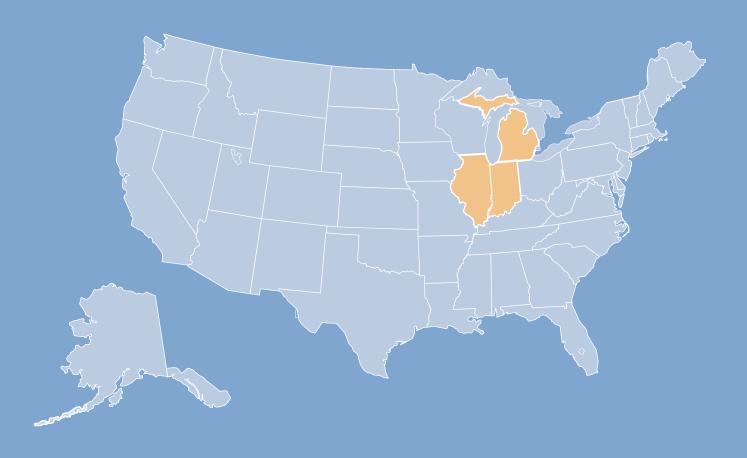
### BASIN ORIENTED STRATEGIES FOR CO<sub>2</sub> ENHANCED OIL RECOVERY:

### **ILLINOIS & MICHIGAN BASINS**



Prepared for
U.S. Department of Energy
Office of Fossil Energy – Office of Oil and Natural Gas

Prepared by Advanced Resources International

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## BASIN ORIENTED STRATEGIES FOR CO<sub>2</sub> ENHANCED OIL RECOVERY: ILLINOIS AND MICHIGAN BASIN OF ILLINOIS, INDIANA, KENTUCKY AND MICHIGAN

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### **TABLE OF CONTENTS**

### 1. SUMMARY OF FINDINGS

- 1.1 INTRODUCTION
- 1.2 ALTERNATIVE OIL RECOVERY STRATEGIES AND SCENARIOS
- 1.3 OVERVIEW OF FINDINGS
- 1.4. ACKNOWLEDGEMENTS

### 2. INTRODUCTION

- 2.1 CURRENT SITUATION
- 2.2 BACKGROUND
- 2.3 PURPOSE
- 2.4 KEY ASSUMPTIONS
- 2.5 TECHNICAL OBJECTIVES
- 2.6 OTHER ISSUES

### 3. OVERVIEW OF ILLINOIS AND MICHIGAN BASIN OIL PRODUCTION

- 3.1 HISTORY OF OIL PRODUCTION
- 3.2 EXPERIENCE WITH IMPROVED OIL RECOVERY
- 3.3 THE "STRANDED OIL" PRIZE
- 3.4 REVIEW OF PRIOR STUDIES

### 4. MECHANISMS OF CO2-EOR

- 4.1 MECHANISMS OF MISCIBLE CO<sub>2</sub>-EOR.
- 4.2 MECHANISMS OF IMMISCIBLE CO<sub>2</sub>-EOR
- 4.3 INTERACTIONS BETWEEN INJECTED CO<sub>2</sub> AND RESERVOIR OIL.

### 5. STUDY METHODOLOGY

- 5.1 OVERVIEW
- 5.2 ASSEMBLING THE MAJOR OIL RESERVOIRS DATA BASE
- 5.3 SCREENING RESERVOIRS FOR CO<sub>2</sub>-EOR.
- 5.4 CALCULATING MINIMUM MISCIBILITY PRESSURE
- 5.5 CALCULATING OIL RECOVERY
- 5.6 ASSEMBLING THE COST MODEL
- 5.7 CONSTRUCTING AN ECONOMICS MODEL
- 5.8 PERFORMING SCENARIO ANALYSES

### 6. RESULTS BY STATE

- 6.1 ILLINOIS
- 6.2 INDIANA AND KENTUCKY
- 6.3 MICHIGAN

### **LIST OF FIGURES**

Figure 1	Impact of Technology and Financial Conditions on Economically Recoverable Oil from Illinois and Michigan Basin's Major Reservoirs Using CO <sub>2</sub> -EOR (Million Barrels)
Figure 2	Location of Major Illinois and Michigan Basin Large Oil Fields Amenable to CO <sub>2</sub> -EOR
Figure 3	Location of Refineries and Hydrogen Capacity Relative to Large Illinois and Michigan Basin Oil Fields
Figure 4 Figure 5 Figure 6A Figure 6B Figure 7A	Illinois and Michigan Basin Historical Oil Production since 1930 One-Dimensional Schematic Showing the CO <sub>2</sub> Miscible Process Carbon Dioxide, CH <sub>4</sub> and N <sub>2</sub> densities at 105°F Carbon Dioxide, CH <sub>4</sub> and N <sub>2</sub> viscosities at 105°F Relative Oil Volume vs. Pressure for a Light West Texas Reservoir Fluid
Figure 7B Figure 8	Oil Swelling Factor vs. Pressure for a Heavy Oil in Turkey Viscosity Reduction Versus Saturation Pressure
Figure 9	Estimating CO <sub>2</sub> Minimum Miscibility Pressure
Figure 10	Correlation of MW C5+ to Tank Oil Gravity
Figure 11	Large Illinois Oil Fields
Figure 12 Figure 13	Large Illinois and Kentucky Anchor Fields Albion/Scipio Oil Field, Michigan
	LIST OF TABLES
Table 1	Size and Distribution of Illinois and Michigan Basin's Oil Reservoirs Data Base
Table 2	Illinois and Michigan Basin's "Stranded Oil" Amenable to CO <sub>2</sub> -EOR
Table 3	Applicability of Miscible and Immiscible CO <sub>2</sub> -EOR
Table 4	Economically Recoverable Resources - Scenario #1: "Traditional Practices" CO <sub>2</sub> -EOR
Table 5	Economically Recoverable Resources — Alternative Scenarios.
Table 6	Potential CO <sub>2</sub> Supply Requirements in the Illinois and Michigan Basin: Scenario #4 ("Ample Supplies of CO <sub>2</sub> ")
Table 7	Matching of CO <sub>2</sub> -EOR Technology with Illinois and Michigan Basin's Oil Reservoirs
Table 8	Crude Oil Annual Production, Ten Largest Illinois and Michigan Basin Oil Fields, 2002-2004 (Million Barrels per Year)
Table 9	Selected Major Oil Fields of the Illinois and Michigan Basin
Table 10	Reservoir Data Format: Major Oil Reservoirs Data Base
Table 11	Illinois and Michigan Basin Oil Reservoirs Screened Amenable for CO <sub>2</sub> -EOR
Table 12	Economic Model Established by the Study
Table 13	Recent History of Illinois Oil Production
Table 14	Status of Large Illinois Oil Fields/Reservoirs as of 2000
Table 15	Reservoir Properties and Improved Oil Recovery Activity, Large Illinois Oil Fields/Reservoirs

Table 16	Economic Oil Recovery Potential Under Two Technologic Conditions, Illinois
Table 17	Economic Oil Recovery Potential with More Favorable Financial Conditions, Illinois
Table 18	Recent History of Indiana Oil Production
Table 19	Recent History of Kentucky Oil Production
Table 20	Status of Large Indiana and Kentucky Oil Fields/Reservoirs (as of 2002)
Table 21	Reservoir Properties and Improved Oil Recovery Activity, Large Indiana Oil Fields/Reservoirs
Table 22	Economic Oil Recovery Potential Under Two Technologic Conditions, Indiana and Kentucky
Table 23	Economic Oil Recovery Potential with More Favorable Financial Conditions, Indiana and Kentucky
Table 24	Recent History of Michigan Oil Production.
Table 25	Status of Large Michigan Oil Fields/Reservoirs as of 2003
Table 26	Reservoir Properties and Improved Oil Recovery Activity, Large Michigan Oil Fields/Reservoirs
Table 27	Economic Oil Recovery Potential Under Two Technologic Conditions, Michigan
Table 28	Economic Oil Recovery Potential with More Favorable Financial Conditions, Michigan

### 1. SUMMARY OF FINDINGS

**1.1 INTRODUCTION**. The Illinois and Michigan Basin oil and gas producing region of Illinois, Indiana, Kentucky and Michigan has an original oil endowment of 17.8 billion barrels. Of this, 6.3 billion barrels (36%) has been produced or proven. As such, nearly 11.5 billion barrels of oil will be left in the ground, or "stranded", following the use of traditional oil recovery practices. A major portion of this "stranded oil" is in reservoirs technically and economically amenable to enhanced oil recovery (EOR) using carbon dioxide (CO<sub>2</sub>) injection.

This report evaluates the future CO<sub>2</sub>-EOR oil recovery potential from the large oil fields of the Illinois and Michigan Basin, highlighting the barriers that stand in the way of achieving this potential. The report then discusses how a concerted set of "basin oriented strategies" could help Illinois and Michigan Basin's oil production industry overcome these barriers helping increase domestic oil production.

**1.2 ALTERNATIVE OIL RECOVERY STRATEGIES AND SCENARIOS.** The report sets forth four scenarios for using CO<sub>2</sub>-EOR to recover "stranded oil" in the Illinois and Michigan Basin producing region.

- The first scenario captures how CO<sub>2</sub>-EOR technology has been applied and has performed in the past. This low technology, high-risk scenario is called "Traditional Practices".
- The second scenario, entitled "State-of-the-art", assumes that the technology progress in CO<sub>2</sub>-EOR, achieved in recent years and in other areas, is successfully applied in the Illinois and Michigan Basin. In addition, this scenario assumes that a comprehensive program of research, pilot tests and field demonstrations help lower the risks inherent in applying new technology to Illinois and Michigan Basin oil reservoirs.
- The third scenario, entitled "Risk Mitigation" examines how the economic potential of CO<sub>2</sub>-EOR could be increased through a strategy involving state production tax reductions, federal investment tax credits, royalty relief and/or higher world oil prices that together would add an equivalent \$10 per barrel to the price that the producer uses for making capital investment decisions for CO<sub>2</sub>-EOR.
- The final scenario, entitled "Ample Supplies of CO<sub>2</sub>," examines the impact of aggregating low-cost, "EOR-ready" CO<sub>2</sub> supplies from various industrial and

natural sources. These CO<sub>2</sub> supply sources include industrial high-concentration CO<sub>2</sub> emissions from hydrogen facilities, gas processing plants, chemical plants and other sources in the region. These would be augmented, in the longer-term, from low concentration CO<sub>2</sub> emissions from refineries and electric power plants. Capture of industrial CO<sub>2</sub> emissions could also be part of a national effort for reducing greenhouse gas emissions.

- **1.3 OVERVIEW OF FINDINGS**. Twelve major findings emerge from the study of "Basin Oriented Strategies for CO<sub>2</sub> Enhanced Oil Recovery: Illinois and Michigan Basin of Illinois, Indiana, Kentucky and Michigan".
- 1. Today's oil recovery practices will leave behind a large resource of "stranded oil" in the Illinois and Michigan Basin. The original oil resource in the Illinois and Michigan Basin reservoirs was 17.8 billion barrels. To date, 6.3 billion barrels of this original oil in-place (OOIP) has been recovered or proved. Thus, without further efforts, 11.5 billion barrels of Illinois and Michigan Basin's oil resource will become "stranded", Table 1.

Table 1. Size and Distribution of the Illinois and Michigan Basin's Oil Reservoirs Data Base

Region	No. of Reservoirs	OOIP (Billion Bbls)	Cumulative Recovery/Reserves* (Billion Bbls)	ROIP (Billion Bbls)
A. Major Oil Reserve	oirs			
Illinois*	82 6.9 2.7		2.7	4.2
Indiana**	17	0.7	0.2	0.5
Kentucky***	35	1.7	0.4	1.3
Michigan****	20	1.4	0.5	0.9
Data Base Total	154	10.6	3.9	6.8
B. Regional Total*	n/a	17.8	6.3	11.5

Estimated from state data on cumulative oil recovery and proved reserves

2. The great bulk of the "stranded oil" resource in the large oil reservoirs of the Illinois and Michigan Basin is amenable to CO<sub>2</sub> enhanced oil recovery. To address the "stranded oil" issue, Advanced Resources assembled a data base that contains 154 major Illinois and Michigan Basin oil reservoirs, accounting for 61% of the region's estimated ultimate oil production. Of these, 72 reservoirs, with 4.5 billion barrels of OOIP and 3.7 billion barrels of "stranded oil" (ROIP)), were found to be favorable for CO<sub>2</sub>-EOR, as shown below by region, Table 2.

Table 2. The Illinois and Michigan Basin's "Stranded Oil" Amenable to CO<sub>2</sub>-EOR

Region	No. of Reservoirs	OOIP (Million Bbls)	Cumulative Recovery/ Reserves (Million Bbls)	ROIP (Million Bbls)
Illinois	46	3,120	490	2,630
Indiana	7	240	50	190
Kentucky	8	210	40	170
Michigan	11	970	230	740
TOTAL	72	4,540	810	3,730

<sup>\*</sup> as of the end of 2001

<sup>\*\*</sup> as of the end of 2002

<sup>\*\*\*</sup> as of the end of 1994/1995

<sup>\*\*\*\*</sup> as of the end of 2004

3. Application of miscible CO<sub>2</sub>-EOR would enable a significant portion of the Illinois and Michigan Basin's "stranded oil" to be recovered. Of the 72 large Illinois and Michigan Basin oil reservoirs favorable for CO<sub>2</sub>-EOR, 24 reservoirs (with 2.2 billion barrels OOIP) screen as being favorable for miscible CO<sub>2</sub>-EOR. The remaining 48 oil reservoirs (with 2.3 billion barrels OOIP) screen as being favorable for immiscible CO<sub>2</sub>-EOR. The total technically recoverable resource from applying CO<sub>2</sub>-EOR in these 72 large oil reservoirs, ranges from 220 million barrels to 810 million barrels, depending on the type of CO<sub>2</sub>-EOR technology that is applied — "Traditional Practices" or "State-of-the-art", Table 3.

Table 3. Applicability of Miscible and Immiscible CO<sub>2</sub>-EOR

	Miscible			Immiscible		
Region	No. of Reservoirs	Technically Recoverable* (MMBbls)		No. of Reservoirs	Technically Recoverable (MMBbls)	
		Traditional Practices	State of the Art		Traditional Practices	State of the Art
Illinois	16	130	300	30	-	190
Indiana	0	-	-	7	-	50
Kentucky	0	-	-	8	-	40
Michigan	8	90	210	3	-	20
TOTAL	24	220	510	48	-	300

4. Under "Traditional Practices" CO<sub>2</sub> flooding technology, high CO<sub>2</sub> costs and high risks, pursuing Illinois and Michigan Basin's "stranded oil" is not economically feasible. Traditional application of miscible CO<sub>2</sub>-EOR technology to the 72 large reservoirs in the data base would enable 220 million barrels of "stranded oil" to become technically recoverable from the Illinois and Michigan Basin. However, with the assumed high costs for CO<sub>2</sub> in the Illinois and Michigan Basin (equal to \$1.50 per Mcf at \$30 Bbl), uncertainties about future oil prices and the performance of CO<sub>2</sub>-EOR technology, none of this "stranded oil" would become economically recoverable at oil prices of \$30 per barrel as adjusted for gravity and location, Table 4.

Table 4. Economically Recoverable Resources - Scenario #1: "Traditional Practices" CO<sub>2</sub>-EOR

	No. of OOIP		Economically* Recoverable		
Region	Reservoirs	(MMBbls)	(# Reservoirs)	(MMBbls)	
Illinois	16	1,360	-	-	
Indiana	-	-	-	-	
Kentucky	-	-	-	-	
Michigan	8	790	-	-	
TOTAL	24	2,150	0	0	

<sup>\*</sup>This case assumes an oil price of \$30 per barrel, a CO<sub>2</sub> cost of \$1.50 per Mcf, and a ROR hurdle rate of 25% (before tax).

5. Introduction of "State-of-the-art" CO<sub>2</sub>-EOR technology, risk mitigation incentives and lower CO<sub>2</sub> costs would enable 0.6 billion barrels of additional oil to become economically recoverable from the Illinois and Michigan Basin. With "State-of-the-art" CO<sub>2</sub>-EOR technology and its higher oil recovery efficiency (but at oil prices of \$30 a barrel and high cost CO<sub>2</sub>) 500 million barrels of the oil remaining in Illinois and Michigan Basin's reservoirs becomes economically recoverable.

Risk mitigation actions and/or higher oil prices, providing an oil price equal to \$40 per barrel, would enable 600 million barrels of oil to become economically recoverable from Illinois and Michigan Basin's large oil reservoirs.

Lower cost CO<sub>2</sub> supplies, equal to \$0.80 per Mcf at \$40 a barrel and assuming a large-scale CO<sub>2</sub> transportation system and incentives for CO<sub>2</sub> emissions capture, would enable the economic potential to increase to 630 million barrels, Figure 1 and Table 5.

Figure 1. Impact of Technology and Financial Conditions on Economically Recoverable Oil from the Illinois and Michigan Basin's Major Reservoirs Using CO<sub>2</sub>-EOR (Million Barrels)

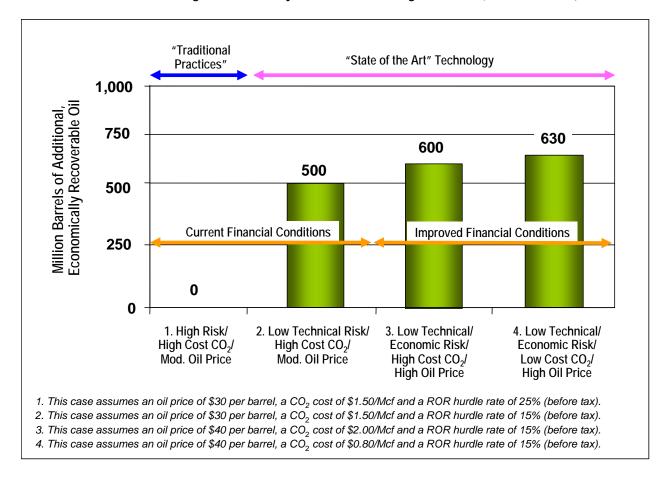


Table 5. Economically Recoverable Resources - Alternative Scenarios

	Scenario	o #2:	Scenario #3:		Scenario #4:	
	"State-of-t	he-art"	"Risk Mi	tigation"	"Ample Supplies of CO <sub>2</sub>	
	(Moderate Oil Price/ High CO <sub>2</sub> Cost)			oil Price/ O₂ Cost)		il Price/ 0₂ Cost)
Region	(# Reservoirs)	(MMBbls)	(# Reservoirs)	(MMBbls)	(# Reservoirs)	(MMBbls)
Illinois	23	380	36	450	37	460
Indiana	0	0	2	30	5	50
Kentucky	8	40	8	40	8	40
Michigan	1	80	1	80	1	80
TOTAL	32	500	47	600	51	630

- 6. Once the results from the study's large oil reservoirs data base are extrapolated to the region as a whole, the technically recoverable CO<sub>2</sub>-EOR potential for the Illinois and Michigan Basin is estimated at nearly 1.5 billion barrels. The large Illinois and Michigan Basin oil reservoirs examined by the study account for 61% of the region's oil resource. Extrapolating the 810 million barrels of technically recoverable EOR potential in these oil reservoirs to the total Illinois and Michigan Basin oil resource provides an estimate of 1,460 million barrels of technical CO<sub>2</sub>-EOR potential. (However, no extrapolation of economic potential has been estimated, as the development costs of the large Illinois and Michigan Basin oil fields may not reflect the development costs for the smaller oil reservoirs in the region.)
- 7. The ultimate additional oil recovery potential from applying CO<sub>2</sub>-EOR in the Illinois and Michigan Basin will, most likely, prove to be higher than defined by this study. Introduction of more advanced "next generation" CO<sub>2</sub>-EOR technologies still in the research or field demonstration stage, such as gravity stable CO<sub>2</sub> injection, extensive use of horizontal or multi-lateral wells and CO<sub>2</sub> miscibility and mobility control agents, could significantly increase recoverable oil volumes. These "next generation" technologies would also expand the state's geologic capacity for storing CO<sub>2</sub> emissions. The benefits and impacts of using "advanced" CO<sub>2</sub>-EOR technology on Illinois and Michigan Basin oil reservoirs may be examined in a separate study.
- 8. A small portion of this CO<sub>2</sub>-EOR potential is already being pursued by operators in the Illinois and Michigan Basin. Three EOR projects are currently underway in small oil fields in Michigan. Together, these three EOR projects have produced or proven over one million barrels of the CO<sub>2</sub>-EOR potential set forth in this study.
- 9. Large volumes of CO<sub>2</sub> supplies will be required in the Illinois and Michigan Basin to achieve the CO<sub>2</sub>-EOR potential defined by this study. The overall market for purchased CO<sub>2</sub> could be over 2.3 Tcf, plus another 4.6 Tcf of recycled CO<sub>2</sub>, Table 6. Assuming that the volume of CO<sub>2</sub> stored equals the volume of CO<sub>2</sub> purchased and that the bulk of purchased CO<sub>2</sub> is from industrial sources, applying CO<sub>2</sub>-EOR to the Illinois and Michigan Basin's oil reservoirs would enable over 115 million metric tonnes of CO<sub>2</sub> emissions to be stored, greatly reducing greenhouse gas emissions. Advanced CO<sub>2</sub>-EOR flooding and CO<sub>2</sub> storage concepts (plus incentives for storing CO<sub>2</sub>) would significantly increase this amount.

