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Barium Sources in Hydraulic Fracturing Systems and Chemical Controls on its Release into Solution

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Abstract

Barite scale in hydraulic fracturing systems is a significant issue for overall oil/gas production. Though it has long been assumed that the Ba necessary for scale formation is derived from the host rock, another potential and possibly dominant source often overlooked is Ba-rich drilling mud often used in these systems. Because drilling mud contains barite concentrations that are two orders of magnitude greater than Ba-rich oil/gas shales (20-60 wt.% in drilling mud versus ~1,000 mg/kg in Ba-rich shales), it is important to determine the potential of drilling mud as a source of both barium and sulfate in hydraulic fracturing systems. In order to assess the validity of drilling mud being a major/primary Ba source, the stability of barite in drilling mud needs to be tested. A series of leaching experiments on pure barite and Ba-rich drilling mud were conducted under a variety of pH's and ionic strengths as well as in the presence of a wide variety of organics common in fracture fluid systems (additives, formation water, produced water) and compared to Ba release from four different oil/gas shale plays.

In experiments where Ba was leached from various oil/gas shales, the total amount of Ba released (< 50% of total Ba) resulted in aqueous Ba concentrations far below levels commonly measured in produced water. Conversely, the leaching experiment using pure barite and more importantly the drilling mud resulted in significant releases of Ba under system-relevant conditions (low initial pH). In these experimental systems the resulting Ba concentrations were closer to those in produced waters. Drilling mud reacted with 15% HCl (similar to that used in the initial acid slug) released > 18% of the total Ba in the drilling mud (20-60 wt.%) over a 72-hour interval. It was found that under most chemical conditions the barite contained in the drilling mud is less stable compared to pure barite, suggesting that drilling mud used in unconventionals is a primary source of Ba in these systems. Because barite is less stable at low pH and high ionic strength, as injected acid is neutralized by the shale (during which both pH and ionic strength increase), a window of time where barite precipitation will occur due to the Ba and SO₄ released from the drilling mud and transported into the newly formed fractures prior to cessation of precipitation due to I.S. increasing to over 1 M. This new scale precipitation will potentially close portions of the newly formed secondary porosity. Based on this work, we propose a new conceptual model for Ba cycling in hydraulic fracturing systems in which drilling mud is an important Ba source resulting in self-inflicted formation damage.

Introduction

In unconventional oil/gas extraction, Ba, both in produced water and as barite scale, is a known problem¹⁻⁵. Over the decades research regarding Ba in conventional and unconventional systems have focused on mitigation of barite scale⁶⁻¹¹. In the case of shale, scale damage is particularly deleterious because it occurs in pore spaces and microfractures within the shale matrix¹², permanently destroying production. By neglecting the source of the Ba in unconventional systems, developing effective new Ba scale mitigation methods becomes more difficult. The main research into the source of Ba in these systems was done by Renock et al., who focused on Ba in formation water and leaching from the shale¹³. They found that the majority (> 60%) of the Ba contained in the rock was inaccessible to chemicals commonly found in hydraulic fracturing system (the majority of Ba required a hydrofluoric acid extraction)¹³. Though Renock et al. indicated that high ionic strength (I.S.) along with reducing conditions can extract Ba from the rock, low pH with lower initial I.S. which occurs at the beginning of fluid injection was not investigated¹³. Other researchers have also tested the leachability of Ba from shale samples and found that a significant amount of Ba in the rock is stable unless extremely harsh chemical extractants not found in unconventional extraction are used^{9, 14}. Besides Ba release from the general shale matrix (small barite grains, associated with pyrite, bound to clays, etc.), there is the potential, albeit less probable, Ba release from nearly pure barite nodules/lenses that are sometimes found in shales¹⁵. Though barite lenses have the potential for providing large quantities of Ba to injected fluids during injection, shut-in, and production, the probability of tapping into these Ba sources across numerous wells in the same play, as well as different plays in order to produce the highly consistent Ba concentrations in produced water, > 1000 mg/L Ba, is highly unlikely.

