

# Energy Efficient Waste Heat Coupled Forward Osmosis for Effluent Water Management at Coal-Fired Power Plants

Project Number DE-FE0031551

N. Rajagopalan, Ph.D.

University of Illinois at Urbana-Champaign

Partners: Trimeric Corporation, Illinois Power Plant

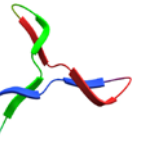
DOE/NETL Project Manager: Mr. Charles Miller



U.S. DEPARTMENT OF  
**ENERGY**

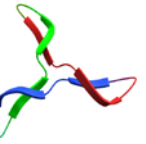


NATIONAL  
ENERGY  
TECHNOLOGY  
LABORATORY



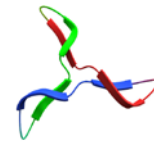
# Section 1

- *Terminology*
- *Objectives*
- *Alignment with DOE*
- *State-of-Art Comparison*



# Terminology

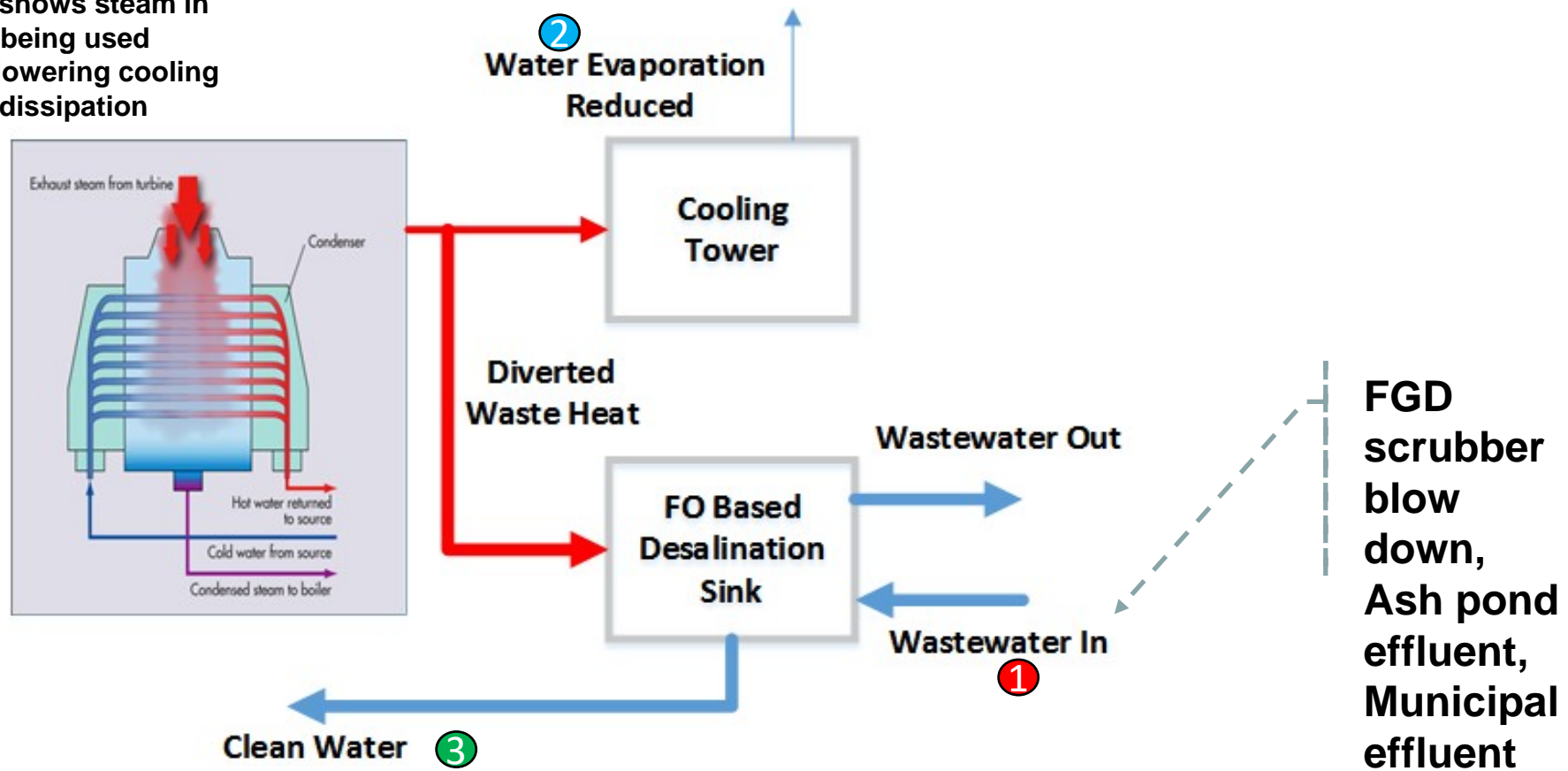
- Power plant effluents: **FGD scrubber blowdown**; cooling tower blowdown; ash transport water, etc.
- Management: Water **reuse/recycling**; Compliance with **ELG /CCR**;
- Waste Heat Coupled: **Treatment** methods driven by flue gas or condenser heat or other sources
- Forward Osmosis: **Thermal energy driven osmotic** membrane based process operating at **ambient pressure/temperature**;
- Energy Efficient: Targets: **<200 kJ/kg thermal** of water produced & **<3.6 kWh/m<sup>3</sup>**

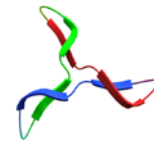


# Waste Heat to Water in Power Plants

Schematic shows steam in condenser being used elsewhere lowering cooling tower heat dissipation

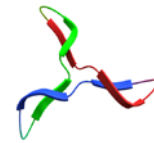
Other sources of waste heat can also be used; e.g. Flue gas





# Project Objectives

- Overall goal
  - Evaluate a transformational low energy (<200 kJ/kg water) waste heat coupled forward osmosis (FO) based water treatment system (the Aquapod<sup>®</sup>), to manage effluents, meet cooling water demands and achieve water conservation in complex and unique environment of a power plant environment
- Specific objectives
  - To map the available wastewater sources and waste heat in a coal-fired power plant of 2009 vintage.
  - To establish the **technical** and **economic feasibility** of utilizing the Aquapod<sup>®</sup> process to recover at least 50% usable water from degraded water sources such as FGD blowdown, other proximal wastewater.
  - To evaluate the ability of FO operational modes to handle highly fouling stream such as FGD blowdown without extensive softening.

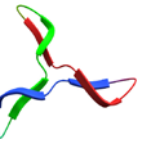


## Alignment with DOE Goals

Current Project aligns with

DE-FOA-0001686/ AOI 5 Effluent Water Management at Coal-Fired Energy Plants goals of

- understanding the overall water balances, understand constituents of concern, and reduce overall treatment requirements
- promoting innovative effluent water management practices at coal-fired energy plants.
- developing water treatment and reuse methods that employ low energy or waste heat solutions

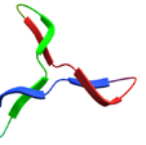


## Aquapod

- Uses heat/waste heat as opposed to electrical energy
- Requires minimal pretreatment
- Low energy consumption; thermal <math><200\text{ kJ/kg}</math>; electrical <math><3.6\text{ kWh/m}^3</math>
- Simple equipment – primarily membrane modules, mixer settler systems
- Benign chemicals
- Range of TDS: 10-12% NaCl

## Other technologies

- RO, NF – use electrical energy
- RO, NF need more extensive pretreatment for high fouling streams such as FGD scrubber blowdown
- Membrane distillation/ ammonium carbamate based FO systems have energy consumption in the range of 400 – 1200 kJ/kg
- Ammonium carbamate FO systems use ammonia, more complex equipment.

