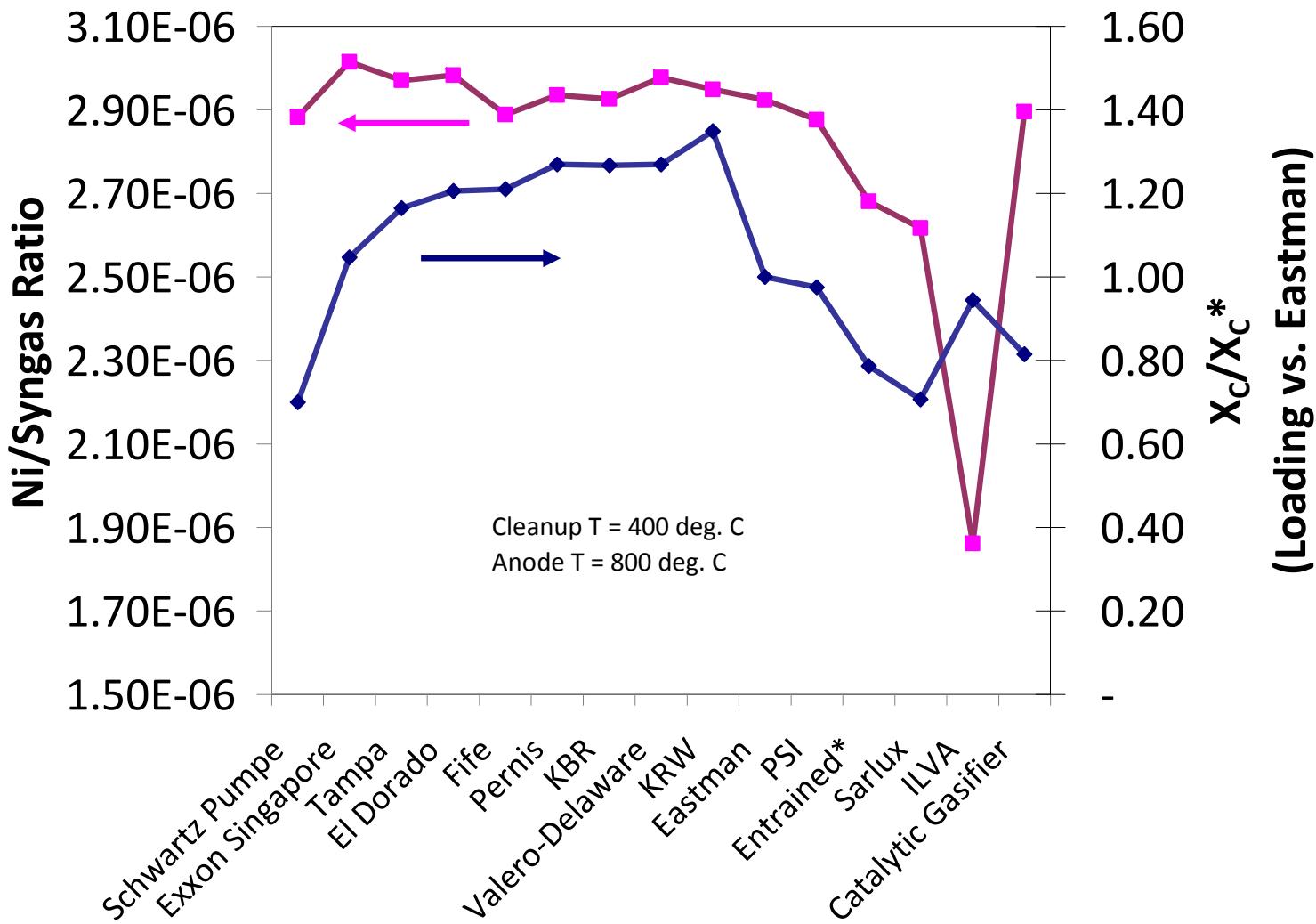
# Cell Operating Voltage

(400 deg. C cleanup; 800 deg. C Anode)



