

# Degradation and Performance Studies of ALD Stabilized SOFC Nano-Composite Cathodes (NCCs) 18 Month Update

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Funded by the Department of Energy Solid Oxide Fuel Cell Core Technology Program through Agreement Number DE-FE0031672

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May 1, 2019





# High Performance Circuit Pastes for Solid Oxide Fuel Cell Applications

# 6 Month Update

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Program Manager: Venkat Venkatraman





# **TALK Outline**

#### **ALD-Stabilized Nano-Composite Cathodes**

- 1. Motivation
- 2. Experimental Methods
- 3. Results and Discussion

#### **Ni-Ag Circuits Pastes**

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#### Motivation for MIEC on IC Nano-Composite SOFC Cathodes SOFC Cathode Reaction: 1/20 + 2e-+ V \*\* = O



Material	Oxygen Surface Exchange Coefficient (k)	Bulk Oxygen Ion Diffusivity (D)	Electronic Conductivity $(\sigma_e)$
Mixed Ionic Electronic Conductor (MIEC)	High	Low	High
Ionic Conductor (IC)	Low	High	Low

Burye and Nicholas, J Power Sources, 276, 54-61 (2015)

#### Standard Nano-Composite Cathode Fabrication



Burye & Nicholas, J Power Sources, 301, 287-298 (2016)

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Burye and Nicholas, J Power Sources, 276, 54-61 (2015)

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#### GDC Pre-Infiltrated Nano-Composite Cathode Fabrication



Burye and Nicholas, J Power Sources, 300, 402-412 (2015)

#### Nano-Composite Cathode Fabrication With Ceria Pre-infiltration

Uninfiltrated Surface



Ceria Pre-Infiltrated Surface





Ceria and LSCF Infiltrated Surface





Burye and Nicholas, J Power Sources, 300, 402-412 (2015)

#### Standard LSCF-GDC Shows Decent Performance and GDC Pre-Infiltration Decreases Cathode Resistance



#### Uncoated GDC Pre-Infiltrated LSCF-GDC Cells Have Stability Problems at 550°C Under Open Circuit Conditions



Burye and Nicholas, J Power Sources, 300, 402-412 (2015)

### ZrO<sub>2</sub> Thin Film Deposited by ALD Could Greatly Improve the Stability of SOFC NCCs



 $LSC (La_{0.6}Sr_{0.4}CoO_{3-\delta}) \text{ nanoparticles supported on a porous } LSGM (La_{0.8}Sr_{0.2}Ga_{0.83}Mg_{0.17}O_{3-\delta}) \text{ scaffold } Sr_{0.4}CoO_{3-\delta}) \text{ scaffold } Sr_{0.4}CoO_{3-\delta} \text{ and } Sr_{0.4}COO_$ 

The Morphology of the ALD Coatings Grown by the Huang Group is More Porous than the Dense Conformal Coatings Reported by Other Groups



Gong et al, Chem. Materials, 25, 4224 (2013)





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#### ZrO<sub>2</sub> Coated Nano-Composite Cathode Fabrication



#### Gold Current Collector Grids with Platinum Plate Push-Contacts were Used for the Measurements Here



### Silver Current Collectors Result in Strange, Unreproducible $R_p$ Behavior at Elevated Temperatures



#### Silver Should NOT Be Used as Current Collector Because of Its Migration at Elevated Temperature







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#### ZrO<sub>2</sub> Overcoat Maintained Conformal Target Thickness After 1000 Hours at 650°C



Tested cell with  $3nm ZrO_2$  overcoat (actual thickness ~3.2nm)



Tested cell with  $5nm ZrO_2$  overcoat (actual thickness ~5.3nm)

#### 1-10 nm Thick Zirconia Overcoats Don't Dramatically Affect Conventional LSCF-GDC NCC Performance



#### 1-10 nm Thick Zirconia Overcoats Don't Dramatically Affect **Conventional LSCF-GDC NCC Performance**

 $Z^{\prime\prime}$  ( $\Omega cm^2$ )

 $Z^{n}$  ( $\Omega cm^{2}$ )



2nm ZrO<sub>2</sub> coated LSCF-GDC



-Z" ( $\Omega cm^2$ )

0.25 0.06 600°C 700°C 500°C 0.80 0.74 0 1.20 1.45 0+2.63.6  $Z'(\Omega cm^2)$ 5nm ZrO<sub>2</sub> coated LSCF-GDC 0.25 0.06 600°C 500°C 700°C 0.87 0.93 1.65 0 + 2.8

 $Z'(\Omega cm^2)$ 

1nm ZrO<sub>2</sub> coated LSCF-GDC

3.8

#### Thicker Zirconia Overcoats Result in Lower 650°C **Rp** Degradation Rates



5nm ZrO<sub>2</sub> coated 12% LSCF

 $18\% (0.015 \Omega cm^2/khrs)$ 12% (0.011 $\Omega$ cm<sup>2</sup>/khrs)