Table 6. Potential CO<sub>2</sub> Supply Requirements in the Illinois and Michigan Basin: Scenario #4 ("Ample Supplies of CO<sub>2</sub>")

Region	No. of Reservoirs	Economically Recoverable (MMBbls)	Market for Purchased CO <sub>2</sub> (Tcf)	Market for Recycled CO <sub>2</sub> (Tcf)
Illinois	37	460	1.7	3.4
Indiana	5	50	0.2	0.4
Kentucky	8	40	0.1	0.2
Michigan	1	80	0.3	0.6
TOTAL	51	630	2.3	4.6

**10.** Significant supplies of industrial CO<sub>2</sub> emissions exist in the Illinois and Michigan Basin, sufficient to meet the CO<sub>2</sub> needs for EOR. The natural CO<sub>2</sub> deposits in the Rocky mountains and Mississippi that supply CO<sub>2</sub> to the Permian Basin and Mississippi CO<sub>2</sub>-EOR fields are absent in the Midwest. However, CO<sub>2</sub> emissions, from gas processing plants and hydrogen plants could provide 13 Bcf per year of high concentration (relatively low cost) CO<sub>2</sub>, equal to 0.3 Tcf of CO<sub>2</sub> supply in 20 years. Finally, almost unlimited supplies of low concentration CO<sub>2</sub> emissions (equal to over 130 Tcf of CO<sub>2</sub> supply in 20 years) would be available from the large power plants and refineries in the region, assuming affordable cost CO<sub>2</sub> capture technology is developed.

11. A public-private partnership will be required to overcome the many barriers facing large scale application of CO<sub>2</sub>-EOR in the Illinois and Michigan Basin's oil fields. The challenging nature of the current barriers — lack of sufficient, low-cost CO<sub>2</sub> supplies, uncertainties as to how the technology will perform in the Illinois and Michigan Basin's oil fields, and the considerable market and oil price risks — all argue that a partnership involving the oil production industry, potential CO<sub>2</sub> suppliers and transporters, the Illinois and Michigan Basin states and the federal government will be needed to overcome these barriers.

- 12. Many entities will share in the benefits of increased CO<sub>2</sub>-EOR based oil production in the Illinois and Michigan Basin. Successful introduction and wide-scale use of CO<sub>2</sub>-EOR in the Illinois and Michigan Basin will stimulate increased economic activity, provide new higher paying jobs, and lead to higher tax revenues for the state. It will also help revive a declining domestic oil production and service industry.
- **1.4 ACKNOWLEDGEMENTS**. Advanced Resources would like to acknowledge the most valuable assistance provided to the study by a series of individuals and organizations in Illinois, Indiana, Kentucky and Michigan.

In Illinois, we would like to thank the Illinois Geologic Survey, Oil and Gas Division, particularly Ms. Beverly Seyler, Mr. Scott Frailey and Mr. Brian Huff, for providing detailed historical oil production and well data for the oil producing fields within the state as well as allowing ARI advanced access to the Oil and Gas Division's waterflood data base. This information was instrumental in allowing ARI to determine the breakout of producing to injecting wells for each oil reservoir within the state.

In Kentucky, we would like to thank the Kentucky Geological Survey, particularly Brian Nuttall, for providing historical oil production for Kentucky.

### 2. INTRODUCTION

**2.1 CURRENT SITUATION.** The Illinois and Michigan Basin oil producing region addressed in the report is mature and in decline. Stemming the decline in oil production will be a major challenge, requiring a coordinated set of actions by numerous parties who have a stake in this problem — Illinois and Michigan Basin state revenue and economic development officials; private, state and federal royalty owners; the Illinois and Michigan Basin oil production and refining industry; the public, and the federal government.

The main purpose of this report is to provide information to these "stakeholders" on the potential for pursuing CO<sub>2</sub> enhanced oil recovery (CO<sub>2</sub>-EOR) as one option for slowing and potentially stopping the decline in the Illinois and Michigan Basin's oil production.

This report, "Basin Oriented Strategies for  $CO_2$  Enhanced Oil Recovery: Illinois and Michigan Basin of Illinois, Indiana, Kentucky and Michigan," provides information on the size of the technical and economic potential for  $CO_2$ -EOR in the Illinois and Michigan Basin oil producing regions. It also identifies the many barriers — insufficient and costly  $CO_2$  supplies, high market and economic risks, and concerns over technology performance — that currently impede the cost-effective application of  $CO_2$ -EOR in the Illinois and Michigan Basin oil producing region.

**2.2 BACKGROUND**. The Illinois and Michigan Basin of Illinois, Indiana, Kentucky and Michigan currently produce 51 thousand barrels of oil per day (in 2004). However, the deep, light oil reservoirs of this region are ideal candidates for miscible carbon dioxide-based enhanced oil recovery (CO<sub>2</sub>-EOR). The Illinois and Michigan Basin oil producing region and the location of its major oil fields amenable to CO<sub>2</sub>-EOR are shown in Figure 2.

Illinois and Michigan Basin Oil Fields Oil Field County Line State Line Michigan City WI Grand Rapids **E**Flint Lansing Rockford Detroit Chicago IA Illinois Fort Wayne Moline Peoria Indiana OH Springfield Decatur Indianapolis Louisville Evansville WV Lexington MO Kentucky 240 Miles 180 120 **VA** 

Figure 2. Location of Major Illinois and Michigan Basins Large Oil Fields Amenable to CO<sub>2</sub>-EOR.

**2.3 PURPOSE**. This report, "Basin Oriented Strategies for CO<sub>2</sub> Enhanced Oil Recovery: Illinois and Michigan Basin of Illinois, Indiana, Kentucky and Michigan" is part of a larger effort to examine the enhanced oil recovery and CO<sub>2</sub> storage potential in key U.S. oil basins. The work involves establishing the geological and reservoir characteristics of the major oil fields in the region; examining the available CO<sub>2</sub> sources, volumes and costs; calculating oil recovery and CO<sub>2</sub> storage capacity; and, examining the economic feasibility of applying CO<sub>2</sub>-EOR. The aim of this report is to provide information that could assist in: (1) formulating alternative public-private partnership strategies for developing lower-cost CO<sub>2</sub> capture technology; (2) launching R&D/pilot projects of advanced CO<sub>2</sub> flooding technology; and, (3) structuring royalty/tax incentives and policies that would help accelerate the application of CO<sub>2</sub>-EOR and CO<sub>2</sub> storage.

An additional important purpose of the study is to develop a desktop modeling and analytical capability for "basin oriented strategies" that would enable Department of Energy/Fossil Energy (DOE/FE) itself to formulate policies and research programs that would support increased recovery of domestic oil resources. As such, this desktop model complements, but does not duplicate, the more extensive TORIS modeling system maintained by DOE/FE's National Energy Technology Laboratory.

**2.4 KEY ASSUMPTIONS**. For purposes of this study, it is assumed that sufficient supplies of CO<sub>2</sub> will become available, by pipeline from industrial sources such as the hydrogen plants and refineries in Whiting, Indiana; and Wood River, Illinois, which produce 35 million cubic feet of CO<sub>2</sub> per day, Figure 3. In addition, gas processing and chemical plants in the region and particularly the electric power plants in these four states could provide a billion cubic feet of CO<sub>2</sub> per day. The study assumes that this CO<sub>2</sub> will become available in the near future, before the oil fields in the region are abandoned.

Illinois and Michigan Basin Oil Fields Oil Field County Line **Michigan** State Line Refinery with Hydrogen Capacity City **Grand Rapids** Flint ₹<u>}</u>-Lansing Rockford Detroit Chicago IA Illinois Moline Fort Wayne Peoria Indiana OH Springfield Decatur Indianapolis Louisville Evansville WV Lexington Kentucky MO 120 180 240 Miles **60**~ **VA** 

Figure 3. Location of Refineries with Hydrogen Capacity Relative to Large Illinois and Michigan Basin Oil Fields.

2-4

- **2.5 TECHNICAL OBJECTIVES.** The objectives of this study are to examine the technical and the economic potential of applying CO<sub>2</sub>-EOR in the Illinois and Michigan Basin oil region, under two technology options:
  - 1. "Traditional Practices" Technology. This involves the continued use of past CO<sub>2</sub> flooding and reservoir selection practices. It is distinguished by using miscible CO<sub>2</sub>-EOR technology in light oil reservoirs and by injecting moderate volumes of CO<sub>2</sub>, on the order of 0.4 hydrocarbon pore volumes (HCPV), into these reservoirs. (Immiscible CO<sub>2</sub> is not included in the "Traditional Practices" technology option). Given the still limited application of CO<sub>2</sub>-EOR in this region and the inherent technical and geologic risks, operators typically add a risk premium when evaluating this technology option in the Illinois and Michigan Basin.
  - 2. "State-of-the-art" Technology. This involves bringing to the Illinois and Michigan Basin the benefits of recent improvements in the performance of CO<sub>2</sub>-EOR process and gains in understanding of how best to customize its application to the many different types of oil reservoirs in the region. As further discussed below, moderately deep, light oil reservoirs are selected for miscible CO<sub>2</sub>-EOR and the shallower light oil and the heavier oil reservoirs are targeted for immiscible CO<sub>2</sub>-EOR. "State-of-the-art" technology entails injecting much larger volumes of CO<sub>2</sub>, on the order of 1 HCPV, with considerable CO<sub>2</sub> recycling.

Under "State-of-the-art" technology, with CO<sub>2</sub> injection volumes more than twice as large, oil recovery is projected to be higher than reported for past field projects using "Traditional Practices". The CO<sub>2</sub> injection/oil recovery ratio may also be higher under this technology option, further spotlighting the importance of lower cost CO<sub>2</sub> supplies. With the benefits of field pilots and pre-commercial field demonstrations, the risk premium for this technology option and scenario would be reduced to conventional levels.

The set of oil reservoirs to which CO<sub>2</sub>-EOR would be applied fall into two groups, as set forth below:

- 1. Favorable Light Oil Reservoirs Meeting Stringent CO<sub>2</sub> Miscible Flooding Criteria. These are the moderately deep, higher gravity oil reservoirs where CO<sub>2</sub> becomes miscible (after extraction of hydrocarbon components into the CO<sub>2</sub> phase and solution of CO<sub>2</sub> in the oil phase) with the oil remaining in the reservoir. Typically, reservoirs at depths greater than 3,000 feet and with oil gravities greater than 25 °API would be selected for miscible CO<sub>2</sub>-EOR. Major Illinois and Michigan Basin light oil fields such as Clay City Consolidated (IL) and Albion-Scipio (MI) fit into this category. The great bulk of past CO<sub>2</sub>-EOR floods have been conducted in these types of "favorable reservoirs".
- 2. Challenging Reservoirs Involving Immiscible Application of CO<sub>2</sub>-EOR. These are the moderately heavy oil reservoirs (as well as shallower light oil reservoirs) that do not meet the stringent requirements for miscibility. This reservoir set includes the large Illinois and Michigan Basin oil fields, such as Griffin Consolidated (IN) and New Harmony Consolidated (IL), which still hold a significant portion of their original oil. Illinois and Michigan Basin reservoirs at depths greater than 2,000 feet with oil gravities between 17.5° and 25 °API (or higher) would generally be included in this category.

Combining the technology and oil reservoir options, the following oil reservoir and CO<sub>2</sub> flooding technology matching is applied to the Illinois and Michigan Basin's reservoirs amenable to CO<sub>2</sub>-EOR, Table 7.

Table 7. Matching of CO<sub>2</sub>-EOR Technology With the Illinois and Michigan Basin's Oil Reservoirs

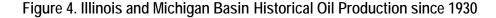
CO₂-EOR Technology Selection	Oil Reservoir Selection
"Traditional Practices" Miscible CO <sub>2</sub> -EOR	<ul> <li>24 Deep, Light Oil Reservoirs</li> </ul>
"State-of-the-art" Miscible and Immiscible CO <sub>2</sub> -EOR	<ul><li>24 Deep, Light Oil Reservoirs</li><li>48 Deep, Moderately Heavy Oil Reservoirs</li></ul>

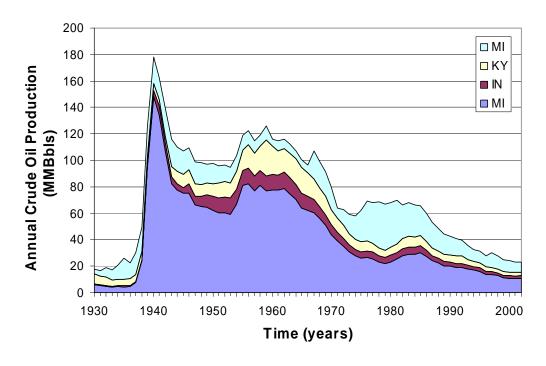
2.6 OTHER ISSUES. This study draws on a series of sources for basic data on the reservoir properties and the expected technical and economic performance of CO<sub>2</sub>-EOR in the Illinois and Michigan Basin's major oil reservoirs. Because of confidentiality and proprietary issues, the results of the study have been aggregated for the three producing areas within the Illinois and Michigan Basin. As such, reservoir-level data and results are not provided and are not available for general distribution. However, selected non-confidential and non-proprietary information at the field and reservoir level is provided in the report and additional information could be made available for review, on a case by case basis, to provide an improved context for the state level reporting of results in this report.

### 3. OVERVIEW OF ILLINOIS AND MICHIGAN BASINOIL PRODUCTION

3.1 HISTORY OF OIL PRODUCTION. Oil production for the Illinois and Michigan Basin of United States — encompassing Illinois, Indiana, Kentucky and Michigan — has declined in the past 60 years, Figure 4. Since reaching a peak in the 1940's, when oil production was over 480 thousand barrels per day, oil production reached a recent low of 18.5 million barrels (51 thousand barrels per day) in 2004.

- Illinois, the largest oil producing state in the region with 9.1 million barrels of oil produced in 2004, has seen a slide in oil production for nearly 60 years.
- Indiana, with 1.9 million barrels of oil produced in 2004, has seen a slide in oil production for nearly 40 years.
- Kentucky, with 2.5 million barrels of oil produced in 2004, has also seen a slide in oil production for nearly 40 years.
- Michigan, with 5.0 million barrels of oil produced in 2004, has seen a slide in production in the past 25 years.





However, the Illinois and Michigan Basin still holds a rich resource of oil in the ground. With 17.8 billion barrels of original oil in-place (OOIP) and approximately 6.3 billion barrels expected to be recovered, 11.5 billion barrels of oil will be "stranded" due to lack of technology, lack of sufficient, affordable CO<sub>2</sub> supplies and high economic and technical risks.

Table 8 presents the status and annual oil production for the ten largest Illinois and Michigan Basin oil fields (based on OOIP) that account for about 28% of the oil production in this region. The table shows that for nine of the largest oil fields production is stable or in decline. Increasing the Illinois and Michigan Basin's oil production could be attained by applying enhanced oil recovery technology, particularly CO<sub>2</sub>-EOR.

Table 8. Crude Oil Annual Production, Ten Largest Illinois and Michigan Basin Oil Fields, 2002-2004 (Million Barrels per Year)

Major Oil Fields	2002	2003	2004	Production Status
Lawrence County Division (IL)	1.3	1.2	1.0	Declining
Clay City Consolidated (IL)	1.1	1.2	1.2	Stable
Main Consolidated (IL)	1.0	1.0	0.9	Stable
Salem Consolidated (IL)	0.6	0.6	0.7	Stable
New Harmony Consolidated (IL)	0.4	0.6	0.6	Increasing
Louden (IL)	0.5	0.5	0.5	Stable
Sailor Springs (IL)	0.3	0.3	0.3	Stable
Dale City (IL)	0.1	0.1	0.1	Stable
Roland (IL)	0.1	0.1	0.1	Stable
Albion/Scipio (MI)	low*	low*	low*	Stable

<sup>\*</sup> field production <10 MBbls/yr.

3.2 EXPERIENCE WITH IMPROVED OIL RECOVERY. Illinois and Michigan Basin oil producers are familiar with using technology for improving oil recovery. For example, producers have used waterflooding in the Illinois basin since the 1950's to improve oil recovery. More recently, two small CO<sub>2</sub>-EOR projects have been ongoing for nearly 10 years in Michigan Additional discussion of the experience with CO<sub>2</sub>-EOR in the Illinois and Michigan Basin is provided in Chapter 6.

**3.3 THE "STRANDED OIL" PRIZE.** Even though the Illinois and Michigan Basin's oil production is declining, this does not mean that the resource base is depleted. The four producing regions in the Illinois and Michigan Basin – Illinois, Indiana, Kentucky and Michigan, still contain 65% of their OOIP after primary and secondary oil recovery. This large volume of remaining oil in-place (ROIP) is the "prize" for CO<sub>2</sub>-EOR.

Table 9 provides information on the maturity and oil production history of 8 large Illinois and Michigan Basin oil fields, each with estimated ultimate recovery of 100 million barrels or more.

Table 9. Selected Major Oil Fields of the Illinois and Michigan Basin

	Field/State	Year Discovered	Cumulative Production (MMBbl)	Estimated Reserves (MMBbl)	Remaining Oil In-Place (MMBbl)
1	Lawrence, IL	1906	428	13.2	631
2	Louden, IL	1937	394	4.4	549
3	Salem Consol., IL	1938	399	6.9	529
4	Main Consol., IL	1906	241	7.9	567
5	New Harmony, IL	1939	133	4.0	176
6	Albion/Scipio, MI	1957	125	0.1	165
7	Dale Consol., IL	1940	96	0.6	170
8	Griffin Consol., IN	1938	80	2.3	154

3.4 REVIEW OF PRIOR STUDIES. CO<sub>2</sub>-EOR is beginning to gain attention in the Illinois and Michigan Basins. A recent study by the Illinois State Geological Survey

and Illinois State University screened the Illinois Basin reservoirs for the potential for CO<sub>2</sub>-miscible EOR.

• "CO<sub>2</sub> Sequestration and Enhanced Oil Recovery Potential in Illinois Basin Oil Reservoirs" by the Illinois State Geological Survey and Illinois State University in 2004. The study classified Illinois Basin reservoirs on the basis of CO<sub>2</sub> miscibility. Of the 14.6 billion barrels of OOIP in the basin, 46% of the OOIP screened miscible or near-miscible. Geological and reservoir modeling was then conducted on several candidate fields to test the potential for EOR through CO<sub>2</sub>-miscible injection. Based on this, the study estimated that an additional 10-12% of the fields' OOIP was recoverable through EOR. Extrapolating this result basin wide, they estimate that 0.7-1.6 billion barrels of oil could be produced through CO<sub>2</sub>-EOR.

### 4. MECHANISMS OF CO2-EOR

**4.1 MECHANISMS OF MISCIBLE CO<sub>2</sub>-EOR.** Miscible CO<sub>2</sub>-EOR is a multiple contact process, involving the injected CO<sub>2</sub> and the reservoir's oil. During this multiple contact process, CO<sub>2</sub> will vaporize the lighter oil fractions into the injected CO<sub>2</sub> phase and CO<sub>2</sub> will condense into the reservoir's oil phase. This leads to two reservoir fluids that become miscible (mixing in all parts), with favorable properties of low viscosity, a mobile fluid and low interfacial tension.

The primary objective of miscible CO<sub>2</sub>-EOR is to remobilize and dramatically reduce the after waterflooding residual oil saturation in the reservoir's pore space. Figure 5 provides a one-dimensional schematic showing the various fluid phases existing in the reservoir and the dynamics of the CO<sub>2</sub> miscible process.

Pure CO<sub>2</sub> Vaporizing Condensing Into Oil

Direction of Displacement

Figure 5. One-Dimensional Schematic Showing the CO<sub>2</sub> Miscible Process.

4.2 MECHANISMS OF IMMISCIBLE CO<sub>2</sub>-EOR. When insufficient reservoir pressure is available or the reservoir's oil composition is less favorable (heavier), the injected CO<sub>2</sub> is immiscible with the reservoir's oil. As such, another oil displacement mechanism, immiscible CO<sub>2</sub> flooding, occurs. The main mechanisms involved in immiscible CO<sub>2</sub> flooding are: (1) oil phase swelling, as the oil becomes saturated with CO<sub>2</sub>; (2) viscosity reduction of the swollen oil and CO<sub>2</sub> mixture; (3) extraction of lighter hydrocarbon into the CO<sub>2</sub> phase; and, (4) fluid drive plus pressure. This combination of mechanisms enables a portion of the reservoir's remaining oil to be mobilized and produced. In general, immiscible CO<sub>2</sub>-EOR is less efficient than miscible CO<sub>2</sub>-EOR in recovering the oil remaining in the reservoir.

**4.3 INTERACTIONS BETWEEN INJECTED CO<sub>2</sub> AND RESERVOIR OIL.** The properties of CO<sub>2</sub> (as is the case for most gases) change with the application of pressure and temperature. Figures 6A and 6B provide basic information on the change in CO<sub>2</sub> density and viscosity, two important oil recovery mechanisms, as a function of pressure.

