

Compressive Seal Development for Solid Oxide Fuel Cells

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**Funded under the SECA Core Technology Program
through US Department of Energy's
National Energy Technology Laboratory (NETL)**

April 17-21, 2005, Asilomar, CA

Outline

- ▶ Status of mica-seal development
- ▶ Current work objective
- ▶ Results of long-term ageing and thermal cycling
 - Problem of degradation/reaction of mica/G18
 - Solutions to reactive interlayer glasses
 - Ageing and thermal cycling with metallic interlayer
 - Issue of long-term Ag volatilization
 - Reproducibility with Ag interlayers
 - Isothermal ageing in 30v% H₂O fuels
 - fractography
 - Issue of long-term mica volatilization in 30v% H₂O
- ▶ Summary and conclusion
- ▶ Future work

Status of compressive mica seal

Hybrid micas survived, ~4000 hr, 47+30+10 cycles
@12 psi, 0.02-0.04 sccm/cm @0.2psi

3 solutions to minimize materials degradation

Final goals:

>40,000 hrs stability

>10² or 10³ cycle

No degradation to mating mat'l

Low stresses

Low cost in SOFC stack

Vibrational stability?

Hybrid micas showed reproducibility

Hybrid Ag micas aged 1000hrs and 39 cycles
in 70%H₂/30%H₂O, 0.02-0.03 sccm/cm

Hybrid micas survived
88 cycles @12.5 psi

Hybrid micas showed low leakage @ 6 psi and Nernst OCV

Hybrid micas survived 1026 thermal cycles
and 2052 hrs @800C, ~2.7%H₂/Ar+3% H₂O and 100 psi

Glass-mica
composites

Infiltrated micas

Hybrid micas

Plain mica paper

Plain Muscovite mica (monolithic)

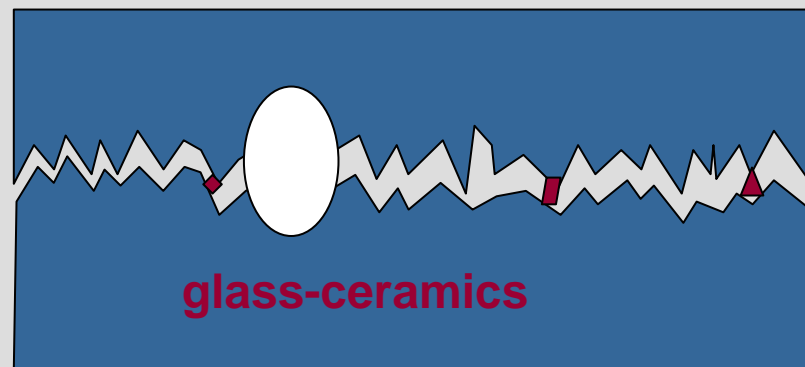
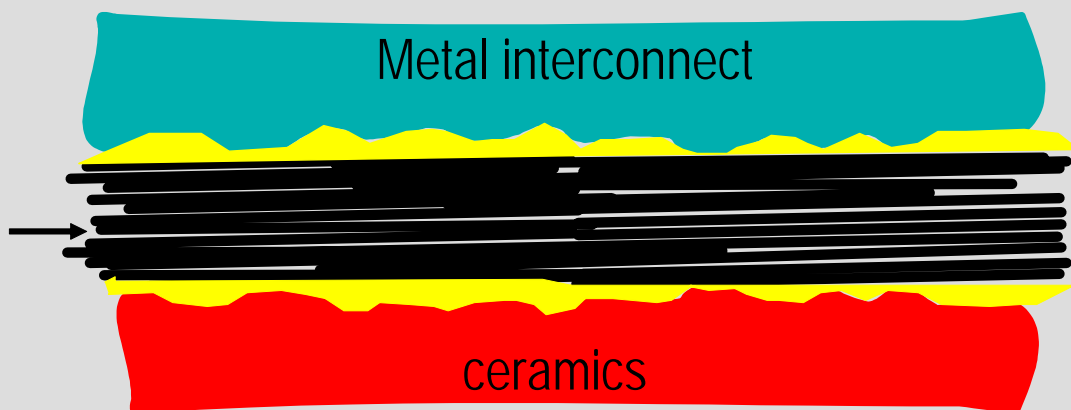
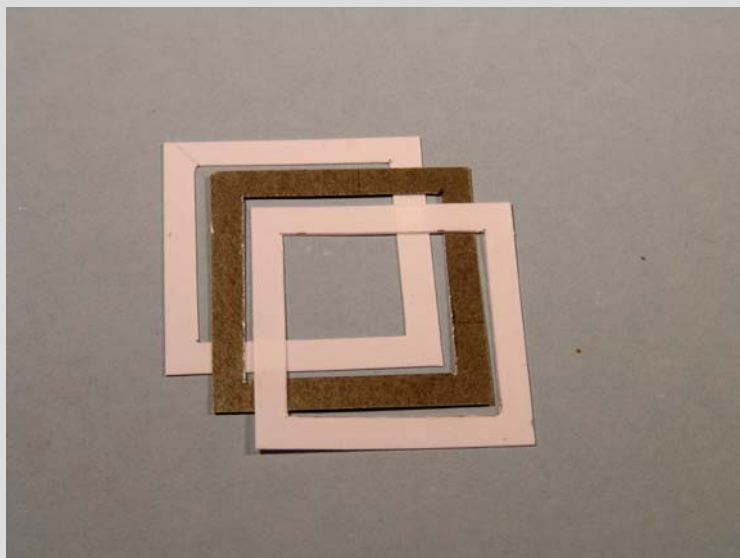
Current work objective

1st and 2nd (FY05) quarters:

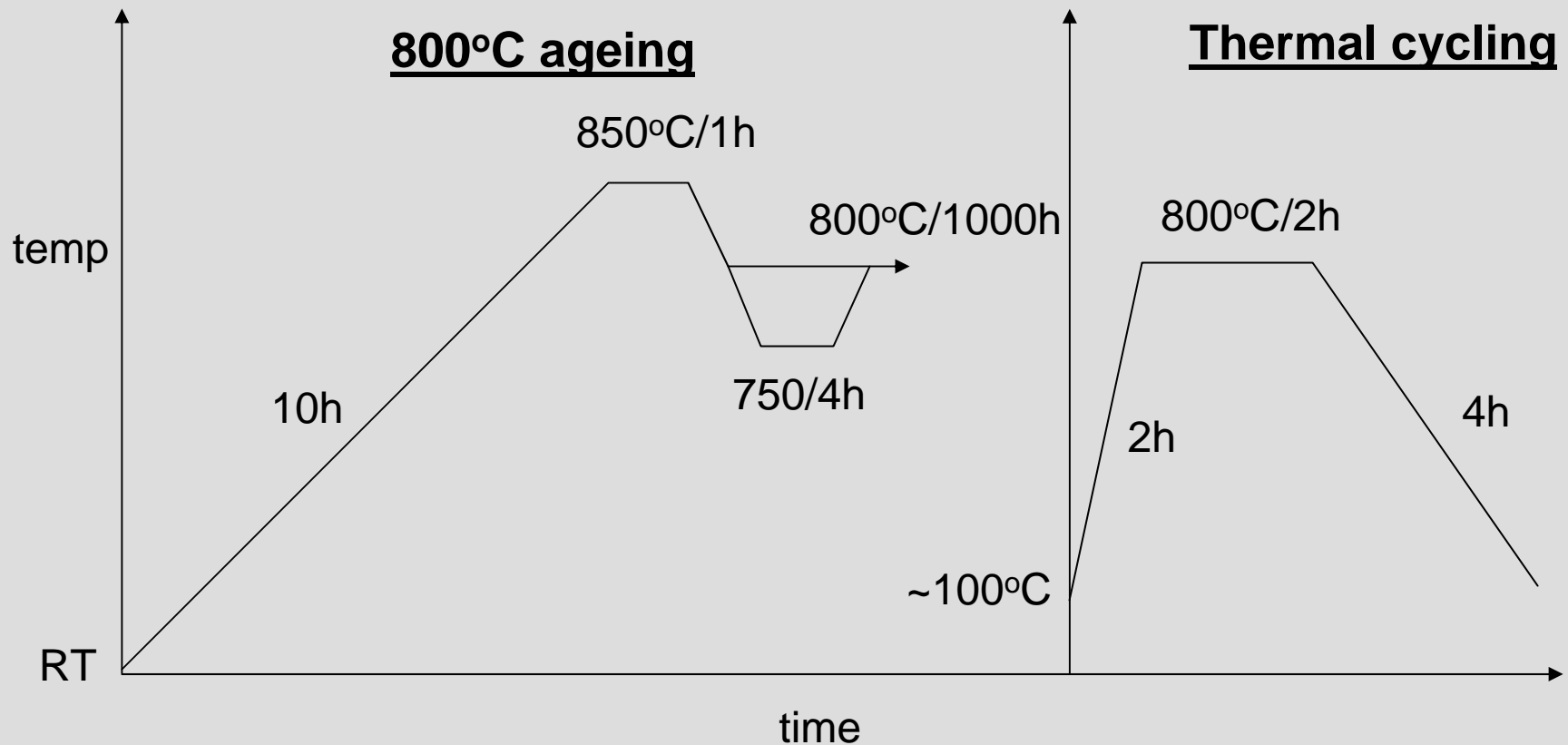
The objective was to evaluate the combined isothermal ageing and thermal cycling effect on hybrid mica seals of metallic interlayers with respect to materials and interfacial degradations in a simulated and high water content (30 v%) SOFC environment.

