

Brazed Seals

Alternative Sealing Technology for Solid Oxide Fuel Cells



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K. S. Weil, J. P. Choi, and J. Y. Kim

Pacific Northwest National Laboratory
Richland, WA 99352
USA

Pacific Northwest
National Laboratory
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What is Brazing?

Definition: A filler metal is heated to melting and under capillary action fills the gap between the sealing surfaces. When cooled, a solid joint forms.

Braze Filler Metal

Base Metal

Base Metal

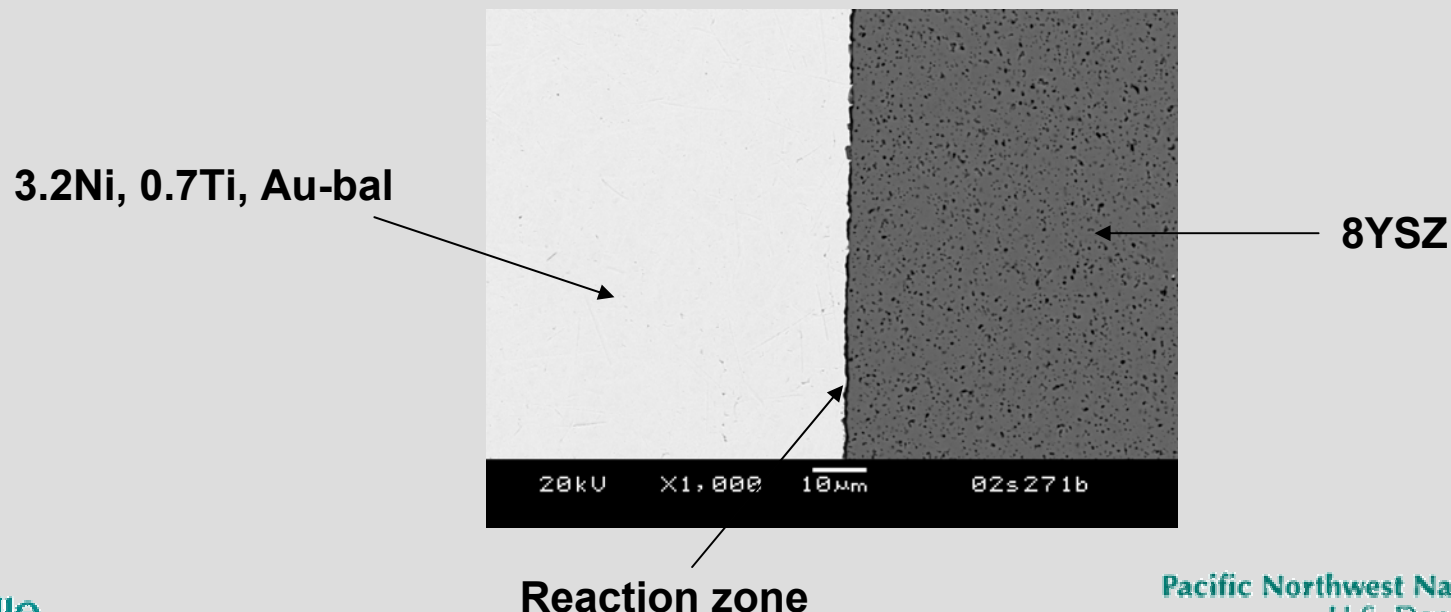
Heat

**Metallurgically
Bonded Joint**

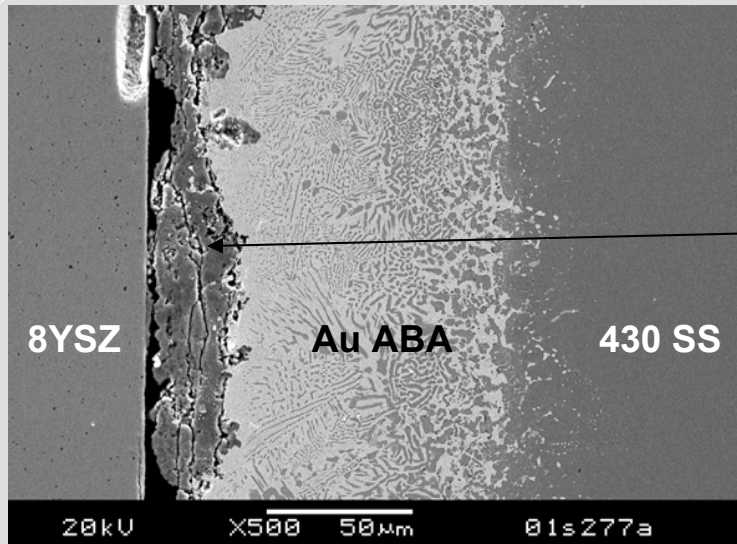
Active Metal Brazing: A specialized technique that employs a reactive element such as titanium to facilitate wetting between the filler metal and a ceramic substrate

Typical Filler Metals: Au-Ni-Ti, Au-Ni-V-Mo, Ag-Cu-Ti, Pd-Ni-V

Process Conditions: Vacuum or inert gas environment
850°C or higher



Joint Oxidation

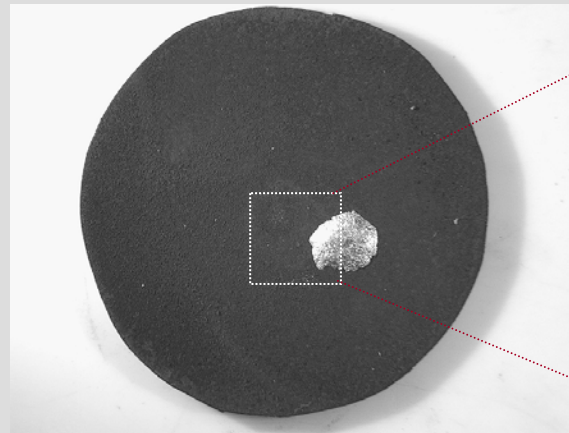


(Cr,Fe)₂O₃ scale formation after 200hrs air exposure at 700°C

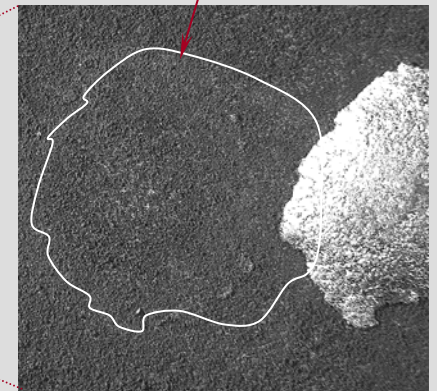
KS Weil and JP Rice, *Scr. Mater.*, 52 (2005) 1081

