### Integrated Water-Gas-Shift Pre-Combustion Carbon Capture Process (Contract No. DE-FE0023684)



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### **Project Objectives**

- The project objective is to demonstrate techno-economic viability of an integrated WGS catalyst/CO<sub>2</sub> removal system for IGCC power plants and CTL plants
  - A high temperature PSA adsorbent is used for CO<sub>2</sub> removal above the dew point of the synthesis gas
  - A commercial low temperature catalyst is used for water-gas-shift
  - An effective heat management system is developed

### • Project Tasks

- Design a fully-equipped slipstream test unit with 10 SCFM raw synthesis gas treatment capacity
- Design and fabricate CFD optimized reactors capable of managing the exotherm of the WGS reaction while maintaining energy efficiency
- Demonstrate critical design parameters including sorbent capacity, CO<sub>2</sub> removal efficiency, extent of WGS conversion as well as H<sub>2</sub> recovery using coal synthesis gas
- Complete a high fidelity process design and economic analysis



### **Project Partners**



#### **Project Duration**

- Start Date = October 1, 2014
- End Date = September 30, 2019

#### **Budget**

- Project Cost = \$5,632,619
- DOE Share = \$4,506,719
- TDA and its partners = \$1,125,900



### **TDA's Approach**

- Conventional IGCC plants use multi-stage WGS with inter-stage cooling
  - WGS is an equilibrium-limited exothermic reaction
- Water is supplied at concentrations well above required by the reaction stoichiometry to completely shift the CO to CO<sub>2</sub>



3-stage WGS unit as described in the DOE/NETL-2007/1281

- In our process, the WGS catalyst is combined with a high temperature CO<sub>2</sub> adsorbent to achieve high CO conversion <u>at low steam:carbon ratios</u>
- Reduced water addition increases process efficiency



### **TDA's Sorbent**

- TDA's uses a mesoporous carbon with surface functional groups that remove CO<sub>2</sub> via strong physical adsorption
  - CO<sub>2</sub>-surface interaction is strong enough to allow operation at elevated temperatures
  - Because CO<sub>2</sub> is not bonded via a covalent bond, energy input for regeneration is low
- Heat of CO<sub>2</sub> adsorption is 4.9 kcal/mol for TDA sorbent
  - Net energy loss in sorbent regeneration is similar to Selexol; much higher IGCC efficiency can be achieved due to high temperature CO<sub>2</sub> capture
- Favorable material properties
  - D Pore size is tuned to 10 to 100 A
  - Mesopores eliminates diffusion limitations



US Patent 9,120,079, Dietz, Alptekin, Jayaraman "High Capacity Carbon Dioxide Sorbent", US 6,297,293; 6,737,445; 7,167,354 US Pat. Appl. 61790193, Alptekin, Jayaraman, Copeland "Precombustion  $CO_2$  Capture System Using a Regenerable Sorbent"



### **Operating Conditions**

- CO<sub>2</sub> is recovered via combined pressure & concentration swing
  - CO<sub>2</sub> recovery at ~150 psia reduces energy need for CO<sub>2</sub> compression
  - Small steam purge ensures high product purity
- Isothermal operation eliminates heat/cool transitions
  - Rapid cycles reduces cycle time and increases sorbent utilization
- Similar PSA systems are used in commercial H<sub>2</sub> plants and air separation plants
- The WGS catalyst was subjected to the same cycle



Source: Honeywell/UOP



### Integrated WGS/CO<sub>2</sub> Capture System



- Reducing the use of excess steam improves power cycle efficiency
  - Lower energy consumption to raise the steam
- Process intensification could potentially reduce the number of hardware components and cost

### Sorbent's point of view:

 Less dilution with water increases CO<sub>2</sub> partial pressure and in turn improves sorbent's working capacity



### **Application of the Technology to CTL**



### **Sorbent Development Work**



TDA 0.1 MW pre-combustion carbon capture unit installed at the National Carbon Capture Center

