

**APPENDIX A**  
**MAPS**

Figure 4-1. Location Map for the Impoundments Studied in the Prairie Dog Creek Watershed

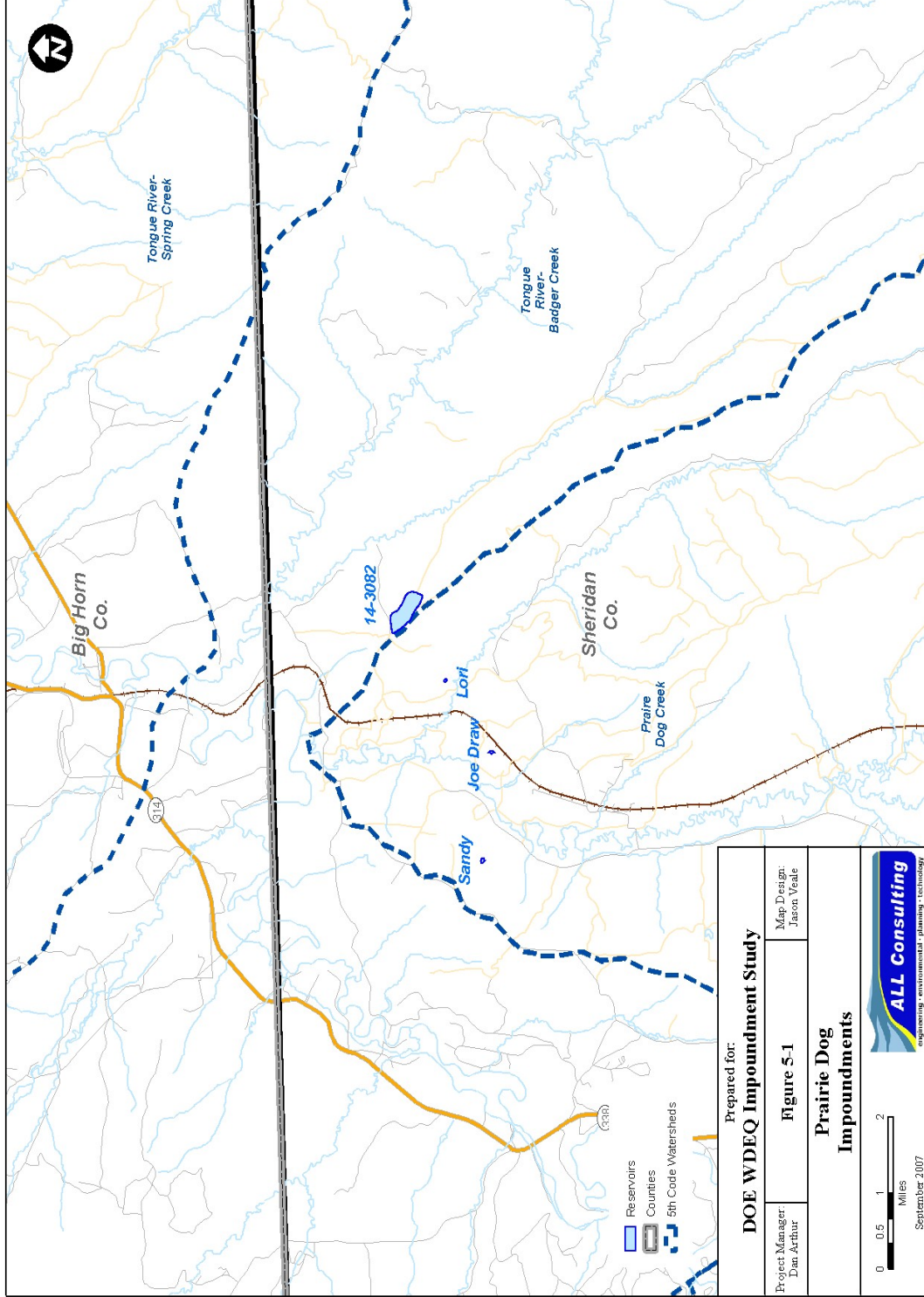
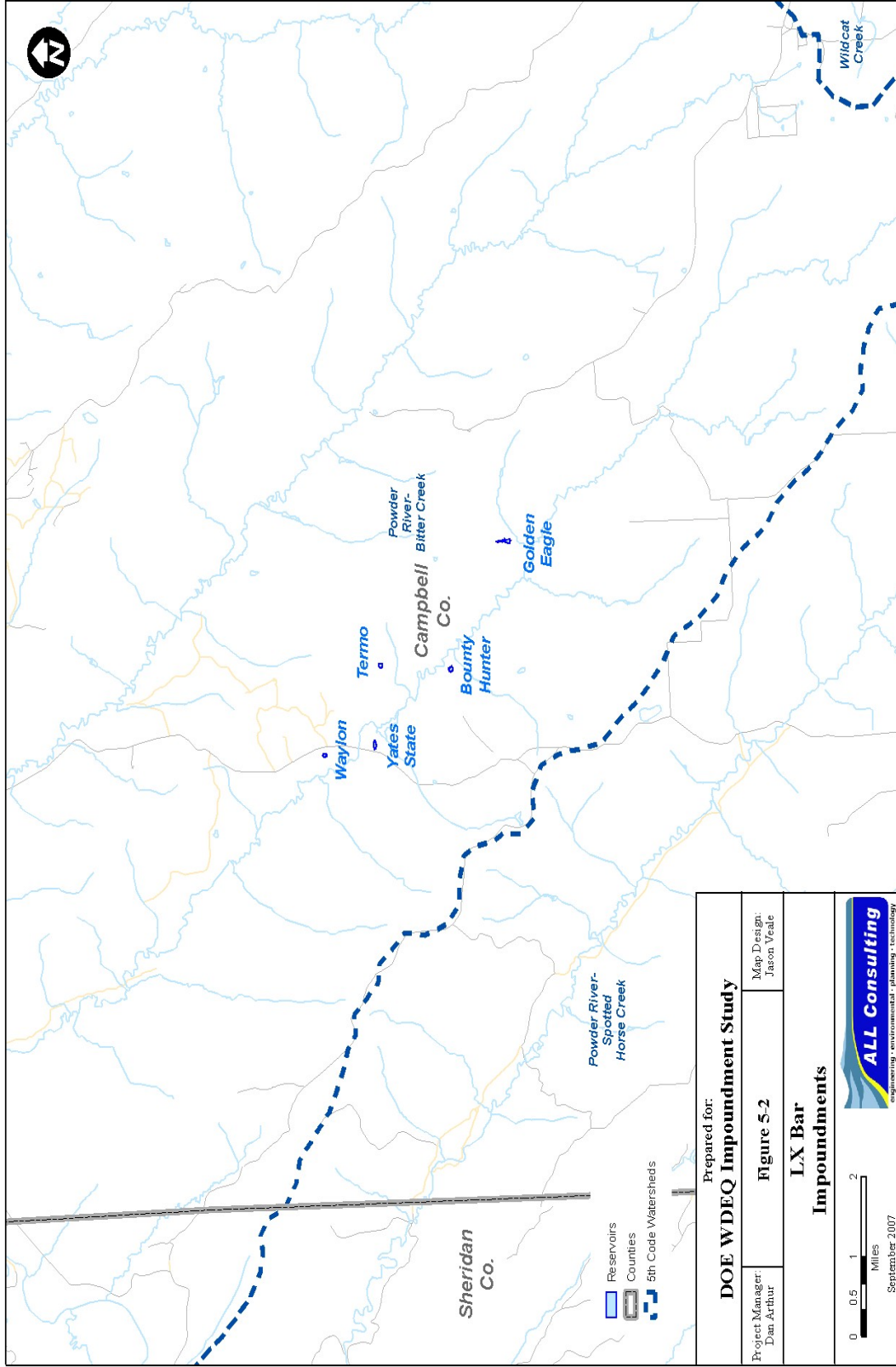


Figure 4-2. Location Map for the Impoundments Studied in the LX Bar Creek Watershed





**Figure 4-3. Location Map for the Impoundments Studied in the LX Bar Creek Watershed**

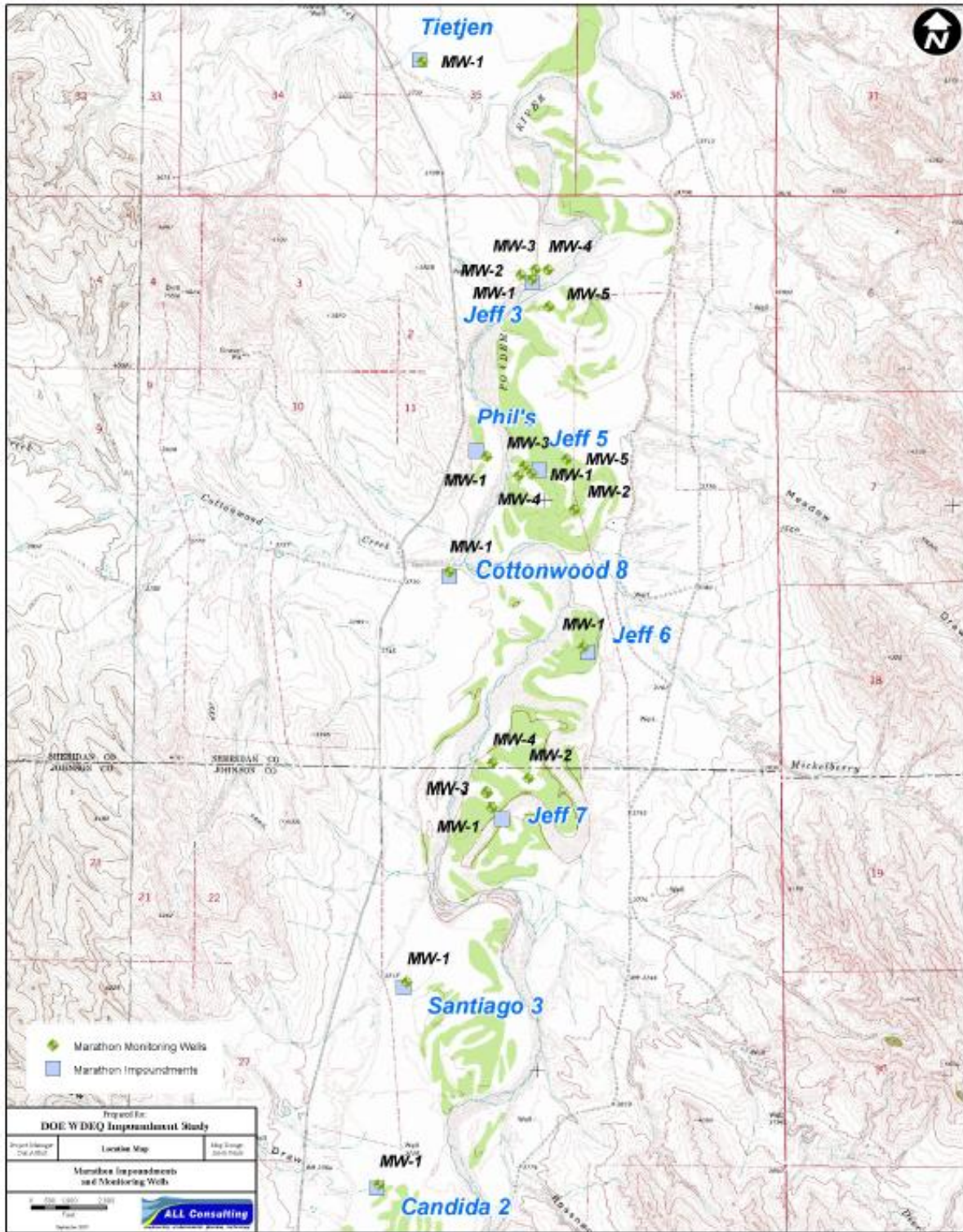




Figure 4-4. Structure map of the Smith Coal seam at the Lori impoundment.

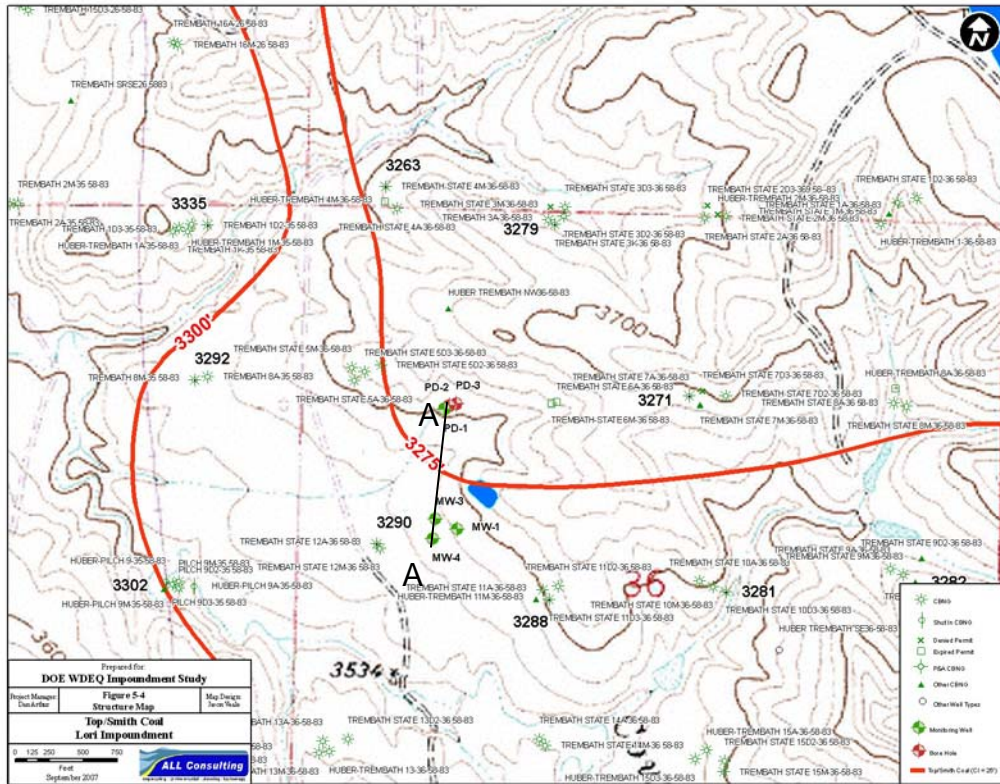
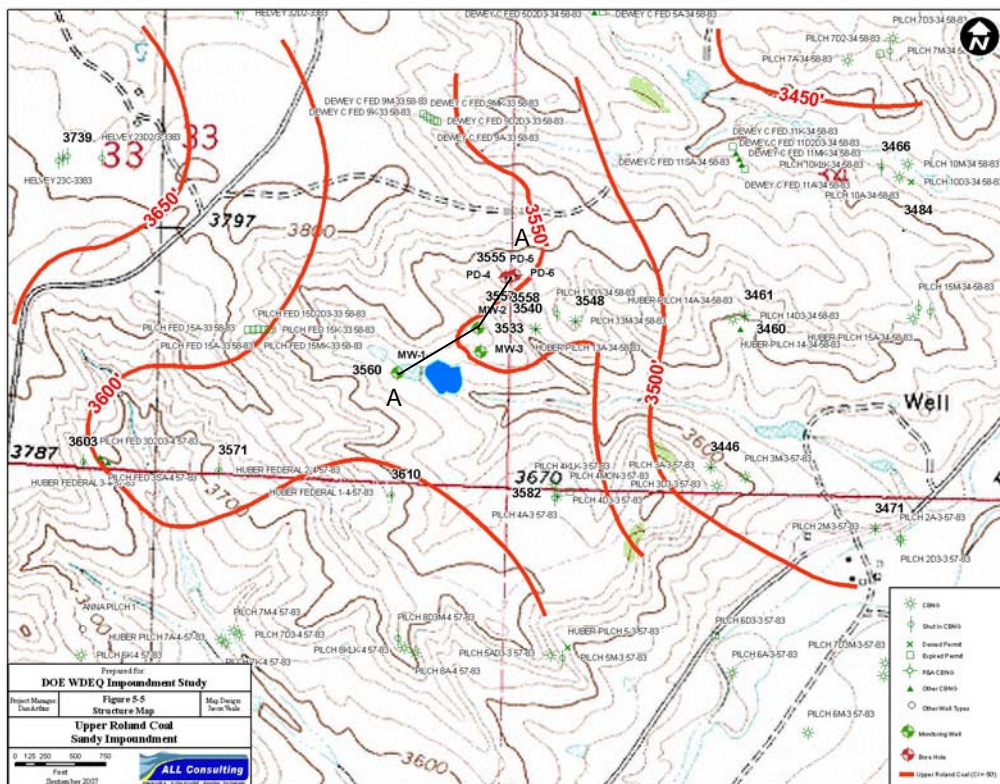
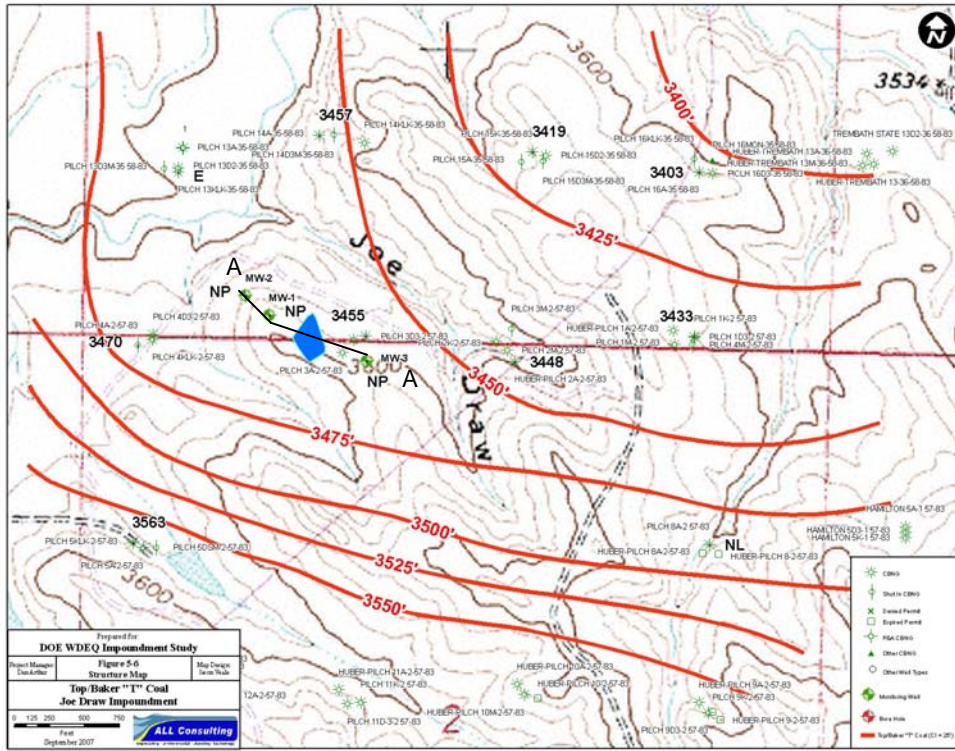


Figure 4-5. Structure map of the Upper Roland Coal seam at the Sandy impoundment.