Cathode Decomposition

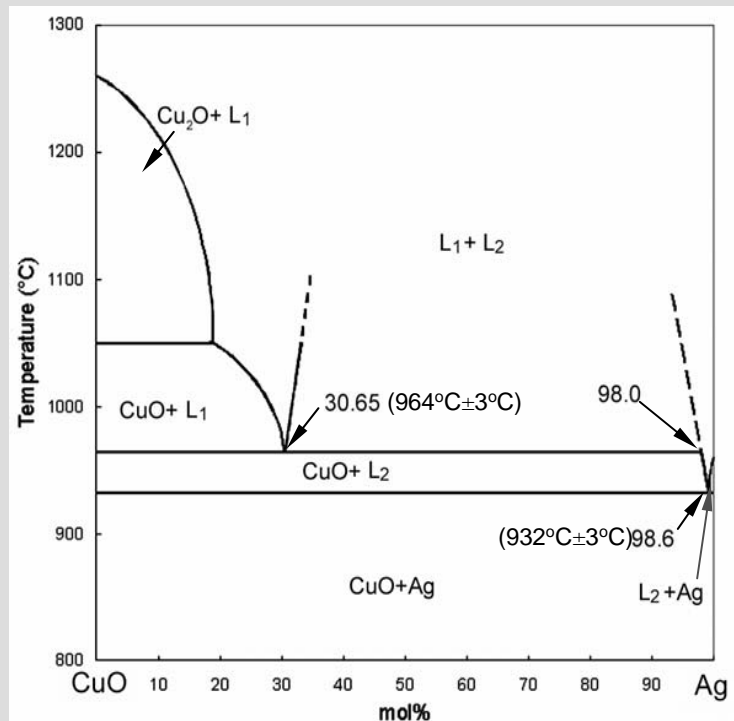
Under vacuum at $T > 700^{\circ}\text{C}$:



Original Braze Position

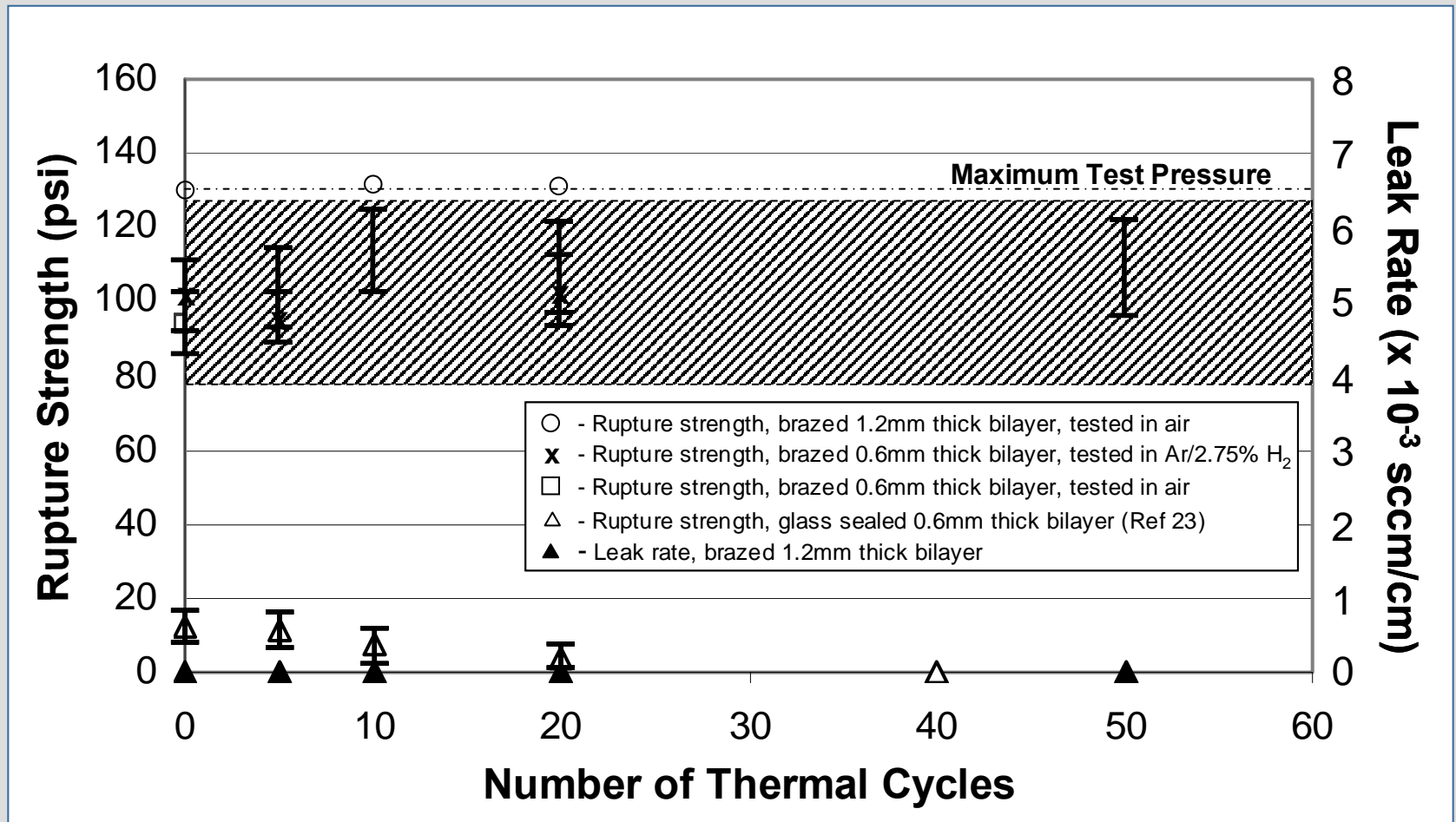


- A new method of ceramic-to-ceramic and ceramic-to-metal joining
- Uses a unique filler metal system: a soluble metal oxide dissolved in a noble metal – e.g. CuO in Ag
 - ▶ Is conducted in open air (i.e. in a simple muffle or continuous belt furnace)
 - ▶ Does not require fluxing or the use of inert cover gas
 - ▶ Confers oxidation resistance and ductility to the joint



