



Sandia National Laboratories

# Engineered Glass Composites for Sealing Solid Oxide Fuel Cells

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# Outline

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- Composite approach to SOFC sealing
- Glass and composite properties
- Composites applied to different seal designs
- Demonstration of different seal properties
- Summary and conclusions

# Composite seals can be engineered to provide a wide range of chemical and mechanical properties

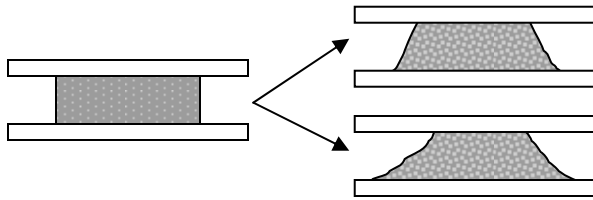
- Composite approach allows glass and filler to be optimized independently
- Glass phase is above its  $T_g$  at SOFC operating temperature to reduce thermal and mechanical strains
- Control viscosity, CTE, etc. by adding unreactive powder
- Volume fraction of glass phase can be reduced to minimum for seal

$$\alpha = \frac{\alpha_1 K_1 V_1 + \alpha_2 K_2 V_2}{K_1 V_1 + K_2 V_2}$$

$$\eta = \left( 1 + \frac{\kappa \phi}{1 - \left( \frac{\phi}{\phi_{\max}} \right)} \right)^2$$

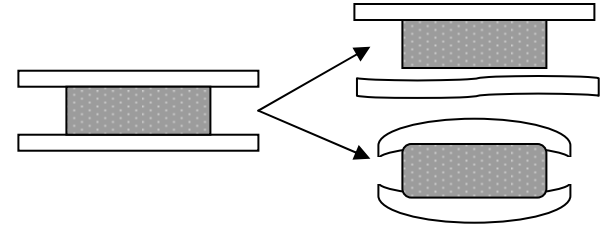
# Glass composites allow us to design for specific seal properties

## Viscosity



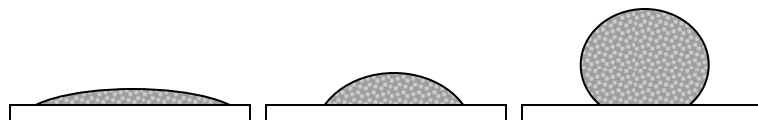
- Flow of glass composite
- Creep of seal

## Coefficient of thermal expansion

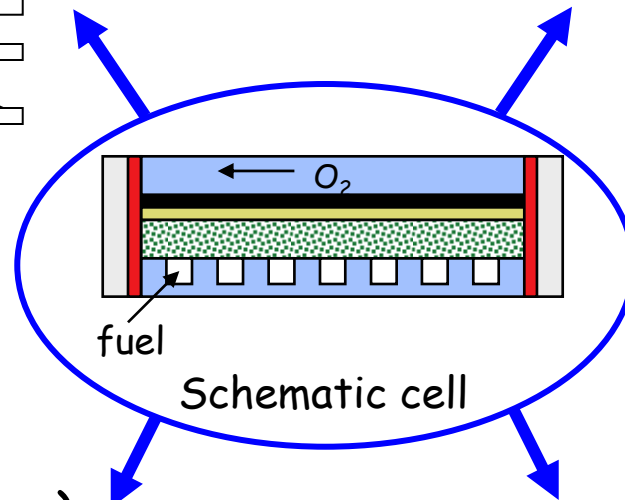


- Residual stresses
- Interfacial decohesion

## Wettability (adhesion)



- Contact angle
- Interfacial strength



fuel

Schematic cell

- anode
- electrolyte
- cathode
- interconnect
- manifold
- sealant

## Interfacial reaction



- Sealing and high temp processes:
- Growth of interfacial rx layer
  - Potential dissolution of additive
  - Crystallization of glassy phase