Oil swelling is an important oil recovery mechanism, for both miscible and immiscible CO<sub>2</sub>-EOR. Figures 7A and 7B show the oil swelling (and implied residual oil mobilization) that occurs from: (1) CO<sub>2</sub> injection into a West Texas light reservoir oil; and, (2) CO<sub>2</sub> injection into a very heavy (12 °API) oil reservoir in Turkey. Laboratory work on the Bradford Field (Pennsylvania) oil reservoir showed that the injection of CO<sub>2</sub>, at 800 psig, increased the volume of the reservoir's oil by 50%. Similar laboratory work on Mannville "D" Pool (Canada) reservoir oil showed that the injection of 872 scf of CO<sub>2</sub> per barrel of oil (at 1,450 psig) increased the oil volume by 28%, for crude oil already saturated with methane.

Viscosity reduction is a second important oil recovery mechanism, particularly for immiscible CO<sub>2</sub>-EOR. Figure 8 shows the dramatic viscosity reduction of one to two orders of magnitude (10 to 100 fold) that occur for a reservoir's oil with the injection of CO<sub>2</sub> at high pressure.

Figure 6A. Carbon Dioxide, CH<sub>4</sub> and N<sub>2</sub> densities at 105°F. At high pressures, CO<sub>2</sub> has a density close to that of a liquid and much greater than that of either methane or nitrogen. Densities were calculated with an equation of state (EOS).

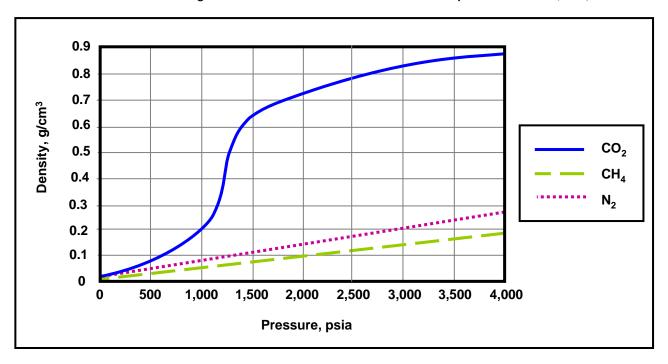
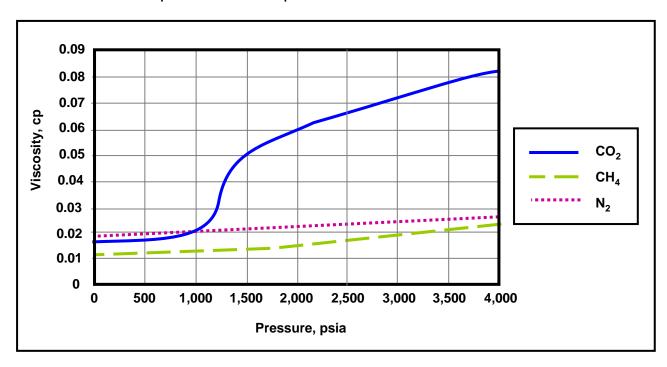


Figure 6B. Carbon Dioxide, CH<sub>4</sub> and N<sub>2</sub> viscosities at 105<sup>0</sup>F. At high pressures, the viscosity of CO<sub>2</sub> is also greater then that of methane or nitrogen, although it remains low in comparison to that of liquids. Viscosities were calculated with an EOS.



February 2006

2500

2000

1000 1500

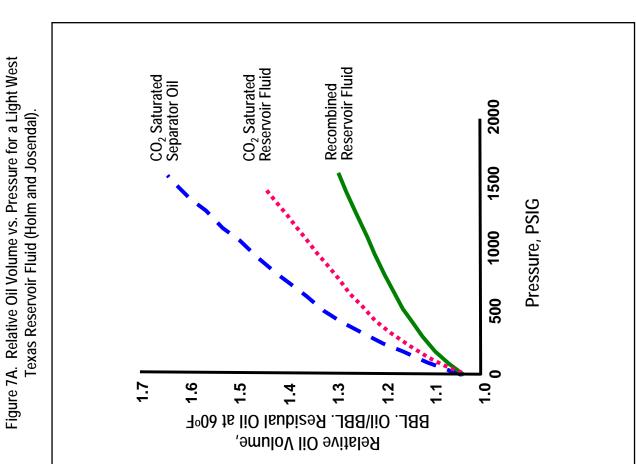
500

Pressure, PSIG

Texas Reservoir Fluid (Holm and Josendal).

Figure 7B. Oil Swelling Factor vs. Pressure for a Heavy Oil

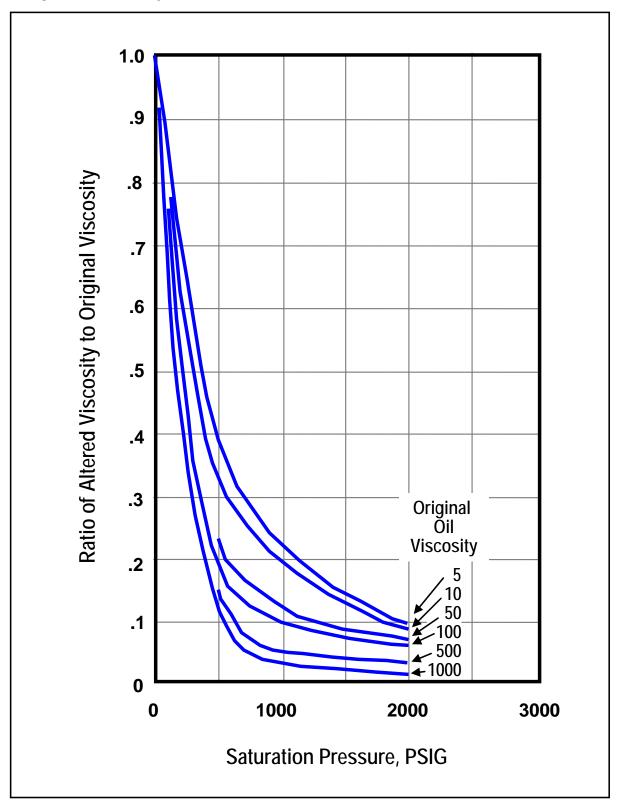
in Turkey (Issever and Topkoya).



1.18 1.16 1.14 1.24 1.22 1.2 1.12 1.06 7: 1.08 1.04 Oil Swelling Factor

4-4





### 5. STUDY METHODOLOGY

5.1 OVERVIEW. A seven part methodology was used to assess the CO<sub>2</sub>-EOR potential of the Illinois and Michigan Basin's oil reservoirs. The seven steps were: (1) assembling the Illinois and Michigan Basin Major Oil Reservoirs Data Base; (2) screening reservoirs for CO<sub>2</sub>-EOR; (3) calculating the minimum miscibility pressure; (4) calculating oil recovery; (5) assembling the cost model; (6) constructing an economics model; and, (7) performing scenario analyses.

An important objective of the study was the development of a desktop model with analytic capability for "basin oriented strategies" that would enable DOE/FE to develop policies and research programs leading to increased recovery and production of domestic oil resources. As such, this desktop model complements, but does not duplicate, the more extensive TORIS modeling system maintained by DOE/FE's National Energy Technology Laboratory.

5.2 ASSEMBLING THE MAJOR OIL RESERVOIRS DATA BASE. The study started with the National Petroleum Council (NPC) Public Data Base, maintained by DOE Fossil Energy. The study updated and modified this publicly accessible data base to develop the Illinois and Michigan Basin Major Oil Reservoirs Data Base for Illinois, Indiana, Kentucky and Michigan.

Table 10 illustrates the oil reservoir data recording format developed by the study. The data format readily integrates with the input data required by the CO<sub>2</sub>-EOR screening and oil recovery models, discussed below. Overall, the Illinois and Michigan Basin Major Oil Reservoirs Data Base contains 154 reservoirs, accounting for 61% of the oil expected to be ultimately produced in Illinois and Michigan Basin by primary and secondary oil recovery processes.

-				ſ		K		
Basin Name								
Field Name								
- 1						į		
Reservoir [						>		
Reservoir Parameters:	TORIS	ARI	Oil Production	TORIS	ARI	Volumes	TORIS	ARI
Area (A)			Producing Wells (active)			OOIP (MMbl)		
Vet Pay (ft)			Producing Wells (shut-in)			Cum P/S Oil (MMbl)		
Depth (ft)			2002 Production (Mbbl)			2002 P/S Reserves (MMbl)		
Porosity			Daily Prod - Field (Bbl/d)			Ult P/S Recovery (MMbl)		
Reservoir Temp (deg F)			Cum Oil Production (MMbbl)			Remaining (MMbbl)		
nitial Pressure (psi)			EOY 2002 Oil Reserves (MMbbl)			P/S Recovery Efficiency (%)		
Pressure (psi)			Water Cut					
						OOIP Volume Check		
30.			Water Production			Reservoir Volume (AF)		
3, @ So, swept			2002 Water Production (Mbbl)			Bbl/AF		
- Soi			Daily Water (Mbbl/d)			OOIP Check (MMbl)		
Swept Zone S <sub>o</sub>			Injection			SROIP Volume Check	×	
·······································			Injection Wells (active)			Reservoir Volume (AF)		
<u></u>			Injection Wells (shut-in)			Swept Zone Bbl/AF		
_ '			2002 Water Injection (MMbbl)			SROIP Check (MMbbl)		
API Gravity			Daily Injection - Field (Mbbl/d)					
/iscosity (cp)			Cum Injection (MMbbl)					
•			Daily Inj per Well (Bbl/d)			ROIP Volume Check	<b>J</b>	
Jykstra-Parsons				•	•	ROIP Check (MMbl)		
			EOR					
			EOR Type					
			2002 EOR Production (MMbbl)	Ш				
			Cum EOR Production (MMbbl)					
			EOR 2002 Reserves (MMbbl)					
			Ultimate Recovery (MMbbl)	_				

Considerable effort was required to construct an up-to-date, volumetrically consistent data base that contained all of the essential data, formats and interfaces to enable the study to: (1) develop an accurate estimate of the size of the original and remaining oil in-place in the Illinois and Michigan Basin; (2) reliably screen the reservoirs as to their amenability for miscible and immiscible CO<sub>2</sub>-EOR; and, (3) provide the CO<sub>2</sub>-PROPHET Model (developed by Texaco for the DOE Class I cost-share program) the essential input data for calculating CO<sub>2</sub> injection requirements and oil recovery.

5.3 SCREENING RESERVOIRS FOR CO<sub>2</sub>-EOR. The data base was screened for reservoirs that would be applicable for CO<sub>2</sub>-EOR. Five prominent screening criteria were used to identify favorable reservoirs. These were: reservoir depth, oil gravity, reservoir pressure, and reservoir temperature and oil composition. These values were used to establish the minimum miscibility pressure for conducting miscible CO<sub>2</sub>-EOR and for selecting reservoirs that would be amenable to this oil recovery process. Reservoirs not meeting the miscibility pressure standard were considered for immiscible CO<sub>2</sub>-EOR.

The preliminary screening steps involved selecting the deeper oil reservoirs that had sufficiently high oil gravity. A minimum reservoir depth of 3,000 feet, at the midpoint of the reservoir, was used to ensure the reservoir could accommodate high pressure CO<sub>2</sub> injection. A minimum oil gravity of 17.5° API was used to ensure the reservoir's oil had sufficient mobility, without requiring thermal injection. Table 11 tabulates the oil reservoirs that passed the preliminary screening step. Because of data limitations, this screening study combined the sands into a single reservoir.

Table 11. Illinois and Michigan Basin Oil Reservoirs Screened Amenable to  ${\rm CO_2\text{-}EOR}$ 

Basin	Field	Formation
A. Illinois		-
Illinois	ALBION	AUX VASES
Illinois	ALBION	MCCLOSKEY
Illinois	ALBION	BETHEL
Illinois	ALBION	BIEHL
Illinois	ALBION	CYPRESS
Illinois	BENTON	TAR SPRINGS
Illinois	CENTRALIA	DEVONIAN
Illinois	CLAY CITY CONSOLIDATED	OHARA
Illinois	CLAY CITY CONSOLIDATED	SPAR MOUNTAIN
Illinois	CLAY CITY CONSOLIDATED	MCCLOSKEY
Illinois	CLAY CITY CONSOLIDATED	ST LOUIS
Illinois	CLAY CITY CONSOLIDATED	SALEM
Illinois	CLAY CITY CONSOLIDATED	AUX VASES
Illinois	CLAY CITY CONSOLIDATED	CYPRESS
Illinois	DALE CITY	AUX VASES
Illinois	DALE CITY	BETHEL
Illinois	INMAN EAST AND WEST	AUX VASES
Illinois	INMAN EAST AND WEST	CYPRESS
Illinois	INMAN EAST AND WEST	TAR SPRINGS
Illinois	JOHNSONVILLE CONSOLIDATED	AUX VASES
Illinois	JOHNSONVILLE CONSOLIDATED	MCCLOSKEY
Illinois	JOHNSONVILLE CONSOLIDATED	SALEM
Illinois	NEW HARMONY CONSOLIDATED	AUX VASES
Illinois	NEW HARMONY CONSOLIDATED	BETHEL
Illinois	NEW HARMONY CONSOLIDATED	CYPRESS
Illinois	NEW HARMONY CONSOLIDATED	MCCLOSKEY
Illinois	PHILLIPSTOWN CONSOLIDATED	MCCLOSKEY
Illinois	PHILLIPSTOWN CONSOLIDATED	AUX VASES
Illinois	PHILLIPSTOWN CONSOLIDATED	BETHEL
Illinois	PHILLIPSTOWN CONSOLIDATED	TAR SPRINGS
Illinois	ROLAND CONSOLIDATED	MCCLOSKEY
Illinois	ROLAND CONSOLIDATED	AUX VASES
Illinois	ROLAND CONSOLIDATED	BETHEL
Illinois	ROLAND CONSOLIDATED	CYPRESS
Illinois	ROLAND CONSOLIDATED	HARDINSBURG
Illinois	ROLAND CONSOLIDATED	WALTERSBURG
Illinois	SAILOR SPRINGS	AUX VASES
Illinois	SAILOR SPRINGS	CYPRESS
Illinois	SAILOR SPRINGS	MCCLOSKEY
Illinois	SAILOR SPRINGS	SPAR MOUNTAIN

Table 11. Illinois and Michigan Basin Oil Reservoirs Screened Amenable to CO<sub>2</sub>-EOR

Basin	Field	Formation
Illinois	SALEM CONSOLIDATED	DEVONIAN
Illinois	SALEM CONSOLIDATED	TRENTON
Illinois	SALEM CONSOLIDATED	MCCLOSKEY
Illinois	SALEM CONSOLIDATED	SALEM
Illinois	SALEM CONSOLIDATED	SPAR MOUNTAIN
Illinois	ST JAMES	CARPER
B. Indiana		
Indiana	GRIFFIN CONSOLIDATED	BETHEL
Indiana	GRIFFIN CONSOLIDATED	CYPRESS
Indiana	GRIFFIN CONSOLIDATED	PAOLI
Indiana	GRIFFIN CONSOLIDATED	STE GENEVIEVE
Indiana	GRIFFIN CONSOLIDATED	TAR SPRINGS
Indiana	GRIFFIN CONSOLIDATED	WALTERSBURG
Indiana	SPRINGFIELD CONSOL.	WALTERSBURG
C. Kentucky		
Kentucky	HITESVILLE CONS	STE GENEVIEVE
Kentucky	HITESVILLE CONS	AUX VASES & WALTERSBURG
Kentucky	HITESVILLE CONS	CHESTER SS
Kentucky	POOLE CONS	CHESTER SS
Kentucky	POOLE CONS	STE GENEVIEVE
Kentucky	SMITH MILLS CONS - SMITH MILLS NORTH	STE GENEVIEVE
Kentucky	SMITH MILLS CONS - SMITH MILLS NORTH	CHESTER SS
Kentucky	UNIONTOWN CONS	CHESTER SS
D. Michigan		
Michigan	ALBION/SCIPIO	TRENTON - BLACK RIVER
Michigan	BUCKEYE NORTH	DUNDEE
Michigan	COLDWATER	DUNDEE
Michigan	DEEP RIVER	DUNDEE
Michigan	KAWKAWLIN	DUNDEE
Michigan	MT PLEASANT	DUNDEE
Michigan	NORWICH EAST	RICHFIELD
Michigan	PORTER	DUNDEE
Michigan	REED CITY	DUNDEE
Michigan	WEST BRANCH	DETROIT RIVER
Michigan	WEST BRANCH	DUNDEE
Michigan	ALBION/SCIPIO	TRENTON - BLACK RIVER

**5.4 CALCULATING MINIMUM MISCIBILITY PRESSURE.** The miscibility of a reservoir's oil with injected  $CO_2$  is a function of pressure, temperature and the

composition of the reservoir's oil. The study's approach to estimating whether a reservoir's oil will be miscible with CO<sub>2</sub>, given fixed temperature and oil composition, was to determine whether the reservoir would hold sufficient pressure to attain miscibility. Where oil composition data was missing, a correlation was used for translating the reservoir's oil gravity to oil composition.

To determine the minimum miscibility pressure (MMP) for any given reservoir, the study used the Cronquist correlation, Figure 9 This formulation determines MMP based on reservoir temperature and the molecular weight (MW) of the pentanes and heavier fractions of the reservoir oil, without considering the mole percent of methane. (Most Illinois and Michigan Basin oil reservoirs have produced the bulk of their methane during primary and secondary recovery.) The Cronquist correlation is set forth below:

 $MMP = 15.988*T^{(0.744206+0.0011038*MW C5+)}$ 

Where: T is Temperature in °F, and MW C5+ is the molecular weight of pentanes and heavier fractions in the reservoir's oil.

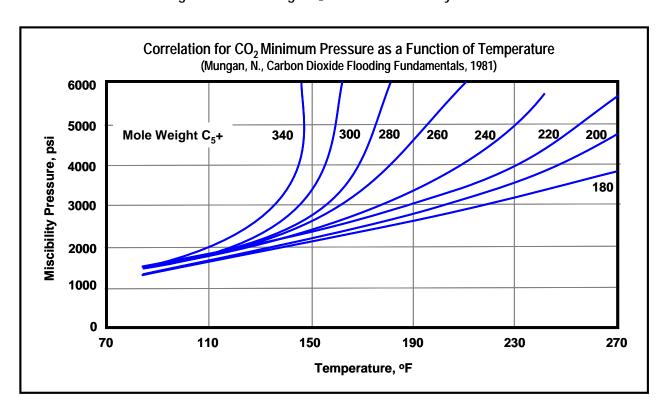


Figure 9. Estimating CO<sub>2</sub> Minimum Miscibility Pressure

The temperature of the reservoir was taken from the data base or estimated from the thermal gradient in the basin. The molecular weight of the pentanes and heavier fraction of the oil was obtained from the data base or was estimated from a correlative plot of MW C5+ and oil gravity, shown in Figure 10.

The next step was calculating the minimum miscibility pressure (MMP) for a given reservoir and comparing it to the maximum allowable pressure. The maximum pressure was determined using a pressure gradient of 0.6 psi/foot. If the minimum miscibility pressure was below the maximum injection pressure, the reservoir was classified as a miscible flood candidate. Oil reservoirs that did not screen positively for miscible CO<sub>2</sub>-EOR were selected for consideration by immiscible CO<sub>2</sub>-EOR.

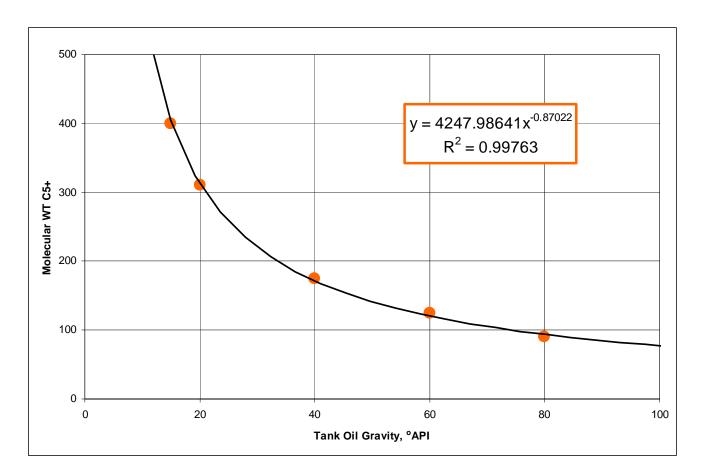


Figure 10. Correlation of MW C5+ to Tank Oil Gravity

**5.5 CALCULATING OIL RECOVERY.** The study utilized  $CO_2$ -PROPHET to calculate incremental oil produced using  $CO_2$ -EOR.  $CO_2$ -PROPHET was developed by the Texaco Exploration and Production Technology Department (EPTD) as part of the DOE Class I cost-share program. The specific project was "Post Waterflood  $CO_2$  Flood in a Light Oil, Fluvial Dominated Deltaic Reservoir" (DOE Contract No. DE-FC22-93BC14960).  $CO_2$ -PROPHET was developed as an alternative to the DOE's  $CO_2$  miscible flood predictive model,  $CO_2$ PM. According to the developers of the model,  $CO_2$ -PROPHET has more capabilities and fewer limitations than  $CO_2$ PM. For example, according to the above cited report,  $CO_2$ -PROPHET performs two main operations that provide a more robust calculation of oil recovery than available from  $CO_2$ PM:

CO<sub>2</sub>-PROPHET generates streamlines for fluid flow between injection and production wells, and

The model performs oil displacement and recovery calculations along the established streamlines. (A finite difference routine is used for oil displacement calculations.)

Appendix A discusses, in more detail, the *CO*<sub>2</sub>-*PROPHET* model and the calibration of this model with an industry standard reservoir simulator.

