
**Innovative Injection and Mixing Systems
for Diesel Fuel Reforming**

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Goodrich Turbine Fuel Technologies

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- **Program Goals and Work Scope**
 - **Technical Approach**
 - Injector and Mixing Concepts
 - CFD Flow Structure and FE Thermal Analyses
 - Experimental Setup and Equipment
 - **Results to Date**
 - Test Rigs
 - Multipoint Impingement Injector and Mixer
 - Single Point Gas-assisted Injector and Mixer
 - High-Energy Piezoelectric Injector
 - **Future Plans**
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● **Objective – The primary objective is to develop cost-effective injection and mixing concepts to enable development of reliable diesel fuel reforming technology for solid oxide fuel cell power system.**

● **Major Tasks**

- Task 1- Evaluate Atomization and Injection Concepts
 - Task 2- Develop Effective Mixing Chamber
 - Task 3- Construct Test Rig and Perform Laser Diagnostics
 - Task 4- Investigate Carbon-resistant Coating Materials and Design features
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- Adequate atomization over the entire operating range
 - High flow rate turndown ratio required
 - Minimum inlet pressure of steam and airflow
 - Uniform distribution of temperature, velocity and fuel mixture at the entrance of the reactor
 - Intrinsically unstable flow
 - Recirculation and flow reversal inside mixing chamber
 - Autoignition
 - Droplet impingement on wall surface
 - Quick mixing between feed streams
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- **Thermal management issues (heat shielding, steam condensation and internal coking)**
 - **Pressure loss and plugging due to small passage and orifice**
 - **Diesel fuel difficult to vaporize and prone to pyrolysis**
 - **Coking and metal corrosion problems**
 - **Simple and robust injector/mixer design**
 - **Cost effective and low power consumption**
 - **Easy to integrate with different reactors**
 - **Multi-fuel capability**
 - **Quick startup and rapid response**
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- **Reformer Types - ATR, CPOX, ATR/SR**
 - **Fuel Types - Diesel, Jet A, JP8**
 - **Fuel Delivery Requirements - 0.6 to 8 lbs/hr, 50~145 psig inlet pressure**
 - **Fuel Turndown Ratio - 2:1 to 10:1**
 - **Air Delivery Requirement - 6 to 40 lbs/hr; temperature 70 ~950°F; maximum inlet pressure less than 2 psig**
 - **Steam Delivery Requirements -3 to 20 lbs/hr; 500~700°F; maximum inlet pressure 10 to 30 psig**
 - **Packaging Requirements - 0.5 ~ 1 liter**
 - **Steam/Carbon Ratio - 0.5 to 3**
 - **Oxygen/Carbon Ratio - 0.8 to 1.3**
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1 psig/1 pph