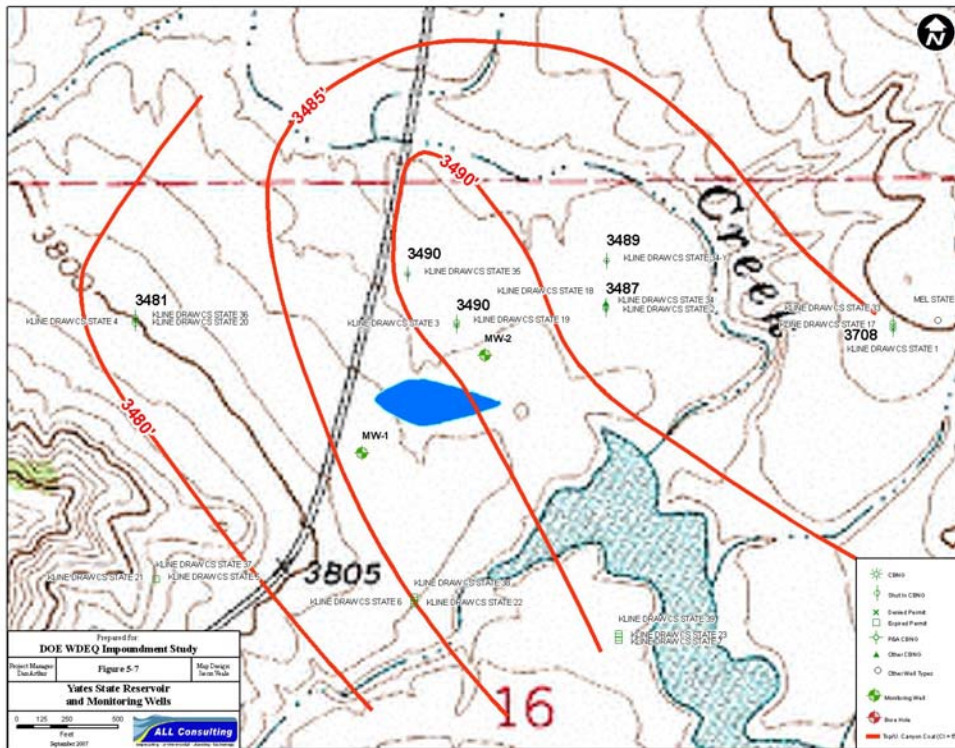




**Figure 4-6.** Structure map of the Baker T Coal seam at Joe Draw Jr impoundment.

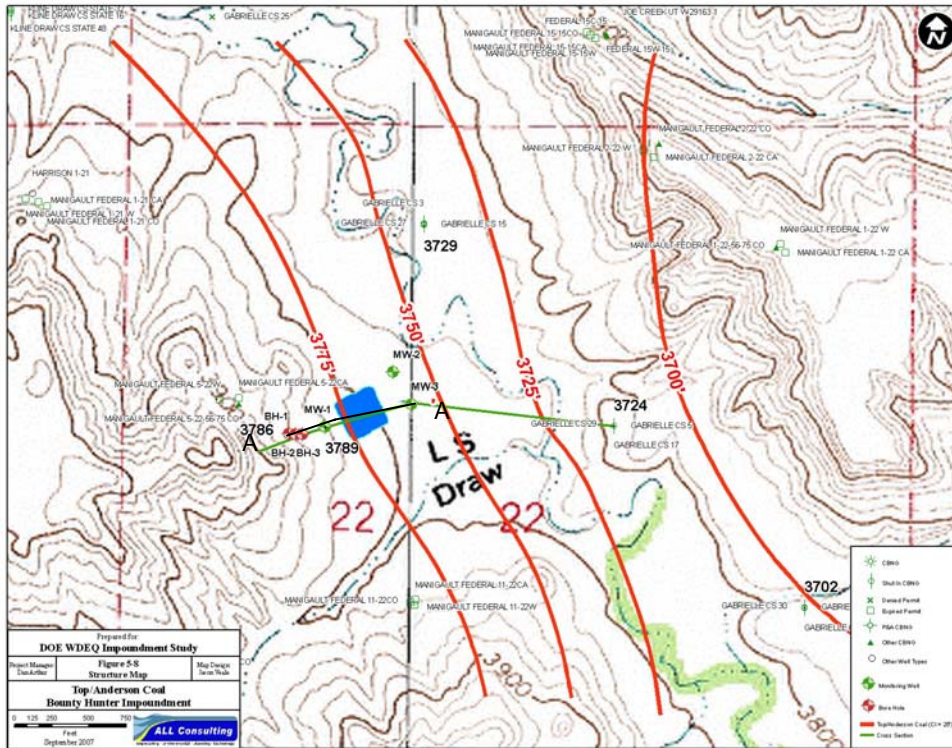


**Figure 4-7.** Structure map for the Upper Canyon Coal seam at the Yates State impoundment.

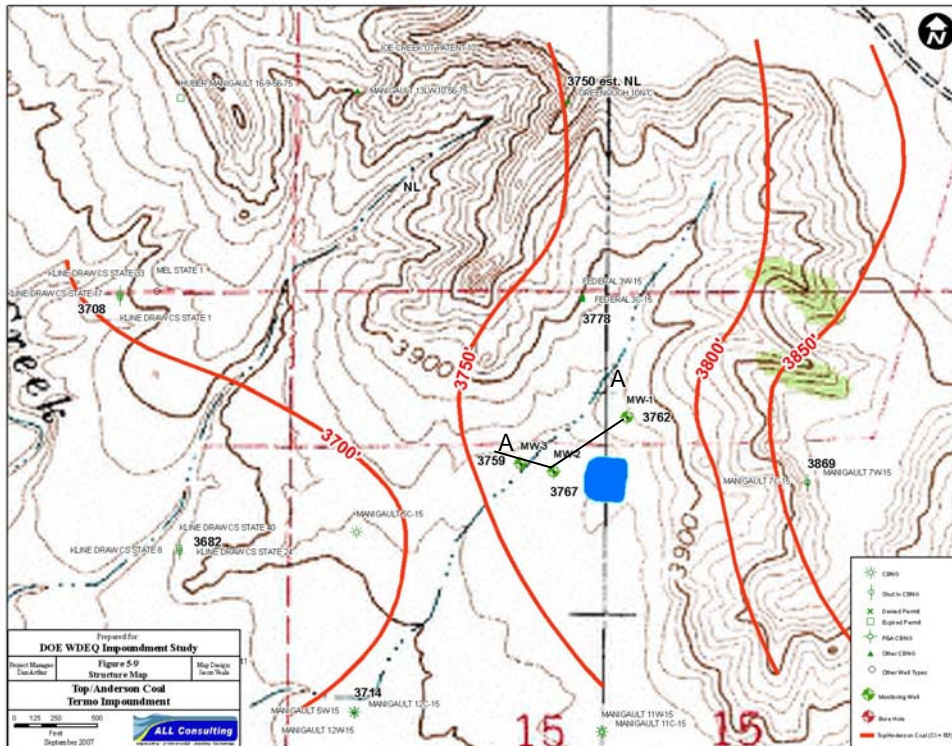




**Figure 4-8.** Structure map of the Anderson Coal Seam at the Bounty Hunter impoundment.

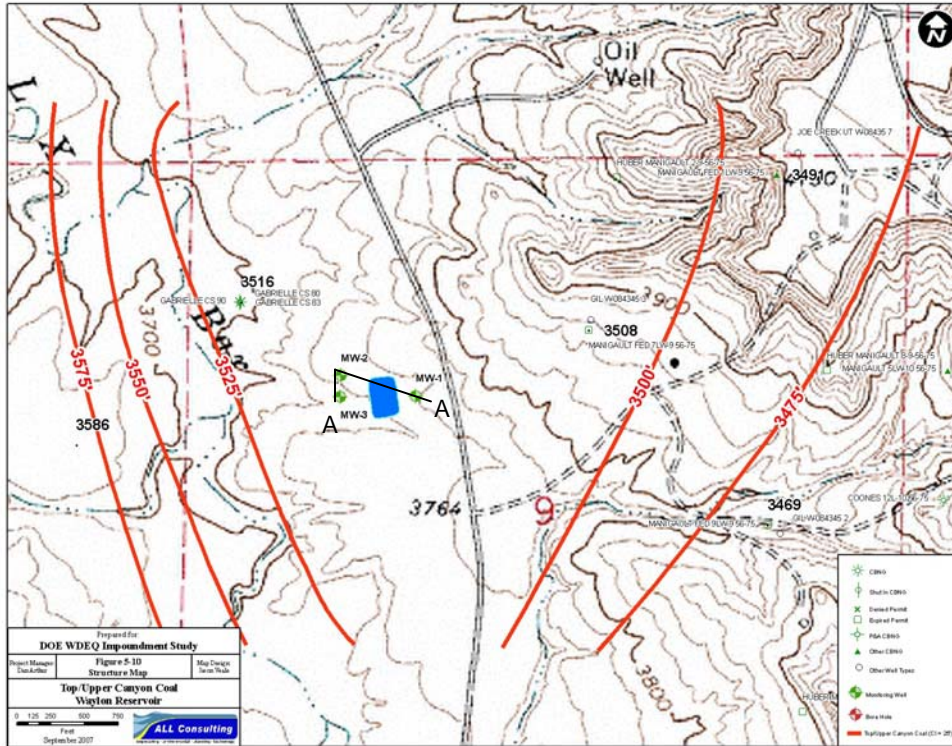


**Figure 4-9.** Structure map of the Anderson Coal seam at the Termo impoundment.

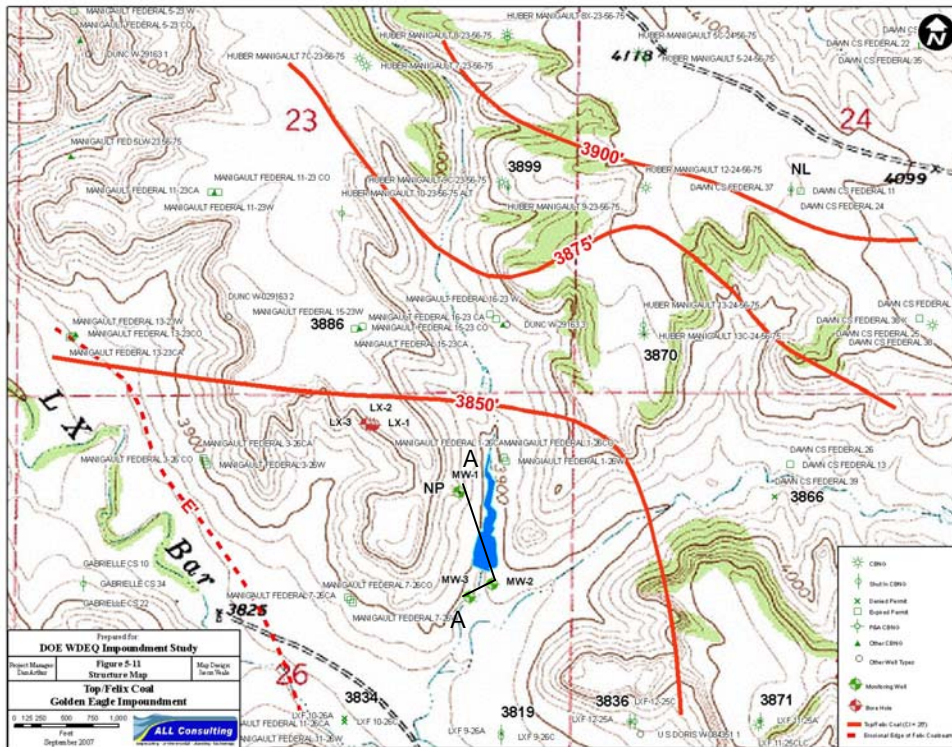




**Figure 4-10.** Structure map of the Upper Canyon Coal seam at the Waylon impoundment.



**Figure 4-11.** Structure map of the Felix Coal seam at the Golden Eagle Reservoir.



## **APPENDIX B**

### **BOREHOLE LITHOLOGIC LOGS AND WELL CONSTRUCTION DIAGRAMS**



**LX Bar Area Bounty Hunter Impoundment**

**Well No. BH DOE 2**

On-site Geologist  
Webster

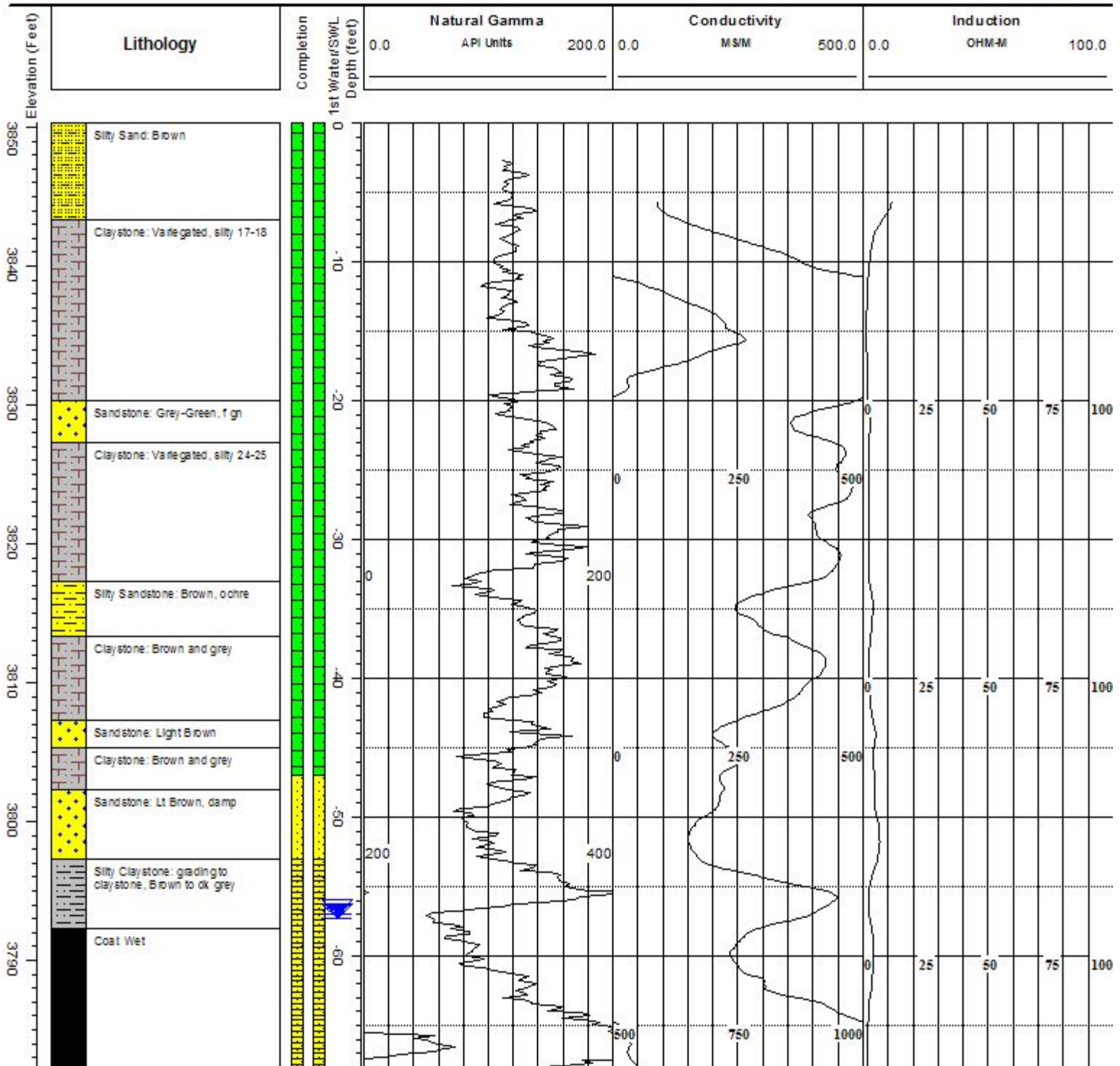
Latitude: 44°49'06.11284 Northing 1905213.52  
 Longitude: 105°52'42.75805" Easting 1689826.931  
 GL Elevation 3850.31

Total Depth: 74  
 Qtr Qtr: SWNW  
 Section: 22  
 Township: 56N  
 Range: 75W

Drilling Contractor Interstate Drilling  
 Driller Dave Proctor

Drilling Dates 6-27-06  
 Hole Diameter 5-7/8"

**Comments: Natural Gamma smoothed to aid resolution  
 SWL from 11-15-06**





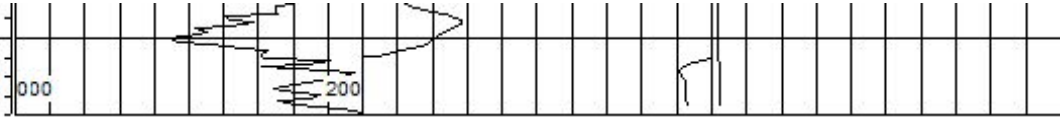
3780



Claystone - Grey



-70



**Major Ion Chemistry (mg/L)**

|          |                  |
|----------|------------------|
| Ca = 385 | CO2/HCO3 = Carbs |
| Mg = 531 | SO4 = 6461       |
| Na = 889 | TDS = 10268      |

|     |                            |       |     |                       |       |     |                    |       |
|-----|----------------------------|-------|-----|-----------------------|-------|-----|--------------------|-------|
| 0.0 | Natural Gamma<br>API Units | 200.0 | 0.0 | Conductivity<br>M/S/M | 500.0 | 0.0 | Induction<br>OHM-M | 100.0 |
|-----|----------------------------|-------|-----|-----------------------|-------|-----|--------------------|-------|

pH = 3.5  
SAR = 7

**WDEQ Ground Water Classification = IV**



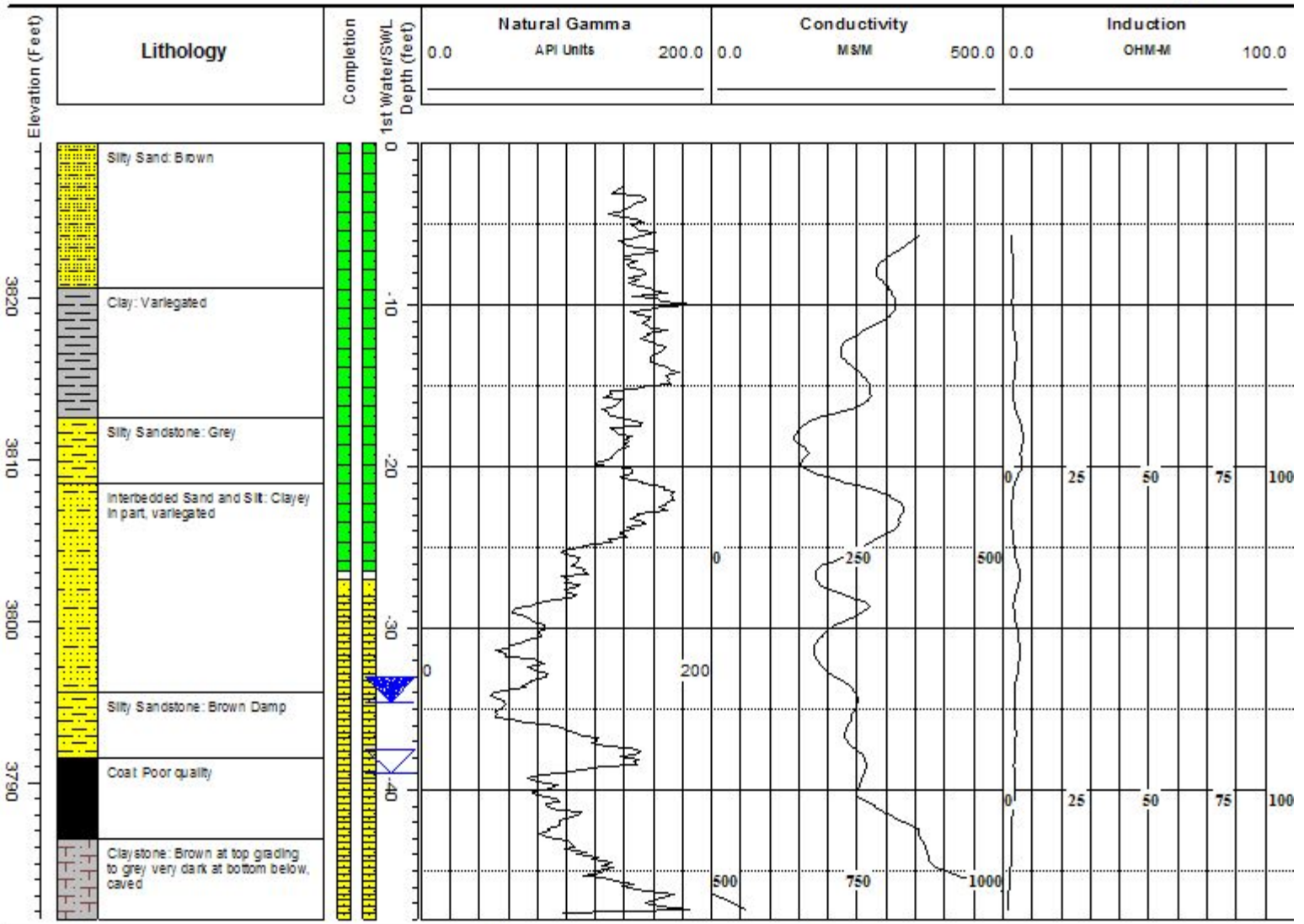
# Geophysical Logs Logs Run and Processed by United States Geological Survey

## LX Bar Area Bounty Hunter Impoundment

### Well No. MW-1

|   |  |   |
|---|--|---|
| On-site Geologist<br><u>Webster</u>   | Latitude: <u>44°49'08.20777"</u> Northing <u>1905268.75</u><br>Longitude: <u>105°52'31.97783"</u> Easting <u>1690022.51</u><br>GL Elevation <u>3829.55</u> | Total Depth: <u>19</u><br>Qtr Qtr: <u>SWNW</u><br>Section: <u>22</u><br>Township: <u>56N</u><br>Range: <u>75W</u> |
| Drilling Contractor <u>Interstate Drilling</u><br>Driller <u>Dave Proctor</u> | Drilling Dates <u>6-25-06</u><br>Hole Diameter <u>5-7/8"</u>   |   |

Comments: Natural Gamma smoothed to aid resolution  
No water chemistry data



#### Major Ion Chemistry (mg/L)

|         |                  |
|---------|------------------|
| Ca = Ca | CO2/HCO3 = Carbs |
| Mg = Mg | SO4 = Sulfate    |
| Na = Na | TDS = TDS        |

| Natural Gamma<br>API Units | Conductivity<br>M/M | Induction<br>OHM-M |
|----------------------------|---------------------|--------------------|
| 0.0                        | 0.0                 | 0.0                |
| 200.0                      | 500.0               | 100.0              |

pH = 7.0  
SAR = 8

**WDEQ Ground Water Classification = IV**



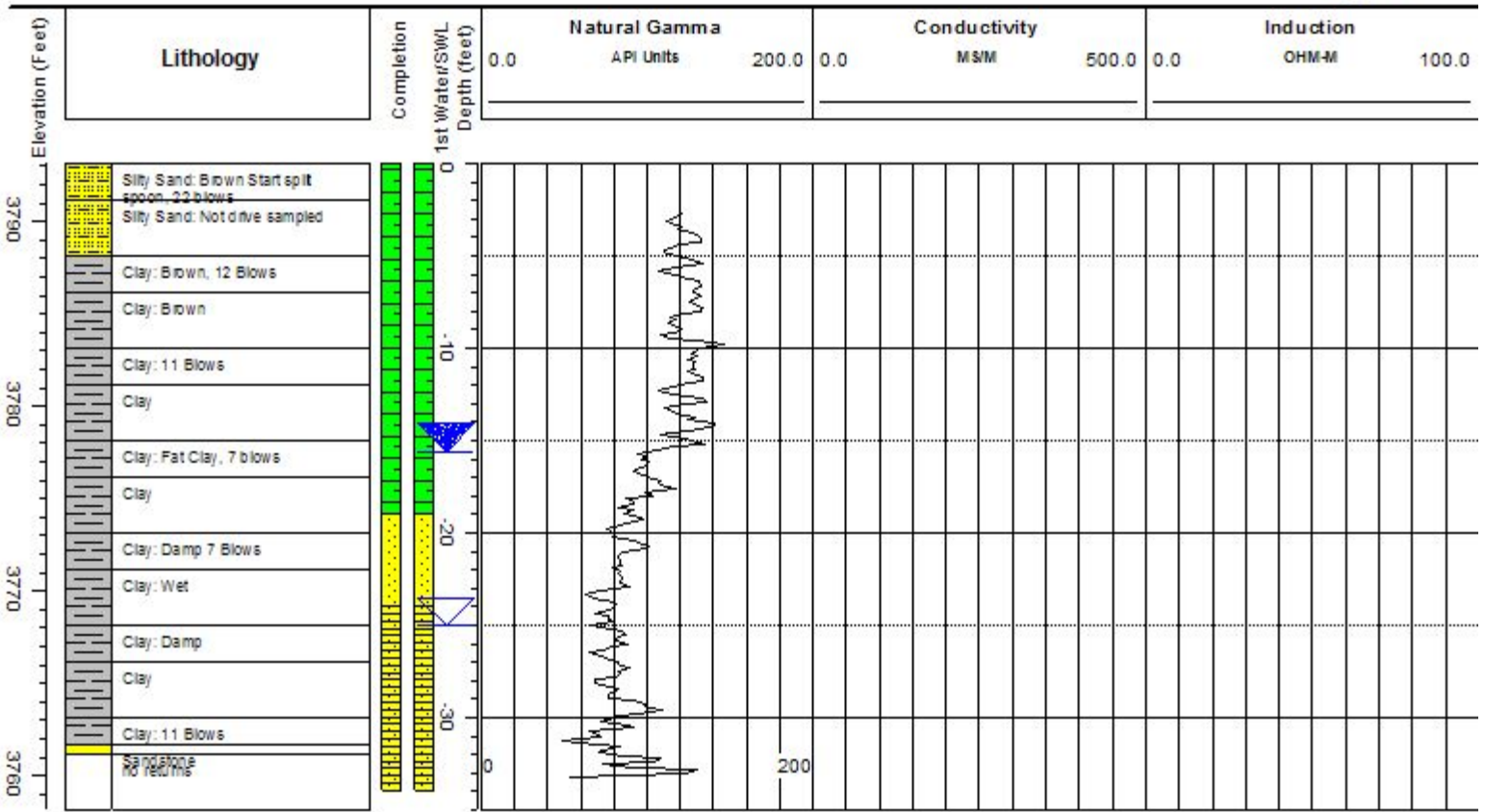
# Geophysical Logs Logs Run and Processed by United States Geological Survey

## LX Bar Area Bounty Hunter Impoundment

### Well No. MW-2

|  |  |                        |
|--|--|------------------------|
| On-site Geologist<br><u>Webster</u>            | Latitude: <u>44°49'10.31308"</u> Northing <u>1905650.52</u>  | Total Depth: <u>35</u> |
|  | Longitude: <u>105°53'33.73889"</u> Easting <u>1690469.39</u> | Qtr Qtr: <u>SWNW</u>   |
|  | GL Elevation <u>3793.14</u>                                  | Section: <u>22</u>     |
| Drilling Contractor <u>Interstate Drilling</u> | Drilling Dates <u>6-25-06</u>                                | Township <u>57N</u>    |
| Driller <u>Dave Proctor</u>                    | Hole Diameter <u>7-1/2"</u>                                  | Range <u>75W</u>       |

Comments: 33 feet of Natural Gamma ONLY Geophysical Log run -- Gamma curve smoothed due to excessive electronic noise  
SWL from 11-7-06



#### Major Ion Chemistry (mg/L)

|          |                 |
|----------|-----------------|
| Ca = 443 | CO2/HCO3 = 1280 |
| Mg = 372 | SO4 = 4402      |
| Na = 844 | TDS = 6168      |

| Natural Gamma | API Units | 200.0 | 0.0 | Conductivity | MS/M | 500.0 | 0.0 | Induction | OHM-M | 100.0 |
|---------------|-----------|-------|-----|--------------|------|-------|-----|-----------|-------|-------|
|---------------|-----------|-------|-----|--------------|------|-------|-----|-----------|-------|-------|

pH = 6.5  
SAR = 7

**WDEQ Ground Water Classification = IV**



# Wyoming Department of Environmental Quality Impoundment Study

## Geophysical Logs      LX Bar Area Bounty Hunter Impoundment



Logs Run and Processed by US Department of Energy  
 Depth Matching by Pete Vogel-WDEQ

**Well Boring No. MW-3**

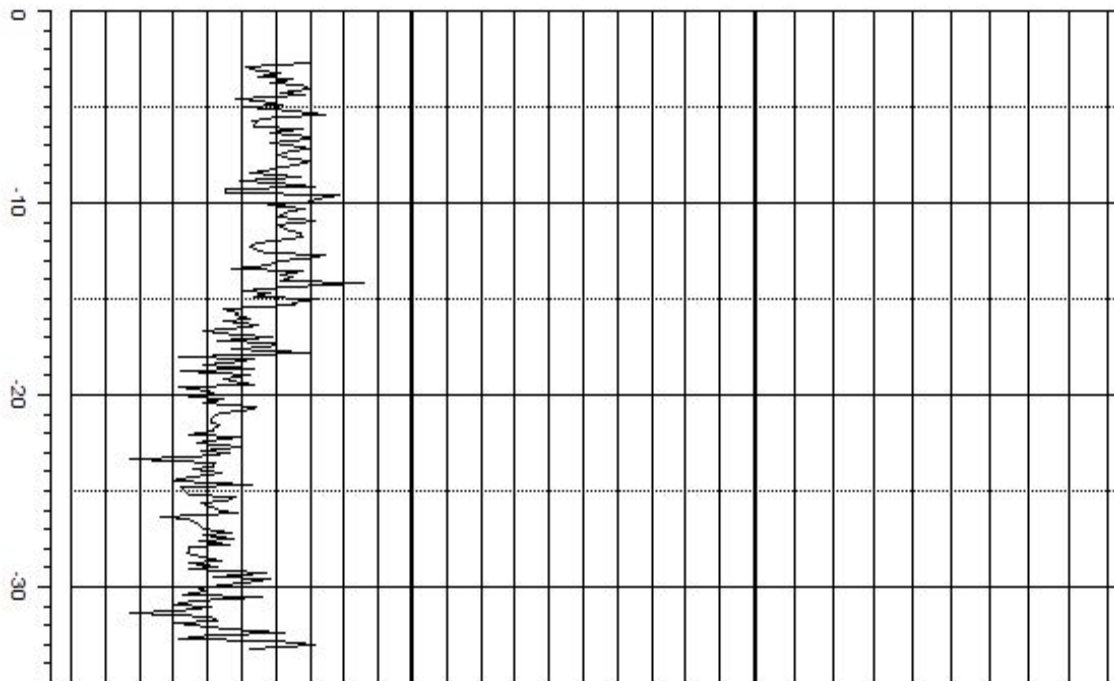
|                     |                                      |                |                   |              |                       |              |             |
|---------------------|--------------------------------------|----------------|-------------------|--------------|-----------------------|--------------|-------------|
| Logging Engineer    | <u>Smith</u>                         | Drilling Dates | <u>2-30-02</u>    | Latitude:    | <u>44.XXXXXXXXX</u>   | Total Depth: | <u>35</u>   |
| On-site Geologist   | <u>Webster</u>                       | Hole Diameter  | <u>5-7/8"</u>     | Longitude:   | <u>-106.XXXXXXXXX</u> | Qtr Qtr      | <u>SWSW</u> |
| Drilling Contractor | <u>Flying by Knight Drilling Co.</u> |                |                   | GL Elevation | <u>3744.87</u>        | Section      | <u>16</u>   |
| Driller             | <u>Doug Oakley</u>                   | Northing       | <u>1905650.52</u> | Township     | <u>57N</u>            | Range        | <u>83W</u>  |
|                     |                                      | Easting        | <u>1690469.39</u> |              |                       |              |             |

Comments: 33 feet of Natural Gamma ONLY Geophysical Log run

1 of 1

| Elevation (Feet) | Lithology | Depth (feet) | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="2" style="text-align: center;">Natural Gamma</th> <th colspan="2" style="text-align: center;">Conductivity</th> <th colspan="2" style="text-align: center;">Induction</th> </tr> <tr> <td style="text-align: center;">0.0</td> <td style="text-align: center;">API Units</td> <td style="text-align: center;">200.0</td> <td style="text-align: center;">0.0</td> <td style="text-align: center;">MSM</td> <td style="text-align: center;">500.0</td> </tr> <tr> <td style="text-align: center;">0.0</td> <td></td> <td></td> <td style="text-align: center;">0.0</td> <td style="text-align: center;">OHM-M</td> <td style="text-align: center;">20.</td> </tr> </table> | Natural Gamma |       | Conductivity |  | Induction |  | 0.0 | API Units | 200.0 | 0.0 | MSM | 500.0 | 0.0 |  |  | 0.0 | OHM-M | 20. |
|------------------|-----------|--------------|--|---------------|-------|--------------|--|-----------|--|-----|-----------|-------|-----|-----|-------|-----|--|--|-----|-------|-----|
| Natural Gamma    |           | Conductivity |  | Induction     |       |              |  |           |  |     |           |       |     |     |       |     |  |  |     |       |     |
| 0.0              | API Units | 200.0        | 0.0  | MSM           | 500.0 |              |  |           |  |     |           |       |     |     |       |     |  |  |     |       |     |
| 0.0              |           |              | 0.0  | OHM-M         | 20.   |              |  |           |  |     |           |       |     |     |       |     |  |  |     |       |     |

|       |   |                               |
|-------|---|-------------------------------|
| 37.40 | Silty Sand: Brown Start split spoon, 22 blows | Silty Sand: Not drive sampled |
|       | Clay: Brown, 12 Blows                         |                               |
|       | Clay: Brown                                   |                               |
|       | Clay: 11 Blows                                |                               |
|       | Clay  |                               |
| 37.30 | Clay: Fat Clay, 7 blows                       |                               |
|       | Clay  |                               |
|       | Clay: Damp 7 Blows                            |                               |
|       | Clay  |                               |
| 37.20 | Clay: Damp                                    |                               |
|       | Clay  |                               |
|       | Clay: 11 Blows                                |                               |
| 37.10 | NO LOGGING                                    |                               |





# Geophysical Logs Logs Run and Processed by United States Geological Survey

## LX Bar Area Golden Eagle Impoundment

### Well No. MW-1

On-site Geologist  
Webster

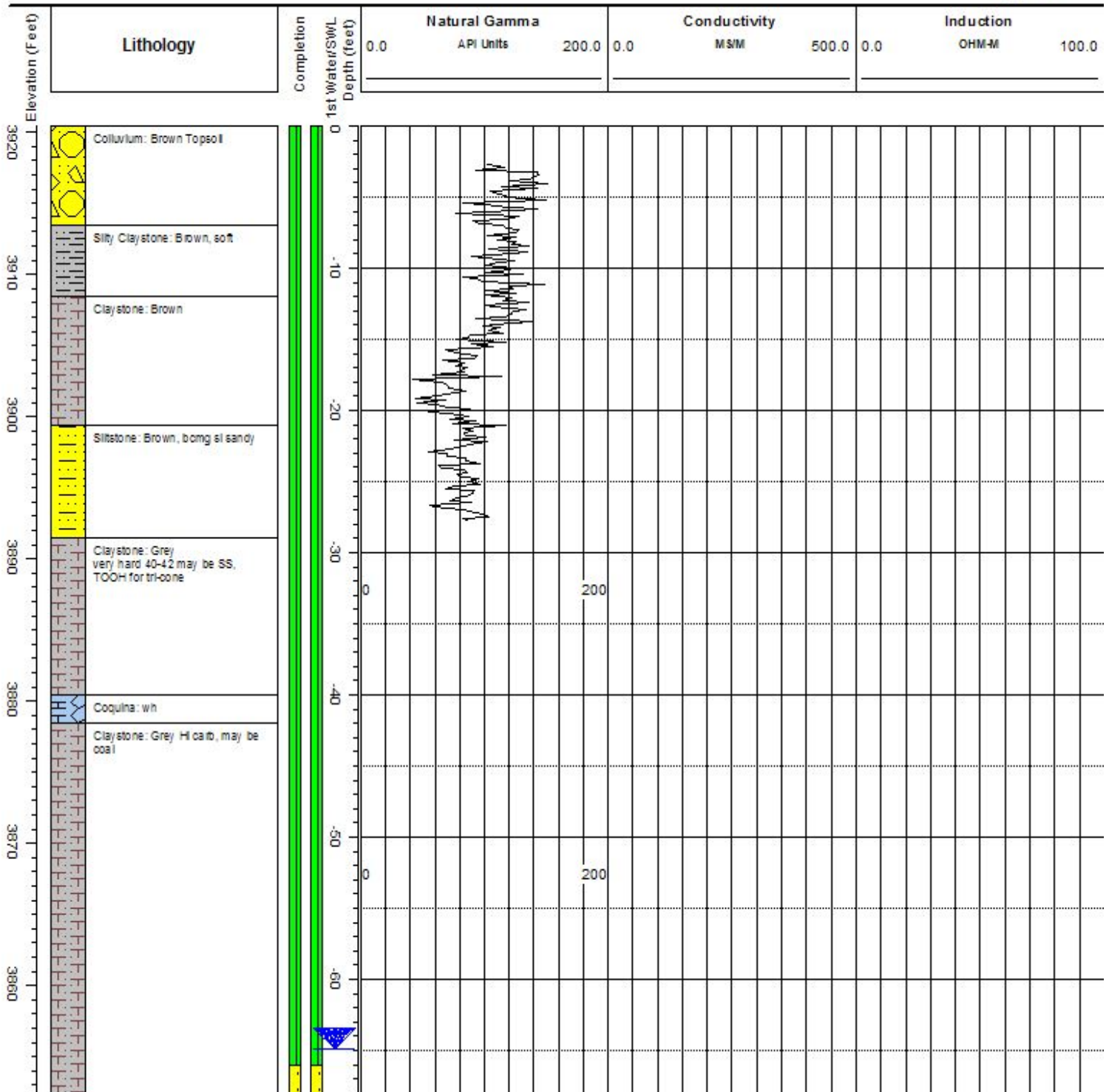
Latitude: 44°48'26.01904" Northing 1901305.48  
 Longitude: 105°50'46.06339" Easting 1698312.44  
 GL Elevation 3920.43