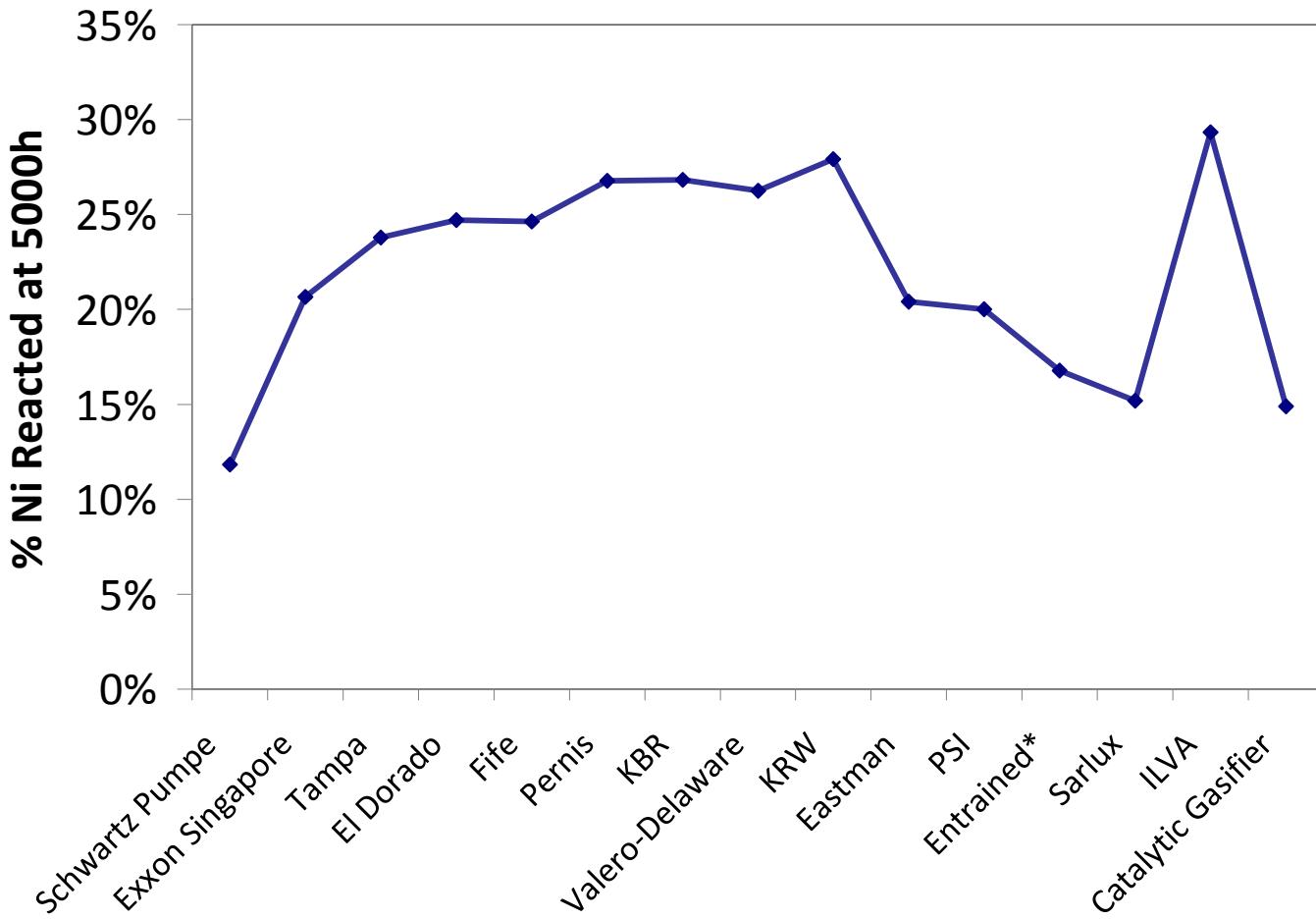
# Results for 5000h

(400 deg. C cleanup; 800 deg. C Anode)



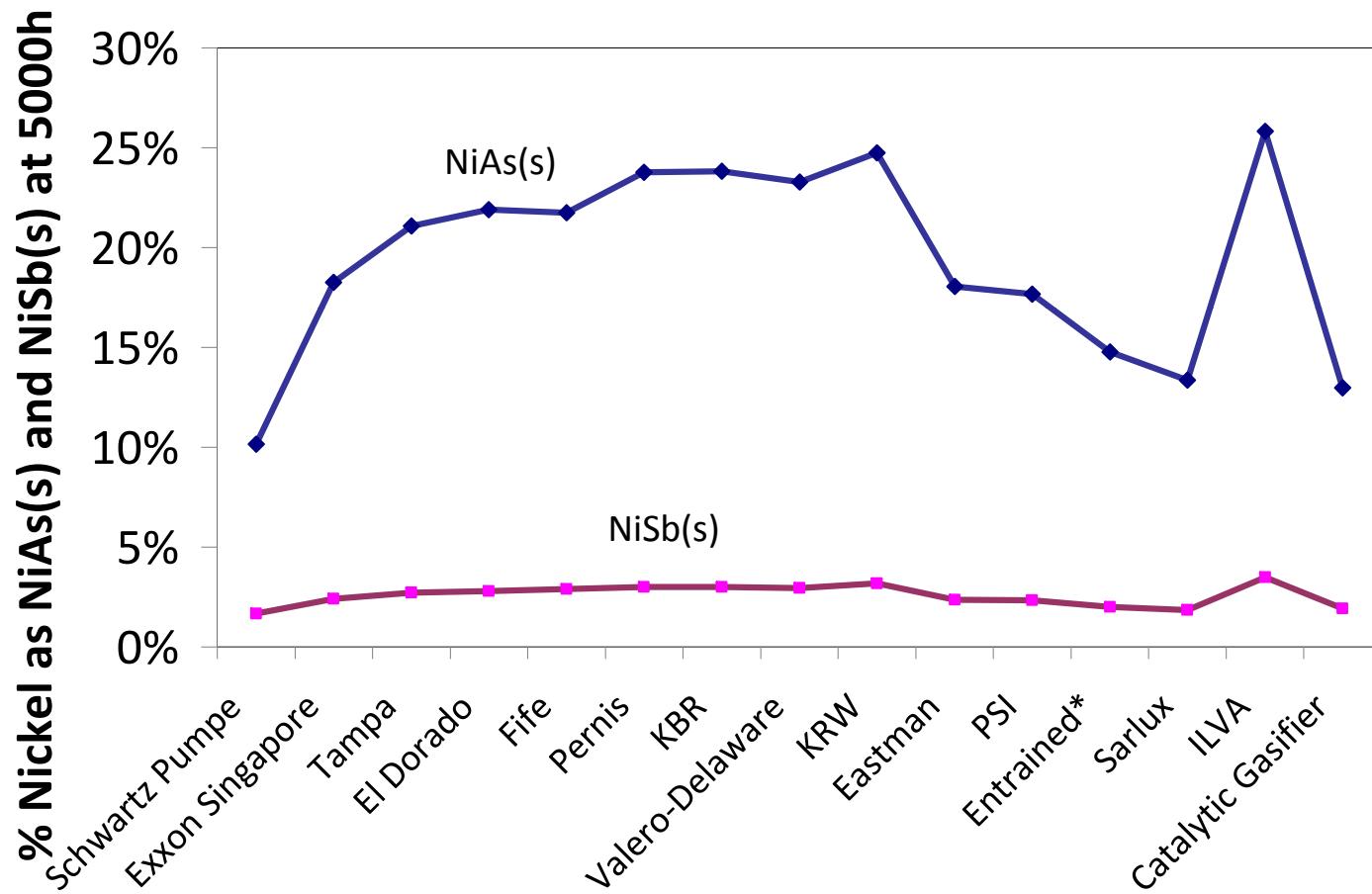
# Results for 5000h

(400 deg. C cleanup; 800 deg. C Anode)



# Results for 5000h

(400 deg. C cleanup; 800 deg. C Anode)



# Analysis Summary

- Detailed thermodynamic analysis method applied to determine behavior of different gasification technology on anode attack.
- Catalytic gasifier approach appears beneficial compared to other technology regarding potential for contaminant attack.
- Several other technologies could also be considered ...their gasification efficiencies need to be evaluated.