Even with these improvements, it is important to note the CO<sub>2</sub>-PROPHET is still primarily a "screening-type" model, and lacks some of the key features, such as gravity override and compositional changes to fluid phases, available in more sophisticated reservoir simulators.

5.6 ASSEMBLING THE COST MODEL. A detailed, up-to-date CO<sub>2</sub>-EOR Cost Model was developed by the study. The model includes costs for: (1) drilling new wells or reworking existing wells; (2) providing surface equipment for new wells; (3) installing the CO<sub>2</sub> recycle plant; (4) constructing a CO<sub>2</sub> spur-line from the main CO<sub>2</sub> trunkline to the oil field; and, (5) various miscellaneous costs.

The cost model also accounts for normal well operation and maintenance (O&M), for lifting costs of the produced fluids, and for costs of capturing, separating and reinjecting the produced CO<sub>2</sub>. A variety of CO<sub>2</sub> purchase and reinjection costs options are available to the model user. (Appendices B, C and D provide state-level details on the Cost Model for CO<sub>2</sub>-EOR prepared by this study.)

5.7 CONSTRUCTING AN ECONOMICS MODEL. The economic model used by the study is an industry standard cash flow model that can be run on either a pattern or a field-wide basis. The economic model accounts for royalties, severance and ad valorem taxes, as well as any oil gravity and market location discounts (or premiums) from the "marker" oil price. A variety of oil prices are available to the model user. Table 12 provides an example of the Economic Model for CO<sub>2</sub>-EOR used by the study.

5.8 PERFORMING SCENARIO ANALYSES. A series of analyses were prepared to better understand how differences in oil prices, CO<sub>2</sub> supply costs and financial risk hurdles could impact the volumes of oil that would be economically produced by CO<sub>2</sub>-EOR from the Illinois and Michigan Basin's major oil reservoirs.

- Two technology cases were examined. As discussed in more detail in Chapter 2, the study examined the application of two CO<sub>2</sub>-EOR options "Traditional Practices" and "State-of-the-art" Technology.
- Two oil prices were considered. A \$30 per barrel oil price was used to represent the moderate oil price case; a \$40 per barrel oil price was used to represent the availability of federal/state risk sharing and/or the continuation of the current high oil price situation.
- Two CO<sub>2</sub> supply costs were considered. The high CO<sub>2</sub> cost was set at 5% of the oil price (\$1.50 per Mcf at \$30 per barrel) to represent the costs of a new transportation system bringing natural CO<sub>2</sub> to the Illinois and Michigan Basin's oil basins. A lower CO<sub>2</sub> supply cost equal to 2% of the oil price (\$0.80 per Mcf at \$40 per barrel) was included to represent the potential future availability of low-cost CO<sub>2</sub> from industrial and power plants as part of CO<sub>2</sub> storage.
- Two minimum rate of return (ROR) hurdles were considered, a high ROR of 25%, before tax, and a lower 15% ROR, before tax. The high ROR hurdle incorporates a premium for the market, reservoir and technology risks inherent in using CO<sub>2</sub>-EOR in a new reservoir setting. The lower ROR hurdle represents application of CO<sub>2</sub>-EOR after the geologic and technical risks have been mitigated with a robust program of field pilots and demonstrations.

These various technology, oil price, CO<sub>2</sub> supply cost and rate of return hurdles were combined into four scenarios, as set forth below:

- The first scenario captures how CO<sub>2</sub>-EOR technology has been applied and has performed in the past. In this low technology, high risk scenario, called "Traditional Practices".
- The second scenario, entitled "State-of-the-art", assumes that the technology progress in CO<sub>2</sub>-EOR, achieved in the past ten years in other areas, is successfully applied to the oil reservoirs of the Illinois and Michigan Basin. In addition, this scenario assumes that a comprehensive program of research, pilot tests and field demonstrations will help lower the risk inherent in applying new technology to these Illinois and Michigan Basin oil reservoirs.
- The third scenario, entitled "Risk Mitigation," examines how the economic potential of CO<sub>2</sub>-EOR could be increased through a strategy involving state production tax reductions, federal tax credits, royalty relief and/or higher world oil prices that together would add an equivalent \$10 per barrel to the price that the producer uses for making capital investment decisions for CO<sub>2</sub>-EOR.
- The final scenario, entitled "Ample Supplies of CO<sub>2</sub>," low-cost, "EOR-ready" CO<sub>2</sub> supplies are aggregated from various industrial and natural sources. These include industrial high-concentration CO<sub>2</sub> emissions from hydrogen facilities, gas processing plants, chemical plants and other sources in the region. These would be augmented, in the longer-term, from concentrated CO<sub>2</sub> emissions from refineries and electric power plants. Capture of industrial CO<sub>2</sub> emissions could be part of a national effort for reducing greenhouse gas emissions.

Table 12. Economic Model Established by the Study

Pattern-Level Cashflow Model		Advanced													
State				New Injectors	ectors	0.39							_		
Field				Existing Injectors	ectors	0.00				2	•				
Formation			Conv	Converted Producers	ducers	0.61					,		L		
Depth				New Producers	ducers	0.0									
Distance from Trunkline (mi)			Ë	Existing Producers	ducers	1.34									
# of Patterns				Disposal Wells	Wells	0.00									
Miscibility:	Immiscible		_	_	-	_			+	_					
CO2 Injection (MMcf)	Year	0	-	285	2	3	285	2	285	285	7 242	190	9 190	100	11
H2O Injection (Mbw)			1,	143	143	143	143		143	143	164	190			
Di Drodintion (MAP)				ď	26	77	/6		ď	4	17	7			•
H2O Production (MBw)			2	246	224	176	164		169	160	156	168	184	190	188
CO2 Production (MMcf)			'		13	108	169		195	200	220	214			166
CO2 Purchased (MMcf)			0	285	272	177	116		06	85	22		18		
CO2 Recycled (MMcf)			'	2	13	108	169		195	200	220	190	172	169	166
Oil Brice (#Bhl)	\$		40 00	θ	0000	00 07	30.00	е	\$ 00 0V	00 07	00 07	00 0V \$	9	_	40.00
Oll Flice (4/65)	7			9 €	_			9 6		-			9 €	9 6	9 6
Gravity Adjustment	38	Deg	\$ 38.50	<b>₽</b>	_	_	r)	÷ €	_	$^+$	ñ	ñ	<u>ო</u> •	<u>ო</u> •	<del>ა</del>
Gross Revenues (\$M)	40 60			327 \$	9/8		916	A 6	_	\$ 109			<u>ب</u>	A 6	6 م
Royally (\$M)	-12.3%			_		_			_	_		(79) &	A 6	<del>0</del> 6	A 6
Severance Taxes (and)	%0.1- %0.0			_	A 4 (8)	(71)	(o) -	_	ભ <del>હ</del> ઉ	(c)		4 (4)	A 64	e e	
Net Revenue (\$M)	200		÷ +	283	\$47	1 147	707	÷ 4	310	200	557	430	417	080	374
Capital Costs (\$M)				_	+	+		+	_	_			<b>→</b>	•	•
New Well - D&C		\$ (138)													
Reworks - Producers to Producers		(61)													
Reworks - Producers to Injectors		\$ (16)													
Reworks - Injectors to Injectors															
CO2 Recycling Plant		(81)	¥	(384)		T	·	¥	4				e		·
Water Injection Plant		• •	9 4:		÷ +:			<del>)</del>	÷ ÷	•		· ·	· •	· ·	· ·
Trunkline Construction		(34)	_	<b>+</b>	•		<b>+</b>	<b>•</b>	<b>+</b>			<b>+</b>			
Total Capital Costs		\$ (268)	s	(384) \$	٠		- \$	<del>s</del>	<del>\$</del>	٠		ج	ج	ج	ا ج
Cap Ex G&A	%0	· •	\$	€	٠		۰ چ	<del>ss</del>	φ.	'	,	ج	-	ج	ج
CO2 Costs (\$M)			6	6 (000)	(000)	(405)	(464)	6	450	4 40)	(405)	6	(co)	Φ (	φ
O&M Costs					(522)	_		9					Ð	9	0
Operating & Maintenance (\$M)			\$	\$ (09)	(09)	(09)	(09)	\$	\$ (09)	(09)	(09)	(09)	(09) \$ (0	(09) \$ (	(99)
iffing Costs (\$/bbl)	\$ 0.25		<del>\$</del>	(64)	\$ (69)	(53)	(47)	\$	(44)	(44)	(43)	(42)	(67) \$ (13)	(50)	(20)
G&A					_	(23)		_					+	•	
Total O&M Costs			\$	(148) \$	(147) \$	-	\$ (128)	s	(125) \$	-	\$ (123)	\$ (126)	\$	\$	\$ (132)
( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )			€			oc o		+	$\vdash$	$\vdash$			€	€	€
Net Cash Flow (\$M)		997)	<del>∧</del> €	9 6	φ (ξ	828	200	<del>م</del> د	-		328	228	Ð	A 6	<b>₽</b> €
Cum. Cash Flow	260/		Ð	(745)	\$ (797)	261	1,066	Ð	1,101	1,349	1,6//	4 1,905			_
Disc Net Cash Flow	22		<del>U</del> .			٠.	207	υ.	12 5	+			€.	<b>€</b>	
Disc. Cum Cash Flow		\$ (268)	₩	(649)	(343) \$	-	\$ 287	8	_	364 \$	7	\$ 471	\$	\$ 505	\$
NPV (BTx)	25%														
NPV (BIX)	20%	\$ 720													
NPV (BTX)	10%														
IRR (BTx)		53.27%	9	L				L		F			L	L	
				-					-						

Table 12. Economic Model Established by the Study (cont'd)

throng			-	-						-								
Distance from Trumbline (mi)			+															
# of Patterns			+	+														
Miscibility:	Immiscible																	
•	Year	12		13	14	15	16	17		18	19	20	21	22		23	24	25
CO2 Injection (MMcf)		1	190	190	190	190	190		69							-		•
H2O Injection (Mbw)		-	190	190	190	190			251	285	285	285	285		285	285	285	285
Oil Production (Mbbl)			10	9	4	3	4		2	7	6	11	11		6	80	8	
H2O Production (MBw)		-	189	192	193	194			201	221	247	255	262		266	270	271	272
CO2 Production (MMcf)		7	89	169	172	174	173		181	146	74	46	30		24	19	14	13
CO2 Purchased (MMcf)			22	21	18	16	17							ľ			-	ľ
CO2 Recycled (MMcf)		1	168	169	172	174	. 173		69	•								
Oil Price (\$/Bbl)	\$ 40.00	\$ 40.00	s	40.00	40.00	\$ 40.00	\$ 40.00	S	40.00	40.00	40.00	3 40.00	\$ 40.00	\$ 40.00	s	40.00	40.00	\$ 40.00
Gravity Adjustment		s	s	38.50 \$	38.50		s	s	မှ	_	38.50 \$	38.50	s	s	s	38.50 \$		
Gross Revenues (\$M)					139		s	s	204 \$				\$	ક	350 \$			
Royalty (\$M)	-12.5%	<u>`</u>	(46)		(17)	_	) \$	) \$	(26)	(32)	(43) \$	(54)	s ·	φ,	(44)			(36)
Severance Taxes (\$M)	-1.0%		<u>@</u>	(2)	(1)			<del>⇔</del> €	(2)	(2)	(3)	(4)	s e	φ.	(3)	(9)	(3)	(3)
Ad Valorum (\$M)	%0.0		-	_			<del>∞</del> •	÷ €	-	+	+			<del>.,</del>	_	$\boldsymbol{+}$		
Net Revenue(\$M)		e S	31/	200	120	100	13/	Ð	\$ //[	\$ 077	767	3//	\$ 3/4	Ð	303	\$ 197	270	197. \$
Capital Costs (am)			+	$\dagger$	ĺ				1	-								
Reworks - Producers to Producers			+	$\dagger$					+	$\frac{1}{1}$	$\dagger$				+			
Reworks - Producers to Injectors			-	ŀ	İ				-	-								
Reworks - Injectors to Injectors			-															
Surface Equipment (new wells only)																		
CO2 Recycling Plant		*	\$	-	-	- \$	*	*			-	- \$	*	*	\$	-	-	*
Water Injection Plant		\$	↔	<del>\$</del>		ج	- ج	• •	<del>∽</del>	<del>⇔</del> '	'	- \$	· \$	٠ <del>\$</del>	↔	٠		· \$
Trunkline Construction		,	,	,		,		,	,				,	,	,	,		,
Total Capital Costs	/00	ω .									T							
Cap Ex G&A	%0	· •	₽	,		٠	· •	٠	<del>.</del>	<del>ب</del>	'	٠	·	· •	₽	<del>ب</del>		٠
CO2 Costs (\$M)		4	\$ (82)	(85)	(83)	(82)	(83)	¥	\$ (20)	4		,	<del>U</del>	e e	¥	<i>₩</i>		· •
O&M Costs				_			•	<del>)</del>		→	T			•	•	•		
Operating & Maintenance (\$M)		\$	\$ (09)	(09)	(09)	(09)	(09) \$ (0	€	\$ (09)	\$ (09)	\$ (09)	(09)	(09)	<del>s</del>	\$ (09)	\$ (09)	(09)	(09)
Lifting Costs (\$/bbl)	\$ 0.25	s	\$ (09)	(20)	(49)	(49)	(49)	s	(52)	(24)	(64)	(29)	(89)	€	\$ (69)	\$ (69)	(76)	(92)
G&A					(22)					_								
Total O&M Costs		\$	(131) \$	(131) \$	(131)	\$ (131)	) \$ (131)	s	(134) \$	(140) \$	(149) 8	\$ (152)	\$ (154)	<del>69</del>	(154) \$	(155) \$	(163)	\$ (163)
Net Cash Flow (\$M)		\$	101	(16)	(44)	(113)		<del>U</del> .	16	& .	148	225	\$ 220	<del>U</del> .	149	112	107	104
Cum. Cash Flow		7	မ	2,414   \$	2,320	\$ 2,207	8	S	မ	+	_	2,599	8	\$	S	+	(5)	3
Discount Factor	25%	1			0.04					-		0.01			-	0.01	0.00	
Disc. Net Cash Flow			2	(1) \$	4	\$ (4)	<del>S</del>	\$			2 \$	3		\$		1		
Disc. Cum Cash Flow		\$	525 \$	524 \$	520			છ	514 \$	516 \$	518	\$ 521	\$ 523	s	524 \$	524 \$	525	\$ 525
NPV (BTv)	25%																	
(XLQ) (XLQ)	20.00																	
NPV (BTx)	15%		+	ŀ											-			
NPV (BTx)	10%		+	t	ĺ				1		T							
INFV (BIX)	0/01	$\downarrow$	+	$\dagger$	T		$\downarrow$	$\downarrow$	+	$\frac{1}{1}$	$\dagger$			$\downarrow$	-			
(יים) עעו			$\left  \right $						$\left  \right $						1	1		

Table 12. Economic Model Established by the Study (cont'd)

Depth															
Distance from Trunkline (mi)															
# of Patterns															
Miscibility:	Immiscible														
	Year	26	27	28	29	6	30	31	32	٥.	33	34	35	(,)	36
CO2 Injection (MMcf)					-								•		
H2O Injection (Mbw)		282	285		285	285	75								
Oil Production (Mbbl)		7	7		9	9	-								
H2O Production (MBw)		274	275		276	277	73								
CO2 Production (MMcf)		10			7	7	2						'		
CO2 Purchased (MMcf)				'											
CO2 Recycled (MMcf)															
Oil Drice (#G/Bhl)	30.00	40.00	40.00	00 00 \$	ь	\$ 0007	40.00	¥	θ	θ	1	θ	Ð	θ	
Gravity Adjustment		€.	÷ 4.	÷ 4:	→ 4:	_	+	(1.50)	÷ 65	(0)	(1.50)	2	÷ 4:	÷ 4:	(1.50)
Gross Revenues (\$M)	3	69	69	6	6	223 \$	-	· · ·	69			- 8	6	69	- (200)
Royalty (\$M)	-12.5%		· <del>S</del>	8	+-	+		. 8		· <del>\$</del>		ج	· &	s	
Severance Taxes (\$M)	-1.0%		s	မှ	_		-			r				မှ	
Ad Valorum (\$M)	%0.0	· •	\$	\$		φ.	-			<b>↔</b>		ج		ક	
Net Revenue(\$M)		\$ 230		\$	210 \$	193 \$	47	- \$	s	·		\$	\$	s	
Capital Costs (\$M)															
New Well - D&C															
Reworks - Producers to Producers															
Reworks - Producers to Injectors															
Reworks - Injectors to Injectors															
CO2 Recycling Plant			4	· &	¥				ь				·	ч	
Water Injection Plant			•	·	9				·				·	6	,
Trunkline Construction					•				•	t				•	
Total Capital Costs		5	ج	ج	s	٠		\$	s			&	\$	s	
Cap Ex G&A	%0	s	ا ج	5	69				မှ	9		چ	ا ج	69	
CO2 Costs (\$M)															
Total CO2 Cost (\$M)		ج	ج	ج	ક	<del>د</del>			ક	<del>د</del>		چ	ج	ક	
O&M Costs			,	,	_	_			,	•		,	,	,	
Operating & Maintenance (\$M)		(09)	(09)	မှ	\$ (09)	(09)	(09)	ج	s	<del>د</del>		ج	٠ ج	မှ	
Lifting Costs (\$/bbl)	\$ 0.25	\$ (75)	\$ (75)	s	(75)	(75)	(20)	9	s	9		· •	9	s	
G&A	70%					(27)	(16)						•		
Total O&M Costs		\$ (162)	\$ (162)	(162)	s	(162) \$	(36)		છ	<b>⇔</b> -		&	۰ ج	9	
Net Cash Flow (\$M)		€ €	÷	G	48	32	(49)	G	e e			<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>		G	
Cum. Cash Flow		\$ 3.358	\$ 3.4	\$ 3.4	8	3.493 \$		\$ 3.444	69	3.444	3.444	\$ 3.444	3.444	6	3.444
Discount Factor	72%		٠	٠		+	0.00			-	0.00		٠		0.00
Disc. Net Cash Flow			0	ક	ક્ક	-			s	-			မ	မ	
Disc. Cum Cash Flow		\$ 526	52	s	526 \$	526 \$	526	\$ 526	s	526 \$	526	\$ 526	s	526 \$	526
A. T. C. Marie	200														
NPV (BTx)	25%														
NPV (BIX)	20%														
NPV (BIX)	10%						l								
NPV (BIX)	0/01			1	+	$\dagger$	T		1	$\dagger$	T			1	
ואו פן אחו														_	

### 6. RESULTS BY STATE

*6.1 ILLINOIS*. Illinois is a major oil producing state with a rich history of oil and gas development. Crude oil production began in 1904, and has reached a cumulative recovery of 3.6 billion barrels through 2004. In 2004, Illinois ranked 14<sup>th</sup> in oil production in the onshore U.S., providing 9.1 MMBbls of oil (25 MBbls/day). It has about 16,737 producing oil wells and oil reserves of 92 MMBbls. Illinois has seen a steady drop in production in recent years, (Table 13).

Table 13. Recent History of Illinois Oil Production

	Annual Oi	l Production
	(MMBbls/year)	(MBbls/day)
2000	10.8	30
2001	10.4	28
2002	10.9	30
2003	9.1	25
2004	9.1	25

*Illinois Oil Fields*. To better understand the potential of using CO<sub>2</sub>-EOR in Illinois's light oil fields, this section examines, in more depth, five large oil fields, shown in Figure 11.

- Clay City Consolidated (McCloskey Reservoir)
- Salem Consolidated (Devonian Reservoir)
- Johnsonville Consolidated (McCloskey Reservoir)
- New Harmony Consolidated (Bethel Reservoir)
- Sailor Springs (Cypress Reservoir)

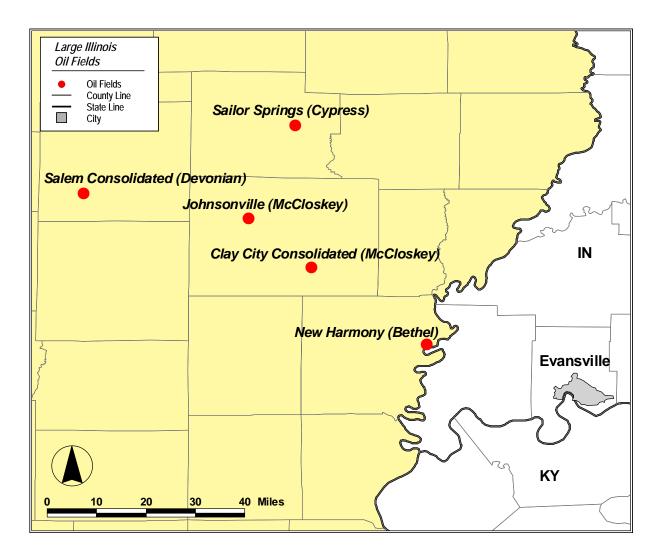


Figure 11. Large Illinois Oil Fields

These five fields, distributed across Illinois, could serve as the "anchor" sites for CO<sub>2</sub>-EOR projects in the state that could later be extended to other fields. The cumulative oil production, proved reserves and remaining oil in place (ROIP) for these 5 large light oil fields are set forth in Table 14.