Hybrid Phlogopite mica

Phlogopite is more thermally stable ($\sim 960^{\circ}\text{C}$) than Muscovite ($\sim 600^{\circ}\text{C}$)

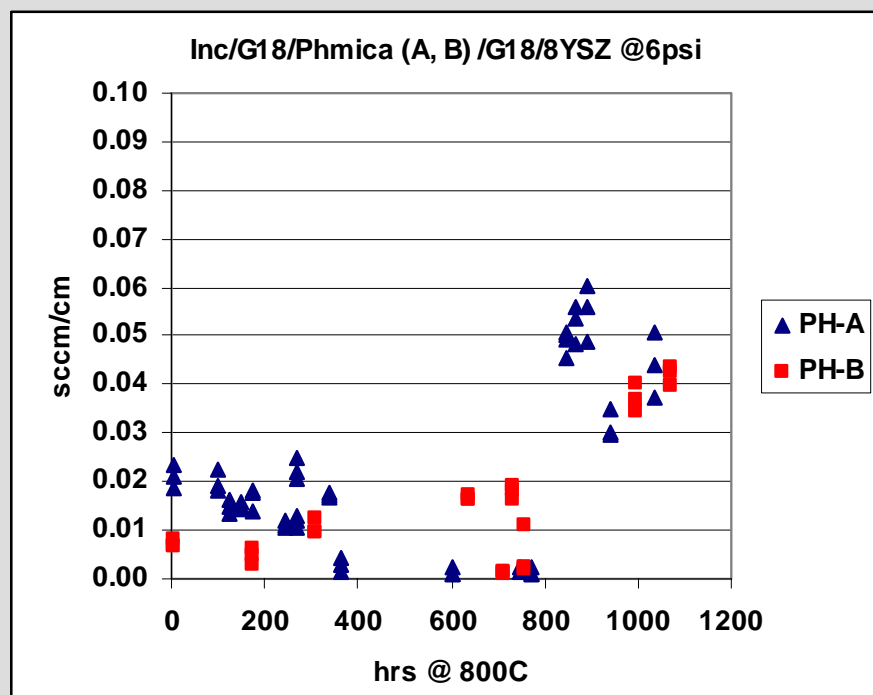


Isothermal ageing and short-term thermal cycling

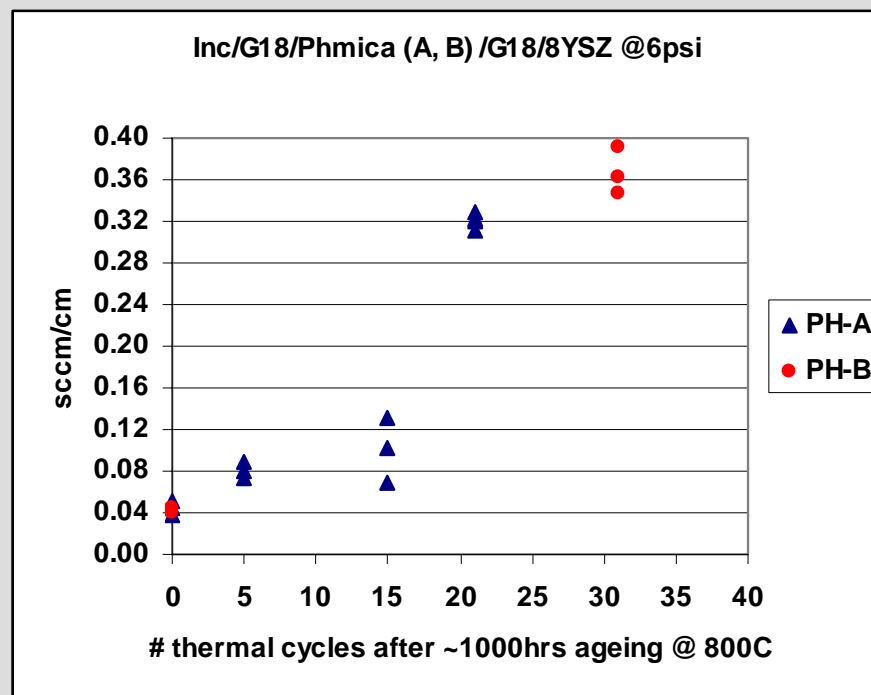


Combined ageing and thermal cycling of hybrid mica with G18 glass interlayers

Inc/G18/PH-A or PH-B/G18/8YSZ @ 6psi with flowing $\sim 2.7\% \text{H}_2/\text{Ar} + \sim 3\% \text{H}_2\text{O}$



800°C ageing

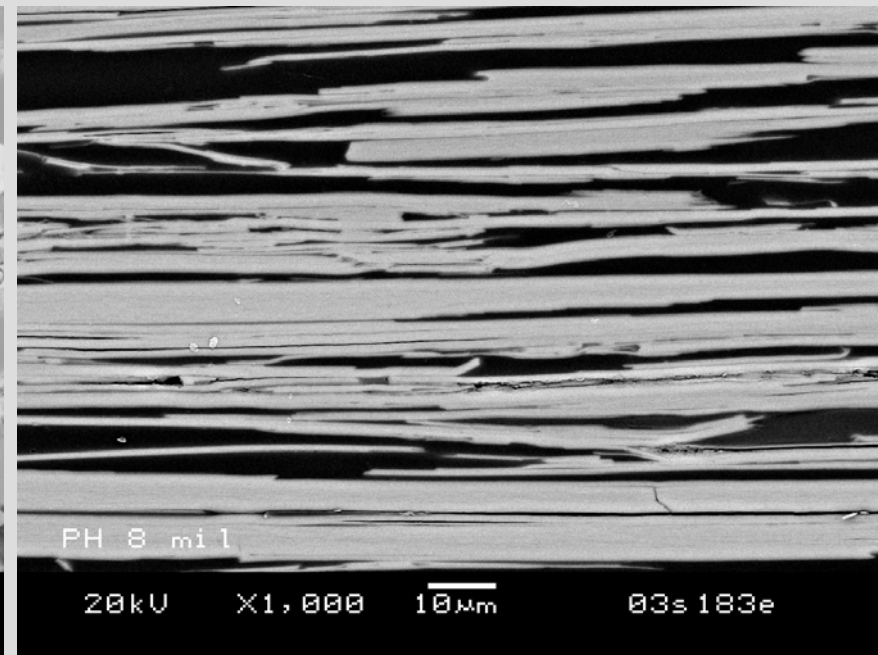
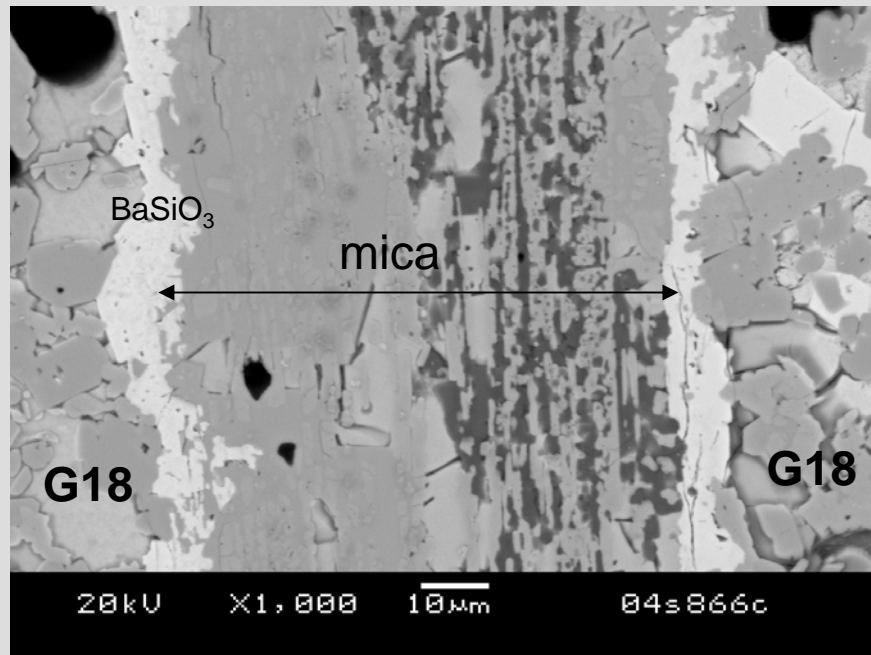