- 0.1 MW<sub>e</sub> test in a world class IGCC plant to demonstrate full benefits of the technology
  - Field Test #1 at NCCC
  - Field Test #2 at Sinopec Yangtzi Petrochemical Plant, Nanjing, Jiangsu Province, China
- Full operation scheme
  - B reactors and all accumulators
  - Utilize product/inert gas purges
  - $\square$  H<sub>2</sub> recovery/CO<sub>2</sub> purity



Yangtzi Petro-chemical Plant



### **NCCC Field Test – Early Work**



- 90+% capture at steam:CO ratio= 1:1.1 with average 96.4% CO conversion
- All objectives met (no coking etc.) but high reactor T was observed



### Technology Status/R&D Needs

- Sorbent is developed under a separate DOE project (DE-FE0000469)
- WGS catalyst is commercially available mature technology
- Early-stage concept demonstration has already been completed (DE-FE0007966 and DE-FE0012048)
  - Integrated sorbent/catalyst operation
  - Pointed out the need to incorporate effective heat management
  - Implemented the heat management scheme in a 4-bed PSA system using coal derived synthesis gas at 1 kg/hr CO<sub>2</sub> removal
- Key R&D need is the design/development of a high fidelity prototype to fully demonstrate the concept using actual coalderived synthesis gas
  - Reactor design to address the heat management needs
  - A 10 kg/hr CO<sub>2</sub> removal is being developed
  - Testing of the high fidelity system will be carried out at Praxair



### **T Profiles - During CO<sub>2</sub> Capture Only**



- Heat generated during adsorption is removed during regeneration
  - Near isothermal operation through the cycle



### Heat Wave WGS & CO<sub>2</sub> Capture



- Integrated WGS & CO<sub>2</sub> capture results in higher ∆T
- Not ideal for CO<sub>2</sub> capture (the WGS heat accumulates in the beds)



### **Conventional Heat Management Options**

### 10 kg/hr CO<sub>2</sub> Removal Pilot Test System – 6" reactors





### Heat Integrated WGS & CO<sub>2</sub> Capture

- Advanced heat management concept based on direct water injection has proven to achieve much better temperature control
  - Also much better heating efficiency (i.e., kJ heat removed per kg water)
- Objective is to achieve a more uniform cooling without having hot or cold spots
- The temperature rise is optimal when the catalyst is distributed into two layers with water injections before each layer

#### T Contours (°C) Single Injection Layer



#### **T** Contours (°C) Multiple Injection Layers



# **Injector Design**





- We designed our own injector nozzles and the water output control system that will allow these to effectively operate inside the reactor hot zone between 200-350°C
- The water flow rate is controlled by controlling injector pulse duration and pulse delay time



## **Bench-Scale Evaluations**





- 8L reactors were modified with water injectors
- Successful proof-of-concept demonstrations have been completed
- ∆T <10°C was maintained over extended cycling (much lower than those observed in the early field tests)



## Life Tests – Sorbent Activity



We completed 32,000 cycles showing stable performance for the WGS catalyst and CO<sub>2</sub> sorbent



# Life Tests – Catalyst Activity



 By evaluating continuous catalytic activity (alone) we showed that cycling between reducing and oxidizing conditions (i.e., steam exposure) had no adverse effect on the WGS catalyst



### Integrated WGS/CO<sub>2</sub> Capture System





## **Fabrication of the Prototype**





### **Installation at Praxair**



 Fabrication of the Prototype unit was completed in 2018 Q2 and installation at Praxair R&D Center (Tonawanda, NY) was completed in 2018 Q3



# **Reactor Loading at Praxair**

- Reactors were loaded with the catalyst and the sorbent in 2018 Q2
- Catalyst has been reduced
- Shakedown tests and preliminary experiments were completed in 2018 Q3





# **Control of Water Injection**

We demonstrated that precise amounts of water can be injected and their individual flow rates can be controlled within tolerances of less than 0.5 g/min between injectors



### **Temperature Management via Water Injection**

- We observed an increase in bed temperature by increasing the inlet steam:CO from 1 to 2
- The bed temperature was maintained at ~40°C lower when injecting the same amount water directly into the beds