Table 14. Status of Large Oil Illinois Fields/Reservoirs (as of 2000)

		Original Oil In-Place	Cumulative Production	Proved Reserves	Remaining Oil In-Place
	Large Fields/Reservoirs	(MMBbls)	(MMBbls)	(MMBbls)	(MMBbls)
1	Clay City Consolidated (McCloskey)	404	116	4	284
2	Salem Consolidated (Devonian)	174	75	1	98
3	Johnsonville Consolidated (Mccloskey)	89	36	1	52
4	New Harmony Consolidated (Behel)	105	41	1	63
5	Sailor Springs (Cypress)	92	31	1	60

These five large "anchor" fields, each with over 60 million barrels of ROIP, may be favorable for miscible or immiscible CO<sub>2</sub>-EOR, based on their reservoir properties, Table 15. Illinois Basin fields often produce from several reservoirs at varying depths. Deeper reservoirs in the Salem Consolidated, Johnsonville Consolidated, and Clay City Consolidated fields screen miscible, while the shallower reservoirs in the Salem Consolidated and Clay City Consolidated, as well as all of the New Harmony and Sailor Springs reservoirs screen immiscible

Table 15. Reservoir Properties and Improved Oil Recovery Activity, Large Illinois Oil Fields/Reservoirs

	Large Fields/Reservoirs	Depth (ft)	Oil Gravity (°API)	Active Waterflood or Gas Injection
	Clay City Consolidated			
1	(McCloskey)	3,050	39.0	Undergoing Waterflood
2	Salem Consolidated (Devonian)	3,440	40.0	Undergoing Waterflood
	Johnsonville Consolidated			
3	(McCloskey)	3,170	38.0	Undergoing Waterflood
	New Harmony Consolidated			
4	(Behel)	2,700	37.0	Undergoing Waterflood
5	Sailor Springs (Cypress)	2,550	37.2	Undergoing Waterflood

Past CO<sub>2</sub>-EOR Projects. Illinois oil producers have had limited experiences with CO<sub>2</sub> injection. A small pilot was initiated in the Forsyth field, utilizing CO<sub>2</sub> from the Archer-Daniels-Midland Ethanol Processing Facility in Decatur, IL and results from this project have been published. In the early 1990s, a single-well "huff-and-puff" CO<sub>2</sub> pilot project began in the Mattoon field. The well was drilled to a depth of 1,800 feet in the Cypress reservoir, and CO<sub>2</sub> was again supplied from ADM's ethanol plant in Decatur, IL. After several months of operation, the pilot was shutdown due to high CO<sub>2</sub> costs compared to the oil recovery rate. Currently, there is considerable work underway by the Illinois Geological Survey on locating and characterizing reservoirs suitable for CO<sub>2</sub>-EOR.

Future CO<sub>2</sub>-EOR Potential. Illinois contains 16 reservoirs that are candidates for miscible CO<sub>2</sub>-EOR and 30 reservoirs that are candidates for immiscible CO<sub>2</sub>-EOR. Under "Traditional Practices" (and Base Case financial conditions, defined above), however, none of these fields are economically attractive for miscible CO<sub>2</sub> flooding. Applying "State-of-the-art Technology" (involving higher volume CO<sub>2</sub> injection) and establishing lower risk financial conditions, the number of economically favorable for CO<sub>2</sub>-EOR oil reservoirs in Illinois is 23, providing 380 million barrels of additional oil recovery, Table 16.

Table 16. Economic Oil Recovery Potential Under Two Technologic Conditions, Illinois

	No. of	Original Oil In-Place	Technical Potential	Economic Pote	ential*
CO₂-EOR Technology	Reservoirs Studied	(MMBbls)	(MMBbls)	(No. of Reservoirs)	(MMBbls)
"Traditional Practices"	16	1,357	133	0	0
"State-of-the-art" Technology	46	3,115	494	23	380

<sup>\*</sup> Oil price of \$30 per barrel; CO<sub>2</sub> costs of \$1.50/Mcf.

Combining "State-of-the-art" technologies with risk mitigation incentives and/or higher oil prices and lower cost CO<sub>2</sub> supplies would enable CO<sub>2</sub>-EOR in Illinois to recover 460 million barrels of CO<sub>2</sub>-EOR oil from 37 major reservoirs, Table 17.

Table 17. Economic Oil Recovery Potential with More Favorable Financial Conditions, Illinois

	Technical Potential	Economic Po	tential
More Favorable Financial Conditions	(MMBbls)	(No. of Reservoirs)	(MMBbls)
Plus: Risk Mitigation Incentives*	494	36	450
Plus: Low Cost CO <sub>2</sub> Supplies**	494	37	460

<sup>\*</sup> Oil price of \$40 per barrel, adjusted for gravity and location differentials; CO<sub>2</sub> supply costs, \$2/Mcf

6.2 INDIANA AND KENTUCKY. Indiana is the 23<sup>rd</sup> largest onshore oil producing state. Crude oil production in the state began in the 1883, reaching a cumulative recovery of 550 million barrels through 2004. In 2004, the state's production was 1.9 MMBbls (5.2 MBbls/day). Indiana has about 5,000 producing oil wells and oil reserves of 11 MMBbls. Indiana oil production has been low, but steady in resent years, Table 18.

Table 18. Recent History of Indiana Oil Production

	Annual Oil I	Production
	(MMBbls/year)	(MBbls/day)
2000	2.0	5
2001	2.0	5
2002	2.0	5
2003	1.9	5
2004	1.9	5

Kentucky is the 20<sup>th</sup> largest onshore oil producing state and produced 2.5 MMBbls (7 MBbls/day) of oil (in 2004), from about 18,000 producing wells and 27 MMBbls of crude oil reserves. Oil production began in 1883 in Kentucky and cumulative

<sup>\*\*</sup> CO<sub>2</sub> supply costs, \$0.80/Mcf

production has reached 780 MMBbls. The state's oil production has been in slight decline in recent years, Table 19.

Table 19. Recent History of Kentucky Oil Production

	Annual Oil I	Production
	(MMBbls/year)	(MBbls/day)
2000	2.9	8
2001	2.8	8
2002	2.7	7
2003	2.5	7
2004	2.5	7

Indiana and Kentucky Oil Fields. The light oil fields of the Illinois Basin of Indiana and Kentucky are too shallow for miscible CO<sub>2</sub>-EOR, making them amenable to immiscible CO<sub>2</sub>-EOR. To better understand the potential of using CO<sub>2</sub>-EOR in Indiana and Kentucky's light oil fields, this section examines, in more depth, two large oil fields, shown in Figure 12.

- Griffin Consolidated Field, IN (Reservoirs >2,000 feet)
- Poole Consolidated Field, KY (Reservoirs >2,000 feet)

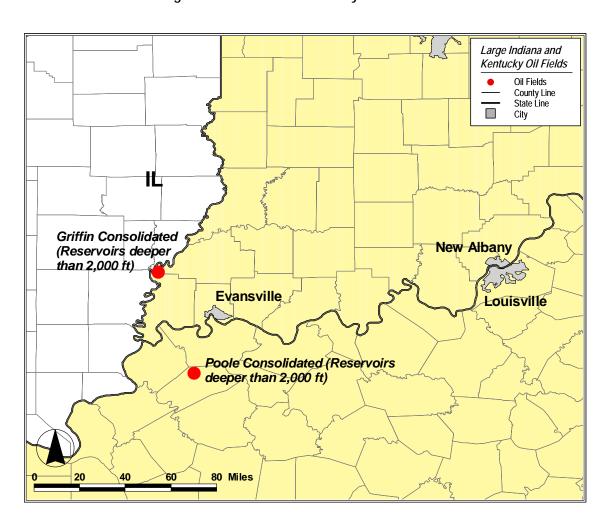


Figure 12. Illinois and Kentucky Anchor Fields

These major oil fields could serve as anchor sites for CO<sub>2</sub> projects that could later extend to small fields in the states. The cumulative oil production, proved reserves and remaining oil in-place (ROIP) for the oil reservoirs in this field are set forth in Table 20.

Table 20. Status of Large Indiana and Kentucky Oil Fields/Reservoirs (as of 2002)

		Original Oil In-Place	Cumulative Production	Proved Reserves	Remaining Oil In-Place
	Large Fields/Reservoirs	(MMBbls)	(MMBbls)	(MMBbls)	(MMBbls)
1	Griffin Consolidated (All>2,000 Feet*)	236	84	2	150
2	Poole Consolidated (All>2,000 Feet**)	70	27	2	41

<sup>\*</sup>including Waltersburg, Tar Springs, Paoli, Cypress, Bethel, and Ste. Genevieve reservoirs.

These large oil fields each contain several individual light oil reservoirs amenable to immiscible CO<sub>2</sub>-EOR due to their shallow depth. Table 21 provides the reservoir and oil properties these fields and their current secondary oil recovery activities.

Table 21. Reservoir Properties and Improved Oil Recovery Activity, Large Indiana Oil Fields/Reservoirs

	Large Fields/Reservoirs	Depth (ft)	Oil Gravity (°API)	Active Waterflood or Gas Injection
1	Griffin Consolidated (All >2,000 Feet)	2,050-2,850	38	Undergoing Waterflood
2	Poole Consolidated (>2,000 Feet	2,030-2,560	36	Undergoing Waterflood

<sup>\*</sup>including Waltersburg, Tar Springs, Paoli, Cypress, Bethel, and Ste. Genevieve reservoirs.

**Past and Current CO<sub>2</sub>-EOR Projects.** To date, there have been no CO<sub>2</sub>-EOR projects in Indiana or Kentucky. However, due to the similarity in reservoir characteristics to those in Illinois, projects in that state may serve as a guide for Indiana/Kentucky EOR projects.

<sup>\*\*</sup> including Ste. Genevieve and Chester s.s. reservoirs

<sup>\*\*</sup> including Ste. Genevieve and Chester s.s. reservoirs

Future CO2-EOR Potential. Indiana and Kentucky contains no oil reservoirs that are candidates for miscible CO<sub>2</sub>-EOR due to their shallow depths. Therefore, there is no potential for applying "Traditional Practices" EOR in these states. However, when applying "State-of-the-art Technology" (involving higher volume CO<sub>2</sub> injection, immiscible EOR, and lower risk), 15 immiscible EOR oil reservoirs become technically feasible and 8 reservoirs are economically feasible, Table 22.

Table 22. Economic Oil Recovery Potential Under Two Technologic Conditions, Indiana and Kentucky

	No. of	Original Oil In- Place	Technical Potential		nomic ential*
CO <sub>2</sub> -EOR Technology	Reservoirs Studied	(MMBbls)	(MMBbls)	(No. of Reservoirs)	(MMBbls)
"Traditional Practices"	0	0	0	0	0
"State-of-the-art" Technology	15	446	86	8	40

<sup>\*</sup> Oil price of \$30 per barrel; CO<sub>2</sub> costs of \$1.50/Mcf.

Combining "State-of-the-art" technology with risk mitigation incentives and/or higher oil prices plus lower cost CO<sub>2</sub> supplies, would enable an additional 80 million barrels of CO<sub>2</sub>-EOR Indiana and Kentucky from 5 major oil reservoirs, Table 23.

Table 23. Economic Oil Recovery Potential with More Favorable Financial Conditions, Indiana and Kentucky

	Technical Potential	Economic Potential		
More Favorable Financial Conditions	(MMBbls)	(No. of Reservoirs)	(MMBbls)	
Plus: Risk Mitigation Incentives*	86	10	60	
Plus: Low Cost CO <sub>2</sub> Supplies**	86	13	80	

<sup>\*</sup> Oil price of \$40 per barrel, adjusted for gravity and location differentials; CO2 supply costs, \$2/Mcfs

6.3 MICHIGAN. Michigan is the 17<sup>th</sup> largest domestic oil producing state,
 providing 5 MMBbls (14 MBbls/day) of oil in 2004, from almost 4,000 producing wells.
 Oil production in the state of Michigan began in 1925. Cumulative oil recovery in the

<sup>\*\*</sup> CO<sub>2</sub> supply costs, \$0.80/Mcf

state is 1.25 billion barrels with 53 million barrels of reserves. In recent years, oil production in Michigan has been in decline, Table 24.

Table 24. Recent History of Michigan Oil Production

	Annual Oil	Annual Oil Production			
	(MMBbls/year)	(MBbls/day)			
1999	8.6	24			
2000	8.4	23			
2001	8.1	22			
2002	7.5	21			
2003	6.7	18			
2004	5.0	14			

**Michigan Fields**. Michigan contains 8 large oil fields that may be amenable to miscible CO<sub>2</sub>-EOR, Figure 13. To better understand the potential of using CO<sub>2</sub>-EOR in Michigan's light oil fields, this section examines, in more depth, the state's largest miscible EOR field:

Albion/Scipio Field (Trenton-Black River Reservoir)

Large Michigan Oil Fields
Oil Fields
County Line
State Line
City

Cly

Albion-Scipio (Trenton-Black River)

0 10 20 30 40 Miles

Figure 13. Albion/Scipio Oil Field, Michigan

The cumulative oil production, proved reserves and remaining oil in-place (ROIP) in this large oil reservoir are provided in Table 25.

Table 25. Status of Large Michigan Oil Fields/Reservoirs (as of 2003)

Fields/Reservoirs	Original Oil	Cumulative	Proved	Remaining
	In-Place	Production	Reserves	Oil In-Place
	(MMBbls)	(MMBbls)	(MMBbls)	(MMBbls)
Albion/Scipio (Trenton-Black River)	312	125	low	187

This large oil reservoir, with over 180 million barrels of ROIP, is technically amenable for miscible CO<sub>2</sub>-EOR. Table 26 provides the reservoir and oil properties for these reservoirs and their current oil recovery activities.

Table 26. Reservoir Properties and Improved Oil Recovery Activity, Large Michigan Oil Fields/Reservoirs

Fields/Reservoir	Depth	Oil Gravity	Active Waterflood or
	(ft)	(°API)	Gas Injection
Albion/Scipio (Trenton-Black River)	3,900	41.3	none

Past and Current CO<sub>2</sub>-EOR Projects. Two small miscible CO<sub>2</sub>-EOR floods have been ongoing in Michigan for the past 10 years using CO<sub>2</sub> from an Antrim shale gas processing plant. In 1996, Core Energy, LLC, began CO<sub>2</sub> miscible flood projects on two Niagran pinnacle reef field reservoirs at 5200 feet depth, Dover 33 and Dover 36, with OOIP's of 4.1 and 3.7 MMBbls, respectively. Dover 36 is expected to ultimately produce an estimated 31% of its OOIP through primary production. Injection of 5.4 Bcf of CO<sub>2</sub> has increased production by an additional 5% of the field OOIP. Dover 33 is expected to perform better, with primary production netting 33% of the OOIP. CO<sub>2</sub> EOR is expected to produce an additional 18% OOIP after 21 Bcf of CO<sub>2</sub> injection. The field operator attributes the low recovery efficiency at Dover 36 to the highly heterogeneous nature of the reservoir. The more optimized well patterns for CO<sub>2</sub> injection in Dover 33 account for the higher expected recovery efficiency.

A third CO<sub>2</sub> EOR project is being conducted by a joint venture between Michigan Technical University, Western Michigan University and Jordan Development Company, LLC on the Dover 35 field. This Niagran pinnacle reef field is similar in size and reservoir characteristics to the Dover 33 and 36 fields. CO<sub>2</sub> injection began in 2004 and the operators expect to produce an additional 10-25% of the field's 2.2 MMBbls of OOIP in addition to an expected ultimate primary recovery of 44% OOIP.

Future CO2-EOR Potential. Michigan contains 11 large oil reservoirs that are candidates for miscible or immiscible CO<sub>2</sub>-EOR technology. The potential for economically developing these oil reservoirs is examined first under Base Case financial criteria that combine an oil price of \$30 per barrel, CO<sub>2</sub> supply costs (\$1.50/Mcf), and a high risk rate of return (ROR) hurdle (25% before tax).

Under "Traditional Practices" (involving a small volume of high cost CO<sub>2</sub> injection and high risk financial conditions), miscible CO<sub>2</sub> flooding would not be economically attractive in the large Michigan oil fields. Applying "State-of-the-art Technology" (involving higher volume CO<sub>2</sub> injection, immiscible EOR, and lower risk), one large oil reservoir in Michigan becomes economically feasible, providing 80 million barrels of additional oil recovery, Table 27.

Table 27. Economic Oil Recovery Potential Under Two Technologic Conditions, Michigan

		Original Oil In-Place	Technical Potential	Economic Potential*	
	No. of			(No. of	
CO <sub>2</sub> -EOR Technology	Reservoirs	(MMBbls)	(MMBbls)	Reservoirs)	(MMBbls)
"Traditional Practices"	8	793	94	0	0
"State-of-the-art" Technology	11	971	230	1	80

<sup>\*</sup> Oil price of \$30 per barrel.

Combining "State-of-the-art" technologies with risk mitigation incentives and/or higher oil prices plus lower cost CO<sub>2</sub> supplies does not enable any additional large oil fields in Michigan to become economic, Table 28.

Table 28. Economic Oil Recovery Potential with More Favorable Financial Conditions, Michigan

	Technical Potential	Economic Potential		
More Favorable Conditions	(MMBbls)	(No. of Reservoirs)	(MMBbls)	
Plus: Risk Mitigation*	230	1	80	
Plus: Low Cost CO <sub>2</sub> **	230	1	80	

<sup>\*</sup>Oil price of \$40 per barrel, adjusted for gravity differential; CO2 supply costs, \$2/Mcf

<sup>\*\*</sup> CO<sub>2</sub> supply costs, to \$0.80/Mcf

## Appendix A

Using *CO<sub>2</sub>-PROPHET* for Estimating Oil Recovery

#### **Model Development**

The study utilized the *CO*<sub>2</sub>-*PROPHET* model to calculate the incremental oil produced by CO<sub>2</sub>-EOR from the large Illinois and Michigan Basin oil reservoirs. *CO*<sub>2</sub>-*PROPHET* was developed by the Texaco Exploration and Production Technology Department (EPTD) as part of the DOE Class I cost share program. The specific project was "Post Waterflood CO<sub>2</sub> Flood in a Light Oil, Fluvial Dominated Deltaic Reservoir" (DOE Contract No. DE-FC22-93BC14960). *CO*<sub>2</sub>-*PROPHET* was developed as an alternative to the DOE's CO<sub>2</sub> miscible flood predictive model, *CO*<sub>2</sub>*PM*.

### **Input Data Requirements**

The input reservoir data for operating  $CO_2$ -PROPHET are from the Major Oil Reservoirs Data Base. Default values exist for input fields lacking data. Key reservoir properties that directly influence oil recovery are:

- Residual oil saturation,
- Dykstra-Parsons coefficient,
- Oil and water viscosity,
- Reservoir pressure and temperature, and
- Minimum miscibility pressure.

A set of three relative permeability curves for water, CO<sub>2</sub> and oil are provided (or can be modified) to ensure proper operation of the model.

## Calibrating CO<sub>2</sub>-PROPHET

The  $CO_2$ -PROPHET model was calibrated by Advanced Resources with an industry standard reservoir simulator, GEM. The primary reason for the calibration was to determine the impact on oil recovery of alternative permeability distributions within a multi-layer reservoir. A second reason was to better understand how the absence of a gravity override function in  $CO_2$ -PROPHET might influence the calculation of oil recovery.  $CO_2$ -PROPHET assumes a fining upward permeability structure.

The California San Joaquin Basin's Elk Hills (Stevens) reservoir data set was used for the calibration. The model was run in the miscible CO<sub>2</sub>-EOR model using one hydrocarbon pore volume of CO<sub>2</sub> injection.

The initial comparison of  $CO_2$ -PROPHET with GEM was with fining upward and coarsening upward (opposite of fining upward) permeability cases in GEM. All other reservoir, fluid and operational specifications were kept the same. As Figure A-1 depicts, the  $CO_2$ -PROPHET output is bounded by the two GEM reservoir simulation cases of alternative reservoir permeability structures in an oil reservoir.

A second comparison of  $CO_2$ -PROPHET and GEM was for randomized permeability (within the reservoir modeled with multiple layers). The two GEM cases are High Random, where the highest permeability value is at the top of the reservoir, and Low Random, where the lowest permeability is at the top of the reservoir. The permeability values for the other reservoir layers are randomly distributed among the remaining layers. As Figure A-2 shows, the  $CO_2$ -PROPHET results are within the envelope of the two GEM reservoir simulation cases of random reservoir permeability structures in an oil reservoir.

Based on the calibration, the  $CO_2$ -PROPHET model seems to internally compensate for the lack of a gravity override feature and appears to provide an average calculation of oil recovery, neither overly pessimistic nor overly optimistic. As such,  $CO_2$ -PROPHET seems well suited for what it was designed — providing project scoping and preliminary results to be verified with more advanced evaluation and simulation models.