Jet Fuel SMD > 120 μm

Diesel SMD > 140 μm



5 psig/2.7 pph

Jet Fuel SMD = 80 μm

Diesel SMD = 90 μm



20 psig/4.8 pph

Jet Fuel SMD = 60 μm

Diesel SMD = 70 μm



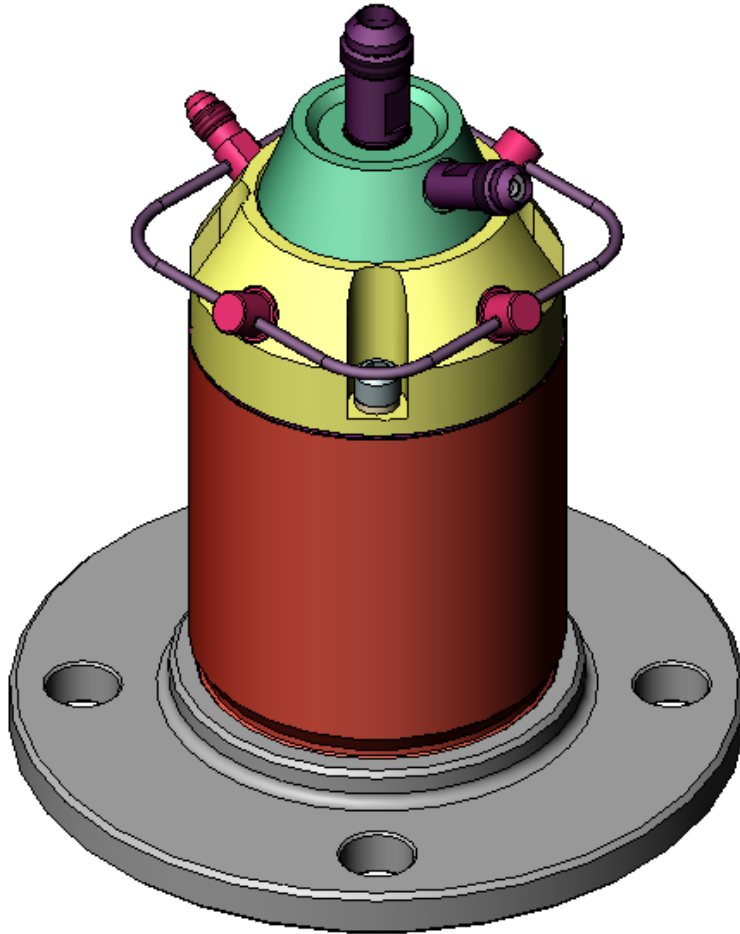
50 psig/7.25 pph

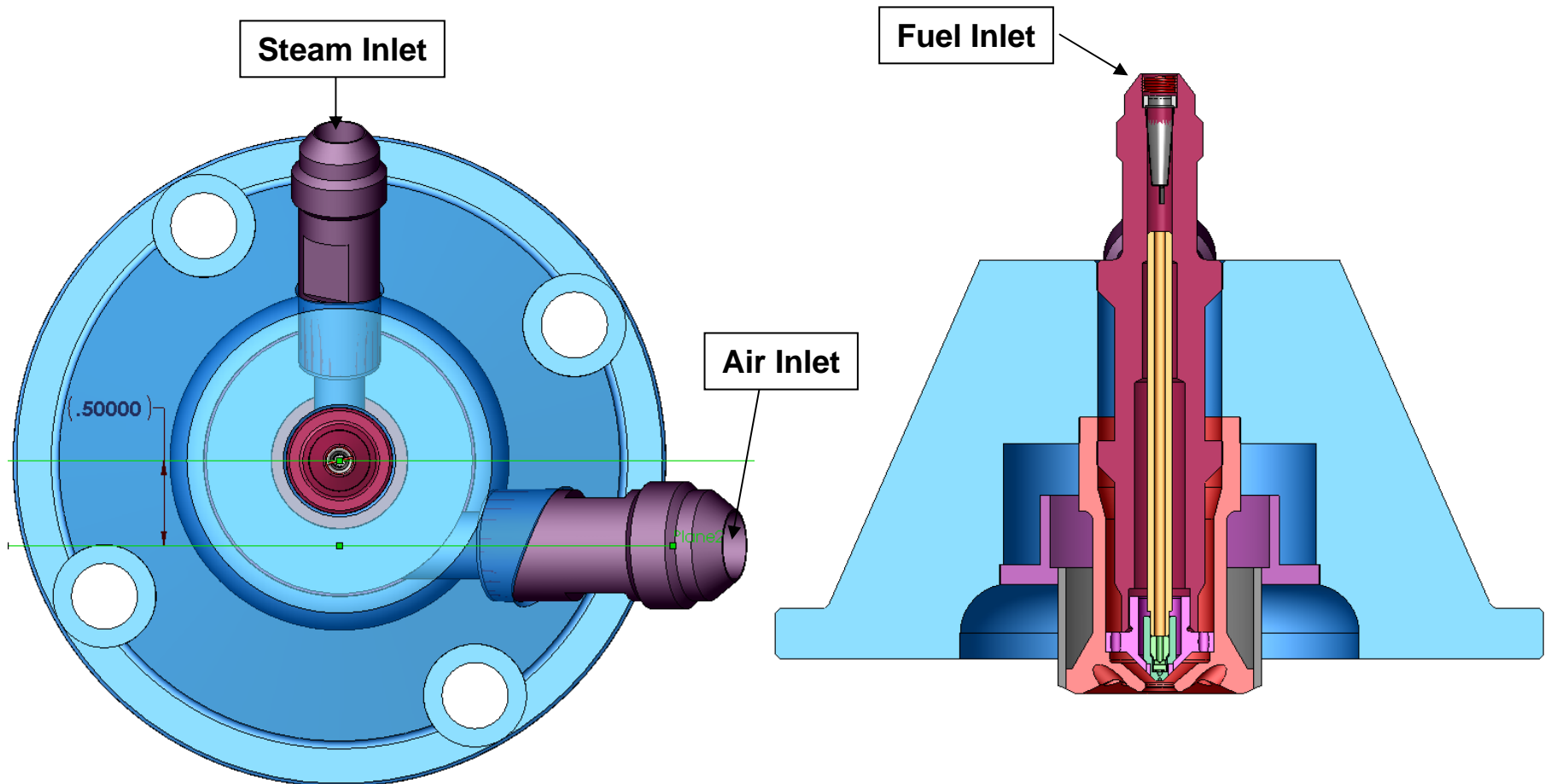
Jet Fuel SMD = 45 μm

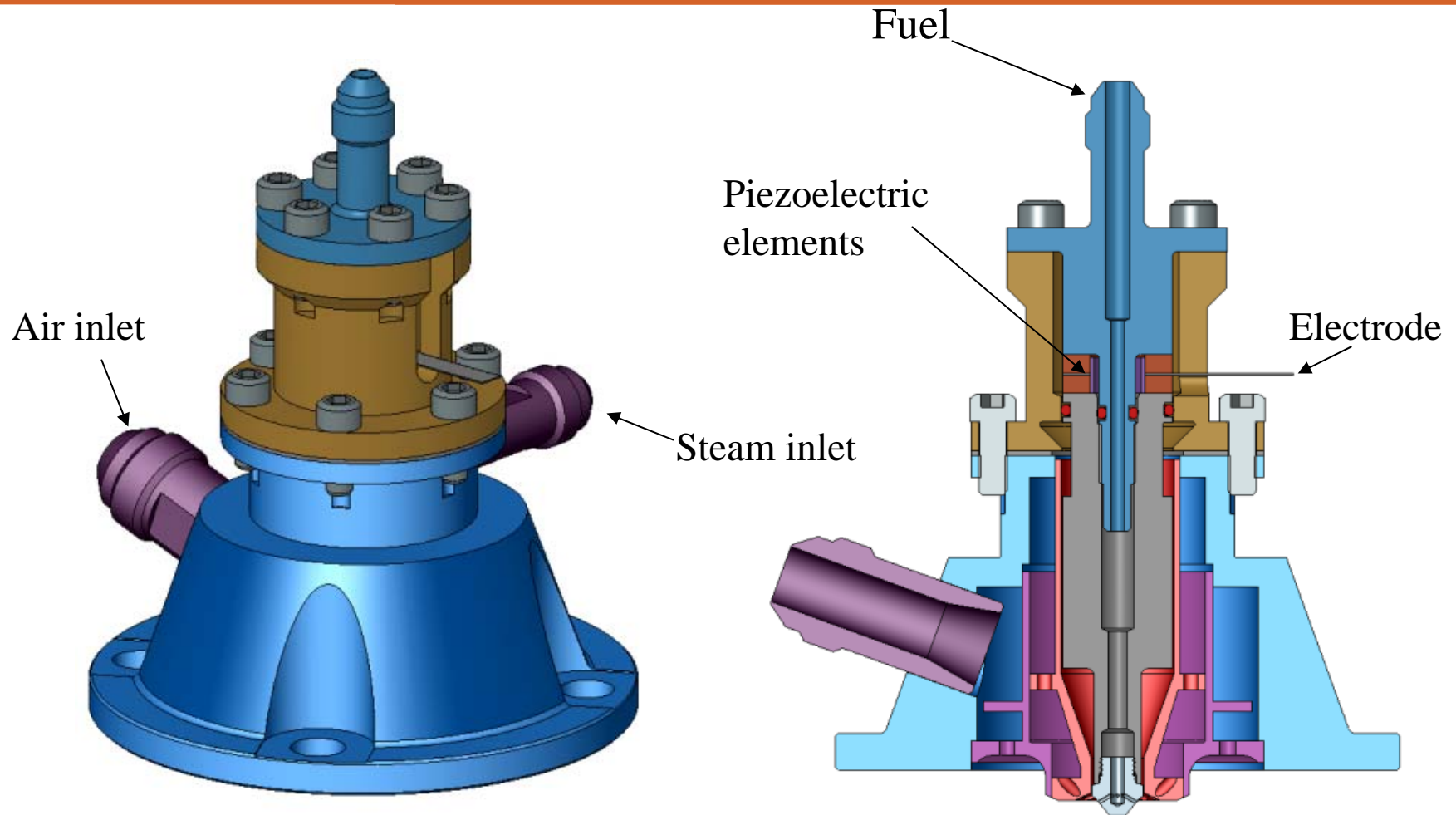
Diesel SMD = 55 μm

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- **Conduct a thorough evaluation of various injection and mixing concepts**
 - **Establish threshold and target performance data**
 - **Perform Design of Experiment (DOE) to map out the operating conditions for the most promising concepts**
 - **Utilize CFD and FEA tools to help predict and understand flow-field structure and injector/mixer performance**
 - **Perform detailed laser diagnostics for performance evaluation and design substantiation**
 - **Incorporate carbon-resistant or coke-tolerant design features**
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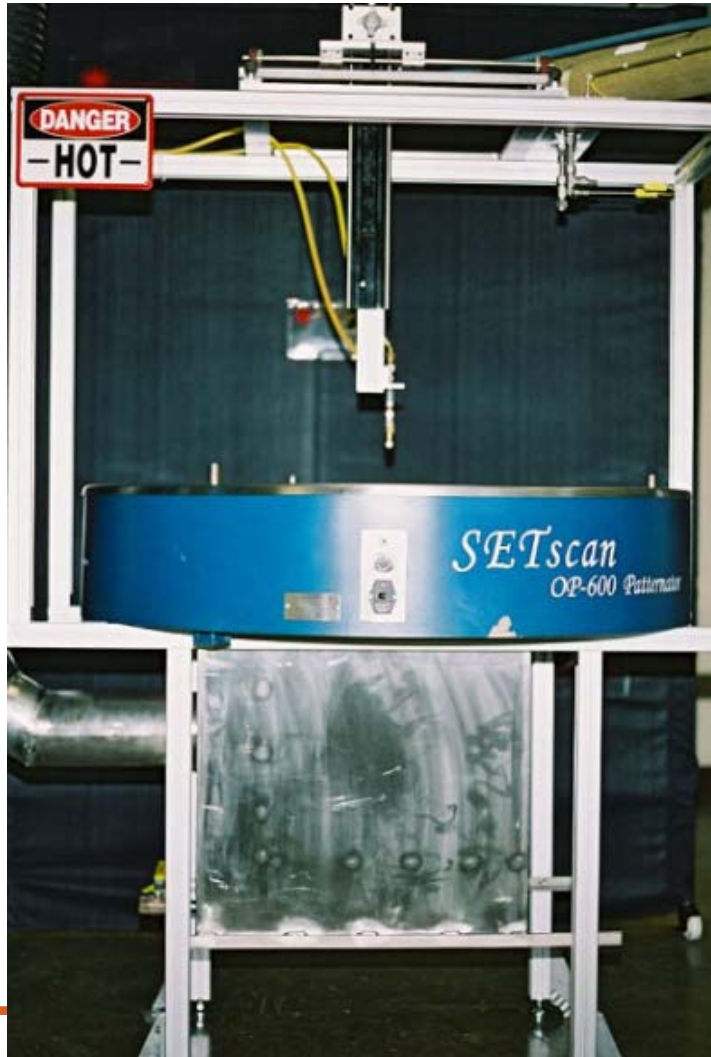
- ◆ **Multipoint Impingement Injector**
 - ◆ **Single-Point Steam or Air-assisted Simplex Injector**
 - ◆ **High-Energy Piezoelectric Simplex Injector**
 - ◆ **Preheating Simplex Fuel Injector**
 - ◆ **Pulse Modulated Fuel Injection**
 - ◆ **Effective Mixing Swirlers and Mesh Screens**
 - ◆ **Carbon Tolerant Design Features**
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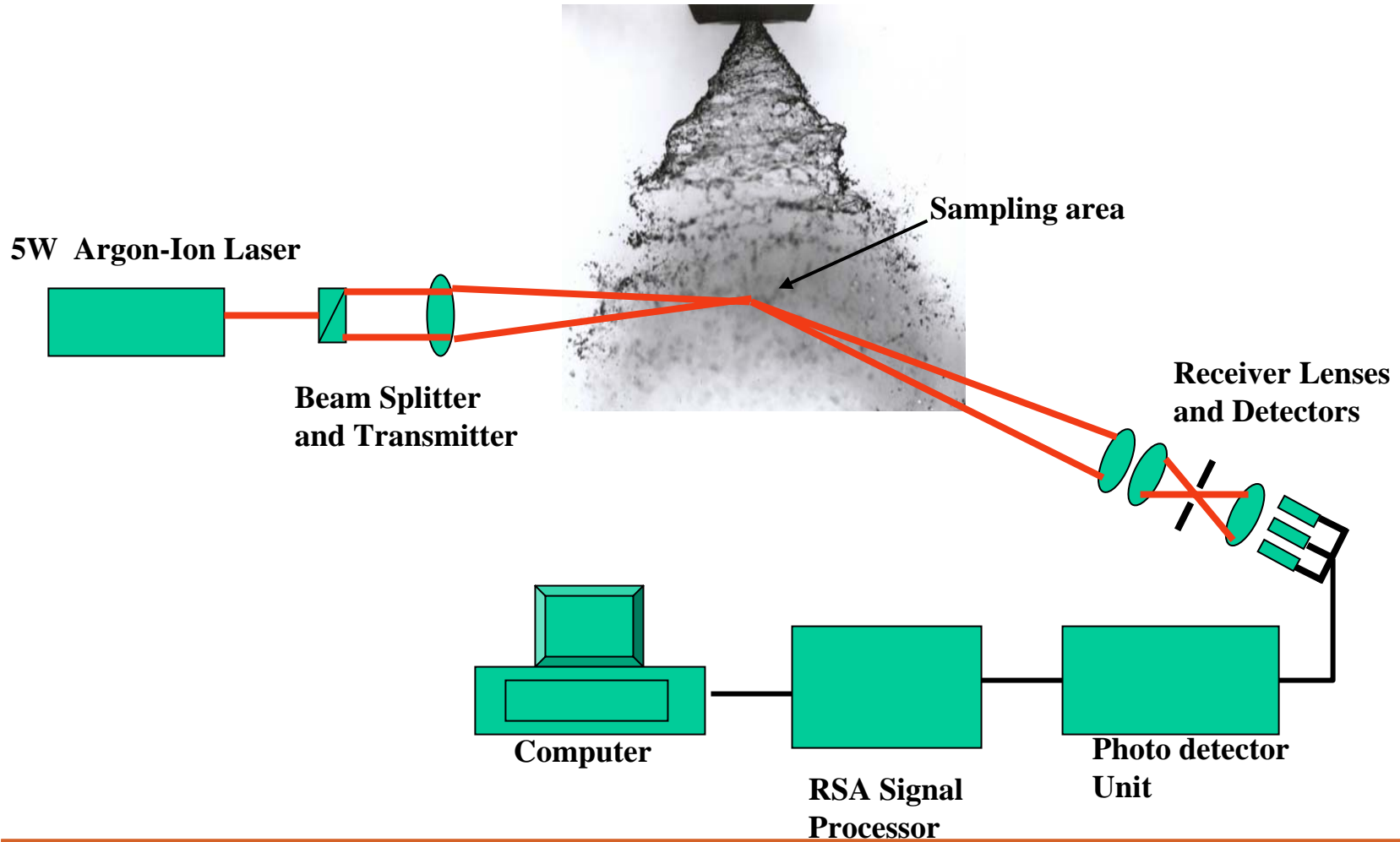