Besides the source rock being a source of Ba in a hydraulic fracturing system, another possible source is drilling mud, which contains barite at concentrations ranging from 20 to 60 wt.%. Though barite laden drilling mud is widely used throughout the conventional and unconventional industries, there has been little research into the stability of the Ba in these materials¹⁶⁻¹⁸. The most robust study, from the 1980's, focused on the bioavailability of the overall drilling mud has focused on conventional oil/gas exploration, which differs significantly from hydraulic fracturing systems where chemicals are injected into the subsurface allowing them to interact/react with drilling mud leftover in the system. Because of the injection process for hydraulic fracturing, the drilling mud and shale experience a wide range of pH, I.S., metal leaching, and long fluid residence times that need to be addressed.

There currently is no major study on the stability of drilling mud in a hydraulic fracturing system. In order to determine if Ba-rich drilling mud is a major source of Ba in hydraulic fracturing systems, a series of Ba-leaching experiments were performed in this study to assess the stability of Ba in drilling mud. The experiments reported here were compared to leaching experiments of four oil/gas shales and pure barite crystals. Besides identifying the likely Ba source in these systems, a variety of chemical treatments, both inorganic parameters (pH and I.S.) and commonly used organic chemicals (additives, formation, produced waters), were compared both to determine which chemical parameter is most responsible for Ba release and to potentially identify at which point during the hydraulic fracturing process release is likely to occur. Based on these results, a new model for Ba cycling in hydraulic fracturing systems is presented.

Methods:

Reactor experiments:

For determining potential Ba sources, a total of six types of solids/slurries (4 shales, pure barite, and drilling mud slurry) were selected for reaction with various chemical treatments. The four shale samples (Eagle Ford, Green River, Barnett, and Marcellus) contain a wide range of carbonate, clay, and organic concentrations along with wide ranges in Ba concentrations. A pure barite sample was selected from the Stanford Research Mineral Collection as a control while the drilling mud (DM) used was procured from National Energy Technology Laboratory which was used during the installation of the MSEEL site in Morgantown, WV. All solid samples were ground to a particle size of 150-250 µm in order to speed up reaction and allow a more uniform comparison in which shale porosity/permeability was less of a factor.

The experimental design differed between reactors containing shale and reactors containing either pure barite or drilling mud. Barium results for the shale reactors are a subset of data, previously unpublished, from earlier experiments that have been published^{12, 19, 20}. In these reactors, 1 g of ground shale was reacted, unagitated, for a total of 3-weeks at 80°C in 200 mL of fluid with ~40 mL of headspace (headspace was at equilibrium with environment before sealing. All experiments were conducted in acid washed borosilicate serum bottles with butyl rubber stoppers and aluminum crimp seals. Fluid sampling was done every three days with samples being filtered through 20 nm Anatop[®] filters and preserved with trace metal grade 2% HNO₃. In reactors using either pure barite or drilling mud, 0.1 g of pure barite or 0.2 g of drilling mud slurry were reacted in a 40 mL I-chem[®] borosilicate vials with Teflon[®] lined lids. The larger amount of drilling mud was selected in order to have similar concentrations of barite in the vials. The MSDS for the drilling mud states that barite concentrations are between 20 and 60 wt.%. Organic and inorganic parameters (Table 1) tested for the barite and drilling mud are consistent with values found in fracture fluid formulations²¹ and produced/flowback waters^{1, 2, 14}. Barite/DM reactors were placed on an end-overend tumbler at 70 rpm for agitation at 80°C for 72 hours. Preliminary testing showed that in all cases Ba concentrations reached steady state by 72 hours. Samples were filtered through 20 nm Anatop® filters and immediately diluted 1:100 with trace metal grade 10% HNO₃, in order to prevent any Ba from precipitating as temperature dropped. Barium concentrations for both the shale reactors and the Barite/DM reactors were measured using a Fisher Scientific iCAP 6300 ICP-OES.

