

Effects of Wet Air and Synthetic Combustion Gas Atmospheres on the Oxidation Behavior of Mo-Si-B Alloys

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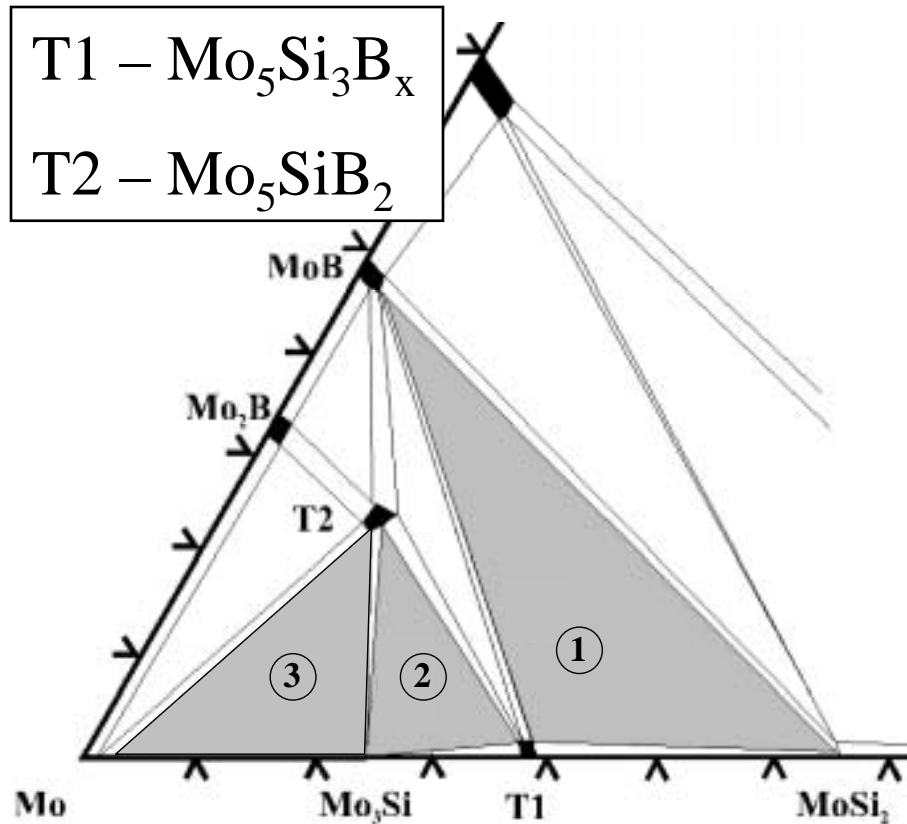
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Mo-Si-B Intermetallic System

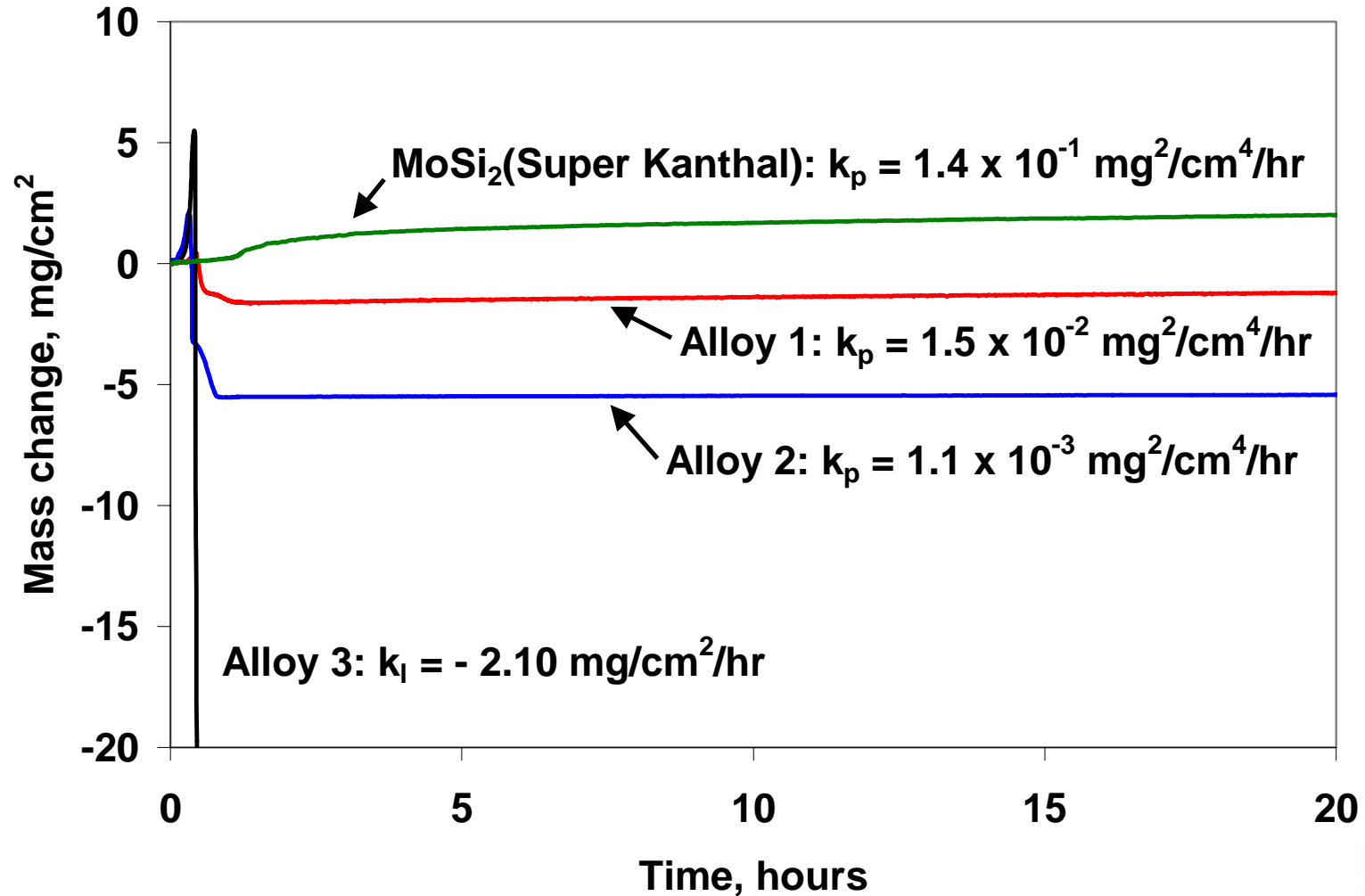


- T1-containing assemblages ① & ②
 - Excellent oxidation resistance and creep strength
 - Low fracture toughness
- Mo-containing assemblage ③
 - Improved fracture toughness
 - Reduced oxidation resistance
- Processible by:
 - Casting, sintering, plasma spraying
- Electrically conductive

Multiphase composites can meet several of the Vision 21 Goals, but additional research is needed to develop optimum alloy meeting all of the goals



Isothermal Oxidation at 1600°C in Dry Air



Looking to the Future: Vision 21 Goals to Develop New High Temperature Materials

- **Turbine Components**

- **Target FY08**

- **1000 hrs. 3000°F (1650°C)**
 - **Corrosive environment**

- **Heat Exchangers**

- **Target FY04**

- **Alloy-tube**

- 1000 hrs. 2300°F (1260°C)**

- **Ceramic-tube**

- 1000 hrs. 3000°F (1650°C)**

- **Mo-Si-B Alloys**

- **T1-based alloys stable for 240 hrs at 2900°F (1600°C) in dry air**
 - **Effect of combustion gases?**
 - **Enhance fracture toughness?**
 - **Fatigue tolerant?**



Project Objectives

- **Near Term**

- **Mo-Si-B**
- **T1-based alloys now meet temperature criteria for heat exchangers**

Issues to be addressed:

- **Fabrication**
- **Corrosion**
- **Improvements with minor alloy additions**

- **Future**

- **Derivative Mo-Si-B alloys**
- **T1-based alloys now meet creep resistance and temperature criteria for turbine applications**

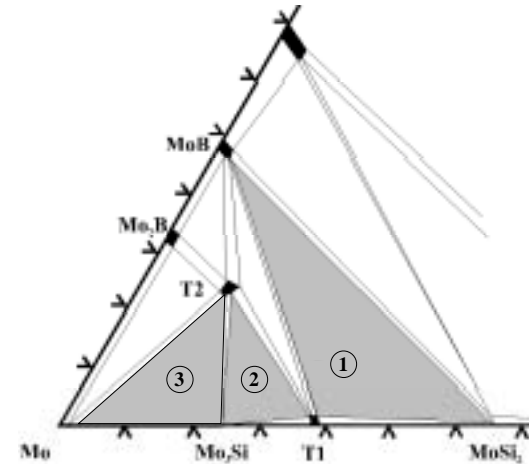
Issues to be addressed:

- **Near-net shape processing**
- **Low fracture toughness**
- **Long term oxidation resistance**
- **Cyclic oxidation resistance**



Alloy Compositions Tested

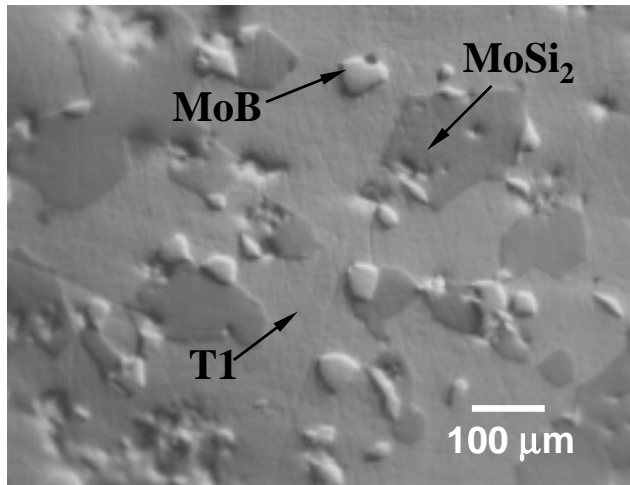
- Commercially procured, pre-alloyed powders
- Sintered at 1800°-1900°C in Ar atmosphere to > 95% density