# Outline

- **Analysis**
  - Identify potential interactions between trace species and anode across a variety of gasification systems
- **Experimental**
  - Perform individual trace specie evaluations
    - Naphthalene, Benzene, Hg

# Concentrations Tested

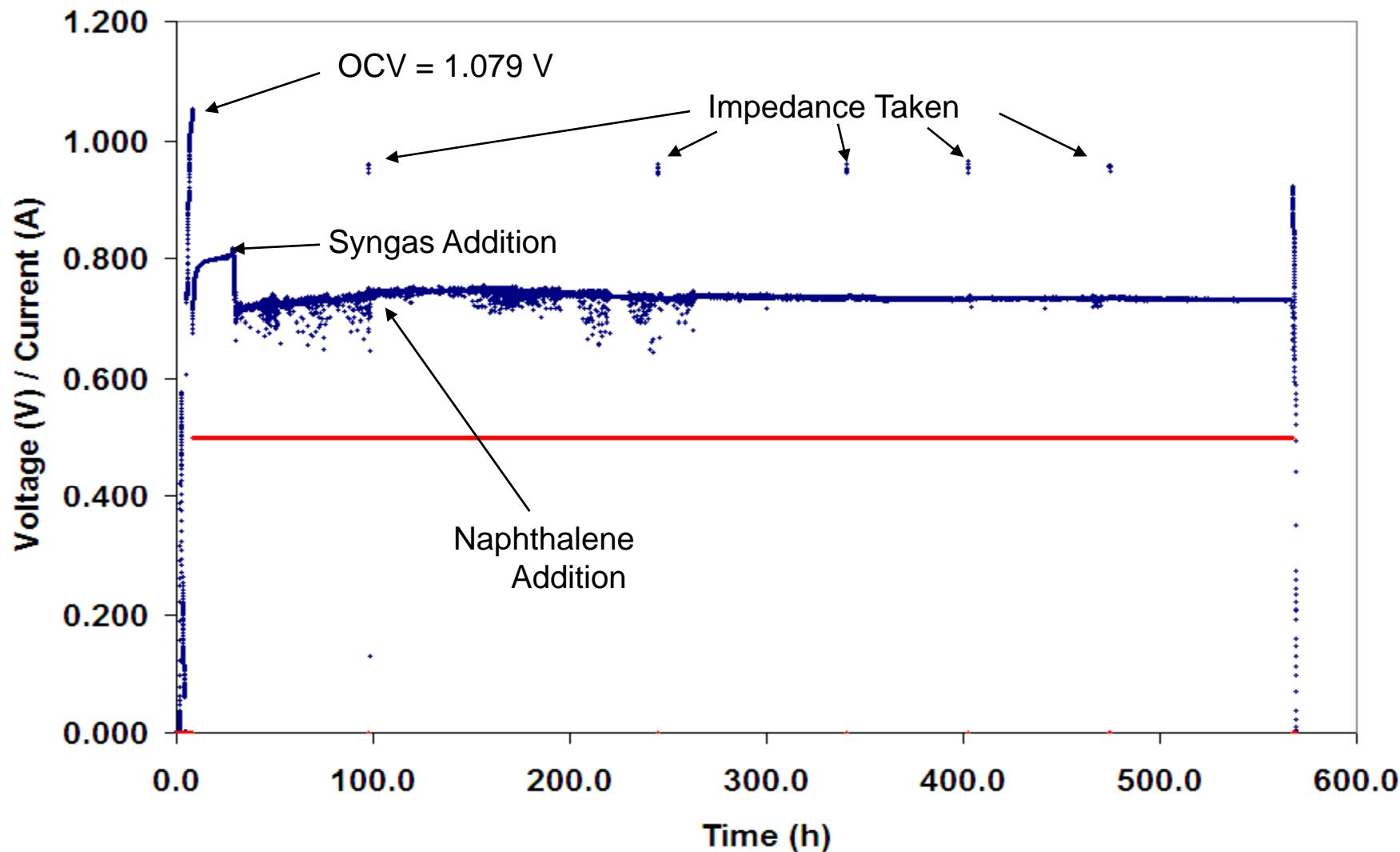
- Overview of contaminant testing and data analysis
- Summary of results
  - Mercury
    - 1 ppm
    - 10 ppm
  - Benzene
    - 15 ppm
    - 150 ppm (in progress)
  - Naphthalene
    - 100 ppm
    - 500 ppm