Total Depth: 87  
 Qtr Qtr: NENE  
 Section: 26  
 Township 56N  
 Range 75W

Drilling Contractor Interstate Drilling  
 Driller Dave Proctor

Drilling Dates 6-23-06  
 Hole Diameter 5-7/8"

**Comments: 27 feet of Natural Gamma ONLY Geophysical Log run  
 SWL from 12-8-06**







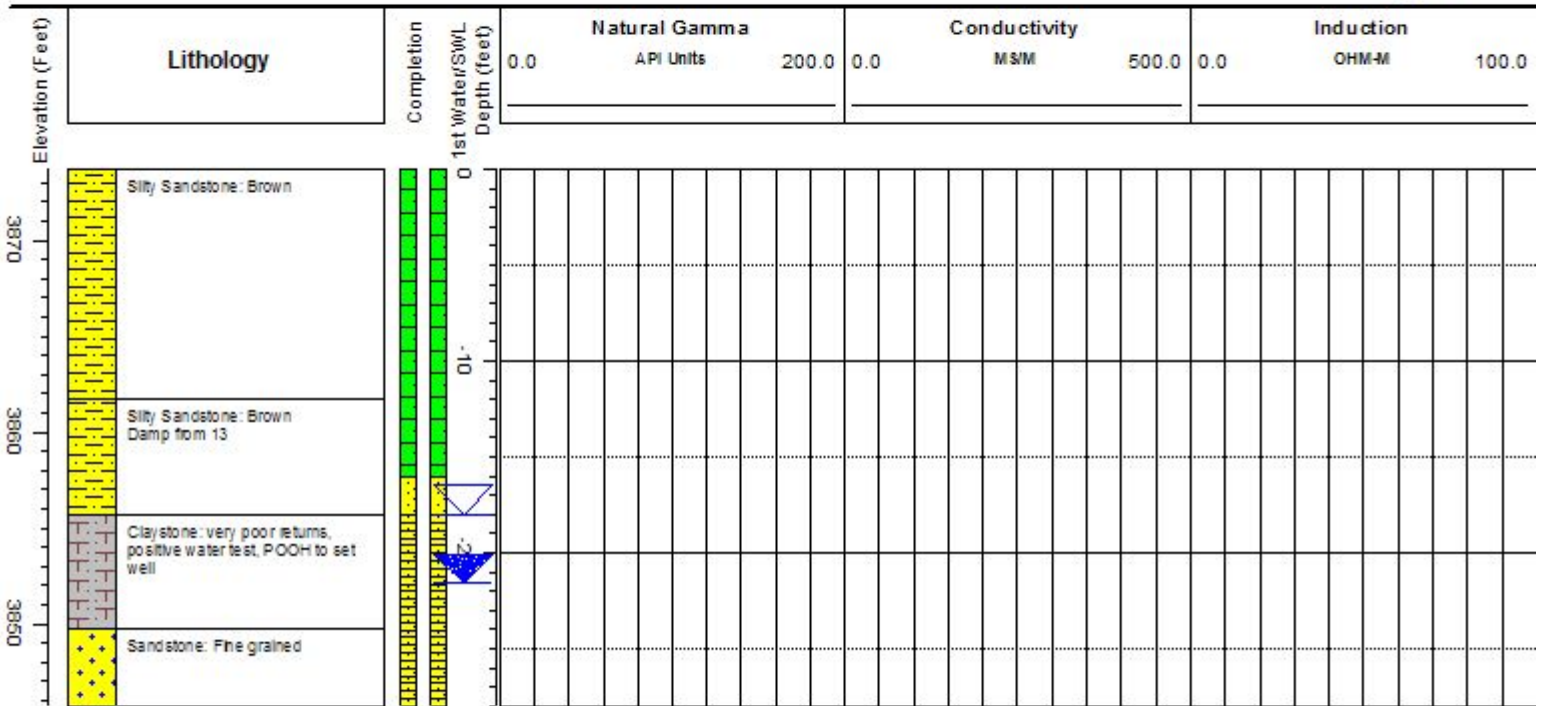
# Geophysical Logs Logs Run and Processed by United States Geological Survey

## LX Bar Area Golden Eagle Impoundment

### Well No. MW-2

|  |  |                        |
|--|--|------------------------|
| On-site Geologist<br><u>Webster</u>            | Latitude: <u>44°48'17.31163"</u> Northing <u>1900429.63</u>  | Total Depth: <u>26</u> |
|  | Longitude: <u>105°50'41.55974"</u> Easting <u>1698653.27</u> | Qtr Qtr: <u>SENE</u>   |
|  | GL Elevation <u>3873.70</u>                                  | Section: <u>26</u>     |
| Drilling Contractor <u>Interstate Drilling</u> | Drilling Dates <u>6-24-06</u>                                | Township <u>56N</u>    |
| Driller <u>Dave Proctor</u>                    | Hole Diameter <u>5-7/8"</u>                                  | Range <u>75W</u>       |

**Comments: NO Geophysical Logs Run  
SWL from 12-6-06**



**Major Ion Chemistry (mg/L)**

|          |                |
|----------|----------------|
| Ca = 475 | CO2/HCO3 = 780 |
| Mg = 429 | SO4 = 3740     |
| Na = 652 | TDS = 6450     |

| Natural Gamma<br>API Units | Conductivity<br>M/M | Induction<br>OHM-M |
|----------------------------|---------------------|--------------------|
| 0.0                        | 0.0                 | 0.0                |
| 200.0                      | 500.0               | 100.0              |

pH = 7.1  
SAR = 5

**WDEQ Ground Water Classification = IV**



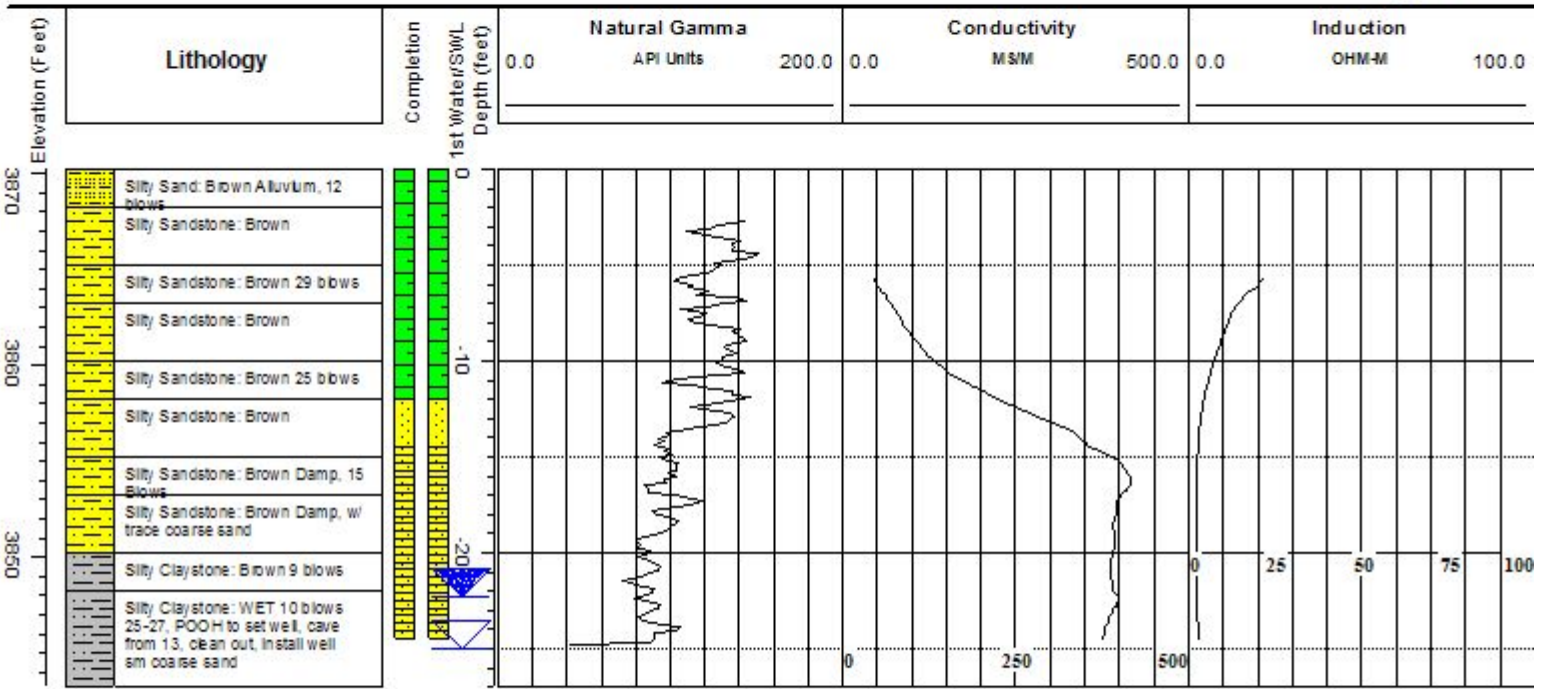
**Geophysical Logs** Logs Run and Processed by United States Geological Survey

**LX Bar Area Golden Eagle Impoundment**

**Well No. MW-3**

On-site Geologist **Terry Webster**      Latitude: 44°48'16.06870"    Northing 1900299.814    Total Depth: 27  
Longitude: 105°50'44.54532"    Easting 1698440.325    Qtr Qtr: SENE  
GL Elevation 3870.23    Section: 26  
Drilling Contractor Interstate Drilling    Drilling Dates 6-25-06    Township 56N  
Driller Dave Proctor    Hole Diameter 7-1/2"    Range 75W

**Comments:** Natural Gamma Curve smoothed due to excessive electronic noise  
SWL on 12-8-06



**Major Ion Chemistry (mg/L)**  
Ca = 427      CO<sub>2</sub>/HCO<sub>3</sub> = 622  
Mg = 691      SO<sub>4</sub> = 4659  
Na = 550      TDS = 7920

| Natural Gamma<br>API Units | Conductivity<br>M/M | Induction<br>OHM-M |
|----------------------------|---------------------|--------------------|
| 0.0                        | 0.0                 | 0.0                |
| 200.0                      | 500.0               | 100.0              |

pH = 7.22  
SAR = 4

**WDEQ Ground Water Classification = IV**





**Prairie Dog Area Joe Draw Jr Impoundment**

**Well No. MW-1**

On-site Geologist  
**Webster**

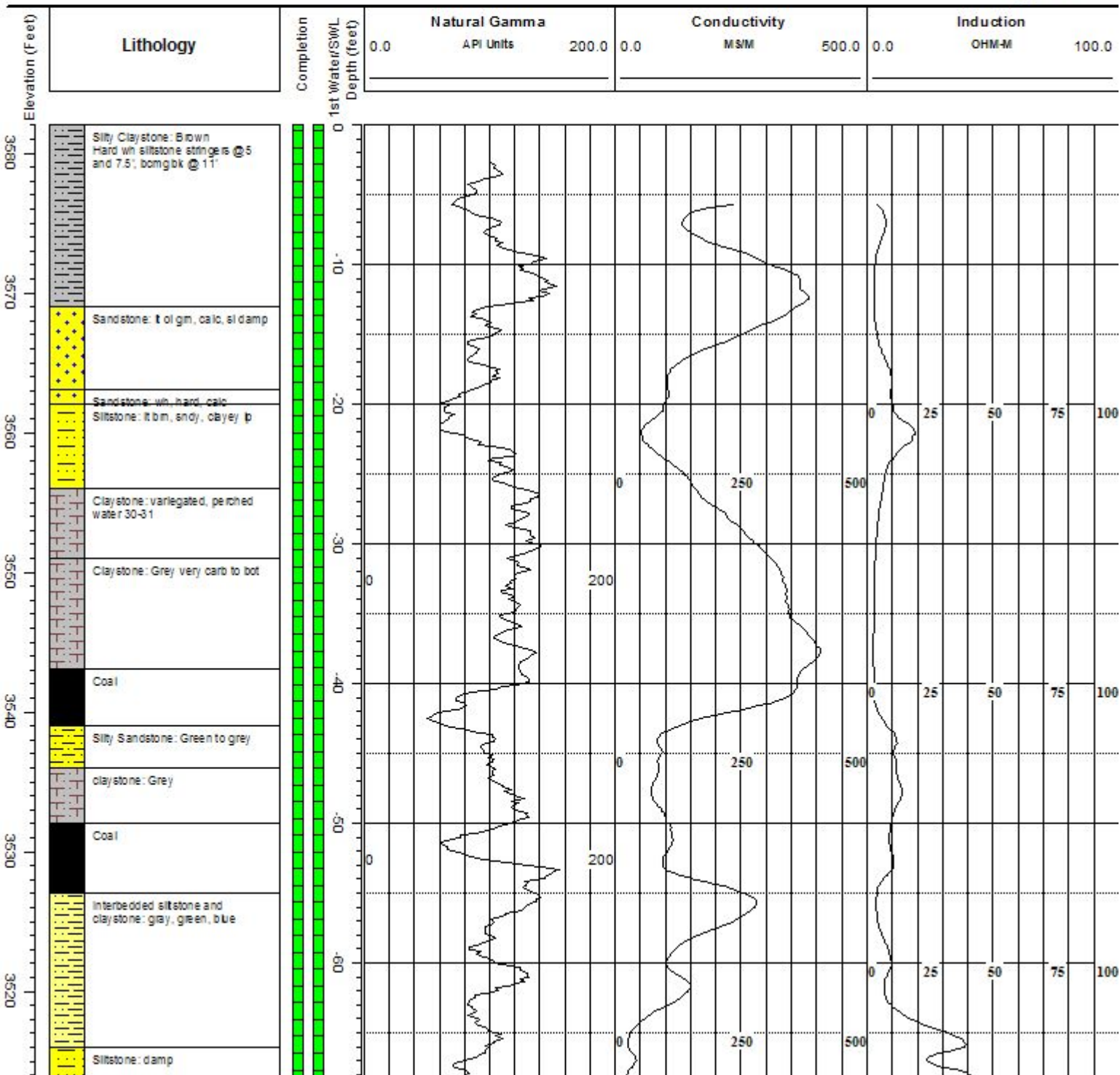
Latitude: 44°57'03.91205" Northing 1950613.68  
 Longitude: -106°50'17.19139" Easting 1440540.63  
 GL Elevation 3582.04

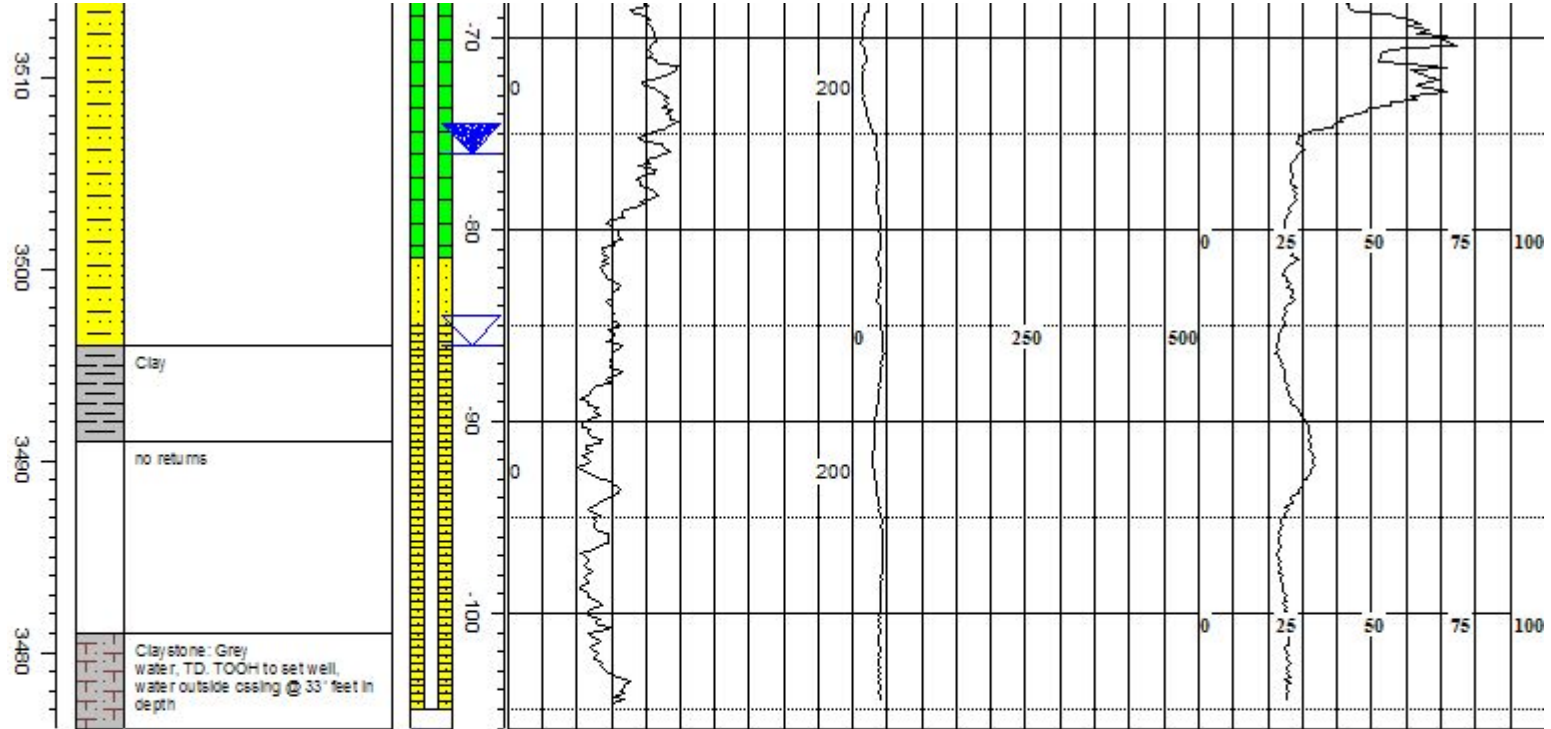
Total Depth: 106  
 Qtr Qtr: SESW  
 Section: 35  
 Township 58N  
 Range 83W

Drilling Contractor Interstate Drilling  
 Driller Dan Krueger

Drilling Dates 6/11/2006  
 Hole Diameter 5-7/8"

Comments: Natural Gamma Curve smoothed due to excessive electronic noise  
 SWL from 10-16-06 -- First water questionable due to drilling conditions





**Major Ion Chemistry (mg/L)**  
 Ca = 6      CO<sub>2</sub>/HCO<sub>3</sub> = 926  
 Mg = 2      SO<sub>4</sub> = 0  
 Na = 316    TDS = 1116

| Natural Gamma<br>API Units |       | Conductivity<br>M/S/M |       | Induction<br>OHM-M |       |
|----------------------------|-------|-----------------------|-------|--------------------|-------|
| 0.0                        | 200.0 | 0.0                   | 500.0 | 0.0                | 100.0 |

pH = 7.83  
SAR = 28

**WDEQ Ground Water Classification = III**





# Geophysical Logs Logs Run and Processed by United States Geological Survey

## Prairie Dog Area Joe Draw Jr Impoundment

### Well No. MW-2

On-site Geologist  
Webster

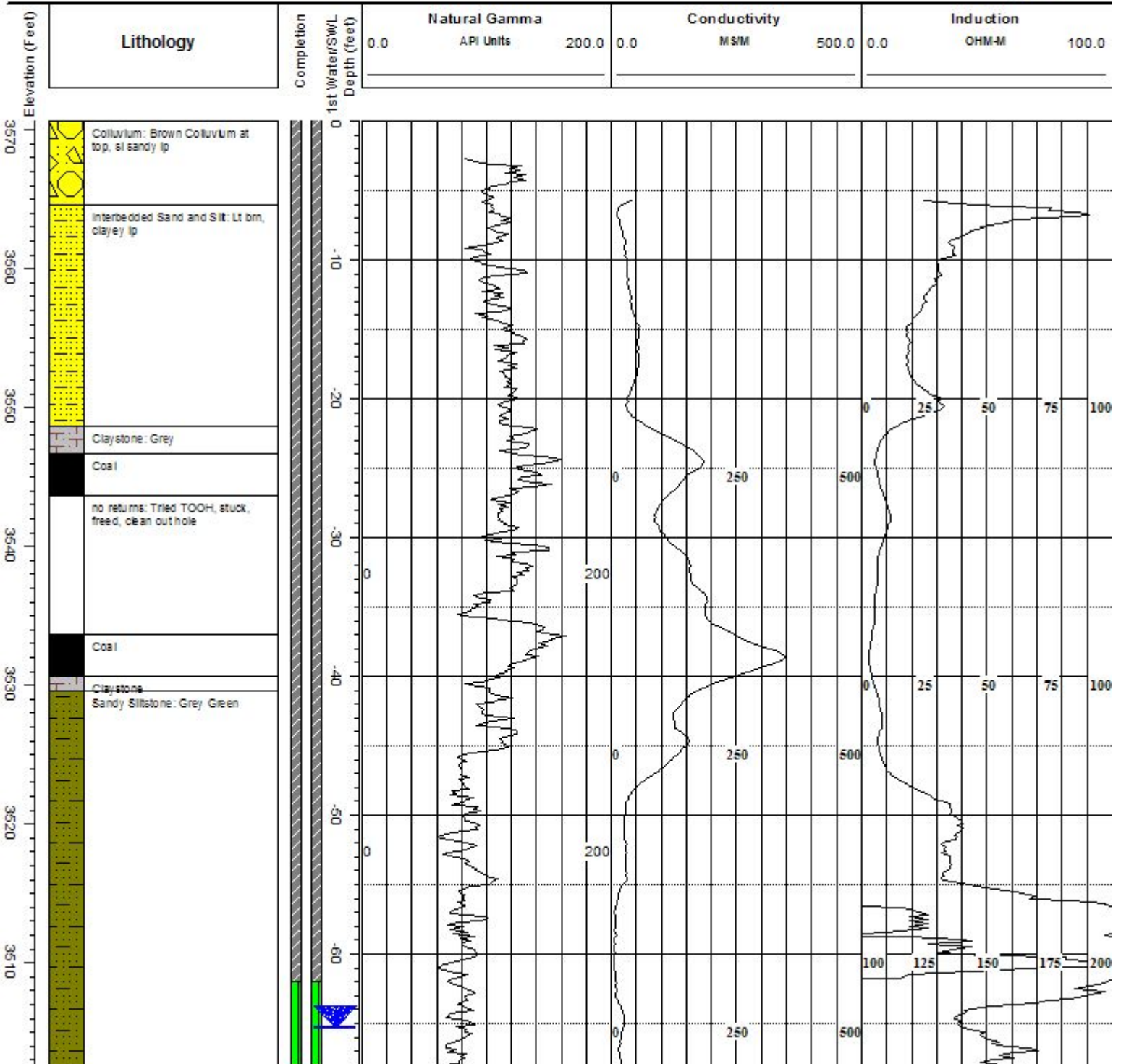
Latitude: 44°57'05.25621" Northing 1950748.76  
 Longitude: -106°50'19.55964" Easting 1440369.49  
 GL Elevation 3570.65

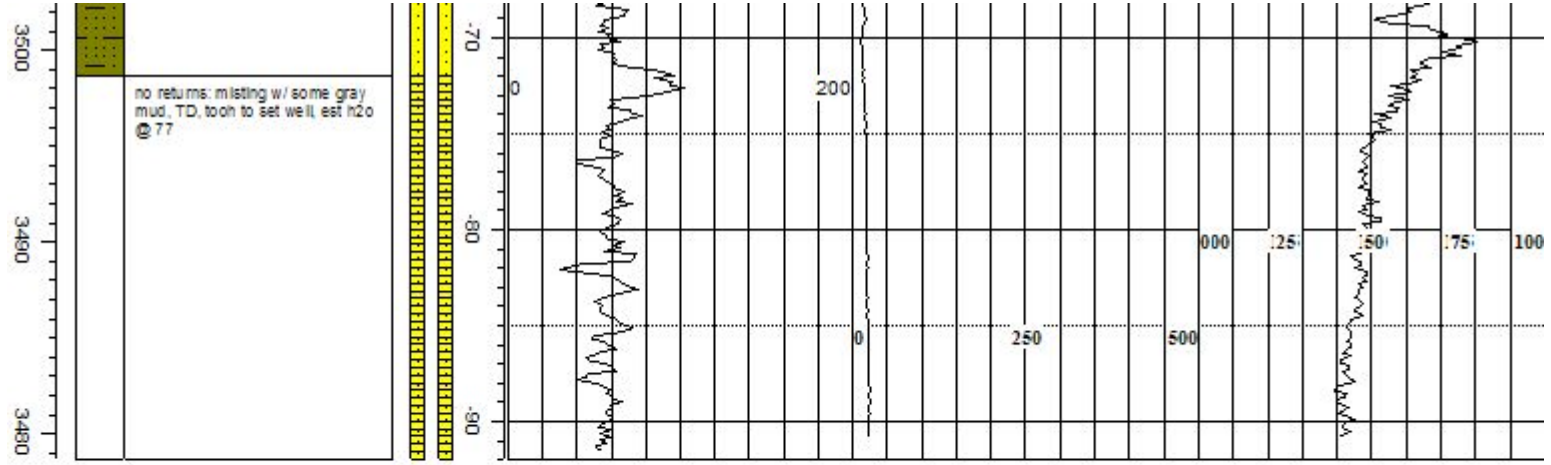
Total Depth: 92  
 Qtr Qtr: SESW  
 Section: 35  
 Township 58N  
 Range 83W

Drilling Contractor Interstate Drilling  
 Driller Dan Krueger

Drilling Dates 6/12/2006  
 Hole Diameter 5-7/8"

Comments: Natural Gamma Curve smoothed due to excessive electronic noise  
 Swl from 10-25-06