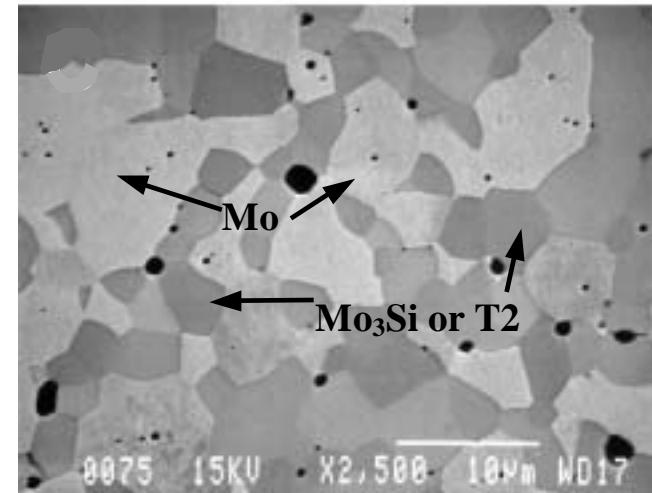
Alloy	Wt %			Phase Fraction (Vol %)					
	Mo	Si	B	T1	MoB	MoSi ₂	T2	Mo ₃ Si	Mo
1	84.0	13.4	2.6	66	22	12			
2	88.6	9.9	1.5	45			31	24	
3	94.6	4.3	1.1				30	27	43



Typical Microstructures

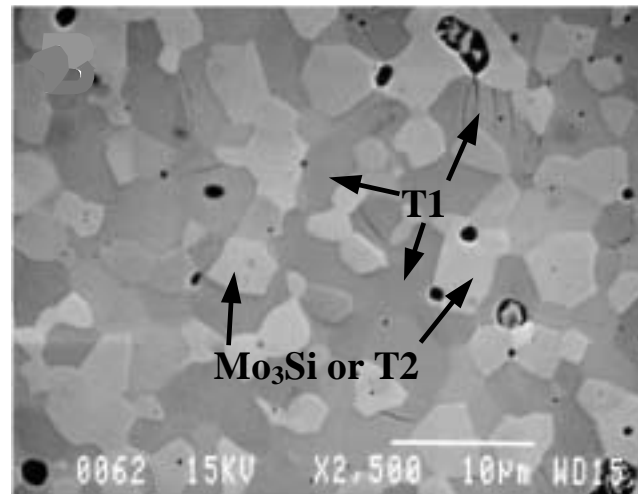


Alloy 1



Alloy 2

Alloy 3



Results and Discussion Outline

- **Review of alloy oxidation in dry and wet air (150 Torr H₂O)**
- **Isothermal oxidation in dry air to 1600°C and wet air to 1000°C**
- **Effect of pre-oxidation on scale formation of Alloy 3**
- **Effect of synthetic oxidizing combustion gas mixture N₂ - 13 CO₂ - 10H₂O - 4O₂ at 1000° and 1100°C**



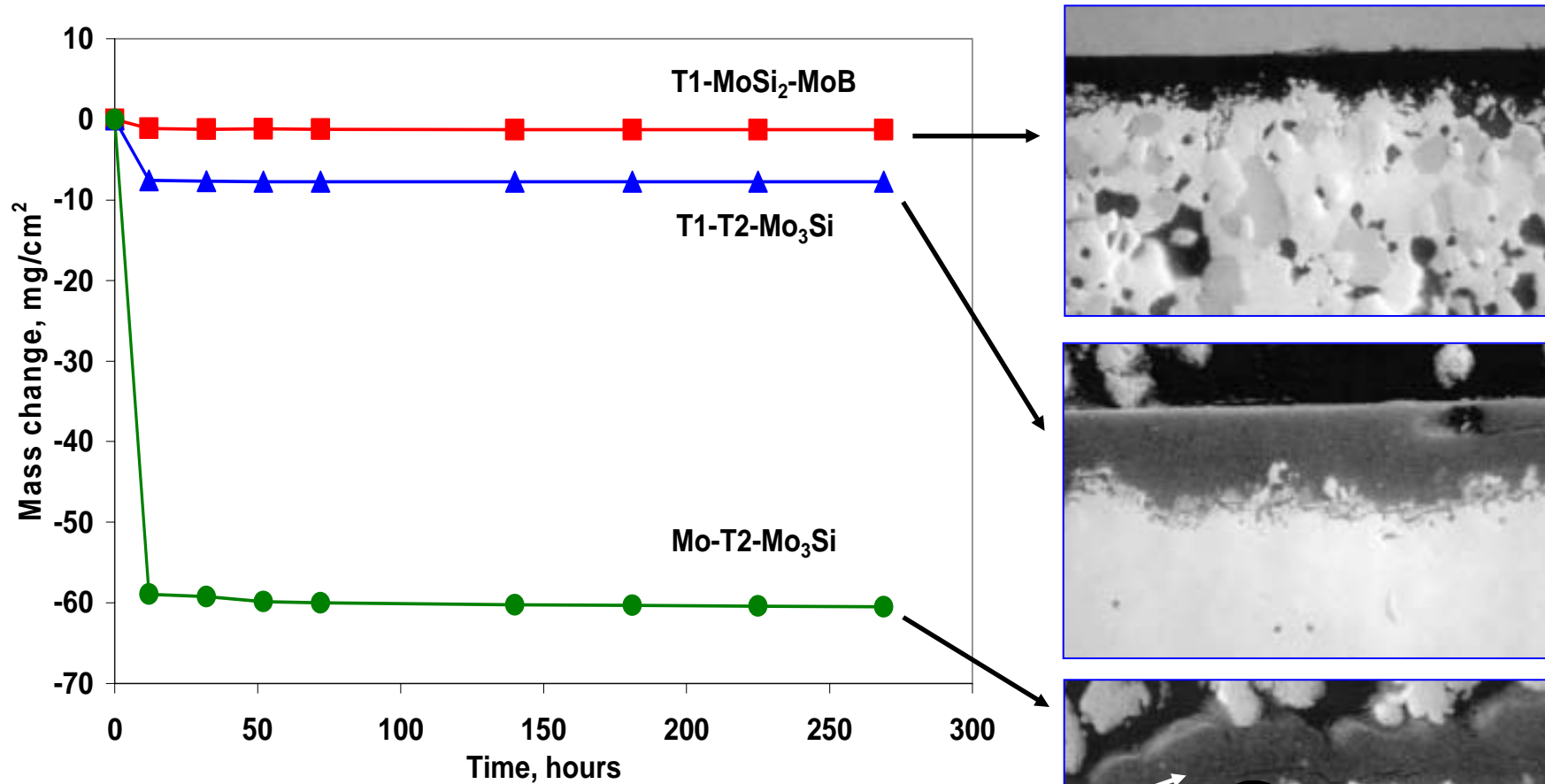
Isothermal Measurements in Wet/Corrosive Gases



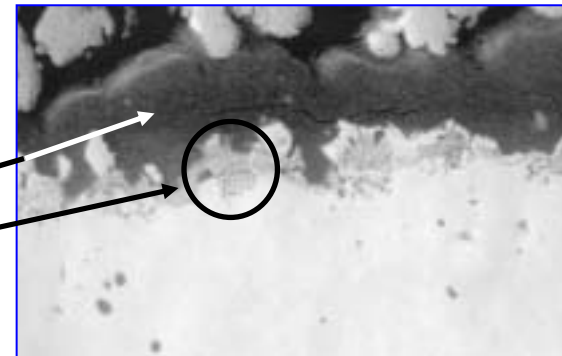
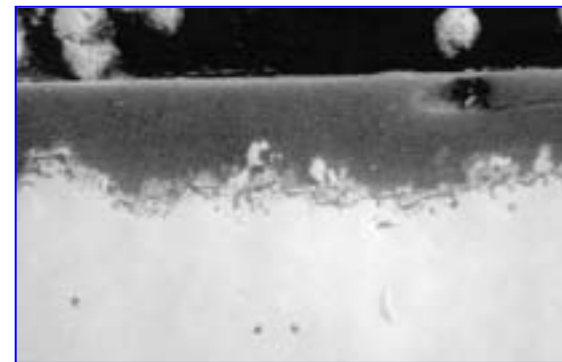
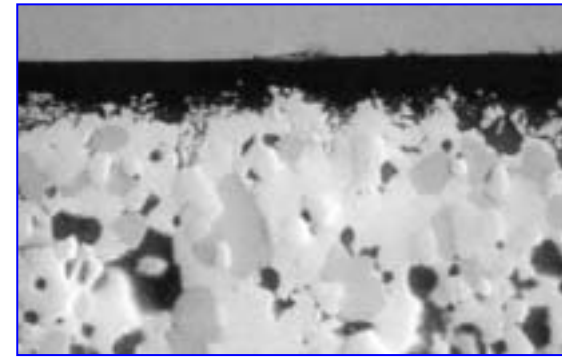
- Requires use of purge and reactive gases to achieve gas separation and protect balance mechanism
- Condensation of MoO_3 onto hangdown can occur in Alloy 3
- Used pre-oxidation in tube furnace to induce initial mass loss