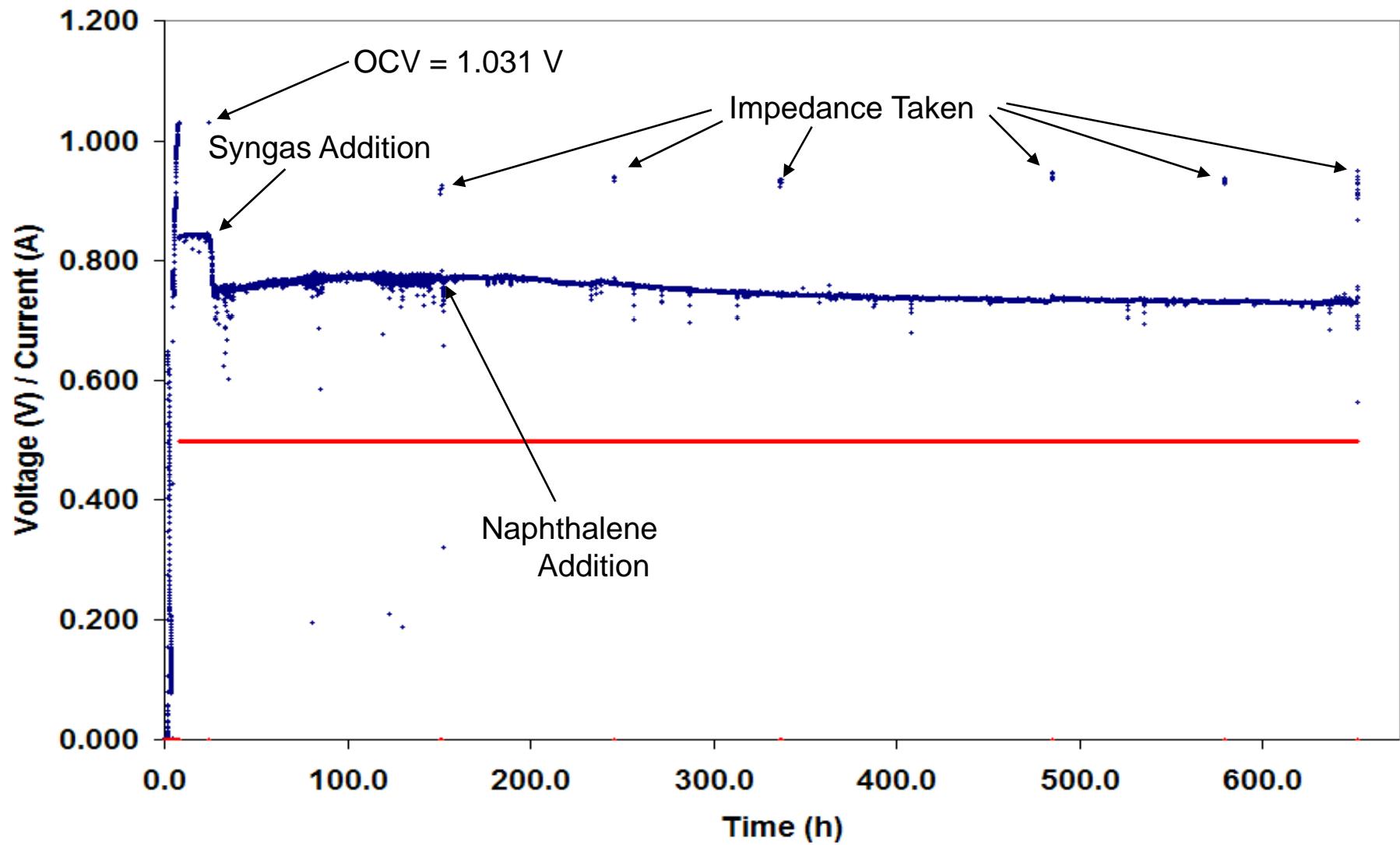
# Test Conditions

- All tests at 800°C and 250 mA/cm<sup>2</sup> load
- Gas mixture is simulated syngas
  - 28.6% CO
  - 29.1% H<sub>2</sub>
  - 27.1% H<sub>2</sub>O
  - 3.2% N<sub>2</sub>
  - 12.0% CO<sub>2</sub>
- Cells equilibrated on 3% H<sub>2</sub>O / bal H<sub>2</sub> under load for over 12 hours, equilibrated on syngas for 48 hours
- Trace contaminant exposure commences after equilibration, 500 hour duration
- Cells ‘quenched’ to preserve trace material, post-operational analysis by SEM/EDS, XRD, XPS

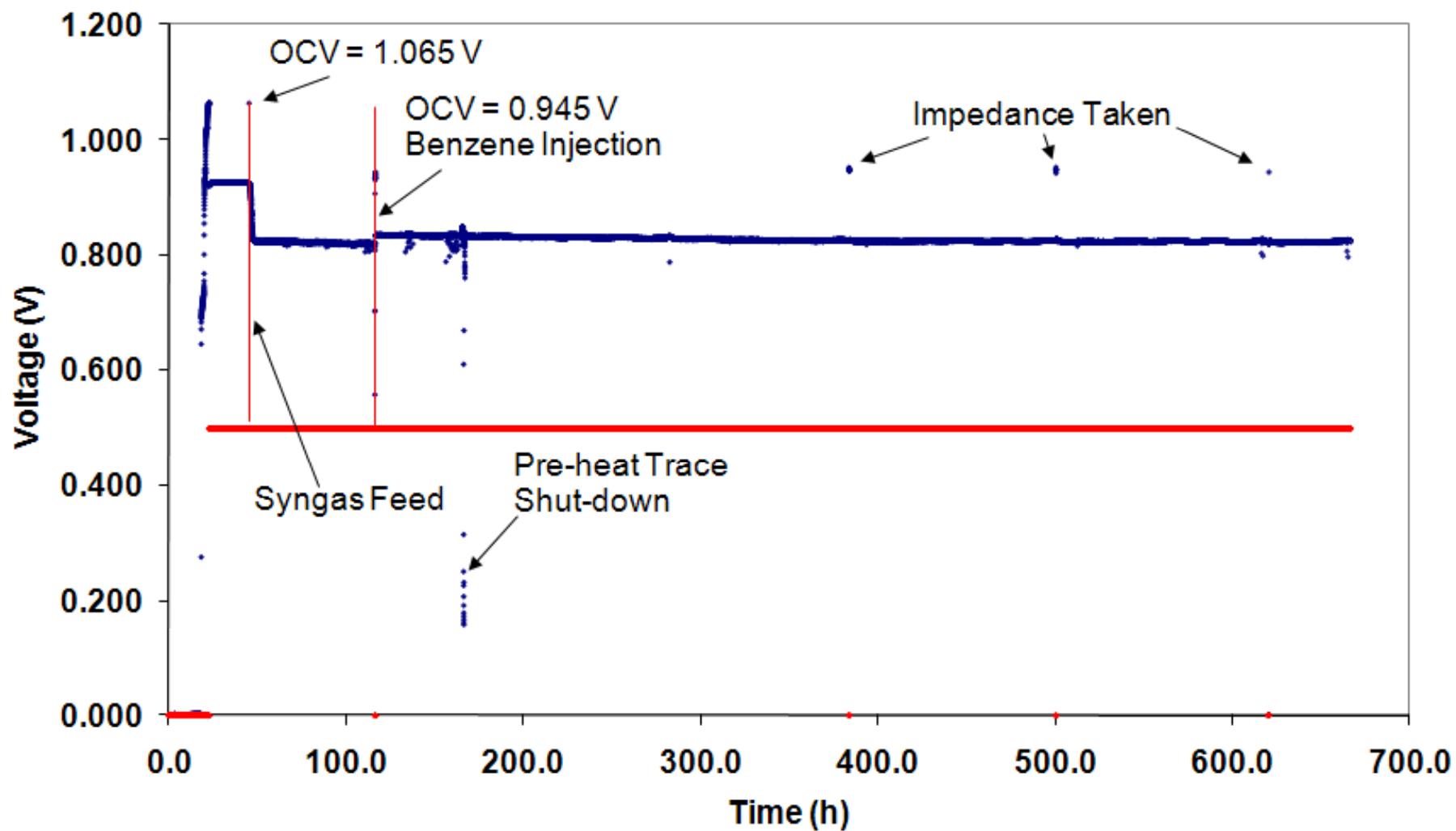
## V-I Response of Button Cell on Syngas Doped with 100 ppm Naphthalene