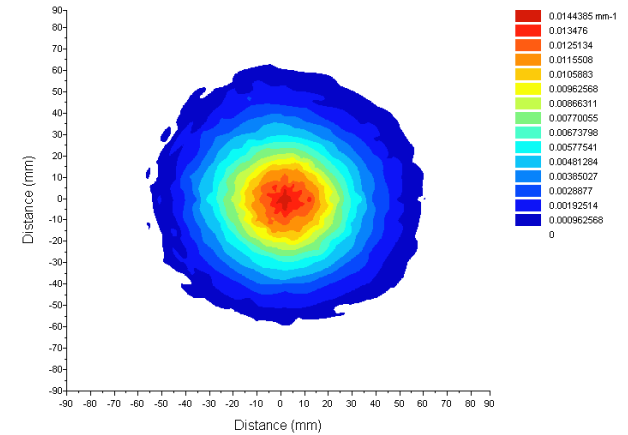
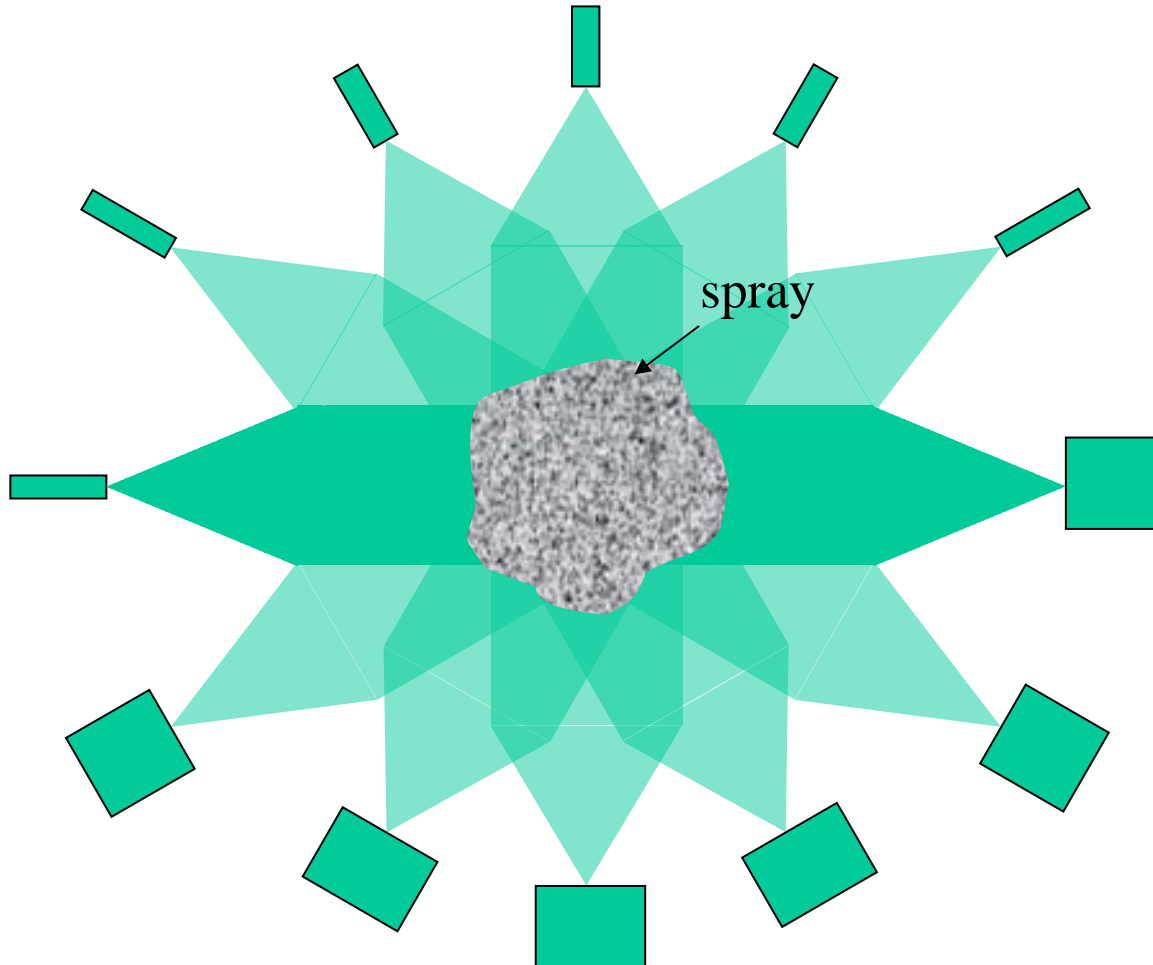


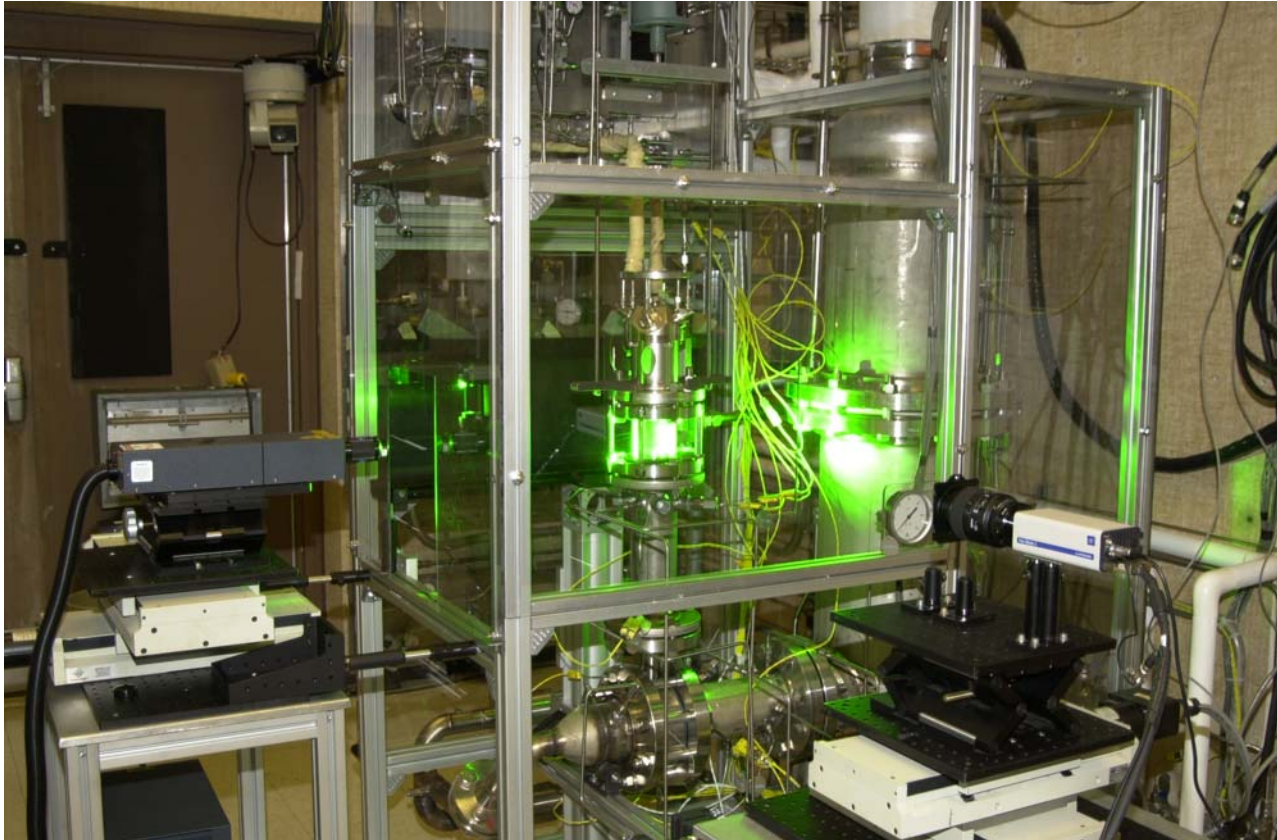


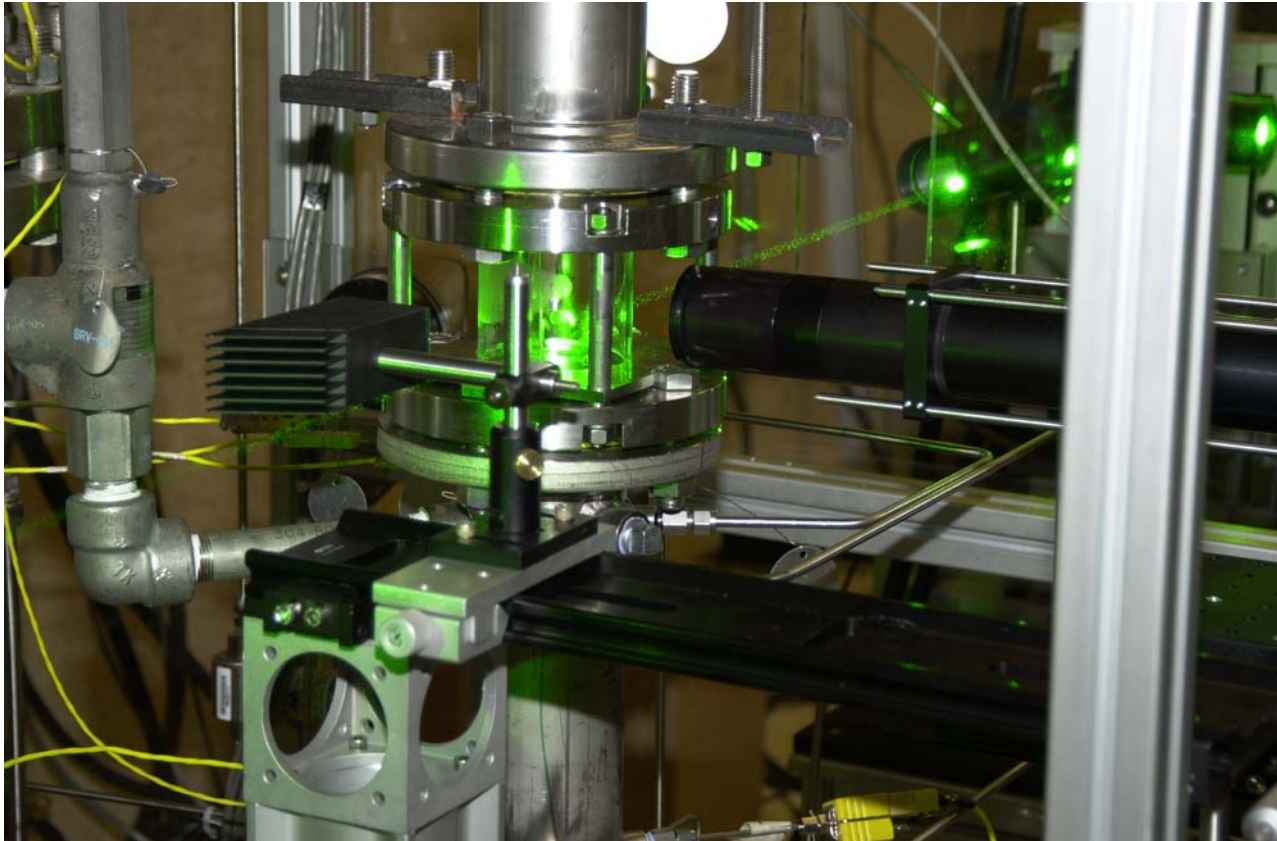
- ◆ **Advanced developmental machine shop**
 - ◆ **Test rig representative of 3~10 kW reformer operation**
 - ◆ **Phase Doppler Interferometry**
 - ◆ **SETscan Optical Patternator**
 - ◆ **Fuel Reformer Diagnostic Equipment from NASA Glenn**
 - Particle Imaging Velocimetry (PIV)
 - Raman Spectroscopy
 - Gas Chromatography
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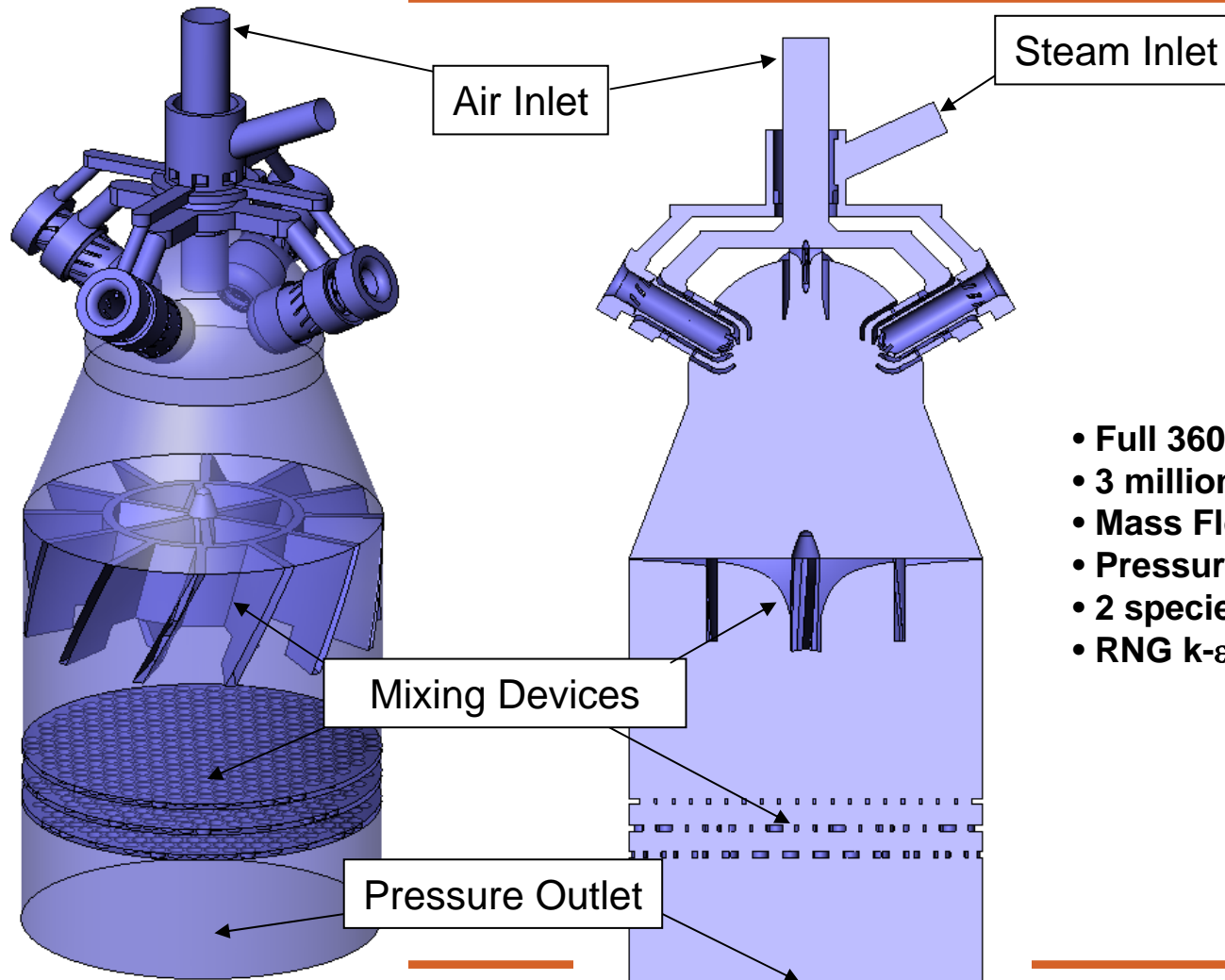