Bulk shale, barite, drilling mud parameters:

Drilling mud slurry was separated into its solid and liquid components by centrifugation at 12,200 rpm for 4 hours. The supernatant was removed and was serially filtered using a 0.45 µm GMF filtered followed by a 0.2 µm PES filter and diluted 1:1000 using 2% trace metal grade HNO₃. Though the supernatant was pre-filtered to 0.2 µm, the solution was not able to pass through the alumina matrix of the 20 nm Anatop[®] filters. The pellet was washed with double de-ionized water (DDI) and dried at 80°C. For comparison, a subset of the drilling mud slurry was dried at 80°C without any prior separation. Dried pellet samples of the shales (before and after reaction), both drilling muds, and barite were analyzed using a Rigaku Microflex X-ray diffractometer. Analyses of collected diffractograms were conducted using the JADE diffraction analysis program²² where the first five most intense phases were fit with reference diffraction patterns from the National Institute of Standards and Technology (NIST) database followed by least-square fitting of the data to quantify wt.% of detected mineral phases. Bulk elemental analysis of all solids was completed using a Spectro Analytical XRF model XEPOS HE with an additional certified reference standard (Montana Soil 2711a). Total metal/anions in the filtered DM fluid was analyzed using Fisher Scientific XSeries 2 ICP-MS.

Table 1: Inorganic and organic parameters tested. Ionic strength (I.S.) was set using NaCl and titrated to pH = 7 using NaOH. Organic chemical
concentrations are set to literature values. Fracture fluid recipe is similar to that used in NETL's Greene Co. Well E and has been used in
previous experiments ²³ . Type of solids: Barite (B), Drilling Mud (DM), Shale (S). All parameters for shale have reactors containing one of the
following: Eagle Ford, Green River, Barnett, or Marcellus.

Chemical parameter	Use/Source	Solids tested
15% HCl (pH = -0.3)	Initial acid slug following perforation	B, DM
pH 2		B, S
pH 4		B, DM, S
pH 5		В
pH 7		B, DM, S
I.S. 0.01		B, DM
I.S. 0.1		B, DM
I.S. 2.3		B, DM
Citrate	Fe-control	В
Guar Gum	Gellant	В
Ethylene Glycol	Winterizing agent, scale control	B, DM
Glutaraldehyde	Biocide	B, DM
Polyethylene glycol	Biocide	B, DM
Bitumen (Marcellus-derived)	Native to shale	В
Acetate	Formation water	B, DM
Benzene	Produced water	В
Kerosene	Friction reducer	В
Methanol	Fe-control, surfactant	B, DM
Fracture fluid		B, DM

Results

Bulk Shale and Drilling Mud Characterization:

The bulk mineralogy of the four shale samples used in these experiments have been described previously and is presented in **Table 2**^{12, 19, 20}. Two shale samples contained > 50 wt.% carbonates (Eagle Ford and Green River), while the two clay-rich samples (Barnett and Marcellus) had < 12 wt.% carbonates (**Table 2**). Bulk XRF analyses of these four shales show a wide range of total Ba with Eagle Ford containing the least, followed by Barnett, Green River, and Marcellus (**Table 3**). For the drilling mud, XRD analysis of the DM that was dried without any prior separation shows a significant amount of NaCl that precipitated during the drying process (> 90 wt.%) with the remaining portion being barite (**Table 4**). When the DM was separated from the carrier fluid via centrifugation, the amount of detectable NaCl dropped to 24 wt.% allowing for the detection of other mineral species (**Table 4**). The large concentrations being 192.3 g/L. XRF data of the drilling mud with and without fluid separation confirms that mechanically separating the solid and liquid portions resulted in a large decrease of Cl when the samples were dried (**Table 5**). Assuming that all the Ba in the drilling mud is in the form of barite, the calculated barite concentration using the XRF data results in 20.1 wt.% barite which is in good agreement with the quantitative XRD results.

Table 2: Bulk mineralogy of Eagle Ford, Green River, Barnett, and Marcellus shale samples before reaction with fracture fluid. "X" denotes nondetectable phase.

	Quartz	Calcite	Dolomite	Illite	Kaolinite	Pyrite	Feldspar	Analcime
Eagle	25.2	64.5	Х	Х	7.6	2.7	Х	Х
Ford								
Green	31.4	23.2	28.9	Х	Х	Х	8.0	8.5
River								
Barnett	44.2	8.2	Х	40.6	Х	2.1	4.9	Х

Marcellus	42.2	11.6	1.1	35.0	Х	6.4	3.7	Х	
Table 3: Sele	cted XRF data for	Eagle Ford (EF), Green River (C	GR), Barnett (B), and Marcellus	(M) shales befo	ore and after 3-we	eek reaction with	h
fracture fluid.									