Shao et al, *J. Am. Ceram. Soc.* [1993]
2663

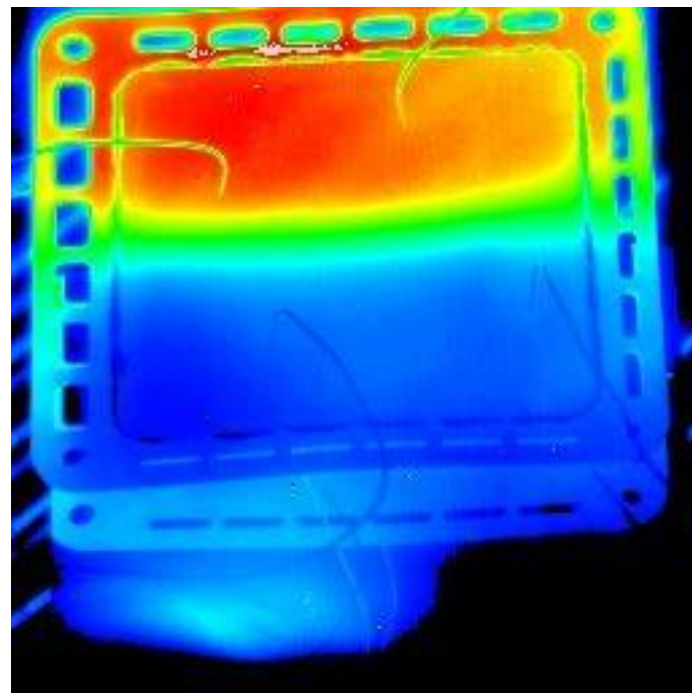
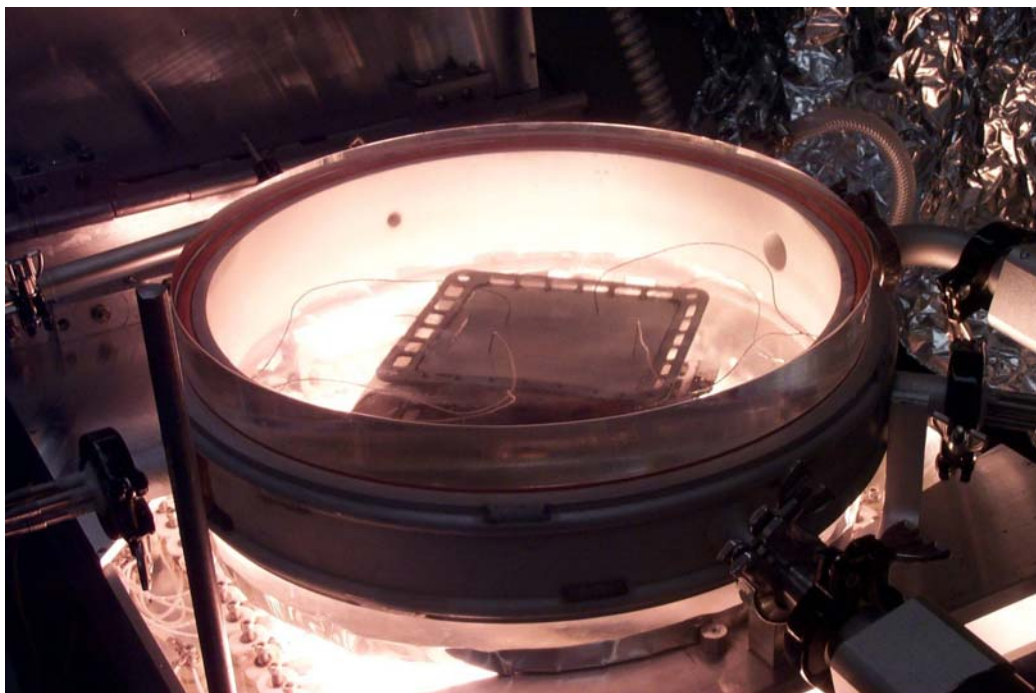
Thermal Cycling (75°C/min, RT → 750°C):



KS Weil, CA Coyle, JT Darsell, GG Xia, and JS Hardy, *J. Power Sources*, 152 (2005) 97

Air Brazing: Joining Scaled-Up Components

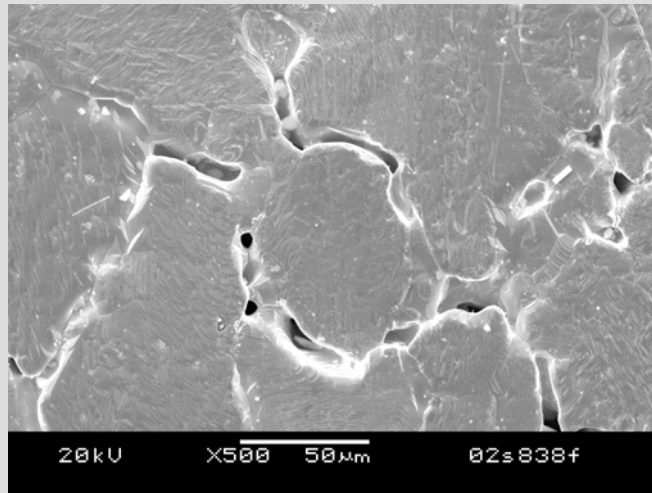
Preliminary testing with full-scale components is very encouraging:



Seal remains hermetic after testing through five thermal cycles

- High-temperature degradation in a dual atmosphere environment

Pure Silver



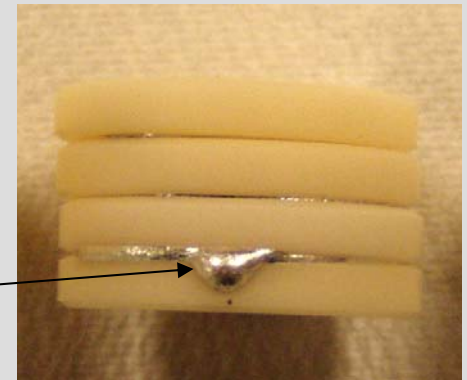
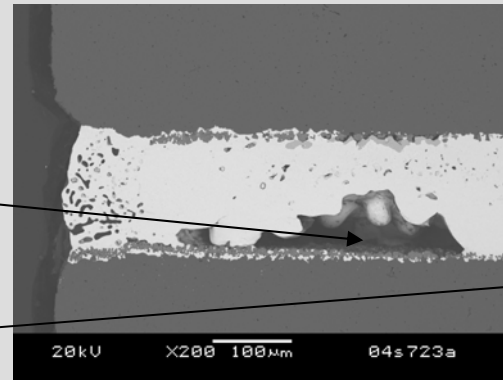
Singh et al., *J. Mater. Eng. Perform.*,
13 (2004) 287

- Process consistency

Pore formation due to poor wetting and/or cooling upon shrinkage

and

“Squeeze-out”