## Comparison of CO2-PROPHET and CO2PM

According to the  $CO_2$ -PROPHET developers, the model performs two main operations that provide a more robust calculation of oil recovery than available from  $CO_2PM$ :

Figure A-1. *CO2-PROPHET* and *GEM*: Comparison to Upward Fining and Coarsening Permeability Cases of *GEM* 

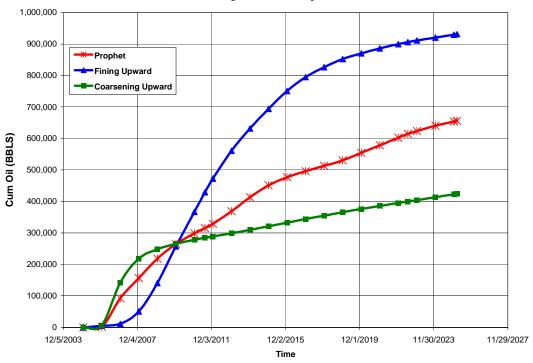
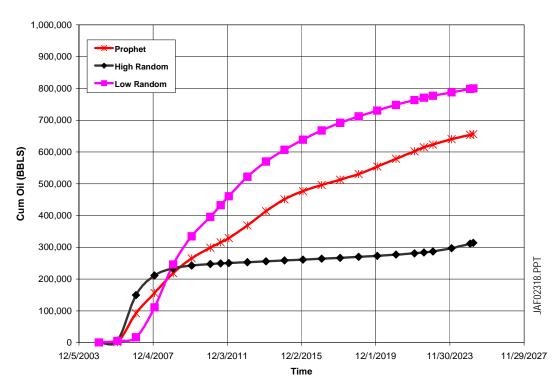


Figure A-2. CO<sub>2</sub>-PROPHET and GEM: Comparison to Random Permeability Cases of GEM



- CO<sub>2</sub>-PROPHET generates streamlines for fluid flow between injection and production wells, and
- The model then performs oil displacement and recovery calculations along the streamlines. (A finite difference routine is used for the oil displacement calculations.)

Other key features of  $CO_2$ -PROPHET and its comparison with the technical capability of  $CO_2$ PM are also set forth below:

- Areal sweep efficiency in  $CO_2$ -PROPHET is handled by incorporating streamlines that are a function of well spacing, mobility ratio and reservoir heterogeneity, thus eliminating the need for using empirical correlations, as incorporated into  $CO_2PM$ .
- Mixing parameters, as defined by Todd and Longstaff, are used in CO<sub>2</sub>-PROPHET for simulation of the miscible CO<sub>2</sub> process, particularly CO<sub>2</sub>/oil mixing and the viscous fingering of CO<sub>2</sub>.
- A series of reservoir patterns, including 5 spot, line drive, and inverted 9 spot, among others, are available in  $CO_2$ -PROPHET, expanding on the 5 spot only reservoir pattern option available in  $CO_2$ PM.
- CO<sub>2</sub>-PROPHET can simulate a variety of recovery processes, including continuous miscible CO<sub>2</sub>, WAG miscible CO<sub>2</sub> and immiscible CO<sub>2</sub>, as well as waterflooding. CO<sub>2</sub>PM is limited to miscible CO<sub>2</sub>.

# Appendix B

Illinois CO<sub>2</sub>-EOR Cost Model

## Cost Model for CO<sub>2</sub>-Based Enhanced Oil Recovery (CO<sub>2</sub>-EOR)

This appendix provides documentation for the cost module of the desktop CO<sub>2</sub>-EOR policy and analytical model (COTWO) developed by Advanced Resources for DOE/FE-HQ. The sections of this cost documentation report are organized according to the normal sequence of estimating the capital and operating expenditures for a CO<sub>2</sub>-EOR project:

1. Well Drilling and Completion Costs. The costs for well drilling and completion (D&C) are based on the 2003 JAS cost study recently published by API for Illinois.

The well D&C cost equation has a fixed cost constant for site preparation and other fixed cost items and a variable cost equation that increases with depth. The total equation is:

Well D&C Costs =  $a_0 e^{a_1D}$ Where:  $a_0$  is 83085  $a_1$  is 0.00052 D is well depth

Figure B-1 provides the details for the cost equation and illustrates the "goodness of fit" for the well D&C cost equation for Illinois.

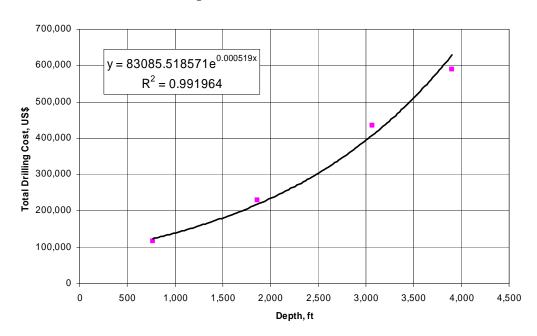


Figure B-1. Oil Well D&C Costs for Illinois

In order to bring the 2003 API drilling costs (the most recent available) into 2004 numbers where increased oil prices are expected to result in significantly increased drilling costs, a relationship was established between average drilling costs and average annual oil prices. Drillings costs from the ten year period of 1994-2003 (API data) were plotted versus the three year weighted average annual oil prices for those years (EIA Annual Energy Review, 2004) and the following relationship was established:

Drilling costs (per foot) = \$5.04(annual oil price) – \$3.2116.

Applying the 2004 average oil price of \$36.77 gives a drilling cost of \$182 per foot and an increase of 25.6% over the 2003 cost of \$145 per foot. Therefore, drilling and completion costs were increased by 25% over the Illinois D&C cost calculations to reflect this increase in 2004 drilling costs.

2. <u>Lease Equipment Costs for New Producing Wells.</u> The costs for equipping a new oil production well are based on data reported by the EIA in their 2004 "Cost and Indices for Domestic Oil and Gas Field Equipment and Production Operations" report. This survey provides estimated lease equipment costs for 10 wells producing with artificial lift, from depths ranging from 2,000 to 12,000 feet, into a central tank battery.

The equation contains a fixed cost constant for common cost items, such as free water knock-out, water disposal and electrification, and a variable cost component to capture depth-related costs such as for pumping equipment. The total equation is:

Production Well Equipping Costs =  $c_0 + c_1D$ 

Where:  $c_0 = $80,938 \text{ (fixed)}$ 

 $c_1 = $4.8025 \text{ per foot}$ 

D is well depth

Figure B-2 illustrates the application of the lease equipping cost equation for a new oil production well as a function of depth.



Figure B-2. Lease Equipping Cost for a New Oil Production Well in Illinois vs. Depth

3. <u>Lease Equipment Costs for New Injection Wells.</u> The costs for equipping a new injection well in Illinois include gathering lines, a header, electrical service as well as a water pumping system. The costs are estimated from the EIA Cost and Indices Report.

6,000

Depth, ft

8,000

10,000

12,000

14,000

Equipment costs include a fixed cost component and a depth-related cost component, which varies based on surface pressure requirements. The equation for Illinois is:

Injection Well Equipping Costs =  $c_0 + c_1D$ 

Where:  $c_0 = $10,820$  (fixed)  $c_1 = $16.33$  per foot

2,000

4,000

0 +

D is well depth

Figure B-3 illustrates the application of the lease equipping cost equation for a new injection well as a function of depth for West Texas. The West Texas cost data for lease equipment provides the foundation for the Illinois cost equation.

140,000 Costs 120,000 y = 14.63x + 9277.3Linear (Costs)  $R^2 = 0.9674$ 100,000 80,000 Costs, US\$ 60,000 Ratio to W. TX Basin c<sub>o</sub> US\$ c<sub>1</sub> US\$/ft 40,000 W TX 0.80 7,463 30.73 2.10 RM 14,051 20,000 S TX 1.68 1.19 15,555 17.40 1.86 17,214 16.34 0 0 1,000 2,000 3,000 4,000 7,000 8,000 5,000 6,000 9,000 Depth, ft

Figure B-3. Lease Equipping Costs for a New Injection Well in West Texas vs. Depth

4. Converting Existing Production Wells into Injection Wells. The conversion of existing oil production wells into CO<sub>2</sub> and water injection wells requires replacing the tubing string and adding distribution lines and headers. The costs assume that all surface equipment necessary for water injection are already in place on the lease.

The existing well conversion costs include a fixed cost component and a depth-related cost component, which varies based on the required surface pressure and tubing length. The equation for Illinois is:

Well Conversion Costs =  $c_0 + c_1D$ Where:  $c_0 = \$10,438$  (fixed)  $c_1 = \$6.97$  per foot D is well depth

Figure B-4 illustrates the average cost of converting an existing producer into an injection well for West Texas. The West Texas cost data for converting wells provide the foundation for the Illinois cost equation.

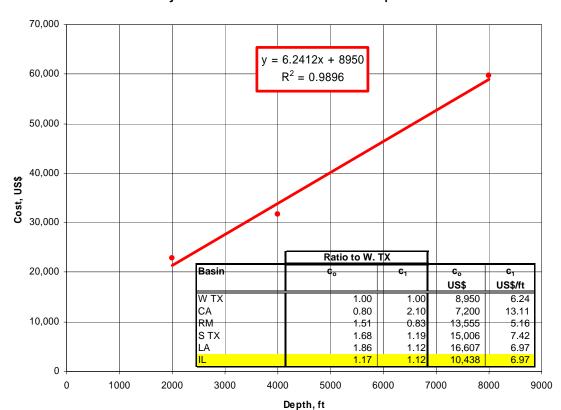


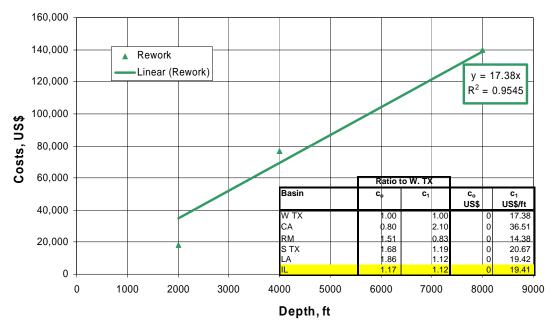
Figure B-4. Cost of Converting Existing Production Wells into Injection Wells in West Texas vs. Depth

5. Costs of Reworking an Existing Waterflood Production or Injection Well for CO<sub>2</sub>-EOR (First Rework). The reworking of existing oil production or CO<sub>2</sub>-EOR injection wells requires pulling and replacing the tubing string and pumping equipment. The well reworking costs are depth-dependent. The equation for Illinois is:

Well Rework Costs =  $c_1D$ Where:  $c_1$  = \$19.41 per foot D is well depth

Figure B-5 illustrates the average cost of well conversion as a function of depth for West Texas. The West Texas cost data for reworking wells provides the foundation for the Illinois cost equation.

Figure B-5. Cost of an Existing Waterflood Production or Injection Well for CO<sub>2</sub>-EOR in West Texas vs. Depth



6. Annual O&M Costs, Including Periodic Well Workovers. The EIA Cost and Indices report provides secondary operating and maintenance (O&M) costs only for West Texas. As such, West Texas and Illinois primary oil production O&M costs (Figure B-6) are used to estimate Illinois secondary recovery O&M costs. Linear trends are used to identify fixed cost constants and variable cost constants for each region, Table B-1.

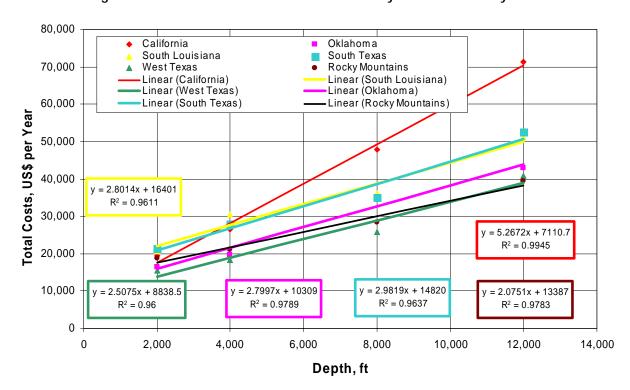


Figure B-6. Annual Lease O&M Costs for Primary Oil Production by Area

Table B-1. Regional Lease O&M Costs and Their Relationship to West Texas

			Ratio to W. TX		
Basin	c。 US\$	c₁ US\$/ft	C <sub>o</sub>	C <sub>1</sub>	
W TX	8,839	2.508	1.00	1.00	
CA	7,111	5.267	0.80	2.10	
RM	13,387	2.075	1.51	0.83	
STX	14,820	2.982	1.68	1.19	
LA	16,401	2.801	1.86	1.12	
IL	10,309	2.800	1.17	1.12	

To account for the O&M cost differences between waterflooding and CO<sub>2</sub>-EOR, two adjustments are made to the EIA's reported O&M costs for secondary recovery. Workover costs, reported as surface and subsurface maintenance, are doubled to reflect the need for more frequent remedial well work in CO<sub>2</sub>-EOR projects. Liquid lifting are subtracted from annual waterflood O&M costs to allow for the more rigorous accounting of liquid lifting volumes and costs for CO<sub>2</sub>-EOR. (Liquid lifting costs for CO<sub>2</sub>-EOR are discussed in a later section of this appendix.)

Figure B-7 shows the depth-relationship for CO<sub>2</sub>-EOR O&M costs in West Texas. These costs were adjusted to develop O&M for Illinois, shown in the inset of Figure B-7. The equation for Illinois is:

Well O&M Costs =  $b_0 + b_1D$ Where:  $b_0 = $24,166$  (fixed)  $b_1 = $8.71 \text{ per foot}$ D is well depth

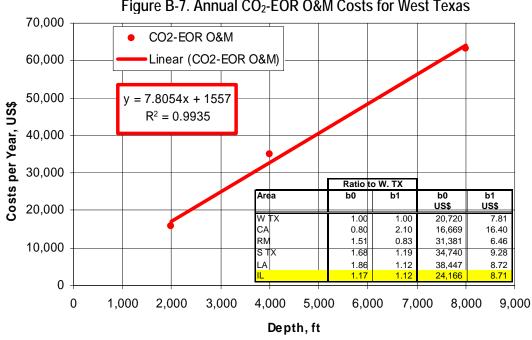


Figure B-7. Annual CO<sub>2</sub>-EOR O&M Costs for West Texas

7. CO<sub>2</sub> Recycle Plant Investment Cost. Operation of CO<sub>2</sub>-EOR requires a recycling plant to capture and reinject the produced CO<sub>2</sub>. The size of the recycle plant is based on peak CO<sub>2</sub> production and recycles requirements.

The cost of the recycling plant is set at \$700,000 per MMcf/d of CO<sub>2</sub> capacity. As such, a small CO<sub>2</sub>-EOR project in the St. Louis formation of the Clay City Consolidated field, with 16 MMcf/d of CO<sub>2</sub> reinjection, will require a recycling plant costing \$10.9 million. A large project in the Aux Vases formation of the Dale City field, with 73 MMcf/d of CO<sub>2</sub> reinjection and 138 injectors requires a recycling plant costing \$51.4 million.

The model has three options for installing a CO<sub>2</sub> recycling plant. The default setting costs the entire plant one year prior to CO<sub>2</sub> breakthrough. The second option places the full CO<sub>2</sub> recycle plant cost at the beginning of the project (Year 0). The third option installs the CO<sub>2</sub> recycle plant in stages. In this case, half the plant is built (and half the cost is incurred) in the year of CO<sub>2</sub> breakthrough. The second half of the plant is built when maximum recycle capacity requirements are reached.

#### 8. Other COTWO Model Costs.

a. CO<sub>2</sub> Recycle O&M Costs. The O&M costs of CO<sub>2</sub> recycling are indexed to energy costs and set at 1% of the oil price (\$0.25 per Mcf @ \$25 Bbl oil).

- b. <u>Lifting Costs.</u> Liquid (oil and water) lifting costs are calculated on total liquid production and costed at \$0.25 per barrel. This cost includes liquid lifting, transportation and re-injection.
- c.  $\underline{CO_2}$  Distribution Costs. The  $CO_2$  distribution system is similar to the gathering systems used for natural gas. A distribution "hub" is constructed with smaller pipelines delivering purchased  $CO_2$  to the project site.

The distribution pipeline cost is dependent on the injection requirements for the project. The fixed component is \$150,000. The variable cost component accounts for increasing piping diameters associated with increasing  $CO_2$  injection requirements. These range from \$80,000 per mile for 4" pipe ( $CO_2$  rate less than 15 MMcf/d), \$120,000 per mile for 6" pipe ( $CO_2$  rate of 15 to 35 MMcf/d), \$160,000 per mile for 8" pipe ( $CO_2$  rate of 35 to 60 MMcf/d), and \$200,000 per mile for pipe greater than 8" diameter ( $CO_2$  rate greater than 60 MMcf/d). Aside from the injection volume, cost also depends on the distance from the  $CO_2$  "hub" (transfer point) to the oil field. Currently, the distance is set at 10 miles.

The CO<sub>2</sub> distribution cost equation for Illinois is:

Pipeline Construction Costs = \$150,000 + C<sub>D</sub>\*Distance

Where: C<sub>D</sub> is the cost per mile of the necessary pipe diameter (from the CO<sub>2</sub> injection rate)

Distance = 10.0 miles

- d. <u>G&A Costs.</u> General and administrative (G&A) costs of 20% are added to well O&M and lifting costs.
  - e. Royalties. Royalty payments are assumed to be 12.5%.
- f. <u>Production Taxes.</u> Severance and ad valorum taxes are both set at 0% on the oil production stream.
- g. <u>Crude Oil Price Differential.</u> To account for market and oil quality (gravity) differences on the realized oil price, the cost model incorporated the current basis differential for Illinois (-\$1.00 per barrel) and the current gravity differential (-\$0.25 per API, from a basis of 40 API) into the average wellhead oil price realized by each oil reservoir. The equation for Illinois is:

Wellhead Oil Price = Oil Price + (-\$1.00) – [\$0.25\*(40 - °API)]
Where: Oil Price is the marker oil price (West Texas intermediate)

API is oil gravity

If the oil gravity is less than 40 °API, the wellhead oil price is reduced; if the oil gravity is greater than 40 °API, the wellhead oil price is increased.

# Appendix C

Indiana CO<sub>2</sub>-EOR Cost Model

## Cost Model for CO<sub>2</sub>-Based Enhanced Oil Recovery (CO<sub>2</sub>-EOR)

This appendix provides documentation for the cost module of the desktop CO<sub>2</sub>-EOR policy and analytical model (COTWO) developed by Advanced Resources for DOE/FE-HQ. The sections of this cost documentation report are organized according to the normal sequence of estimating the capital and operating expenditures for a CO<sub>2</sub>-EOR project:

1. Well Drilling and Completion Costs. The costs for well drilling and completion (D&C) are based on the 2003 JAS cost study recently published by API for Indiana.

The well D&C cost equation has a fixed cost constant for site preparation and other fixed cost items and a variable cost equation that increases with depth. The total equation is:

Well D&C Costs =  $a_0 e^{a_1D}$ Where:  $a_0$  is 83085  $a_1$  is 0.00052 D is well depth

Figure C-1 provides the details for the cost equation and illustrates the "goodness of fit" for the well D&C cost equation for Indiana.

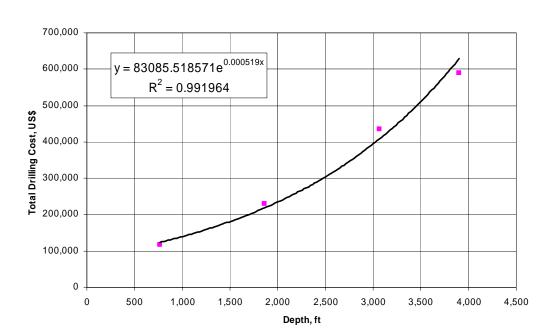


Figure C-1. Oil Well D&C Costs for Indiana

In order to bring the 2003 API drilling costs (the most recent available) into 2004 numbers where increased oil prices are expected to result in significantly increased drilling costs, a relationship was established between average drilling costs and average annual oil prices. Drillings costs from the ten year period of 1994-2003 (API data) were plotted versus the three year weighted average annual oil prices for those years (EIA Annual Energy Review, 2004) and the following relationship was established:

Drilling costs (per foot) = \$5.04(annual oil price) – \$3.2116.

Applying the 2004 average oil price of \$36.77 gives a drilling cost of \$182 per foot and an increase of 25.6% over the 2003 cost of \$145 per foot. Therefore, drilling and completion costs were increased by 25% over the Indiana D&C cost calculations to reflect this increase in 2004 drilling costs.

2. <u>Lease Equipment Costs for New Producing Wells.</u> The costs for equipping a new oil production well are based on data reported by the EIA in their 2004 "Cost and Indices for Domestic Oil and Gas Field Equipment and Production Operations" report. This survey provides estimated lease equipment costs for 10 wells producing with artificial lift, from depths ranging from 2,000 to 12,000 feet, into a central tank battery.

The equation contains a fixed cost constant for common cost items, such as free water knock-out, water disposal and electrification, and a variable cost component to capture depth-related costs such as for pumping equipment. The total equation is:

Production Well Equipping Costs =  $c_0 + c_1D$ 

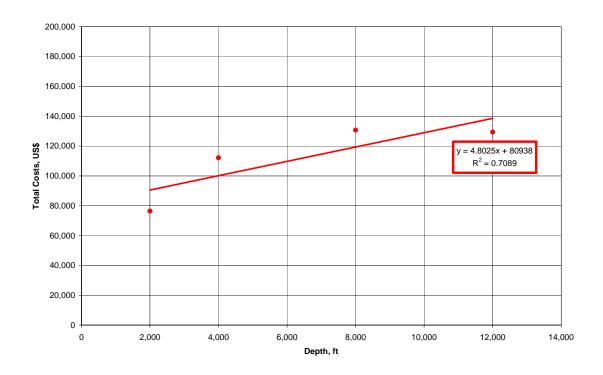
Where:  $c_0 = $80,938 \text{ (fixed)}$ 

 $c_1 = $4.8025 \text{ per foot}$ 

D is well depth

Figure C-2 illustrates the application of the lease equipping cost equation for a new oil production well as a function of depth.