	EF	EF	GR	GR	В	В	Μ	Μ
	Unreacted	Reacted	Unreacted	Reacted	Unreacted	Reacted	Unreacted	Reacted
Ca (wt.%)	16.67	13.46	13.64	9.11	2.51	0.14	4.23	0.07
Mg (wt.%)	0.37	0.47	4.41	3.7	0.63	0.35	0.78	0.47
Al (wt.%)	5.82	6.38	2.66	2.76	7.29	7.67	10.5	7.07
S (wt.%)	1.13	1.19	0.1	0.07	0.9	1.1	2.05	1.73
Fe (mg/kg)	23930	21170	17830	13610	24830	20790	45630	32540
Ba (ppm)	104.8	<1.5	1188	1094	518	215.7	1675	898

	Ba (mg/kg)
M Unreacted	1675
M Reacted	898
M DDI Water	1847
M HCl Only	832.9
M Fracture Fluid, No HCl	2203

Table 4: Quantitative XRD results of Dried drilling mud (no separation of solid and liquid prior to drying) and Centrifuged and dried drilling mud.

	Species	Weight %
Dried Drilling Mud	Halite	90.9
	Barite	9.1
Centrifuged and dried Drilling	Halite	24.0
Mud		
	Barite	24.4
	Illite	44.0
	Calcite	7.6

Table 5: Selected XRF data of Dried drilling mud (no separation of solid and liquid prior to drying) and Centrifuged and dried drilling mud.

	Dried drilling mud	Centrifuged and dried drilling mud
Al (%)	3.62	1.43
Si (%)	9.03	6.23
S (%)	2.33	2.33
Cl (%)	16.22	1.34
Fe (mg/kg)	8517	8779
Br (mg/kg)	371.7	56.7
Cs (mg/kg)	168.2	153.8
Ba (mg/kg)	111400	112100

Barium release from shale:

The release of Ba in the shale reactors for Barnett, Green River, and Marcellus shales reached a plateau within the first 100 hours of experimentation while Eagle Ford continued to increase throughout the experimental time (**Figure 1**). The concentrations of released Ba in these reactors are more than 3-orders of magnitude below that typically found in produced/flowback water (typically 1,000 ppm)^{1, 2, 13, 14}. Of particular interest is the Ba release for the Marcellus shale with and without the addition of HCl in the fluid. As seen in **Figure 2**, in a reactor containing HCl only, the rapid increase of Ba in solution mirrors the case where all the organic additives and HCl are included. In

reactors without any added HCl (pH = 7), the release of Ba is slower than the pH = 2 scenario, but within the 3-week time frame, it reaches concentrations similar to the pH = 2 reactors.

Bulk XRF of the shale sands post-experiment have definite trends. In the case of Barnett, Eagle Ford, and Marcellus shales samples, nearly 50% of the total Ba (nearly 100% for Eagle Ford) in the sample was lost during the 3-week reaction (Table 3). The maximum Ba release of \sim 50% of the total for Marcellus is consistent with results from Renock et al.¹³ Even though Green River shale had the highest concentration of Ba in solution throughout the experiments, the overall Ba weight percentage in the shale did not reduce nearly as much as the other three shale types (Table 3). Based on the XRF data, the Barnett and Marcellus shales lost the largest amount of Ba, but the Barnett also showed the lowest amount of Ba in solution. If the solution concentrations were proportional to the solid concentrations, then Ba concentration in solution for Eagle Ford, Barnett, and Marcellus should be nearly 8fold higher than their present values. As previously shown¹² for these shale samples, pyrite readily oxidizes under these fracture fluid conditions. The oxidation of S from the pyrite provides a source of SO₄ which due to the low solubility of barite could allow for barite precipitation to occur, reducing overall Ba concentrations in solution. In these shale systems, pH is the largest driver for rapid Ba release into solution. The Marcellus samples show that when the starting solution pH is low (pH = 2), Ba is rapidly released into solution (Figure 2). This rapid Ba release, steady state is reached in < 100 hours, occurs with and without the organic additives. These solution data are consistent with the bulk XRF data where the reactors with added HCl showed a large and consistent drop in Ba concentration, ~45-50% (Table 3).