# We are studying a wide variety of glass/powder additive composites

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15 Glass compositions

5 Ceramic powders

3 Metallic powders

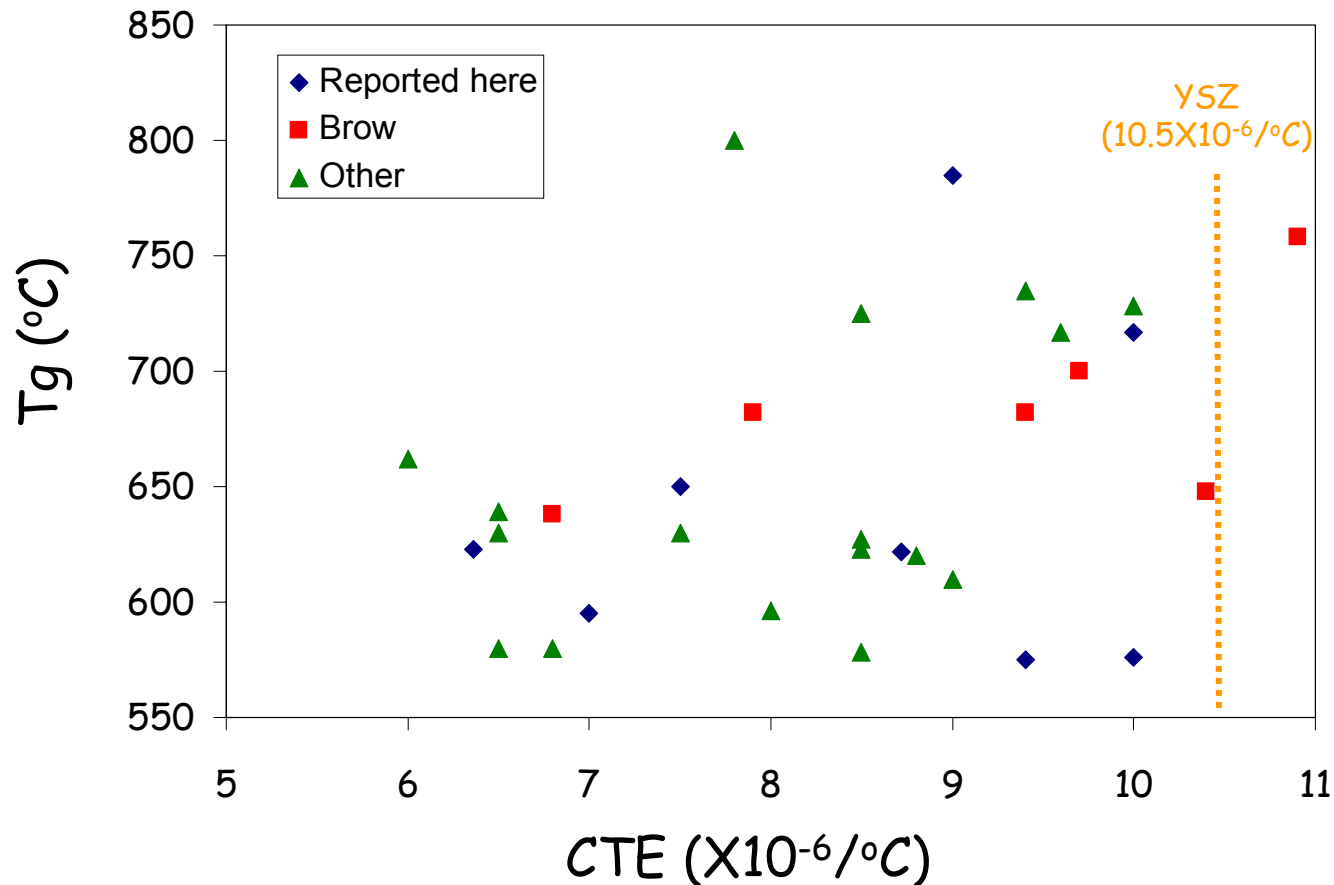
5 Particle sizes

2 Particle aspect ratios

7 Volume fractions of additive

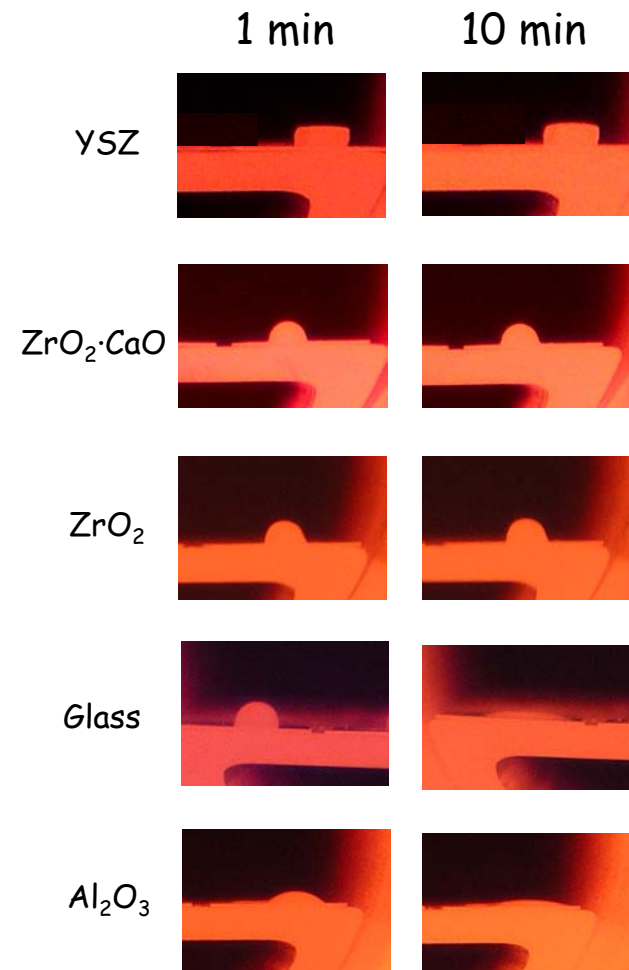
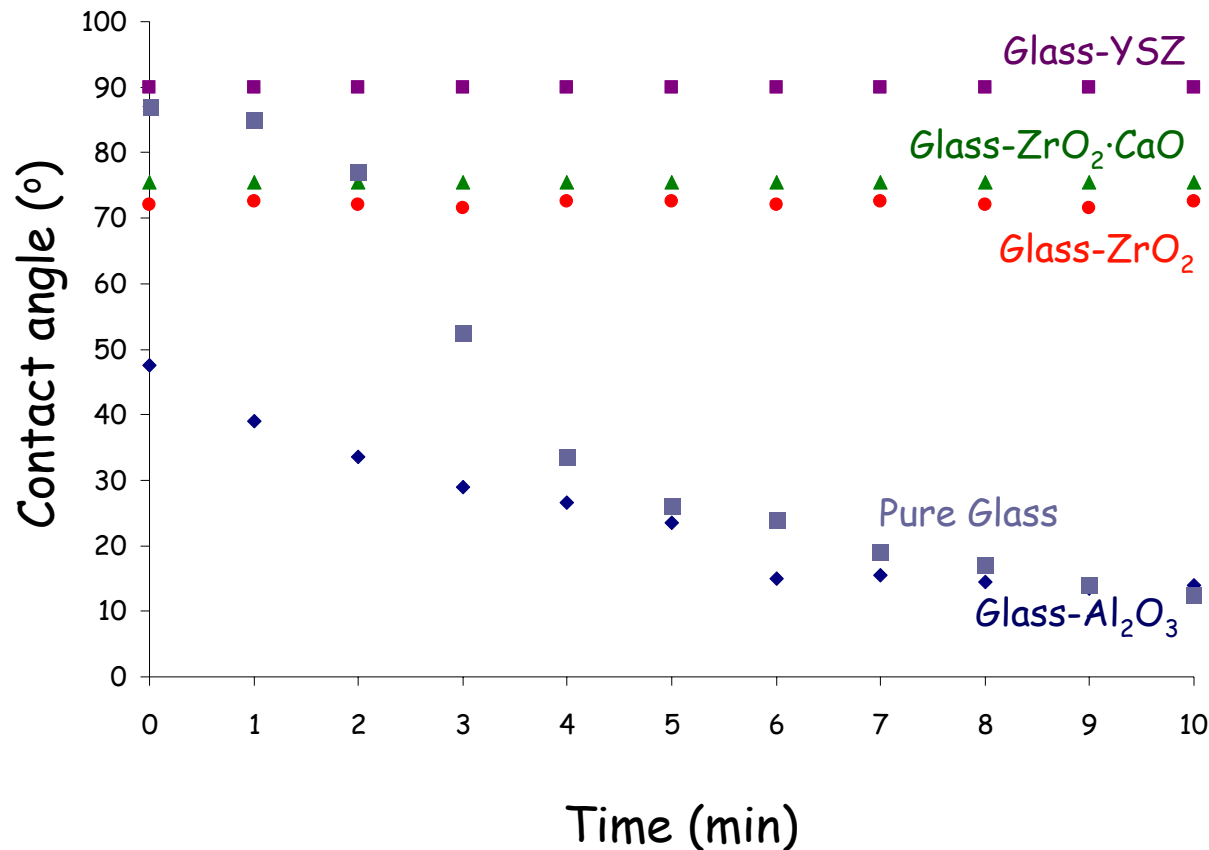
6 Sealing temperatures