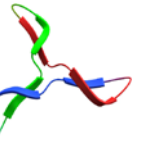


# Section 2

230 MW Coal Fired Power Plant

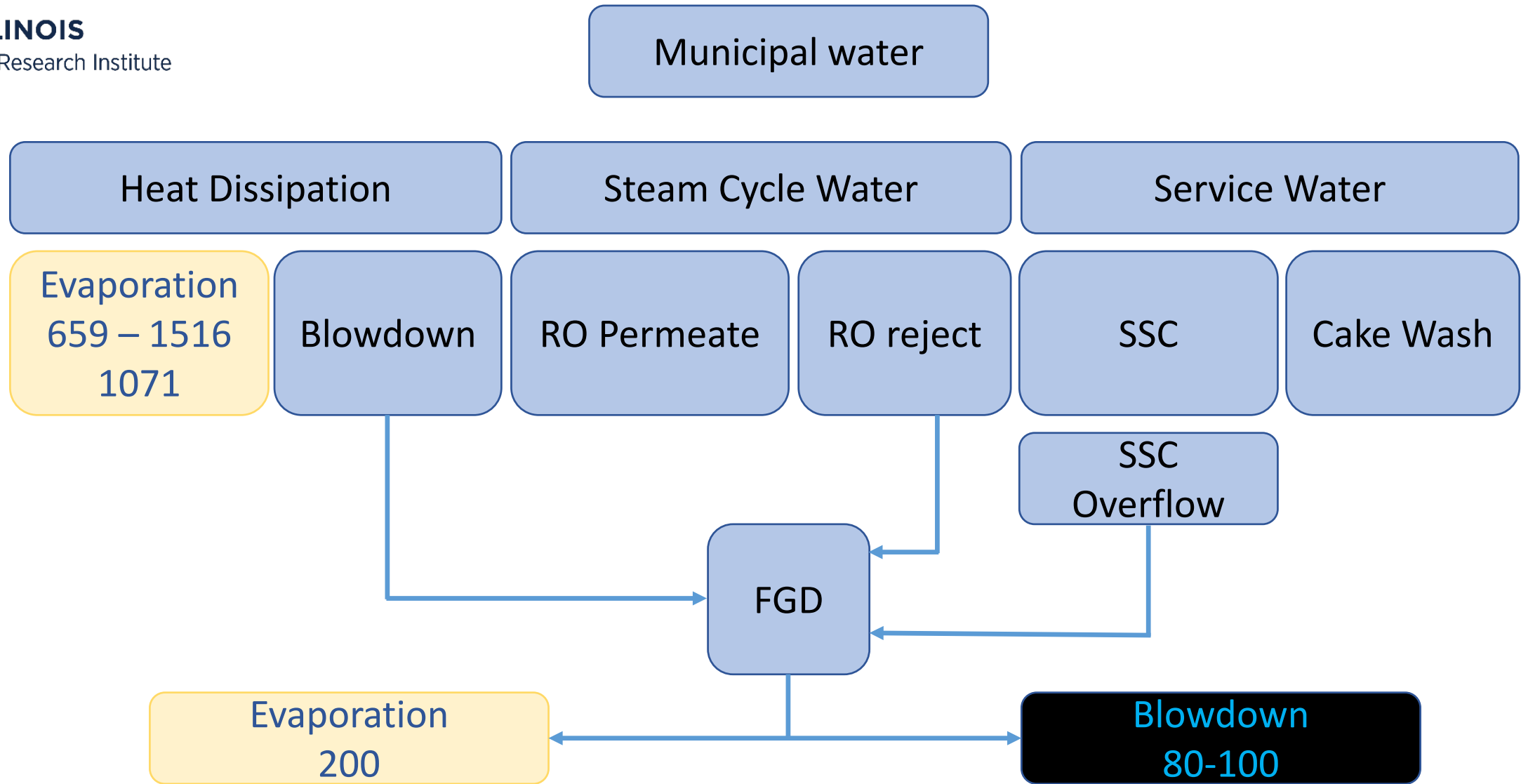
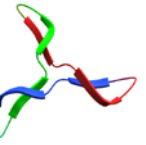
- *Water Use/Effluent In Power Plants*
- *Waste Heat Availability*
- *Conclusions*



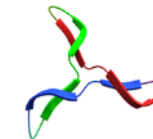


# Mapping Wastewater

230 MW Coal Fired Power Plant



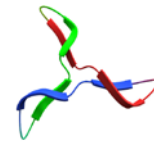
Units:      gpm  
 SSC: Submerged scraper conveyor  
1071 – median value of evaporation in cooling tower



## Potential Wastewater Sources for FO Treatment

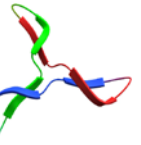
Wastewater Source	Potential Volume Available GPM	Comments	Ability to meet cooling water demands
FGD Blowdown	<b>80-100</b>	Depends on chloride level set point in scrubber; problematic from a regulatory standpoint; high fouling stream	~ <b>2.5-7.5%</b> <sup>a</sup>
On-site WWTP	(4.29 MGD/~3000 gpm)		<b>100 %</b>
Wastewater from nearby municipal wastewater treatment plant	(10 MGD Design Average Flow/~ 7000 gpm)		<b>100 %</b>

<sup>a</sup> FGD blowdown assumed to be between 80 and 100 gpm; 50% reuse of this stream assumed; cooling tower make up water needs are taken to be 659 – 1516 gpm (100 MWh – 230 MWh)



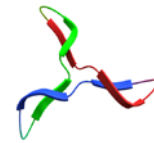
## Wastewater Characteristics Relevant for FO

Stream Description	GPM	Comments	Total Dissolved Solids mg/L	Osmotic Pressure psia	Minerals Exceeding Saturation Potential Scalants
FGD blowdown water	80-100	To municipal wastewater treatment plant	10,000 -12,200	83	Calcite, Fluorite, Barite, <b>Gypsum</b> , Bayerite, Sellaite, Siderite, Brucite
Inlet to on-site wastewater plant	~3000	Currently treated and discharged to Lake; water not used for current unit	320	3	Bayerite, Barite
Secondary Influent from Municipal WWTP	~7000	Available within 10 miles from the IL Power Plant	570	7	Calcite, Siderite, Bayerite



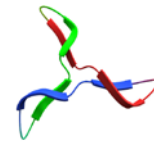
# Mapping Waste Heat

230 MW Coal Fired Power Plant



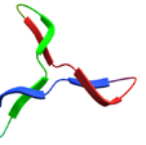
## Waste Heat Sources in IL PP

Stream	Temperature Available °F (°C)	Heat Quantity (MMBTU/Hr)	Quantity of Water Generated by Evaporation assuming 1000 BTU/lb for evaporation
Condenser water	106 (41)	921	Too low for evaporation without excessive vacuum.
Flue gas at Air Preheater Outlet	<b>300 (149)</b>	<b>52</b>	Approximately 100 gpm of water can be evaporated using the heat in flue gas;
Bottom Ash Overflow Water	140 (60)	2.75	Insignificant