Figure 1: Barium release from ground shale samples (150-250 μ m) in the presence of pH = 2 fracture fluid. B = Barnett, EF = Eagle Ford, M = Marcellus, and GR = Green River. Measurement error for triplicate measurements is < 8%.



Figure 2: Barium release from ground Marcellus shale in the presence of fracture fluid, fracture fluid minus HCl, HCl only, and DDI Water only. Measurement error for triplicate measurements is < 8%.

Barium release from pure barite and drilling mud slurry:

Pure ground barite (150-250 μ m) was used to set a baseline for the thermodynamic stability of barite in a variety of inorganic and organic conditions. The inorganic parameters, pH and I.S. had a significant effect on the total amount of Ba released into solution (**Table 6**). The more acidic the solution, the greater release of Ba from the ground barite with 88.8 ppm at conditions similar to the 15% HCl acid slug injected prior to the rest of the completion chemicals. Thermodynamic modeling of the pH effects on barite using Visual Minteq²⁴ are in good agreement with experimental values except for pH = 0, in which modeling predicts 147 ppm rather than the 88.8 ppm measured. The pH 7 reactor is taken as a baseline for comparing dissolution of barite at various I.S. or in the presence of various organic constituents. In **Table 6**, the vast majority of organics were found to slightly thermodynamically stabilize the barite with Ba concentrations at the same level as the control to 0.7 ppm below. A few organics were seen to slightly enhance barite solubility (glutaraldehyde and acetate). The fracture fluid released over 4 times as much Ba compared to the pH 7 control. Additionally, acidic fracture fluid released even more Ba when compared to the pH = 2 reactor, which the majority of released Ba can be attributed to acidity rather than the pH = 2 reactors, the organics are aiding in solubilizing the barite, *i.e.*, after dissolution has occurred.

Parameter	Ba released (ppm)]
pH 0	88.8	(
рН 2	7.5	(
pH4	2.2	I
рН 5	1.99	(
pH 7 (DDI	2.0	I
water)		
I.S. 0.6 mM	2.0	ľ
I.S. 0.01 M	2.8	I
I.S. 0.1 M	5.1	I
I.S. 1 M	13.9	ľ
I.S. 2.3 M	22.2	I
		T

Table 6: Barium release from pure barite in the presence of a variety of inorganic and organic parameters. Measurement error for triplicatemeasurements < 5%.</td>

Parameter	Ba Released (ppm)
Citrate	1.5
Guar Gum	1.6
Ethylene Glycol	1.3
Glutaraldehyde	3.4
Polyethylene glycol	1.8
Marcellus Bitumen	1.8
Acetate	2.3
Benzene	1.8
Methanol	2.1
Fracture Fluid	9.4
DDI water	2.0

Due to the difference in the total amount of Ba added to reactors between experiments using pure Barite and Drilling Mud Slurry, it is more useful to look at the total percentage of Ba released from the amount of Ba-solid added. As seen in **Table 7**, pH is the largest driver of Ba release from both the DM and the pure Barite. At very low pH as seen with the initial 15% HCl slug commonly injected at the beginning of stimulation, over 18% of the total Ba contained in the DM was released into solution. At low pH more than twice as much Ba is released from the DM compared to pure Barite. The percentage of Ba released from both types of materials for various I.S. is similar over a wide range of salinity. The organics on the other hand does show definite differences in Ba release from DM and Barite based on the additive (**Table 7**). Several organics released similar amount of Ba into solution for both materials: glutaraldehyde, polyethylene glycol, acetate, and methanol. These organics tested, ethylene glycol, a common winterizing-agent and scale inhibitor, released significantly more Ba from DM compared to barite. Surprisingly, ethylene glycol released more Ba from DM compared to DDI water control. Fracture fluid (pH = 2), released more Ba from both materials than the pH = 2 reactor suggesting that the organic additives behave differently (*i.e.*, promote dissolution) when mixed together or at lower pH.