# We are considering glasses with a wide range of properties

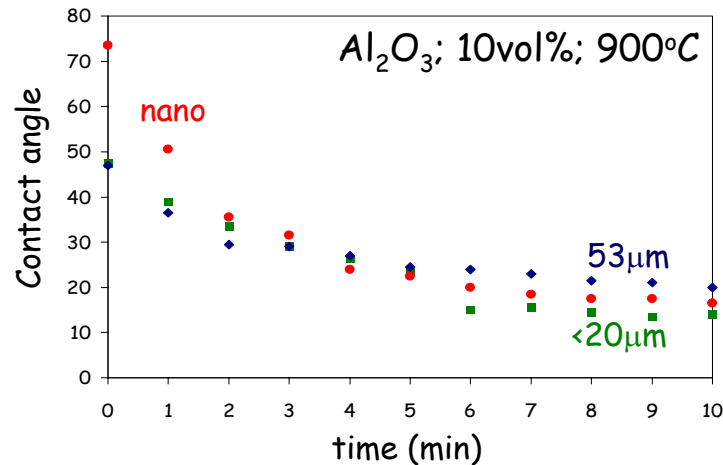


# Wetting and flow can be controlled by varying the ceramic powder additive

(Glass 14a; 900°C; 10vol%; powder < 20 μm)



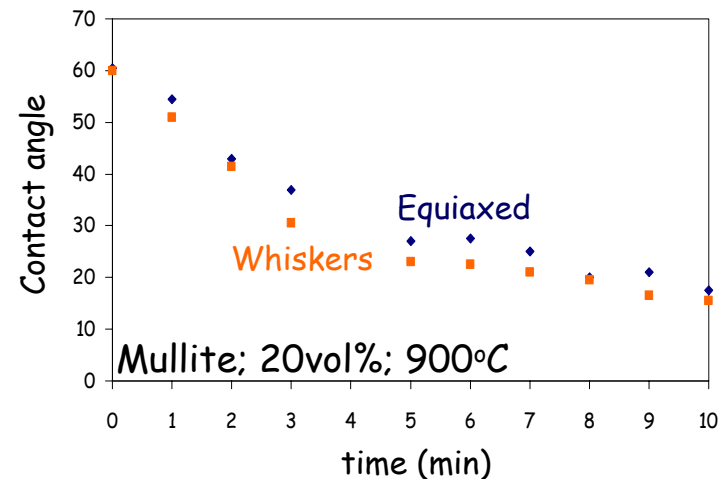
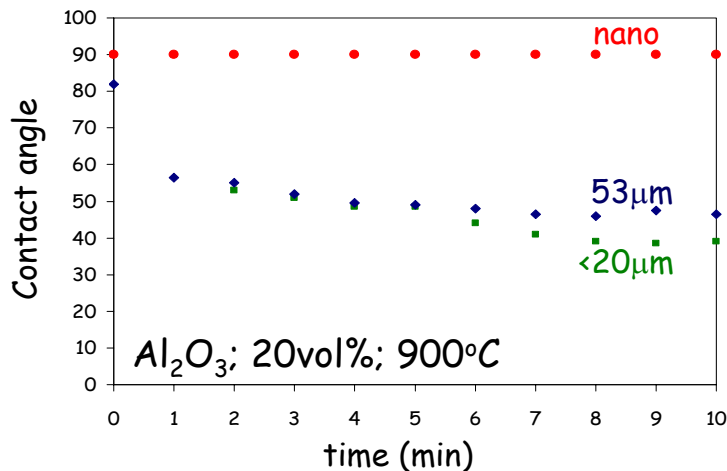
# Glass composite viscosity varies with amount and size of filler particles



Viscosity increases with decreasing filler particle size and with increasing filler concentration

$$\eta = \left( 1 + \frac{\kappa\phi}{1 - \left( \frac{\phi}{\phi_{\max}} \right)} \right)^2$$

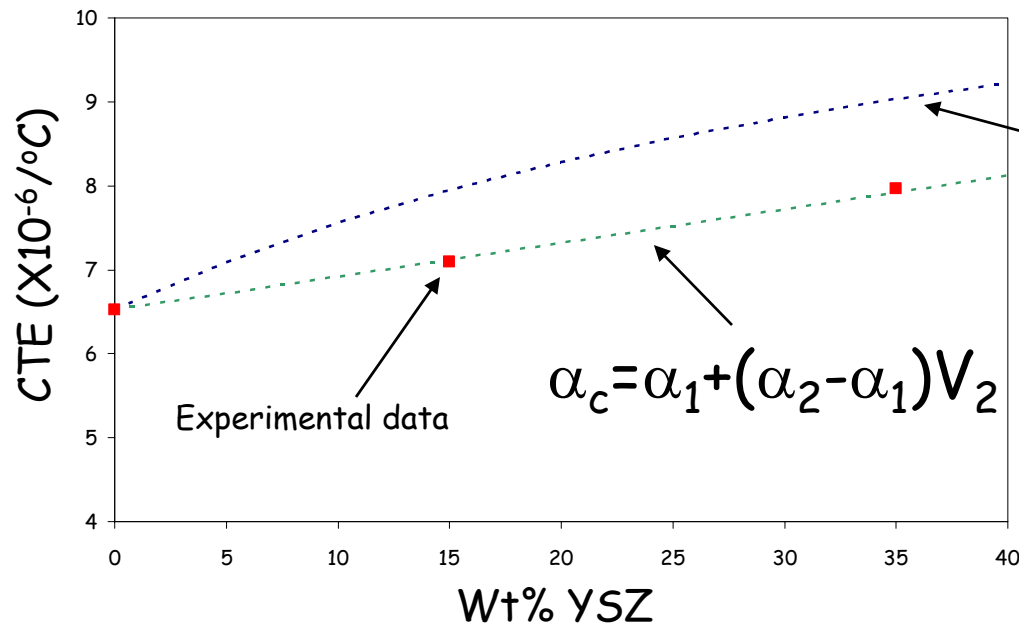
$K \propto 1/\text{particle size}$   
 $\phi\Phi = \text{particle packing density}$   
 $\phi_{\max}$  (volume fraction)