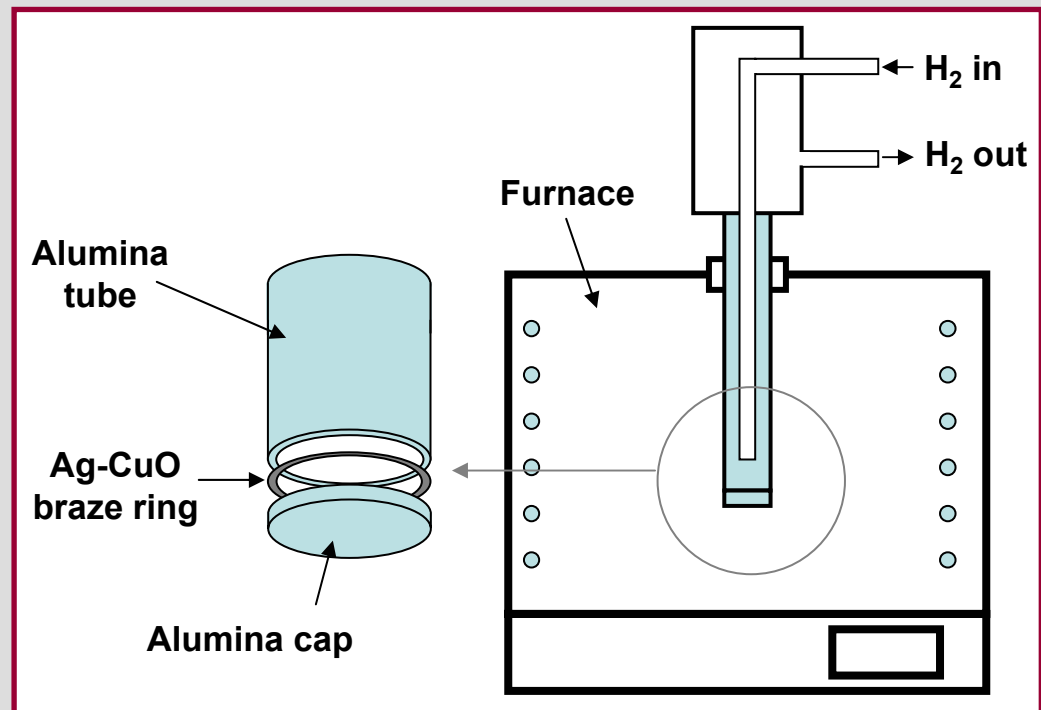


- **Dual atmosphere degradation**
 - ▶ Observed three different types of pore defects – all of which we suspect can be mitigated
 - ▶ Phenomenon is not significant with respect to short-term use (up to 2000hrs) – no loss in hermeticity, but a measurable loss of strength
 - ▶ Could potentially be problematic over longer periods of operation
- **Al-Ag-CuO air braze filler metals are being investigated to eliminate long-term dual atmosphere degradation**
 - ▶ Initial alloy compositions have been successfully synthesized, but require further optimization with respect to joint strength
 - ▶ Observe improved joint strength upon H₂ exposure
 - ▶ Dual atmosphere testing currently in progress
- **New composite filler metal composition (containing Al₂O₃ particulate) looks very promising**
 - ▶ Joint strength equal to that of the base material (Al₂O₃)
 - ▶ Can combine with the Al-alloyed material to develop a very durable air braze filler metal

Dual Atmosphere Degradation: Experiments

- Tube testing – 200 - 2000hr aging tests conducted at 800°C with flowing H₂ inside and flowing air outside
- Examined the following variables: exposure time (200, 1000, and 2000hrs), filler metal composition (Ag₂CuO and Ag₈CuO), and braze temperature (980°C and 1100°C)

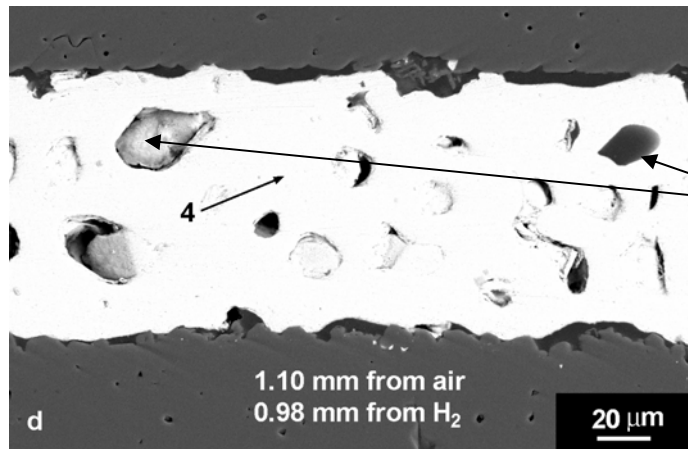
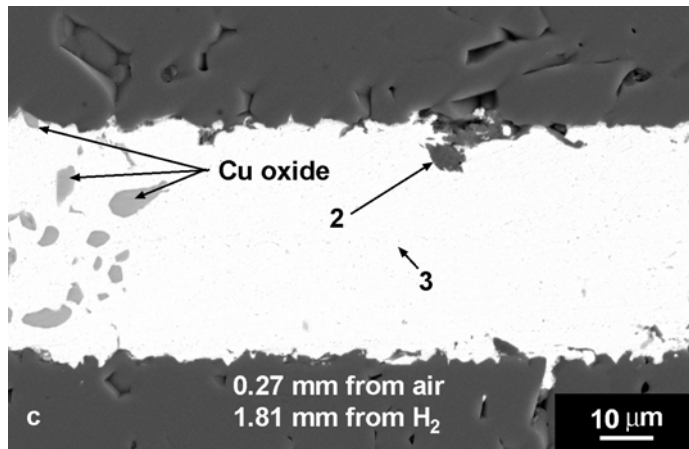
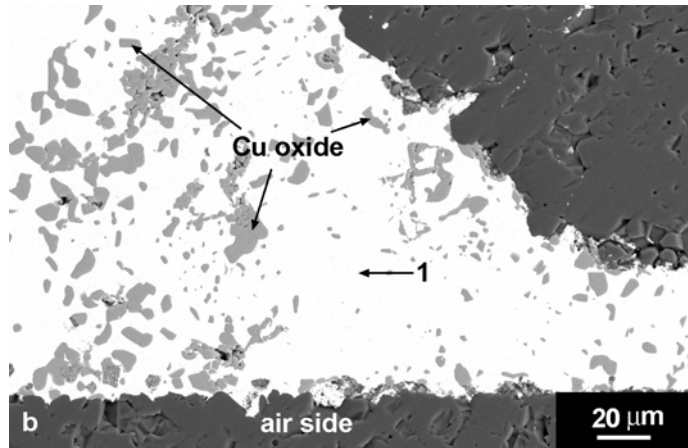
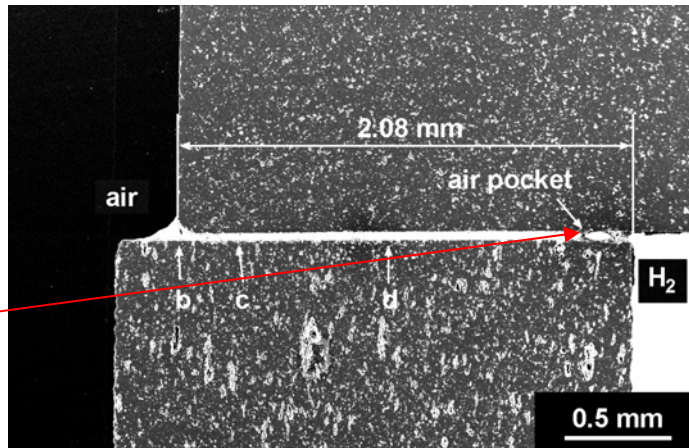
Sealed Tube Exposure Test



- **Three types of pores were found:**
 - ▶ **Air pockets formed during processing (Type 1) - large (mm in size) and often found near the center of the joint**
 - ▶ **Pores (Type 2) formed within 5hrs of exposure due to CuO reduction : $\text{CuO} + 2\text{H}_{\text{diss}} \text{Ag} \rightarrow \text{Cu}_{\text{diss}} \text{Ag} + \text{H}_2\text{O}\uparrow$ - $>5\mu\text{m}$ in size, found first along the boundary exposed to H_2**
 - ▶ **Pores (Type 3) formed around ~2000hrs due to $\text{H}_{\text{diss}} + \text{O}_{\text{diss}} \rightarrow \text{H}_2\text{O}\uparrow$ - sub-micron to micron in size and only found after “extensive” dual atmosphere exposure (within the center of the joint)**
- **In all cases, the porosity remains isolated (not interconnected)**
- **In all cases, the tubes are hermetic at the end of testing**
- **Progression of Type 2 pore front appears to scale with \sqrt{t} fit, which suggests a means of estimating the lifetime of an Ag-CuO seal based on dual atmosphere degradation**