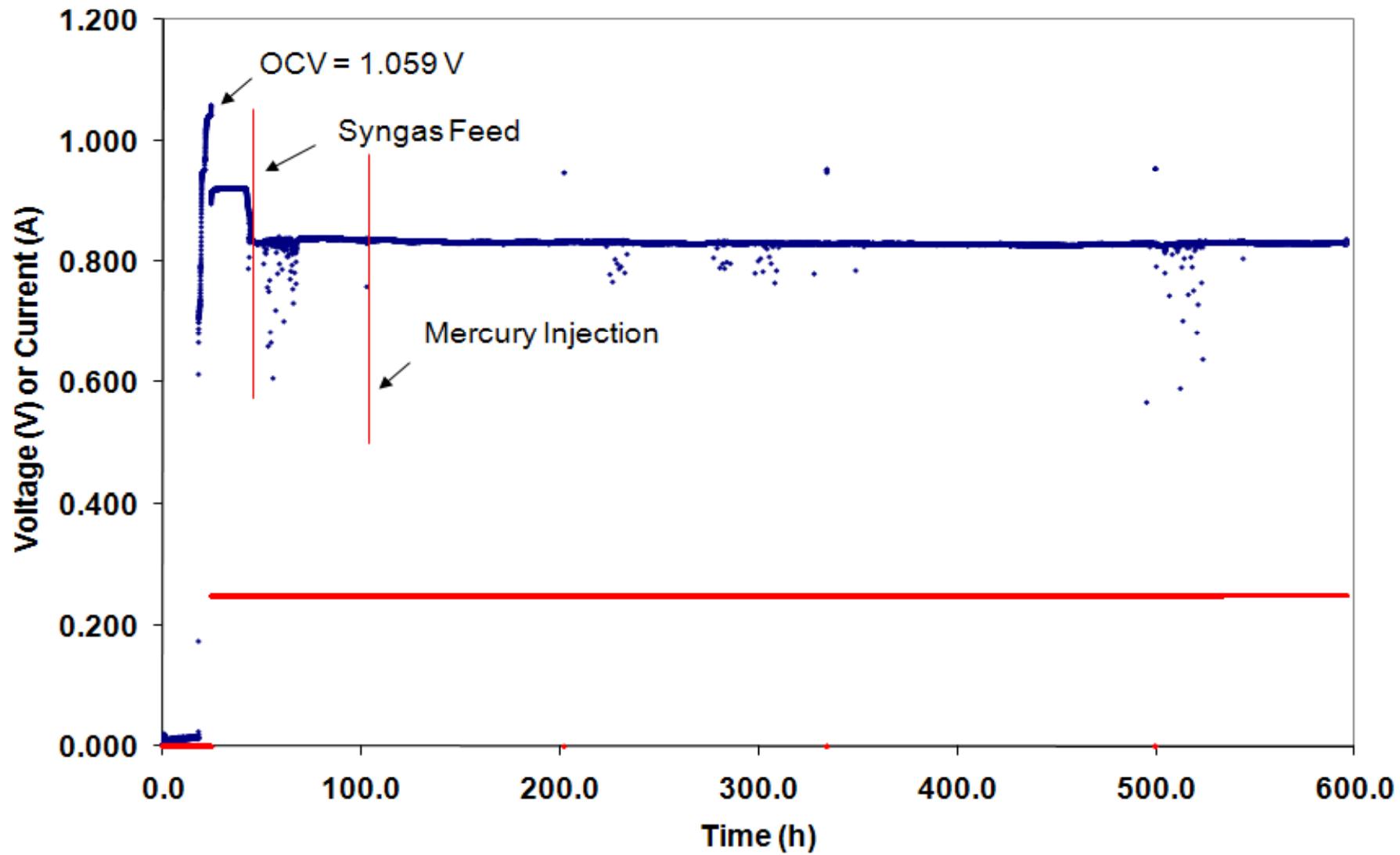
## V-I Response of Button Cell on Syngas Doped with 500 ppm Naphthalene



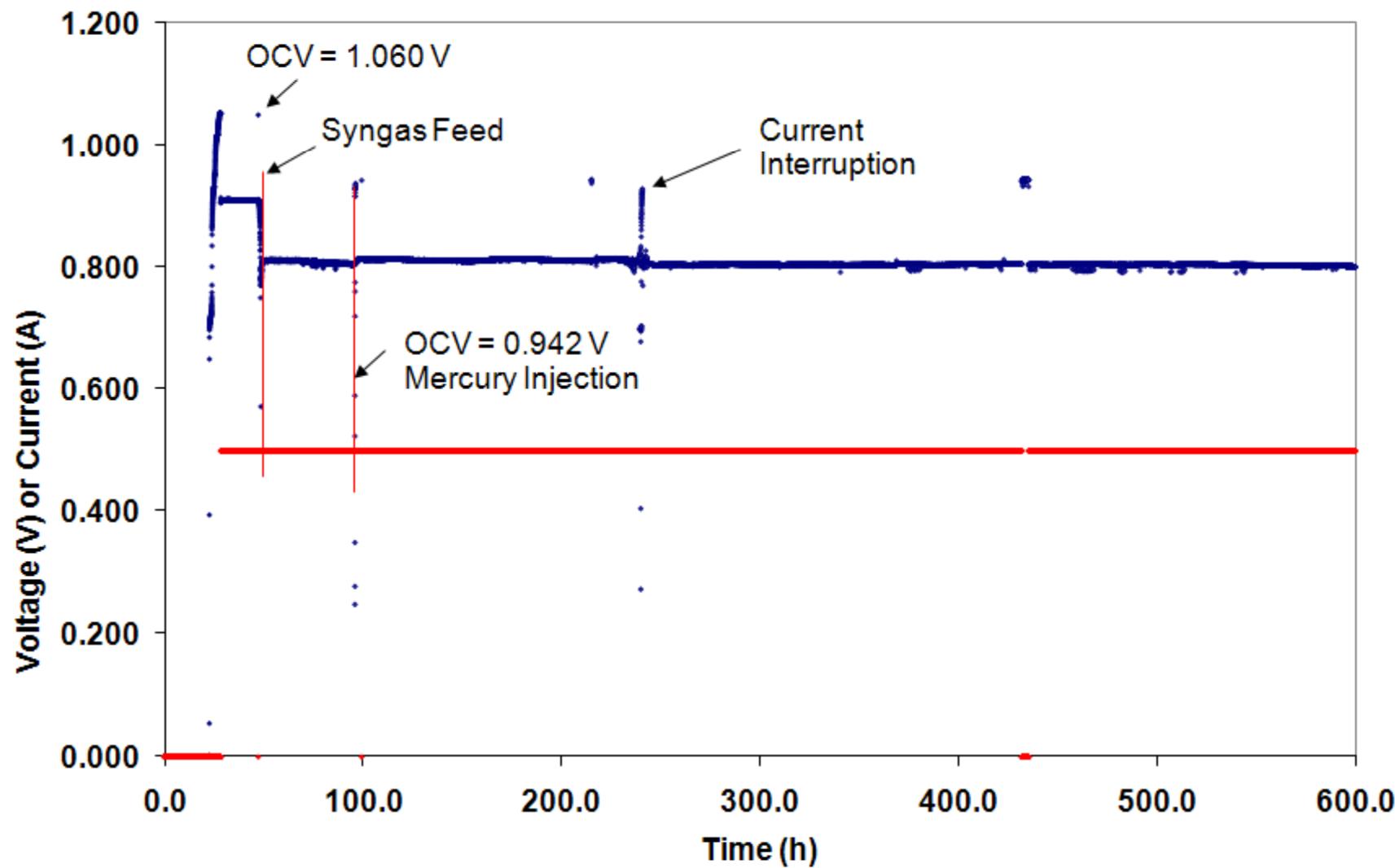
## V-I Response of Button Cell on Syngas Doped with 15 ppm Benzene