thermal cycling

PH-A: Cogebi, cogemica, PH-B: McMaster Carr

Cross-section of aged and cycled hybrid mica with G18 glass

Pressed @6psi after 1036 hrs ageing and 21 cycles

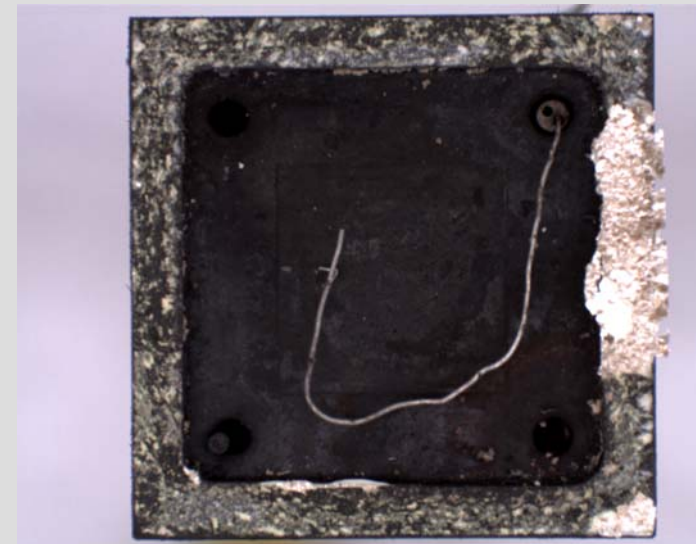
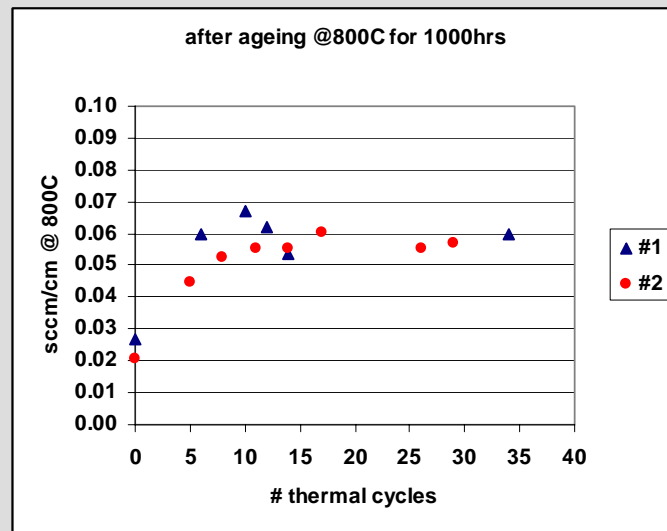
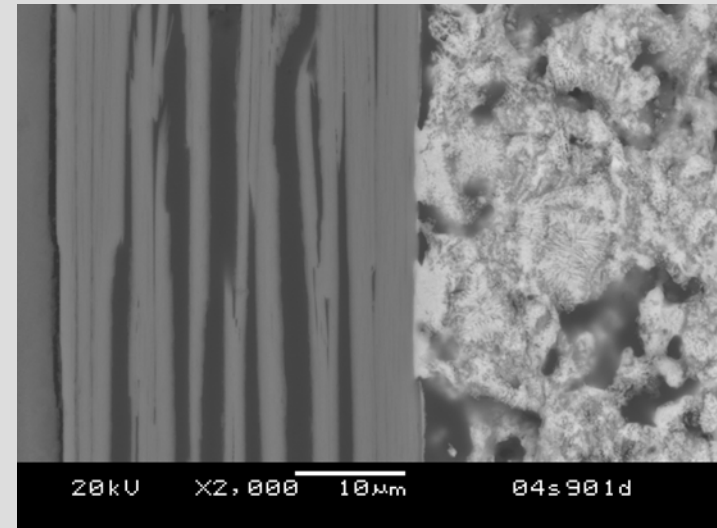
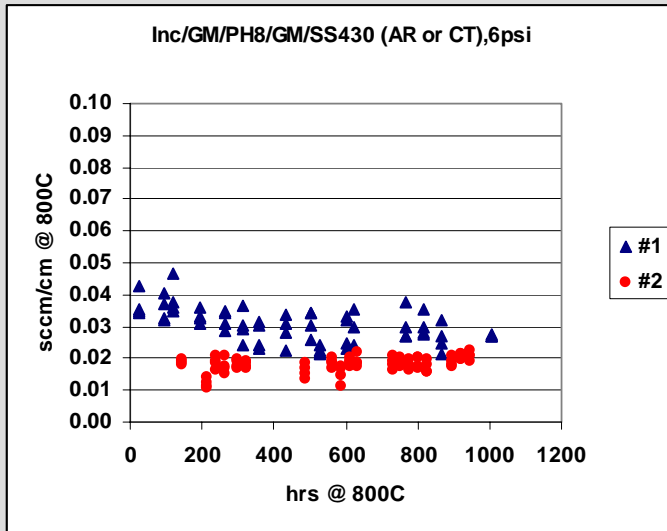


- Fracture occurred along with the G18 glass near the Inconel600 side
- Thick G18 glass showed undesirable porous microstructure

Solutions to minimize mica degradation

- ▶ Promote rapid crystallization of G18 by adding nucleation agent (e.g., TiO_2)
- ▶ Use less reactive (more “**refractory**”) glass G-M (less B_2O_3)
- ▶ Use of non-reactive metallic materials (Ag, Cu, etc)

No degradation of mica with glass G-M



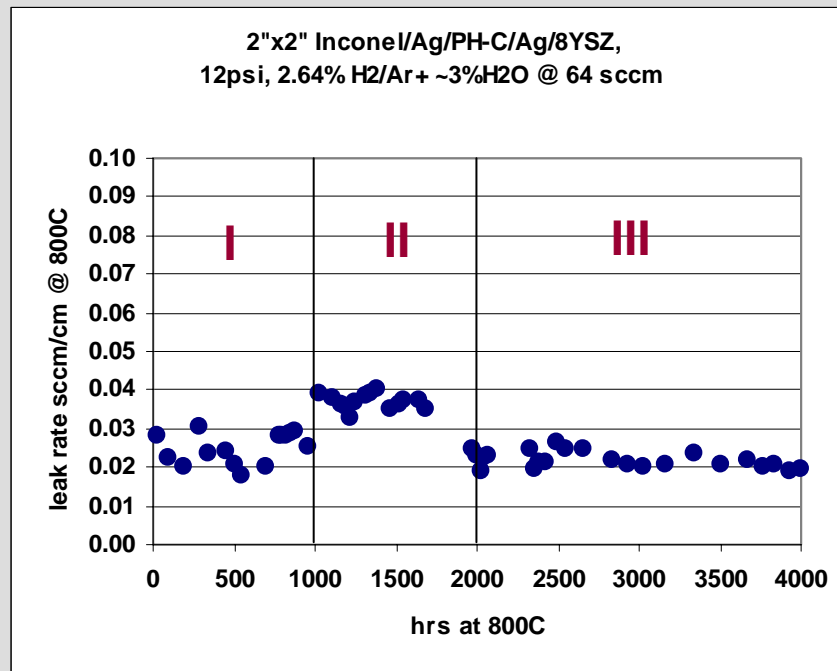
Inconel/GM/PH8/GM/CT SS430 @ 6psi
after 1000 hrs 800°C and 34 cycles

Hybrid mica with metallic interlayers

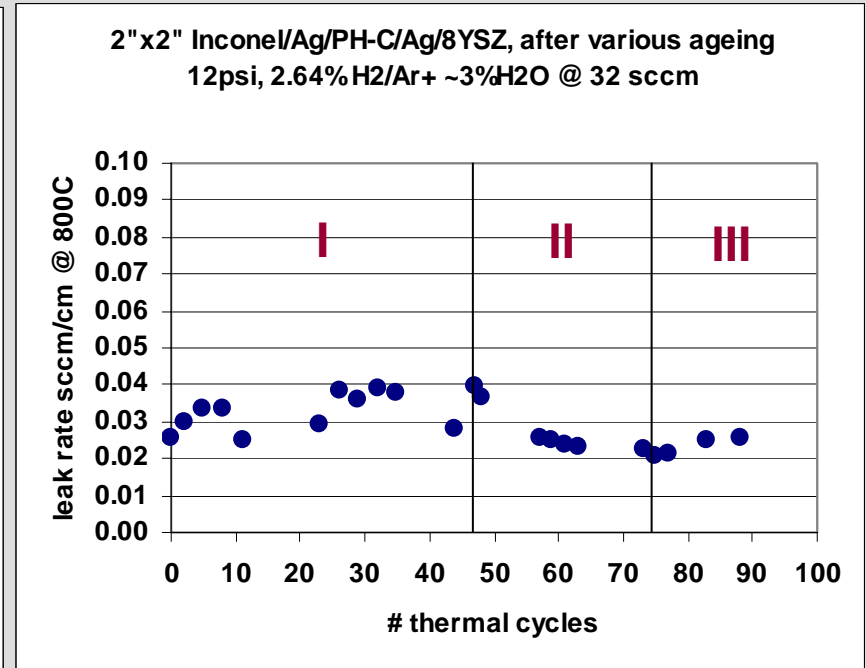
- ▶ **Non-reactive with Mica**
- ▶ **Volatilization issue**
- ▶ **Oxidation issue**
- ▶ **Poison issue**
- ▶ **High water content fuels**
- ▶ **Easily deformed**
- ▶ **Adhere or bonding to metal of high CTE**
- ▶ **Ag, Cu, and brazes**

Ageing and thermal cycling of hybrid mica with Ag interlayers (0-4000 hrs)