**Major Ion Chemistry (mg/L)**  
 Ca = 27      CO2/HCO3 = 981  
 Mg = 3      SO4 = 0  
 Na = 351    TDS = 1160

| Natural Gamma<br>API Units |       | Conductivity<br>M/S/M |       | Induction<br>OHM-M |       |
|----------------------------|-------|-----------------------|-------|--------------------|-------|
| 0.0                        | 200.0 | 0.0                   | 500.0 | 0.0                | 100.0 |

pH = 8.04  
 SAR = 17

**WDEQ Ground Water Classification = III**



# Geophysical Logs Logs Run and Processed by United States Geological Survey

## Prairie Dog Area Joe Draw Jr Impoundment Well No. MW-3

On-site Geologist  
Webster

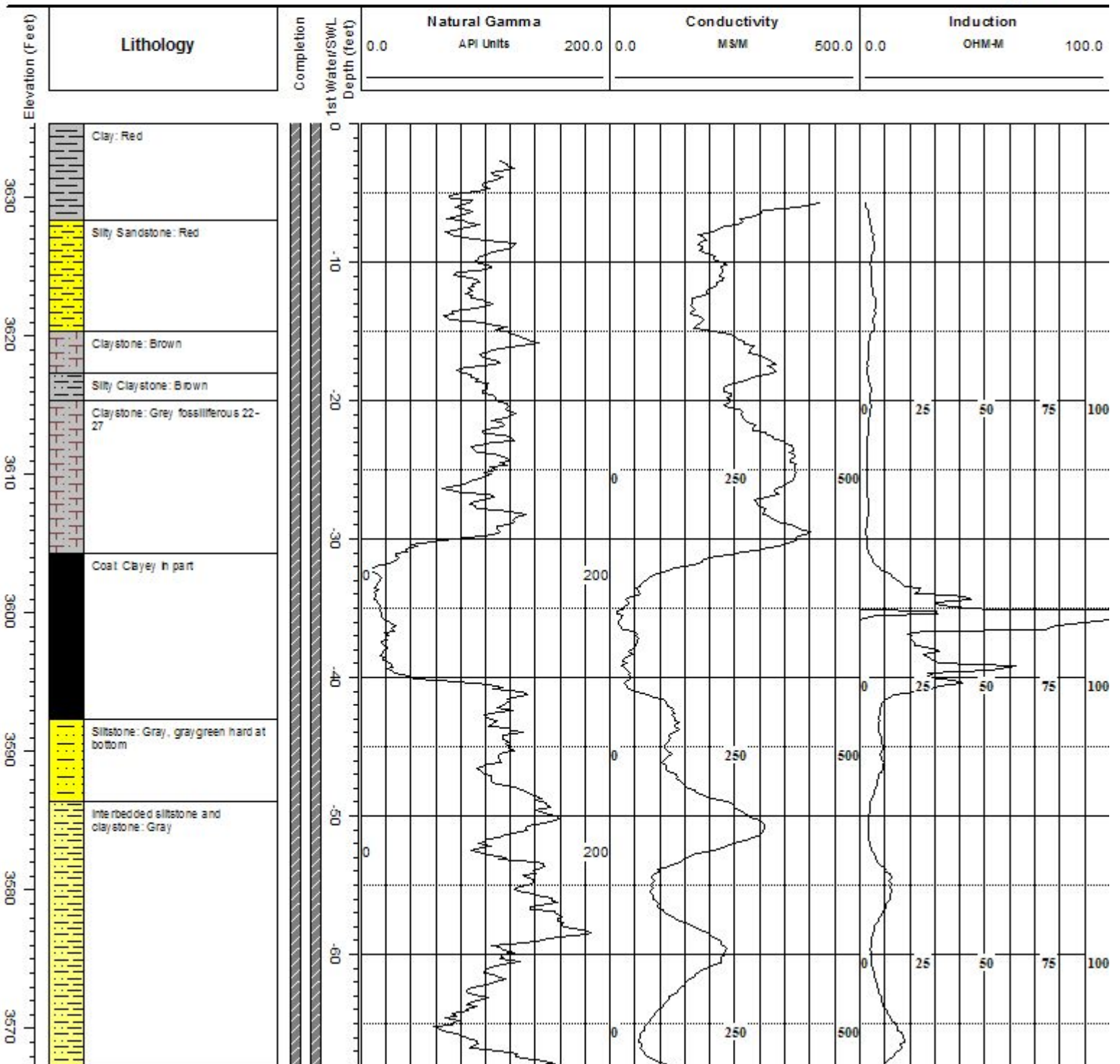
Latitude: 44°57'00.83811" Northing 1950306.69  
Longitude: -106°50.07.38950" Easting 1441247.42  
GL Elevation 3635.36

Total Depth: 167  
Qtr Qtr: NENW  
Section: 2  
Township 57N  
Range 83W

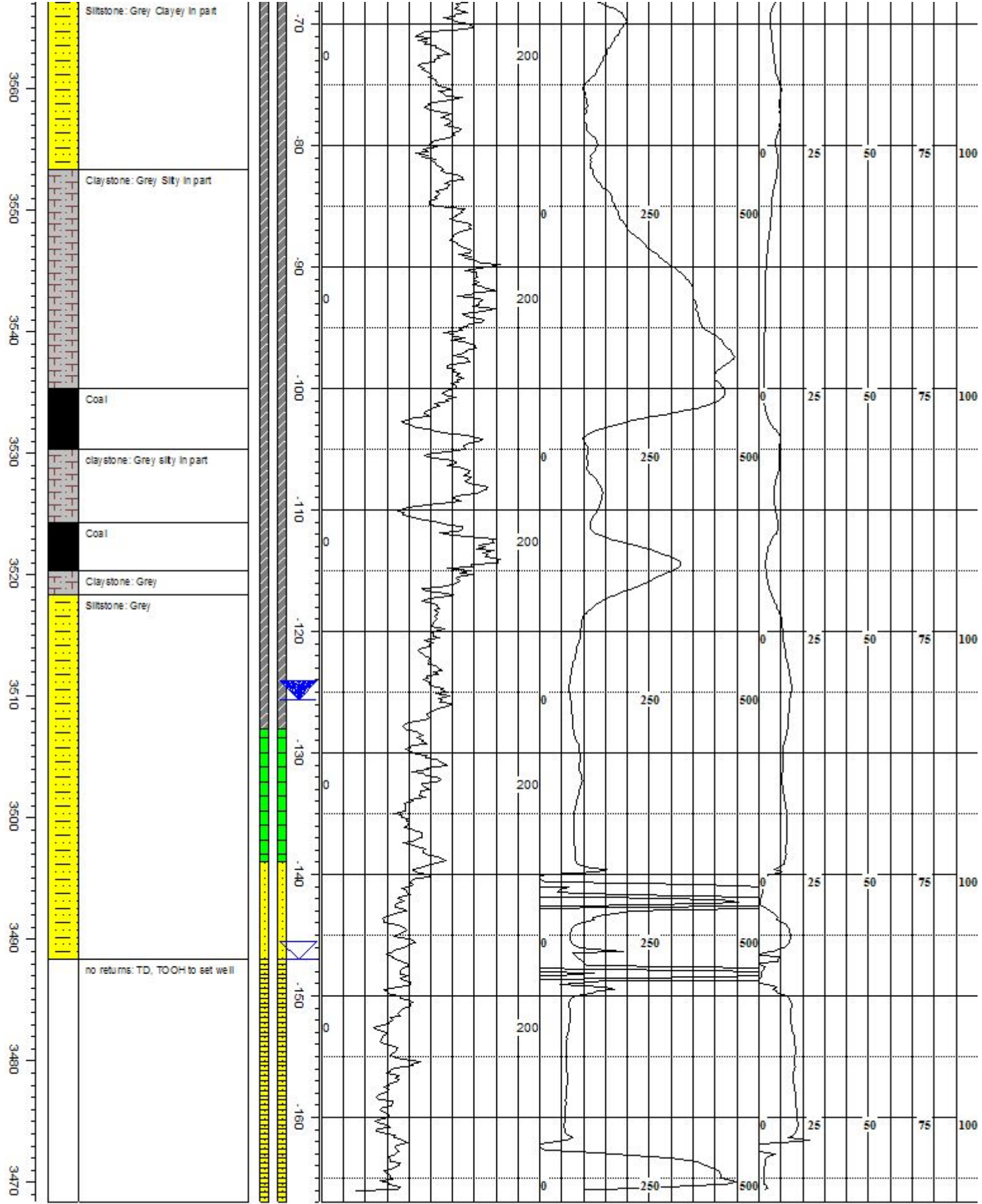
Drilling Contractor Interstate Drilling  
Driller Dan Krueger

Drilling Dates 6/12-13/2006  
Hole Diameter 5-7/8"

Comments: All Curves Smoothed due to excessive electronic noise  
SWL from 10-5-06







**Major Ion Chemistry (mg/L)**

Ca = 21      CO<sub>2</sub>/HCO<sub>3</sub> = 1128

Mg = 3      SO<sub>4</sub> = 0

Na = 382      TDS = 1464

0.0      **Natural Gamma**  
API Units      200.0

0.0      **Conductivity**  
M/S/M      500.0

0.0      **Induction**  
OHM-M      100.0

pH = 8.15

SAR = 21

**WDEQ Ground Water Classification = III**



Prairie Dog Area

Lori Impoundment

Well No. PD-1

On-site Geologist  
Terry Webster

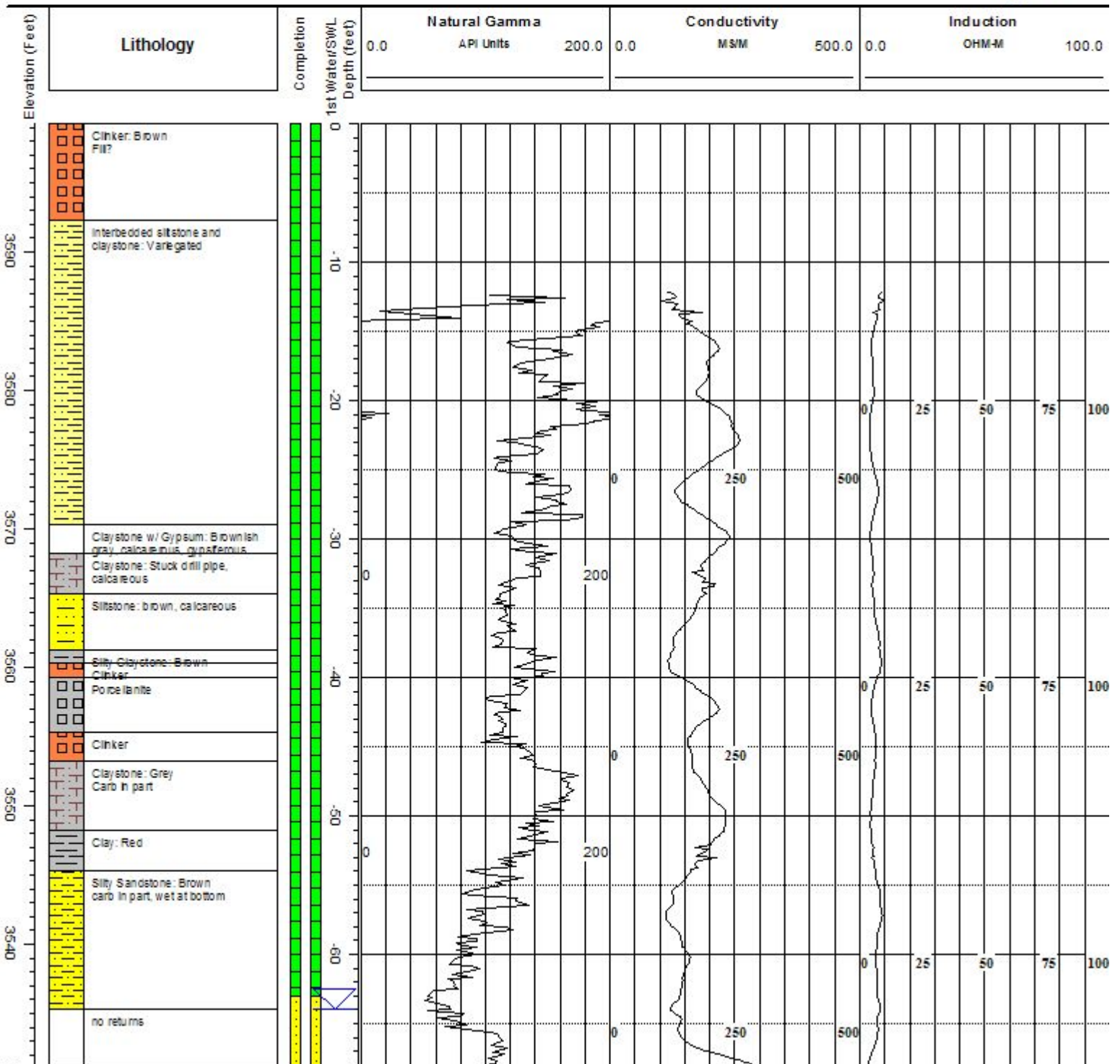
Latitude: 44°57'40.54044" Northing 1954354.77  
 Longitude: -106°49'06.50550" Easting 1445600.31  
 GL Elevation 3599.27

Total Depth: 120  
 Qtr Qtr: SENW  
 Section: 36  
 Township: 58N  
 Range: 83W

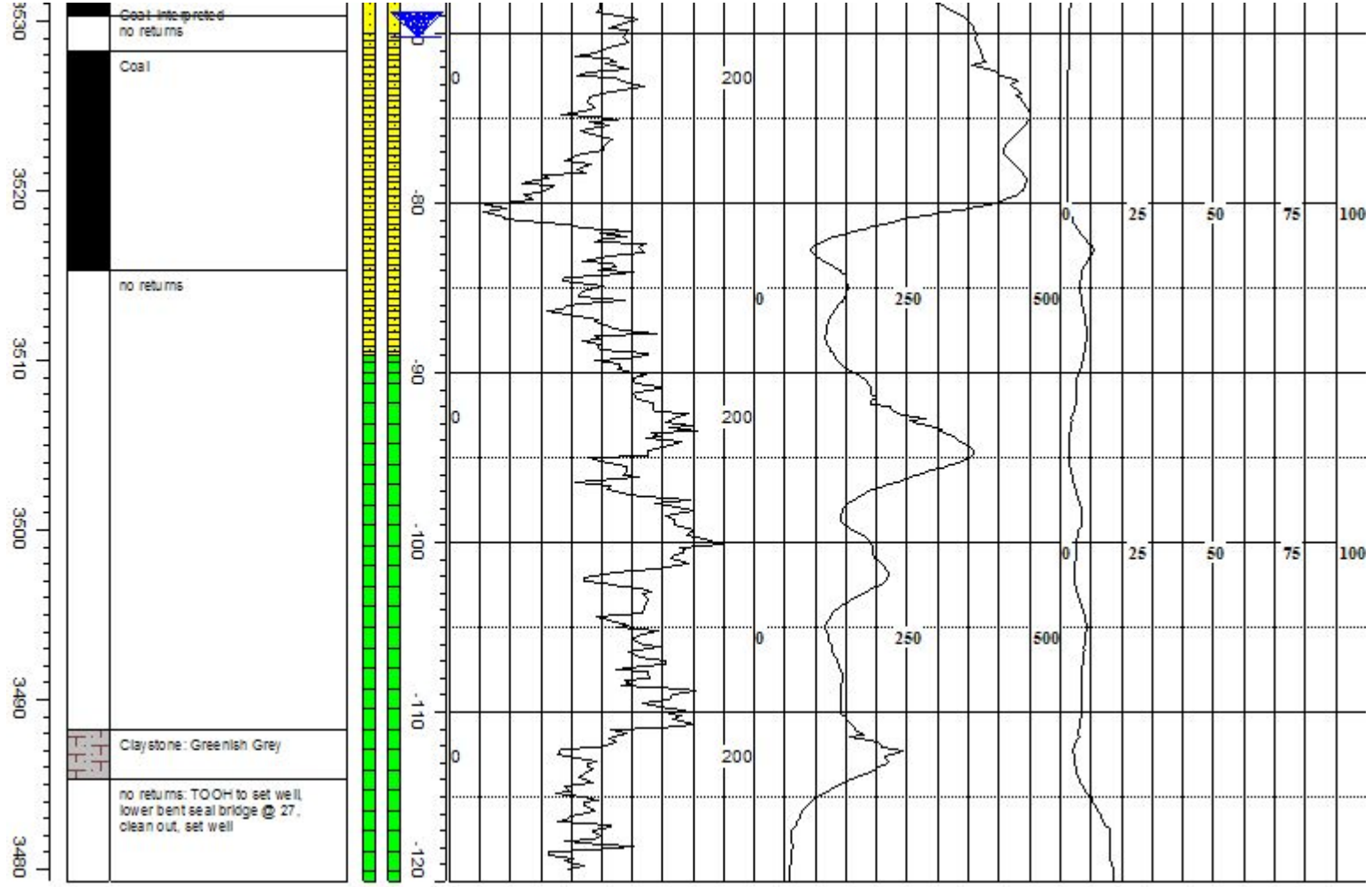
Drilling Contractor Interstate Drilling  
 Driller Dan Krueger

Drilling Dates 5-24-2006  
 Hole Diameter 5-7/8"

Comments: SWL from 10-24-06







**Major Ion Chemistry (mg/L)**  
 Ca = 251      CO<sub>2</sub>/HCO<sub>3</sub> = 1840  
 Mg = 214      SO<sub>4</sub> = 3128  
 Na = 1130      TDS = 5732

| Natural Gamma<br>API Units | Conductivity<br>MS/M | Induction<br>OHM-M |
|----------------------------|----------------------|--------------------|
| 0.0      200.0             | 0.0      500.0       | 0.0      100.0     |

pH = 6.82  
 SAR = 13

**WDEQ Ground Water Classification = IV**



Prairie Dog Area

Lori Impoundment

Well No. MW-1

On-site Geologist  
Webster

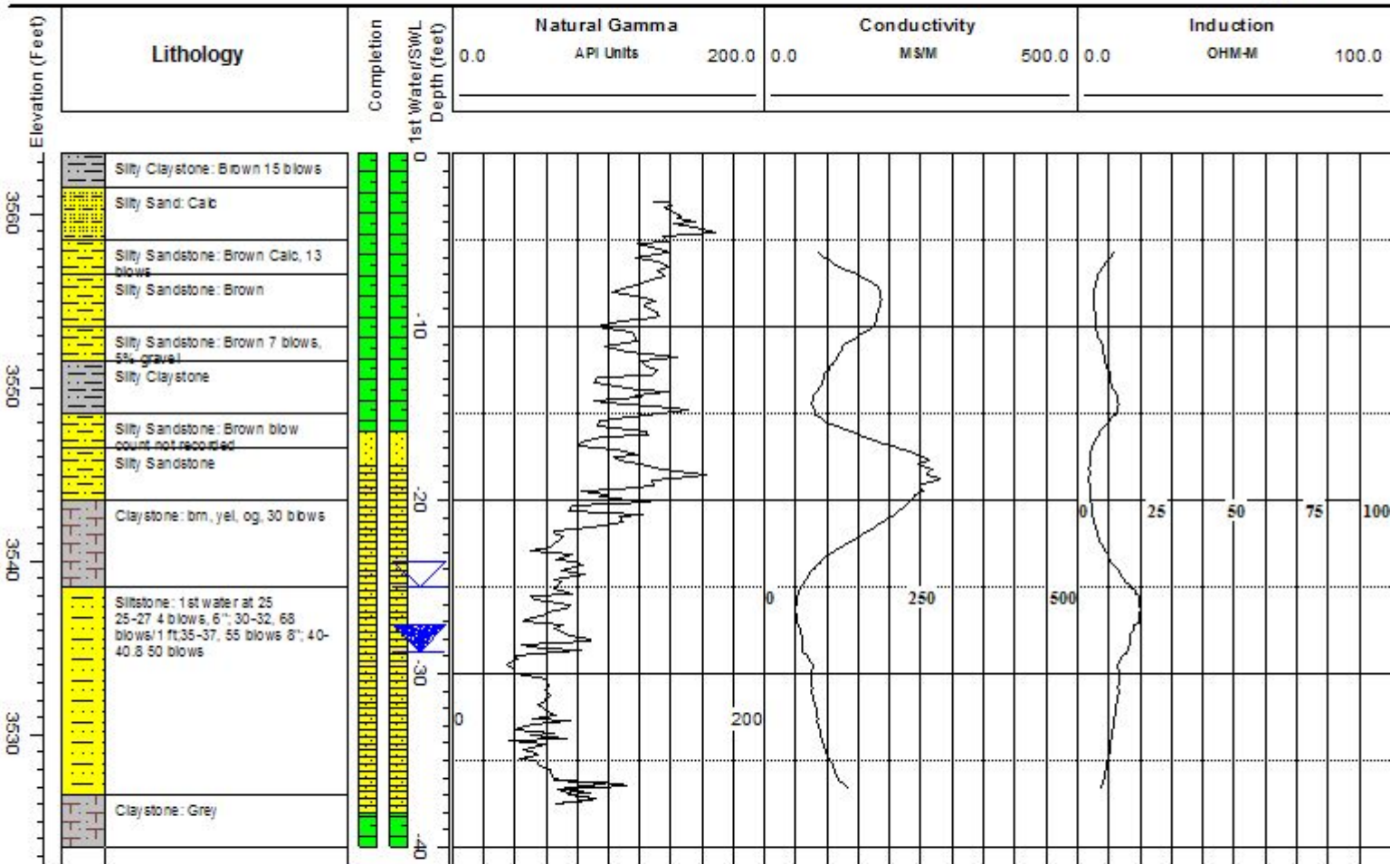
Latitude: 44°57'31.86098" Northing 1953476.51  
 Longitude: -106°49'04.90558" Easting 1445720.94  
 GL Elevation 3563.53

Total Depth: 41  
 Qtr Qtr: NESW  
 Section: 36  
 Township 58N  
 Range 83W

Drilling Contractor Interstate Drilling  
 Driller Dan Krueger

Drilling Dates 5/20/2006  
 Hole Diameter 7-1/2"

Comments: All geophysical log traces appear reversed  
SWL from 10-18-06



**Major Ion Chemistry (mg/L)**  
 Ca = 177      CO2/HCO3 = 1030  
 Mg = 184      SO4 = 2653  
 Na = 938      TDS = 5148

0.0      Natural Gamma      200.0      0.0      Conductivity      500.0      0.0      Induction      100.0  
 API Units      MS/M      OHM-M

pH = 7.39  
 SAR = 12

**WDEQ Ground Water Classification = IV**



Prairie Dog Area

Lori Impoundment

Well No. MW-1

On-site Geologist  
Webster

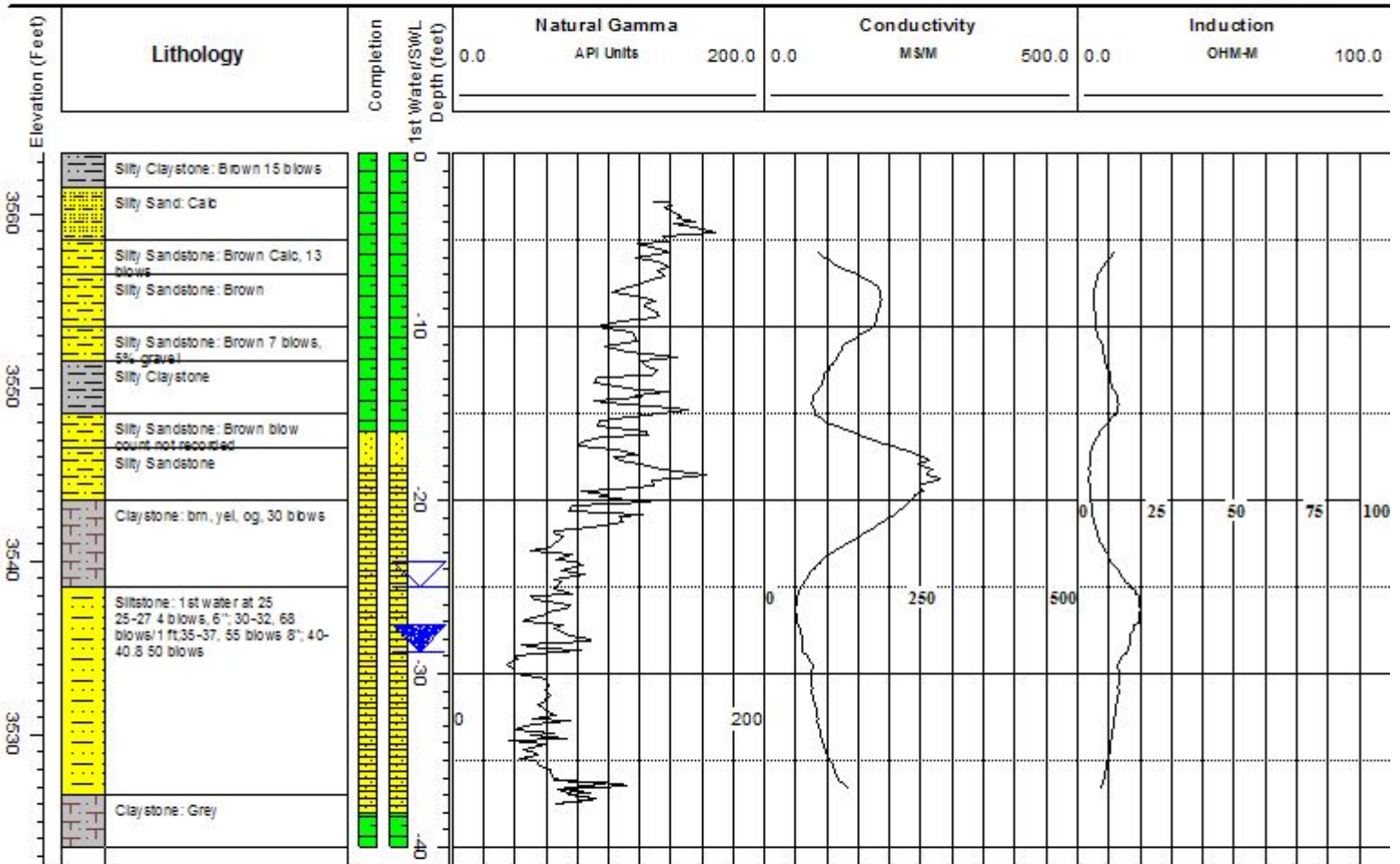
Latitude: 44°57'31.86098" Northing 1953476.51  
 Longitude: -106°49'04.90558" Easting 1445720.94  
 GL Elevation 3563.53

Total Depth: 41  
 Qtr Qtr: NESW  
 Section: 36  
 Township 58N  
 Range 83W

Drilling Contractor Interstate Drilling  
 Driller Dan Krueger

Drilling Dates 5/20/2006  
 Hole Diameter 7-1/2"

Comments: All geophysical log traces appear reversed  
 SWL from 10-18-06



Major Ion Chemistry (mg/L)  
 Ca = 177      CO2/HCO3 = 1030  
 Mg = 184      SO4 = 2653  
 Na = 938      TDS = 5148

Natural Gamma (API Units) 0.0 to 200.0      Conductivity (MS/M) 0.0 to 500.0      Induction (OHM-M) 0.0 to 100.0

pH = 7.39  
 SAR = 12

**WDEQ Ground Water Classification = IV**





**Prairie Dog Area**

**Lori Impoundment**

**Well No. MW-4**

On-site Geologist  
**Terry Webster**

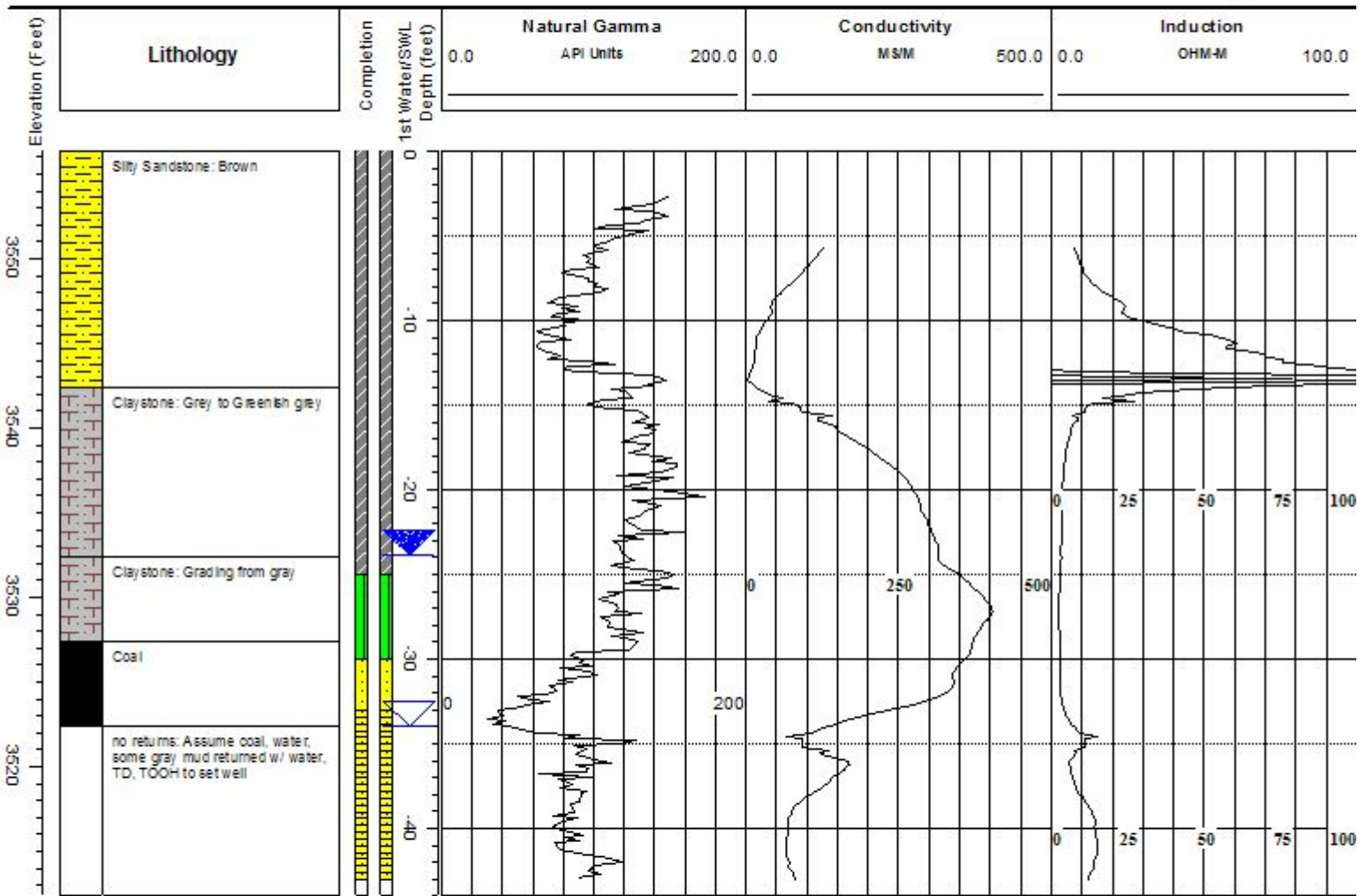
Latitude: 44°57'31.12699" Northing 1953401.04  
 Longitude: -106°49'07.12693" Easting 1445542.9  
 GL Elevation 3556.35

