

Electrogenerative Reactors for Process Intensified Cogeneration Ec Catalytic of Power and Liquid Fuel from Shale Gas **Technologies** Wenyuan Li¹, Ma Liang¹, Xingbo Liu¹, John A. Sofranko², Elena Chung²

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PROJECT OVERVIEW

New technology advances in horizontal drilling and hydraulic fracturing leads to shale gas production in U.S. to significantly increased. Much of the growth in the shale gas has been in "wet" gas, gas that contains significant amount of ethane, propane and other condensable liquids. West Virginia University and EcoCatalytic Technologies, are developing modular solid oxide fuel cell-based electrochemical reactors for the conversion of wet natural gas, specifically ethane, to liquid fuels and electrical power, to enable:

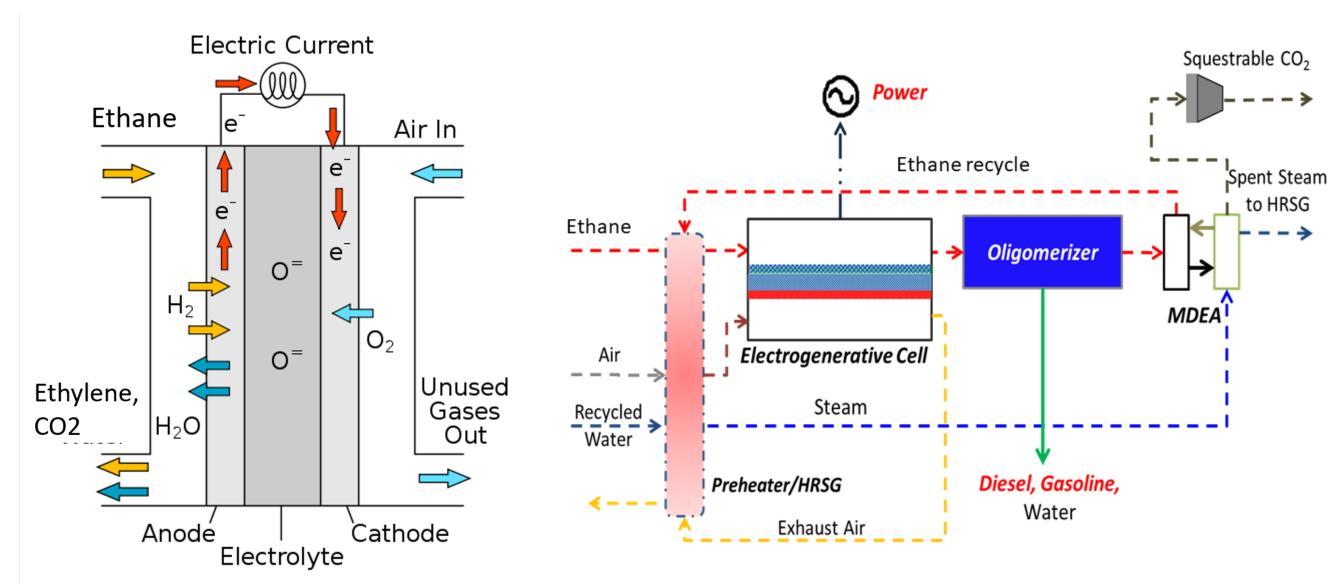
 \succ Lowing the cost of the reactors.

Elimination of need for oxygen separation compared to current gas to liquid facility.

>Cheaper maintenance

Longer service life

NEW APPROACH



Process flow diagram demonstrating that ethane and air are separate in the electrogenearative cell to produce olefins for oligomerization to diesel, gasoline and water. This can be incorporated in a typical with a heat recovery steam generator(HRSG) and amine gas treatment/acid gas removal system such as methyldiethanolamine(MDEA).