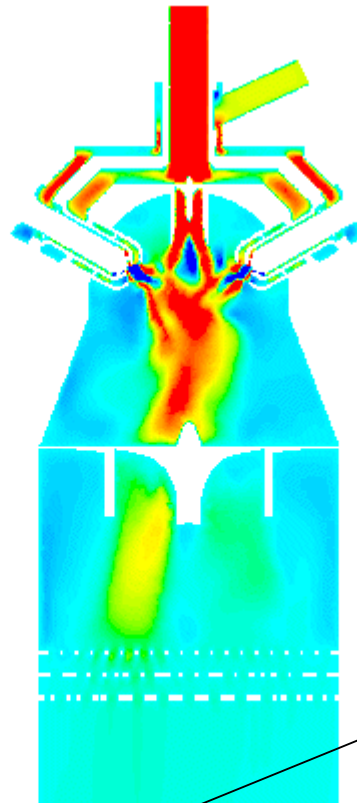
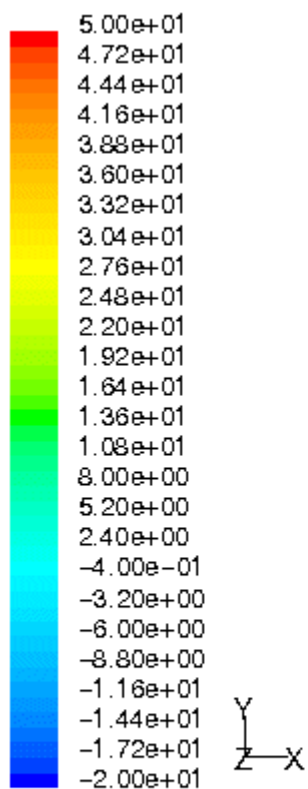


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- **Constructed a hot flow test rig for performance development and concept screening**
 - **Completed the evaluation of the multipoint impingement injector concept in March 2005**
 - **Assembled a gas-assisted simplex injector for detailed performance evaluation**
 - **Fabricated a prototype piezoelectric injector for evaluation of driver electronics and injector operating parameters**
 - **Analyzed various injector and mixing chamber configurations for improved mixing capability and thermal management**
 - **Conducted detailed flow field measurements using phase Doppler interferometry, SETscan optical patternator, Raman spectrometer and porcupine thermocouples.**
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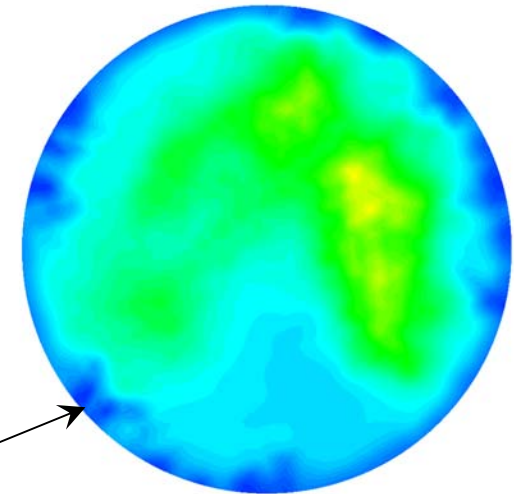
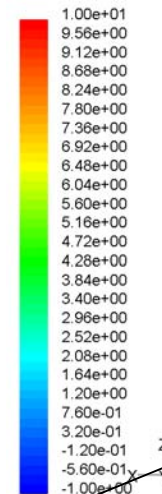


- Full 360° model
- 3 million grid cells
- Mass Flow Inlet Boundaries
- Pressure Outflow Boundaries
- 2 species (air, steam)
- RNG k- ϵ turbulence model

CFD Predicted Axial Velocity Contours (m/s)

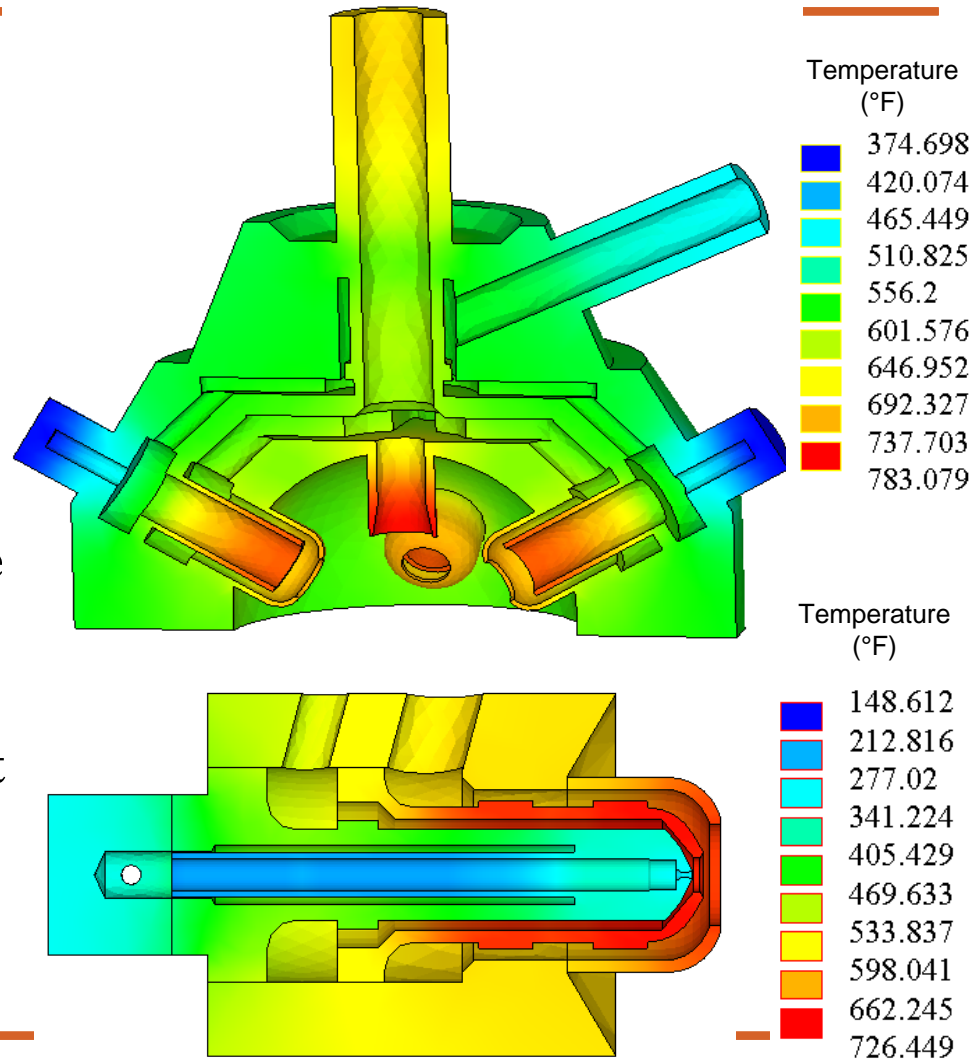


Air: 930 °F, 30 lb_m/hr
Steam: 550 °F, 12 lb_m/hr

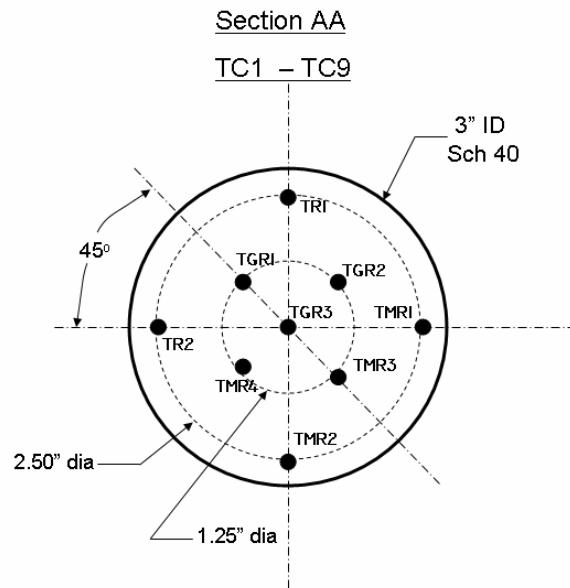


Time-averaged axial velocity
contours at the outlet boundary

- SolidWorks model directly imported into ANSYS
- Wetted wall temperature of the fuel circuit must not exceed 400°F.
- Internal wall temperature of the steam circuit must be above saturation temperature at the operating pressure.
- Temperature gradients of the metal must be low enough not to cause undesired thermal growth and stresses.