# **Impact of Water Injection**

- An overall CO conversion >98% was achieved
- The cycle times were not yet optimized in this run therefore carbon capture was only at 60% (incoming  $CO_2 + CO_2$  from shifted  $CO_2$ )
- We will optimize this during our next test period



### **Effect on Equilibrium Conversion**

By coupling the WGS with the CO<sub>2</sub> sorbent and water injection, we were able to operate the beds at 200°C but achieve the equilibrium CO conversion of a 40°C cooler bed





### Integration with E-Gas<sup>™</sup> Gasifier

Gasifier Type/Make	E-Gas		
Case	1	2	2* (WGS/CO <sub>2</sub> )
	Cold Gas Cleanup	Warm Gas Cleanup	Warm Gas Cleanup
CO <sub>2</sub> Capture Technology	Selexol <sup>™</sup>	TDA's CO <sub>2</sub> Sorbent	TDA's CO <sub>2</sub> Sorbent
CO <sub>2</sub> Capture, %	90	90	90
Gross Power Generated, kW	710,789	670,056	693,542
Gas Turbine Power	464,000	425,605	427,980
Steam Turbine Power	246,789	244,450	265,562
Syngas Expander Power	-	-	-
Auxiliary Load, kW	194,473	124,138	138,741
Net Power, kW	516,316	545,917	554,801
Net Plant Efficiency, % HHV	31.0	34.1	34.7
Coal Feed Rate, kg/h	220,549	212,265	212,265
Raw Water Usage, GPM/MW	10.9	10.3	10.0
Total Plant Cost, \$/kW	3,464	3,042	2,990
COE without CO <sub>2</sub> TS&M, \$/MWh	136.8	120.5	118.8
COE with CO <sub>2</sub> TS&M, \$/MWh	145.7	128.6	126.7
Cost of CO <sub>2</sub> Captured, \$/tonne	53.2	37.4	35.8

- IGCC plant efficiency is estimated as 34.7% with TDA's WGS/CO<sub>2</sub> system
- Cost of CO<sub>2</sub> capture is estimated as less than \$26/tonne (including TS&M less than \$35.8/tonne)



### **Process Economic Analysis - CTL**

Gasifier	Sh	ell		
Coal	Bituminous			
Case	9	10A		
		Wann Gas		
	Cold Gas	Cleanup		
	Cleanup	TDA's CO <sub>2</sub>		
CO <sub>2</sub> Capture Technology	<b>Rectisol</b> <sup>™</sup>	Sorbent		
CO2 Capture, %	90	90		
Gross Power Generated, kW	462,568	458,830		
Gas Turbine Power	130,283	130,519		
Steam Turbine Power	332,285	<b>328,3</b> 11		
Syngas Expander Power	-	-		
Auxiliary Load, kW	397,803	365,956		
Net Power, kW	64,764	92,875		
Net Plant Efficiency, % HHV	1.08	1.55		
Naphtha Production rate, ST/D	1,803	1,722		
Diesel Production rate, ST/D	4,789	4,933		
Coal Feed Rate, kg/h	793,864	793,864		
Raw Water Usage, GPM	14,032.6	12,394.0		
Total Plant Cost, \$/kg/D	949.87	864.94		
NAPHTHA				
1st year Required Selling Price (RSP)				
w/o CO2 TS&M, \$/bbl	107.0	100.0		
DIESEL				
1st year Required Selling Price (RSP)				
w/o CO2 TS&M, \$/bbl	153.0	143.0		

- Integrated WGS with CO<sub>2</sub> capture reduced the required selling price for Naphtha to \$100 per bbl compared to \$107 per bbl for a CTL plant with Rectisol
- Integrated WGS with CO<sub>2</sub> capture reduced the required selling price for Diesel to \$143 per bbl compared to \$153 per bbl for a CTL plant with Rectisol



### **Future Work**

- **Testing of the unit at Praxair Field Test Campaign #2**
- **Complete CFD Model validation with Praxair Test Data**
- **Complete a high-fidelity system design/analysis and cost estimate**
- **Complete an Environmental, Health and Safety (EHS) assessment**



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