# Composite coefficient of thermal expansion varies with ceramic addition

Composite CTE depends on individual CTE and modulus values



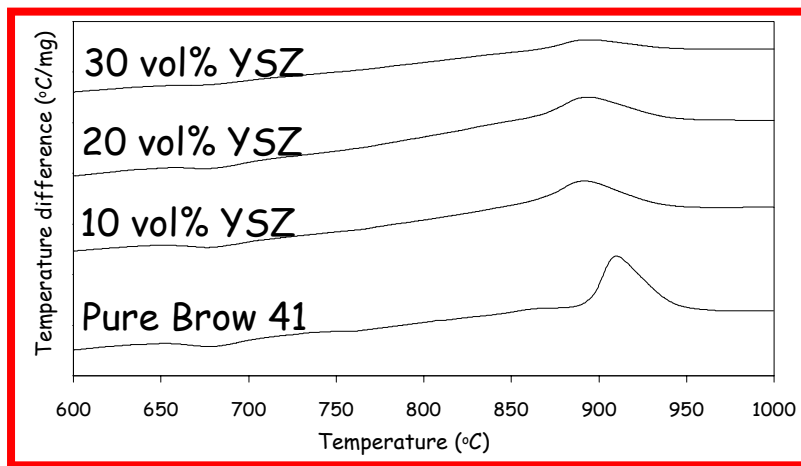
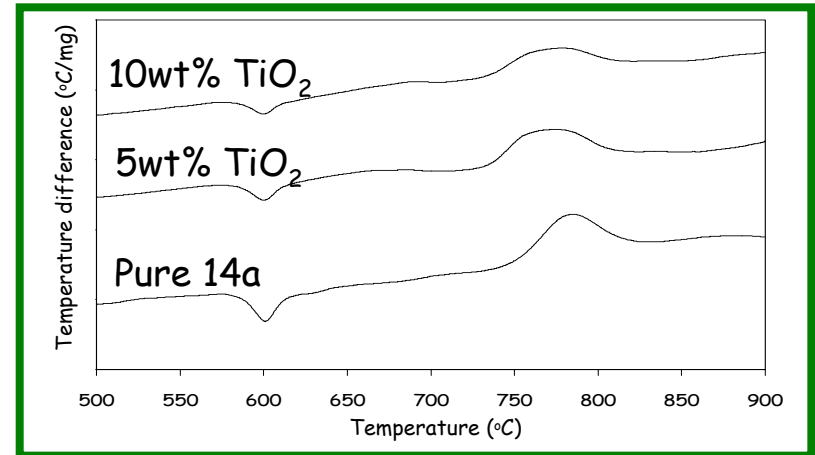
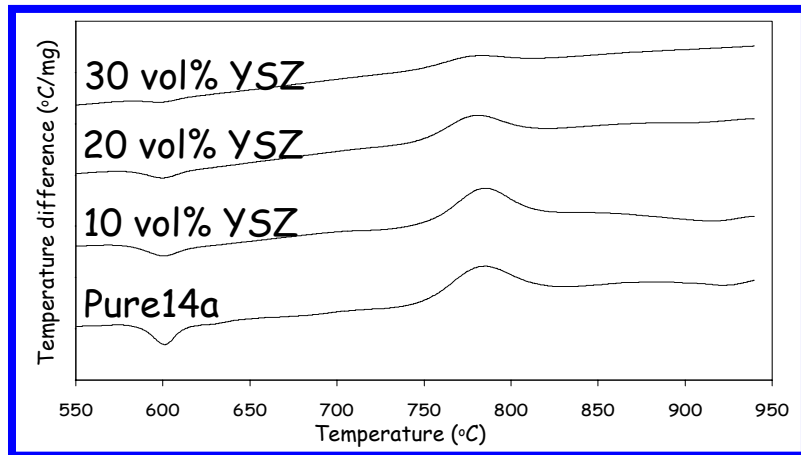
$$\alpha = \frac{\alpha_1 K_1 V_1 + \alpha_2 K_2 V_2}{K_1 V_1 + K_2 V_2}$$

$K_i$  = Young modulus

$V_i$  = volume fraction

In this case, a simple rule-of-mixture is a better fit

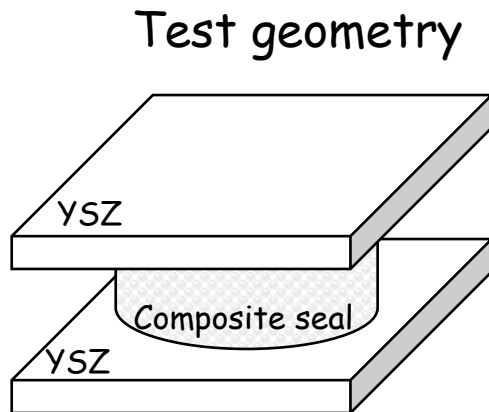
# Glass crystallization can be controlled by varying the glass and ceramic powder compositions



## Glass systems:

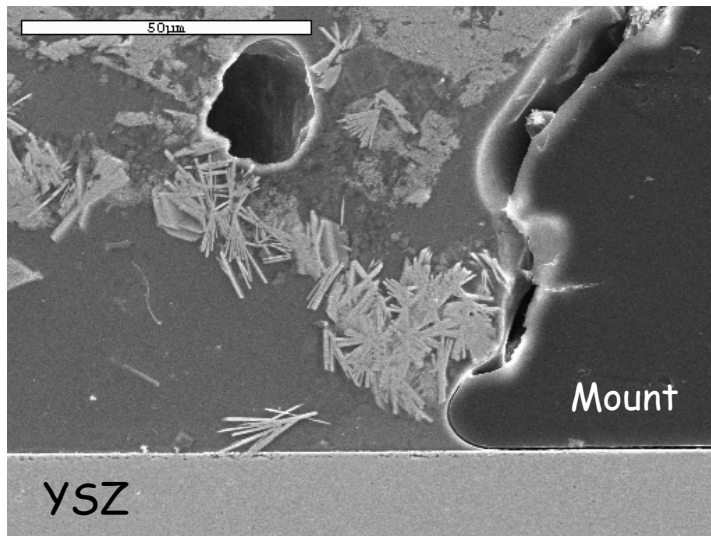
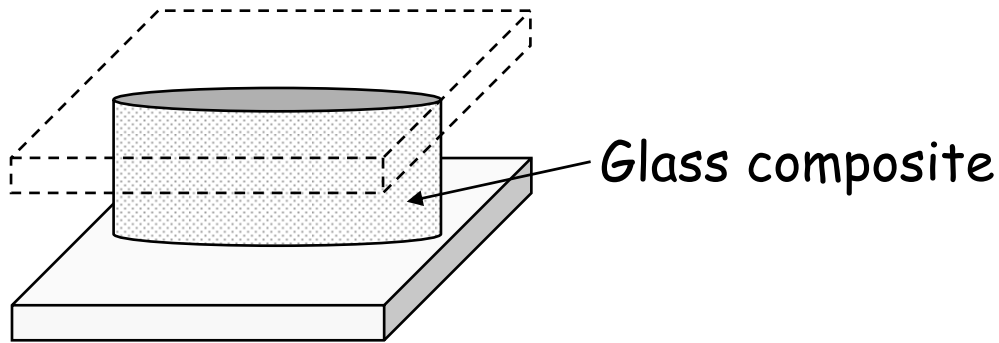
- Crystallization is independent of reinforcement (glass 14a)
- Crystallization is dependant on reinforcement (glass Brow 41)
- Controlled crystallization of independent system (glass 14a +  $\text{TiO}_2$ )

# Glass composites can be used to make a wide variety of different seal designs



- Basic glass composite seals
- Multi-layer seals
- Thermal shock resistant seals
- Glass/Metal Composite Seals
- Electrically conductive seals
- Thermal shock resistant and electrically conductive seals