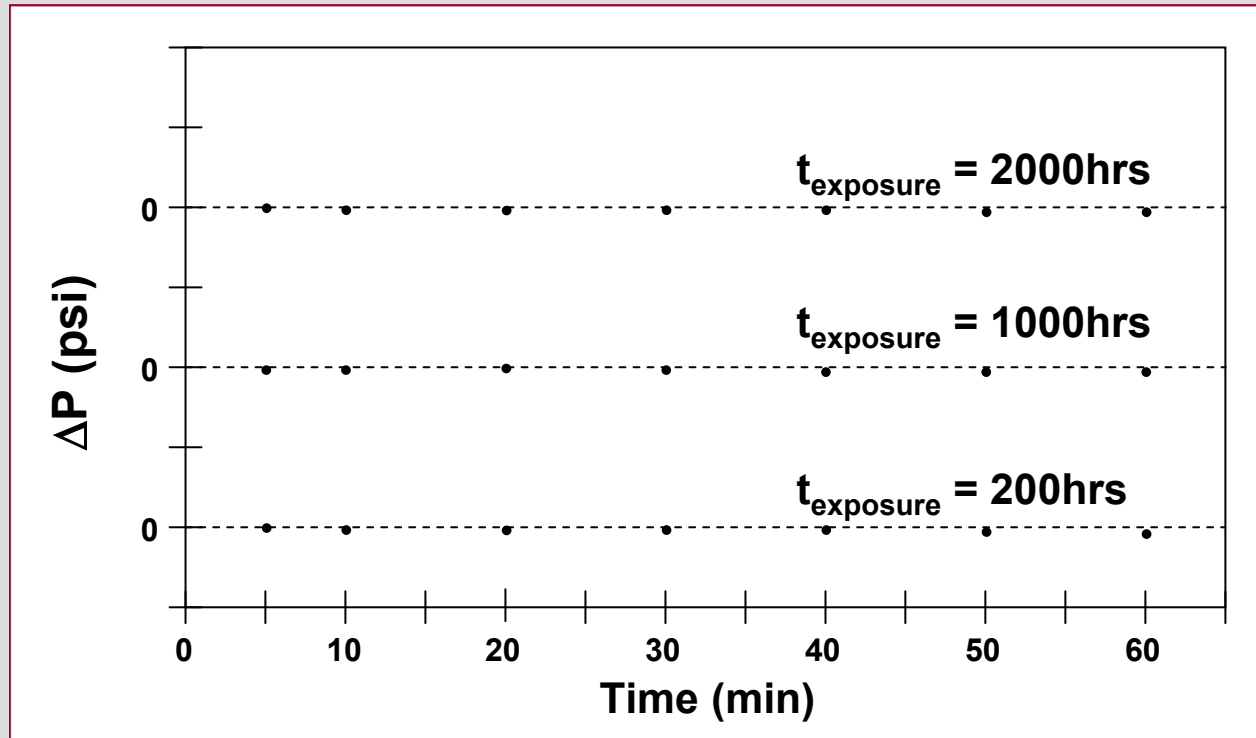
Dual Atmosphere Degradation: Example

Ag8CuO brazed at 980°C; dual atm exposure at 800°C for 1000hrs



Dual Atmosphere Degradation: Hermeticity

Seal hermeticity:



Progression of the Type 2 pore front appears to scale with \sqrt{t} .

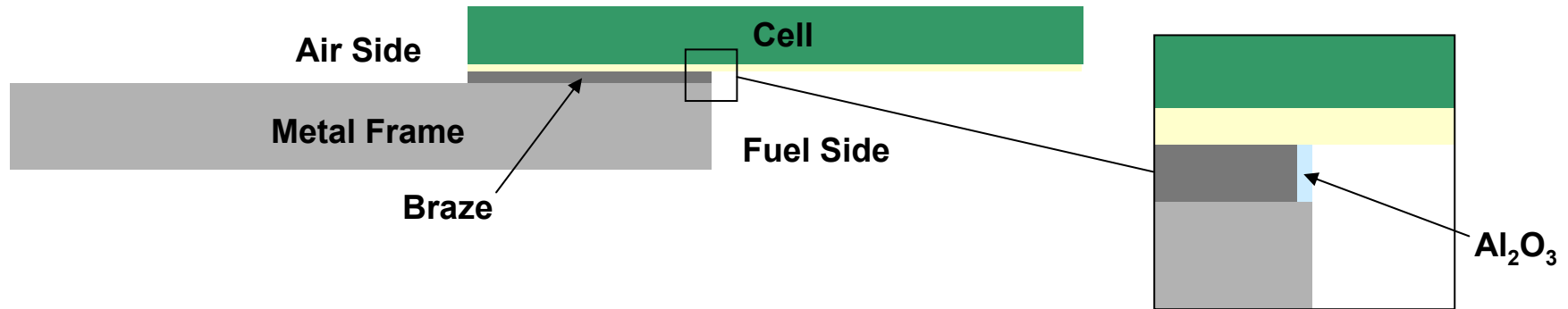
Based on this, we can roughly extrapolate the lifetime of the seal:

$t_{95\% \text{ Degradation}} \sim 5,200\text{hrs at } 800^\circ\text{C and } \sim 12,600\text{hrs at } 750^\circ\text{C}$

\therefore standard filler metal needs to be modified for longer-term use

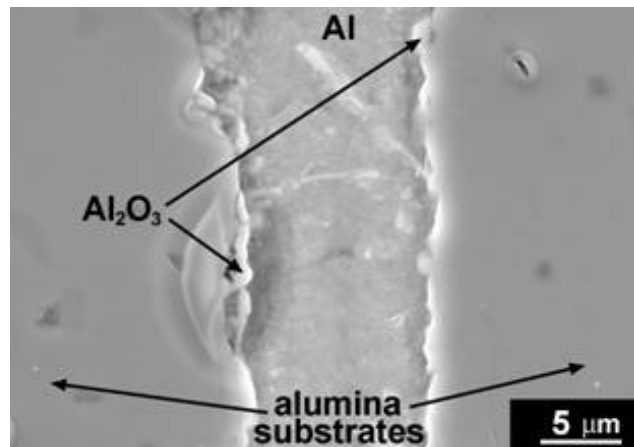
Aluminum Alloying Additions

Concept: develop a passivation layer that inhibits H and O diffusion and eliminates pore Types 2 & 3