## V-I Response of Button Cell on Syngas Doped with 1 ppm Mercury

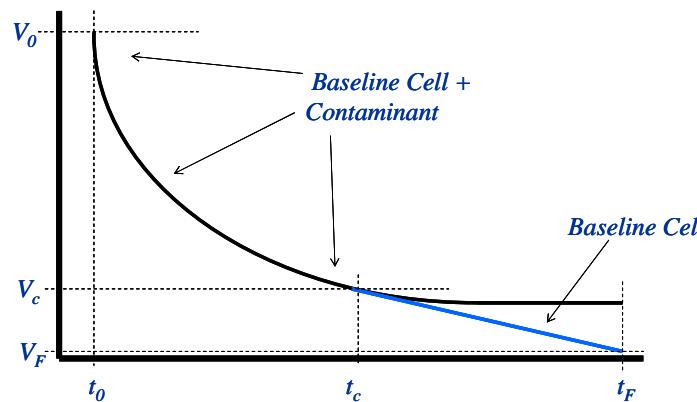


## V-I Response of Button Cell on Syngas Doped with 10 ppm Mercury



# Observed Behavior

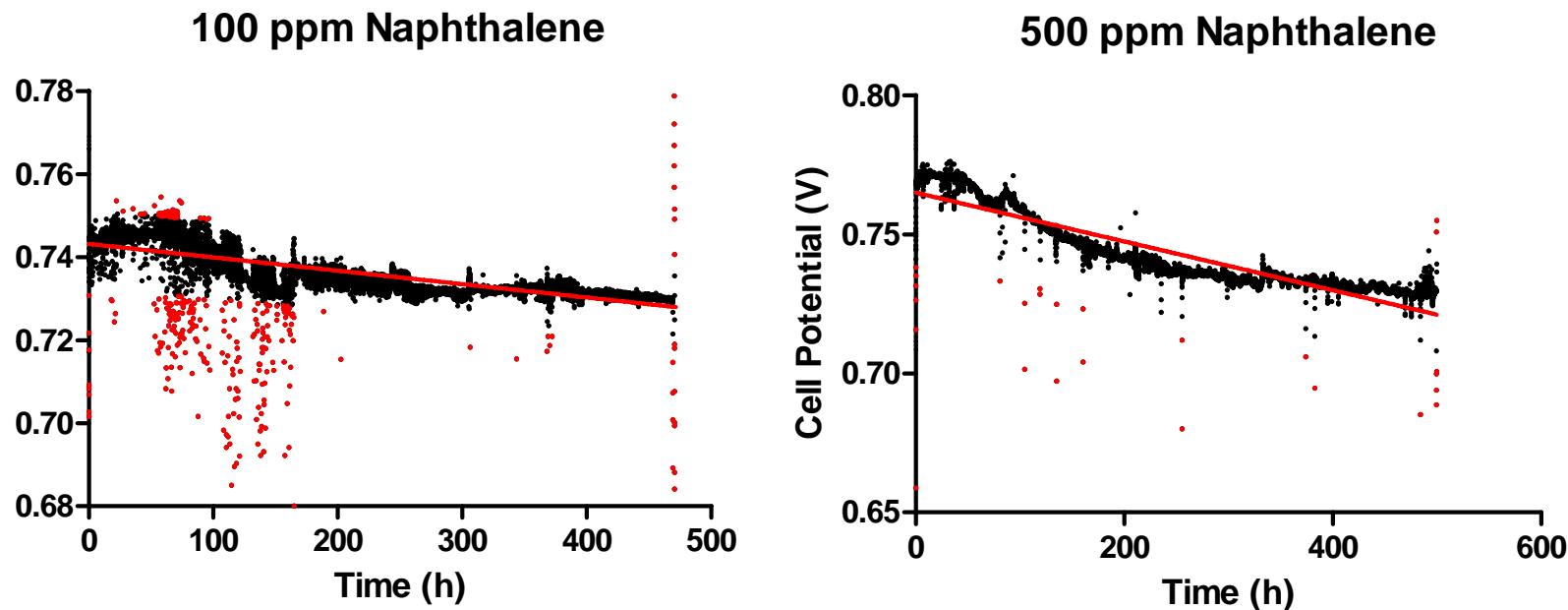
- Two-phase decay expected
  - Phase 1:
    - Exponential decay model applied from  $t_0$  to  $t_c$
    - $t_c$  determined at instantaneous decay rate of baseline cell (e.g., 1% / 1000 hours)
  - Phase 2:
    - Linear decay applied from  $t_c$  to  $t_{final}$
    - Linear decay rate of baseline cell (1.0%/1000 hours)



# Statistical Data Analysis

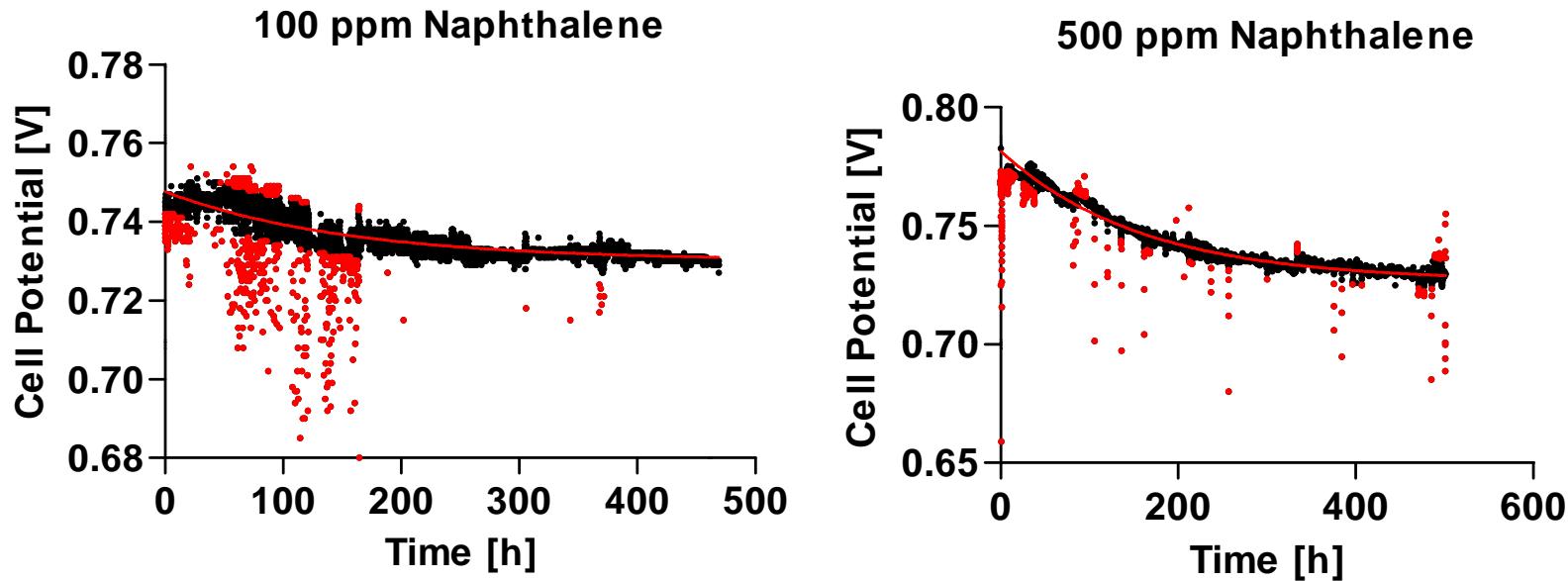
- Data are used to fit an **exponential or linear decay equation** by minimizing the least squares difference through non-linear regression (PRISM)
- Comparisons between ‘all data’ and ‘data with outlier removal’