Inconel/Ag/Phlogopite/Ag/8YSZ @12psi



Isothermal ageing

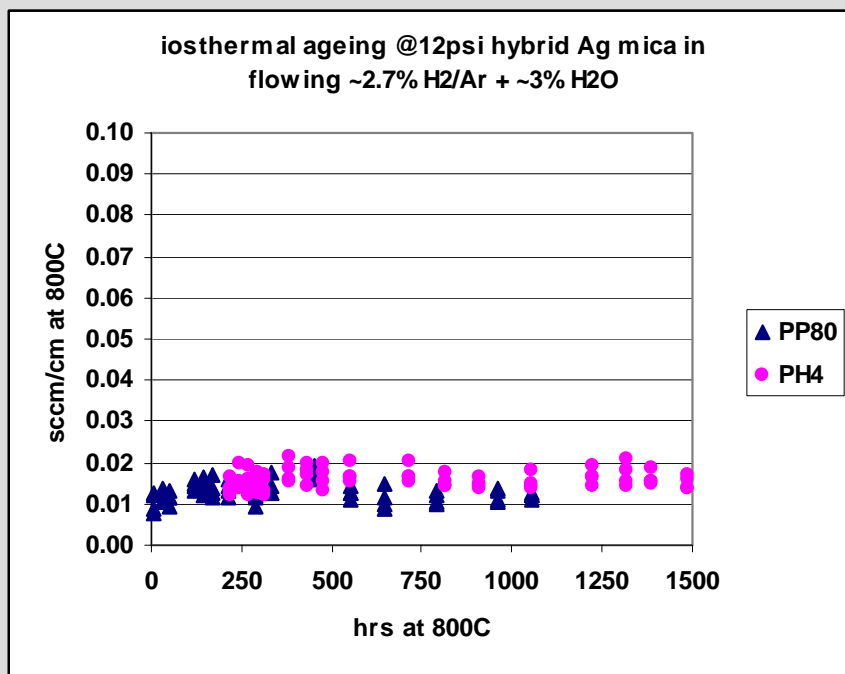


Thermal cycling after ageing

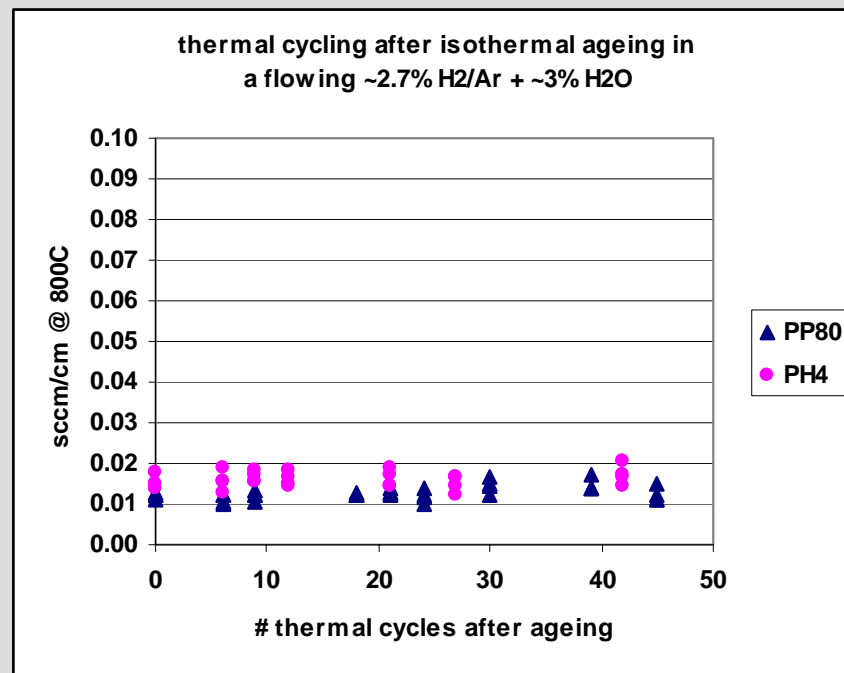
***fuel loss = 0.2% @0.03 sccm/cm, 0.2 psid, 0.7V, 0.5 W/cm², 800°C,
80% fuel utilization of pure hydrogen of a 6"x6" SOFC cell
SECA target: fuel loss <1% @ 0.1 psid after 10 thermal cycles for 6"x6"***

Good reproducibility for hybrid mica with Ag interlayers

Inconel/Ag/Ph-mica/Ag/SS430 @12psi, 2.7% H_2 /Ar+~3% H_2O

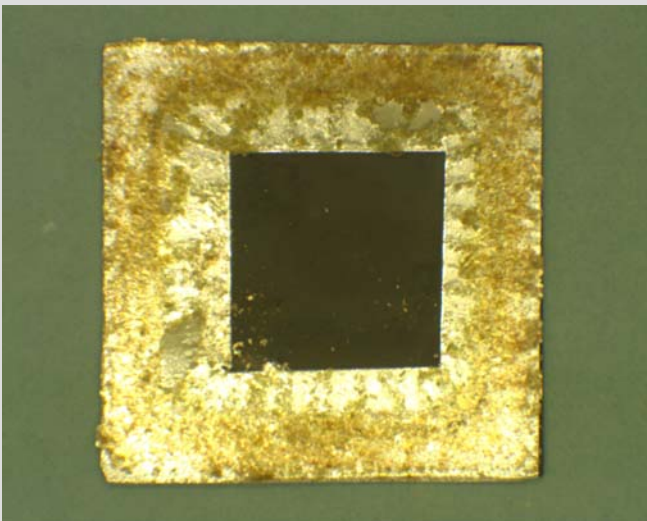
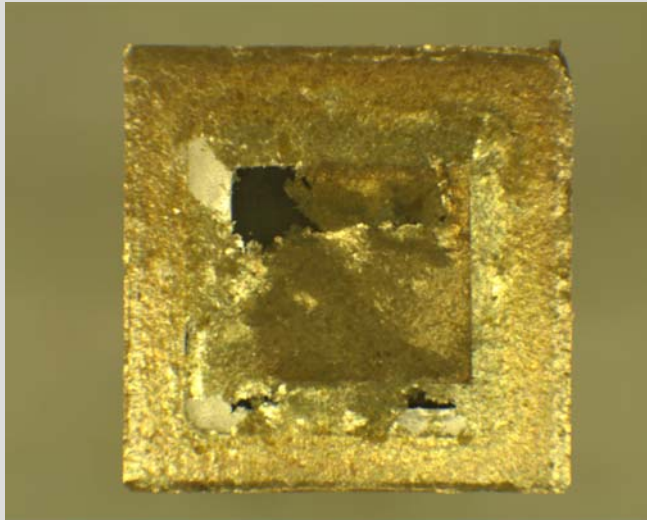


Isothermal ageing

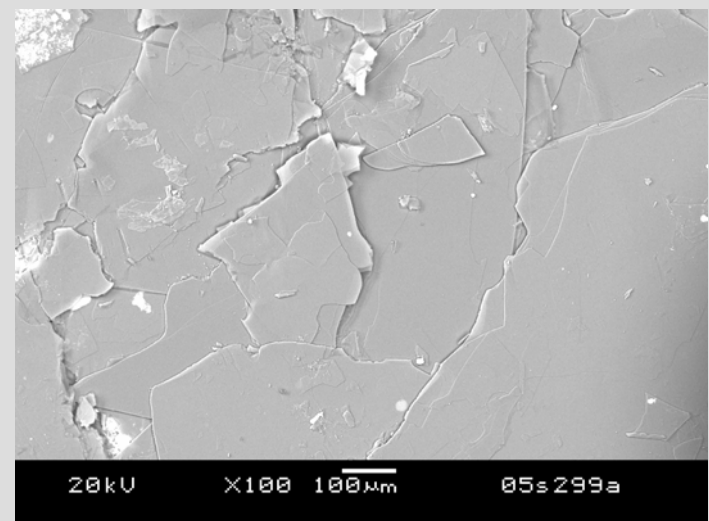
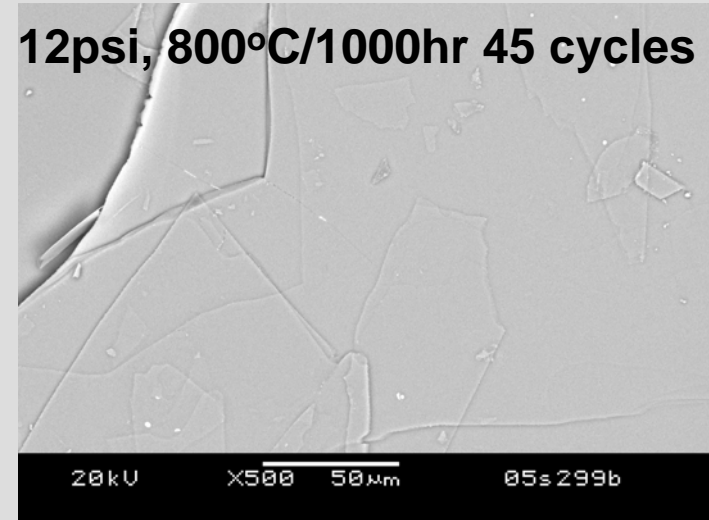