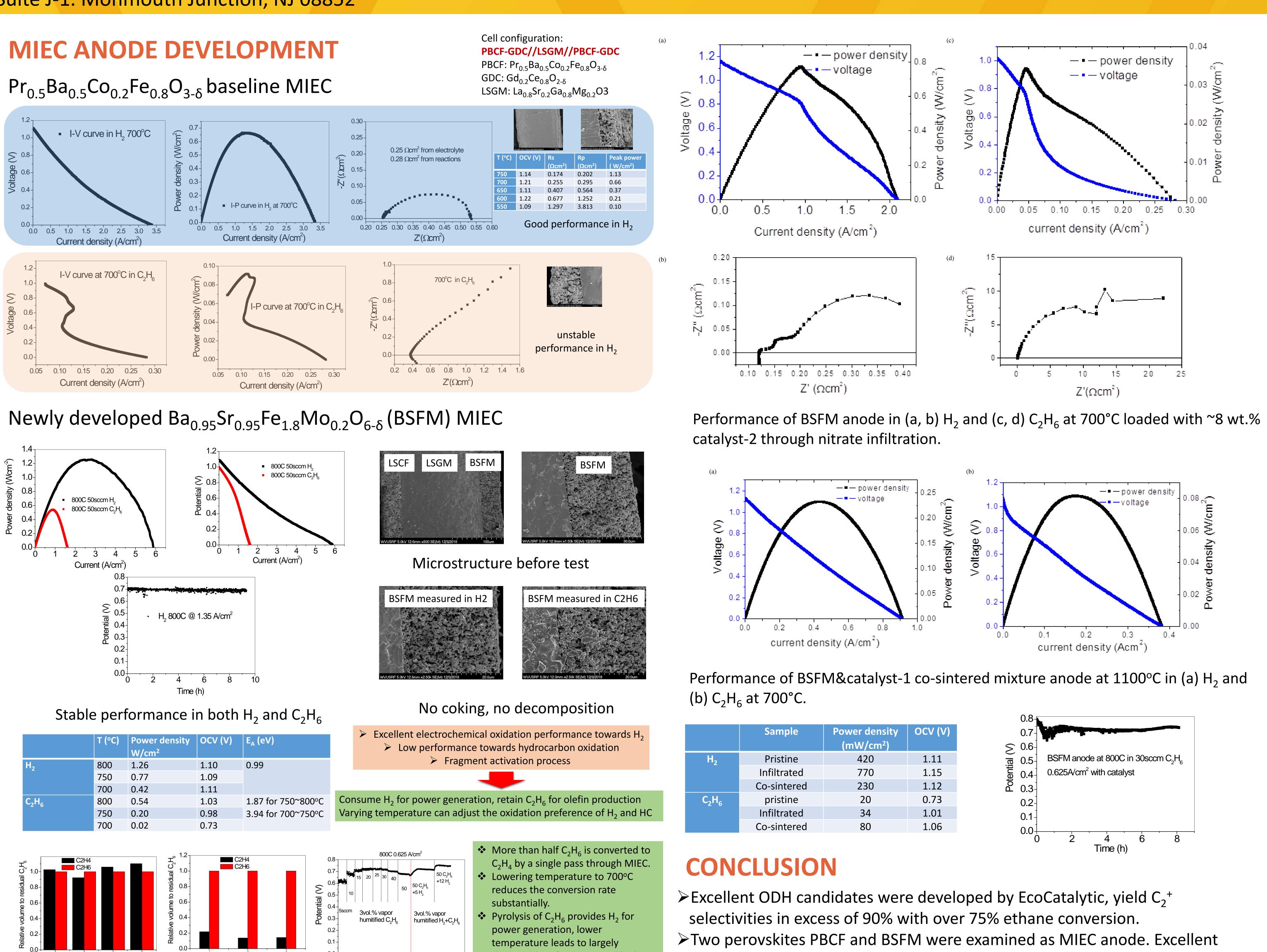
Metal oxide MIEC anode materials (WVU)