Figure C-2. Lease Equipping Cost for a New Oil Production Well in Indiana vs. Depth



3. <u>Lease Equipment Costs for New Injection Wells.</u> The costs for equipping a new injection well in Indiana include gathering lines, a header, electrical service as well as a water pumping system. The costs are estimated from the EIA Cost and Indices Report.

Equipment costs include a fixed cost component and a depth-related cost component, which varies based on surface pressure requirements. The equation for Indiana is:

Injection Well Equipping Costs =  $c_0 + c_1D$ 

Where:  $c_0 = $10,820$  (fixed)

 $c_1 = $16.33 \text{ per foot}$ 

D is well depth

Figure C-3 illustrates the application of the lease equipping cost equation for a new injection well as a function of depth for West Texas. The West Texas cost data for lease equipment provides the foundation for the Indiana cost equation.

140,000 Costs 120,000 y = 14.63x + 9277.3Linear (Costs)  $R^2 = 0.9674$ 100,000 80,000 Costs, US\$ 60,000 Ratio to W. TX Basin 40,000 US\$ US\$/ft W TX 1.00 1.00 0.80 7,463 30.73 2.10 RM 1.51 0.83 14,051 12.11 20,000 STX 1.68 1.19 15,555 17.40 16.34 1.86 1.12 17,214 16.33 0 0 1,000 2,000 3,000 4,000 5,000 6,000 7,000 8,000 9,000 Depth, ft

Figure C-3. Lease Equipping Costs for a New Injection Well in West Texas vs. Depth

4. <u>Converting Existing Production Wells into Injection Wells.</u> The conversion of existing oil production wells into CO<sub>2</sub> and water injection wells requires replacing the tubing string and adding distribution lines and headers. The costs assume that all surface equipment necessary for water injection are already in place on the lease.

The existing well conversion costs include a fixed cost component and a depth-related cost component, which varies based on the required surface pressure and tubing length. The equation for Indiana is:

Well Conversion Costs =  $c_0 + c_1D$ Where:  $c_0 = \$10,438$  (fixed)  $c_1 = \$6.97$  per foot D is well depth

Figure C-4 illustrates the average cost of converting an existing producer into an injection well for West Texas. The West Texas cost data for converting wells provide the foundation for the Indiana cost equation.

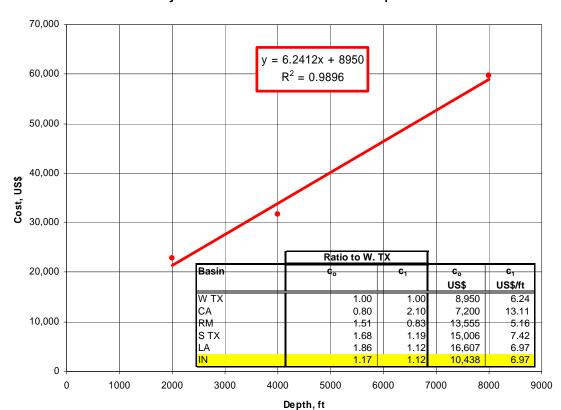


Figure C-4. Cost of Converting Existing Production Wells into Injection Wells in West Texas vs. Depth

5. Costs of Reworking an Existing Waterflood Production or Injection Well for CO<sub>2</sub>-EOR (First Rework). The reworking of existing oil production or CO<sub>2</sub>-EOR injection wells requires pulling and replacing the tubing string and pumping equipment. The well reworking costs are depth-dependent. The equation for Indiana is:

Well Rework Costs =  $c_1D$ Where:  $c_1$  = \$19.41 per foot D is well depth

Figure C-5 illustrates the average cost of well conversion as a function of depth for West Texas. The West Texas cost data for reworking wells provides the foundation for the Indiana cost equation.

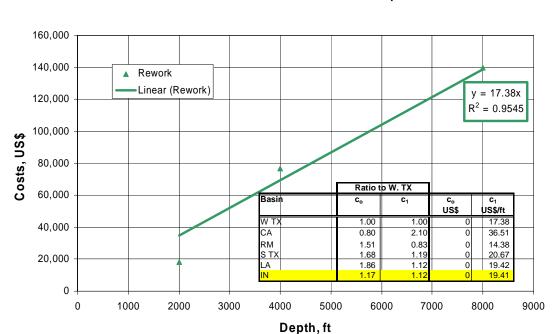


Figure C-5. Cost of an Existing Waterflood Production or Injection Well for CO<sub>2</sub>-EOR in West Texas vs. Depth

6. Annual O&M Costs, Including Periodic Well Workovers. The EIA Cost and Indices report provides secondary operating and maintenance (O&M) costs only for West Texas. As such, West Texas and Indiana primary oil production O&M costs (Figure C-6) are used to estimate Indiana secondary recovery O&M costs. Linear trends are used to identify fixed cost constants and variable cost constants for each region, Table C-1.

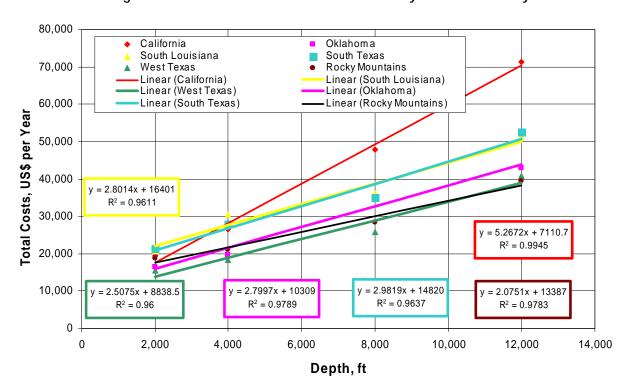


Figure C-6. Annual Lease O&M Costs for Primary Oil Production by Area

Table C-1. Regional Lease O&M Costs and Their Relationship to West Texas

			Ratio to W. TX		
Basin	c。 US\$	c₁ US\$/ft	C <sub>o</sub>	C <sub>1</sub>	
W TX	8,839	2.508	1.00	1.00	
CA	7,111	5.267	0.80	2.10	
RM	13,387	2.075	1.51	0.83	
STX	14,820	2.982	1.68	1.19	
LA	16,401	2.801	1.86	1.12	
IN	10,309	2.800	1.17	1.12	

To account for the O&M cost differences between waterflooding and CO<sub>2</sub>-EOR, two adjustments are made to the EIA's reported O&M costs for secondary recovery. Workover costs, reported as surface and subsurface maintenance, are doubled to reflect the need for more frequent remedial well work in CO<sub>2</sub>-EOR projects. Liquid lifting are subtracted from annual waterflood O&M costs to allow for the more rigorous accounting of liquid lifting volumes and costs for CO<sub>2</sub>-EOR. (Liquid lifting costs for CO<sub>2</sub>-EOR are discussed in a later section of this appendix.)

Figure C-7 shows the depth-relationship for CO<sub>2</sub>-EOR O&M costs in West Texas. These costs were adjusted to develop O&M for Indiana, shown in the inset of Figure C-7. The equation for Indiana is:

Well O&M Costs =  $b_0 + b_1D$ Where:  $b_0 = $24,166$  (fixed)  $b_1 = $8.71$  per foot D is well depth

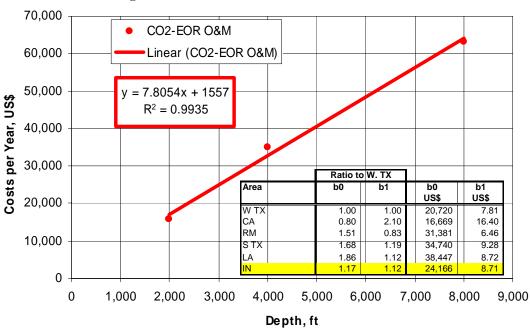


Figure C-7. Annual CO<sub>2</sub>-EOR O&M Costs for West Texas

7.  $\underline{\text{CO}_2}$  Recycle Plant Investment Cost. Operation of  $\text{CO}_2$ -EOR requires a recycling plant to capture and reinject the produced  $\text{CO}_2$ . The size of the recycle plant is based on peak  $\text{CO}_2$  production and recycles requirements.

The cost of the recycling plant is set at \$700,000 per MMcf/d of CO<sub>2</sub> capacity. As such, a CO<sub>2</sub>-EOR project in the Waltersburg formation of the Springfield Consolidated field, with 65 MMcf/d of CO<sub>2</sub> reinjection, will require a recycling plant costing \$45 million

The model has three options for installing a  $CO_2$  recycling plant. The default setting costs the entire plant one year prior to  $CO_2$  breakthrough. The second option places the full  $CO_2$  recycle plant cost at the beginning of the project (Year 0). The third option installs the  $CO_2$  recycle plant in stages. In this case, half the plant is built (and half the cost is incurred) in the year of  $CO_2$  breakthrough. The second half of the plant is built when maximum recycle capacity requirements are reached.

### 8. Other COTWO Model Costs.

a.  $\underline{CO_2}$  Recycle O&M Costs. The O&M costs of  $CO_2$  recycling are indexed to energy costs and set at 1% of the oil price (\$0.25 per Mcf @ \$25 Bbl oil).

- b. <u>Lifting Costs.</u> Liquid (oil and water) lifting costs are calculated on total liquid production and costed at \$0.25 per barrel. This cost includes liquid lifting, transportation and re-injection.
- c. <u>CO<sub>2</sub> Distribution Costs.</u> The CO<sub>2</sub> distribution system is similar to the gathering systems used for natural gas. A distribution "hub" is constructed with smaller pipelines delivering purchased CO<sub>2</sub> to the project site.

The distribution pipeline cost is dependent on the injection requirements for the project. The fixed component is \$150,000. The variable cost component accounts for increasing piping diameters associated with increasing  $CO_2$  injection requirements. These range from \$80,000 per mile for 4" pipe ( $CO_2$  rate less than 15MMcf/d), \$120,000 per mile for 6" pipe ( $CO_2$  rate of 15 to 35 MMcf/d), \$160,000 per mile for 8" pipe ( $CO_2$  rate of 35 to 60 MMcf/d), and \$200,000 per mile for pipe greater than 8" diameter ( $CO_2$  rate greater than 60 MMcf/d). Aside from the injection volume, cost also depends on the distance from the  $CO_2$  "hub" (transfer point) to the oil field. Currently, the distance is set at 10 miles.

The CO<sub>2</sub> distribution cost equation for Indiana is:

Pipeline Construction Costs = \$150,000 + C<sub>D</sub>\*Distance

Where: C<sub>D</sub> is the cost per mile of the necessary pipe diameter (from the CO<sub>2</sub> injection rate)

Distance = 10.0 miles

- d. <u>G&A Costs.</u> General and administrative (G&A) costs of 20% are added to well O&M and lifting costs.
  - e. Royalties. Royalty payments are assumed to be 12.5%.
- f. <u>Production Taxes.</u> Severance tax is set at 1% and ad valorum tax is set at 0% on the oil production stream.
- g. <u>Crude Oil Price Differential</u>. To account for market and oil quality (gravity) differences on the realized oil price, the cost model incorporated the current basis differential for Indiana (-\$1.00 per barrel) and the current gravity differential (-\$0.25 per API, from a basis of 40 API) into the average wellhead oil price realized by each oil reservoir. The equation for Indiana is:

Wellhead Oil Price = Oil Price + (-\$1.00) – [\$0.25\*(40 - ^API)]
Where: Oil Price is the marker oil price (West Texas intermediate)
API is oil gravity

If the oil gravity is less than 40 °API, the wellhead oil price is reduced; if the oil gravity is greater than 40 °API, the wellhead oil price is increased.

# Appendix D

# Kentucky CO<sub>2</sub>-EOR Cost Model

## Cost Model for CO<sub>2</sub>-Based Enhanced Oil Recovery (CO<sub>2</sub>-EOR)

This appendix provides documentation for the cost module of the desktop CO<sub>2</sub>-EOR policy and analytical model (COTWO) developed by Advanced Resources for DOE/FE-HQ. The sections of this cost documentation report are organized according to the normal sequence of estimating the capital and operating expenditures for a CO<sub>2</sub>-EOR project:

1. <u>Well Drilling and Completion Costs.</u> The costs for well drilling and completion (D&C) are based on the 2003 JAS cost study recently published by API for Kentucky.

The well D&C cost equation has a fixed cost constant for site preparation and other fixed cost items and a variable cost equation that increases with depth. The total equation is:

Well D&C Costs =  $a_0 e^{a_1D}$ Where:  $a_0$  is 83085  $a_1$  is 0.00052 D is well depth

Figure D-1 provides the details for the cost equation and illustrates the "goodness of fit" for the well D&C cost equation for Kentucky.

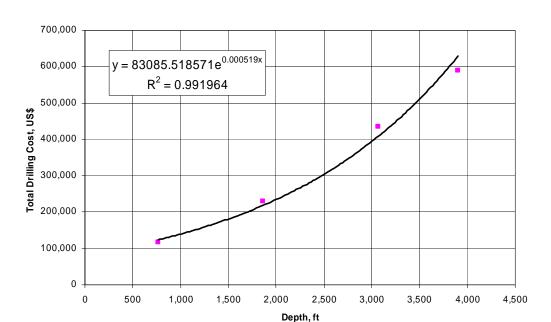


Figure D-1. Oil Well D&C Costs for Kentucky

In order to bring the 2003 API drilling costs (the most recent available) into 2004 numbers where increased oil prices are expected to result in significantly increased drilling costs, a relationship was established between average drilling costs and average annual oil prices. Drillings costs from the ten year period of 1994-2003 (API data) were plotted versus the three year weighted average annual oil prices for those years (EIA Annual Energy Review, 2004) and the following relationship was established:

Drilling costs (per foot) = \$5.04(annual oil price) – \$3.2116.

Applying the 2004 average oil price of \$36.77 gives a drilling cost of \$182 per foot and an increase of 25.6% over the 2003 cost of \$145 per foot. Therefore, drilling and completion costs were increased by 25% over the Kentucky D&C cost calculations to reflect this increase in 2004 drilling costs.

2. <u>Lease Equipment Costs for New Producing Wells.</u> The costs for equipping a new oil production well are based on data reported by the EIA in their 2004 "Cost and Indices for Domestic Oil and Gas Field Equipment and Production Operations" report. This survey provides estimated lease equipment costs for 10 wells producing with artificial lift, from depths ranging from 2,000 to 12,000 feet, into a central tank battery.

The equation contains a fixed cost constant for common cost items, such as free water knock-out, water disposal and electrification, and a variable cost component to capture depth-related costs such as for pumping equipment. The total equation is:

Production Well Equipping Costs =  $c_0 + c_1D$ 

Where:  $c_0 = $80,938 \text{ (fixed)}$ 

 $c_1 = $4.8025 \text{ per foot}$ 

D is well depth

Figure D-2 illustrates the application of the lease equipping cost equation for a new oil production well as a function of depth.

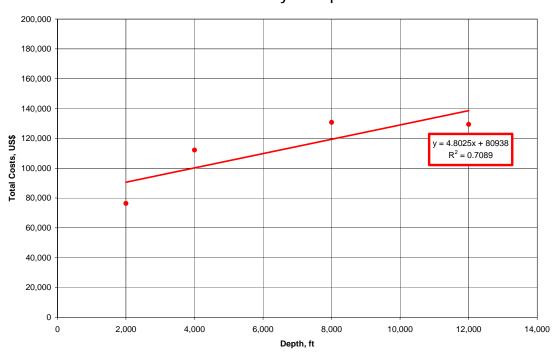


Figure D-2. Lease Equipping Cost for a New Oil Production Well in Kentucky vs. Depth

3. <u>Lease Equipment Costs for New Injection Wells.</u> The costs for equipping a new injection well in Kentucky include gathering lines, a header, electrical service as well as a water pumping system. The costs are estimated from the EIA Cost and Indices Report.

Equipment costs include a fixed cost component and a depth-related cost component, which varies based on surface pressure requirements. The equation for Kentucky is:

Injection Well Equipping Costs =  $c_0 + c_1D$ 

Where:  $c_0 = $10,820$  (fixed)  $c_1 = $16.33$  per foot D is well depth

Figure D-3 illustrates the application of the lease equipping cost equation for a new injection well as a function of depth for West Texas. The West Texas cost data for lease equipment provides the foundation for the Kentucky cost equation.

140,000 Costs 120,000 y = 14.63x + 9277.3Linear (Costs)  $R^2 = 0.9674$ 100,000 80,000 Costs, US\$ 60,000 Ratio to W. TX Basin c。 US\$ 40,000 US\$/ft 1.00 14.63 7,463 0.80 2.10 30.73 RM 1.51 0.83 14.051 12.11 20,000 S TX 1.19 15,555 17.40 17,214 1 86 1 12 16.34 16.33 0 1,000 2,000 3,000 4,000 5,000 6,000 7,000 8,000 9,000 Depth, ft

Figure D-3. Lease Equipping Costs for a New Injection Well in West Texas vs. Depth

4. <u>Converting Existing Production Wells into Injection Wells.</u> The conversion of existing oil production wells into CO<sub>2</sub> and water injection wells requires replacing the tubing string and adding distribution lines and headers. The costs assume that all surface equipment necessary for water injection are already in place on the lease.

The existing well conversion costs include a fixed cost component and a depth-related cost component, which varies based on the required surface pressure and tubing length. The equation for Kentucky is:

Well Conversion Costs =  $c_0 + c_1D$ Where:  $c_0 = \$10,438$  (fixed)  $c_1 = \$6.97$  per foot D is well depth

Figure D-4 illustrates the average cost of converting an existing producer into an injection well for West Texas. The West Texas cost data for converting wells provide the foundation for the Kentucky cost equation.

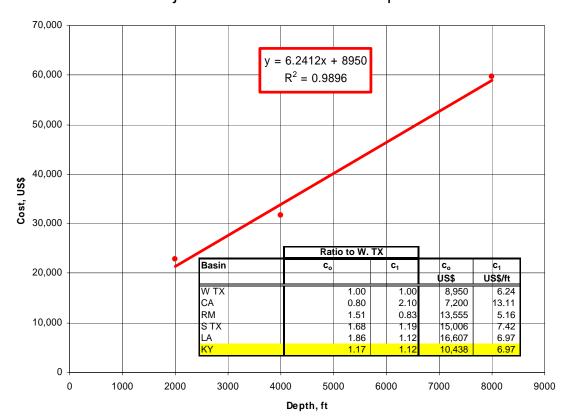


Figure D-4. Cost of Converting Existing Production Wells into Injection Wells in West Texas vs. Depth

5. Costs of Reworking an Existing Waterflood Production or Injection Well for CO<sub>2</sub>-EOR (First Rework). The reworking of existing oil production or CO<sub>2</sub>-EOR injection wells requires pulling and replacing the tubing string and pumping equipment. The well reworking costs are depth-dependent. The equation for Kentucky is:

Well Rework Costs =  $c_1D$ Where:  $c_1 = $19.41$  per foot D is well depth

Figure D-5 illustrates the average cost of well conversion as a function of depth for West Texas. The West Texas cost data for reworking wells provides the foundation for the Kentucky cost equation.

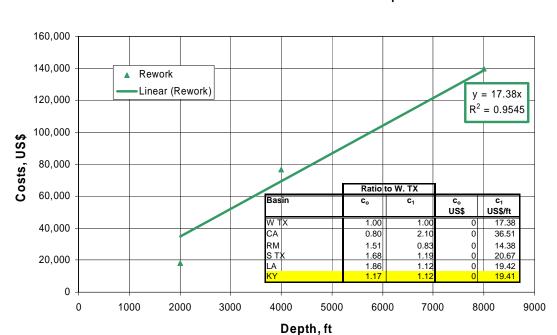


Figure D-5. Cost of an Existing Waterflood Production or Injection Well for CO<sub>2</sub>-EOR in West Texas vs. Depth

6. Annual O&M Costs, Including Periodic Well Workovers. The EIA Cost and Indices report provides secondary operating and maintenance (O&M) costs only for West Texas. As such, West Texas and Kentucky primary oil production O&M costs (Figure D-6) are used to estimate Kentucky secondary recovery O&M costs. Linear trends are used to identify fixed cost constants and variable cost constants for each region, Table D-1.

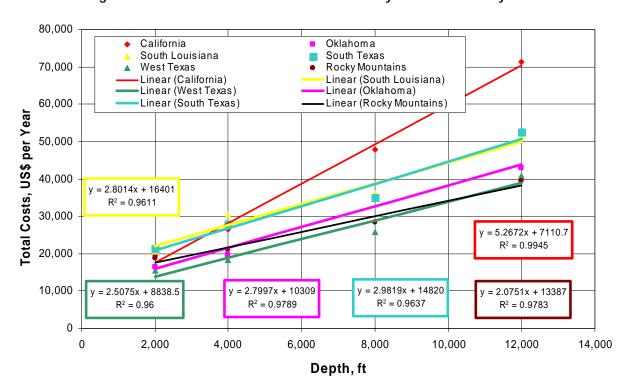


Figure D-6. Annual Lease O&M Costs for Primary Oil Production by Area

Table D-1. Regional Lease O&M Costs and Their Relationship to West Texas

			Ratio to W. TX	
Basin	c <sub>o</sub> US\$	c₁ US\$/ft	C <sub>o</sub>	C <sub>1</sub>
W TX	8,839	2.508	1.00	1.00
CA	7,111	5.267	0.80	2.10
RM	13,387	2.075	1.51	0.83
STX	14,820	2.982	1.68	1.19
LA	16,401	2.801	1.86	1.12
KY	10,309	2.800	1.17	1.12

To account for the O&M cost differences between waterflooding and CO<sub>2</sub>-EOR, two adjustments are made to the EIA's reported O&M costs for secondary recovery. Workover costs, reported as surface and subsurface maintenance, are doubled to reflect the need for more frequent remedial well work in CO<sub>2</sub>-EOR projects. Liquid lifting are subtracted from annual waterflood O&M costs to allow for the more rigorous accounting of liquid lifting volumes and costs for CO<sub>2</sub>-EOR. (Liquid lifting costs for CO<sub>2</sub>-EOR are discussed in a later section of this appendix.)