Total Depth: 44  
 Qtr Qtr: NESW  
 Section: 16  
 Township: 58N  
 Range: 83W

Drilling Contractor Interstate Drilling  
 Driller Dan Krueger

Drilling Dates 5-22-2006  
 Hole Diameter 5-7/8"

Comments: SWL from 5/22/06, Not recorded on sampling date 10-24-06



**Major Ion Chemistry (mg/L)**  
 Ca = 156      CO2/HCO3 = 1146  
 Mg = 94      SO4 = 1168  
 Na = 603      TDS = 2840

Natural Gamma API Units      Conductivity M/S/M      Induction OHM-M

pH = 6.84  
 SAR = 9

**WDEQ Ground Water Classification = III**



Prairie Dog Area

Sandy Impoundment

Well No. MW-1

On-site Geologist  
Webster

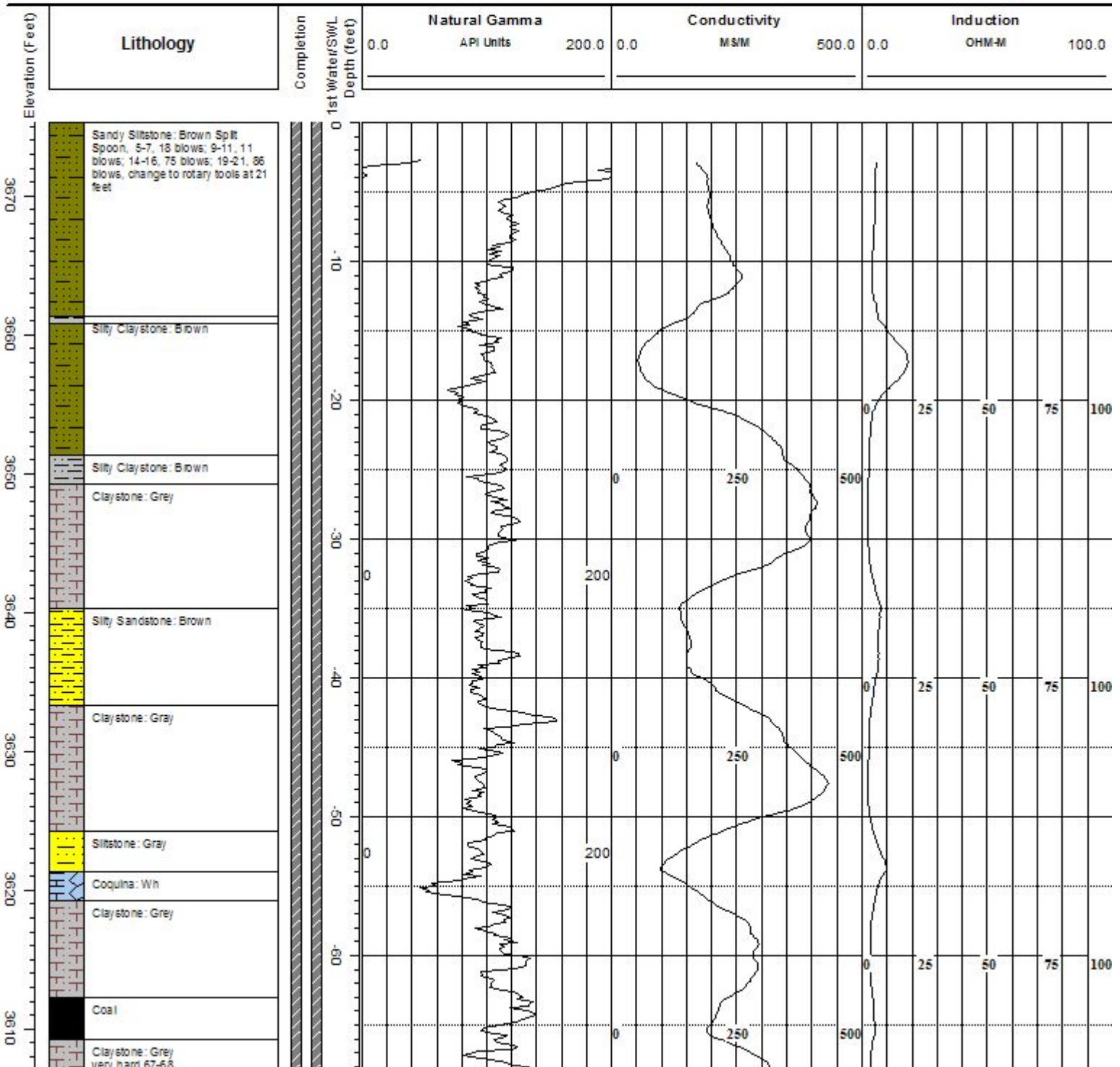
Latitude: 44°57'11.50839" Northing 1951338.11  
 Longitude: -106°52'02.46863" Easting 1432965.39  
 GL Elevation 3675.29

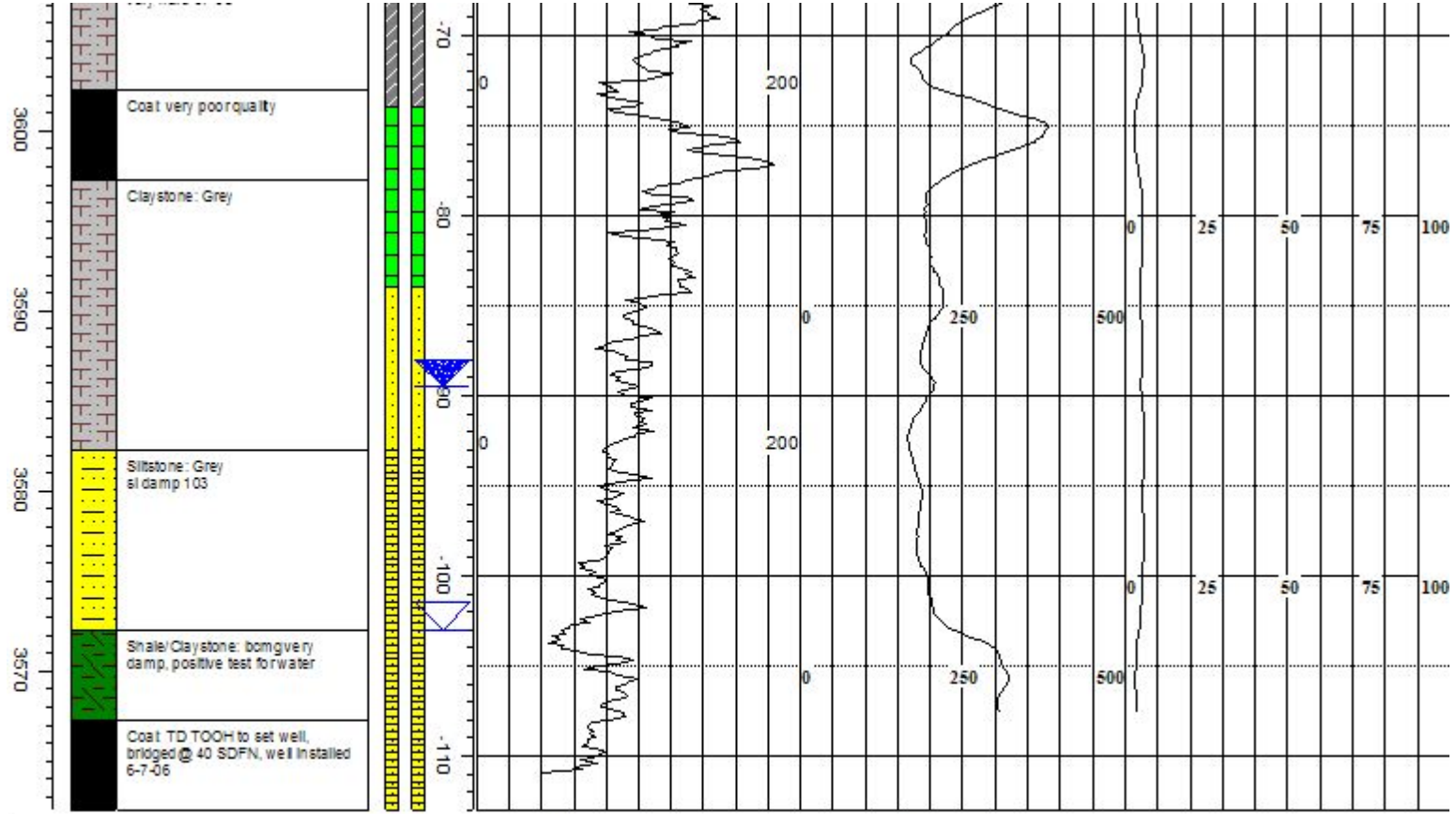
Total Depth: 113  
 Qtr Qtr: SESE  
 Section: 33  
 Township 57N  
 Range 83W

Drilling Contractor Interstate Drilling  
 Driller Dan Krueger

Drilling Dates 6/06-07/2006  
 Hole Diameter 5-7/8"

Comments: Natural Gamma curve smoothed to aid in interpretation  
 SWL from 10-2-06





**Major Ion Chemistry (mg/L)**

Ca = 30      CO2/HCO3 = 963  
Mg = 226      SO4 = 3464  
Na = 964      TDS = 5816

| Natural Gamma<br>API Units | Conductivity<br>M/S/M | Induction<br>OHM-M |
|----------------------------|-----------------------|--------------------|
| 0.0                        | 0.0                   | 0.0                |
| 200.0                      | 500.0                 | 100.0              |

pH = 7.12  
SAR = 13

**WDEQ Ground Water Classification = IV**





**Prairie Dog Area**

**Sandy Impoundment**

**Well No. MW-2**

On-site Geologist  
Webster

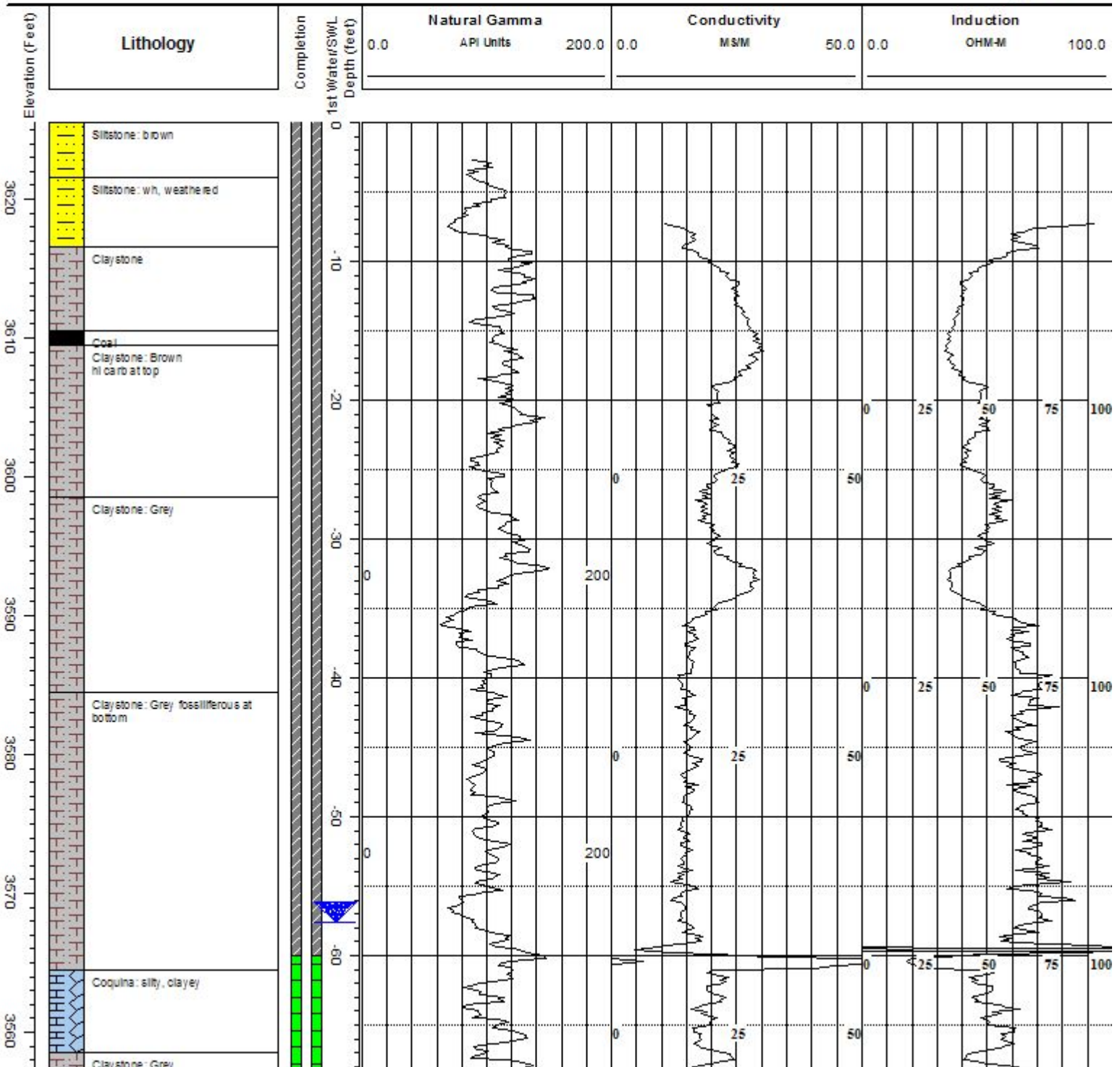
Latitude: 44°57'15.32785" Northing 1951728.72  
 Longitude: 106°51'53.27517" Easting 1433624.26  
 GL Elevation 3625.52

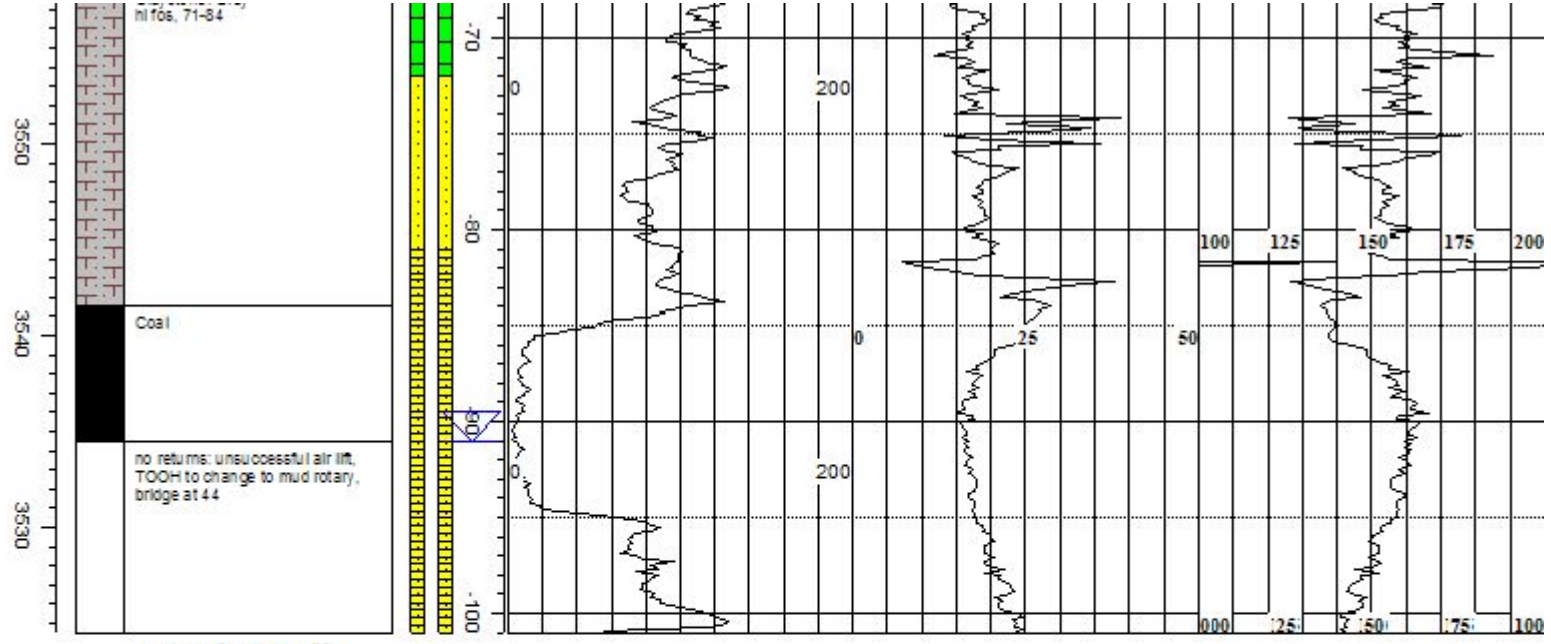
Total Depth: 101  
 Qtr Qtr: SESE  
 Section: 33  
 Township 57N  
 Range 83W

Drilling Contractor Interstate Drilling  
 Driller Dan Krueger

Drilling Dates 6-7-2006  
 Hole Diameter 5-7/8"

Comments: Natural Gamma Curve Smoothed to aid interpretation  
SWL from 10-3-06





**Major Ion Chemistry (mg/L)**

Ca = 188      CO<sub>2</sub>/HCO<sub>3</sub> = 573

Mg = 63      SO<sub>4</sub> = 3060

Na = 1320    TDS = 5288

| Natural Gamma<br>API Units | Conductivity<br>MS/M | Induction<br>OHM-M |
|----------------------------|----------------------|--------------------|
| 0.0                        | 0.0                  | 0.0                |
| 200.0                      | 50.0                 | 100.0              |

pH = 7.64

SAR = 21

**WDEQ Ground Water Classification = IV**



Prairie Dog Area

Sandy Impoundment

Well No. MW-3

On-site Geologist  
Terry Webster

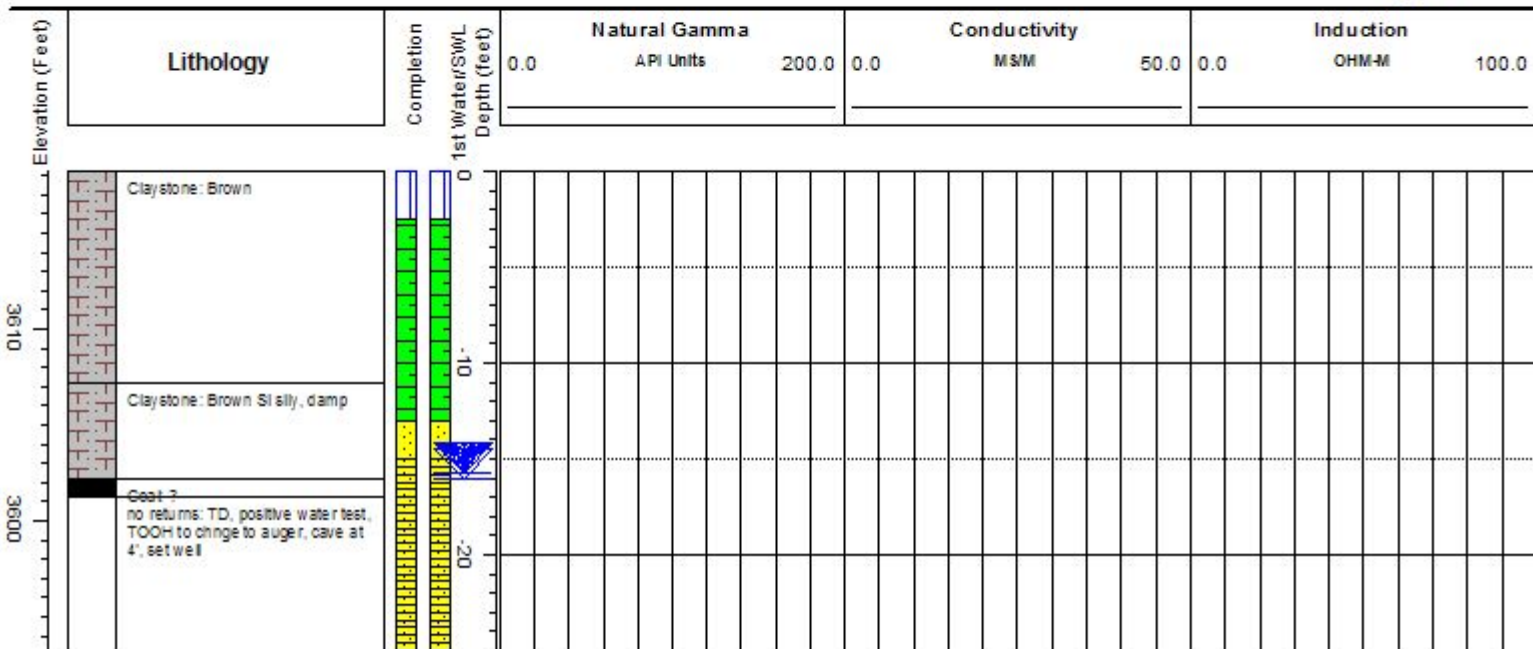
Latitude: 44°57'13.39706" Northing 1951533.32  
 Longitude: -106°51'52.94648" Easting 1433649.03  
 GL Elevation 3618.22

Total Depth: 25  
 Qtr Qtr: SESE  
 Section: 33  
 Township 57N  
 Range 83W

Drilling Contractor Interstate Drilling  
 Driller Dan Krueger

Drilling Dates 6-11-2006  
 Hole Diameter 7-1/2"

Comments: Geophysical logs not run  
SWL: from 10-4-06



**Major Ion Chemistry (mg/L)**

Ca = 539      CO2/HCO3 = 829  
 Mg = 408      SO4 = 3290  
 Na = 609      TDS = 5080

pH = 6.86  
 SAR = 5

**WDEQ Ground Water Classification = IV**





# Geophysical Logs Logs Run and Processed by United States Geological Survey

## LX Bar Area

## Termo Impoundment

### Well No. MW-1

On-site Geologist  
Webster

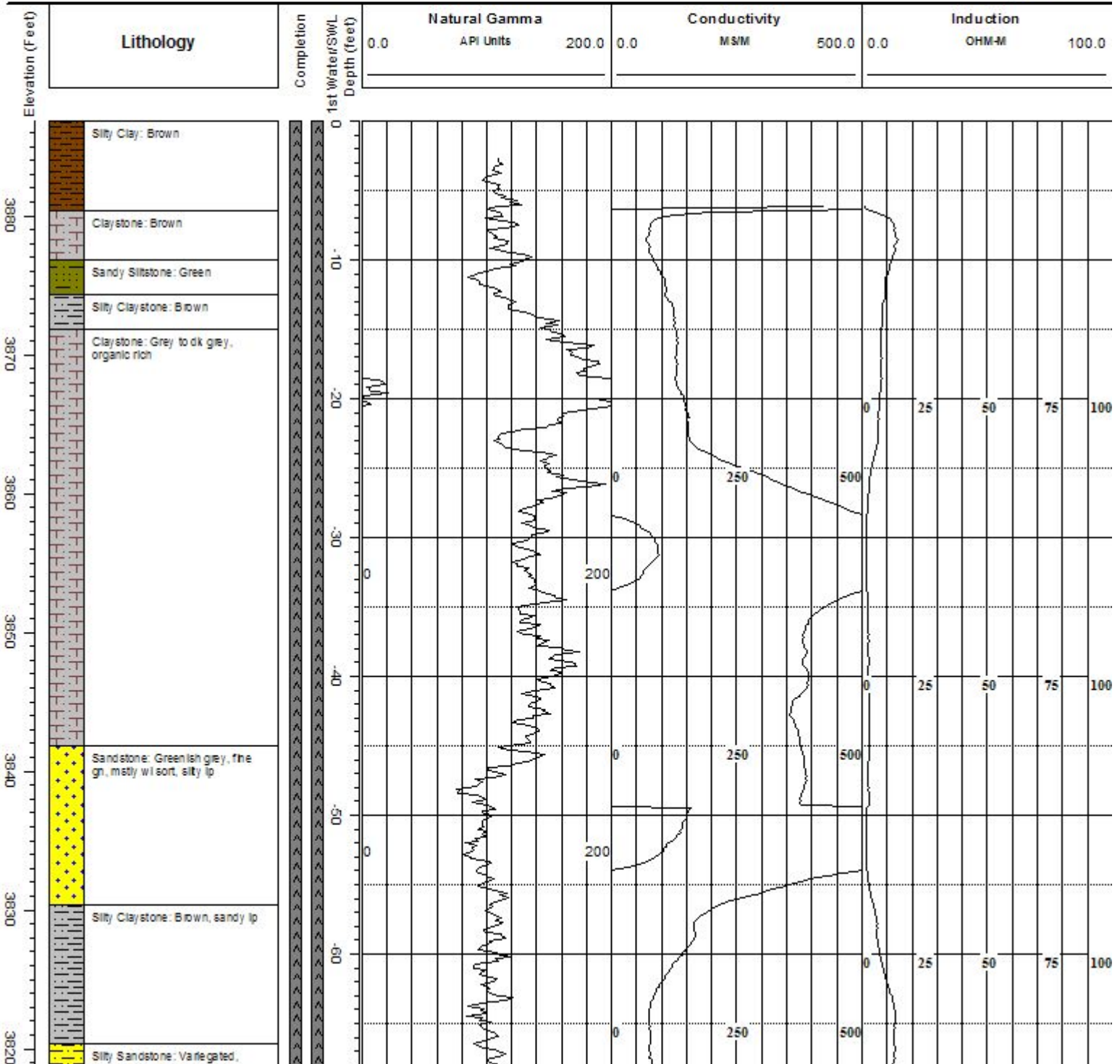
Latitude: 44°50'04.77249" Northing 1911172.772  
 Longitude: 105°52'28.21364" Easting 1690768.625  
 GL Elevation 3886.84