## Section 2: Conclusions

- Waste heat available in flue gas sufficient to desalinate ~1000 gpm of wastewater through low energy FO process (200 kJ/kg)
- Part of the waste heat in condenser water can be used in the FO process as well
- FGD scrubber blowdown most troublesome from treatment and regulatory point; of greatest interest to utility; can satisfy only small portion of cooling tower demands; best suited for FO due to high fouling nature
- Other wastewater (onsite/offsite) can supplement cooling tower requirements



# Section 3

230 MW Coal Fired Power Plant

*Aquapod – Working Principle*

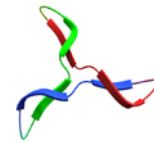
*FGD-FO Data*

*Salt-Polymer Selection Considerations*

*Summary*

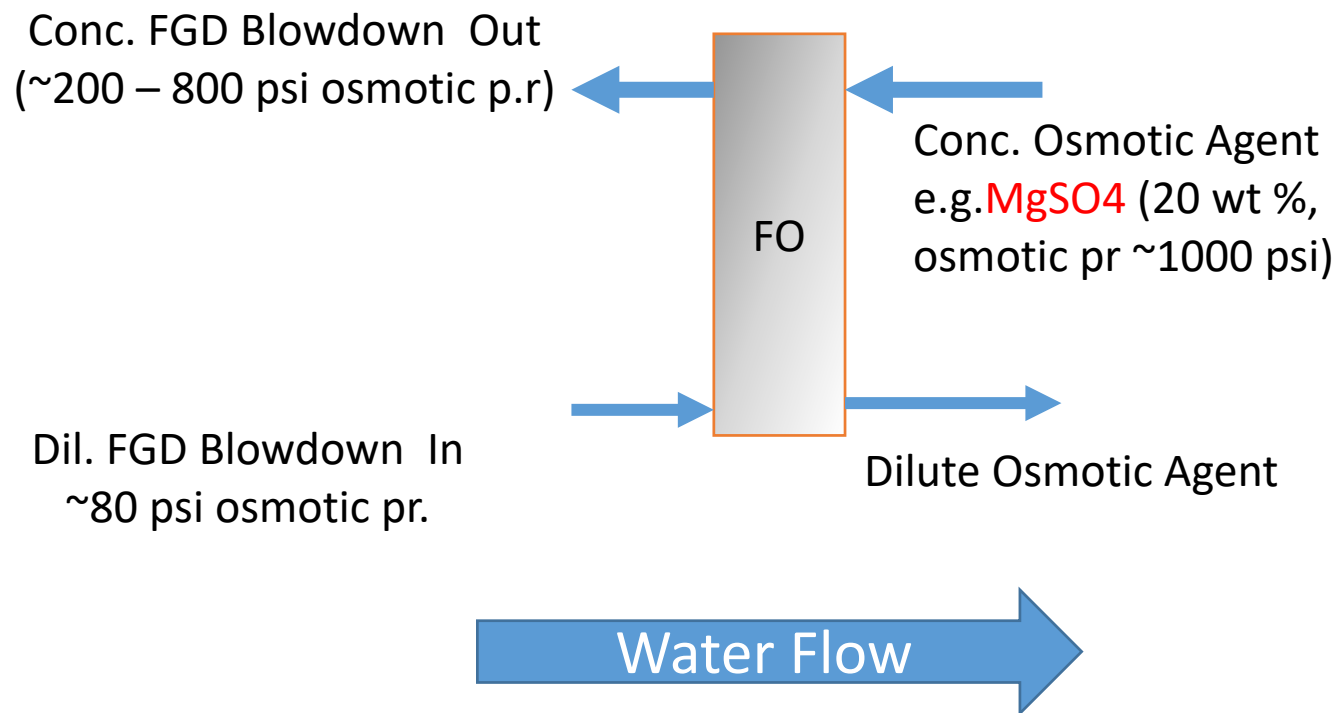
*Next Steps*





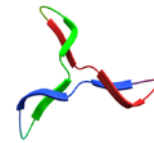
# Aquapod FO Process Principle

## Step 1: Conventional FO Using Inorganic Salt



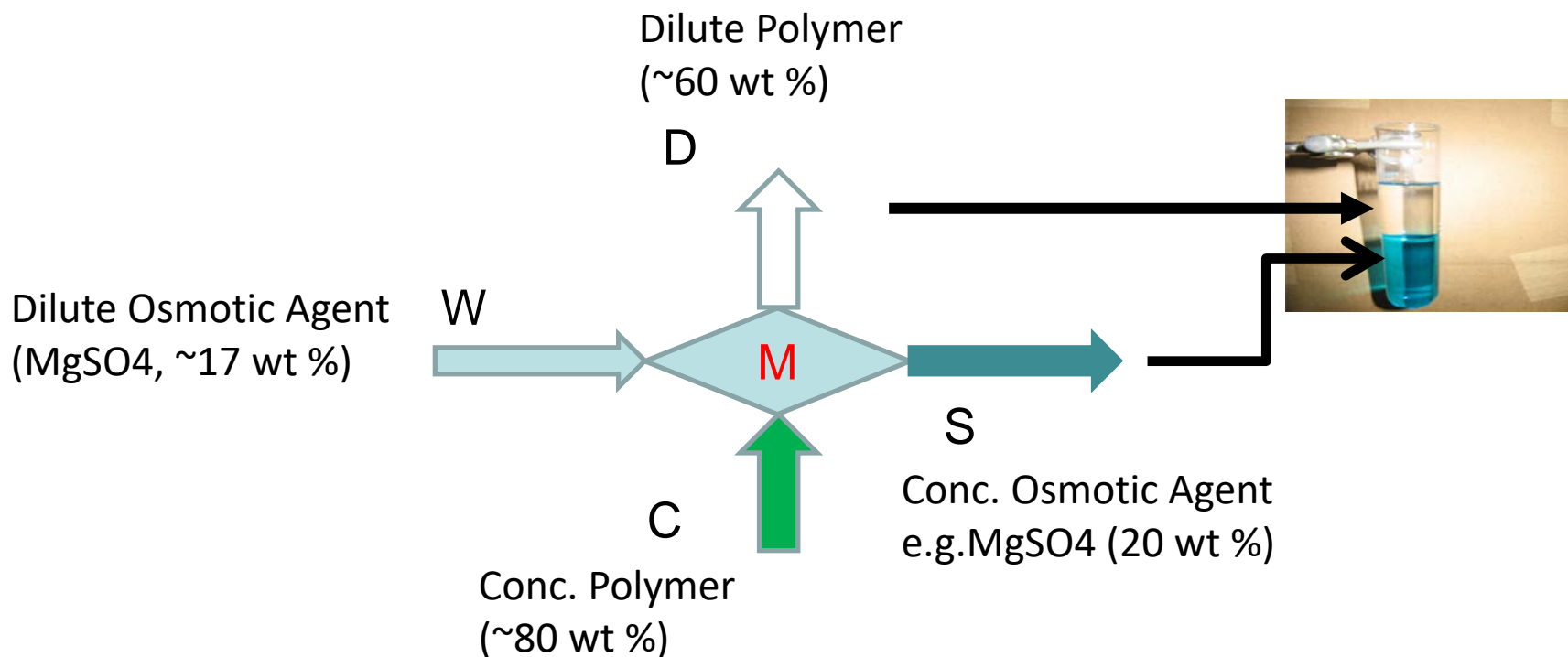
MgSO<sub>4</sub> used as osmotic agent in this project