Thermal cycling after ageing

Fracture surface of aged and cycled hybrid mica with Ag interlayers

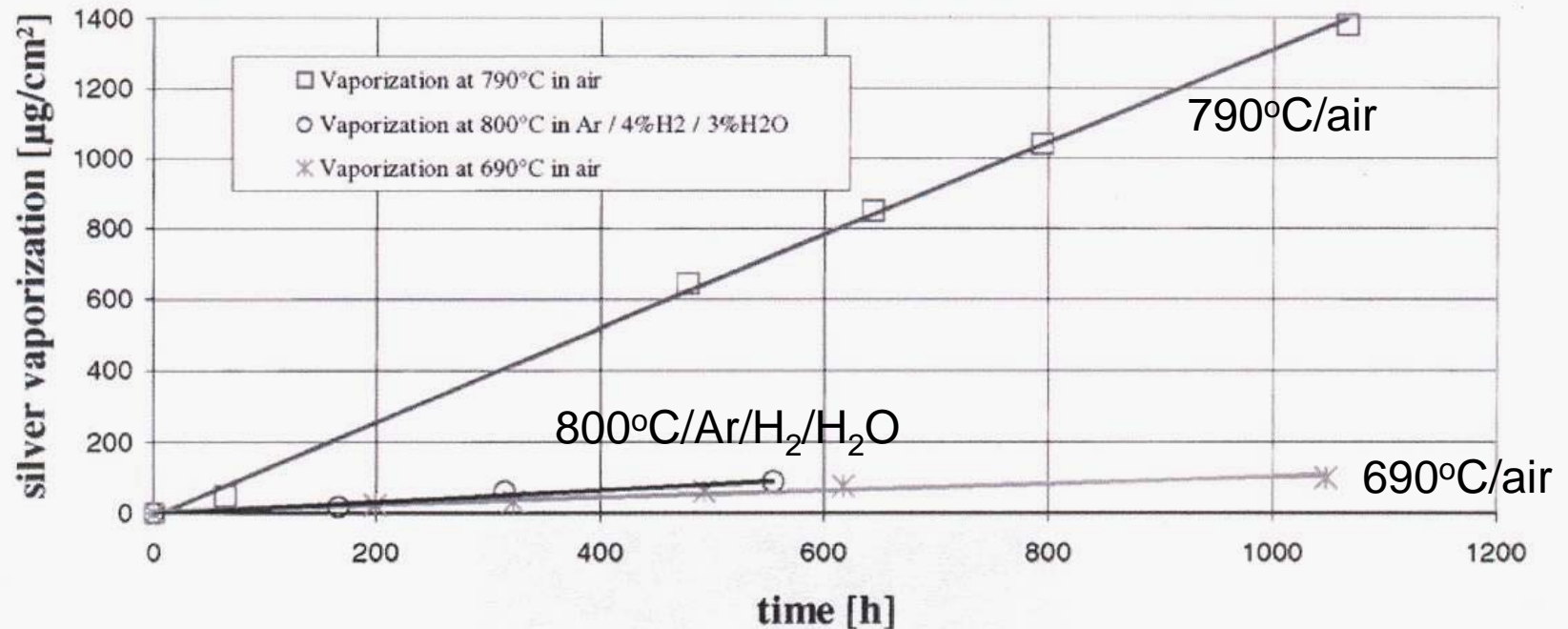


12psi, 800°C/1000hr 45 cycles



Issue of vaporization loss of Ag

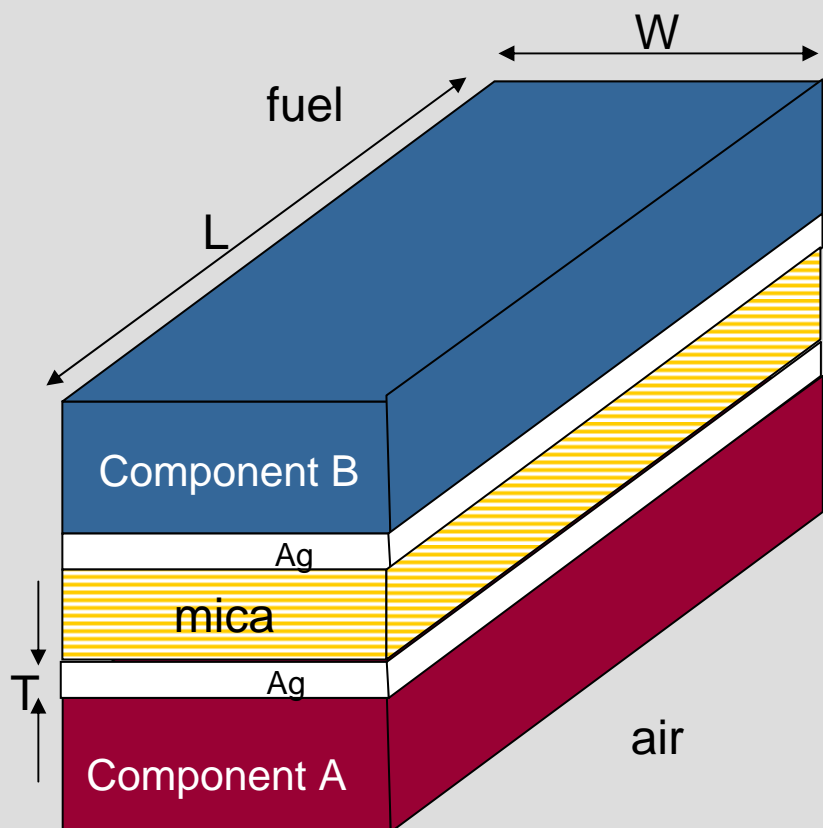
From Meulenberget al J. mater. Sci., 36 [6] 3189-3195 (2001)



690°C/air: $0.094 \mu\text{g}/\text{cm}^2/\text{h}$
790°C/air: $1.29 \mu\text{g}/\text{cm}^2/\text{h}$
800°C/Ar/H₂/H₂O: $0.161 \mu\text{g}/\text{cm}^2/\text{h}$

2.16% @40,000hrs
28.7% @40,000 hrs
2.33% @40,000 hrs

~1 wt% loss of Ag in hybrid mica over 40,000 hrs @ 790-800°C



For a width (W) = 0.5 cm
 $\rho(\text{Ag}) = 10.5 \text{ g/cc}$

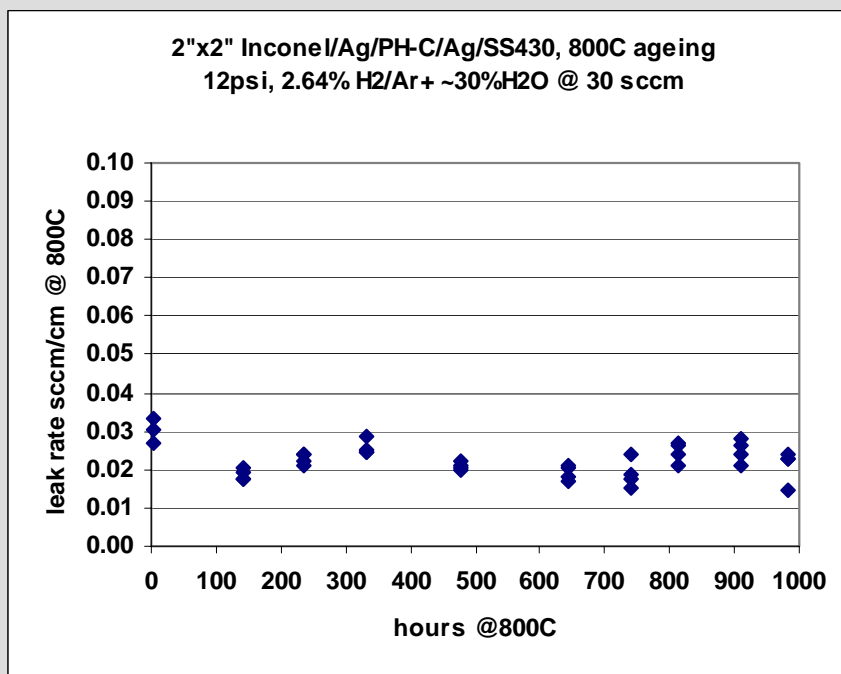
Ag loss on fuel side
 $= 40,000(aTL)/(\rho TWL) = 0.12\%$

Ag loss on air side
 $= 40,000(bTL)/(\rho TWL) = 0.98\%$

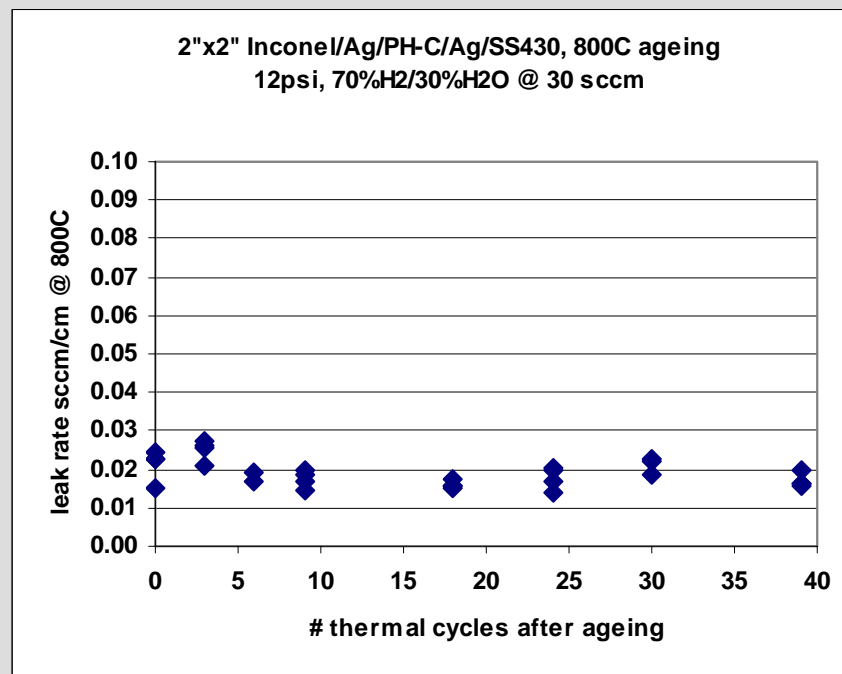
- Loss from exposed edges only
- No diffusion loss to metals
- **Electrical shorting?**
- **Degradation of electrochemical performance unknown; however, possible solutions are available.**