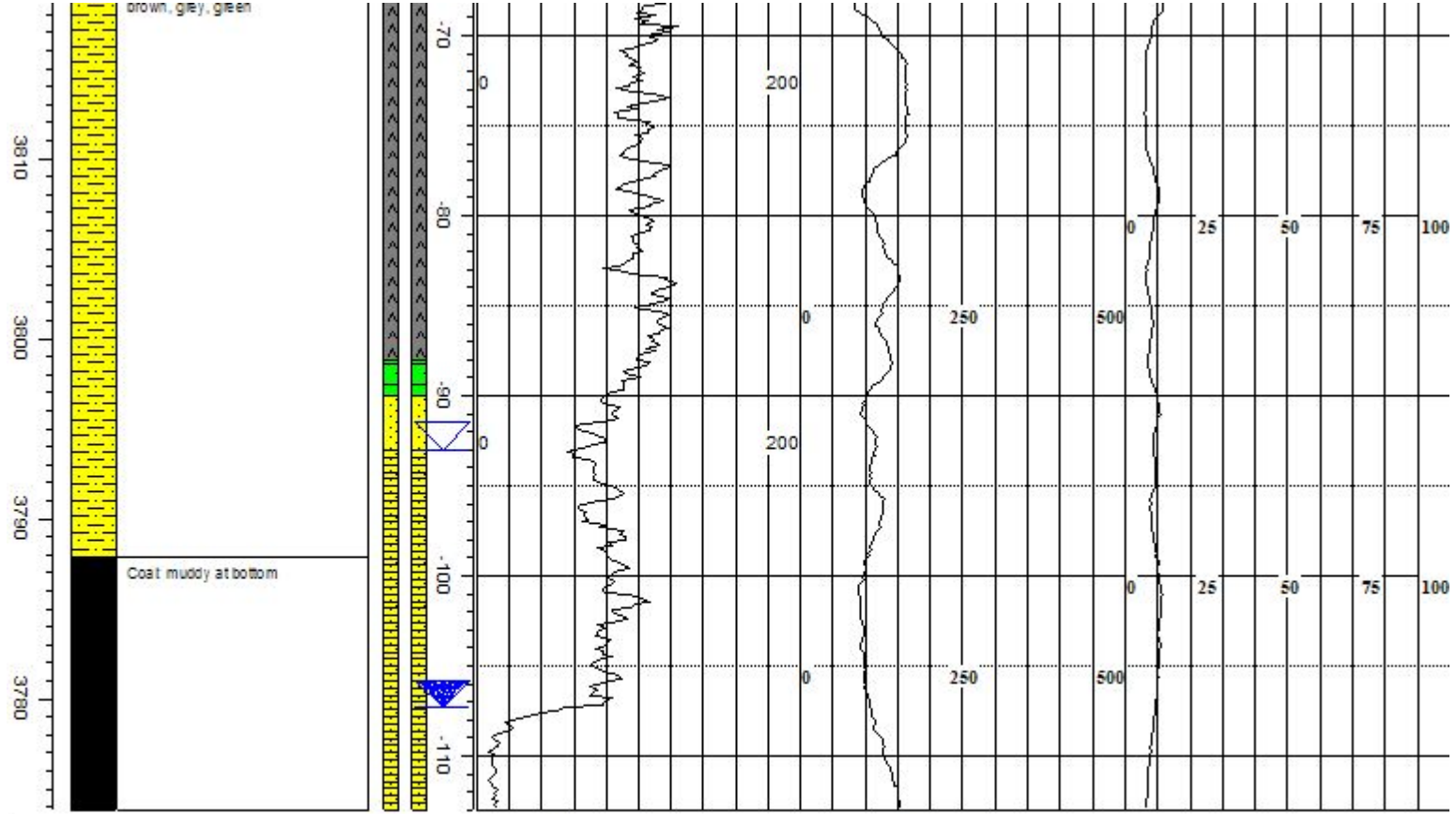
Total Depth: 113  
 Qtr Qtr: SENW  
 Section: 15  
 Township: 56N  
 Range: 75W

Drilling Contractor Interstate Drilling  
 Driller Dave Proctor

Drilling Dates 6-20-06  
 Hole Diameter 5-7/8"

Comments: Conductivity and Induction Interval from 6 feet to 49.3 feet rerun -- data questionable  
Natural Gamma curve smoothed due to excessive electronic noise SWL from 11-21-08





**Major Ion Chemistry (mg/L)**

Ca = 245      CO<sub>2</sub>/HCO<sub>3</sub> = 780  
 Mg = 171      SO<sub>4</sub> = 2074  
 Na = 444      TDS = 3760

|     |                            |       |     |                       |       |     |                    |       |
|-----|----------------------------|-------|-----|-----------------------|-------|-----|--------------------|-------|
| 0.0 | Natural Gamma<br>API Units | 200.0 | 0.0 | Conductivity<br>M/S/M | 500.0 | 0.0 | Induction<br>OHM-M | 100.0 |
|-----|----------------------------|-------|-----|-----------------------|-------|-----|--------------------|-------|

pH = 6.41  
 SAR = 5

**WDEQ Ground Water Classification = III**



**LX Bar Area**

**Termo Impoundment**

**Well No. MW-2**

On-site Geologist  
**Webster**

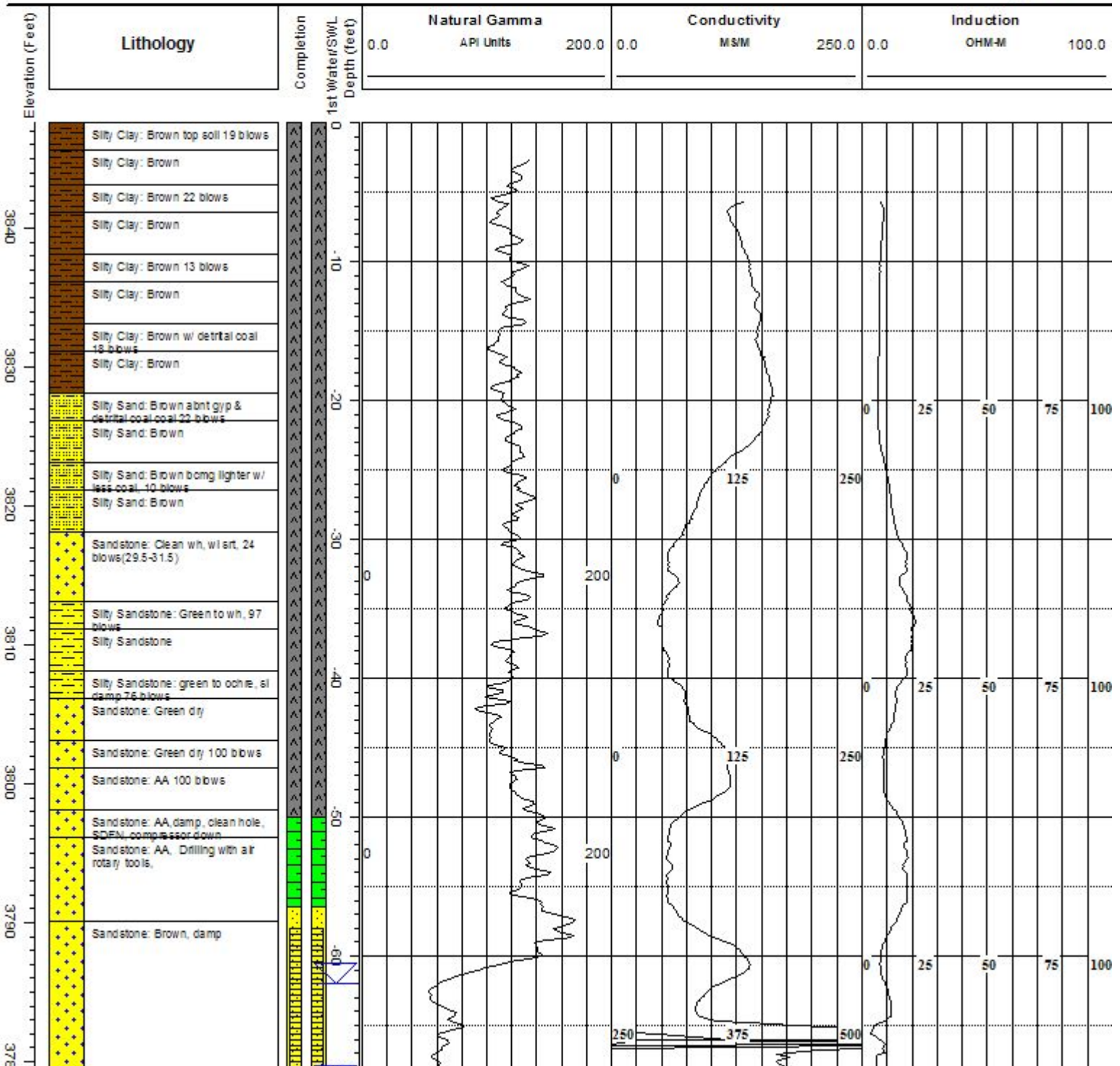
Latitude: 44°50'01.45675" Northing 1910829.1  
 Longitude: 105°52'34.31635" Easting 1690334.9  
 GL Elevation 3847.60

Total Depth: 78  
 Qtr Qtr: SENW  
 Section: 15  
 Township 56N  
 Range 75W

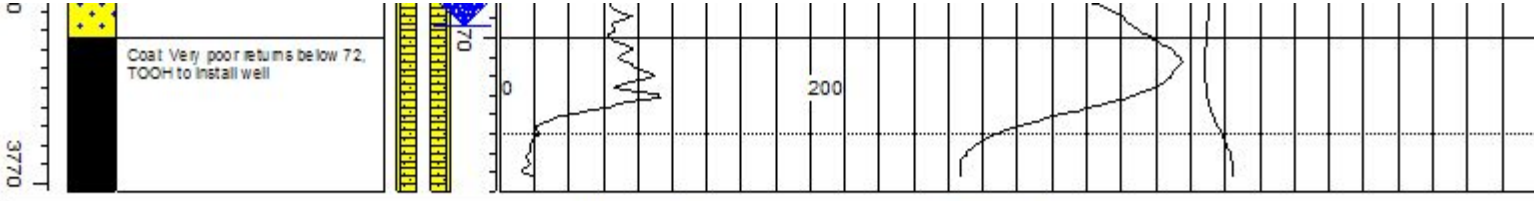
Drilling Contractor Interstate Drilling  
 Driller Dave Proctor

Drilling Dates 6-22-06  
 Hole Diameter 7-1/2 / 5-7/8"

Comments: SWL from 11-27-06







**Major Ion Chemistry (mg/L)**

Ca = 510      CO2/HCO3 = 768  
 Mg = 302      SO4 = 4172  
 Na = 758      TDS = 7000

|     |                            |       |     |                       |       |     |                    |       |
|-----|----------------------------|-------|-----|-----------------------|-------|-----|--------------------|-------|
| 0.0 | Natural Gamma<br>API Units | 200.0 | 0.0 | Conductivity<br>M/S/M | 250.0 | 0.0 | Induction<br>OHM-M | 100.0 |
|-----|----------------------------|-------|-----|-----------------------|-------|-----|--------------------|-------|

pH = 6.41  
 SAR = 7

**WDEQ Ground Water Classification = IV**



# Geophysical Logs Logs Run and Processed by United States Geological Survey

## LX Bar Area

## Termo Impoundment

### Well No. MW-3

On-site Geologist  
Webster

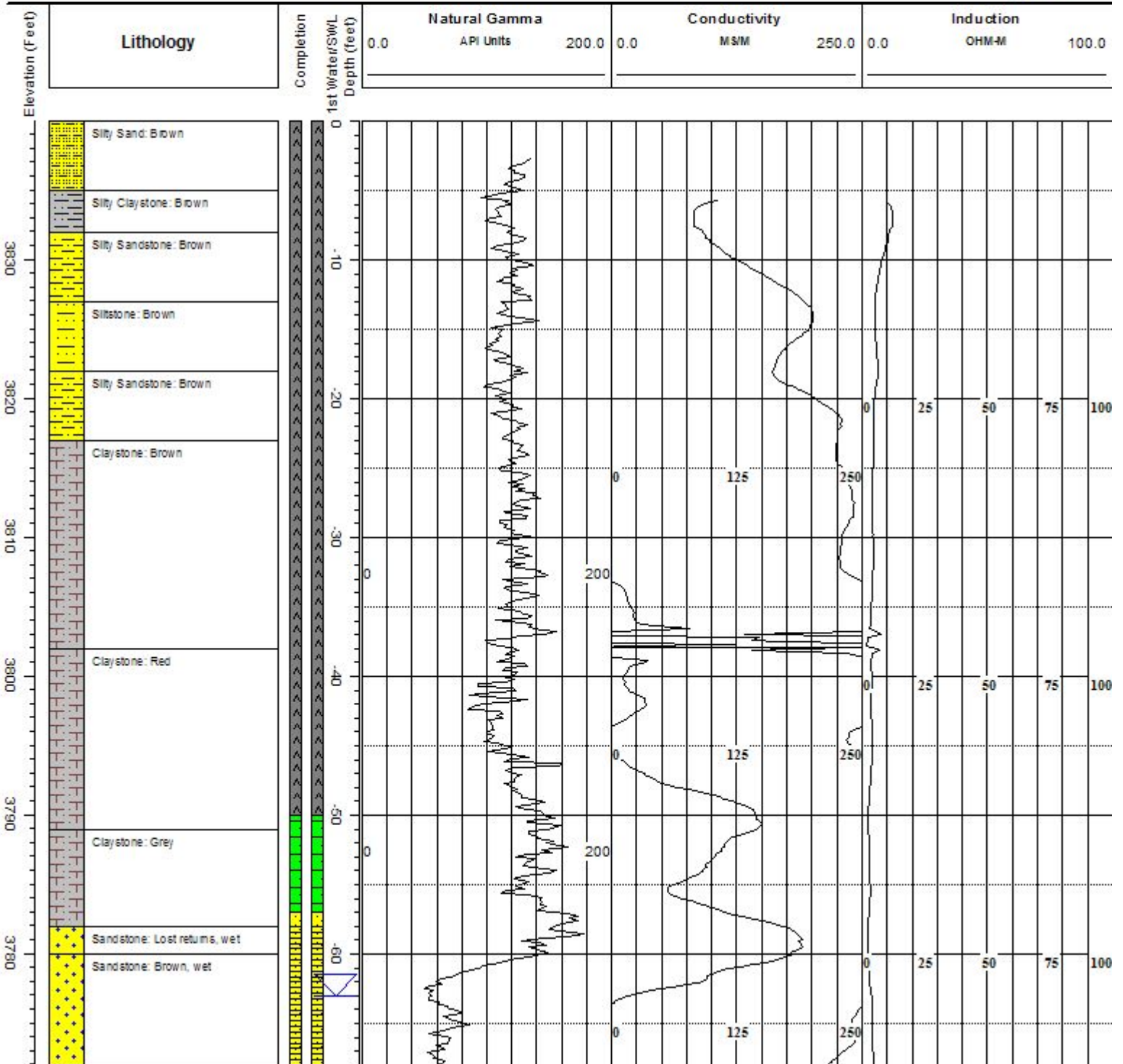
Latitude: 44°50'01.91123" Northing 1911172.772  
 Longitude: 105°52'37.08461" Easting 1910871.544  
 GL Elevation 3839.96

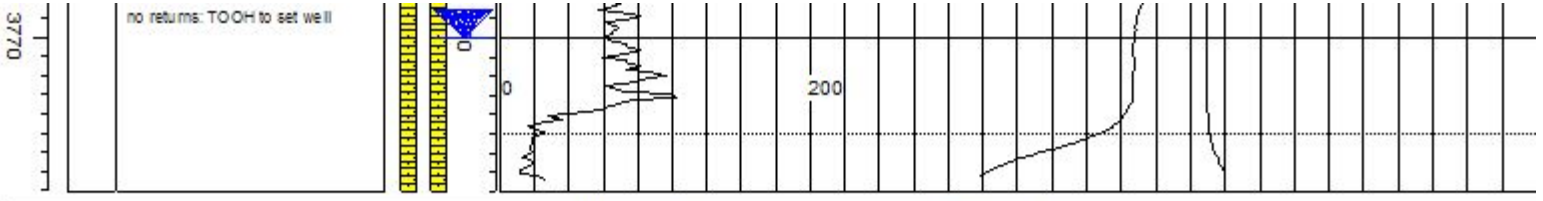
Total Depth: 78  
 Qtr Qtr: SENW  
 Section: 15  
 Township: 56N  
 Range: 75W

Drilling Contractor Interstate Drilling  
 Driller Dave Proctor

Drilling Dates 6-22-06  
 Hole Diameter 5-7/8"

Comments: SWL from 12-4-06





**Major Ion Chemistry (mg/L)**

Ca = 300      CO2/HCO3 = 987  
 Mg = 169      SO4 = 2530  
 Na = 809      TDS = 4776

|                            |                      |                    |
|----------------------------|----------------------|--------------------|
| Natural Gamma<br>API Units | Conductivity<br>MS/M | Induction<br>OHM-M |
| 0.0      200.0             | 0.0      250.0       | 0.0      100.0     |

pH = 6.8  
 SAR = 9

**WDEQ Ground Water Classification = IV**





# Geophysical Logs Logs Run and Processed by United States Geological Survey

## LX Bar Area

## Waylon Impoundment

### Well No. MW-1

On-site Geologist  
Webster

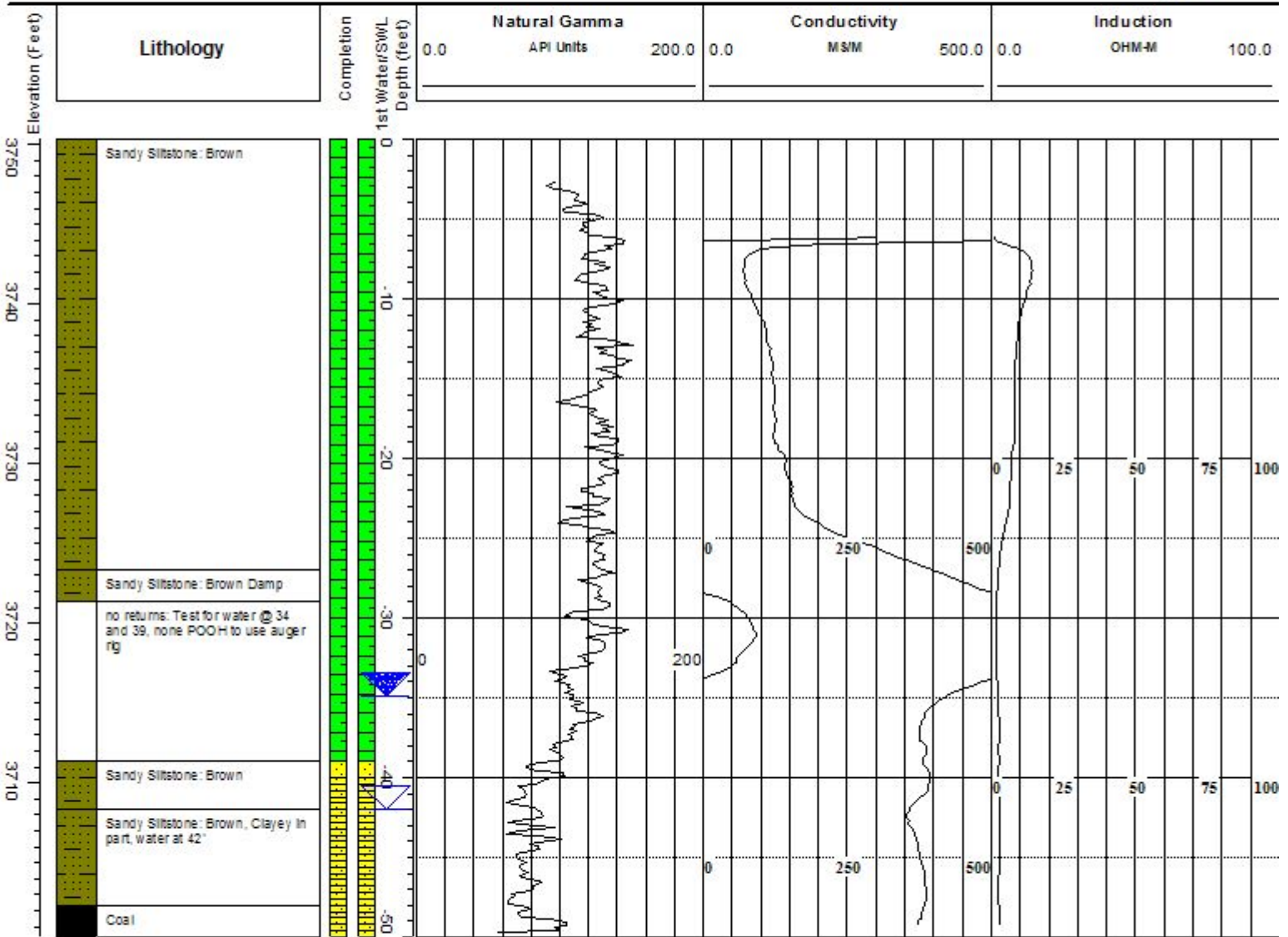
Latitude: 44°50'46.17192" Northing 1915255.753  
 Longitude: 105°53'53.57445" Easting 1684543.589  
 GL Elevation 3750.33

Total Depth: 50  
 Qtr Qtr: SENW  
 Section: 9  
 Township 56N  
 Range 75W

Drilling Contractor Interstate Drilling  
 Driller Dave Proctor

Drilling Dates 7-12-06  
 Hole Diameter 5-7/8"

Comments: SWL from 11-21-06



#### Major Ion Chemistry (mg/L)

Ca = 451      CO<sub>2</sub>/HCO<sub>3</sub> = 811  
 Mg = 553      SO<sub>4</sub> = 4362  
 Na = 760      TDS = 7840

pH = 7.19  
 SAR = 6

**WDEQ Ground Water Classification = IV**



# Geophysical Logs Logs Run and Processed by United States Geological Survey

## LX Bar Area

## Waylon Impoundment

### Well No. MW-2

On-site Geologist  
**Webster**

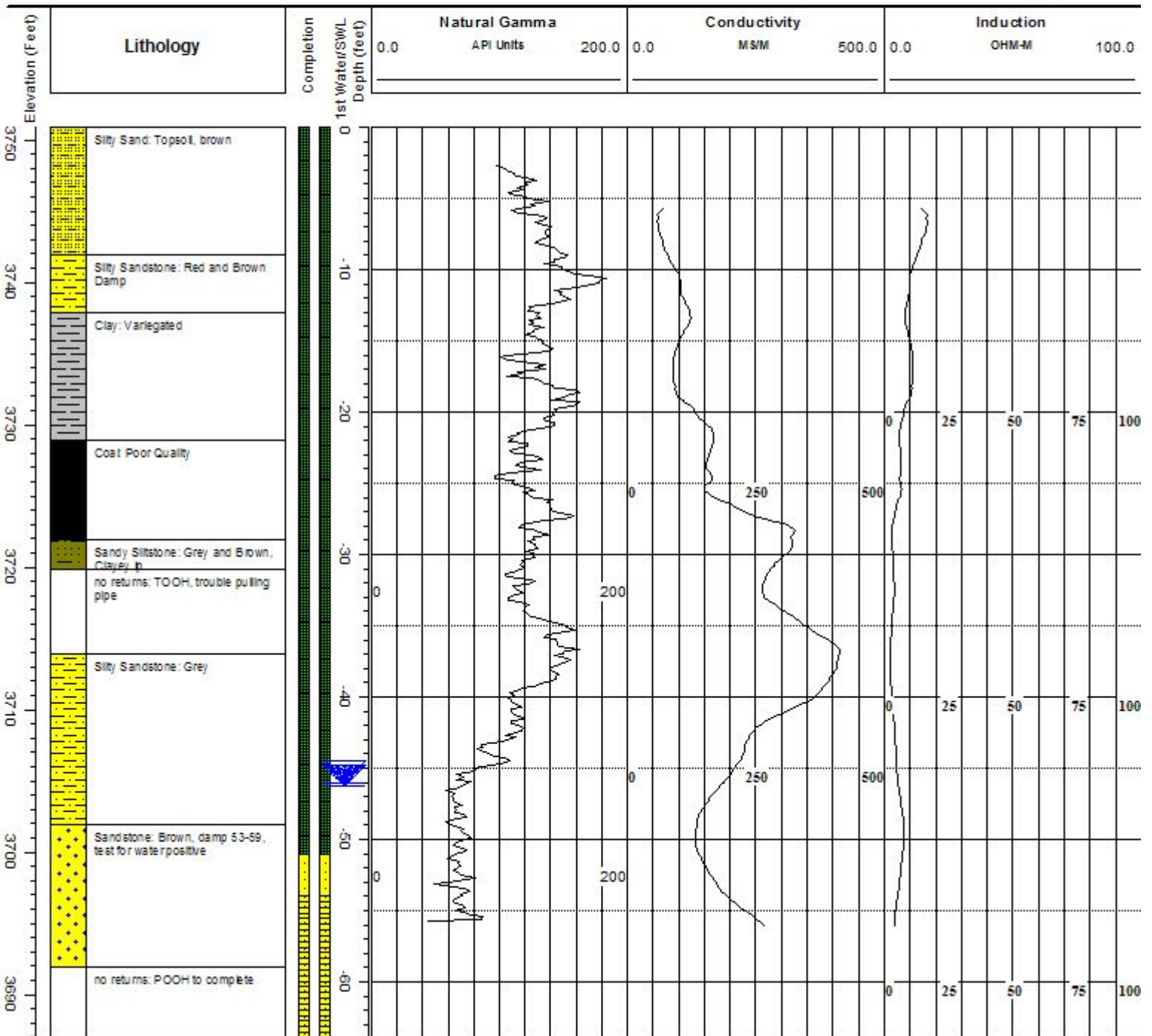
Latitude: 44°50'47.69186" Northing 1915409.752  
 Longitude: 105°53'53.51575" Easting 1684545.099  
 GL Elevation 3750.89

Total Depth: 64  
 Qtr Qtr: SENW  
 Section: 16  
 Township: 56N  
 Range: 83W

Drilling Contractor Interstate Drilling  
 Driller Dave Proctor

Drilling Dates 7-11-06  
 Hole Diameter 5-7/8"

Comments: Natural Gamma Curve Smoothed due to excessive noise  
 SWL from 11-18-06



**Major Ion Chemistry (mg/L)**

Ca = 343      CO<sub>2</sub>/HCO<sub>3</sub> = 744

Mg = 300      SO<sub>4</sub> = 3311

Na = 761      TDS = 6406

0.0      **Natural Gamma**  
API Units      200.0

0.0      **Conductivity**  
M/S/M      500.0

0.0      **Induction**  
OHM-M      100.0

pH = 7.36

SAR = 7

**WDEQ Ground Water Classification = IV**





**Geophysical Logs** Logs Run and Processed by United States Geological Survey

**LX Bar Area**

**Waylon Impoundment**

**Well No. MW-3**

On-site Geologist  
**Terry Webster**

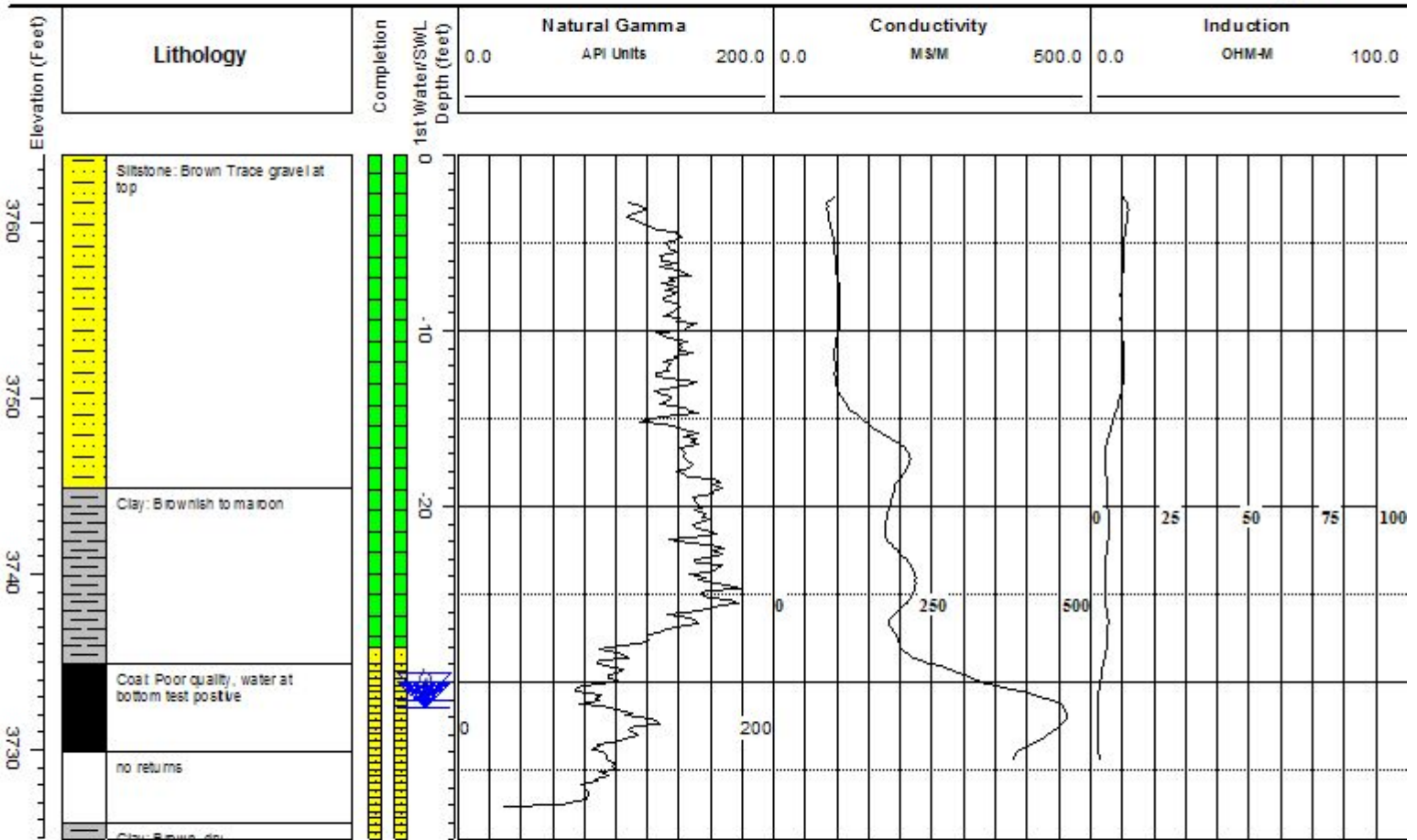
Latitude: 44°50'46.26189" Northing 1915274.682  
 Longitude: 105°53'45.86640" Easting 1685098.748  
 GL Elevation 3763.85