Oxidation in Dry Air at 1100°C

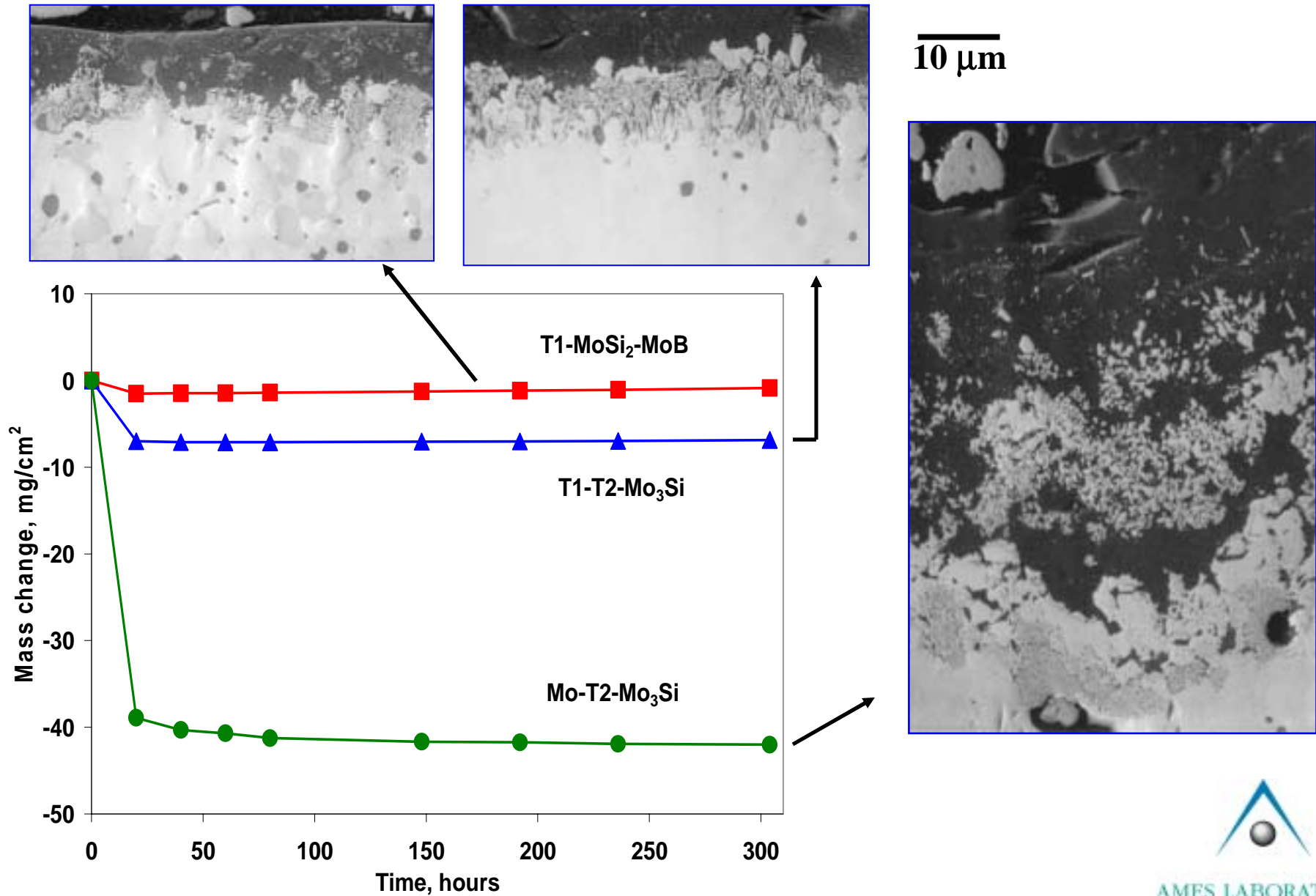


- External borosilicate glassy scale with subscale Mo and MoO₂



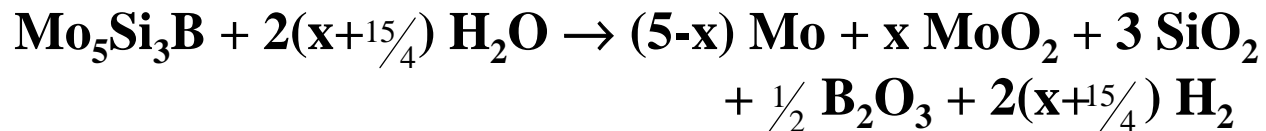
10 μm

Oxidation in Wet Air at 1100°C



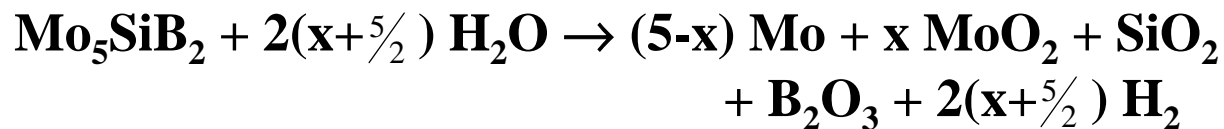
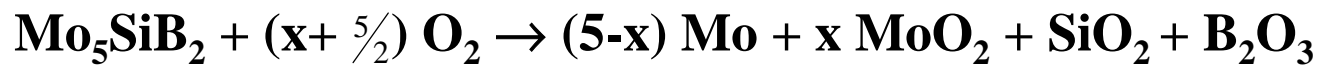
Scale Formation Reactions

- **T1 phase (Alloy 1 and Alloy 2):**



borosilicate glass ~ 14 at% B₂O₃

- **T2 phase (Alloy 2 and Alloy 3):**

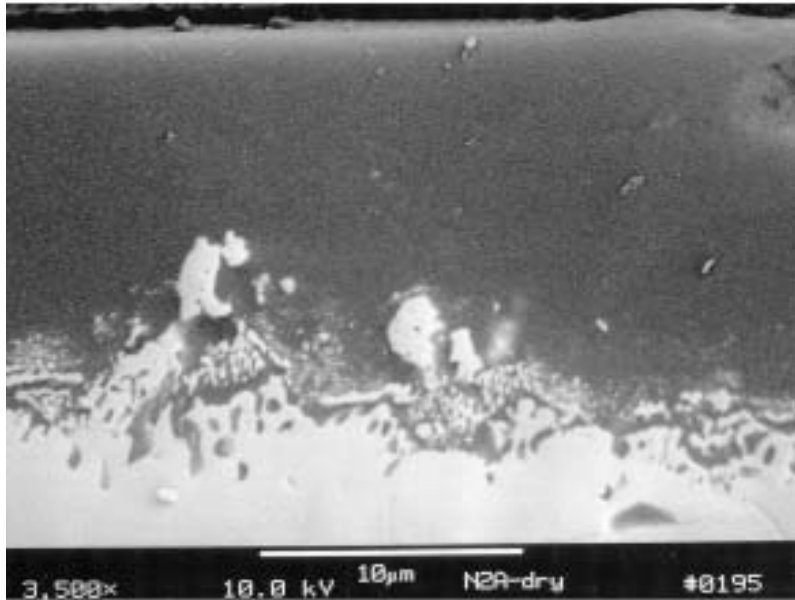


borosilicate glass ~ 50 at% B₂O₃ η(T2) << η(T1)



Enhanced Interlayer Growth (Alloy 2 as example)