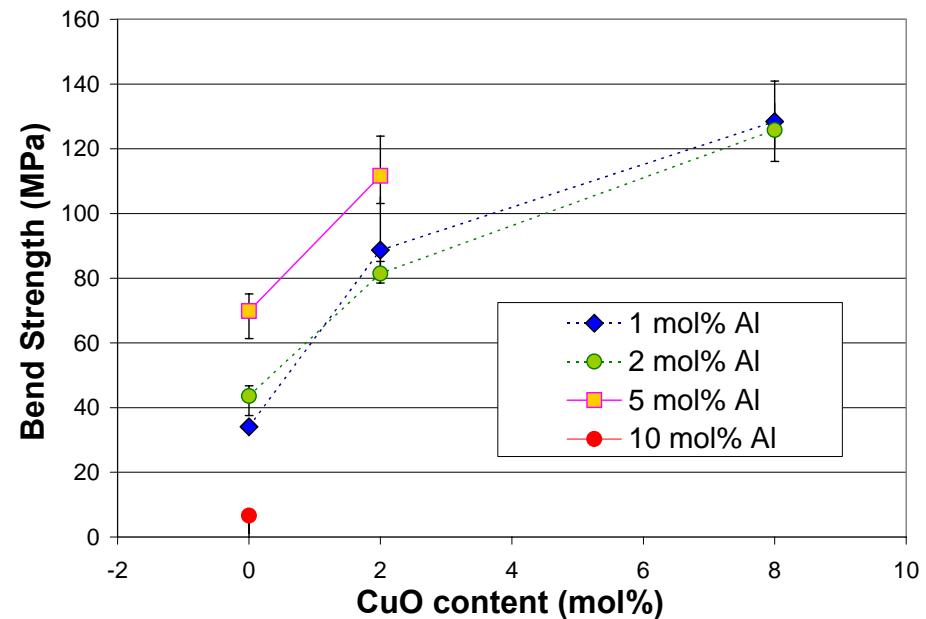
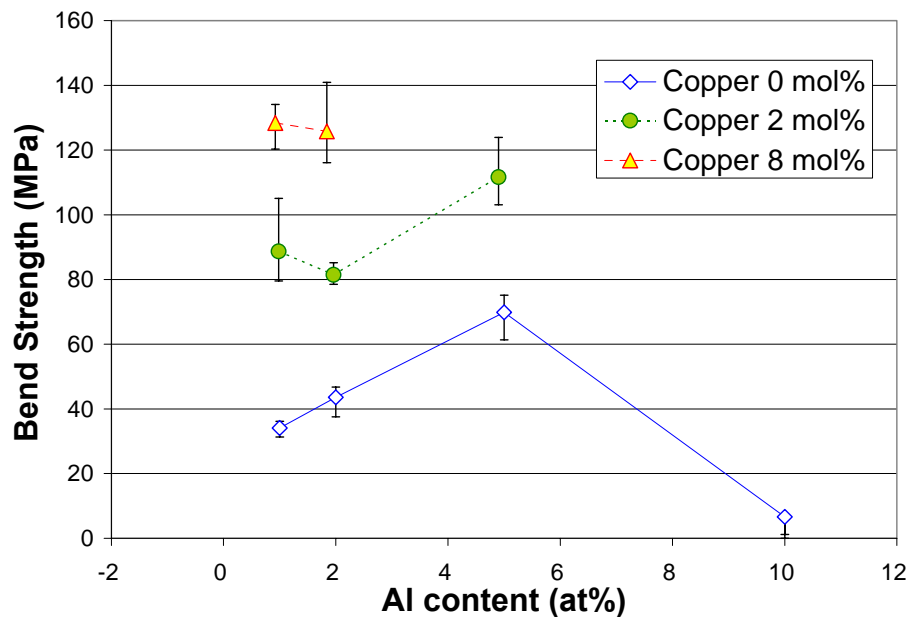
Prior work on $\text{Al}_2\text{O}_3/\text{Al}/\text{Al}_2\text{O}_3$ joining:

1000°C, 10hr, Air:

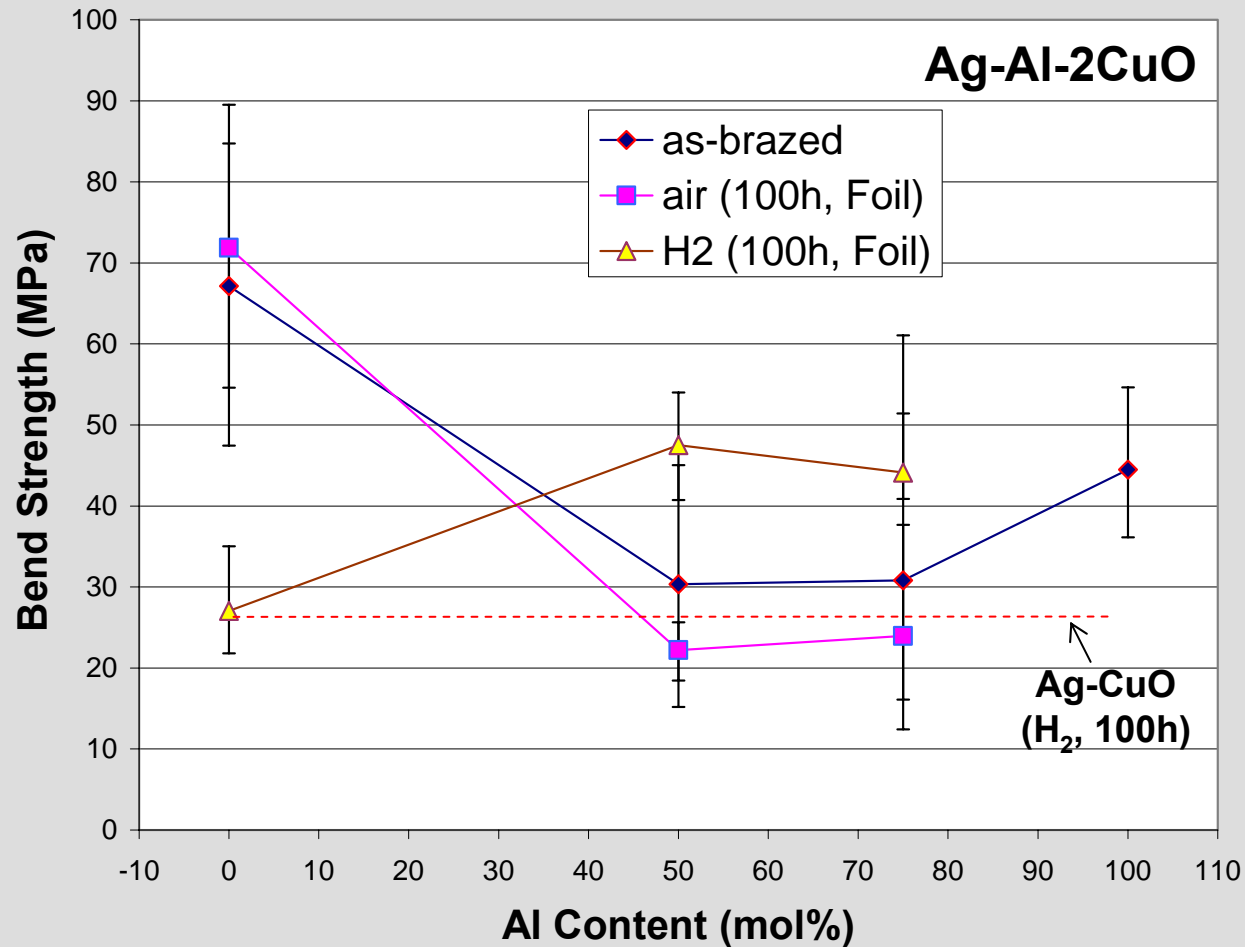


Forms an adherent Al_2O_3 scale that protects the underlying metal

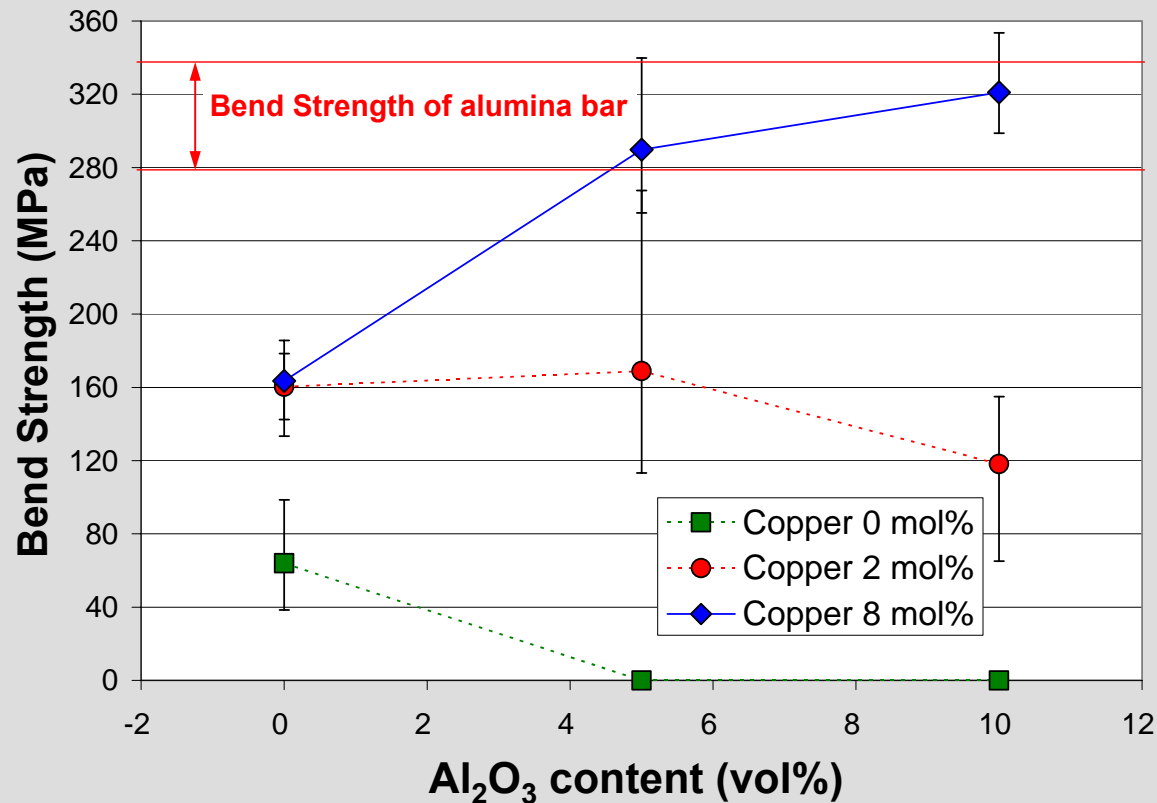
- Started by fabricating Ag-Al binary compositions
- Observed adequate joining, but found poor joint strength
- Turned to the Ag-Al-CuO system



Observe improved strength after H₂ exposure



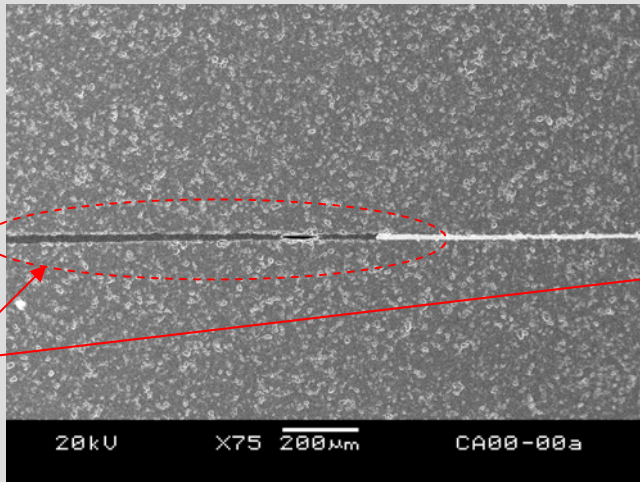
Al₂O₃-modified Ag-CuO Filler Metal



- Alumina addition to high CuO content filler metals leads to a dramatic increase in bend strength. ***The joints are as strong as the ceramic substrate!***
- For no or low CuO, the alumina addition did not improve bend strength

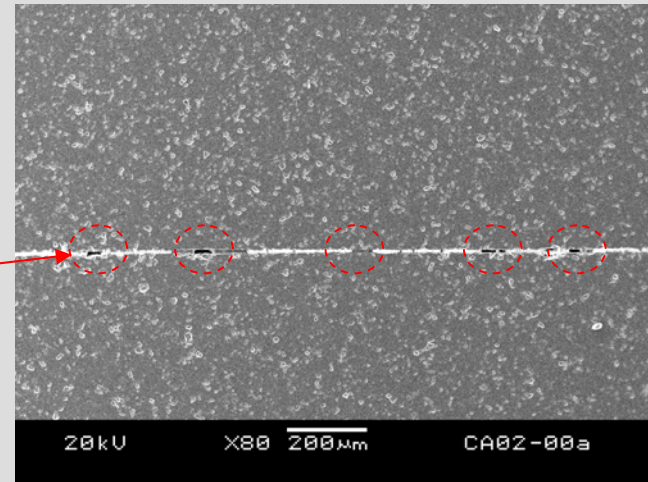
Al_2O_3 -modified Ag-CuO Filler Metal

Ag-2CuO

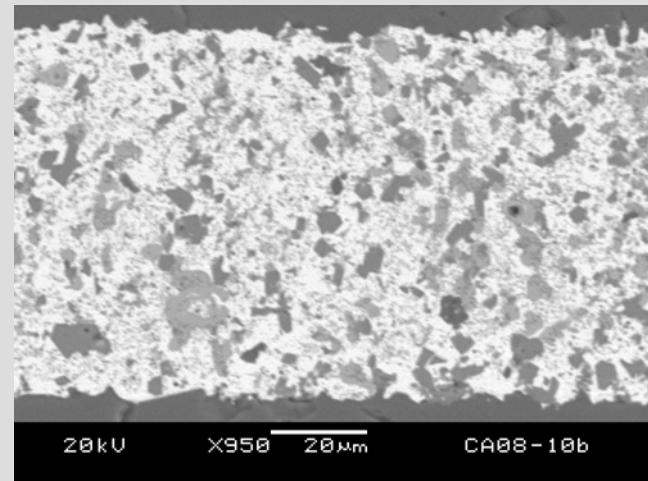
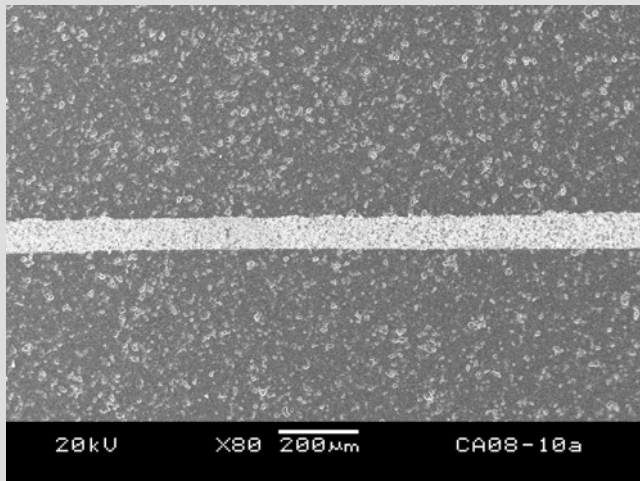