Total Depth: 39  
 Qtr Qtr: SENW  
 Section: 9  
 Township 57N  
 Range 75W

Drilling Contractor Interstate Drilling  
 Driller David Proctor

Drilling Dates 7-12-06  
 Hole Diameter 5-7/8"

Comments: Natural Gamma curve smoothed due to excessive electronic noise  
 SWL from 11-18-06



**Major Ion Chemistry (mg/L)**  
 Ca = 431      CO2/HCO3 = 0  
 Mg = 1047    SO4 = 7328  
 Na = 849      TDS = 12624

| 0.0 | Natural Gamma<br>API Units | 200.0 | 0.0 | Conductivity<br>MS/M | 500.0 | 0.0 | Induction<br>OHM-M | 100.0 |
|-----|----------------------------|-------|-----|----------------------|-------|-----|--------------------|-------|
|-----|----------------------------|-------|-----|----------------------|-------|-----|--------------------|-------|

pH = 3.1  
 SAR = 5

**WDEQ Ground Water Classification = IV**



**LX Bar Area Yates State Impoundment**

**Well No. MW-1**

On-site Geologist  
Webster

Latitude: 44 50'05.19835" Northing 1911114.73  
 Longitude: -105 53'46.99453" Easting 1685091.03  
 GL Elevation 3770.94

Total Depth: 57.5  
 Qtr Qtr: SENW  
 Section: 16  
 Township 57N  
 Range 75W

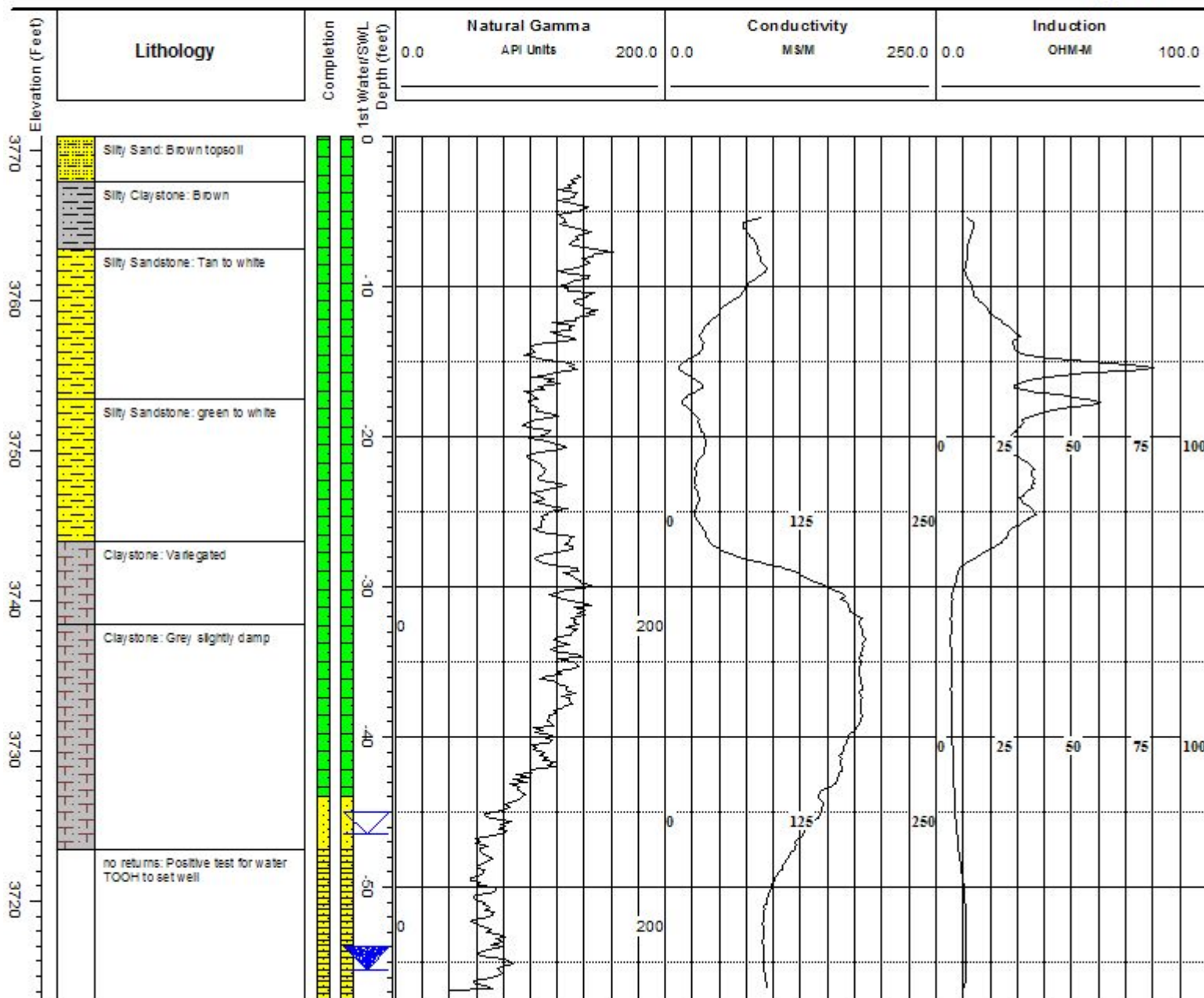
Drilling Contractor Interstate Drilling

Drilling Dates 6-12-06

Driller Dave Proctor

Hole Diameter 5-7/8"

Comments: Natural Gamma Curve smoothed due to excessive electronic noise  
 SWL from 11-2-06



**Major Ion Chemistry (mg/L)**

Ca = 176      CO<sub>2</sub>/HCO<sub>3</sub> = 610

Mg = 119      SO<sub>4</sub> = 693

Na = 82      TDS = 1568

0.0      **Natural Gamma**  
API Units      200.0

0.0      **Conductivity**  
M/S/M      250.0

0.0      **Induction**  
OHM-M      100.0

pH = 7.03

SAR = 1

**WDEQ Ground Water Classification = III**





**Geophysical Logs** Logs Run and Processed by United States Geological Survey

**LX Bar Area Yates State Impoundment**

**Well No. MW-2**

On-site Geologist  
**Webster**

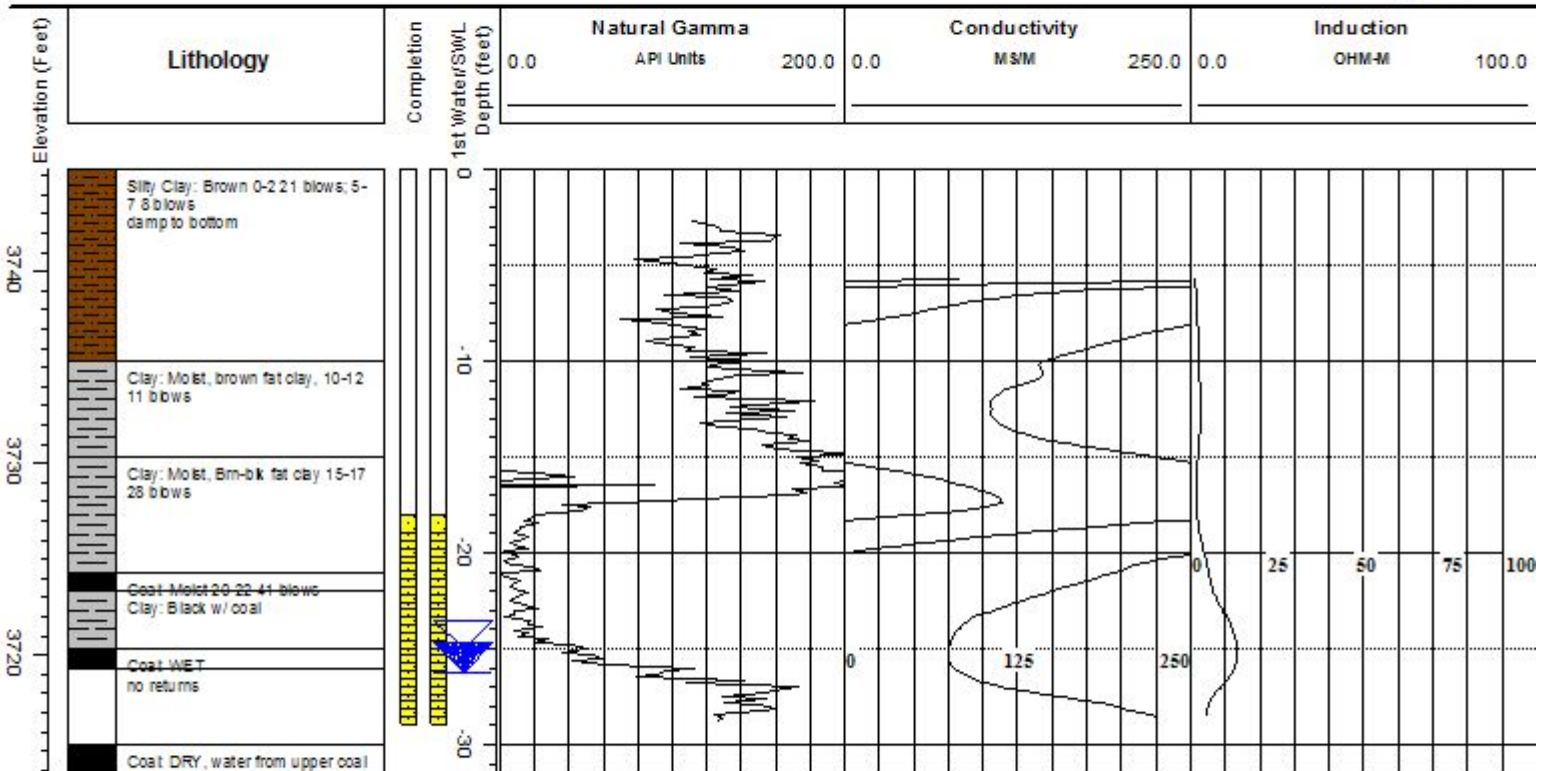
Latitude: 44 50'09.99240" Northing 1911610.83  
 Longitude: -105 53'38.68128" Easting 1685681.47  
 GL Elevation 3745.33

Total Depth: 31.5  
 Qtr Qtr: SENW  
 Section: 16  
 Township 56N  
 Range 75W

Drilling Contractor Interstate Drilling  
 Driller Dave Proctor

Drilling Dates 06-20-06  
 Hole Diameter 5-7/8"

Comments: SWL from 11-7-06



**Major Ion Chemistry (mg/L)**  
 Ca = 112      CO2/HCO3 = 841  
 Mg = 88      SO4 = 326  
 Na = 157      TDS = 1200

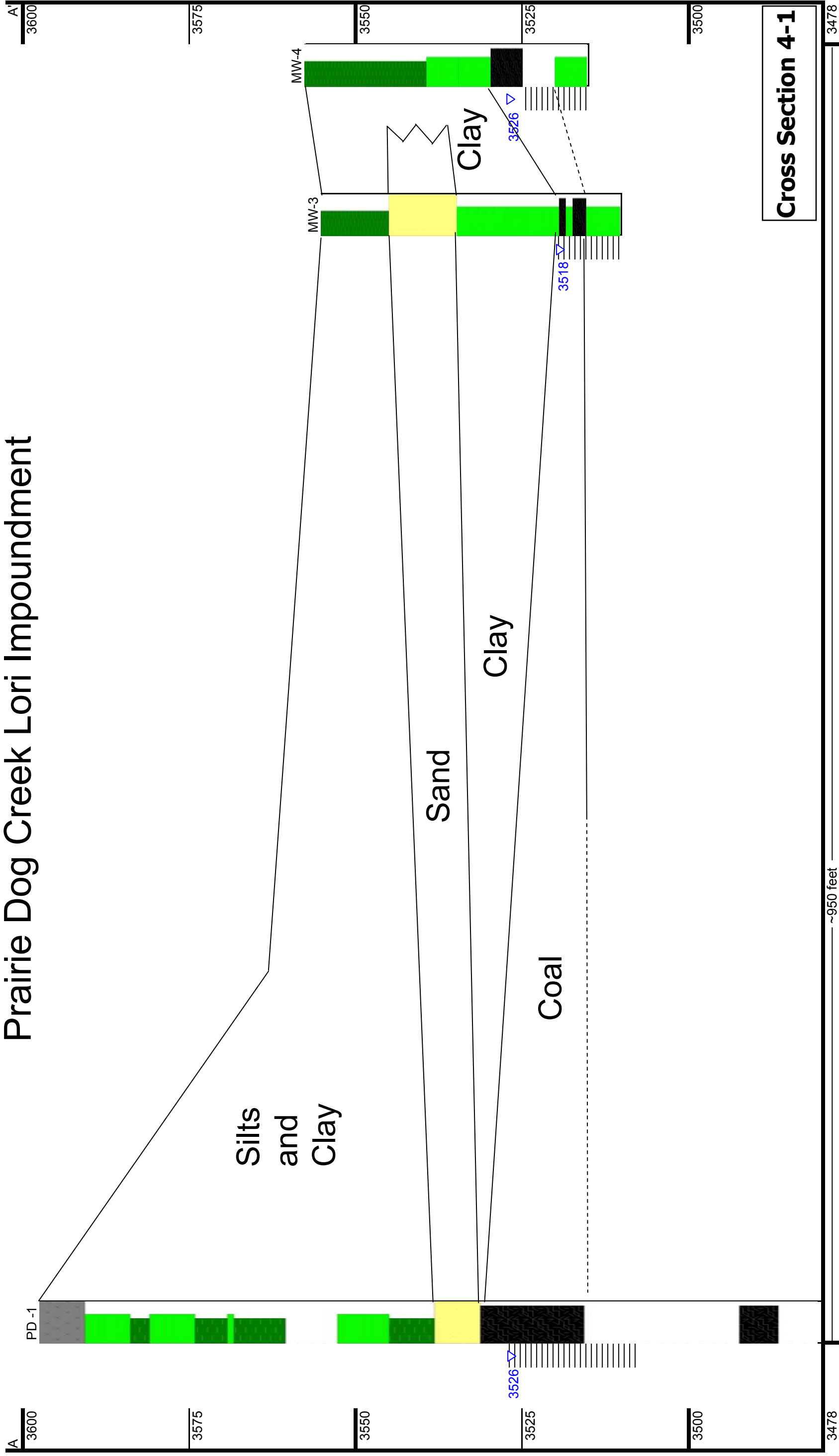
| Natural Gamma |       | Conductivity |       | Induction |       |
|---------------|-------|--------------|-------|-----------|-------|
| API Units     | 200.0 | M/S/M        | 250.0 | OHM-M     | 100.0 |

pH = 6.2  
 SAR = 3

**WDEQ Ground Water Classification = III**

**APPENDIX C**  
**CROSS SECTIONS**

# Prairie Dog Creek Lori Impoundment

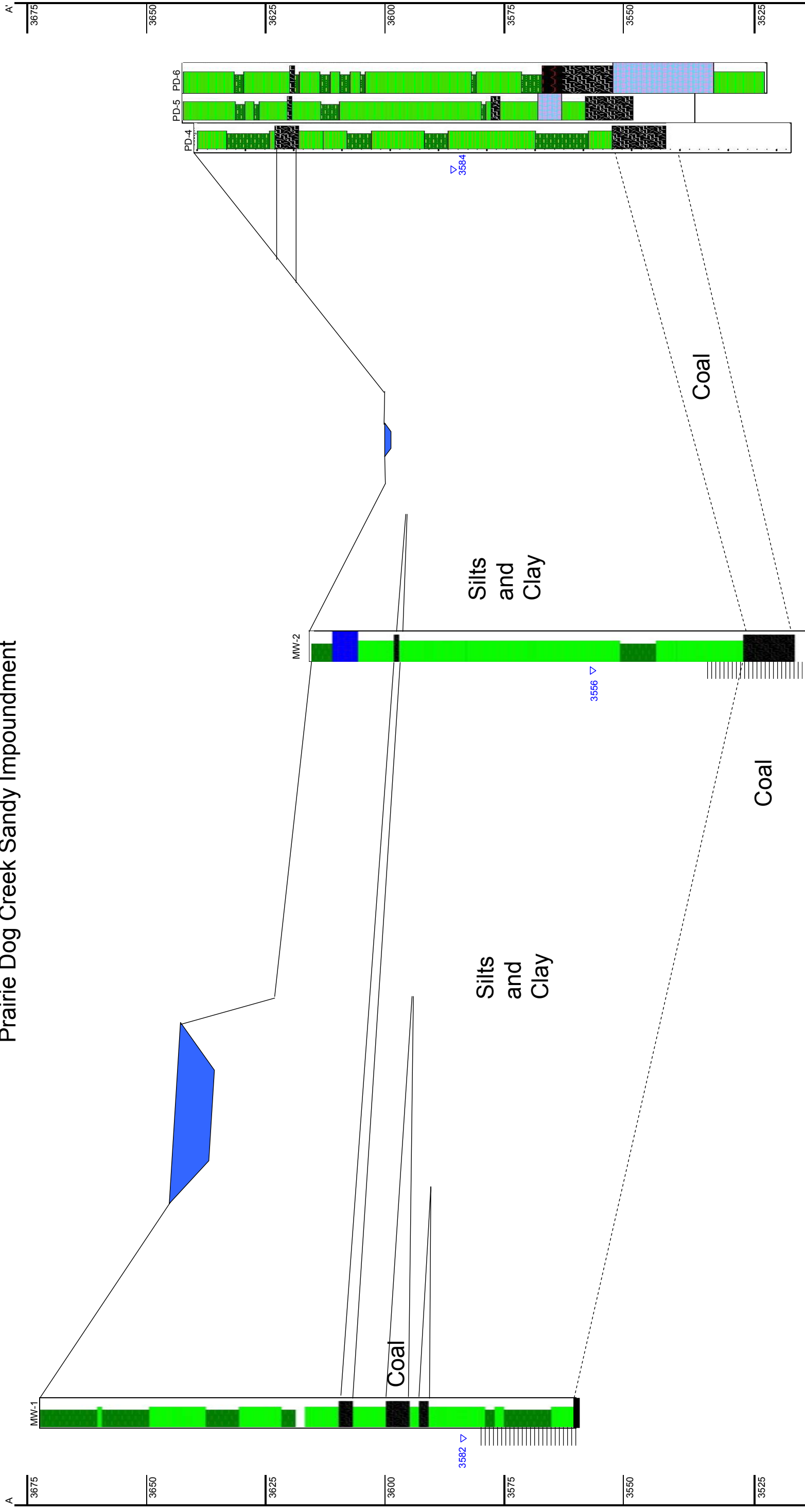


Cross Section 4-1

~950 feet



# Prairie Dog Creek Sandy Impoundment

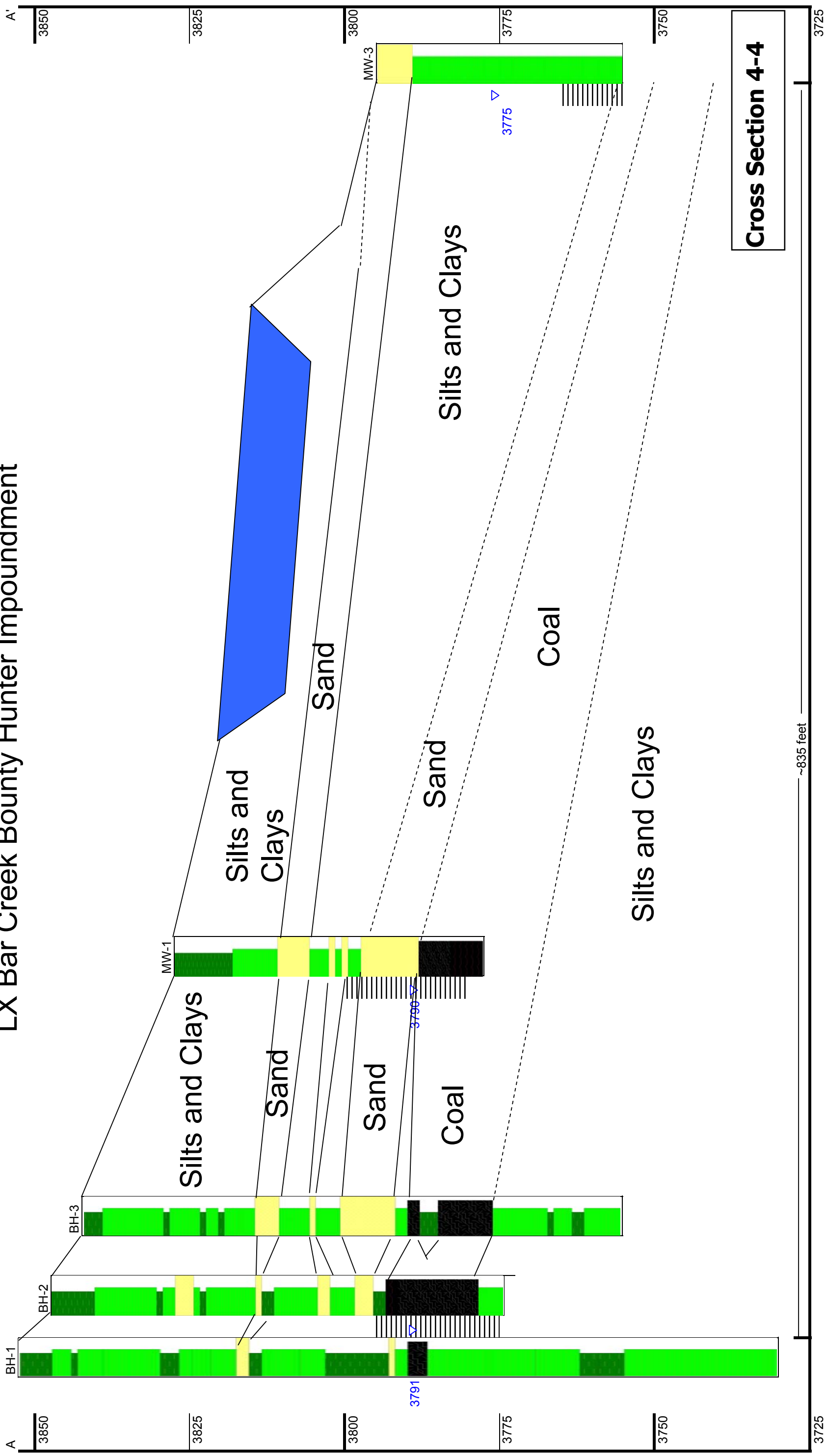


**Cross Section 4-2**

# Prairie Dog Creek Joe Draw Impoundment



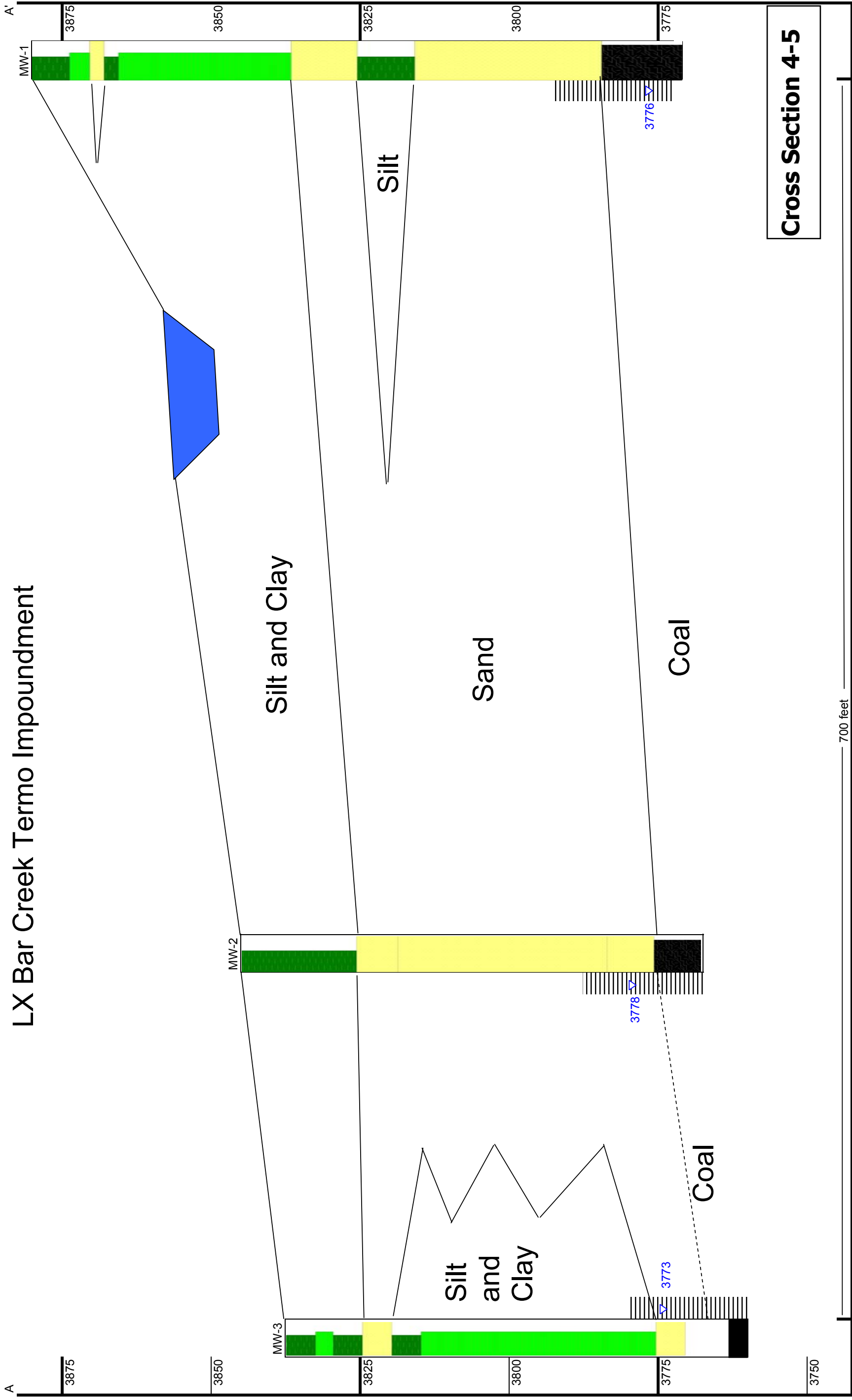
# LX Bar Creek Bounty Hunter Impoundment