- Nontoxic
- Noncorrosive
- Adequate osmotic pressure (upto 1800 psi)
- Low reverses salt flux
- Cheap



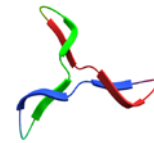
# Aquapod FO Process Principle

## Step 2: Polymer EXTRACTS water from MgSO4 solution



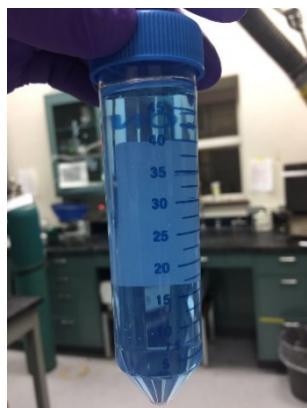
Polymer and MgSO<sub>4</sub> are insoluble  
Form two phases at room temperature

Streams D and S are in chemical equilibrium  
i.e., osmotic pressure of streams are same



# Aquapod FO Process Principle

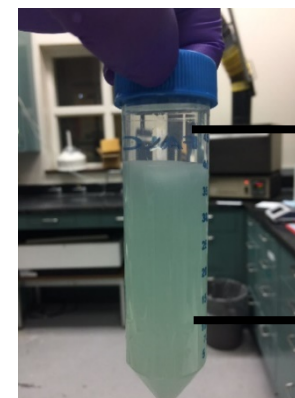
## Step 3: Heat polymer to extract water



Dilute Polymer  
(~60 wt %)



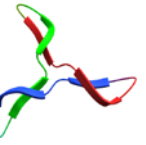
Heat above cloud point  
(e.g., 80 C)



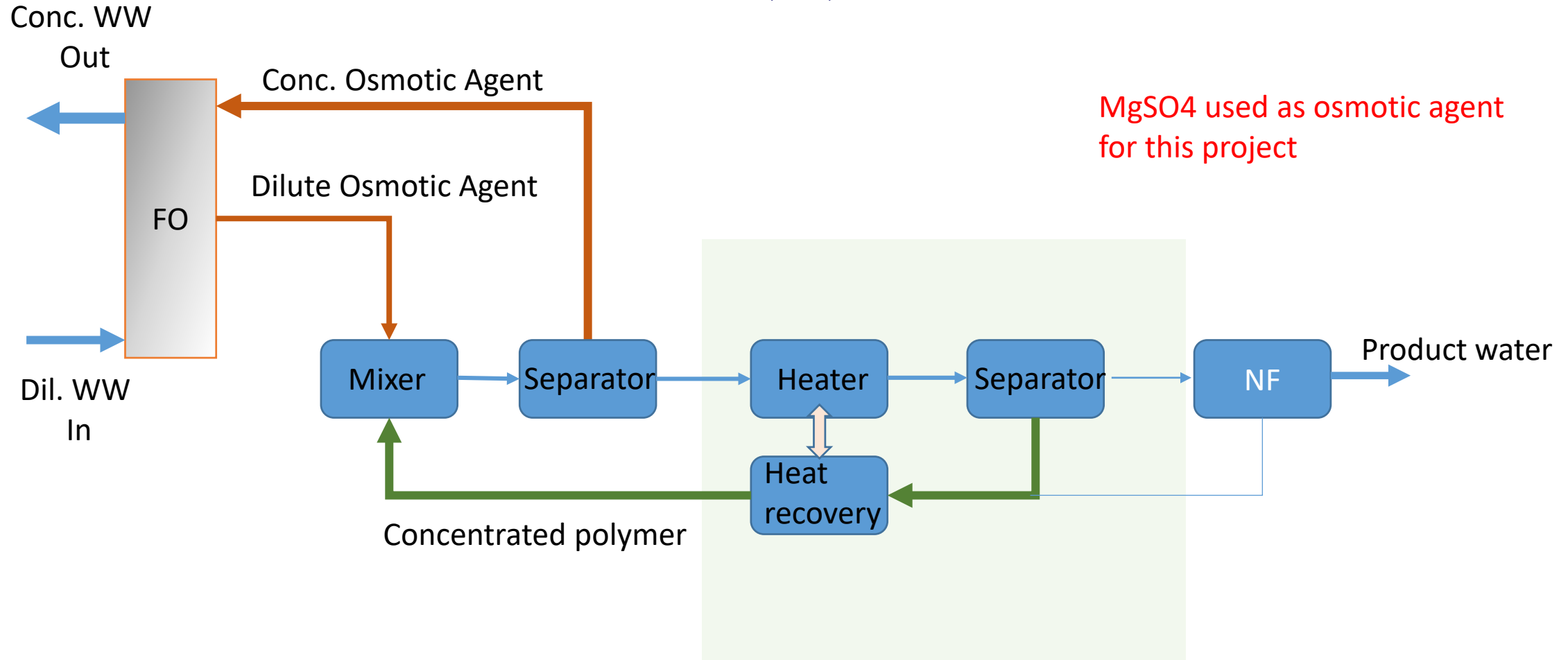
Water

Conc. Polymer  
(~80 wt %)