3" Test Section Spool – TC Layout



TC = ●
TYPE K

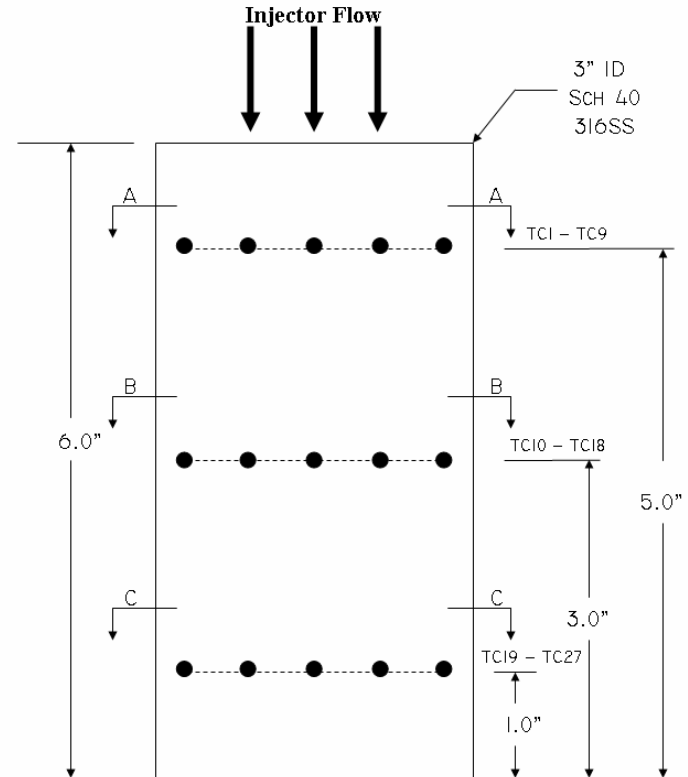
Note: Spool will use existing TC Input Channels from 10 kWATR Reactor (30 available)

Scale: 1.0" = 1.0"

Flanges Not Shown

TMT 3/12/05

3" Test Section Spool – TC Layout (Porcupine)



TC = ●
TYPE K

Total 27 TC's

Flanges Not Shown

TMT 3/12/05

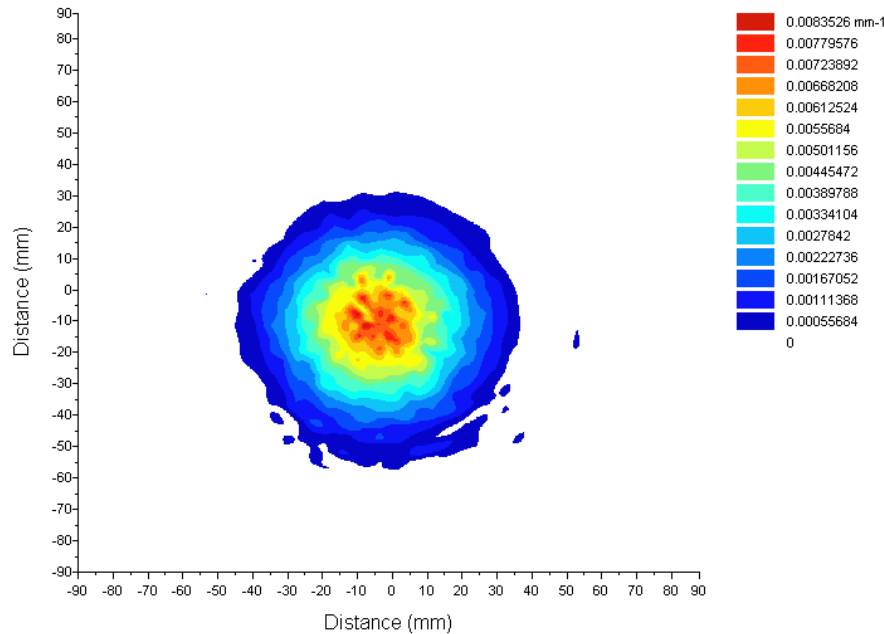
Scale: 1.0" = 1.0"

	Section A-A (1" downstream)			Section C-C (5" downstream)		
Test Point	Ave. (°F)	Max-Min. (°F)	UI(%)	Ave. (°F)	Max-Min. (°F)	UI(%)
Pt.1 - Fuel 5 pph, Air 25pph/930F, steam 10pph/550F	525	10	1.91	515	30	5.82
Pt.2 - Fuel 5 pph, Air 25 pph/930 F, steam 6.5pph/550F	549	26	4.74	538	34	6.32
Pt.3 - Fuel 5 pph, Air 25 pph/930 F, steam 3 pph/550F	554	21	3.74	545	29	5.32
Pt.4 - Fuel 1.5 pph, Air 7.5 pph/930 F, steam 3 pph/550 F	551	23	4.17	544	25	4.59
Pt.5 - Fuel 2 pph, Air 12 pph/930 F, steam 5 pph/550 F	553	20	3.62	547	23	4.20

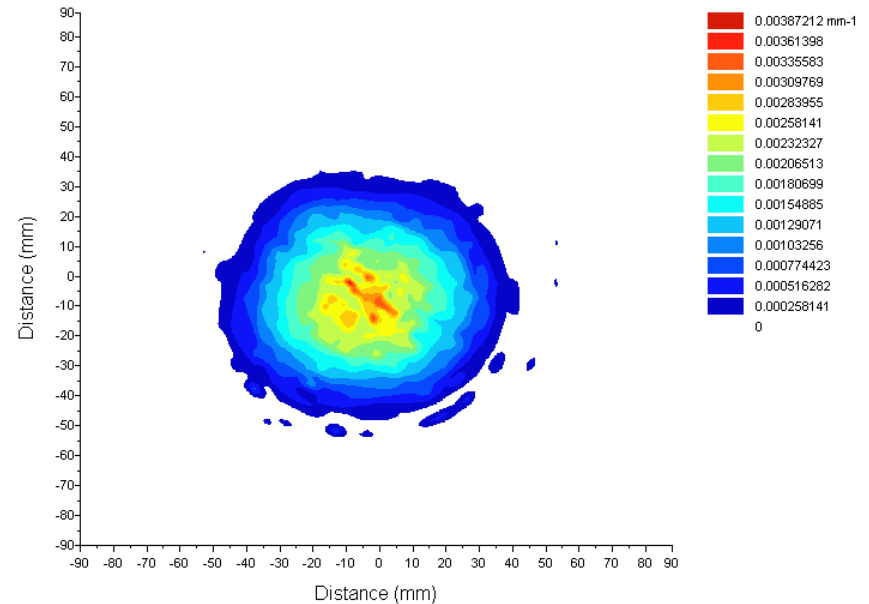
Uniformity Index $UI = (Max.-Min.)/Average$

Temperature is considered very uniform for UI less than 5% .

Cold Flow Tests Using SETscan Optical Patternator

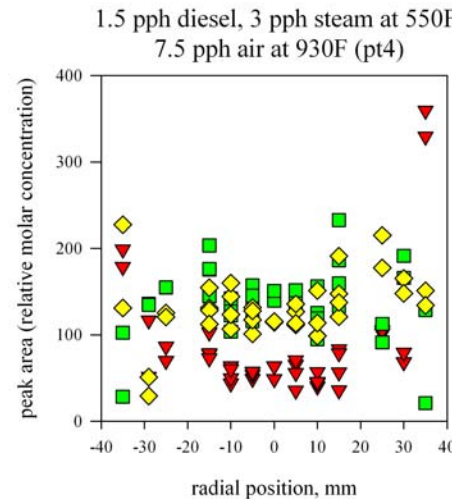
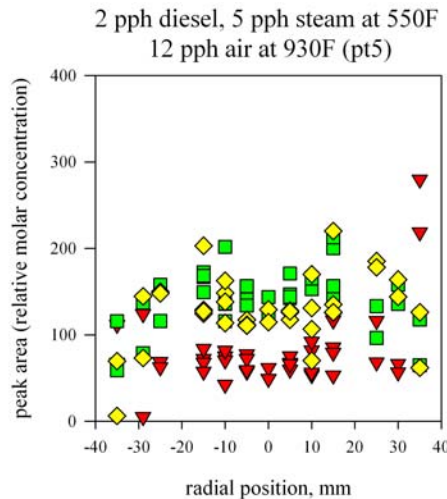
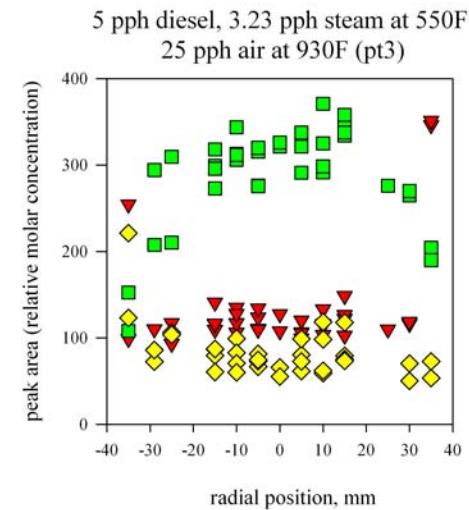
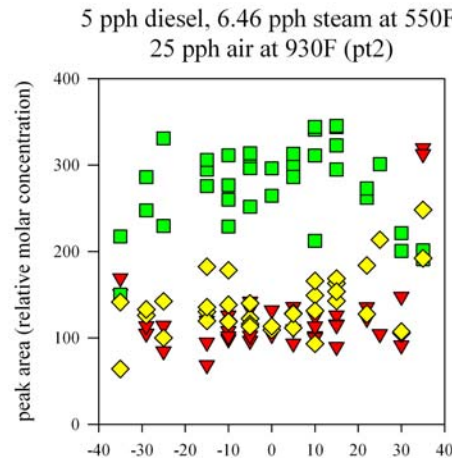
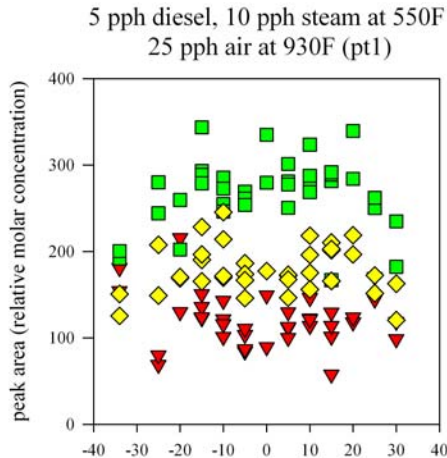


2 pph fuel, 15 pph steam, 15 pph air



2 pph fuel, 5 pph steam, 15 pph air

Note: Shop air was used in the steam circuit for cold flow patternation tests.