Dry Air



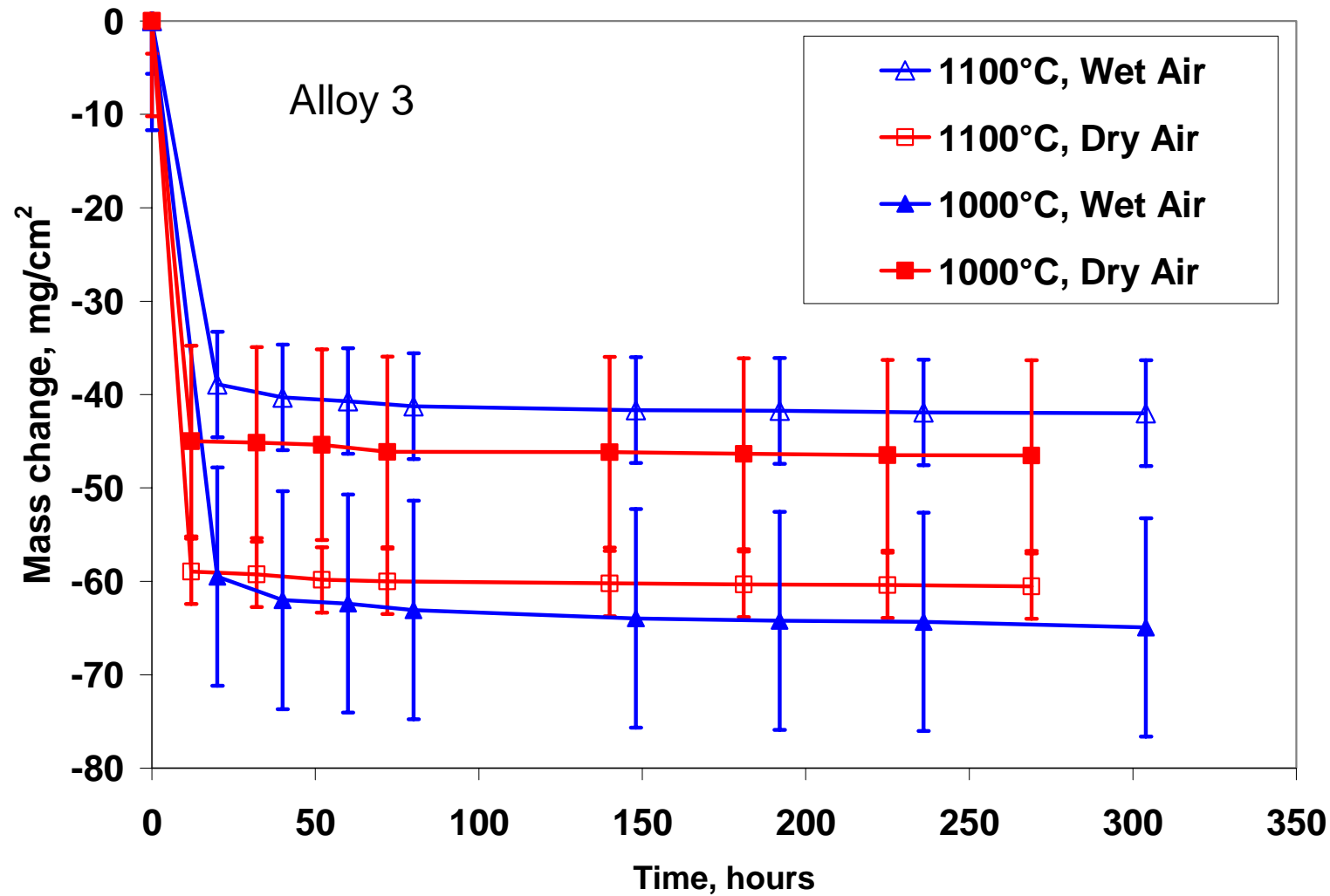
Wet Air



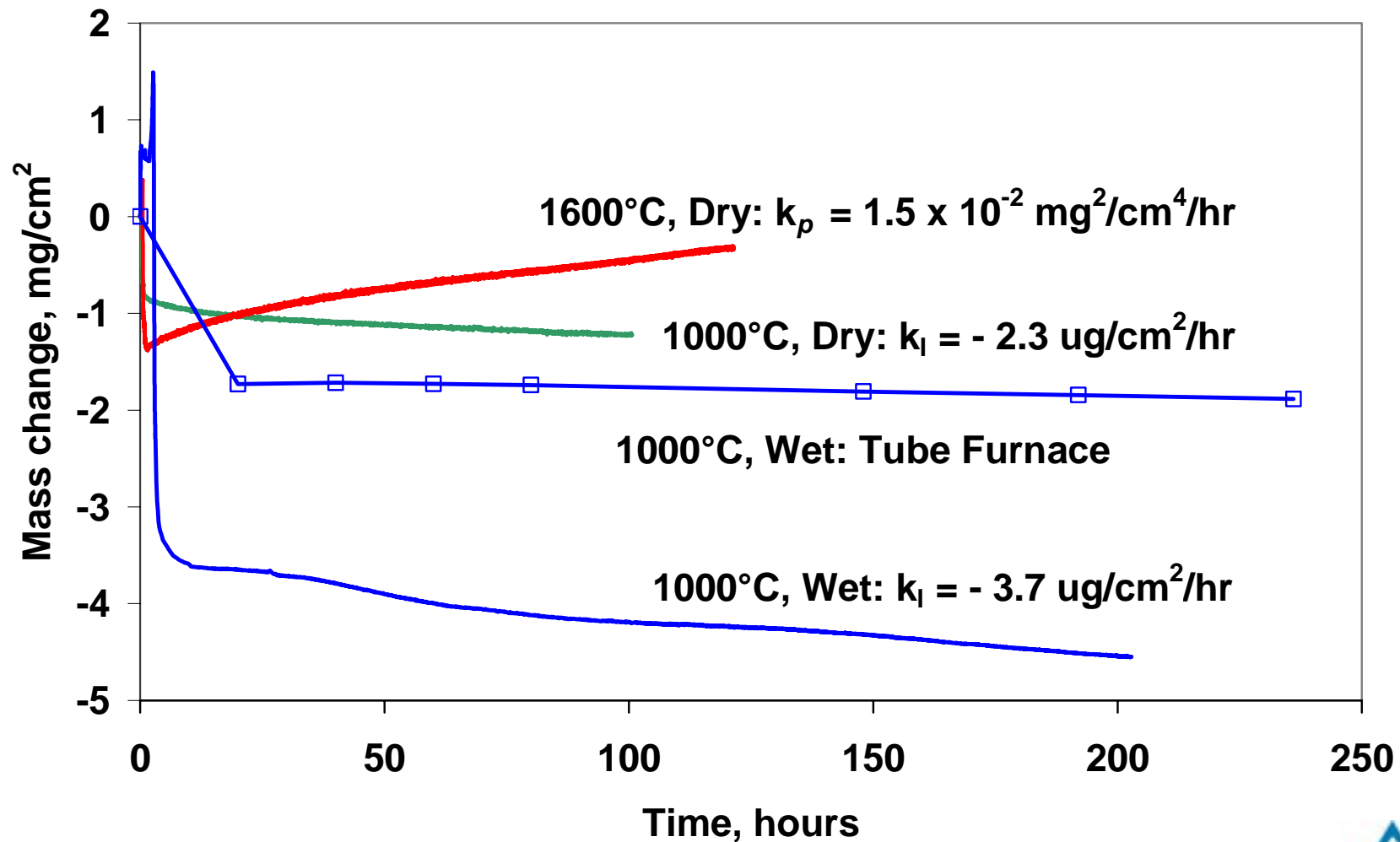
- Interlayer appears as fine, eutectic-like Mo-rich phase dispersed in a thin, continuous matrix of darker silica; larger grains of MoO₂ are detectable
- Insufficient spatial resolution for EDS to determine if eutectic-like areas correspond to Mo or MoO₂



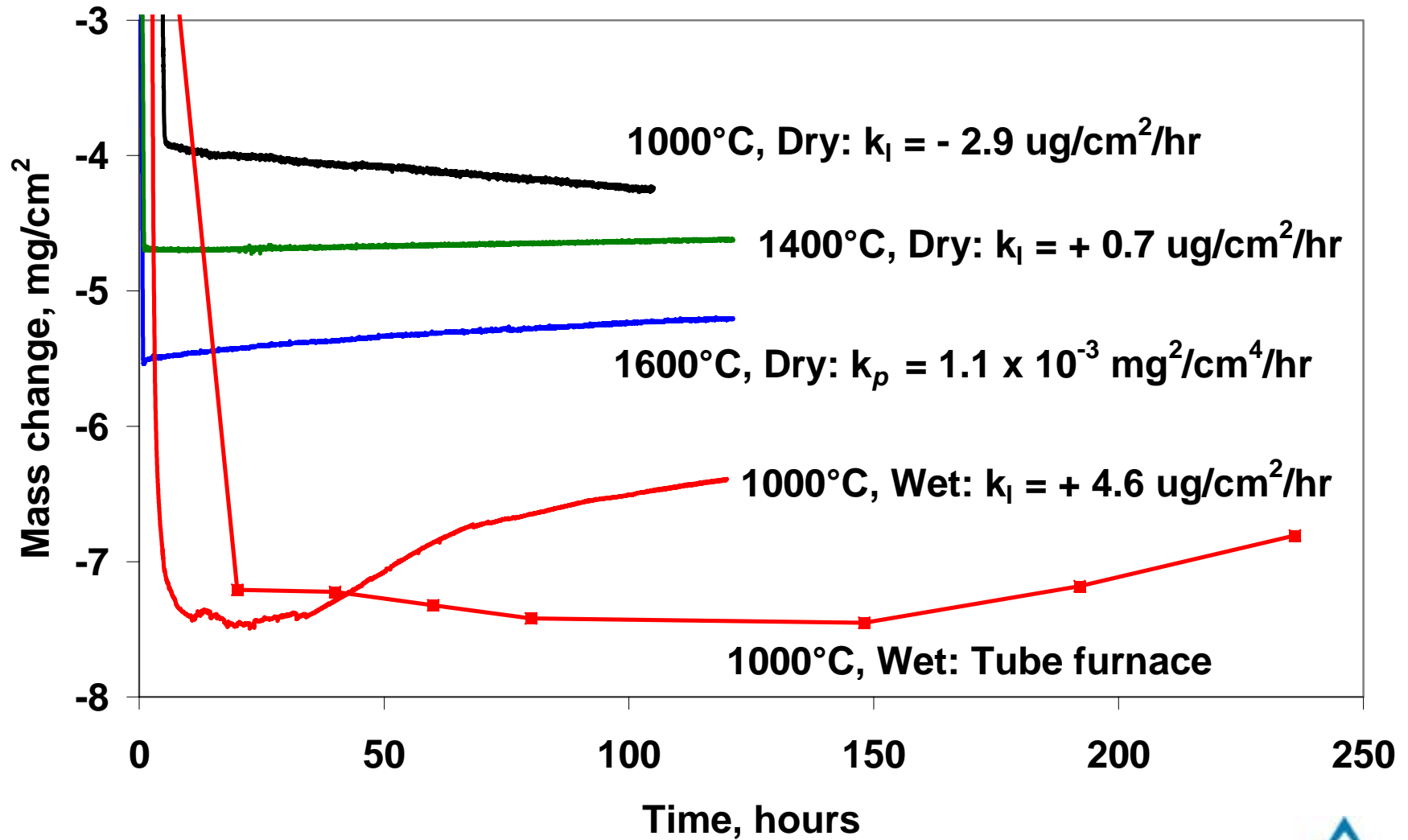
Why Isothermal Oxidation Measurements?