Ageing and thermal cycling of hybrid mica in high humidity (30v%) fuel gas

Inconel/Ag/Phlogopite/Ag/8YSZ @12psi



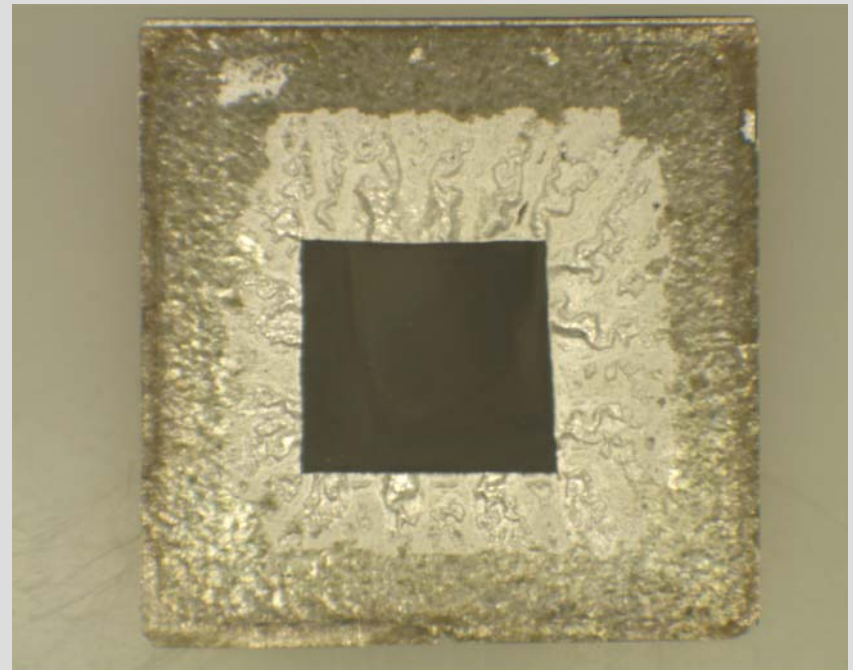
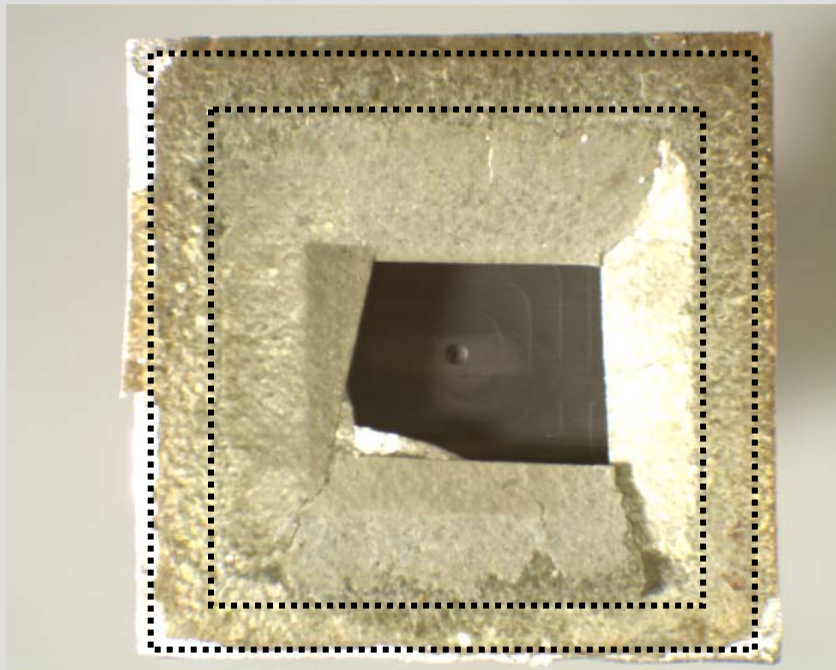
Isothermal ageing



Thermal cycling after ageing

Fracture surface of aged hybrid mica in 70% H₂/30% H₂O @800°C

Inconel/Ag/Phlogopite/Ag/8YSZ @12psi, 1000hrs and 39 cycles



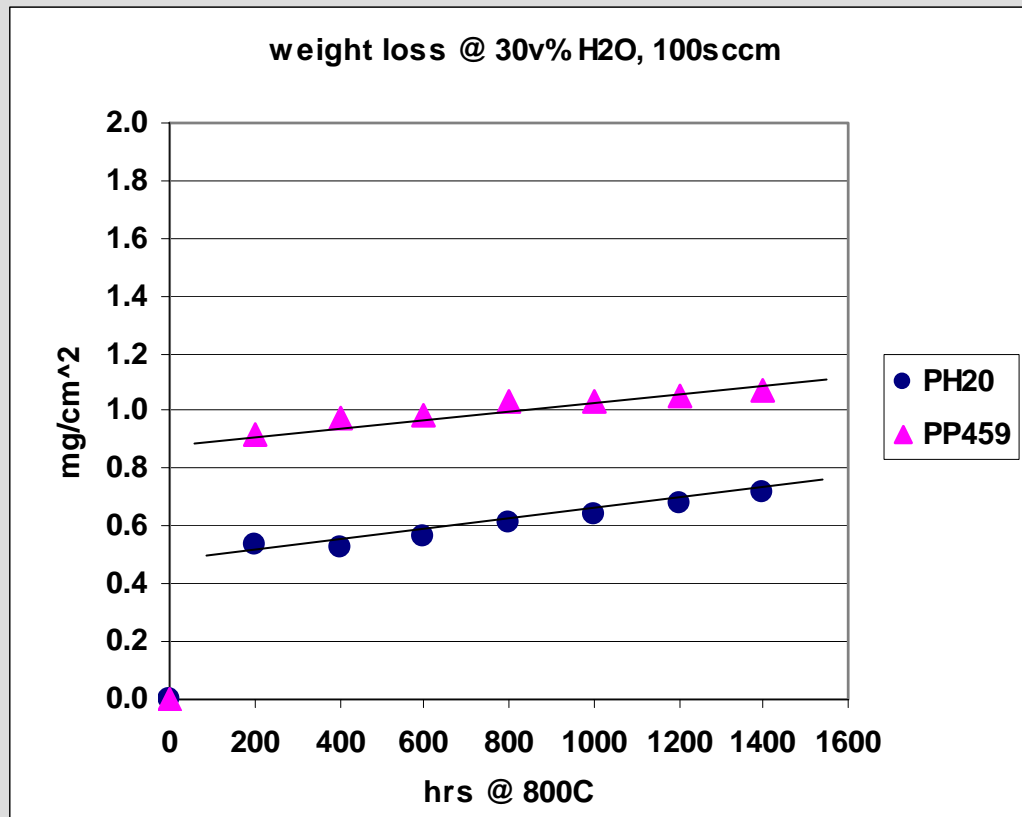
Majority fracture between mica flakes, one spot of mica/Ag interface

Issue of vaporization loss of Phlogopite mica, $\text{KMg}_3(\text{AlSi}_3\text{O}_{10})(\text{F},\text{OH})_2$

- ▶ Silicate glass material loss by $\text{Si}(\text{OH})_4$ g
- ▶ 1"x1" mica exposed in 2.7% H_2 /bal. Ar + ~30v% H_2O @ 100 sccm, 800°C

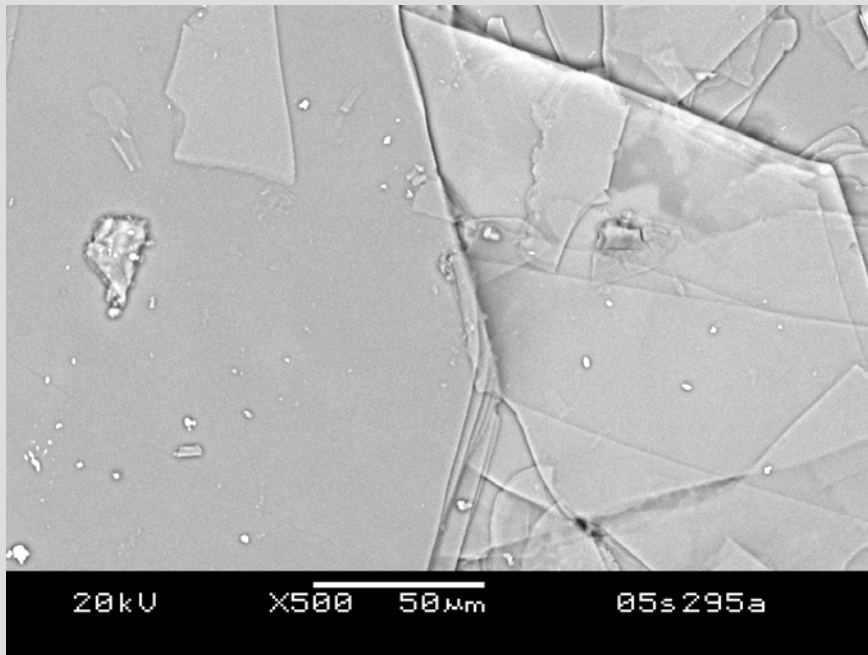
slope =
 $\sim 1.2 \times 10^{-4} \text{mg/cm}^2/\text{h}$
 $\sim 1.6 \times 10^{-4} \text{mg/cm}^2/\text{h}$