Table 7: Percentage of total Ba added to reactors either in the form of Drilling Mud or pure Barite in the presence of various inorganic and organic parameters.

	% Ba released from Drilling Mud	% Ba released from pure Barite
рН 0	18.4	6.0
рН 2	0.44	0.39
рН 4	0.18	0.15
рН 7	0.2	0.14
I.S. 0.01	0.16	0.19
I.S. 0.1	0.3	0.35
I.S. 1	0.91	0.95
I.S. 2.3	1.54	1.51
Ethylene glycol	0.33	0.09
Glutaraldehyde	0.2	0.23
Polyethylene glycol	0.15	0.12
Acetate	0.17	0.16
Methanol	0.15	0.14
Ammonium persulfate	0.03	0.01
Fracture fluid $(pH = 2)$	0.55	0.64

Discussion

There are at least two major potential sources of Ba in hydraulic fracturing systems: source rock and drilling mud. The amount of Ba native to the oil/gas shales can vary significantly depending not only on the different shale play, but within the shale play itself. Analyses of 4 different shale samples (Eagle Ford, Green River, Barnett, and Marcellus) show that Ba concentrations can vary by over an order of magnitude (**Table 3**). Even though Ba concentrations in the shale can reach levels of 1000 mg/kg or more (assumed to predominantly bound to clays¹³), these levels are significantly lower than those in DM which can vary from 20-60 wt.% barite depending on the manufacturer. Though there are instances in unconventional systems where there are lenses of nearly pure barite¹⁵ present, the high consistency of Ba in produced waters over a variety of plays^{1, 2, 13, 14} casts doubt that these barite lenses would be a large contributor of barite in these systems. The consistency of Ba concentration in produced waters also casts doubt on the shale (excluding the barite lenses) being the primary source of Ba into the fluid system. As seen in **Table 3** and **Figures 1 & 2**, besides the Eagle Ford samples, a significant amount of the Ba (> 40%) is still contained in the rock after reaction. Based on the amount of Ba in rock and the total amount of Ba that can be released from the shale, the amount of extractable Ba from the source rock seems unlikely to produce the Ba concentrations detected in produced waters. This suggests another Ba source is more important in these systems.

Drilling mud common to oil/gas systems, both conventional and unconventional, contains a significant amount of Ba (20-60 wt.%). These concentrations are over 2-orders of magnitude greater than the higher end of Ba concentrations in the shales tested (**Table 3**). Even though operators in unconventional systems attempt to clean the bore hole as much as possible prior to injection of chemicals, the ability to remove all the DM from the system due to embedment in the bore wall (either on the surface or pushed into newly formed cracks due to the drilling process) is not possible. Because of the high concentration of barite in the drilling mud compared to that of the source rock, dissolution of even a small fraction of the barite in the DM will result in solution Ba concentrations significantly higher than derived from the shale. Additionally, since the DM resides in the vicinity of the bore hole, it is more accessible to fluids than the shale matrix, which is accessible only when fluids imbibe into the shale.

As shown with the shale, barite, and DM reactors, low pH in the form of HCl is the most important parameter with regards to the stability of Ba in both pure crystals and DM. The next important variable in these systems is I.S. Because the DM contains significant quantities of Na and Cl in the carrier fluid as indicated by the amount that precipitates when dried and ICP-MS data, this additional I.S. results in enhanced dissolution of barite in the DM as seen at low pH (Table 7), due to the lowering of the activity coefficients for Ba and SO₄. Organics additives on their own in these systems appear to have little impact on the stability of barite, both pure and in DM, when compared to pH and I.S. In the case of the fracture fluid (pH = 2), there is an enhancement in Ba release from both barite and DM when compared to the pH = 2 reactor (**Table 7**). This is due most likely to the presence of the gellant guar gum in the fracture fluid. Guar gum has a high chelating potential and should bind Ba released in solution, which could lead to additional barite dissolution due to the low pH of the fluid. Based on the higher I.S. of the DM experiment it could be predicted that the DM reactor should release more Ba than the pure barite system. Though great care was taken to homogenize the fracture fluid prior use in the reaction vessels, due to guar gum not fully dissolving into solution, there is a high possibility that there is a variation in guar gum concentrations in these reactors. In the case of fracture fluid, organics (presumably guar gum) enhances the dissolution of barite at low pH. Even though the organics aid in dissolution, the other experiments conclusively show that pH is the most important variable for solubilizing Ba and SO₄ from drilling mud.