# Naphthalene Summary – Linear Decay Approach



Conc [ppm]	Case	y-int	slope	R <sup>2</sup>	Ave. Deg [% khr <sup>-1</sup> ]
100	all data	0.743	-3.11E-05	0.2150	4.19
100	outliers removed	0.743	-3.26E-05	0.7227	4.39
500	all data	0.765	-8.69E-05	0.6370	11.36
500	outliers removed	0.765	-5.91E-05	0.8599	7.73

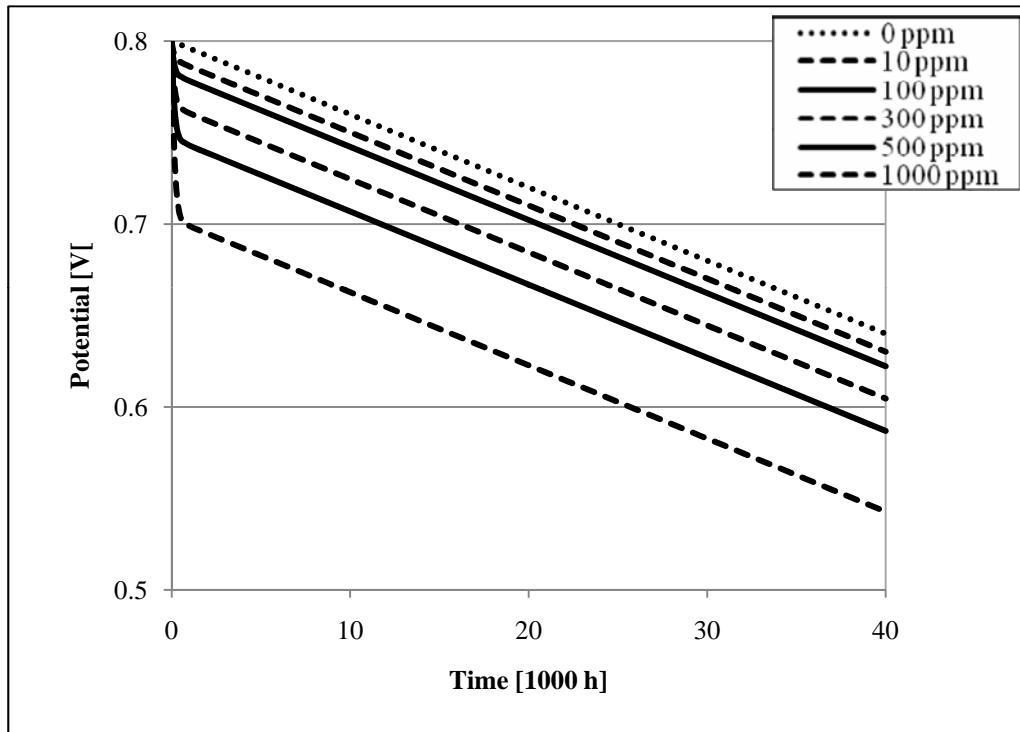
# Naphthalene Summary – Two-phase Decay



Conc [ppm]	Case	V[V] @ t=0	t <sub>c</sub> [h]	V[V] @ t=40khr	Ave. Deg [% khr <sup>-1</sup> ]
100	all data	0.748	408	0.442	1.023
100	outliers removed	0.748	427	0.442	1.024
500	all data	0.778	654	0.441	1.082
500	outliers removed	0.782	598	0.441	1.089