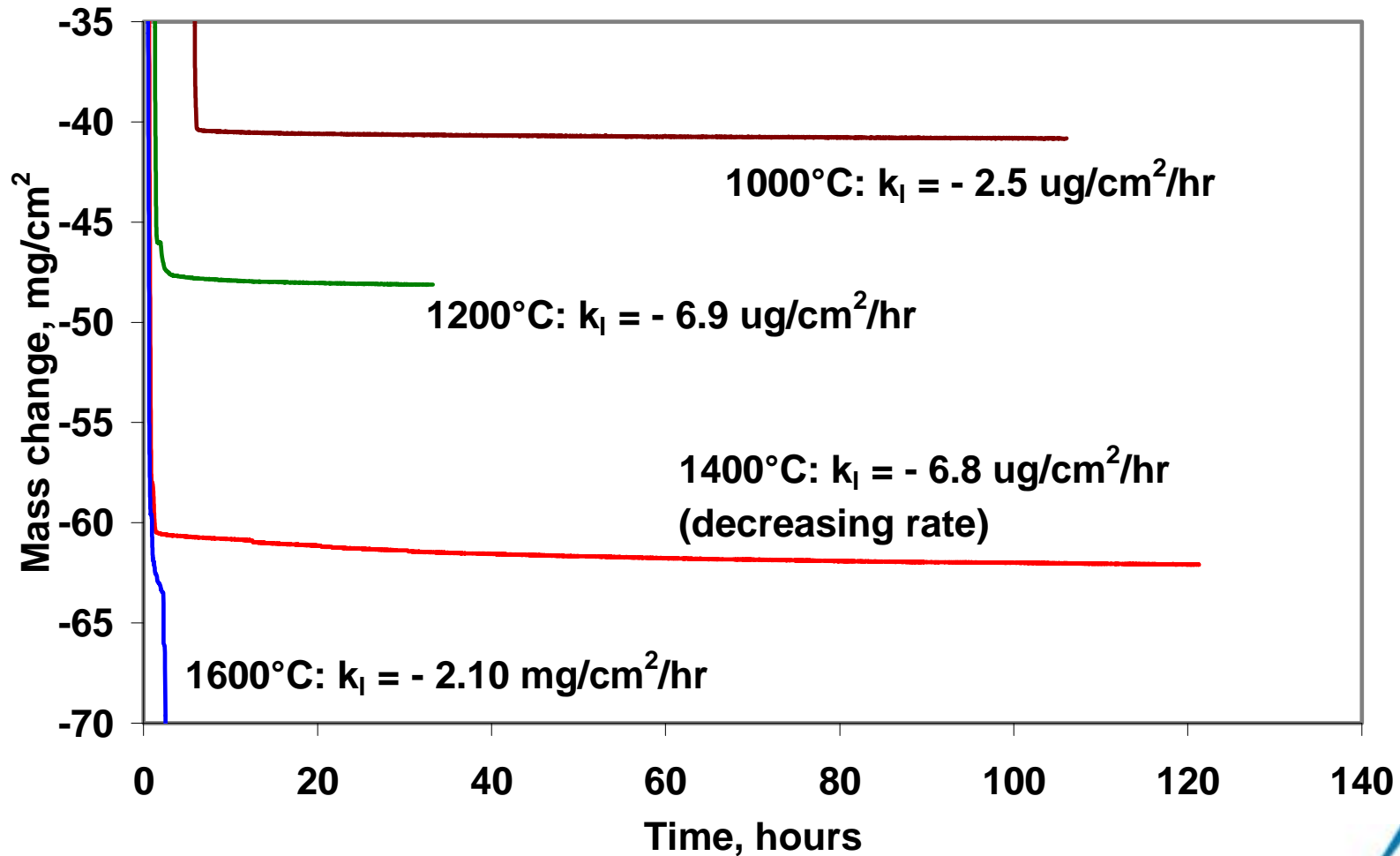
Isothermal Oxidation of Alloy 1



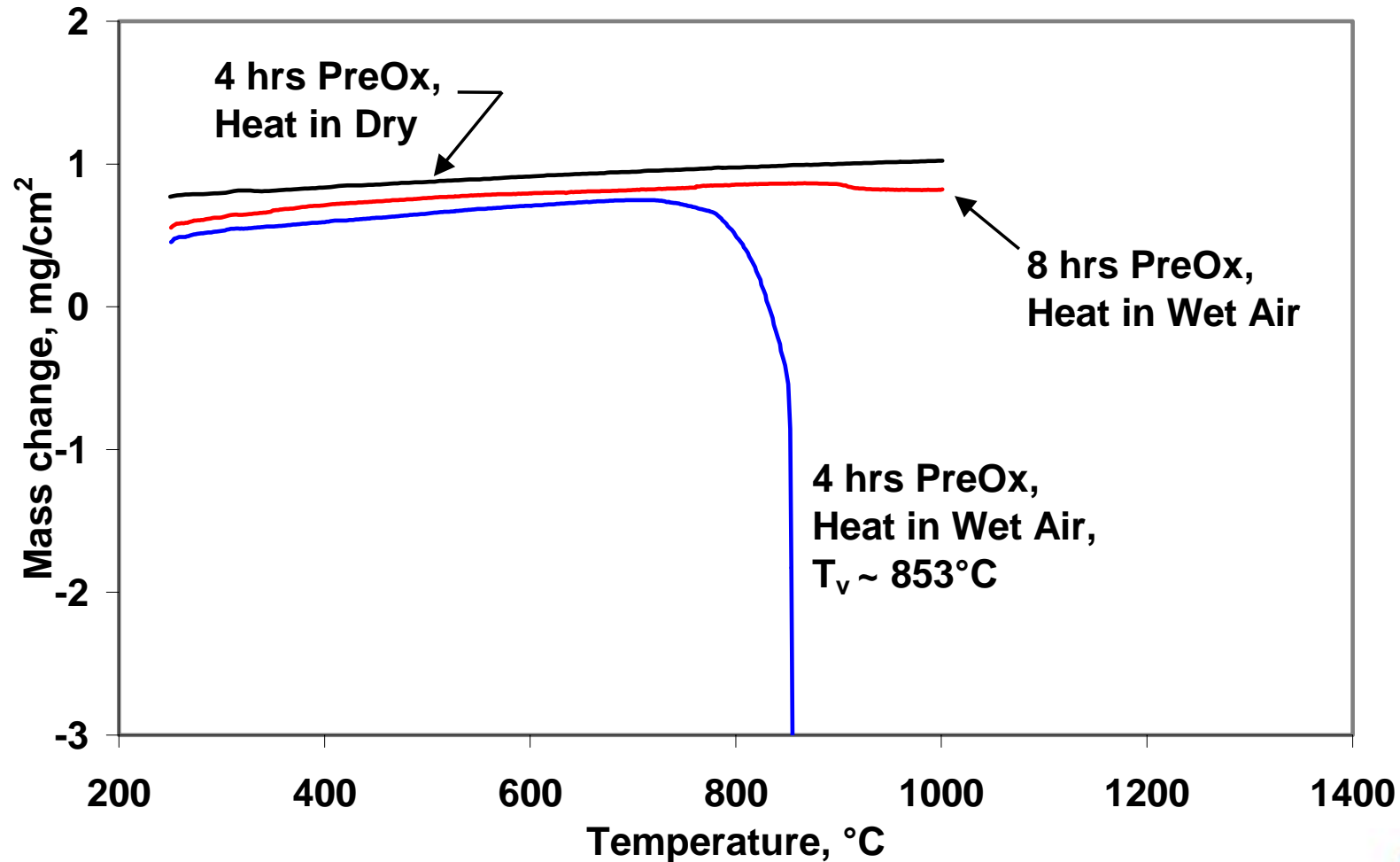
Isothermal Oxidation of Alloy 2



Isothermal Oxidation of Alloy 3 in Dry Air

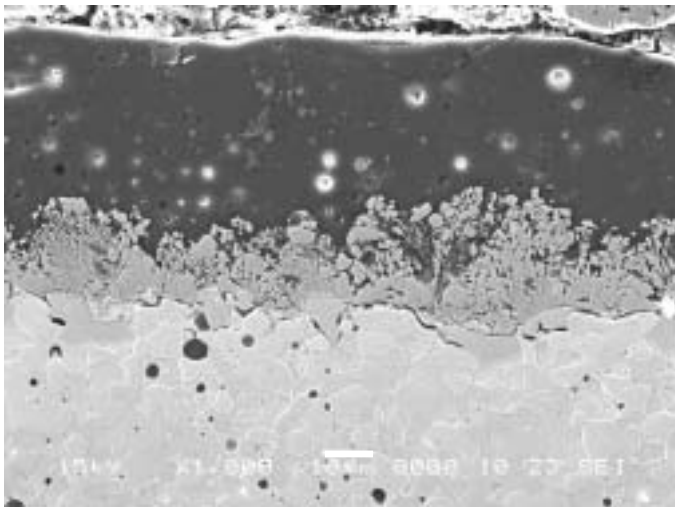
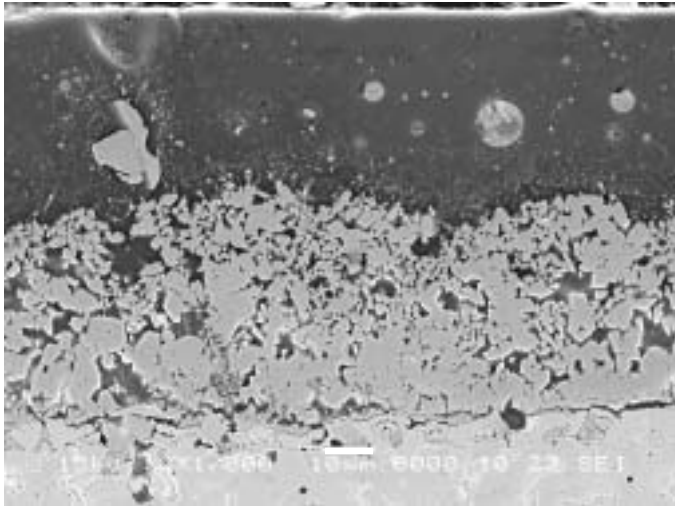


Pre-Oxidation Effect on Alloy 3 Scale Formation

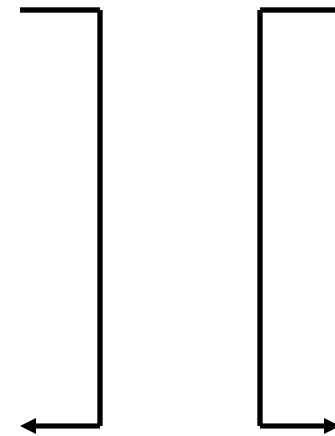
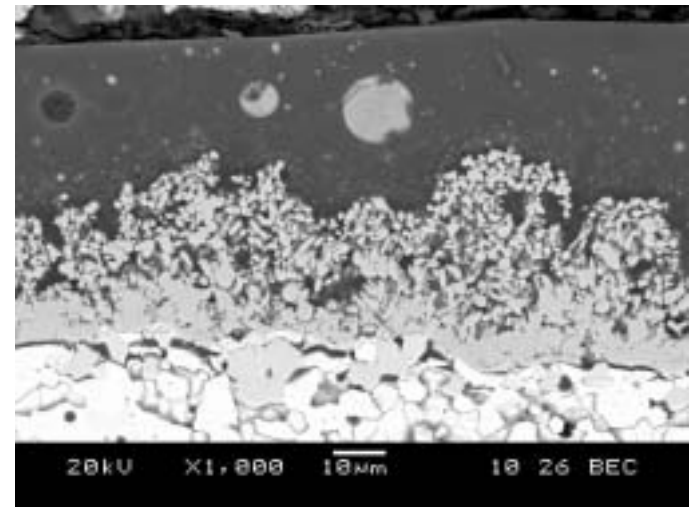
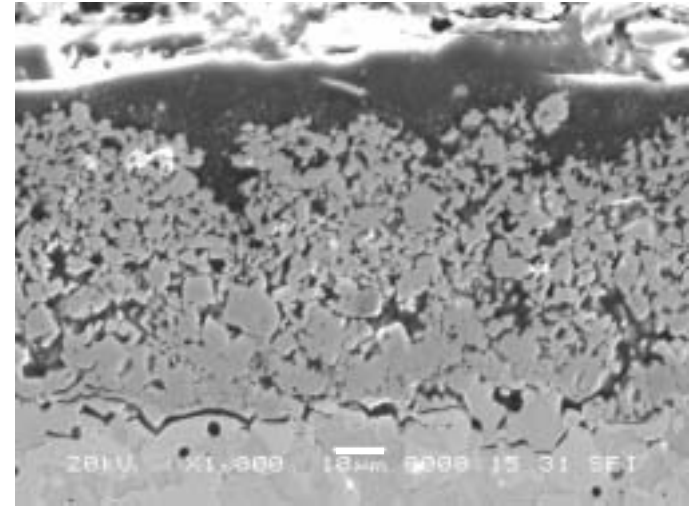