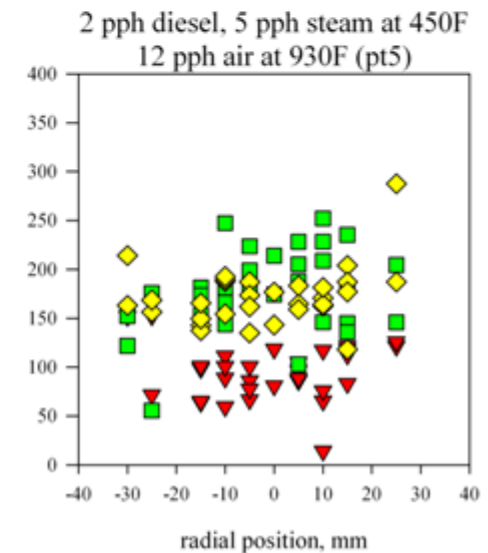
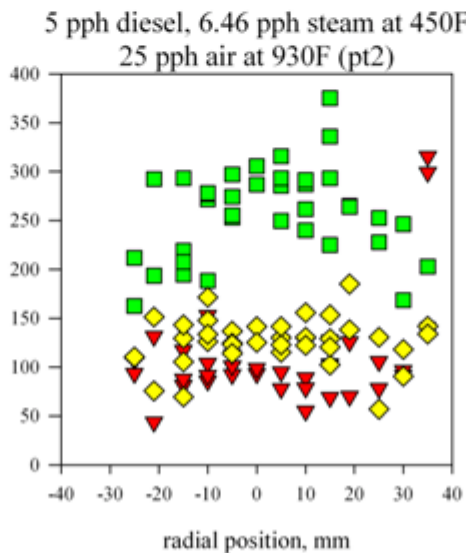
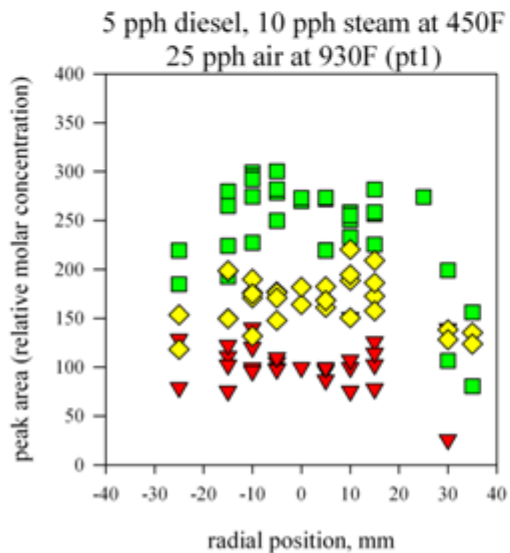
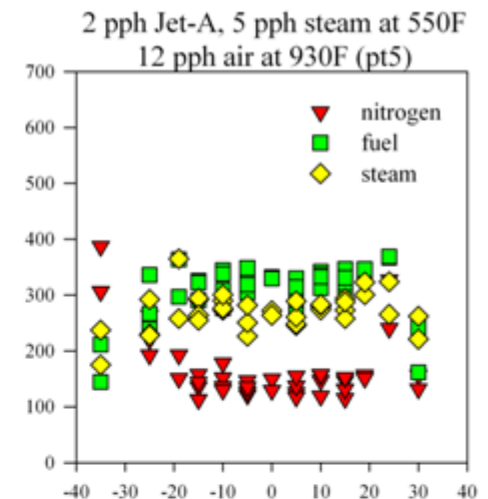
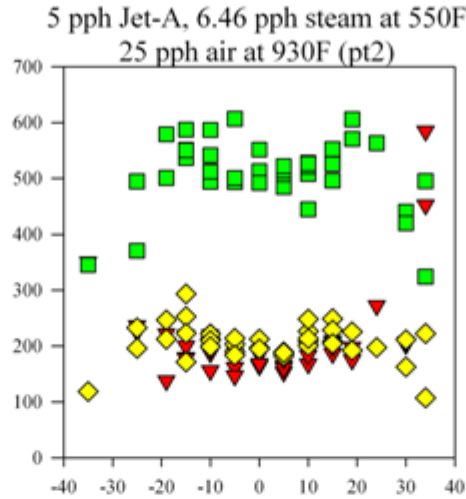
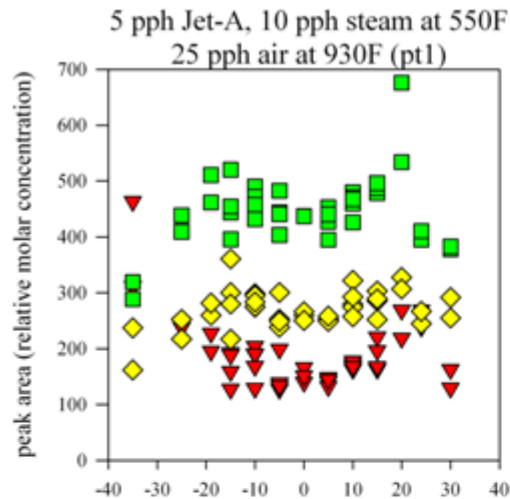


▼ nitrogen
■ fuel
◆ steam

Multipoint impingement injector

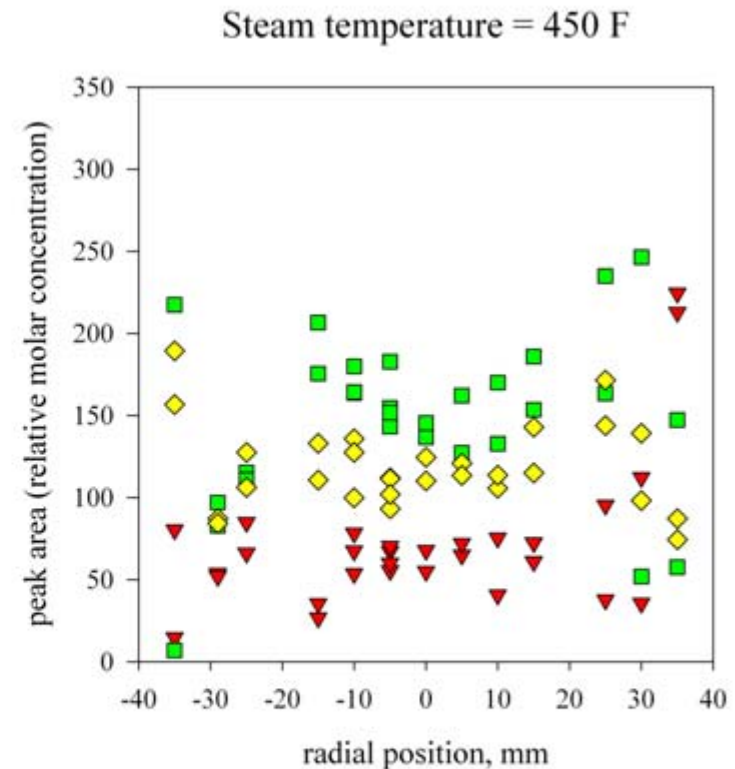
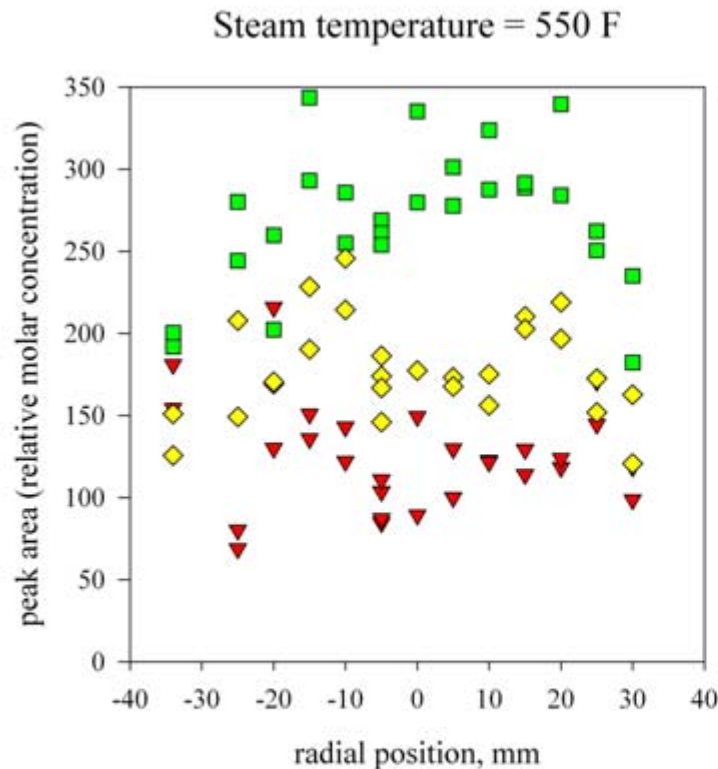
-2 mixing chamber without mixing devices