Concentration of polymer in polymer  
phase is a function of temperature

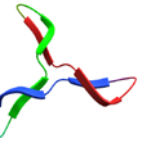


# Aquapod FO Flowsheet 1, 2, 3...



Osmotic Agent Concentration

Polymer Recycle  
Water Recovery



# Section 3

230 MW Coal Fired Power Plant

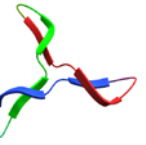
*Aquapod – Working Principle*

*FGD-FO Data*

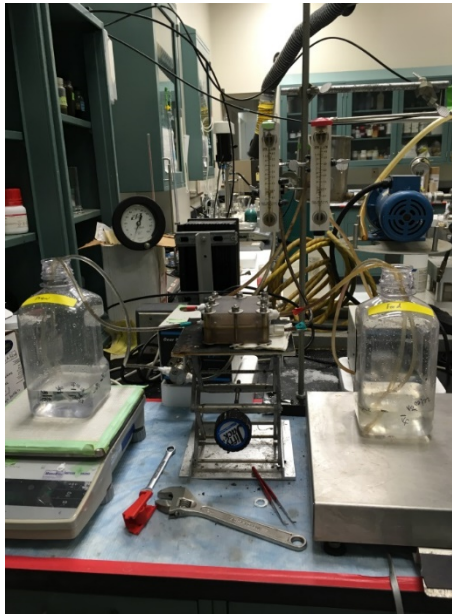
*Salt-Polymer Selection Considerations*

*Summary*

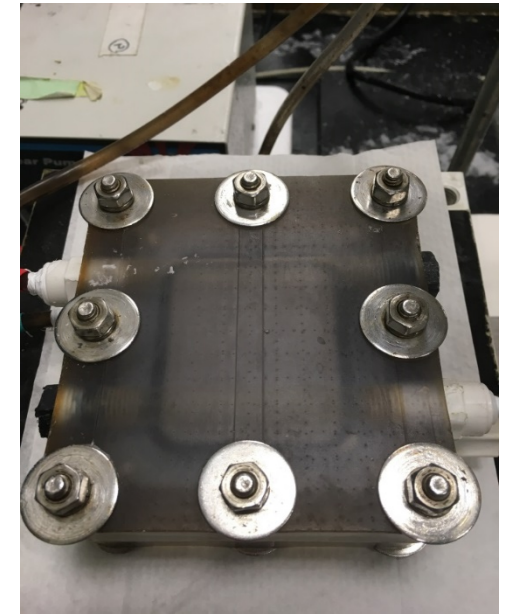
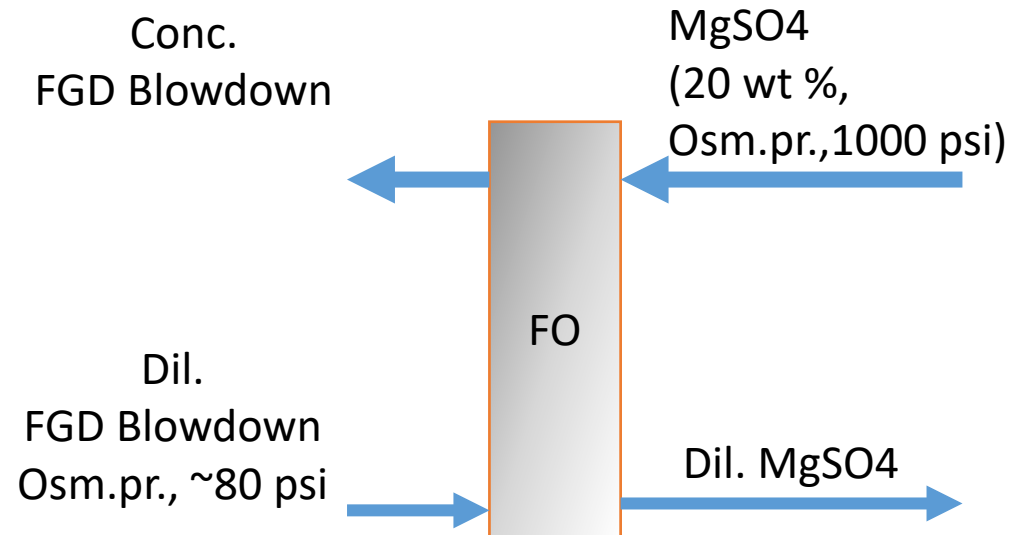
*Next Steps*



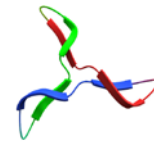
# FGD Blowdown Concentration FO Testing



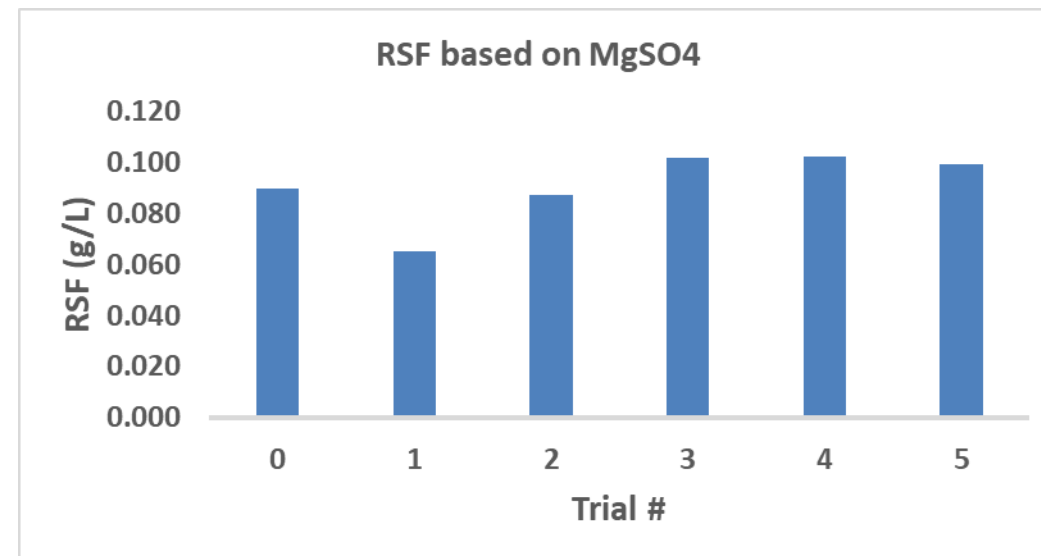
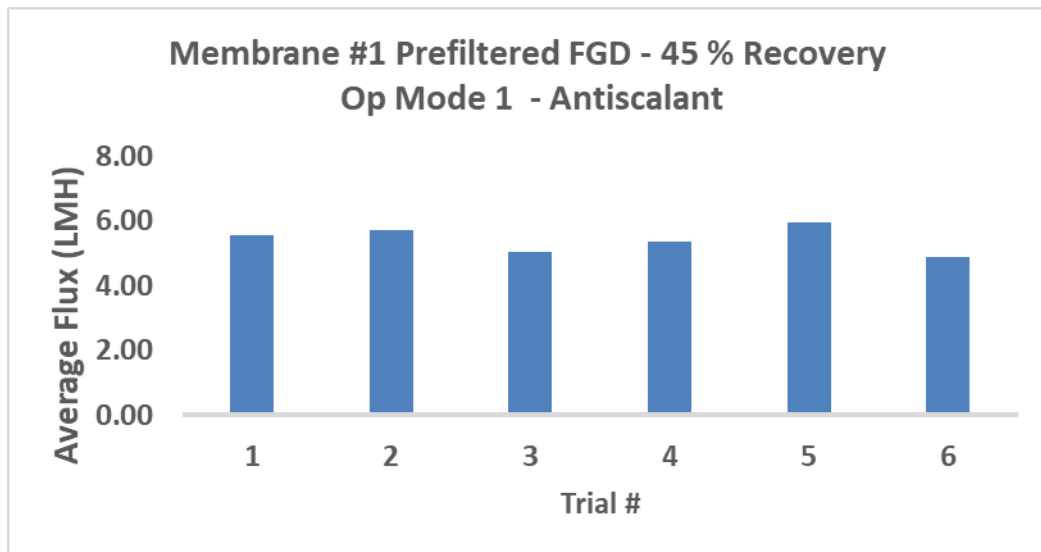
FO Batch  
Testing