Type 1
Pores

Ag-4CuO



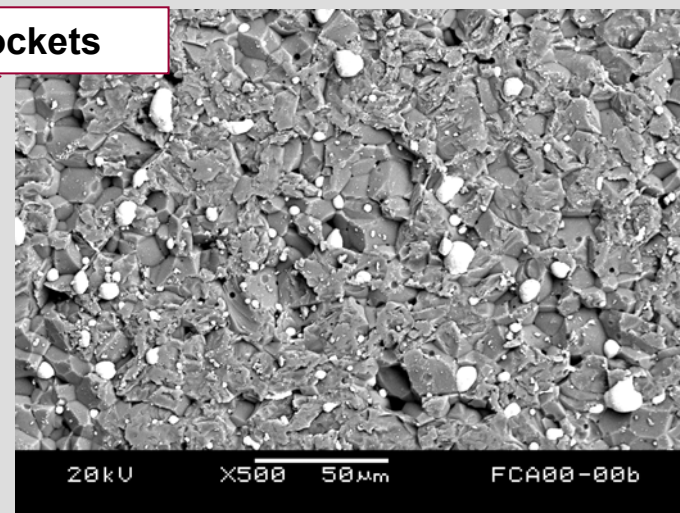
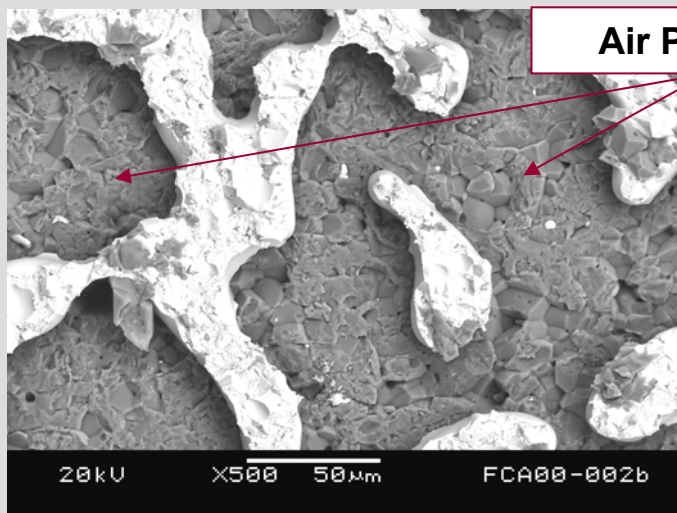
Ag-8CuO-10 Al_2O_3



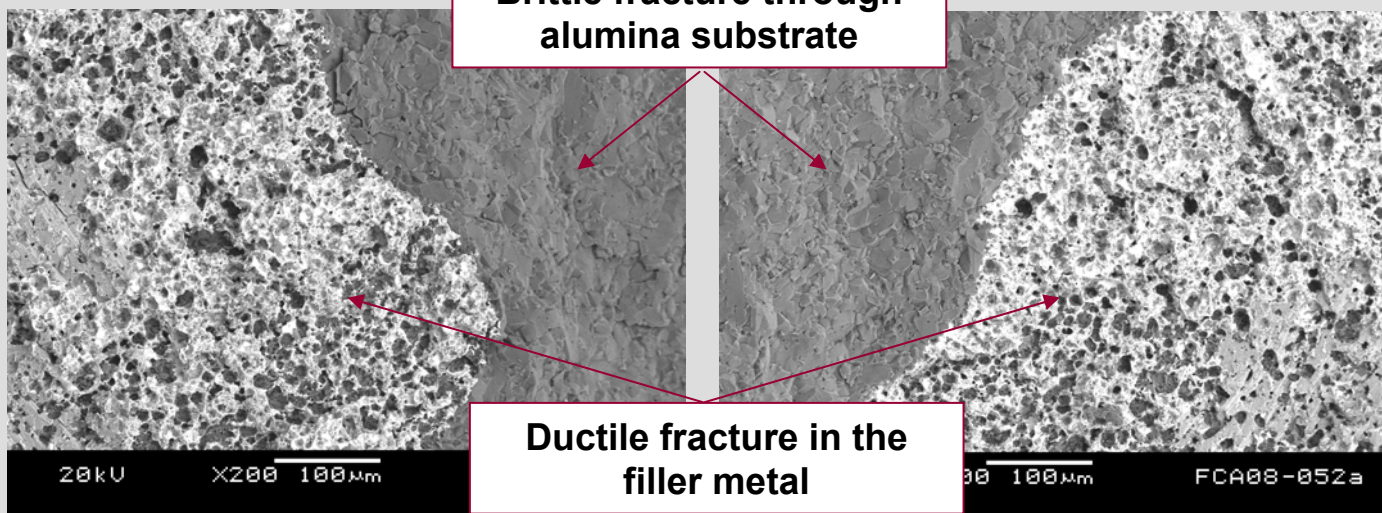
No squeeze out or porosity observed in the Al_2O_3 -modified filler metals

Ag8CuO

0 vol% Al_2O_3



5 vol% Al_2O_3



- Have identified three types of pores that can form in Ag-CuO air brazed joints exposed to a high-temperature, dual atmosphere environment
 - ▶ Type 1 – air pockets formed during joining
 - ▶ Type 2 – micron-sized pores formed due to reduction of CuO ppts
 - ▶ Type 3 – pores formed along the matrix grain boundaries due to reaction between dissolved H and O (observed at ~2000hrs of exposure)
- The pores do not appear to be problematic in short-term testing (2000hrs or less)
- Can eliminate Type 1 pores using filler metals containing Al_2O_3 particulate and a high CuO content
- Preliminary testing indicates that Type 2 and possibly Type 3 pores can be eliminated by adding Al as an alloying agent

- Investigate the use of Al_2O_3 in combination with high CuO-containing Ag-Al-CuO filler metals as a means of achieving high strengths and mitigating dual atmosphere degradation
- Examine the mechanical properties of Ag-Al-CuO- Al_2O_3 brazed joints after single atmosphere exposure for $t_{\text{exposure}} < 1000\text{hrs}$ and compare with prior results obtained on bend specimens joined using the Ag-CuO, Ag-Al, and Ag-Al-CuO filler metals
- Conduct 1000+hr dual atmosphere exposure testing on tube specimens sealed using the Ag-Al-CuO- Al_2O_3 filler metals
- Conduct post-exposure hermeticity testing and metallographic analysis
- Carry out preliminary joining studies using prototypic SOFC materials

- **John Hardy, Joe Rice, Jim Coleman, Nat Saenz, and Shelly Carlson**
- **Support: U. S. DOE, Office of Fossil Energy, SECA program**

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