Alloy 3 Pre-Oxidation and Scale Formation

4 hrs Pre-Ox in Dry Air



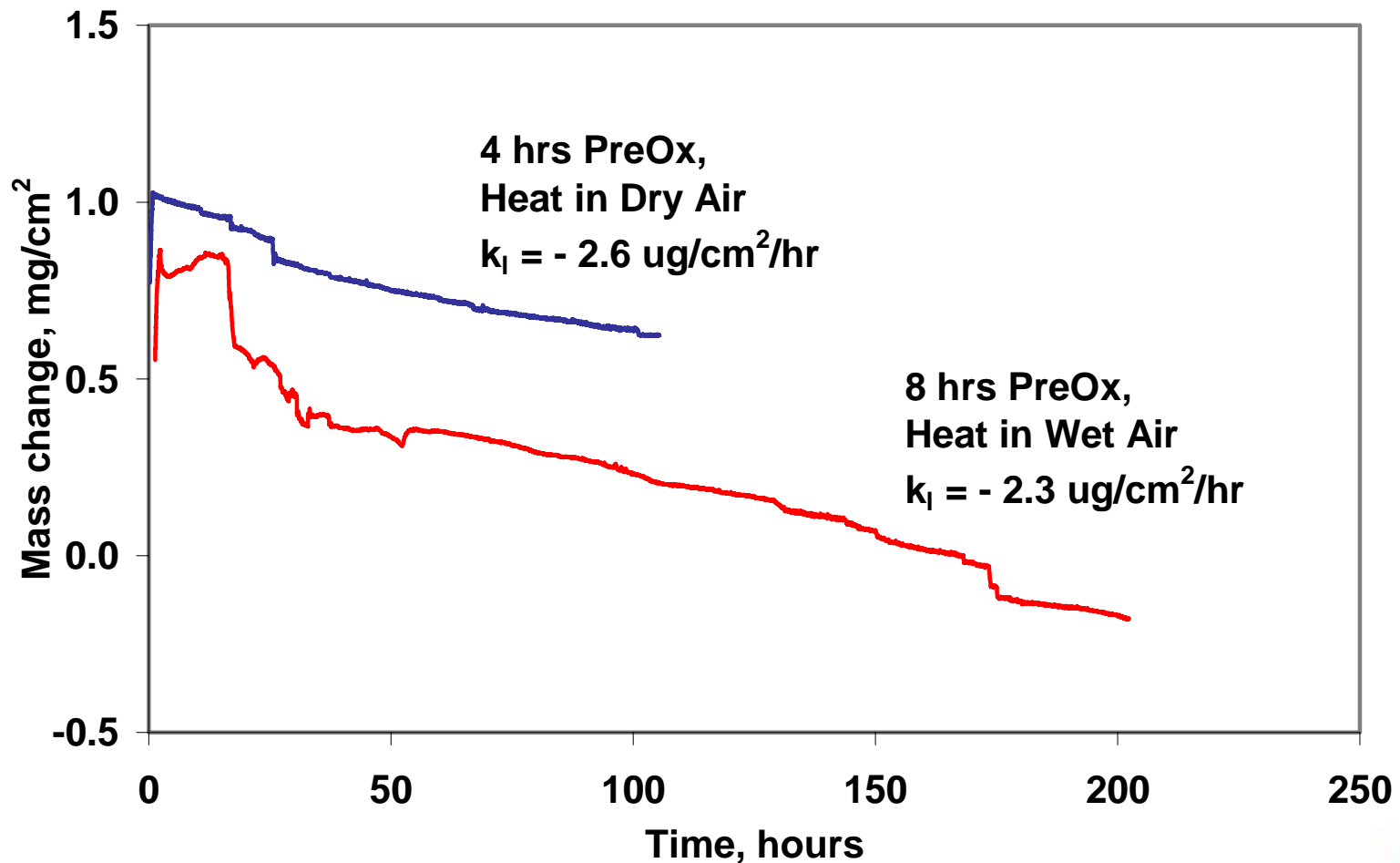
8 hrs Pre-Ox in Dry Air



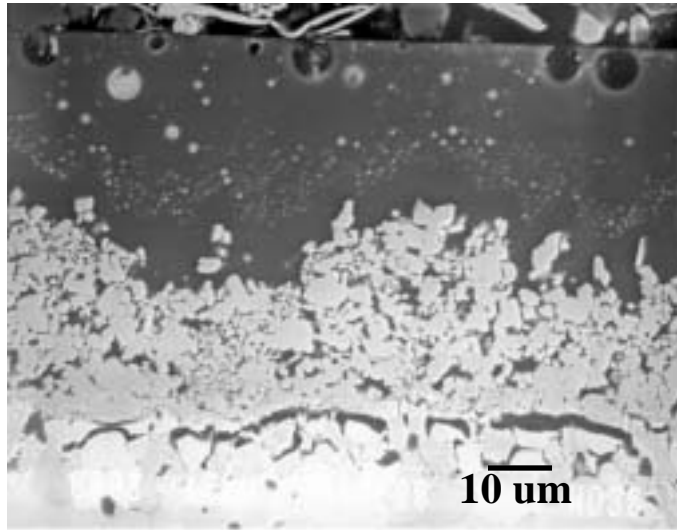
3 hr exposure
to Wet Air

—
10 μ m

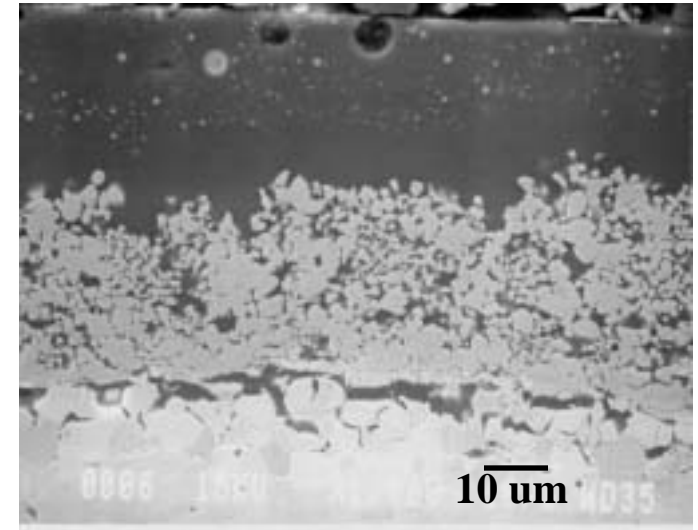
Oxidation of Alloy 3 in Wet Air at 1000°C



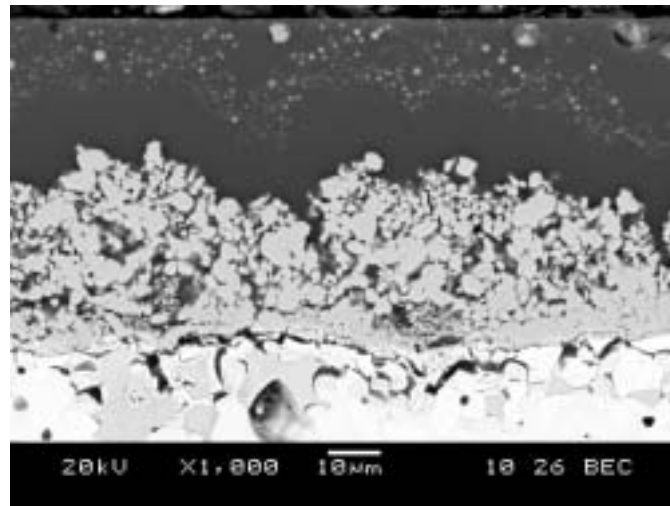
Scale Evolution During Alloy 3 Oxidation