Membrane Cell  
0.00266 m<sup>2</sup>



## FGD Blowdown Concentration FO Membrane

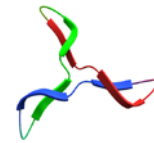


Membrane stable

RSF low

No precipitation of gypsum observed

Prefiltered 0.45 micron  
Antiscalant addition ~4 ppm



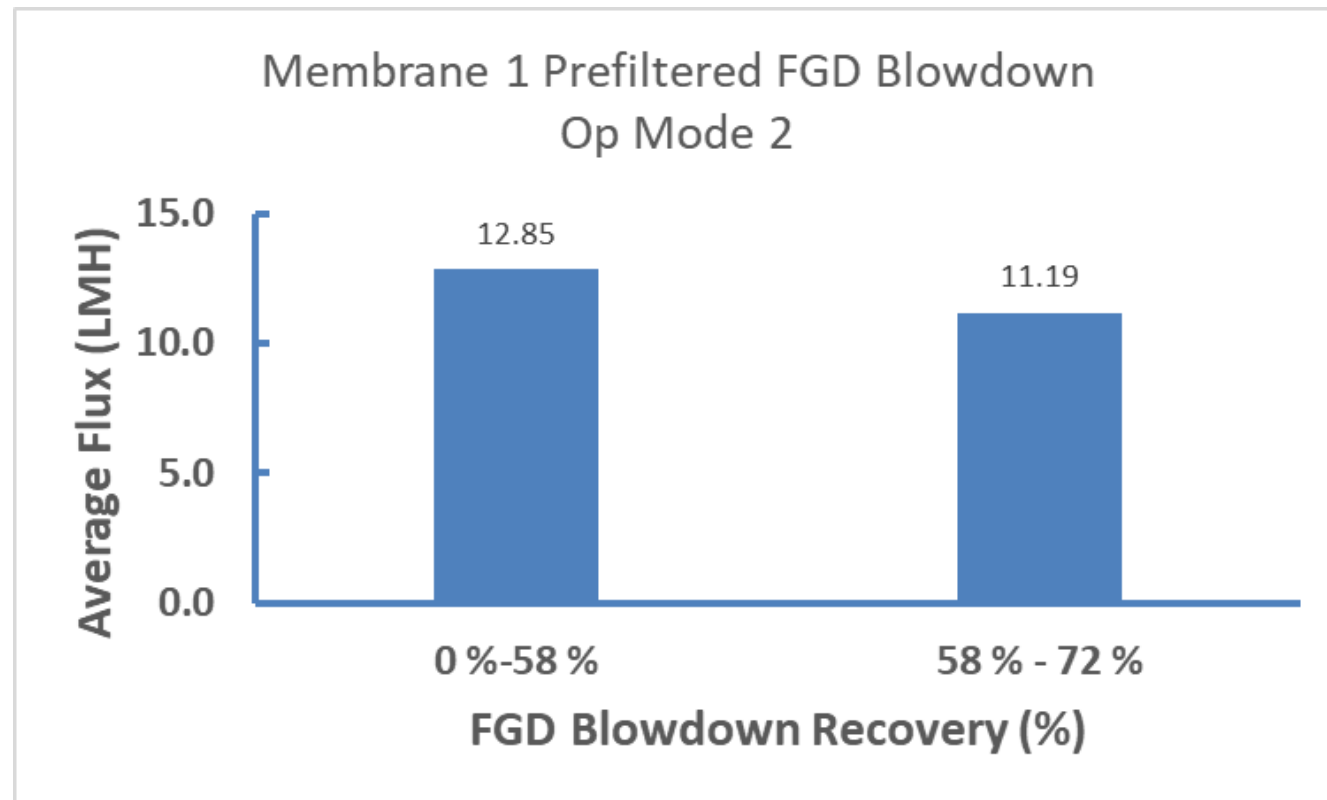
## FGD Blowdown Concentration FO Membrane

75% recovery achievable  
Minimal pretreatment  
No gypsum precipitation  
Future work to target 90% recovery

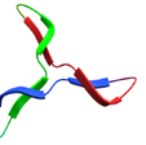
Prefiltered 0.45 micron (gear pump requirement)