# Example of basic glass composite seal with glass crystallization



## Seal Characteristics

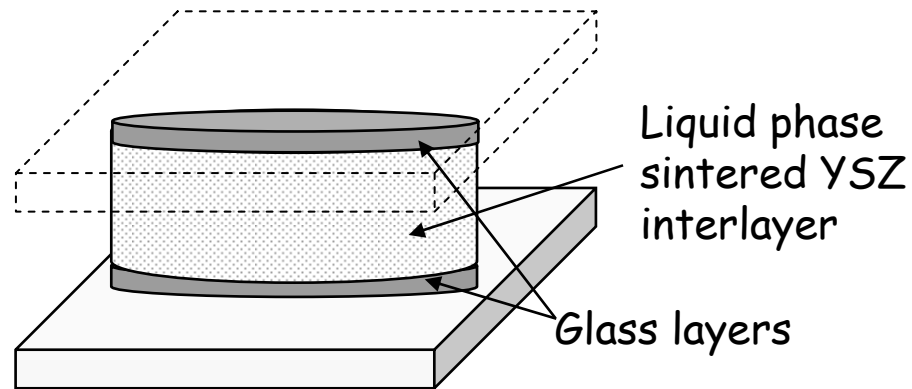
$T_g$	575°C
Onset Cryst	750°C
Max Cryst T	810°C
Powder/ Vol%	YSZ / 30
$CTE_{(200-550^{\circ}C)}$	$8.9 \times 10^{-6}/^{\circ}C$

## Sealing parameters

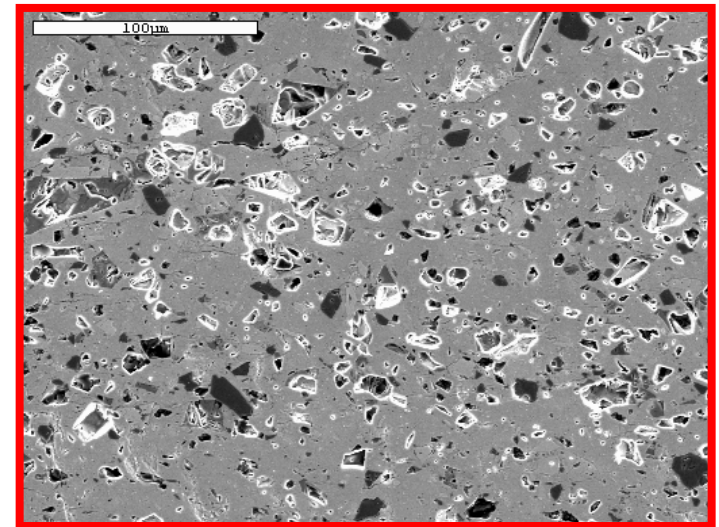
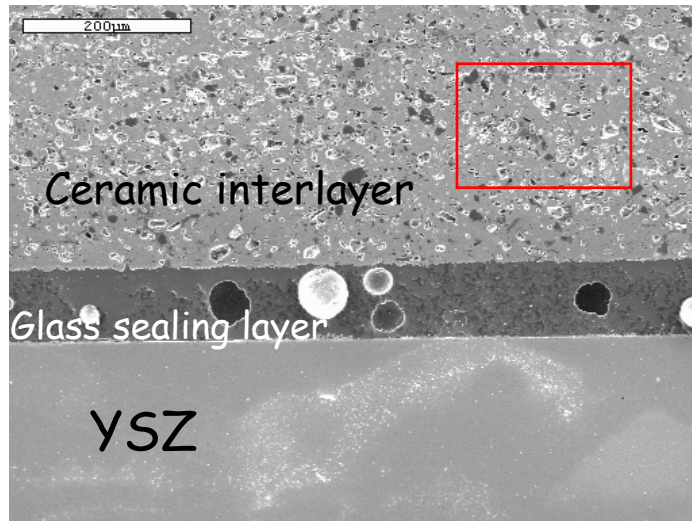
Temp	900°C
time	10 min

# Glass composites can be used to make multi layer seals

Concept: reduce sealing glass to thin interfacial layer



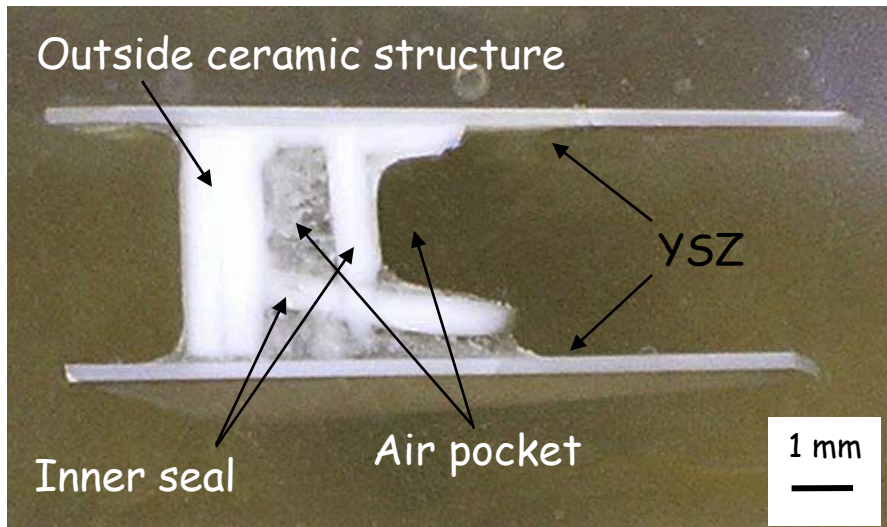
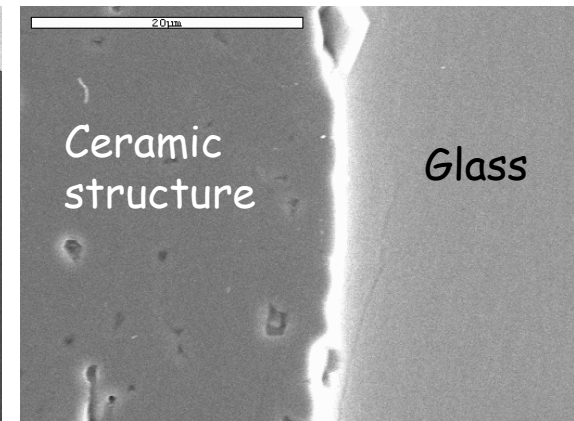
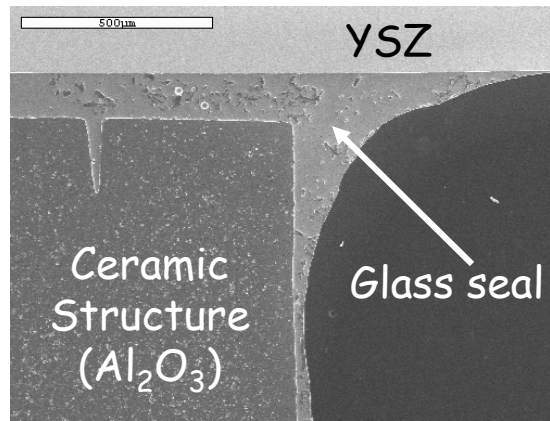
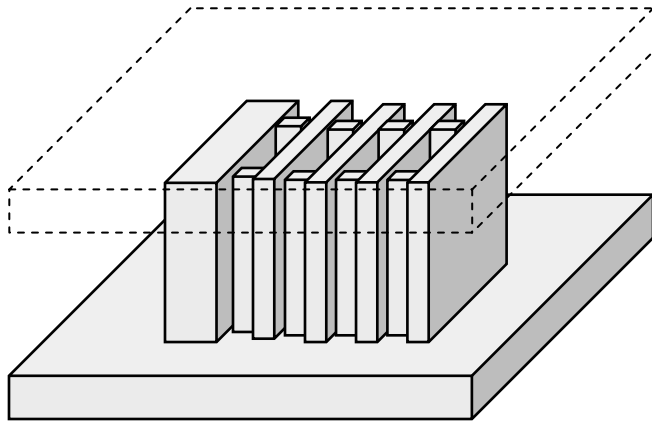
- Ceramic: 70 vol% YSZ
- Glass:  $T_g = 703^\circ\text{C}$  ,  $\text{CTE} = 9.7 \times 10^{-6}/^\circ\text{C}$
- Composite  $\text{CTE} = 10.2 \times 10^{-6}/^\circ\text{C}$  (200-700°C)