6.3%

#### Independent 650°C Degradation Tests at the University of South Carolina Showed Similar Results



#### No Obvious Particle Coarsening Was Observed for All Cells after 1000h Degradation at 650°C



As-produced 12% standard LSCF-GDC NCC



12% standard LSCF-GDC NCC after 1000h at 650°C



1nm ZrO<sub>2</sub> coated 12% standard LSCF-GDC NCC after 1000h at <u>650°C</u>



2nm ZrO<sub>2</sub> coated 12% standard LSCF-GDC NCC after 1000h at 650°C



 $5nm ZrO_2$  coated 12% standard LSCF-GDC NCC after 1000h at 650°C

## Suppression of Sr Segregation Is Suspected to Contribute to the LSCF-GDC NCC Performance Improvement with ZrO<sub>2</sub> Overcoat



#### XPS Deconvolution Suggests There is Not Much Change in the Partition Between Sr Surface Sites with ALD Overcoat



Using Peak Assignments found in Crumlin, Ethan J., et al. Energy & Environmental Science 5.3 (2012)

### R<sub>p</sub> Improvement in the Low Temperature Region Was Observed for Coated GDC Pre-infiltrated LSCF-GDC NCCs



#### 5nm ZrO<sub>2</sub> Coated 7.5% GDC Pre-infiltrated 12% LSCF Showed *Rp* Degradation Rates of ~22%/khrs









1.  $ZrO_2$  ALD overcoats of 1-5 nm in thickness improved the long-term stability of standard LSCF-GDC NCCs without significantly altering the 400-700°C LSCF-GDC  $R_p$ .

2. A possible reason for the improved  $R_p$  is Sr surface segregation alterations induced by the zirconia overcoat.

3. ALD overcoats reduced the activation energy for oxygen incorporation into the GDC-preinfiltrated LSFC-GDC NCCs.

4. Although the results are promising, more work is needed to realize cathode degradation rates meeting DOE targets of <1%/khrs.





# High Performance Circuit Pastes for Solid Oxide Fuel Cell Applications

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# ALK Outline

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#### **Conventional Silver-Copper Oxide Reactive Air Brazes Have many Benefits**



- Brazes are less Permeable to H<sub>2</sub> and O<sub>2</sub> than Glass Seals
- Brazes are more ductile than glass seals, so CTE Mismatch
   is not a concern
- Reactive air brazing can be performed in air
- The enhanced wetting provided by CuO allows Ag-CuO brazes to be used on a variety of ceramics



Delphi Technologies Inc, U.S. Patent No US7855030B2

Kim, J.Y., J.S. Hardy, and K.S. Weil, Journal of the American Ceramic Society, 2005. 88 (9): p. 2521-2527.

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G18

Air

Cathode

Air

Air

#### **Reactive Air Brazes Have Several Fatal Flaws**

ALO.

Air

t~50 µm

Ferritic Stainless Steel Picture Frame

Ag-CuO Braze

- 1. Braze joint will be exposed to dual atmospheres ( $H_2$ /Air) in SOFC operation.
- 2. Reactive air silver brazes are only partially wetting, resulting in occasional manufacturing defects (**Type I Pores**);
- 3. Reduction of reactive air additions (CuO) by hydrogen during SOFC operation can result in **Type II Pores;**
- 4. Type III pore formation due to  $H_2$  and  $O_2$  reaction. CuO additions do not prevent the formation of Type III Pores produced when hydrogen and oxygen dissolved in the braze meet and form water pockets.

~ 4 mm H. Yttria Stabilized Zirconia Mechanically Supporting Anode H, H, H, b) Ag-CuO Braze Pore Top-view ~ 4 mm Ag-8CuO Window sheet Cell 100 µm

Image b) Courtesy of Delphi Automotive.

Bause, T., et al., Damage and Failure of Silver Based Ceramic/Metal Joints for SOFC Stacks. Fuel Cells, 2013. 13 (4): p. 578-583.

#### Dense Braze Joints Can be Produced and the Porous Nickel Layer is Transient



Zhou, Q., T. R. Bieler and J. D. Nicholas. "Transient Porous Nickel Interlayers for Improved Silver-Based Solid Oxide Fuel Cell Brazes." *Acta Materialia* 148: 156-162, http://dx.doi.org/10.1016/j.actamat.2018.01.061 (2018)

# Ag-Ni Brazes Show Superior Dual Atmosphere tolerance After 300 hrs of Isothermal 750°C Aging,

or 300 25°C/min 35-830°C Rapid Thermal Cycles



*Zhou et al.*, Dual Atmosphere Isothermal Aging and Rapid Thermal Cycling of Ag-Ni and Ag-CuO Stainless Steel to Zirconia Braze Joints, Intl. J. Hydrogen Energy, Submitted (2019).



