Improving the Performance of Creep-Strength-Enhanced Ferritic Steels

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Purpose is to build fundamental understanding needed to increase operating temperatures

Specific goals include:

- Improving the structural performance of creep-strengthenhanced ferritic steels (9-12Cr-Mo steels)
- Provide science-based guidelines for maximizing safe operating temperatures
- Understand the fundamental causes of current temperature limitations
- Develop approaches for increasing practical operating temperatures



Activities combine basic & applied R&D with strong power industry interactions

- CRADA with Alstom Power, Inc. "Analysis of Off-Normal Metallurgical Conditions on the Performance of Advanced Cr-Mo Steels"
- Collaboration with National Institute for Materials Science (NIMS), Japan - "*Mechanisms of Type IV Weld Failures in Cr-Mo Steels*"
- Involvement with materials issues relating to the ASME Boiler and Pressure Vessel Code (Section II: Materials)
- Technical support for DOE/OCDO Ultrasupercritical Steam Boiler Consortium not included in defined ORNL Tasks
- MOA with Central Research Institute of Electric Power Industry (CRIEPI), Japan - "Joint Research on Properties of Alloy 263 and 263 Weldments"



Milestones/Progress:

- FY2009
 - Complete design of a furnace and a plan to install it on a loading frame at the High-Flux Isotope Reactor neutron diffraction beam line

Status: Suspended due to funding constraints

 Prepare a technical paper manuscript or CRADA report related to control of alloy composition and heat treatment Status: On-schedule



Long-time properties may not meet projections from short-time data



- Type IV failure of Cr-Mo steel welds is due to weakened microstructures in HAZs
- Unexpected behavior that causes unscheduled, premature utility outages



Experimental 9Cr steels developed at NIMS appear resistant to Type IV failure



N130B: 0.077C-0.49Mn-0.30Si-8.97Cr-0.046Nb-0.18V-

2.87W-2.91Co-0.0015N-0.013B

P92 (ref.): 0.09C-0.47Mn-0.16Si-8.72Cr-0.06Nb-0.21V-

1.87W-0.45Mo-0.050N-0.002B

Key features of N130 B – low N, high B



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Heating to low peak temperatures transformed P92 rapidly to high fraction of austenite



• Result: 15% untransformed α , 22% new α , 60.4% new α' , 2.3% γ

Heating to low peak temperatures retained a high fraction of untransfomed α in N130B



• Result: 56% untransformed α , 21% new α , 23% new α' , 0% γ



Microstructures were consistent with diffraction data at low HAZ peak T's

N130B



- $T_{Peak} = 911^{\circ}C (A_3 = 860^{\circ}C)$
- 56% untransformed α , 21% new α , 23% new α' , 0% γ
- *H_V* = 2.57 GPa



- $T_{Peak} = 896^{\circ}C (A_3 = 893^{\circ}C)$
- 15% untransformed α, 22% new α, 60.4% new α', 2.3% γ
- *H_V* = 4.02 GPa



Carbide dissolution in N130B was also sluggish



	Predicted M ₂₃ C ₆ Composition, at%								
Alloy	Fe	Cr	Со	Mn	Мо	V	W	В	С
N130B	23.3	53.1	0.3	0.6		0.6	1.4	3.9	16.8
P92	21.6	50.8		0.8	3.5	0.6	2.1	0.08	20.6

Summary:

- For low HAZ peak temperatures, < ~ 980°C, neither steel transformed completely to austenite
 - Both contained untransformed ferrite with greater amounts in N130B
 - During cooling, new ferrite appeared in both
 - For similar conditions, N130B contained lesser amounts of new martensite
- For similar conditions, N130B retained less γ (if any)
- Dissolution of M₂₃C₆ in N130B was also sluggish, possibly due to B content

Do these differences influence properties? How? Why?



Milestones/Progress:

- FY2010
 - Initiate creep testing of specimens subjected to simulated heat-affected zone heat treatments during synchrotron diffraction
 - Status: On-schedule
 - Heat treatments/diffraction experiments are complete
 - Data is being analyzed
 - Preferred creep specimen geometry is under discussion



CSEF steels must be heat treated as specified to achieve desired properties

- CRADA with Alstom Power, Inc. "Analysis of Off-Normal Metallurgical Conditions on the Performance of Advanced Cr-Mo Steels"
 - Can these heat treatments be accepted without compromising creep properties of 9Cr steel :
 - Tempering for exceptionally long times (100 h-vs-2 h)?
 - Tempering in α + γ phase field under any circumstances?
 - Slowly cooling from austenitizing temperatures in N + T?
 - Holding metal for long times at ~ 500°C during cooling from normalizing treatments?
 - How does one know these have *not* been done?



Real-time diffraction from 9Cr steel Ht 30176 during slow cooling from 1050°C



- Austenite begins transforming to ferrite between ~ 770-870°C
- Result is martensite + ferrite rather than ferrite
- Creep properties are not likely to be as desired



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Creep-fatigue loading dramatically reduces life of nickel-based alloys



(a) Aged, 750°C, 216hr



(c) Creep, 750°C, 180MPa, 3013.1hr



(b) Fatigue, 750°C, 0.7%, 2070Cycles



(d) Creep-fatigue, 750°C, 0.7%, TH6min, 737Cycles 200μm

 MOA with Central Research Institute of Electric Power Industry (CRIEPI), Japan -*"Joint Research on Properties of Alloy 263 and 263 Weldments"*



Rotation of atomic planes near grain boundaries increases strain concentration



- 15 degrees rotation within 10 microns from GB in creep-fatigue condition
 - High dislocation density
 - High mismatch of strain
- Concentration of "creep deformation" near the GB is likely cause of remarkably low life, intergranular failure in C-F conditions

Source: Dr. Masato Yamamoto, CRIEPI, Japan, from work done at ORNL



Improving Performance of CSEF Steels and Ni-based Alloys

Highlights:

- Using advanced tools like APS to better understand new highperformance alloys
 - Collaboration with NIMS, Alstom CRADA
- Leveraging resources to investigate ways to increase performance of Ni-based alloys
 - Collaboration with CRIEPI
- Using unique capabilities and fundamental understanding to assist ASME and manufacturers in better informed use of CSEF steels and Ni-based alloys
 - Using computational thermodynamic analysis to enable more robust alloy specifications
 - Supporting component design and reliability with testing and analysis of mechanical behavior