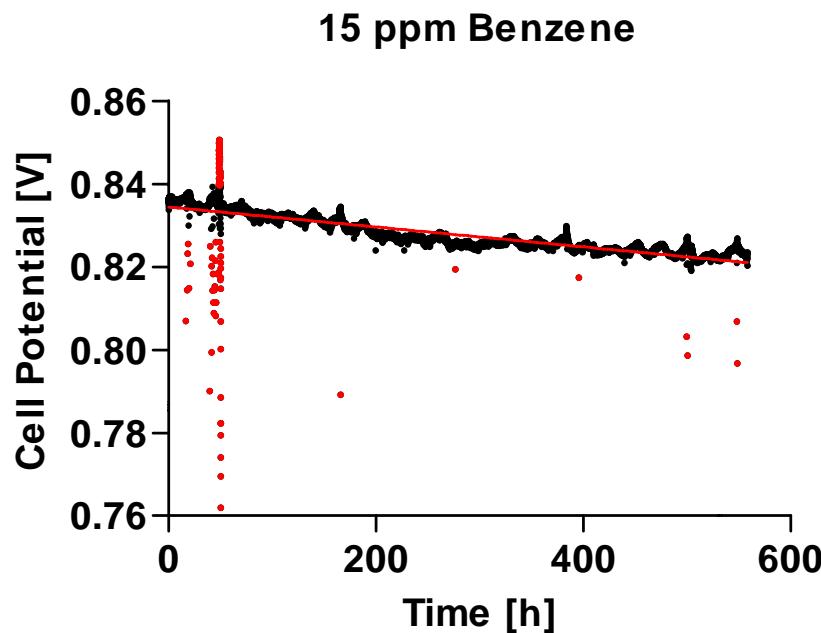
# Predicted Naphthalene Cleanup Targets

*Based upon 0.50% per 1000 h  
Baseline Cell Degradation*



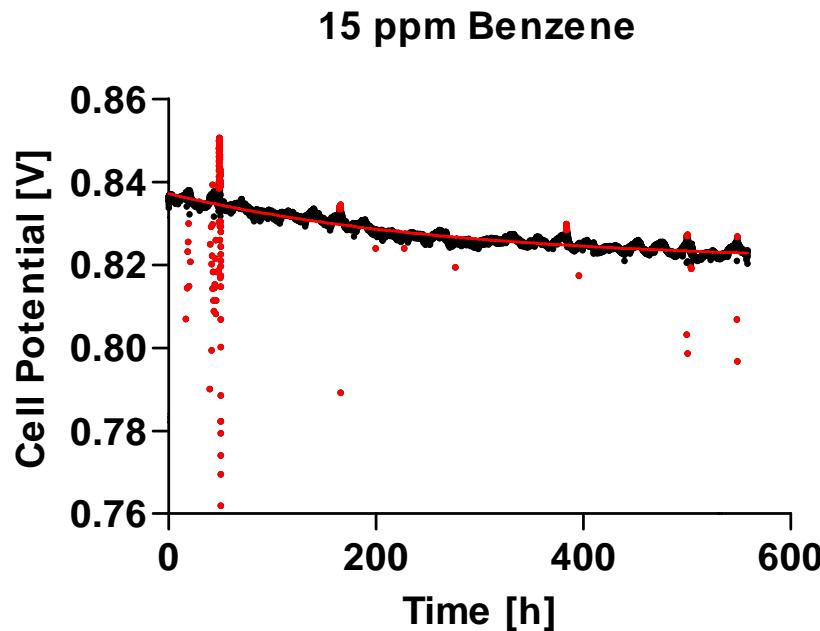
A baseline cell degradation of 0.50% allows a conc. of 360 ppm to produce 0.6 V after 40,000 h of operation.

## Benzene Summary – Linear Decay Approach



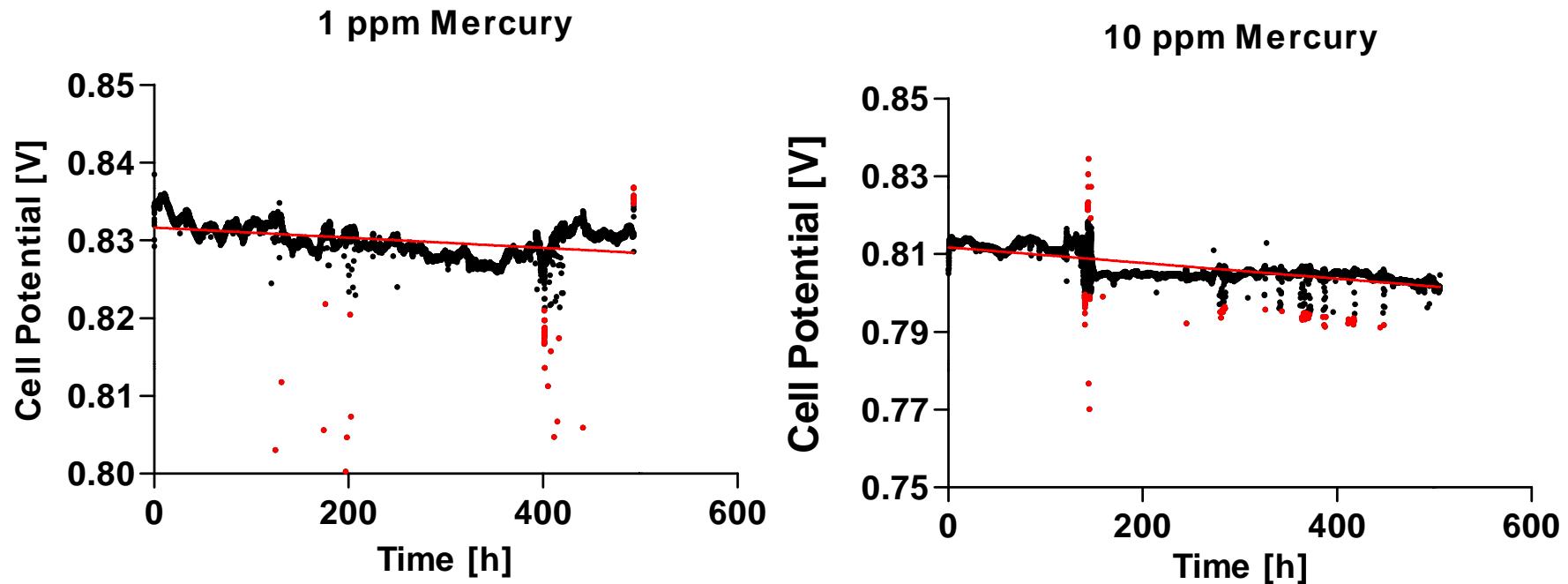
Conc [ppm]	Case	y-int	slope	R <sup>2</sup>	Ave. Deg [% khr <sup>-1</sup> ]
15	all data	0.834	-2.53E-05	0.0345	3.035
15	outliers removed	0.834	-2.40E-05	0.8817	2.880

## Benzene Summary - Two-phase Decay



Conc [ppm]	Case	$V_0$ [V]	Tc [h]	$V_F$ [V]	Ave. Deg [% khr <sup>-1</sup> ]
15	all data	0.835	1285	0.497	1.011
15	outliers removed	0.837	519	0.498	1.012

# Mercury Summary – Linear Decay Approach



Conc [ppm]	Case	y-int	slope	R <sup>2</sup>	Ave. Deg [% khr <sup>-1</sup> ]
1	all data	0.832	-6.73E-06	0.0465	0.809
1	outliers removed	0.832	-6.53E-06	0.2266	0.785
10	all data	0.812	-1.63E-05	0.0319	2.012
10	outliers removed	0.812	2.02E-05	0.6473	2.482

## Q4 Testing

- **Collection of baseline cell degradation data**
- **Complete second mercury test at 1 ppm**
- **Repeat 150 ppm benzene test**

# Individual Contaminant Summary

- **Mercury effect is small relative to the base cell degradation**
  - Mercury exposure is 10-1000 times greater than raw syngas
- **Naphthalene exposure initially accelerates degradation**
  - Degradation rate slows as test progresses
  - Methods for predicting cleanup targets are under development
- **Benzene exposure initially accelerates degradation**
  - Degradation rate slows as test progresses
  - 150 ppm exposure test pending
- **Results valid for conditions tested**
  - Postulated to be sensitive to current density and temperature