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## The Controlled Wetting and Spreading of Ag can be used for High Temp Semiconductors, **High Power SOFCs, Etc.** As-printed As-fabricated Air/850°C,5 hrs 1 mm 1 mm 1 mm ~556 µm ~551 µm 100 µm 100 µm 100 µm

Zhou et al., Controlled Wetting and Spreading of Metals on Substrates Using Porous Interlayers and Related Articles, USPTO Provisional Patent (Submitted April 17, 2018) Zhou et al., Controlled Wetting and Spreading of Ag on Various Ceramic Substrates with Porous Ni Interlayers, Scr. Mater, 2018. (In Preparation) 37

#### Molten Ag Will Also Infiltrate and Spread Through a Contiguous Ni Pattern



Zhou et al., Controlled Wetting and Spreading of Metals on Substrates Using Porous Interlayers and Related Articles, USPTO Provisional Patent (Submitted April 17, 2018)

Zhou et al., Controlled Wetting and Spreading of Ag on Various Ceramic Substrates with Porous Ni Interlayers, Scr. Mater, 2018. (In Preparation)

#### The Electrical and Adhesion properties of Ag-Ni Circuit Pastes are Being Compared to Conventional Circuit Pastes



Screen printed samples for sheet resistance measurements

Following Manufacturer Suggested fabrication Procedures Results in Heraeus C870 Circuits that are delaminated, DAD-87 Circuits that are Nanoporous, and Ag-Ni Circuits that are Dense and Well Adhered



#### The Ag-Ni Circuits Have a Resistivity Close to that of Pure Silver, as Expected



Matula, R.A., Electrical resistivity of copper, gold, palladium, and silver, J. Phys. Chem. Ref. Data, 1979. 8(4): p. 1147-1298. Lide, D.R., CRC Handbook of Chemistry and Physics, Internet Version. 2005: CRC Press, Boca Raton, FL.

10 Hours of 750°c Isothermal Aging Produces Dense, partially delaminated Heraeus C8710 Porous, Well-Adhered DAD-87, and Dense, Well-adhered Ag-Ni with lots of Brittle NiO











1. Conventional silver circuit pastes have significant delamination and/or conductivity problems

2. Ag-Ni circuits are one of the few ways to make dense, thick-film, well-bonded, low resistivity circuits for SOFCs, power electronics and other applications.

3. Techniques to eliminate NiO is needed in Ag-Ni circuits

## **Backup Slides**



Voltage, U

Two layers Pure silver and silver-nickel mixture

Current, I

*I*, current through the circuit cross section *U*, voltage between two ends *R*, resistance *ρ*, resistivity *A*, area *l*, length *f*, area fraction

 $R = \rho \frac{\iota}{A}$  $I = U(\frac{1}{R_{Ag}} + \frac{1}{R_{Ni}})$  $\frac{1}{R_{mix}} = \frac{1}{R_{Ag}} + \frac{1}{R_{Ni}}$  $\frac{A}{\rho_{mix}l} = \frac{f_{Ag}A}{\rho_{Ag}l} + \frac{f_{Ni}A}{\rho_{Ni}l}$  $\frac{1}{\rho_{mix}} = \frac{f_{Ag}}{\rho_{Ag}} + \frac{f_{Ni}}{\rho_{Ni}}$ 



Two layers Pure silver and silver-nickel mixture

 $R = \rho \frac{l}{A}$ 

#### Current, I

I, current through the<br/>circuit cross sectionU, voltage between twoendsR, resistance $\rho_{mix}$  $\rho$ , resistivityA, areal, lengthf, area fraction

 $U = IR_{Ag} + IR_{Ni}$ 

 $R_{mix} = R_{Ag} + R_{Ni}$ 

$$\rho_{mix}\frac{l}{A} = \rho_{Ag}\frac{lf_{Ag}}{A} + \rho_{Ni}\frac{lf_{Ni}}{A}$$

$$\rho_{mix} = \rho_{Ag} f_{Ag} + \rho_{Ni} f_{Ni}$$

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Overall circuit minimum case

Overall circuit maximum case

Two layers Pure silver and silver-nickel mixture

$$\frac{1}{\rho_{overall}} = \frac{f_{Ag}f_{mix}}{\rho_{Ag}} + \frac{f_{Ni}f_{mix}}{\rho_{Ni}} + \frac{f_{pure}}{\rho_{Ag}}$$

$$\frac{1}{\rho_{overall}} = \frac{f_{mix}}{\rho_{Ag}f_{Ag} + \rho_{Ni}f_{Ni}} + \frac{f_{pure}}{\rho_{Ag}}$$

#### **Ni Particles Improve Ag Wetting on YSZ**



#### Ag on bare YSZ



#### Ag on YSZ with Ni particles



In calculation, area fraction is transformed to atomic fraction.



Explanation for deviation of theory: the fractions of Ag and Ni are measured in local areas, different from the overall relationship between Ag-Ni in the circuit.

R<sub>p</sub> for Infiltrated Co<sub>3</sub>O<sub>4</sub>-GDC Is Not Satisfactory



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#### Anode NiO Infiltration Saw an Improvement in I-V Performance for LSCF-GDC NCC/YSZ/Ni-YSZ



#### 12% LSCF-GDC NCC/YSZ/Ni-YSZ

12% LSCF-GDC NCC/YSZ/Ni-YSZ with ~8% NiO anode infiltration

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