Ceramic interlayer:  
70vol% YSZ - 30vol% Glass  
Note: no pressure applied

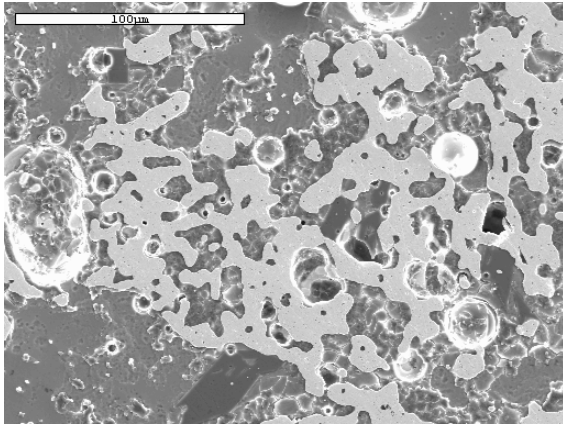


# Robocast cellular structure proposed to make thermal shock resistant seals

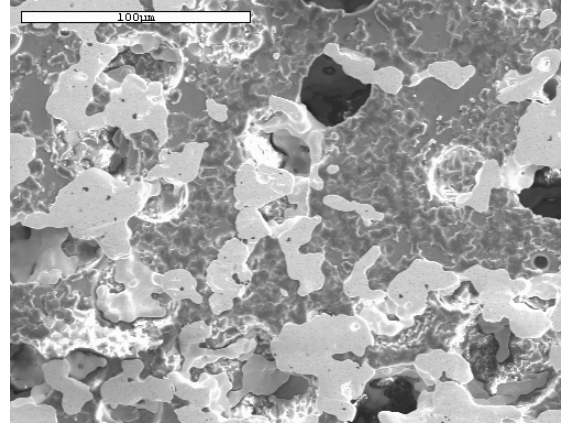


- Cellular ceramic structure provides strength and some compliance
- Compatible glass coating provides seal

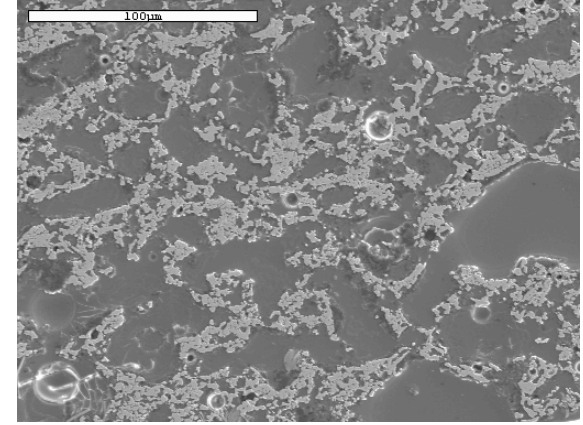
# Glass-metal composite seals can provide electrical connectivity



14a-20vol% Ag  
0.5-1.0 μm



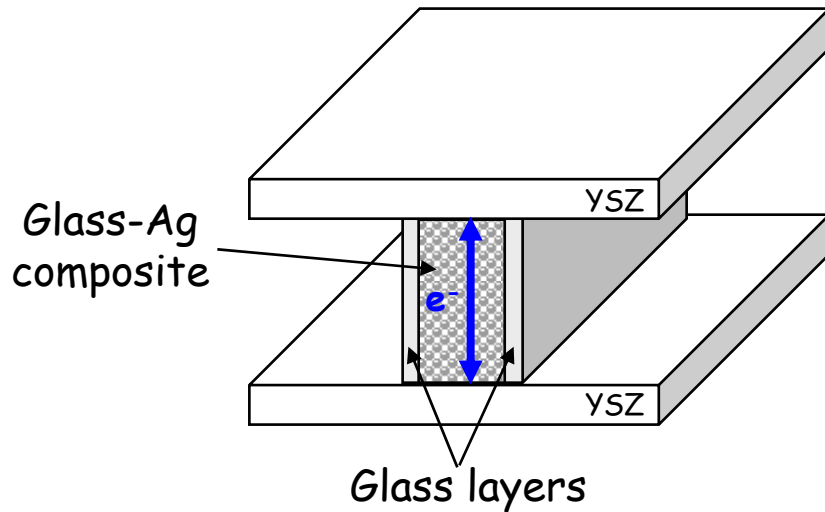
14a-20vol% Au  
5.5-9.0 μm



14a-20vol% Pd  
0.5-1.7 μm

- Percolating network obtained for all metallic additives
- Some dissolution of Ag in glass matrix (EDS analysis)
- No dissolution of Au or Pd in glass matrix (EDS analysis)