**8 hrs Dry Air,
100 hrs Wet Air**

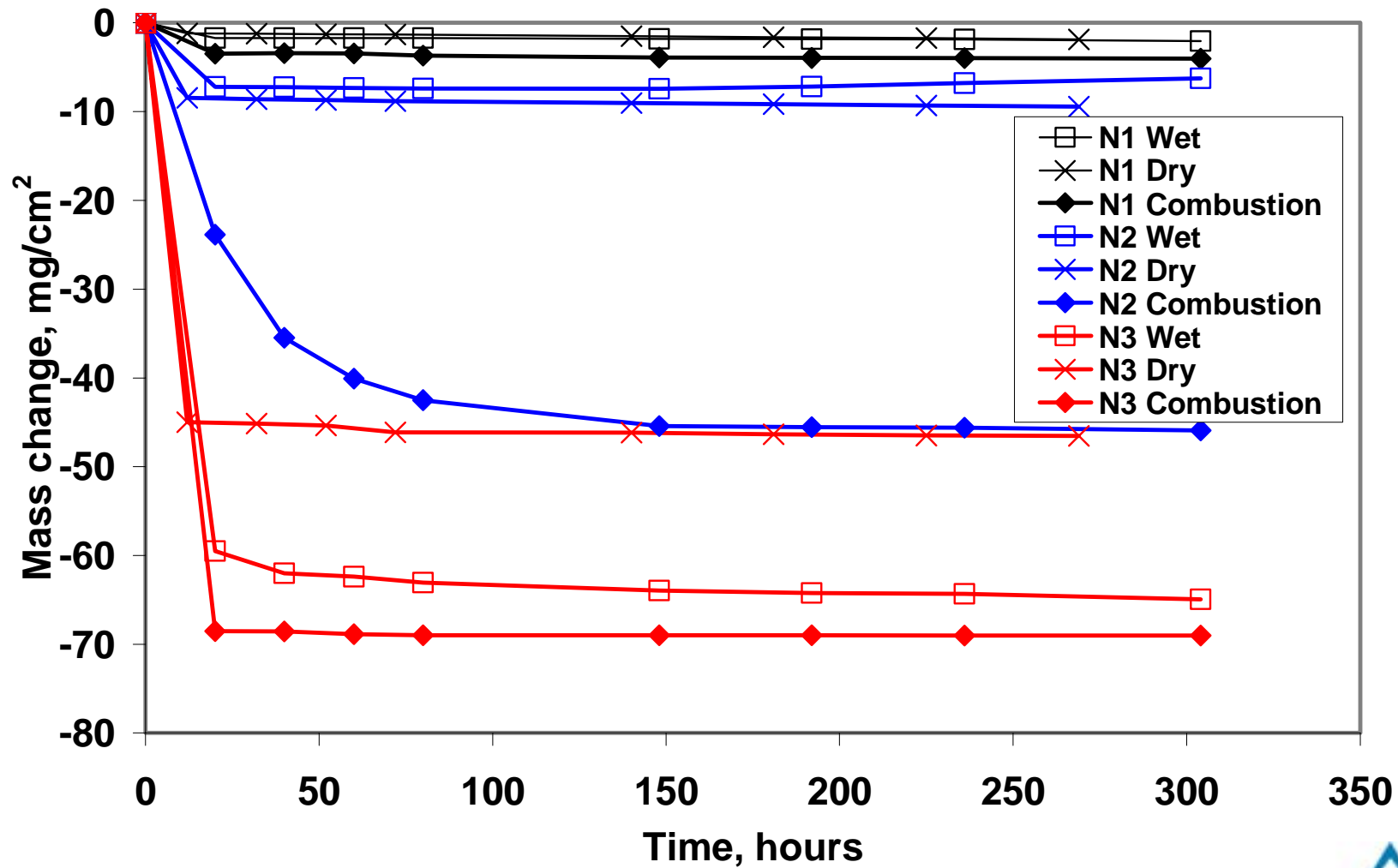


**8 hrs Dry Air,
200 hrs Wet Air**

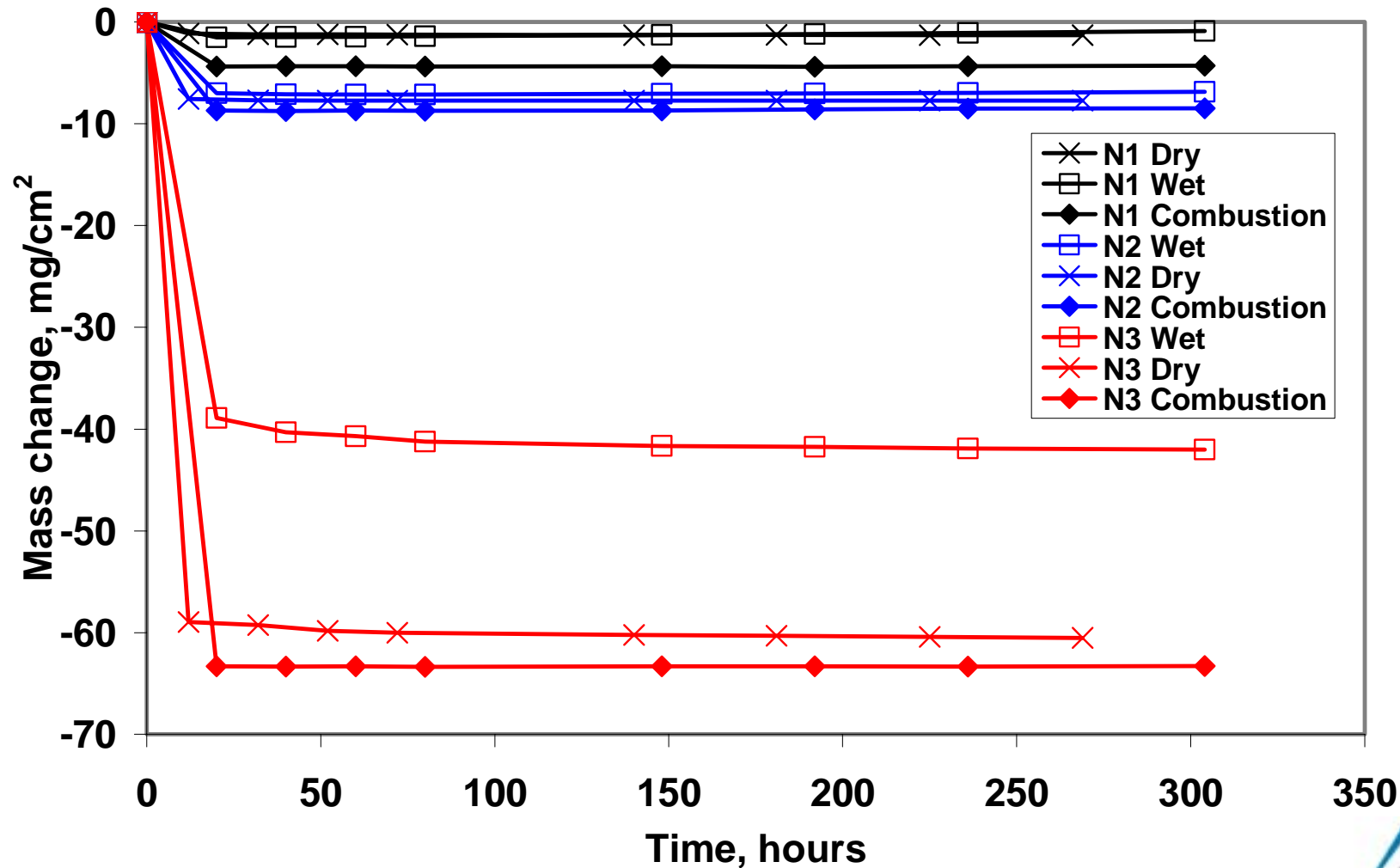


200 hrs Dry Air

Synthetic Combustion Gas Exposure at 1000°C



Synthetic Combustion Gas Exposure at 1100°C



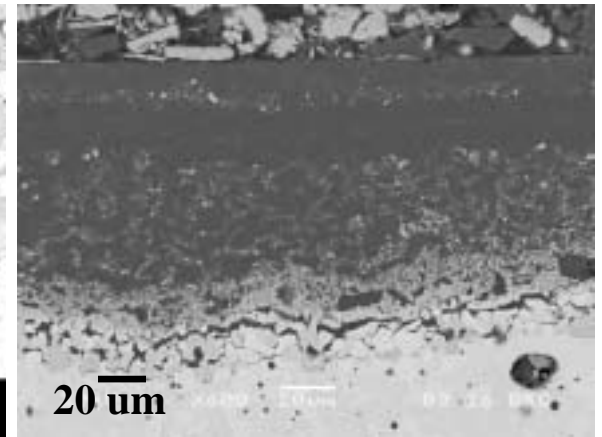
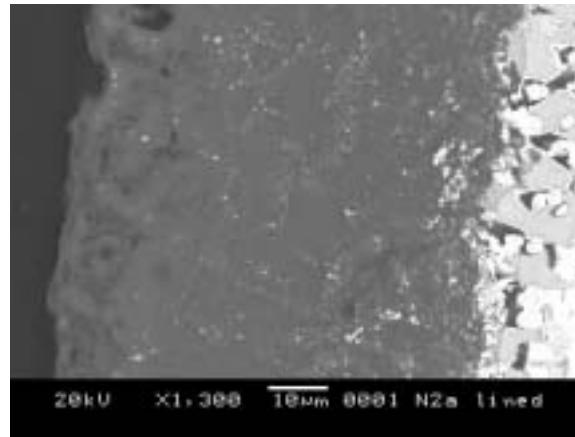
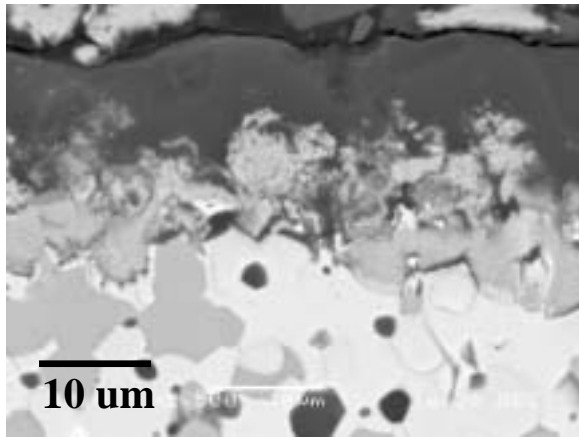
Effect of Combustion Gas Exposure

Alloy 1

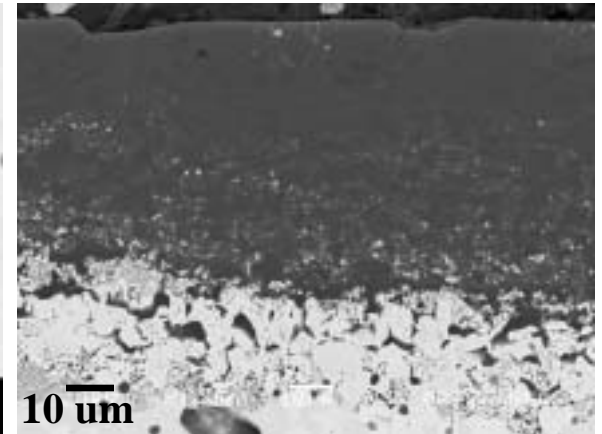
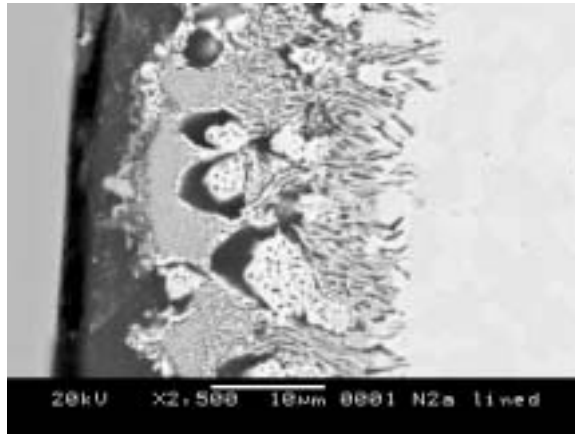
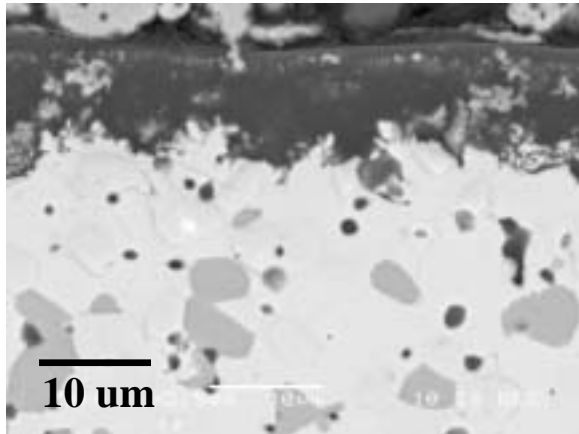
Alloy 2