In general practice, 15% HCl is injected into the subsurface prior to injection of additional chemicals and proppant. Results shown in **Tables 6 and 7** shows that significant quantities of Ba, along with SO₄, are released into solution. This released Ba and SO₄ would then be pushed into the newly formed fractures in the shale by later injection stages where it can precipitate when injected acid is neutralized by carbonates in the shale raising the solution pH. Though I.S. is shown to have an effect on barite stability (**Tables 6 and 7**), and precipitation, its effect is much less than that of pH, especially over the short time scale in which pH is very low (pH < 0). Though the changes in I.S. in the subsurface during injection, shut-in, and production is not fully understood, since I.S. is controlled by mineral dissolution it can be assumed that unless highly saline base fluid is used, the I.S. will slowly rise during shut-in and be inversely related to solution acidity. We propose a new schematic for barite cycling taking into account pH and I.S. (**Figure 3**). During the initial injection of 15% HCl, a significant amount of Ba and SO₄ in drilling mud that comes into contact with the acid will be liberated. This newly released Ba and SO₄ will then be forced into the newly formed fractures by the injection of later stages. As the acid reacts with carbonate in the rocks and mixes with formation water, solution pH will begin to increase. Once the pH rises above pH = 2, barite will begin to precipitate. As the injected acid reacts with minerals in the shale (carbonates, pyrite, clays, etc.) I.S. will increase. Until solution I.S. reaches ~1 M, barite will continue to precipitate from solution. This interplay between acidity and I.S. allows for a window of time for barite precipitation to occur before I.S. gets too high inhibiting further precipitation and eventually dissolving a fraction of the newly precipitate barite. Thermodynamic modeling along results presented in **Table 6** indicate that ~10% of barite that would precipitate in fractures once pH > 2 would dissolve. This proposed model and data presented thus far indicate that barite scale on fracture surfaces and in shale pores in these systems is derived from the dissolution of drilling mud and its interaction with the 15% HCl acid slug.

Conclusions

As we have shown in previous work^{12, 19, 20}, pH is one of the most important parameters in hydraulic fracturing systems. In the case of Ba present in oil/gas shale, low pH solutions will result in the release of Ba into solution. Though up to 50% of the total Ba contained in the shale can be released into solution, the total amount of Ba is not sufficient to explain the high concentrations of Ba measured in produced water. Ba-infused drilling mud contains extremely high concentrations of barite (20-60 wt.%). Dissolving a low percentage of the barite in leftover drilling mud (~8%) should be sufficient to explain the high concentrations of Ba in produced water. We have shown that highly acidic solutions such as the 15% HCl acid slug initially injected into the subsurface can release > 18% of the total Ba contained in drilling mud. Based on these results we have proposed a new model for Ba cycling in the subsurface in which the DM is the primary source of Ba for barite scale production in the newly formed fracture network. Due to the competing trends of pH and I.S. in these systems, a window of barite precipitation will occur in the subsurface once pH > 2 and I.S. < 1 M. Even if I.S. rises to > 1 M, only a fraction of the precipitated barite will re-dissolve. The end result is self-inflicted formation damage caused by the use of Ba-rich DM and a highly acidic acid slug.

Barite dissolution (DM) Ba transport to fractures Amount of total Barite dissolution solid Barite in in fracture space system Precipitation in due to I.S. fracture system Injection of acid slug pН Neutralization of acid slug by shale Mineral dissolution in shale **Ionic Strength**

Schematic of Ba cycling in subsurface



Figure 3: Proposed schematic of Ba cycling in the subsurface of hydraulic fracturing systems.

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