# Glass-Ag composites make electrically conductive seals



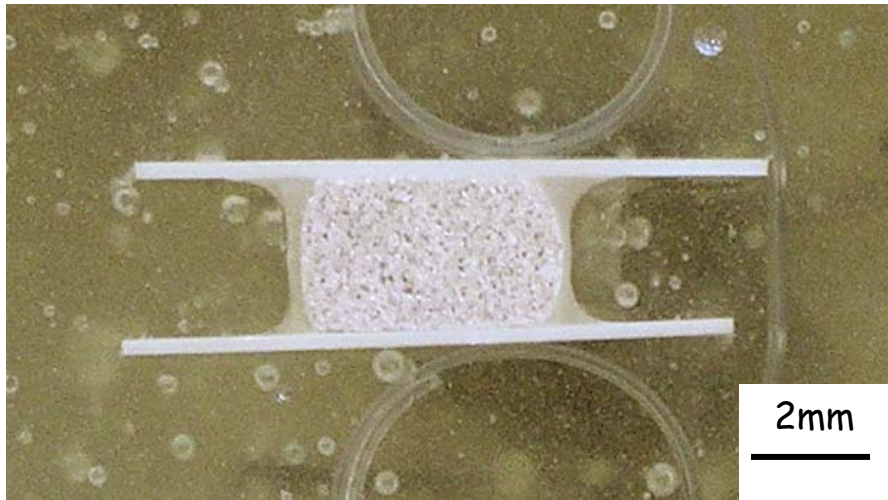
- Vol fraction of metallic phase slightly above the percolation limit
- Glass wets and coats metal to make composite and to provide seal
- Metal encapsulated by glass on exterior

## Electrical resistance measurement

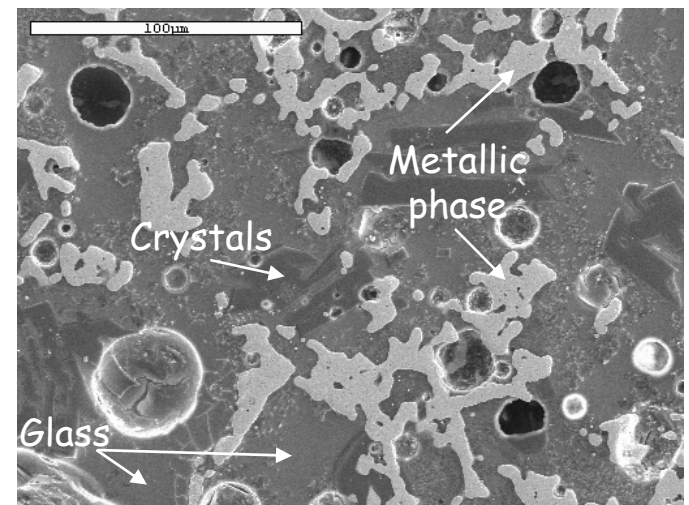
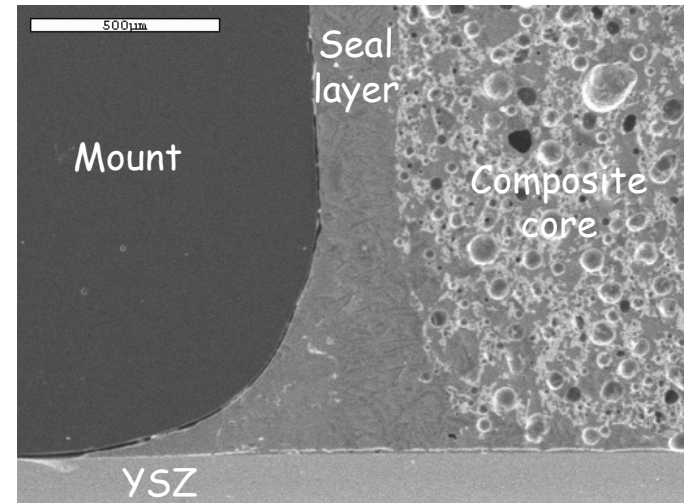




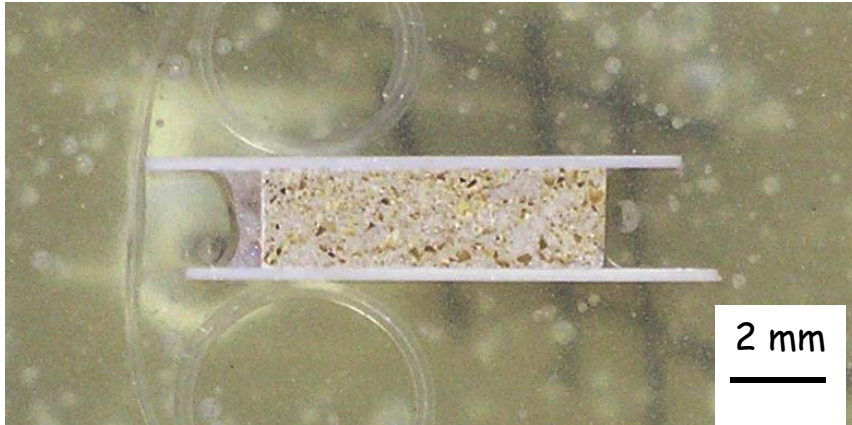
# Micrograph shows electrically conductive seal with glass 14a-Ag composite



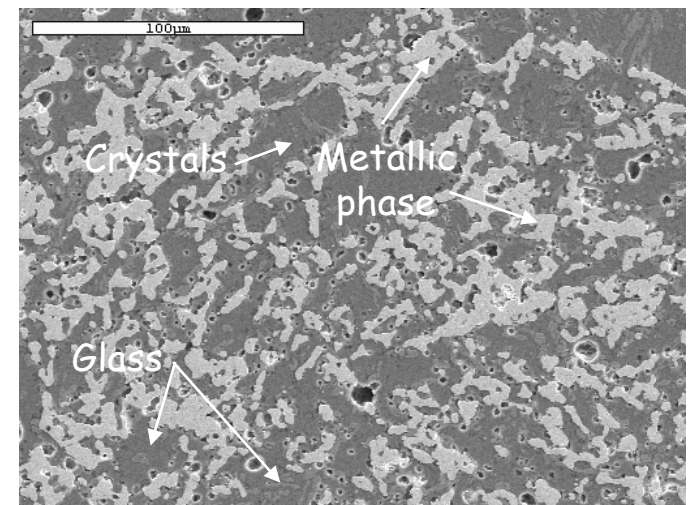
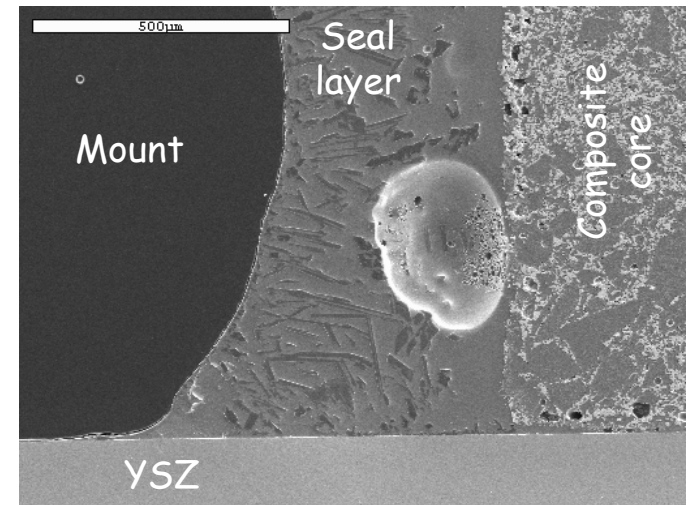
- Glass:  $T_g=575^{\circ}\text{C}$  ,  $\text{CTE}=9.4\times 10^{-6}/^{\circ}\text{C}$
- Filler metal: 20 vol% Ag
- Composite:  $T_g=566^{\circ}\text{C}$ ,  $\text{CTE}=10.5\times 10^{-6}/^{\circ}\text{C}$
- Resistance:  $<0.1\text{ ohm}$