 \succ Coking-resistance to operate in ethane

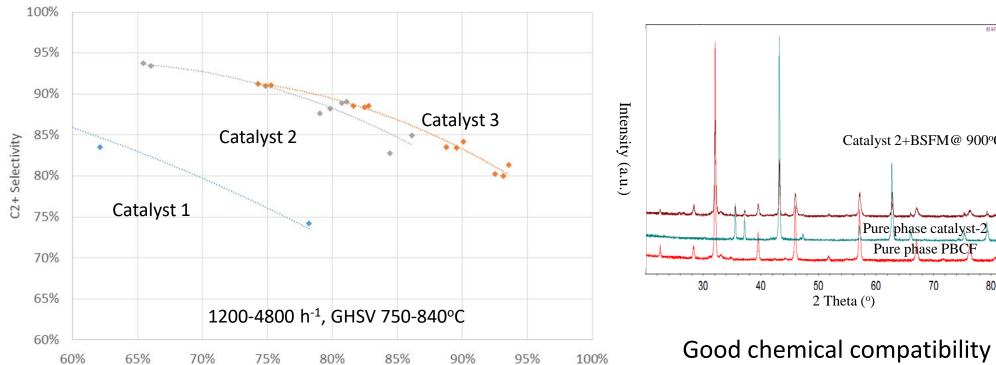
> Fast oxygen conducting to support oxidative dehydrogenation.

> H₂-oxidation preference to generate power and retain olefins production

Oxidative dehydrogenation (ODH) catalyst (EcoCatalytic) \geq High selectivity to desired olefins (ethylene or higher C₂₊) > Tolerance to poisons from the impurity

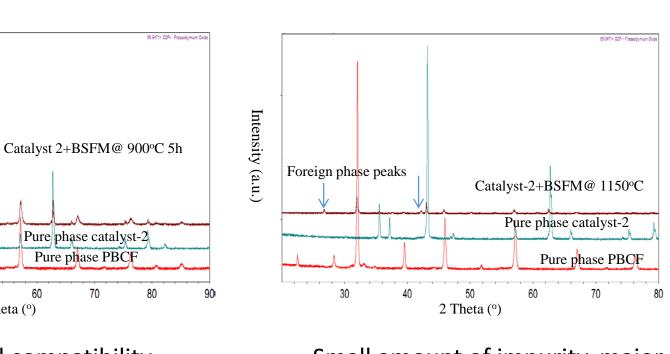


	T (°C)	Power density	OCV (V)	E _A (eV)		> E
		W/cm ²				
H ₂	800	1.26	1.10	0.99		
	750	0.77	1.09			
	700	0.42	1.11			
C ₂ H ₆	800	0.54	1.03	1.87 for 750~800°C		nsume
	750	0.20	0.98	3.94 for 700~750°C	Var	rying t
	700	0.02	0.73			
1.0- 0.8- 0.6- 0.4- 0.2- 0.0 1 2 Cycle of G 800°C s	C measuremen		-	Detential ()	.7 .6 .5 .5 .4 .5 .5 .5 .5 .5 .1 .1 .0 .0 .2	3vol.% humitifi
DDH C 100% 95%	ΆΤΑ	LYST I	LOA	DED CEL	LS	



60 80 100 120 140 160 18 Time (min)

- decreased performance and high apparent activation energy.
- ODH catalyst is needed to promote conversion rate at low temperature



Small amount of impurity, major

	Sample	Power (mW
H ₂	Pristine	4
	Infiltrated	7
	Co-sintered	2
C_2H_6	pristine	2
	Infiltrated	3
	Co-sintered	8

- W/cm² at 800°C.
- effectiveness of such electrode structure.

performance in H₂ was obtained in both recipes, power density as high as 1.26

>Two strategies, nitrate infiltration and powder physical mixing, were carried out to load the catalyst-2 to the BSFM anode. Both methods improved the performance in C_2H_6 operation. The infiltration method limited the maximum loading to only ~8 wt.% to this pre-established BSFM backbone. Due to the access to oxygen in this interconnected BSFM-catalyst-2 network, the cosintered sample improved the performance in C₂H₆ 4 times, proving the

To further improve the performance towards power, liquid fuel cogeneration from C₂H₆, the microstructure and the composition of the BSFM-LMMO co-