Figure D-7 shows the depth-relationship for CO<sub>2</sub>-EOR O&M costs in West Texas. These costs were adjusted to develop O&M for Kentucky, shown in the inset of Figure D-7. The equation for Kentucky is:

Well O&M Costs =  $b_0 + b_1D$ Where:  $b_0 = $24,166$  (fixed)  $b_1 = $8.71$  per foot D is well depth

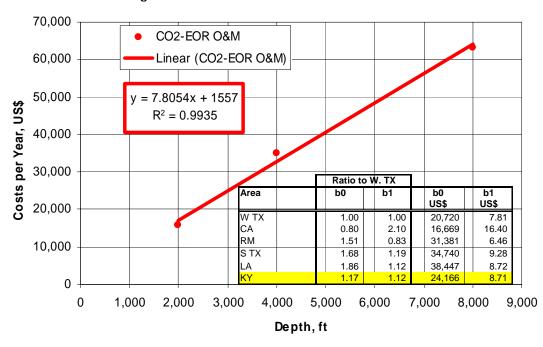


Figure D-7. Annual CO<sub>2</sub>-EOR O&M Costs for West Texas

7.  $\underline{\text{CO}_2}$  Recycle Plant Investment Cost. Operation of  $\text{CO}_2$ -EOR requires a recycling plant to capture and reinject the produced  $\text{CO}_2$ . The size of the recycle plant is based on peak  $\text{CO}_2$  production and recycles requirements.

The cost of the recycling plant is set at \$700,000 per MMcf/d of CO<sub>2</sub> capacity. As such, a CO<sub>2</sub>-EOR project in the Chester Sandstone formation of the Poole Consolidated field, with 12 MMcf/d of CO<sub>2</sub> reinjection, will require a recycling plant costing \$8 million.

The model has three options for installing a  $CO_2$  recycling plant. The default setting costs the entire plant one year prior to  $CO_2$  breakthrough. The second option places the full  $CO_2$  recycle plant cost at the beginning of the project (Year 0). The third option installs the  $CO_2$  recycle plant in stages. In this case, half the plant is built (and half the cost is incurred) in the year of  $CO_2$  breakthrough. The second half of the plant is built when maximum recycle capacity requirements are reached.

### 8. Other COTWO Model Costs.

a.  $\underline{CO_2}$  Recycle O&M Costs. The O&M costs of  $CO_2$  recycling are indexed to energy costs and set at 1% of the oil price (\$0.25 per Mcf @ \$25 Bbl oil).

- b. <u>Lifting Costs.</u> Liquid (oil and water) lifting costs are calculated on total liquid production and costed at \$0.25 per barrel. This cost includes liquid lifting, transportation and re-injection.
- c. <u>CO<sub>2</sub> Distribution Costs.</u> The CO<sub>2</sub> distribution system is similar to the gathering systems used for natural gas. A distribution "hub" is constructed with smaller pipelines delivering purchased CO<sub>2</sub> to the project site.

The distribution pipeline cost is dependent on the injection requirements for the project. The fixed component is \$150,000. The variable cost component accounts for increasing piping diameters associated with increasing  $CO_2$  injection requirements. These range from \$80,000 per mile for 4" pipe ( $CO_2$  rate less than 15MMcf/d), \$120,000 per mile for 6" pipe ( $CO_2$  rate of 15 to 35 MMcf/d), \$160,000 per mile for 8" pipe ( $CO_2$  rate of 35 to 60 MMcf/d), and \$200,000 per mile for pipe greater than 8" diameter ( $CO_2$  rate greater than 60 MMcf/d). Aside from the injection volume, cost also depends on the distance from the  $CO_2$  "hub" (transfer point) to the oil field. Currently, the distance is set at 10 miles.

The CO<sub>2</sub> distribution cost equation for Kentucky is:

Pipeline Construction Costs = \$150,000 + C<sub>D</sub>\*Distance

Where: C<sub>D</sub> is the cost per mile of the necessary pipe diameter (from the CO<sub>2</sub> injection rate)

Distance = 10.0 miles

- d. <u>G&A Costs.</u> General and administrative (G&A) costs of 20% are added to well O&M and lifting costs.
  - e. Royalties. Royalty payments are assumed to be 12.5%.
- f. <u>Production Taxes.</u> Severance taxes are set at 4.5% and ad valorum taxes are both set at 1% on the oil production stream.
- g. <u>Crude Oil Price Differential.</u> To account for market and oil quality (gravity) differences on the realized oil price, the cost model incorporated the current basis differential for Kentucky (-\$1.00 per barrel) and the current gravity differential (-\$0.25 per <sup>°</sup>API, from a basis of 40 <sup>°</sup>API) into the average wellhead oil price realized by each oil reservoir. The equation for Kentucky is:

Wellhead Oil Price = Oil Price + (-\$1.00) – [\$0.25\*(40 - °API)]
Where: Oil Price is the marker oil price (West Texas intermediate)

API is oil gravity

If the oil gravity is less than 40  $^{\circ}$ API, the wellhead oil price is reduced; if the oil gravity is greater than 40  $^{\circ}$ API, the wellhead oil price is increased.

# Appendix E

Michigan CO<sub>2</sub>-EOR Cost Model

## Cost Model for CO<sub>2</sub>-Based Enhanced Oil Recovery (CO<sub>2</sub>-EOR)

This appendix provides documentation for the cost module of the desktop CO<sub>2</sub>-EOR policy and analytical model (COTWO) developed by Advanced Resources for DOE/FE-HQ. The sections of this cost documentation report are organized according to the normal sequence of estimating the capital and operating expenditures for a CO<sub>2</sub>-EOR project:

1. Well Drilling and Completion Costs. The costs for well drilling and completion (D&C) are based on the 2003 JAS cost study recently published by API for Michigan.

The well D&C cost equation has a fixed cost constant for site preparation and other fixed cost items and a variable cost equation that increases with depth. The total equation is:

Well D&C Costs =  $a_0 e^{a_1D}$ Where:  $a_0$  is 83085  $a_1$  is 0.00052 D is well depth

Figure E-1 provides the details for the cost equation and illustrates the "goodness of fit" for the well D&C cost equation for Michigan.

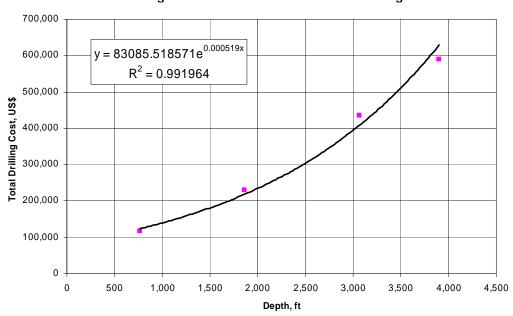


Figure E-1. Oil Well D&C Costs for Michigan

In order to bring the 2003 API drilling costs (the most recent available) into 2004 numbers where increased oil prices are expected to result in significantly increased drilling costs, a relationship was established between average drilling costs and average annual oil prices. Drillings costs from the ten year period of 1994-2003 (API data) were plotted versus the three year weighted average annual oil prices for those years (EIA Annual Energy Review, 2004) and the following relationship was established:

Drilling costs (per foot) = \$5.04(annual oil price) – \$3.2116.

Applying the 2004 average oil price of \$36.77 gives a drilling cost of \$182 per foot and an increase of 25.6% over the 2003 cost of \$145 per foot. Therefore, drilling and completion costs were increased by 25% over the Michigan D&C cost calculations to reflect this increase in 2004 drilling costs.

2. <u>Lease Equipment Costs for New Producing Wells.</u> The costs for equipping a new oil production well are based on data reported by the EIA in their 2004 "Cost and Indices for Domestic Oil and Gas Field Equipment and Production Operations" report. This survey provides estimated lease equipment costs for 10 wells producing with artificial lift, from depths ranging from 2,000 to 12,000 feet, into a central tank battery.

The equation contains a fixed cost constant for common cost items, such as free water knock-out, water disposal and electrification, and a variable cost component to capture depth-related costs such as for pumping equipment. The total equation is:

Production Well Equipping Costs =  $c_0 + c_1D$ 

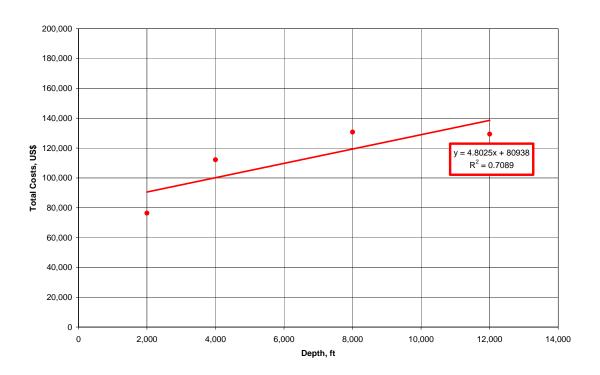
Where:  $c_0 = $80,938 \text{ (fixed)}$ 

 $c_1 = $4.8025 \text{ per foot}$ 

D is well depth

Figure E-2 illustrates the application of the lease equipping cost equation for a new oil production well as a function of depth.

Figure E-2. Lease Equipping Cost for a New Oil Production Well in Michigan vs. Depth



3. <u>Lease Equipment Costs for New Injection Wells.</u> The costs for equipping a new injection well in Michigan include gathering lines, a header, electrical service as well as a water pumping system. The costs are estimated from the EIA Cost and Indices Report.

Equipment costs include a fixed cost component and a depth-related cost component, which varies based on surface pressure requirements. The equation for Michigan is:

Injection Well Equipping Costs =  $c_0 + c_1D$ 

Where:  $c_0 = $10,820$  (fixed)

 $c_1 = $16.33 \text{ per foot}$ 

D is well depth

Figure E-3 illustrates the application of the lease equipping cost equation for a new injection well as a function of depth for West Texas. The West Texas cost data for lease equipment provides the foundation for the Michigan cost equation.

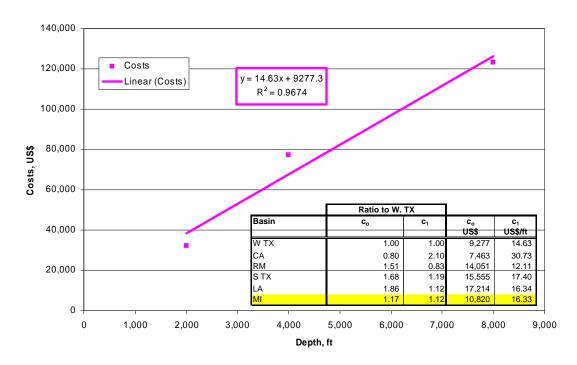


Figure E-3. Lease Equipping Costs for a New Injection Well in West Texas vs. Depth

4. <u>Converting Existing Production Wells into Injection Wells.</u> The conversion of existing oil production wells into CO<sub>2</sub> and water injection wells requires replacing the tubing string and adding distribution lines and headers. The costs assume that all surface equipment necessary for water injection are already in place on the lease.

The existing well conversion costs include a fixed cost component and a depth-related cost component, which varies based on the required surface pressure and tubing length. The equation for Michigan is:

Well Conversion Costs =  $c_0 + c_1D$ Where:  $c_0 = \$10,438$  (fixed)  $c_1 = \$6.97$  per foot D is well depth

Figure E-4 illustrates the average cost of converting an existing producer into an injection well for West Texas. The West Texas cost data for converting wells provide the foundation for the Michigan cost equation.

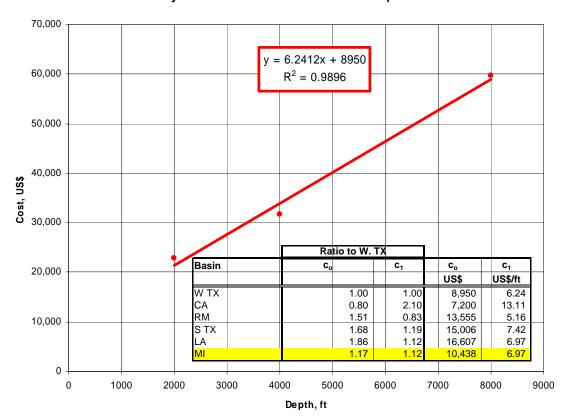


Figure E-4. Cost of Converting Existing Production Wells into Injection Wells in West Texas vs. Depth

5. Costs of Reworking an Existing Waterflood Production or Injection Well for CO<sub>2</sub>-EOR (First Rework). The reworking of existing oil production or CO<sub>2</sub>-EOR injection wells requires pulling and replacing the tubing string and pumping equipment. The well reworking costs are depth-dependent. The equation for Michigan is:

Well Rework Costs =  $c_1D$ Where:  $c_1 = $19.41$  per foot D is well depth

Figure E-5 illustrates the average cost of well conversion as a function of depth for West Texas. The West Texas cost data for reworking wells provides the foundation for the Michigan cost equation.

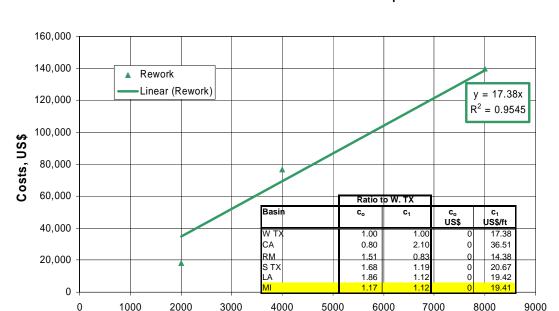


Figure E-5. Cost of an Existing Waterflood Production or Injection Well for CO<sub>2</sub>-EOR in West Texas vs. Depth

6. Annual O&M Costs, Including Periodic Well Workovers. The EIA Cost and Indices report provides secondary operating and maintenance (O&M) costs only for West Texas. As such, West Texas and Michigan primary oil production O&M costs (Figure E-6) are used to estimate Michigan secondary recovery O&M costs. Linear trends are used to identify fixed cost constants and variable cost constants for each region, Table E-1.

Depth, ft

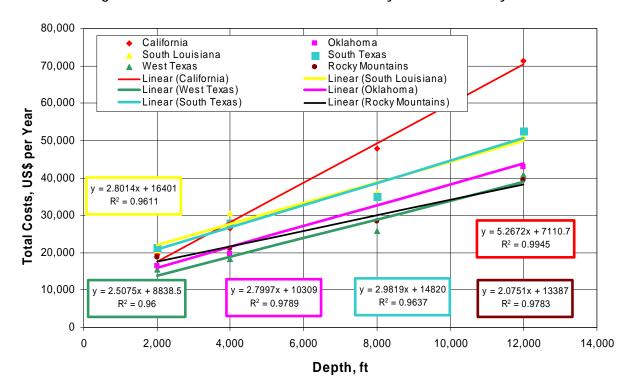


Figure E-6. Annual Lease O&M Costs for Primary Oil Production by Area

Table E-1. Regional Lease O&M Costs and Their Relationship to West Texas

			Ratio to W. TX	
Basin	c <sub>o</sub> US\$	c₁ US\$/ft	C <sub>o</sub>	C <sub>1</sub>
W TX	8,839	2.508	1.00	1.00
CA	7,111	5.267	0.80	2.10
RM	13,387	2.075	1.51	0.83
STX	14,820	2.982	1.68	1.19
LA	16,401	2.801	1.86	1.12
MI	10,309	2.800	1.17	1.12

To account for the O&M cost differences between waterflooding and CO<sub>2</sub>-EOR, two adjustments are made to the EIA's reported O&M costs for secondary recovery. Workover costs, reported as surface and subsurface maintenance, are doubled to reflect the need for more frequent remedial well work in CO<sub>2</sub>-EOR projects. Liquid lifting are subtracted from annual waterflood O&M costs to allow for the more rigorous accounting of liquid lifting volumes and costs for CO<sub>2</sub>-EOR. (Liquid lifting costs for CO<sub>2</sub>-EOR are discussed in a later section of this appendix.)

Figure E-7 shows the depth-relationship for CO<sub>2</sub>-EOR O&M costs in West Texas. These costs were adjusted to develop O&M for Michigan, shown in the inset of Figure E-7. The equation for Michigan is:

Well O&M Costs =  $b_0 + b_1D$ Where:  $b_0 = $24,166$  (fixed)  $b_1 = $8.71$  per foot D is well depth

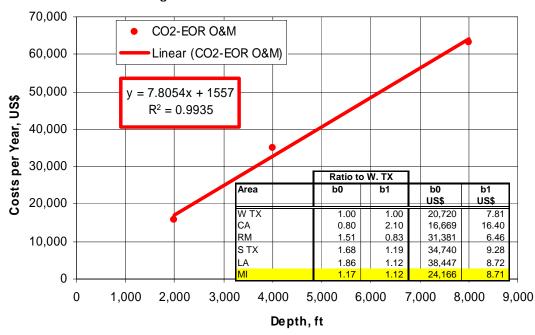


Figure E-7. Annual CO<sub>2</sub>-EOR O&M Costs for West Texas

7.  $\underline{\text{CO}_2}$  Recycle Plant Investment Cost. Operation of  $\text{CO}_2$ -EOR requires a recycling plant to capture and reinject the produced  $\text{CO}_2$ . The size of the recycle plant is based on peak  $\text{CO}_2$  production and recycles requirements.

The cost of the recycling plant is set at \$700,000 per MMcf/d of CO<sub>2</sub> capacity. As such, a CO<sub>2</sub>-EOR project in the Trenton-Black River formation of the Albion/Scipio field, with 72 MMcf/d of CO<sub>2</sub> reinjection, will require a recycling plant costing \$50 million.

The model has three options for installing a  $CO_2$  recycling plant. The default setting costs the entire plant one year prior to  $CO_2$  breakthrough. The second option places the full  $CO_2$  recycle plant cost at the beginning of the project (Year 0). The third option installs the  $CO_2$  recycle plant in stages. In this case, half the plant is built (and half the cost is incurred) in the year of  $CO_2$  breakthrough. The second half of the plant is built when maximum recycle capacity requirements are reached.

### 8. Other COTWO Model Costs.

a.  $\underline{CO_2}$  Recycle O&M Costs. The O&M costs of  $CO_2$  recycling are indexed to energy costs and set at 1% of the oil price (\$0.25 per Mcf @ \$25 Bbl oil).

- b. <u>Lifting Costs.</u> Liquid (oil and water) lifting costs are calculated on total liquid production and costed at \$0.25 per barrel. This cost includes liquid lifting, transportation and re-injection.
- c. <u>CO<sub>2</sub> Distribution Costs.</u> The CO<sub>2</sub> distribution system is similar to the gathering systems used for natural gas. A distribution "hub" is constructed with smaller pipelines delivering purchased CO<sub>2</sub> to the project site.

The distribution pipeline cost is dependent on the injection requirements for the project. The fixed component is \$150,000. The variable cost component accounts for increasing piping diameters associated with increasing  $CO_2$  injection requirements. These range from \$80,000 per mile for 4" pipe ( $CO_2$  rate less than 15MMcf/d), \$120,000 per mile for 6" pipe ( $CO_2$  rate of 15 to 35 MMcf/d), \$160,000 per mile for 8" pipe ( $CO_2$  rate of 35 to 60 MMcf/d), and \$200,000 per mile for pipe greater than 8" diameter ( $CO_2$  rate greater than 60 MMcf/d). Aside from the injection volume, cost also depends on the distance from the  $CO_2$  "hub" (transfer point) to the oil field. Currently, the distance is set at 10 miles.

The CO<sub>2</sub> distribution cost equation for Michigan is:

Pipeline Construction Costs = \$150,000 + C<sub>D</sub>\*Distance

Where: C<sub>D</sub> is the cost per mile of the necessary pipe diameter (from the CO<sub>2</sub> injection rate)

Distance = 10.0 miles

- d. <u>G&A Costs.</u> General and administrative (G&A) costs of 20% are added to well O&M and lifting costs.
  - e. Royalties. Royalty payments are assumed to be 12.5%.
- f. <u>Production Taxes.</u> Severance taxes are set at 4.5% and ad valorum taxes are both set at 1% on the oil production stream.
- g. <u>Crude Oil Price Differential.</u> To account for market and oil quality (gravity) differences on the realized oil price, the cost model incorporated the current basis differential for Michigan (-\$3.92 per barrel) and the current gravity differential (-\$0.25 per API, from a basis of 40 API) into the average wellhead oil price realized by each oil reservoir. The equation for Michigan is:

If the oil gravity is less than 40  $^{\circ}$ API, the wellhead oil price is reduced; if the oil gravity is greater than 40  $^{\circ}$ API, the wellhead oil price is increased.