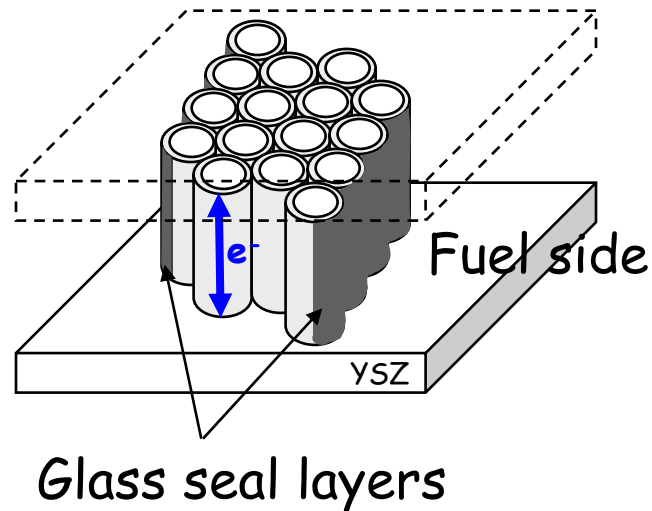
# Micrograph shows electrically conductive seal with Brow 37 glass-Ag composite



- Glass:  $T_g=620^{\circ}\text{C}$  ,  $\text{CTE}=6.8\times 10^{-6}/^{\circ}\text{C}$
- Filler metal: 20 vol% Ag
- Composite:  $T_g=582^{\circ}\text{C}$ ,  $\text{CTE}=9.1\times 10^{-6}/^{\circ}\text{C}$
- Resistance:  $<0.1\text{ohm}$

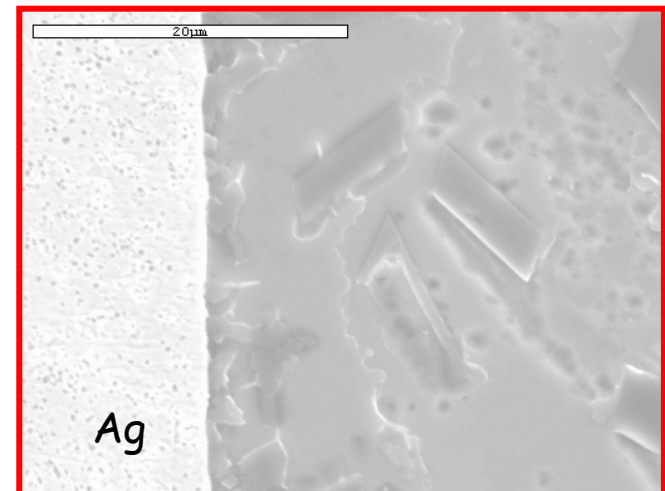
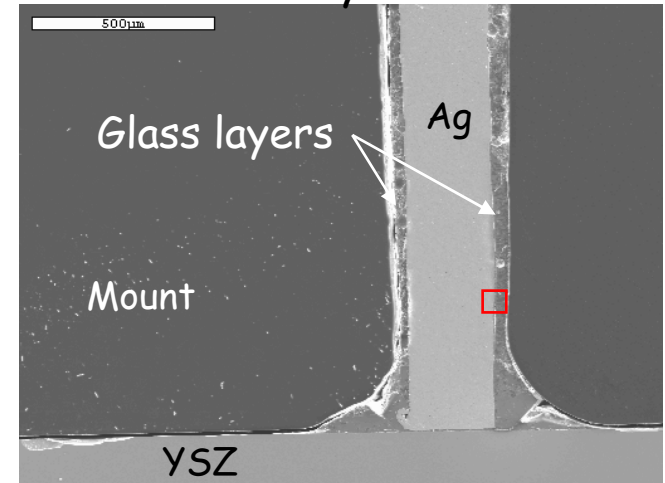


# Electrical Conductive Seal with high thermal shock resistance



Tubular metallic structure provides electrical conductivity and may provide some compliance that will increase thermal shock resistance

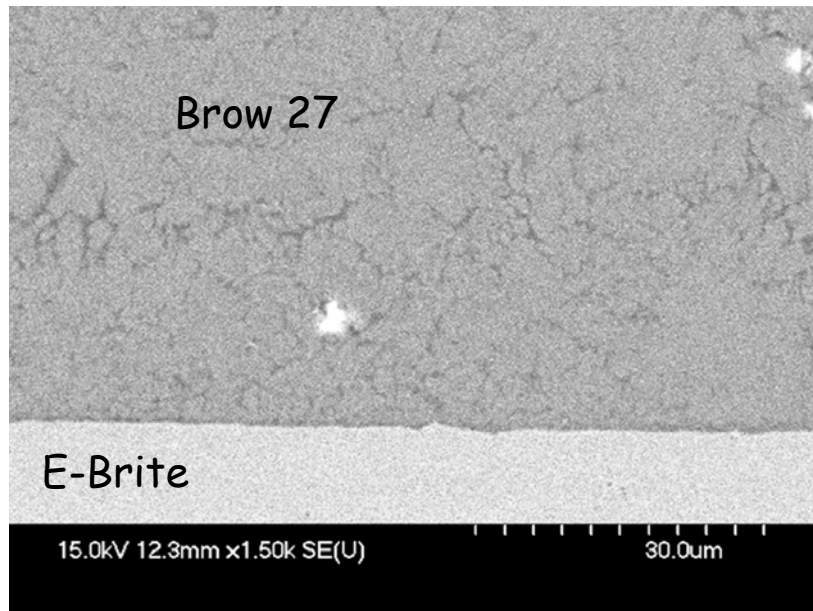
Preliminary results





# Work by R. Brow shows his glass 27 is compatible with E-brite alloy

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Exposure for 96 hours at 750°C

# Work in Progress

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- Analyzing interfacial reactions
- Thermal cycling and long time exposure at service temperature (environmental exposure)
- Mechanical testing of composite seal materials
- Mechanical testing of seal adhesion on YSZ substrates
- Development of seals on alloys such as E-brite

# Conclusions

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- Glass and crystalline compositions can be optimized independently
- Glass composites allow a wide range of properties and seal designs
- Composite approach seems very promising for sealing SOFCs
- We are ready to try to adapt this approach to specific vertical team needs

# Your research team

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