Diesel Fuel



-1 mixing chamber with mixing devices

Diesel Fuel: 5 pph, Air Flow: 25 pph at 930°F, Steam Flow: 10 pph



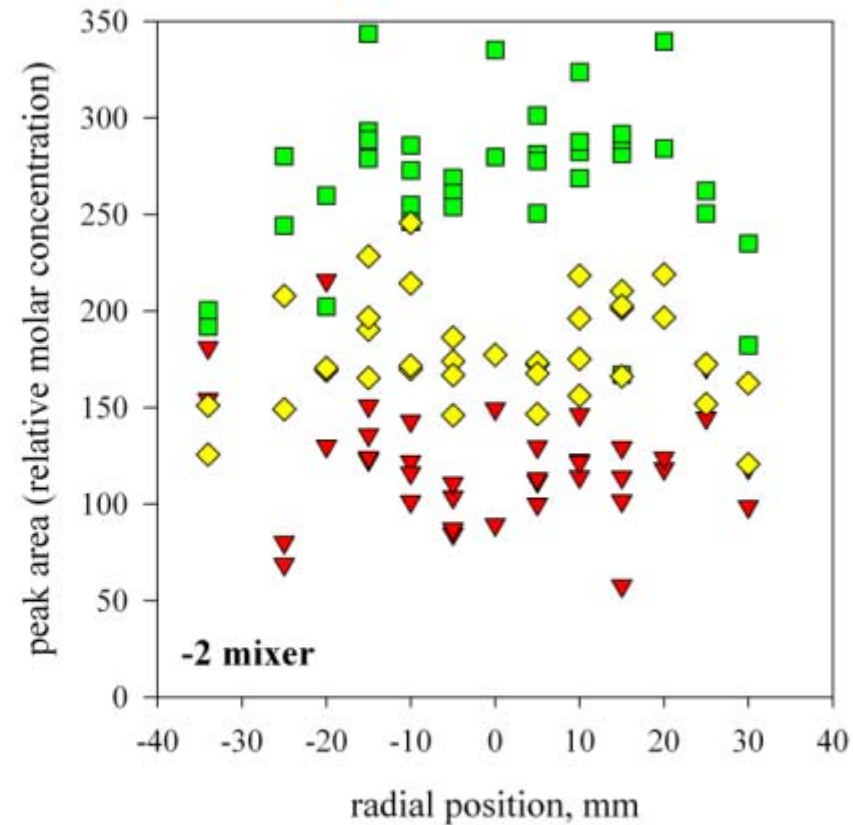
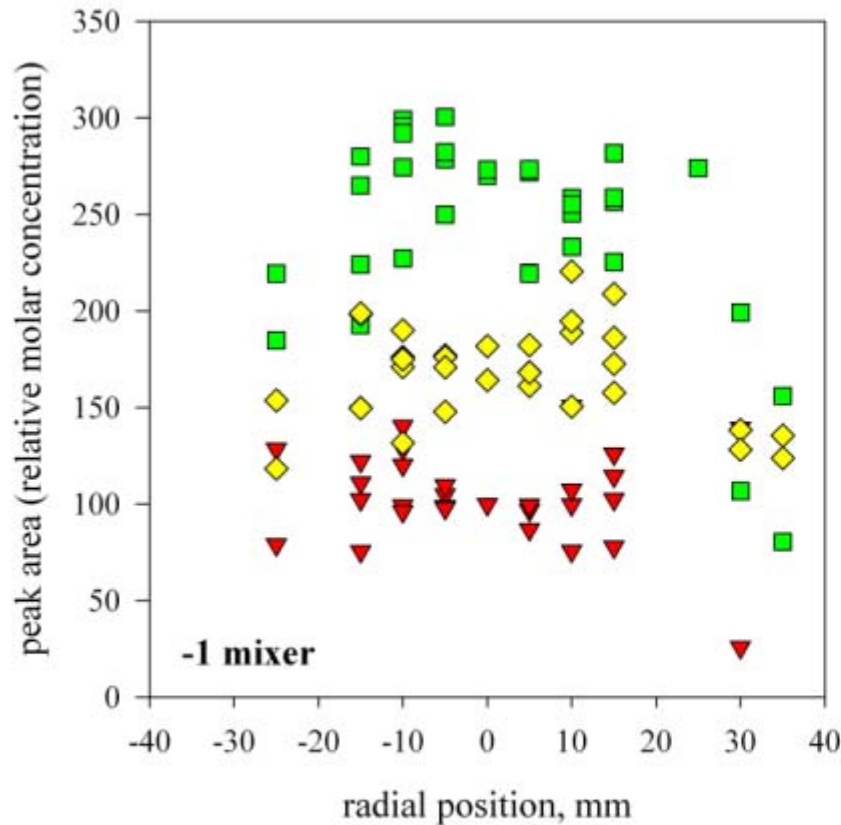
▼ nitrogen
■ fuel
◆ steam

-2 mixing chamber without mixing devices

Diesel Fuel: 5 pph, Air Flow: 25 pph at 930°F, Steam Flow: 10 pph at 450°F

-1 chamber with mixing devices

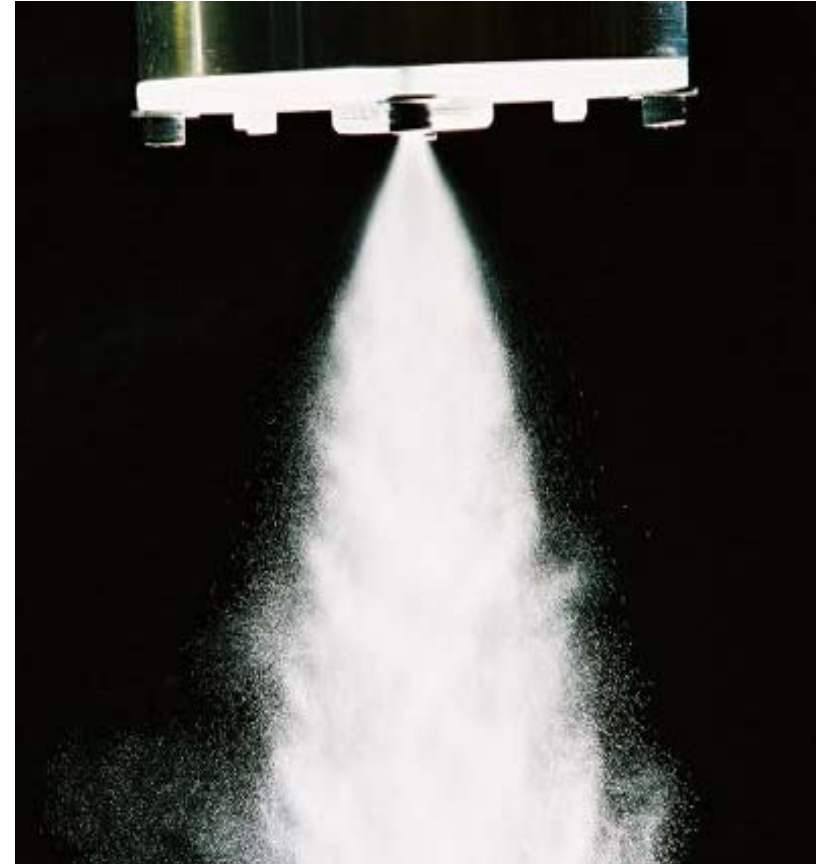
-2 chamber without mixing devices



▼ nitrogen
■ fuel
◆ steam

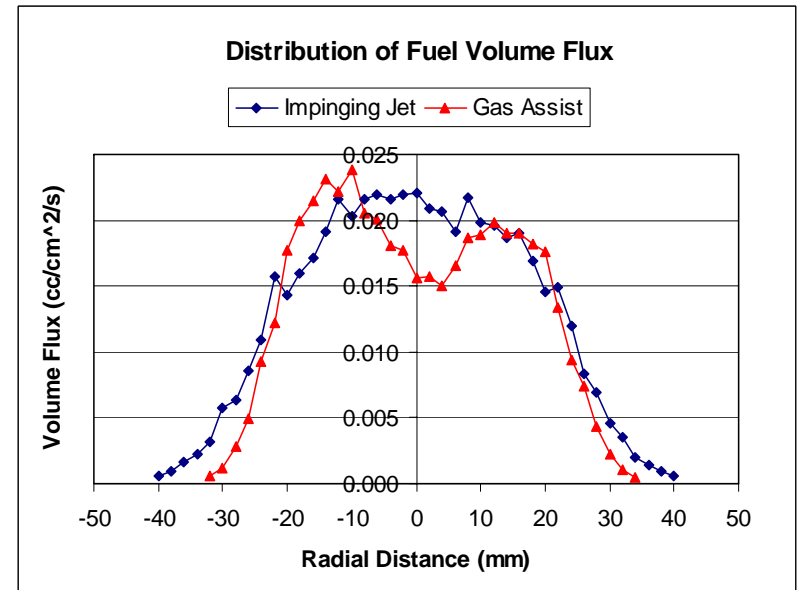
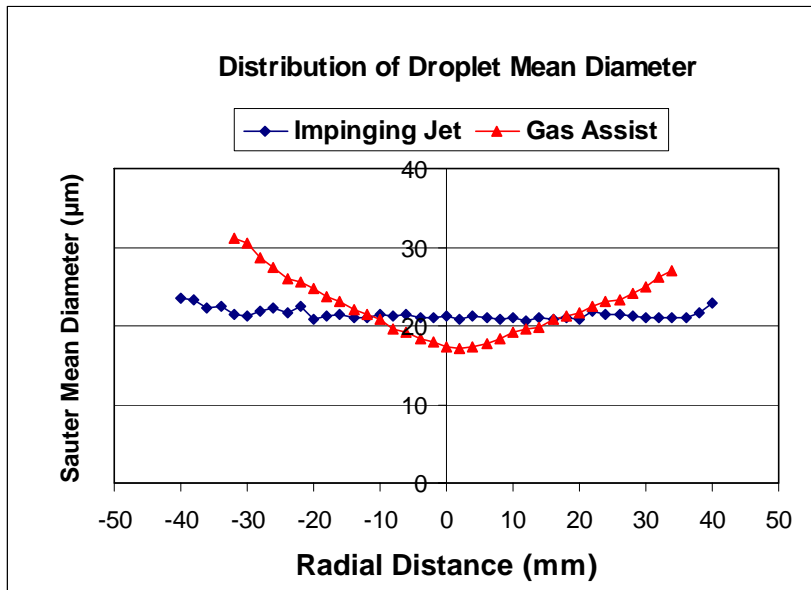
- Present investigation allowed us to evaluate the effect of fuel type, mixing chamber configuration, steam temperature and operating conditions on injector performance.
 - All test conditions exhibited relatively uniform temperature and species distributions.
 - Higher steam temperature appears to provide stronger Raman signals and more uniform mixture distribution in the central region.
 - The overall signal strength for diesel fuel is lower than Jet fuel due to different physical properties. Jet fuel distribution also appears to be both more uniform and more repeatable.
 - Mixing devices do not appear to provide any noticeable benefit to the multipoint impingement injector concept.
 - Species distribution appears to be more scattered as steam/carbon ratio decreases when using mixing devices.
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- Simple, more robust design and less prone to internal coking
- Easily adaptable to a different reformer
- Narrow spray angle to minimize carbon deposition on the chamber wall
- Excellent atomization when there is adequate gas inlet pressure
- Mixing devices are required for uniform mixture distribution