Process will use 2-5 micron filtration

Antiscalant addition ~4 ppm







# Section 3

230 MW Coal Fired Power Plant

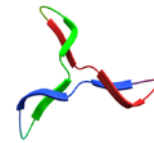
*Aquapod – Working Principle*

*FGD-FO Data*

*Salt-Polymer Selection Considerations*

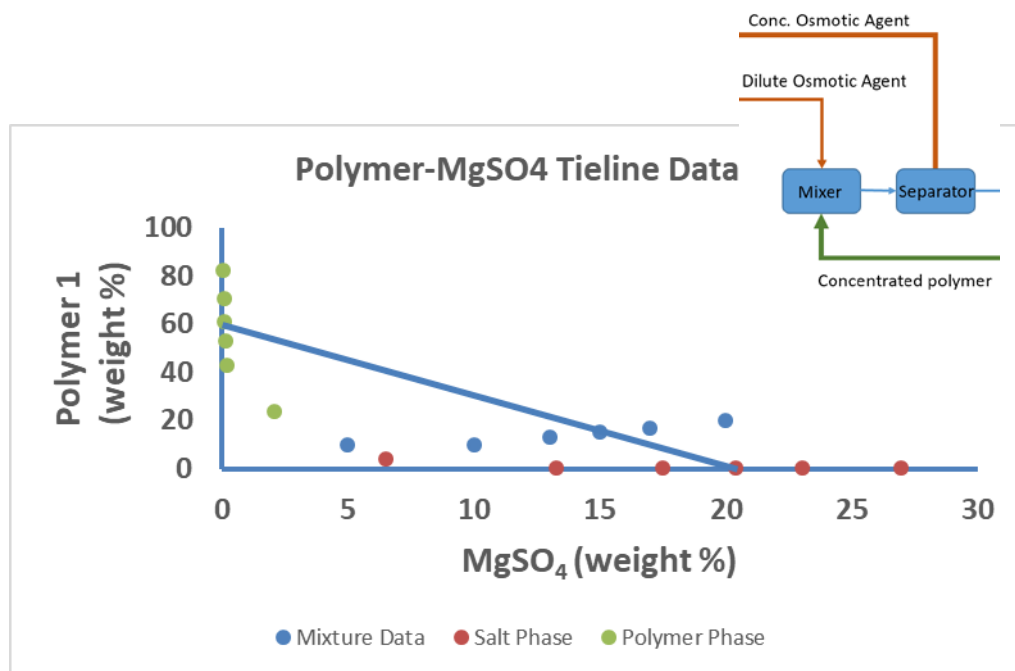
*Summary*

*Next Steps*

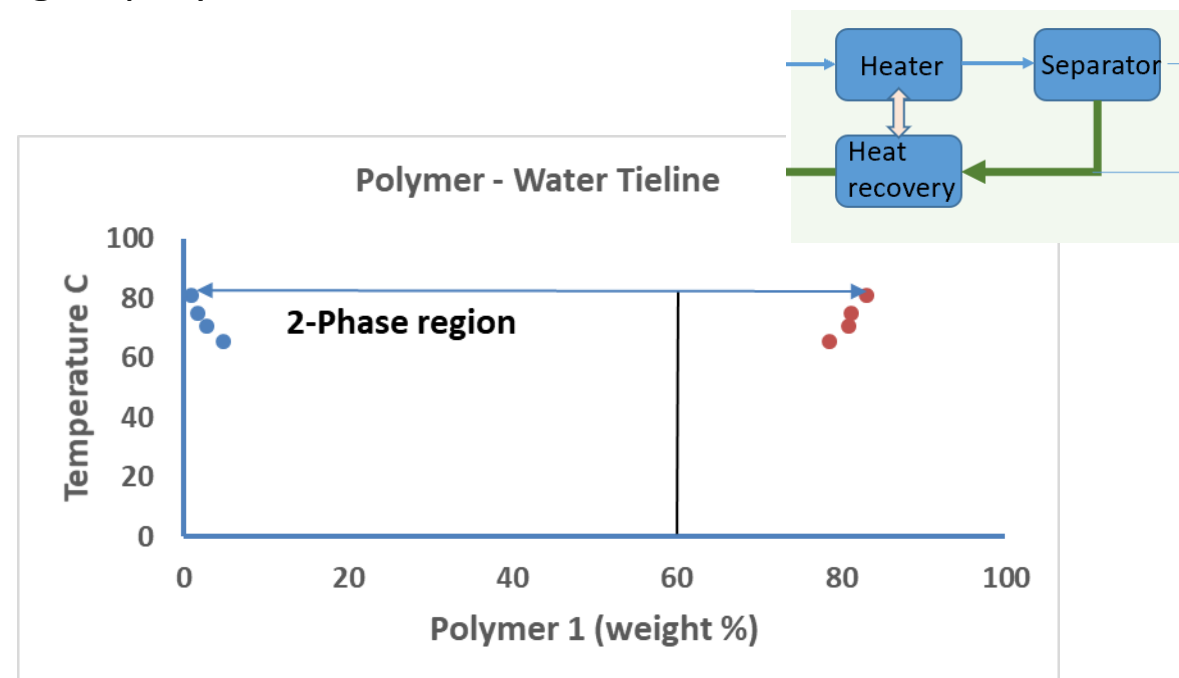


# Polymer Selection Criteria

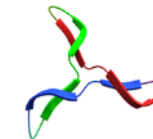
- Polymer ability to extract water from salt solution (MgSO<sub>4</sub>)
  - Required data - salt – polymer tieline data; polymer – water phase diagram as function of temperature - calculate g water extracted/g of polymer



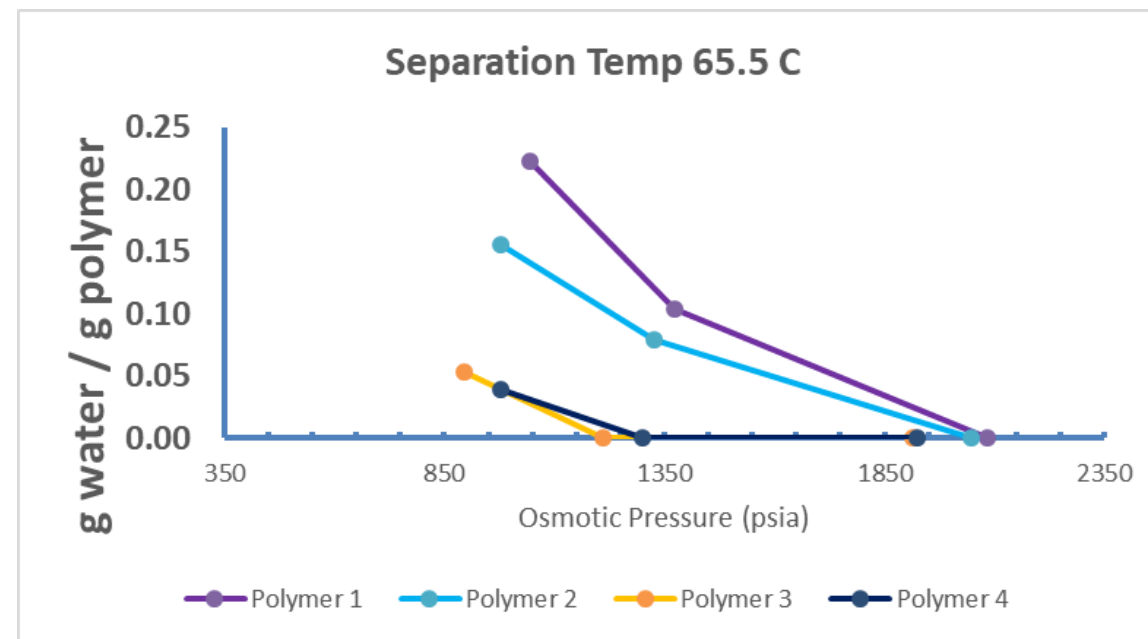
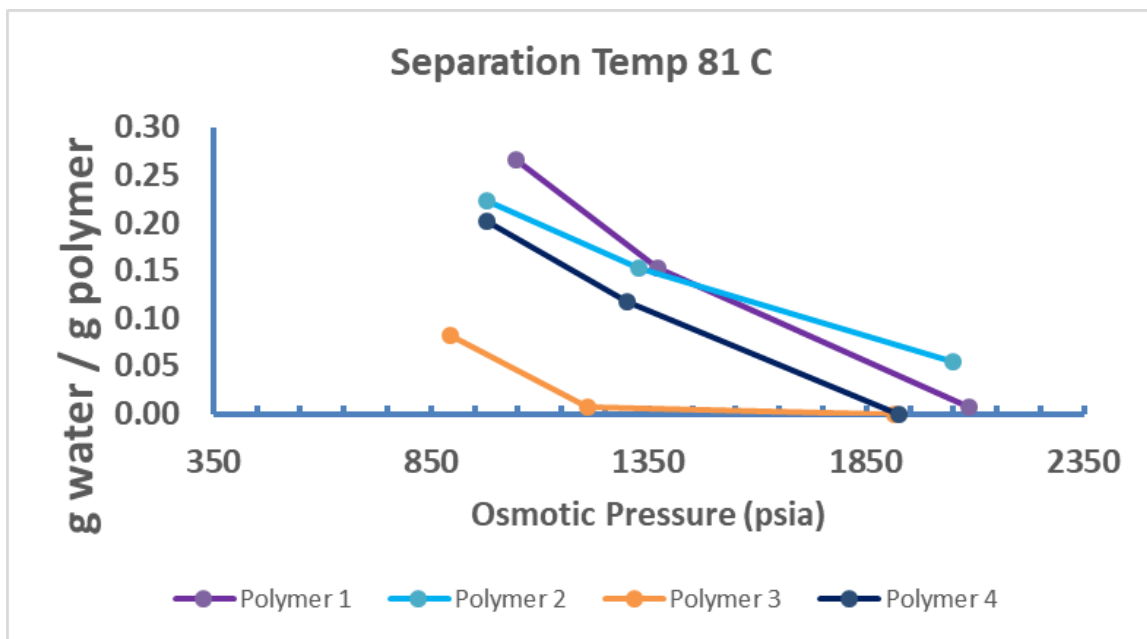
**Step 2**

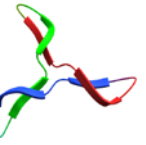


**Step 3**



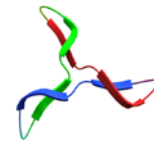
# Water Extraction Capacity of Polymers





# Polymer Selection Criteria

- Polymer – Salt separation kinetics
- Polymer – Water separation kinetics
- Polymer cost
- Polymer stability