Alloy 3

1000°C

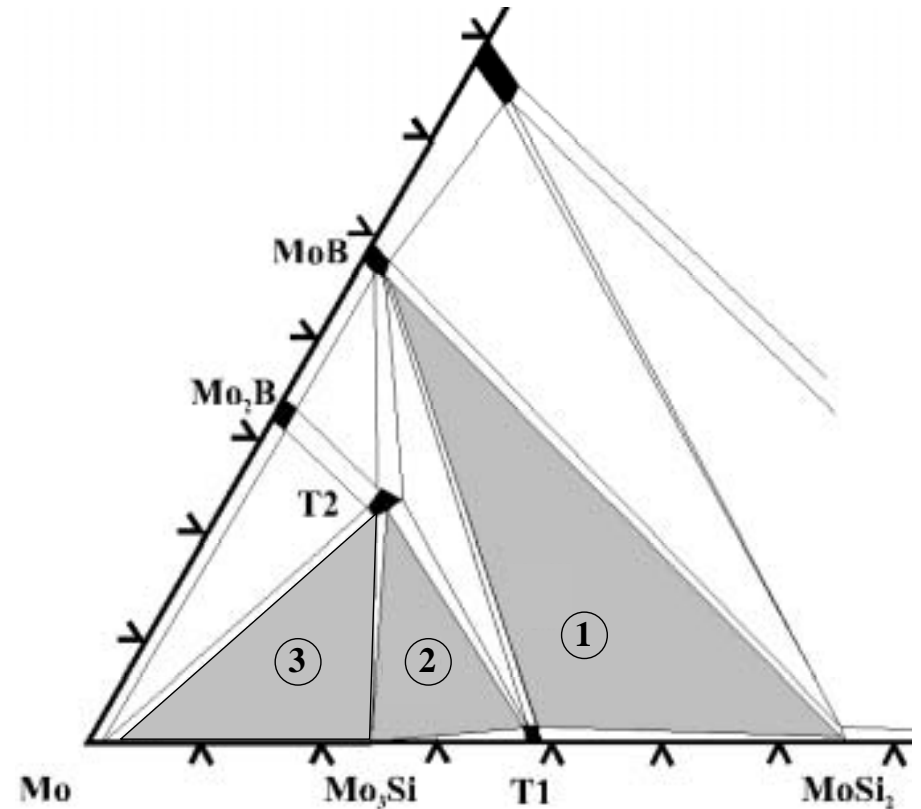


1100°C

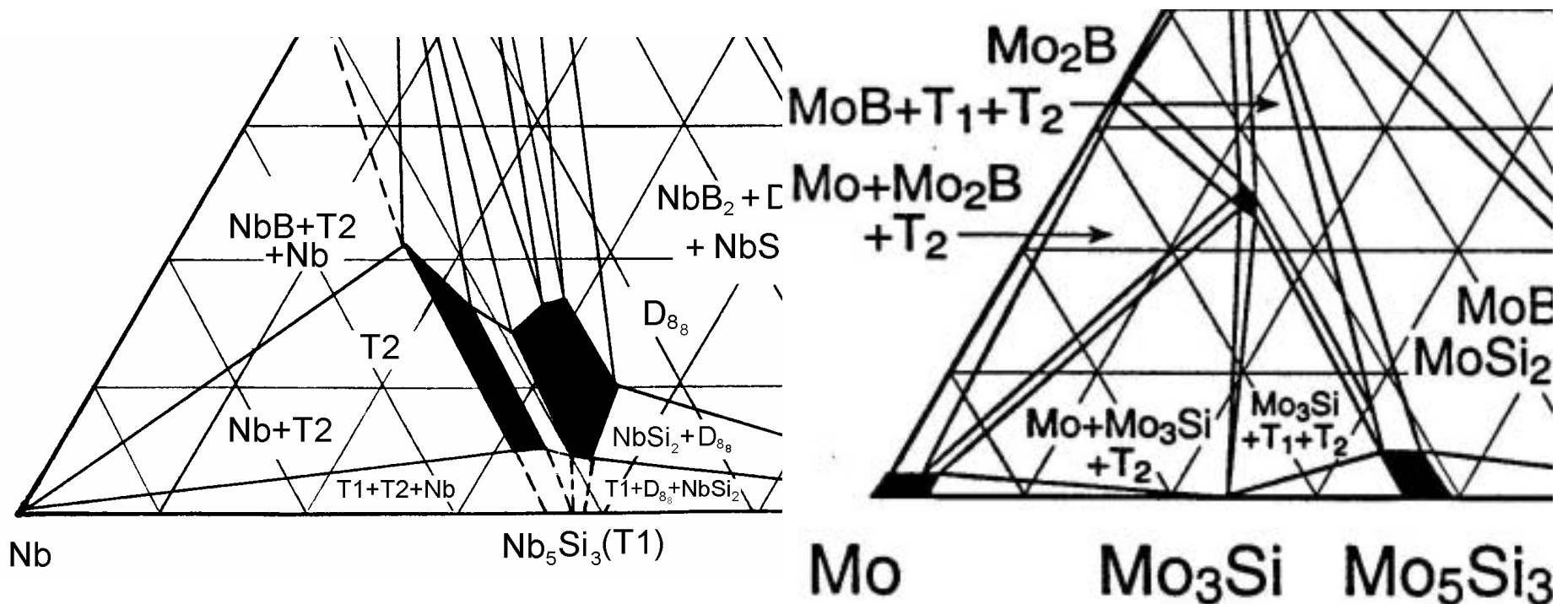


Summary

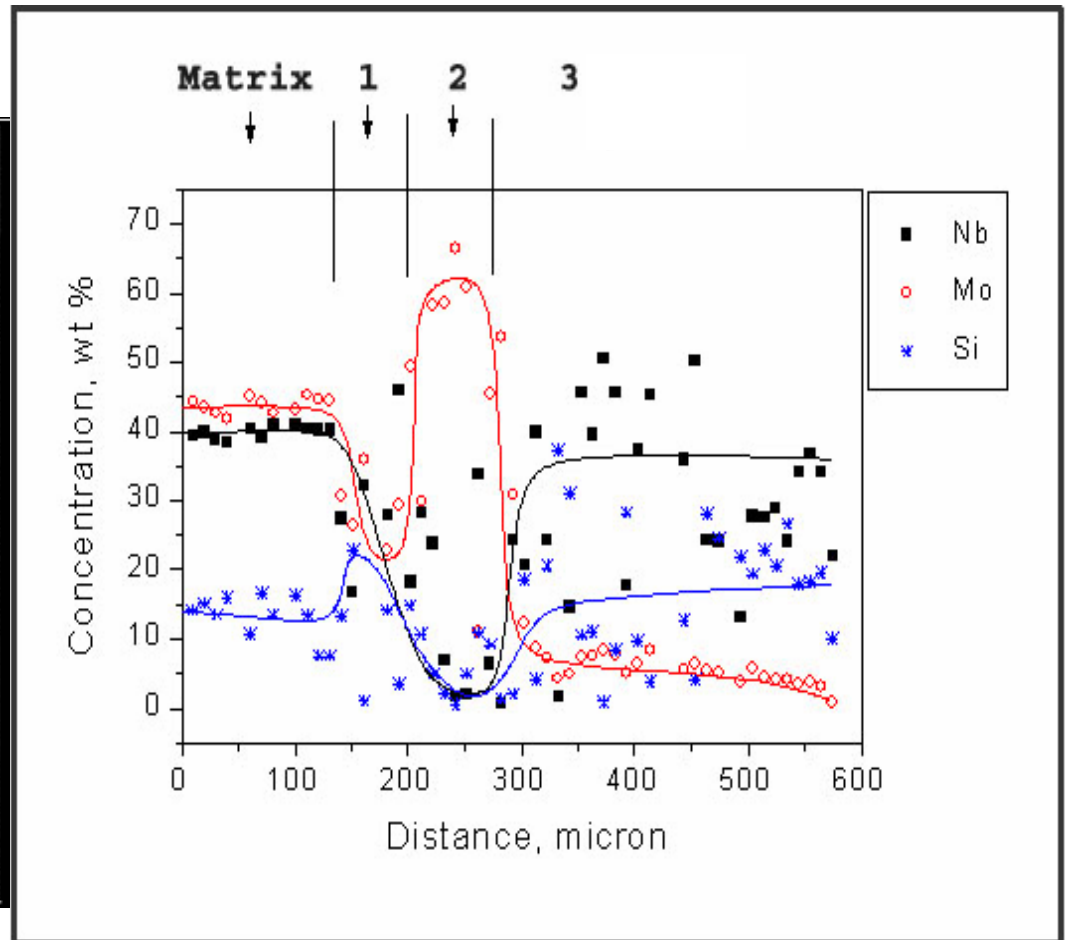
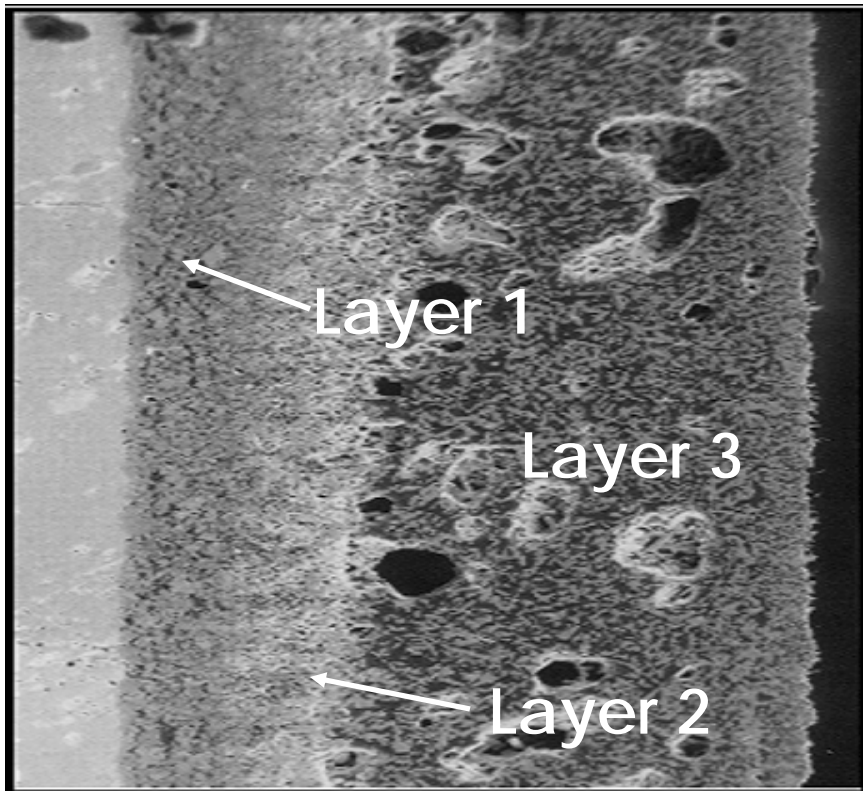
- **Dry Air**
 - All alloys show protective silica scale
 - T up to 1600 C
- **Wet Air**
 - Alloys 1 & 2 protective silica scale
 - Thicker than dry air
 - Alloy 3, highly variable
 - Due to overall low Si content
 - Size and distribution of metal phase
- **Combustion Gas**
 - Alloys 1 & 2 mixed results
 - Better with higher T
 - Viscosity?
 - Alloy 3
 - Pretreatment or protective coatings may be necessary
- **Stability of the Scale**
 - Source and amount of Si
 - Rate of MoO_2 formation
 - Rate of MoO_3 transportation



Comparison of Nb-Si-B and Mo-Si-B Phase Diagrams



EPMA Analysis of Oxide Scale of Nb-Mo-Si-B Alloy



Future Work

- Oxidation
 - Cyclic testing: scale adherence
 - Selected testing in synthetic oxidizing combustion atmosphere to 1500°C
 - Consider alloying strategies to improve Alloy 3 oxidation at higher temps
- Advanced processing techniques
 - Injection molding: test bars (3 x 4 x 25 mm), example components
 - Plasma spraying: Alloy 1/2 coating on Alloy 3 substrates for oxidation testing
- Develop Nb-Mo-Si-B compositions
 - Coexistence of (Nb,Mo) with oxidation resistant quaternary silicide
 - Processing strategies to selectively remove Nb from surface