Incomplete binder
Burnout <200 hrs

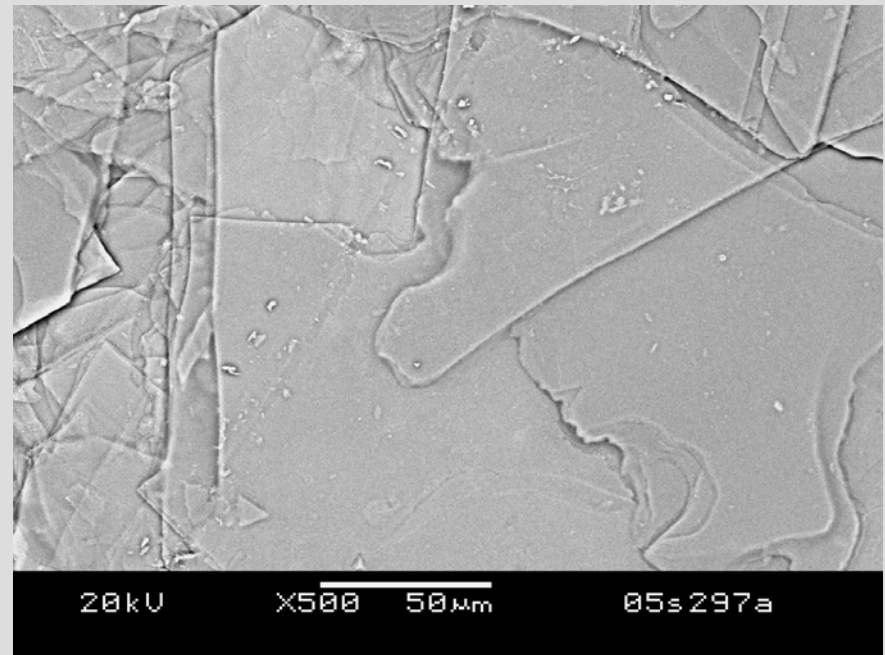


No degradation to mica exposed to 30 v% H₂O @ 800°C/1400hrs

1"x1" mica in 2.7% H₂/bal. Ar + ~30v% H₂O @ 100 sccm, 800°C/1400 hrs

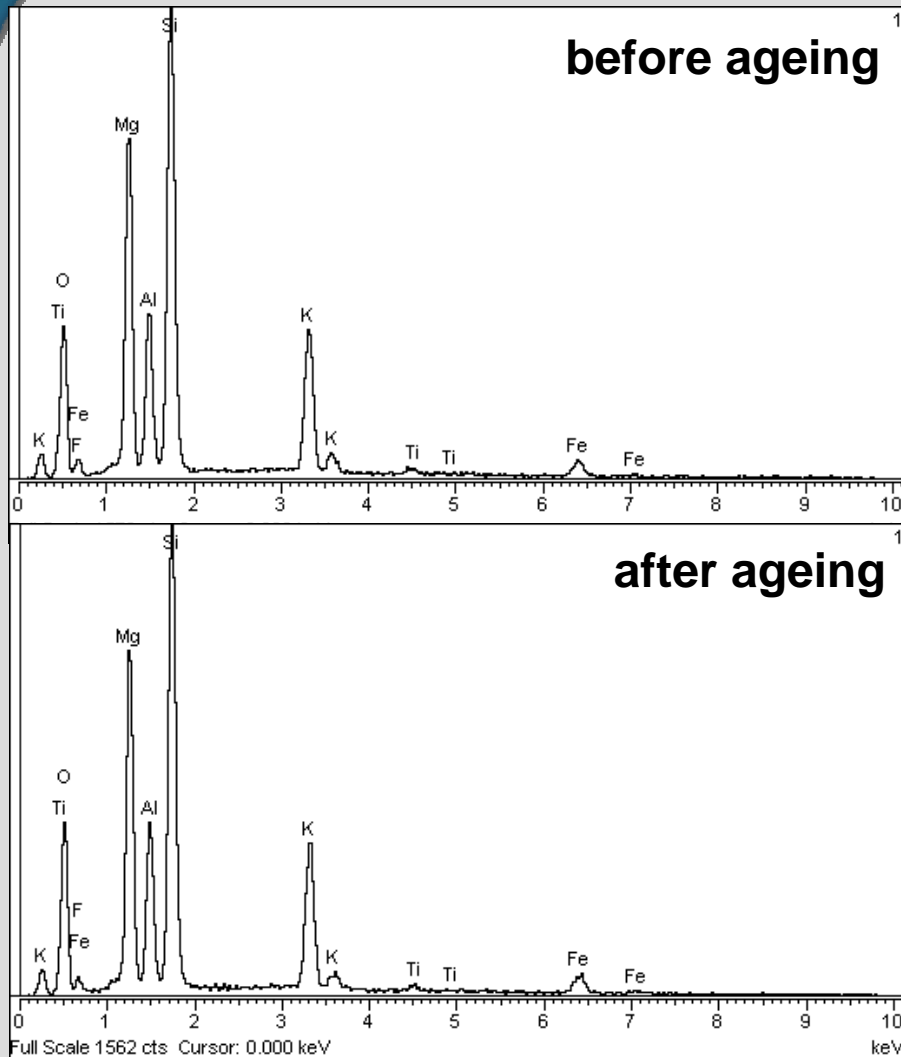


before ageing



after ageing

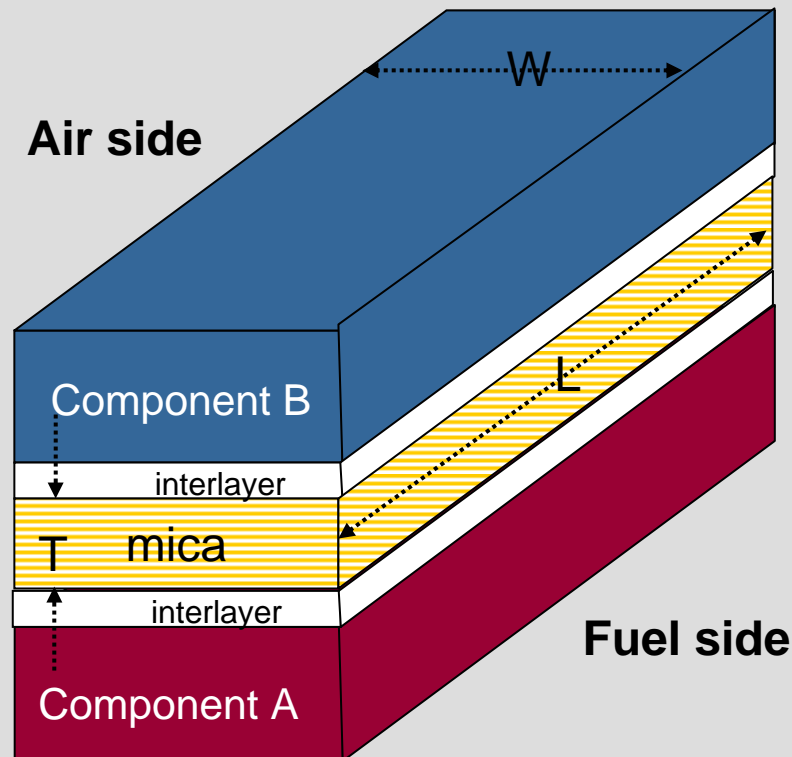
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1"x1" mica in 2.7% H₂/bal. Ar + ~30v% H₂O @ 100 sccm, 800°C/1400 hrs

Element	before	after
O K	46.3	48.1
F K	4.34	4.1
Mg K	14.97	14.44
Al K	6.69	6.56
Si K	20.15	19.51
K K	6.09	5.75
Ti K	0.25	0.23
Fe K	1.22	1.32

Minute loss (<0.5 wt%) of Phlogopite @ 800°C and 30 v% H₂O fuel gas



For a width (W) = 0.5 cm
 $\rho(\text{mica}) = \sim 2.82 \text{ g/cc}$
 $a = 1.2\text{-}1.6 \text{ mg/cm}^2/\text{hr}$

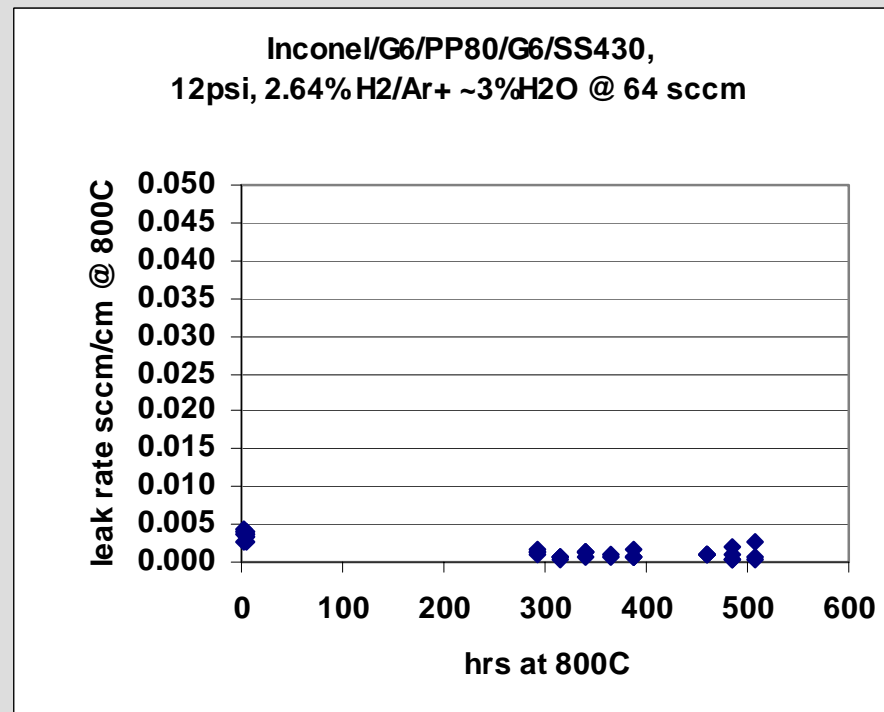
mica loss on fuel side
 $= 40,000(aTL)/(\rho TWL)$
 $= \sim 0.34\text{-}0.45 \text{ wt\%}$