Fuel: 5 pph, Steam: 10 pph (using air), Air: 25 pph

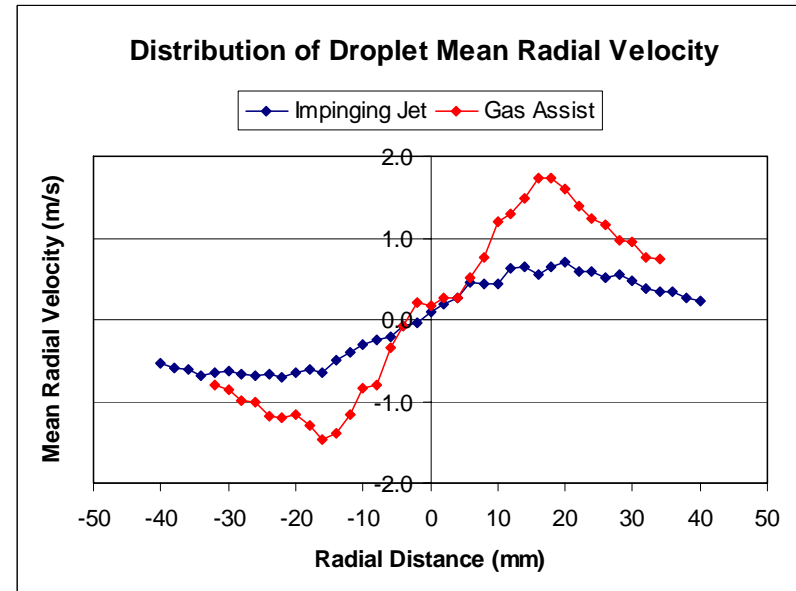
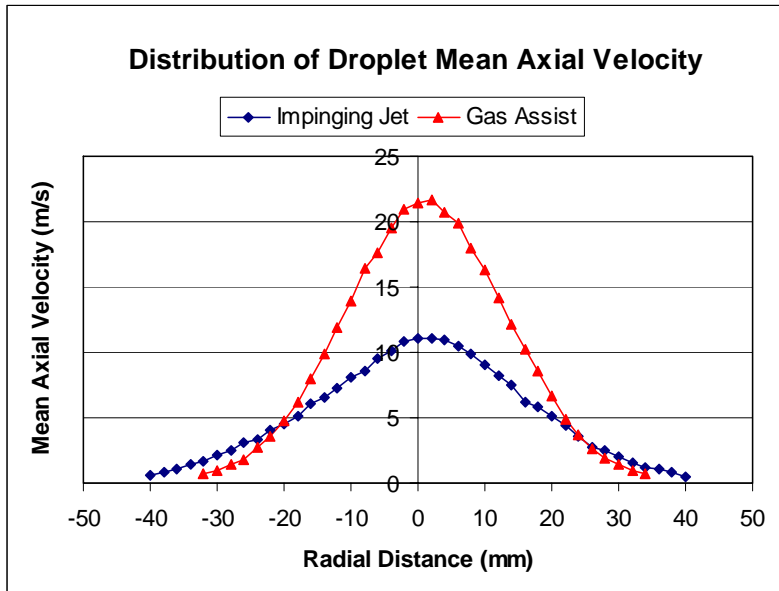
Simulated Cold Flow Tests



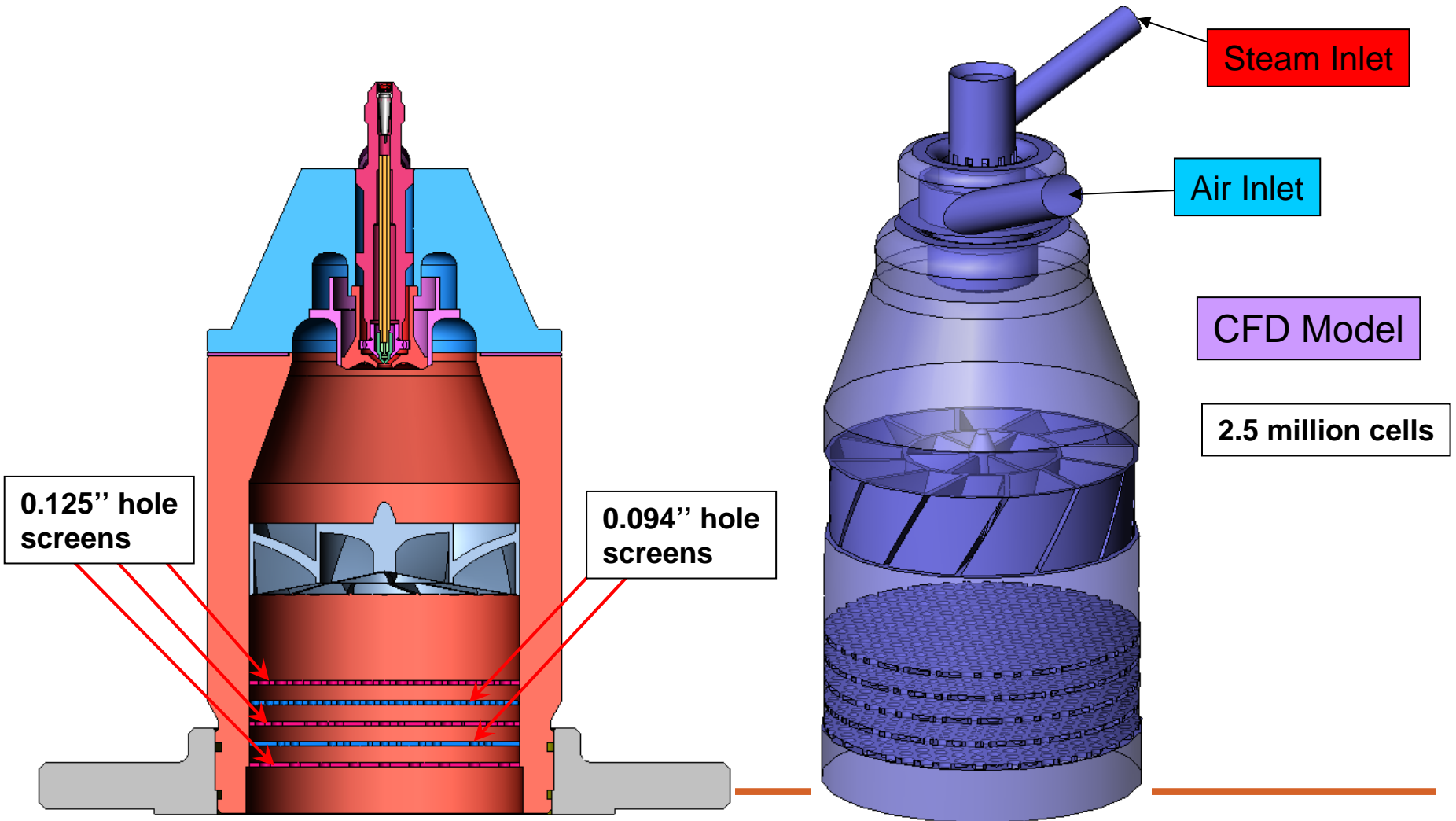
Measurement Distance: 3 inches from injector discharge

Fuel: 5 pph, Steam: 10 pph, Air: 25 pph

Simulated Cold Flow Tests

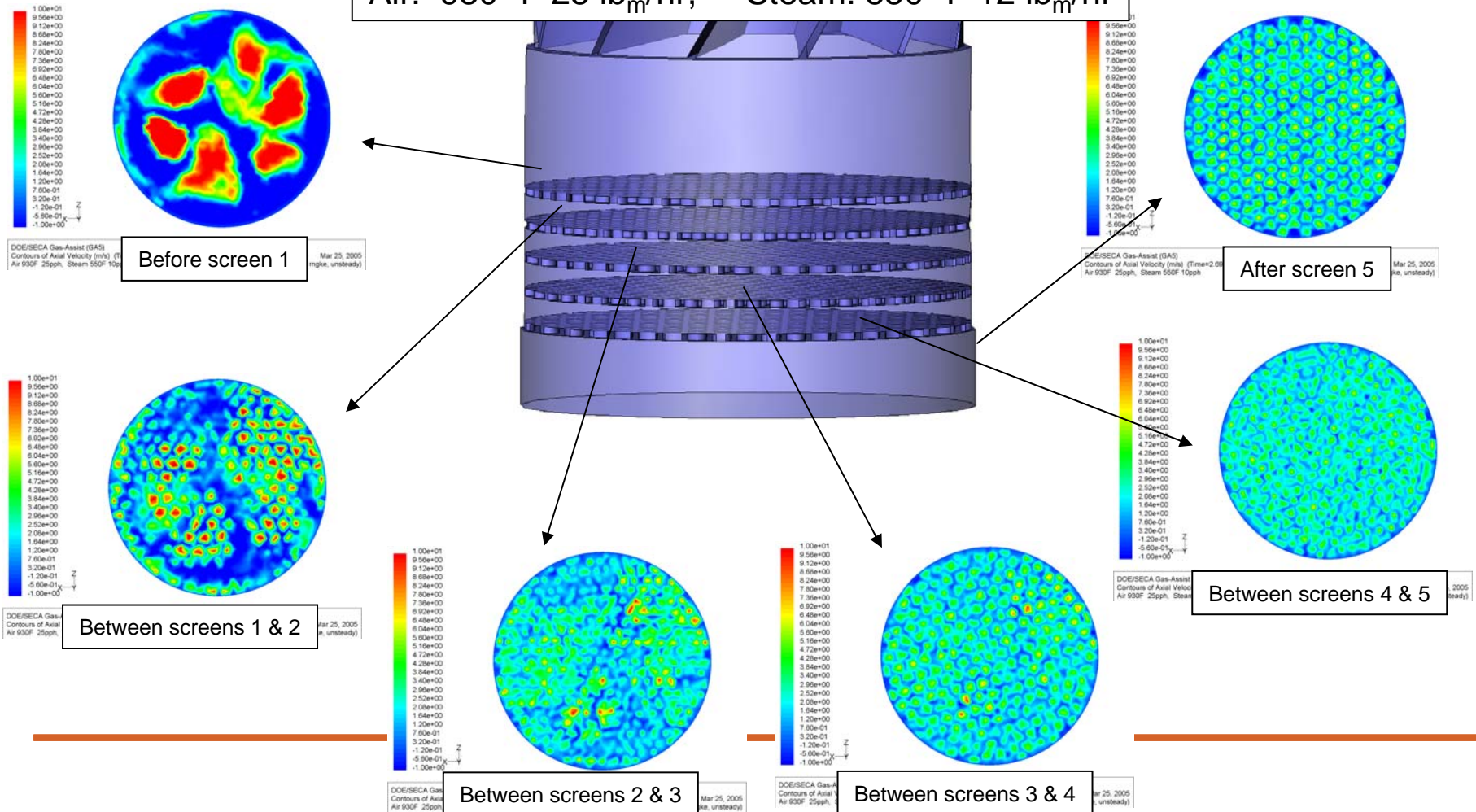


Measurement Distance: 3 inches from injector discharge



CFD Flow Field Results for Gas Assist Injector/Mixer

Axial Velocity Contours (range set -1 to 10 m/s)
Air: 930 °F 25 lb_m/hr, Steam: 550 °F 12 lb_m/hr



- **Excellent atomization for low flow rate applications**
- **High turndown ratio possible (>10:1)**
- **Power consumption needs to be minimized**
- **Drift of operating frequency and spray quality due to changes of temperature and flow rate**
- **Great potential for pulse modulated injection**



2 pph fuel operated at 46 kHz frequency

- **Evaluation of the single-point gas assisted simplex injector/mixer concept will be completed in May 2005.**
 - **The high-energy piezoelectric injector will be constructed to meet the third quarterly milestone in June 2005.**
 - **Evaluation of the preheating simplex injector/mixer concept will be completed in September 2005.**
 - **Laser diagnostics will be performed at NASA Glenn using a reformer test rig for two injector concepts in October 2005.**
 - **The effect of pulse modulated spray will be investigated by December 2005.**
 - **Phase I program will be completed and final report submitted to DOE by March 2006.**
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