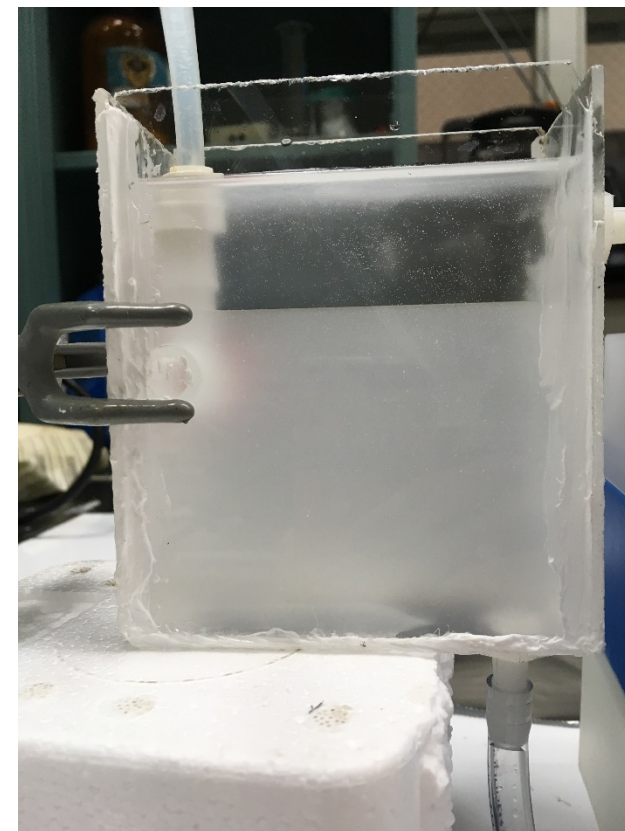
## MgSO<sub>4</sub>-Polymer Separation Kinetics

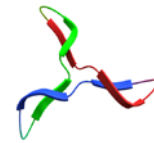
Impeller mixing of all polymers and salt achieves phase equilibrium in <2 minutes

UCON polymer phase separates cleanly in 30 minutes under gravity;

Salt phase hazy with particles of ~10 micron

Ongoing work to lower separation time and reduce carryover in bottom phase;





# Polymer Water Separation Kinetics

- Polymer Water Separation  $\sim 84$  C
  - Polymers 1 and 4 separate readily within 5 minutes for process relevant conditions
  - Polymer 2/3 more difficult
  - Further exploration in scale-up



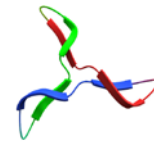
Polymer 1



Polymer 4

Before

<5 min of settling



# Polymer Selection Criteria

## Other Considerations

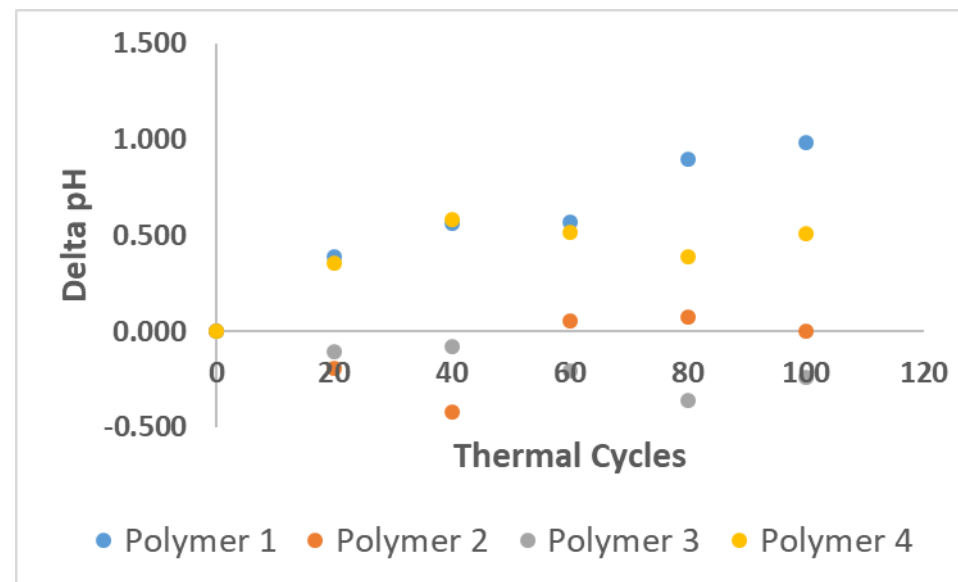
### Cost

Polymer 1~Polymer 4

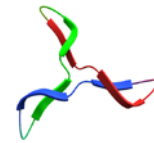
>

Polymer 2~Polymer 3

### Thermal Stability



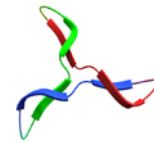
**Polymers 1 & 4 show degradation indicating need for antioxidant stabilizers**



## MgSO<sub>4</sub> – Polymer Pairs

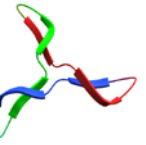
- Four MgSO<sub>4</sub> –polymer pairs identified
- All are able to provide osmotic pressures adequate for >80% recovery of water from FGD wastewater
- Three need a temperature of about 60 - 85 °C – accessible with flue gas;
- Polymer 3 has a low threshold temperature in the vicinity of condenser water temperature (45 ° C) – lower water carrying capacity/g polymer – intriguing possibilities for low TDS, high fouling streams
- Separations of salt-polymer and polymer-water do not seem to present unusual difficulty but will need to be optimized – may need coalescers etc.
- Polymer 1 will be used for scale-up; Polymer 4 is in commercial use; Polymer 2 is backup to polymer 1





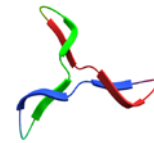
## Summary

- Sufficient waste heat is available within power plant to recover significant amount of water from FGD blowdown using low energy FO.
- 50- 75% recovery water recovery from FGD blowdown has been achieved by FO at this plant **with minimal pretreatment** at small scale with coupons; achieved in short term tests. Next target is 90% recovery.
- Membrane flux is stable and viable at high recoveries;
- Energy target values of <200 kJ/kg and <2 kWh/m<sup>3</sup> achievable based on mass and energy balance, and preliminary PFD.



## Next Steps

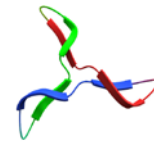
1. Conduct preliminary TEA and identify areas for improvement.
2. Integrate mixing and settling systems for salt-polymer separations.
3. Integrate heating and polymer-water separation units.
4. Test FO modules.
5. Identify residual management options.
6. Complete final TEA.



## Notable Partnerships

- Working closely with FO membrane/equipment vendors, exchanging information, and best practices
- Working with IL Power Plant and leveraging their knowledge base on operation and treatment

***Commercial partners and end-user involvement are critical to advance TRL of technology in subsequent scale-up***



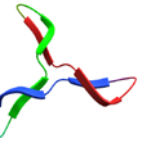
## Acknowledgements

### Project Team

- Mr. P. J. Becker (IL PP)
- Dr. S. Chandrasekaran (Univ of Illinois)
- Ms. Martina del Cerro ((Univ of Illinois)
- Ms. K. Drombowski (Trimeric Corporation)
- Mr. R. McKaskle (Trimeric Corporation)
- Dr. K. C. O'Brien (Univ of Illinois)
- Mr. Vinod Patel (Univ of Illinois)
- Mr. Brandon Powell (IL PP)
- Dr. Xuesong Zhang (Univ of Illinois)

### Project Manager

**Mr. Chuck Miller**  
NETL/USDOE



**THANK YOU**