- mica loss from free exposed edges at fuel side only

Engineering control the leak rate

$$\text{total leak} = K_{\text{eff}} A \frac{dP}{dx} + D_{\text{eff}} A \frac{dC}{dx}$$

Reduce leak by increasing seal width and/or reducing mica thickness



Conclusion

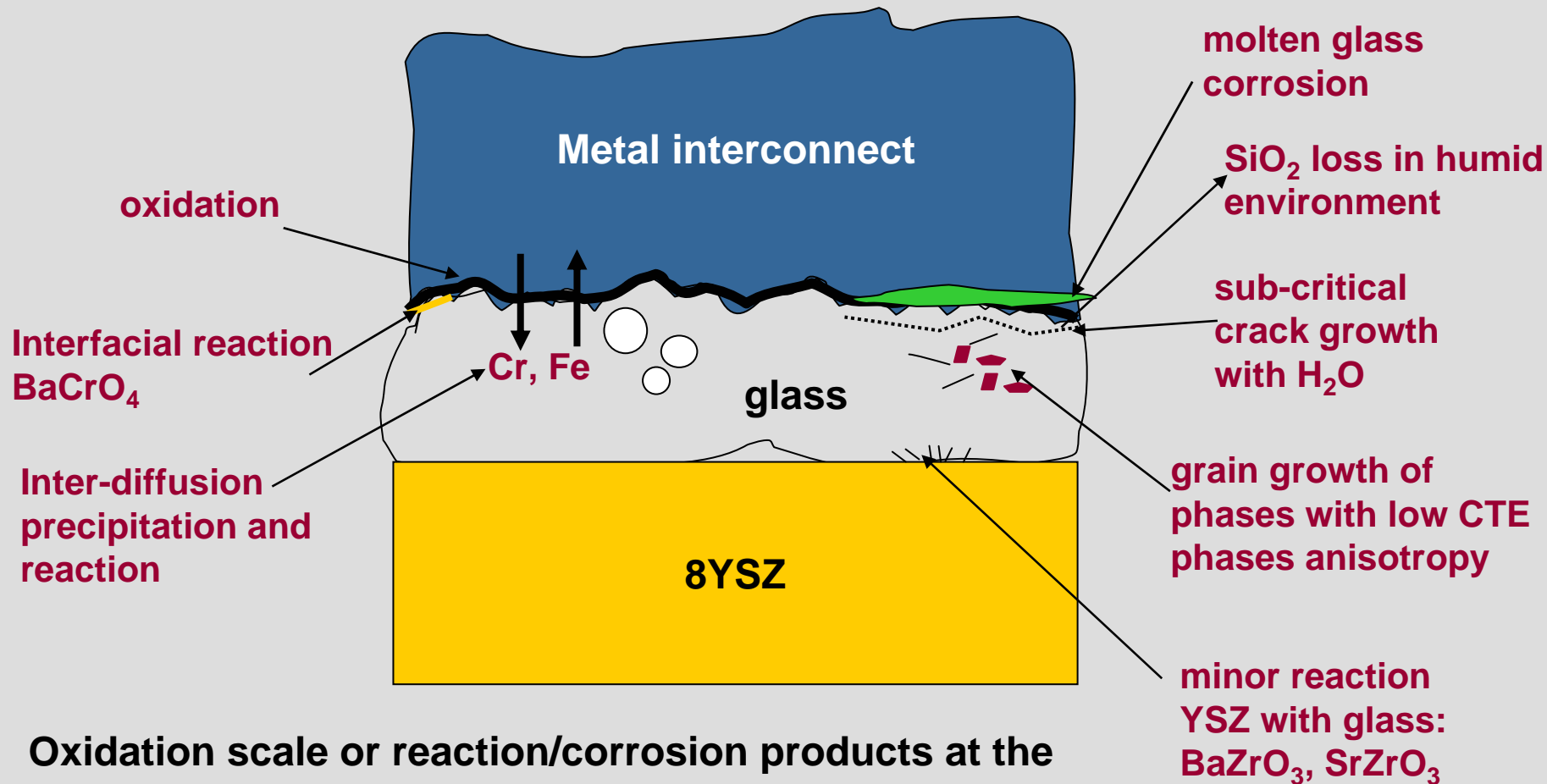
Hybrid Phlogopite mica demonstrated desirable properties as a strong candidate for SOFC sealing:

- ▶ Long-term thermal cycle stability over 1026 cycles.
- ▶ Long-term ageing stability with constant leak rates (~ 0.02 sccm/cm) over 4,000 hrs.
- ▶ Constant leakage during combined ageing and thermal cycling.
- ▶ Low leakage (~ 0.01 - 0.02 sccm/cm) at minimal stress of 6 psi.
- ▶ Good thermal stability in high water content fuels (30 v%), lean and rich in hydrogen.
- ▶ Calculated minute materials loss due to volatilization over 40,000 hrs.
- ▶ Identified the effect of mica thickness and compressive stresses.
- ▶ Identified cause for mica degradations and 3 solutions demonstrated.
- ▶ Good reproducibility and scale-up from 2"x2" to 3.5"x3.5".
- ▶ No effect of temperature gradients on leakage during thermal cycling.
- ▶ Low leakage (~ 0.02 sccm/cm) satisfied SECA's target of $<1\%$ fuel loss.
- ▶ Low cost, easy processing, and engineering.

Future work

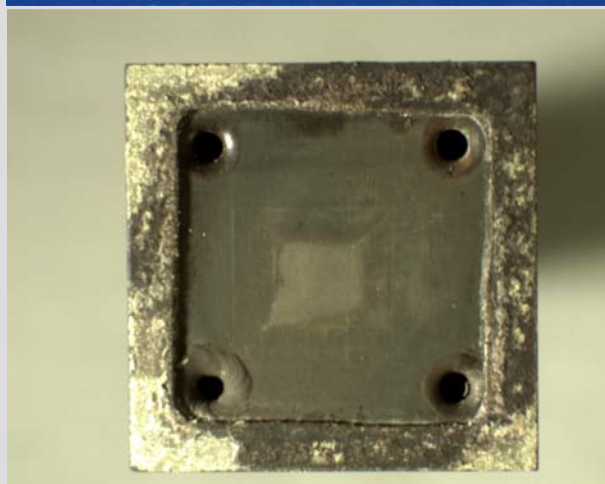
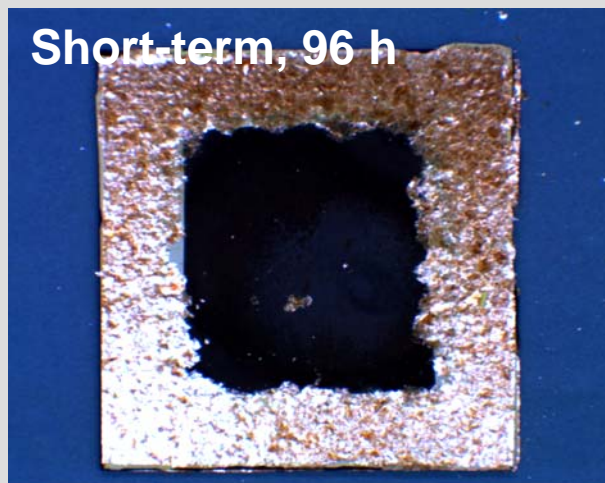
- ▶ Development of durable low-cost glass (glass-ceramics) seals with **minimal materials/interfacial interaction/degradation** and **engineered interface** for optimal shear strength at **various sealing temperatures**.
- ▶ Study interfacial reaction/degradation of G/M and G/C at various stages of operation, temperatures, and environments
- ▶ Understand and model engineered interface for optimal interfacial strength: to prevent Mode II and III fracture
- ▶ Evaluate “**refractory**” glass compositional effect on basic thermal properties (T_g , T_s , T_c , CTE, sealing temperatures, 850-1100°C)
- ▶ Identify the microstructural effect due to crystallization on basic thermal and mechanical properties
- ▶ Candidate metals: Crofer22 and FeCrAl and surface treatment
- ▶ Candidate ceramics: 8YSZ/NiO-YSZ anode bilayers
- ▶ Candidate glasses: alkaline earth-Al-Ca-Silicates

Weakest link is at the metal/glass interface



Oxidation scale or reaction/corrosion products at the metal/glass interfaces often have mismatched CTE.

proposed fracture of a rigid glass (glass-ceramic) seal at various stages



Intermediate stage, 1000 h