**Cross Section 4-4**

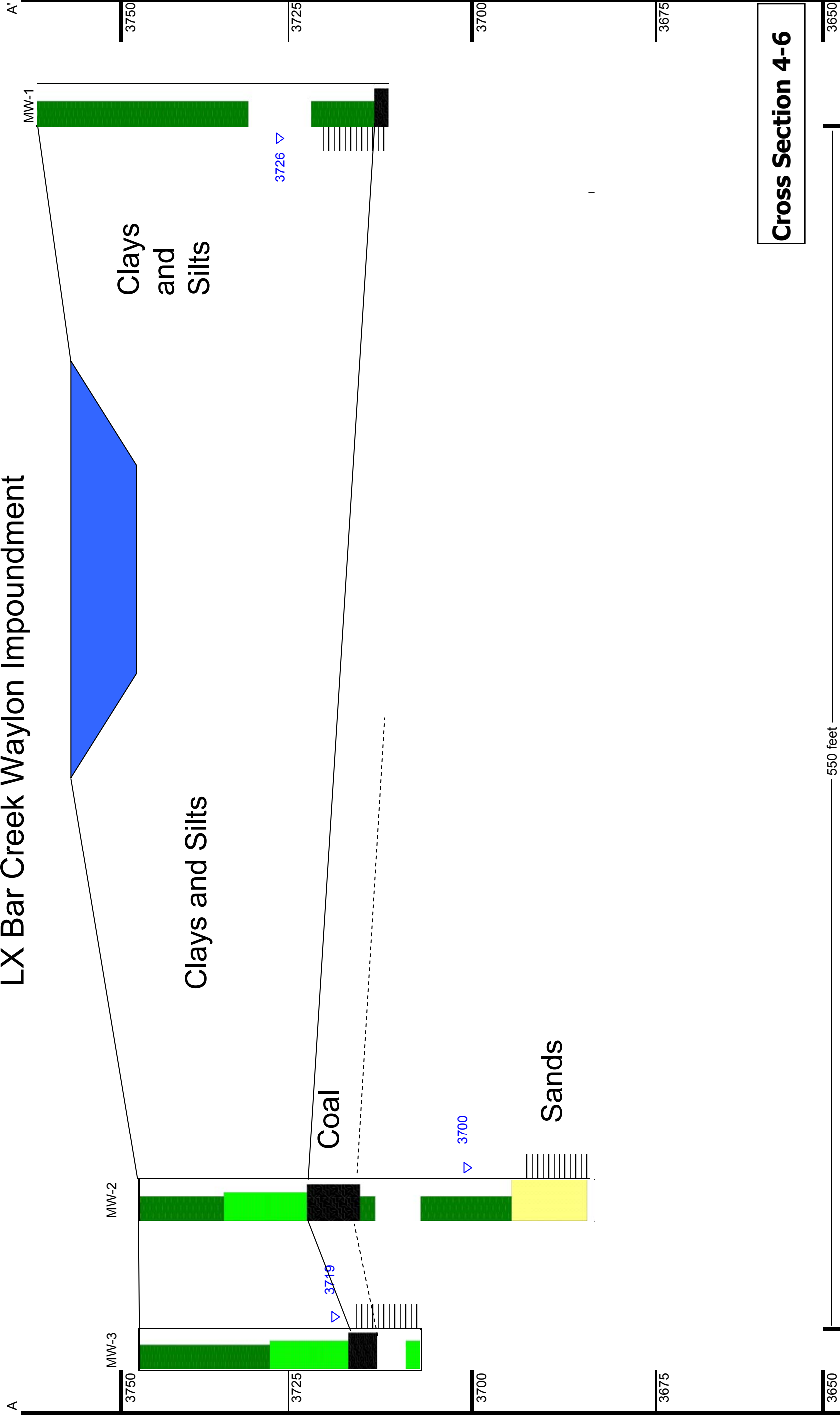


# LX Bar Creek Termo Impoundment

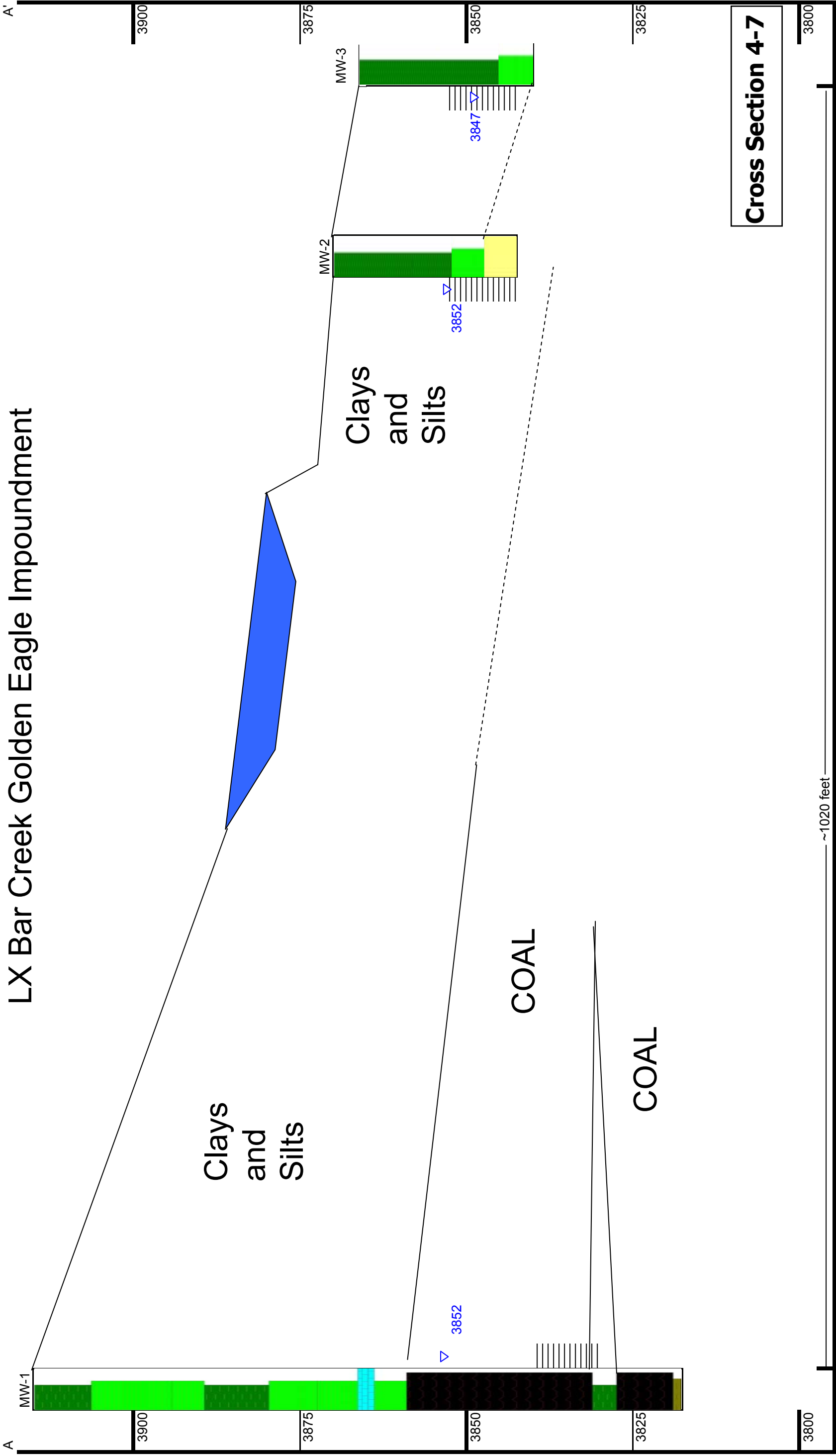


**Cross Section 4-5**

# LX Bar Creek Waylon Impoundment



# LX Bar Creek Golden Eagle Impoundment



Cross Section 4-7



**APPENDIX D**  
**CALCULATIONS**

MW\_Elevations

| OBJECTID | LATITUDE    | LONGITUDE    | ELEV | TYPE | NAME               | X_COORD     | Y_COORD     | GW_ELEV | LABEL | TYPE            | ElevMeters  | ElevFeet    |
|----------|-------------|--------------|------|------|--------------------|-------------|-------------|---------|-------|-----------------|-------------|-------------|
| 1        | 44.88299683 | -106.0521089 | 3609 | MW-1 | Wyoma MW-1         | 416909.1083 | 4970491.337 | 3500    | MW-1  | Monitoring Well | 1100.169067 | 3609.478568 |
| 2        | 44.69024998 | -105.69749   | 4120 | MW-2 | Joan MW-2          | 444731.7176 | 4948778.627 | 0       | MW-2  | Monitoring Well | 1255.710205 | 4119.784137 |
| 3        | 44.68916003 | -105.69779   | 4102 | MW-1 | Joan MW-1          | 444706.9122 | 4948657.756 | 0       | MW-1  | Monitoring Well | 1250.344727 | 4102.180861 |
| 4        | 44.68888004 | -105.69602   | 4118 | MW-3 | Joan MW-3          | 444846.8988 | 4948625.455 | 0       | MW-3  | Monitoring Well | 1255.190063 | 4118.077636 |
| 5        | 44.68485998 | -105.6856    | 4106 | MW-2 | Jim MW-2           | 445668.8286 | 4948171.9   | 0       | MW-2  | Monitoring Well | 1251.656738 | 4106.485362 |
| 6        | 44.68459997 | -105.68663   | 4098 | MW-1 | Jim MW-1           | 445586.9633 | 4948143.706 | 0       | MW-1  | Monitoring Well | 1249.044189 | 4097.914007 |
| 7        | 44.68546    | -105.6871901 | 4117 | MW-3 | Jim MW-3           | 445543.3863 | 4948239.612 | 0       | MW-3  | Monitoring Well | 1254.880981 | 4117.063587 |
| 8        | 44.70205002 | -105.6625199 | 4059 | MW-1 | JW MW-1            | 447513.3659 | 4950066.263 | 0       | MW-1  | Monitoring Well | 1237.146118 | 4058.878334 |
| 9        | 44.70197001 | -105.664     | 4075 | MW-2 | JW MW-2            | 447396.0431 | 4950058.329 | 0       | MW-2  | Monitoring Well | 1242.113159 | 4075.174407 |
| 10       | 44.72140001 | -105.6695999 | 4032 | MW-1 | Prairie Dog MW-1   | 446970.1428 | 4952220.281 | 0       | MW-1  | Monitoring Well | 1229.029053 | 4032.247548 |
| 11       | 44.72032001 | -105.67056   | 4042 | MW-2 | Prairie Dog MW-2   | 446893.1195 | 4952100.937 | 0       | MW-2  | Monitoring Well | 1232.095825 | 4042.309138 |
| 12       | 44.72198002 | -105.67306   | 4047 | MW-3 | Prairie Dog MW-3   | 446696.6504 | 4952286.968 | 0       | MW-3  | Monitoring Well | 1233.409424 | 4046.618845 |
| 13       | 44.76949002 | -105.66853   | 4123 | MW   | Brug 2/3 MW-1      | 447098.7602 | 4957561.539 | 0       | MW    | Monitoring Well | 1256.74585  | 4123.181921 |
| 14       | 44.77848001 | -105.66617   | 4074 | MW   | Brug MW-1          | 447293.6837 | 4958558.643 | 0       | MW    | Monitoring Well | 1241.823242 | 4074.223236 |
| 15       | 44.75843003 | -105.65338   | 4061 | MW   | Brug 1 MW-1        | 448287.7241 | 4956323.225 | 0       | MW    | Monitoring Well | 1237.895264 | 4061.336167 |
| 16       | 44.88207884 | -106.0500393 | 3644 | MW-2 | Wyoma MW-2         | 417071.2372 | 4970387.245 | 3517    | MW-2  | Monitoring Well | 1110.776367 | 3644.27942  |
| 17       | 44.88185538 | -106.0523142 | 3640 | MW-3 | Wyoma MW-3         | 416891.2492 | 4970364.749 | 3503    | MW-3  | Monitoring Well | 1109.578979 | 3640.350983 |
| 18       | 44.759922   | -105.6556327 | 4080 | MW-2 | Brug 1 MW-2        | 448110.7622 | 4964950.392 | 0       | MW-2  | Monitoring Well | 1243.610474 | 4080.086856 |
| 19       | 44.8347773  | -105.8963874 | 3772 | MW-1 | Yates State MW-1   | 429148.1911 | 4964987.307 | 0       | MW-1  | Monitoring Well | 1149.692383 | 3771.956637 |
| 20       | 44.83610898 | -105.8940781 | 3745 | MW-2 | Yates State MW-2   | 429332.3506 | 4965133.225 | 0       | MW-2  | Monitoring Well | 1141.582153 | 3745.348272 |
| 21       | 44.83465905 | -105.8745038 | 3861 | MW-1 | Terro MW-1         | 430877.7614 | 4964955.322 | 3768    | MW-1  | Monitoring Well | 1176.728882 | 3860.659061 |
| 22       | 44.83373801 | -105.8761989 | 3837 | MW-2 | Terro MW-2         | 430742.6727 | 4964854.453 | 3764    | MW-2  | Monitoring Well | 1169.620239 | 3837.336743 |
| 23       | 44.83386421 | -105.876968  | 3832 | MW-3 | Terro MW-3         | 430682.9037 | 4964869.127 | 3769    | MW-3  | Monitoring Well | 1168.00415  | 3832.034618 |
| 24       | 44.81850652 | -105.8777866 | 3827 | MW-1 | Bounty Hunter MW-1 | 430598.9375 | 4963126.832 | 3799    | MW-1  | Monitoring Well | 1166.547119 | 3827.254328 |
| 25       | 44.81953142 | -105.8760386 | 3791 | MW-2 | Bounty Hunter MW-2 | 430738.3336 | 4963276.191 | 3767    | MW-2  | Monitoring Well | 1155.647949 | 3791.495896 |
| 26       | 44.81894657 | -105.8755494 | 3794 | MW-3 | Bounty Hunter MW-3 | 430776.3145 | 4963210.807 | 3775    | MW-3  | Monitoring Well | 1156.403564 | 3793.974949 |
| 27       | 44.81837973 | -105.8787194 | 3847 | BH-1 | Bounty Hunter BH-1 | 430525.0017 | 4963150.544 | 0       | BH-1  | Bore Hole       | 1172.642944 | 3847.253754 |
| 28       | 44.81836465 | -105.8785439 | 3843 | BH-2 | Bounty Hunter BH-2 | 430538.8569 | 4963148.719 | 0       | BH-2  | Bore Hole       | 1171.338501 | 3842.974085 |
| 29       | 44.81836544 | -105.8783754 | 3840 | BH-3 | Bounty Hunter BH-3 | 430552.1815 | 4963148.663 | 3875.5  | MW-1  | Monitoring Well | 1170.279663 | 3839.500207 |
| 30       | 44.80722749 | -105.8461287 | 3952 | MW-1 | Golden Eagle MW-1  | 433088.8579 | 4961884.371 | 3875.5  | MW-1  | Monitoring Well | 1204.465576 | 3951.658714 |
| 31       | 44.80446354 | -105.845707  | 3881 | MW-3 | Golden Eagle MW-3  | 433119.008  | 4961576.995 | 3862    | MW-3  | Monitoring Well | 1182.952759 | 3981.078605 |
| 32       | 44.8089814  | -105.8493128 | 4020 | LX-1 | Golden Eagle LX-1  | 432839.1001 | 4962081.827 | 0       | LX-1  | Bore Hole       | 1225.319092 | 4020.07576  |
| 33       | 44.80898123 | -105.8494447 | 4013 | LX-2 | Golden Eagle LX-2  | 432828.4882 | 4962081.977 | 0       | LX-2  | Bore Hole       | 1220.363011 | 4012.585337 |
| 34       | 44.80999134 | -105.8496103 | 4004 | LX-3 | Golden Eagle LX-3  | 432815.5797 | 4962083.172 | 0       | LX-3  | Bore Hole       | 1220.363403 | 4003.81694  |
| 35       | 44.95108668 | -106.8381087 | 3577 | MW-1 | Joe Draw MW-1      | 355005.6327 | 4979160.232 | 3492    | MW-1  | Monitoring Well | 1090.351929 | 3577.270107 |
| 36       | 44.95146007 | -106.8387666 | 3561 | MW-2 | Joe Draw MW-2      | 354954.6718 | 4979202.887 | 3489    | MW-2  | Monitoring Well | 1085.520142 | 3561.417787 |
| 37       | 44.95023285 | -106.835386  | 3627 | MW-3 | Joe Draw MW-3      | 355218.2569 | 4979060.517 | 3480    | MW-3  | Monitoring Well | 1085.566406 | 3627.186372 |
| 38       | 44.84618385 | -105.896074  | 3759 | MW-1 | Waylon MW-1        | 429186.9356 | 4966254.123 | 3717    | MW-1  | Monitoring Well | 1145.740234 | 3758.99027  |
| 39       | 44.84658107 | -105.8981988 | 3748 | MW-2 | Waylon MW-2        | 429019.5085 | 4966300.102 | 3689    | MW-2  | Monitoring Well | 1142.444214 | 3748.176555 |
| 40       | 44.8461589  | -105.8982151 | 3745 | MW-3 | Waylon MW-3        | 429017.7021 | 4966253.219 | 3716    | MW-3  | Monitoring Well | 1141.420166 | 3744.816818 |
| 41       | 44.80480882 | -105.8448778 | 3886 | MW-2 | Golden Eagle MW-2  | 433184.9881 | 4961614.668 | 3868    | MW-2  | Monitoring Well | 1184.439331 | 3885.955811 |
| 42       | 44.95885028 | -106.8180293 | 3545 | MW-1 | Lori MW-1          | 356608.8855 | 4979986.948 | 3520    | MW-1  | Monitoring Well | 1080.455566 | 3544.801727 |
| 43       | 44.95904212 | -106.8186464 | 3547 | MW-3 | Lori MW-3          | 356560.6901 | 4980009.351 | 3503    | MW-3  | Monitoring Well | 1077.971436 | 3536.651691 |
| 44       | 44.95864643 | -106.8187189 | 3542 | MW-4 | Lori MW-4          | 356553.9859 | 4979965.522 | 3509    | MW-4  | Monitoring Well | 1079.685791 | 3542.276217 |
| 45       | 44.96136389 | -106.8181339 | 3598 | PD-3 | Lori PD-3          | 356606.8929 | 4980266.362 | 0       | PD-3  | Bore Hole       | 1096.805908 | 3598.444581 |
| 46       | 44.96132201 | -106.8184738 | 3590 | PD-2 | Lori PD-2          | 356592.3672 | 4980262.032 | 0       | PD-2  | Bore Hole       | 1094.365845 | 3590.439123 |
| 47       | 44.96126125 | -106.8184738 | 3583 | PD-1 | Lori PD-1          | 356579.8342 | 4980255.561 | 0       | PD-1  | Monitoring Well | 1091.98877  | 3582.64032  |
| 48       | 44.95319679 | -106.8673524 | 3673 | MW-1 | Sandy MW-1         | 352704.2163 | 4979447.356 | 0       | MW-1  | Monitoring Well | 1119.407104 | 3672.595487 |
| 49       | 44.95425771 | -106.8647986 | 3617 | MW-2 | Sandy MW-2         | 352908.3673 | 4979560.572 | 0       | MW-2  | Monitoring Well | 1102.442383 | 3616.936951 |
| 50       | 44.95372141 | -106.8647073 | 3632 | MW-3 | Sandy MW-3         | 352914.1961 | 4979500.831 | 0       | MW-3  | Monitoring Well | 1107.030518 | 3631.989887 |
| 51       | 44.95541847 | -106.8639557 | 3644 | PD-4 | Sandy BH-4         | 352977.8205 | 4979687.989 | 0       | PD-4  | Bore Hole       | 1110.681519 | 3643.968237 |
| 52       | 44.95544413 | -106.8638203 | 3639 | PD-5 | Sandy BH-5         | 352988.5564 | 4979690.279 | 0       | PD-5  | Bore Hole       | 1109.281494 | 3639.374981 |
| 53       | 44.95547651 | -106.8636558 | 3632 | PD-6 | Sandy BH-6         | 353001.6202 | 4979693.892 | 0       | PD-6  | Bore Hole       | 1107.138672 | 3632.344724 |
| 54       | 44.97165012 | -106.8004065 | 3808 | MW-1 | 14-3082 MW-1       | 358030.4091 | 4981377.818 | 0       | MW-1  | Bore Hole       | 1160.673462 | 3807.983799 |
| 55       | 44.96759766 | -106.7934409 | 3796 | MW-2 | 14-3082 MW-2       | 358569.7121 | 4980915.464 | 0       | MW-2  | Monitoring Well | 1156.88501  | 3795.554494 |

MW\_Lines

| Distance    | Direction   | FromMW             | ToMW               | DirectionTxt         |
|-------------|-------------|--------------------|--------------------|----------------------|
| 765.8870958 | 67.44049442 | Sandy MW-1         | Sandy MW-2         | N 67.4404553558127 E |
| 710.8974746 | 78.7815873  | Sandy MW-1         | Sandy MW-3         | N 78.7816105350609 E |
| 218.0331338 | 299.5742085 | Joe Draw MW-1      | Joe Draw MW-2      | N 60.4256112506166 W |
| 770.487108  | 107.4114418 | Joe Draw MW-1      | Joe Draw MW-3      | S 72.5885980390282 E |
| 174.3694327 | 287.2690937 | Lori MW-1          | Lori MW-3          | N 72.7312547746885 W |
| 193.3468992 | 253.5321869 | Lori MW-1          | MW-4               | S 73.5321286089855 W |
| 46.27666834 | 68.84215963 | Lori PD-1          | Lori PD-2          | N 68.8435353882282 E |
| 95.58666677 | 73.1935497  | Lori PD-1          | Lori PD-3          | N 73.1938675068874 E |
| 2330.590467 | 120.1901455 | 14-3082 MW-1       | 14-3082 MW-2       | S 59.80981170912 E   |
| 632.1101339 | 113.9202047 | Wyoma MW-1         | Wyoma MW-2         | S 66.0798161663399 E |
| 419.425421  | 190.1970918 | Wyoma MW-1         | Wyoma MW-3         | S 10.1973561222572 W |
| 569.6372832 | 280.5889269 | Waylon MW-1        | Waylon MW-2        | N 79.4110997875734 W |
| 555.2347281 | 269.332257  | Waylon MW-1        | Waylon MW-3        | S 89.3323250726614 W |
| 770.8685238 | 60.02981828 | Yates State MW-1   | Yates State MW-2   | N 60.0298008137892 E |
| 553.1260065 | 241.4827259 | Termo MW-1         | Termo MW-2         | S 61.482701844776 W  |
| 701.6498237 | 252.1223461 | Termo MW-1         | Termo MW-3         | S 72.1223623313403 W |
| 587.4879846 | 59.61502263 | Bounty Hunter MW-1 | Bounty Hunter MW-2 | N 59.6150278200439 E |
| 602.1076261 | 78.87197962 | Bounty Hunter MW-1 | Bounty Hunter MW-3 | N 78.8719738423227 E |
| 45.84931569 | 94.91106847 | Bounty Hunter BH-1 | Bounty Hunter BH-2 | S 85.088374159193 E  |
| 89.38557267 | 92.37865837 | Bounty Hunter BH-1 | Bounty Hunter BH-3 | S 87.6218447155779 E |
| 34.82704979 | 269.9302455 | Golden Eagle LX-1  | Golden Eagle LX-2  | S 89.9315938189409 W |
| 77.29350013 | 271.9131609 | Golden Eagle LX-1  | Golden Eagle LX-3  | N 88.0868102433483 W |
| 939.3761388 | 152.6521024 | Golden Eagle MW-1  | Golden Eagle MW-2  | S 27.3479034612692 E |
| 1013.290135 | 171.3261941 | Golden Eagle MW-1  | Golden Eagle MW-3  | S 8.67385027858717 E |
| 3333.25431  | 194.7087752 | Brug MW-1          | Brug 2/3 MW-1      | S 14.7088087056019 W |
| 7295.913346 | 150.412033  | Brug MW-1          | Brug 1 MW-2        | S 29.5879744228432 E |
| 8026.455718 | 147.4658794 | Brug MW-1          | Brug 1 MW-1        | S 32.5341114338966 E |
| 466.0103892 | 221.6359725 | Prairie Dog MW-1   | Prairie Dog MW-2   | S 41.6359198496447 W |
| 923.5725837 | 279.5159666 | Prairie Dog MW-1   | Prairie Dog MW-3   | N 80.4840505300118 W |
| 385.79544   | 266.9054008 | Prairie Dog MW-1   | JW MW-2            | S 86.9054508852342 W |
| 284.068942  | 75.83213998 | Jim MW-1           | Jim MW-2           | N 75.8322227010332 E |
| 345.6112756 | 326.9271422 | Jim MW-1           | Jim MW-3           | N 33.072744335085 W  |
| 404.8201006 | 15.3872064  | Joan MW-1          | Joan MW-2          | N 15.3869989559068 E |
| 471.3403195 | 98.98910275 | Joan MW-1          | Joan MW-3          | S 81.0109803217234 E |
| 1195.42734  | 56.81241507 | Sandy MW-1         | Sandy BH-4         | N 56.812424997895 E  |
| 1226.965715 | 57.56537467 | Sandy MW-1         | Sandy BH-5         | N 57.5653767613443 E |
| 1267.391827 | 58.33716642 | Sandy MW-1         | Sandy BH-6         | N 58.3372118800007 E |
| 810.2127833 | 184.4475368 | Lori PD-1          | Lori MW-3          | S 4.44756121574 W    |
| 955.3396392 | 185.3551498 | Lori PD-1          | Lori MW-4          | S 5.35500191626994 W |
| 886.4145695 | 349.5535769 | Lori MW-1          | Lori PD-1          | N 10.446461085837 W  |
| 904.1325013 | 353.3647908 | Lori MW-1          | Lori PD-2          | N 6.63517541031558 W |
| 835.4950612 | 188.2260017 | Lori PD-2          | Lori MW-3          | S 8.22610226806808 W |
| 980.9157963 | 188.5466504 | Lori PD-2          | Lori MW-4          | S 8.5465909860965 W  |
| 916.7355829 | 357.6153494 | Lori MW-1          | Lori PD-3          | N 2.38456525368019 W |
| 36.01556337 | 80.42749842 | Sandy BH-4         | Sandy BH-5         | N 80.4274320329605 E |
| 80.44914691 | 79.04559963 | Sandy BH-4         | Sandy BH-6         | N 79.0457187142449 E |



# Three-Point Problem Solver

## Usage

This spreadsheet calculates the strike and true dip of a structural plane given three points on the plane that have known elevation and relative bearings and distances. Normally this is the case when a planar geologic contact can be traced over irregular topography. The three elevations are determined from topographic contours whereas the bearings are measured with a protractor relative to geographic north. Distances between points are measured using the map scale. Alternatively, contours of subsurface structures may be used to measure the required parameters, however remember that this method assumes that the structure is planar! This spreadsheet may be used to determine the hydraulic flow direction below the water table, which is the true dip direction.

Detailed steps for using the below worksheet can be found in the "Documentation" sheet (next sheet)  
 NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typos. Also note that by default the cells below "App. dip 1" & "App. dip 2" receive the calculated vector attitudes. If you already have the apparent dip attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event that you need to revert back to using elevation and distance measurements. The combined strike and dip attitude is displayed in green at lower right in case the solution needs to be copied to another application such as NETPROG

## Calculation Method

The method works via the cross-product of two vectors. The two vectors, defined by "A-B" and "A-C" must lie within the structural plane for which we want to know the strike and dip. The upper portion of the spreadsheet converts the raw data into the attitude of these two vectors. In the upper portion of the spreadsheet the two vectors are converted into directional cosines, and then the cross-product is taken. The cross-product yields the attitude of the vector perpendicular to the plane that contains the original two vectors. This is analogous to the problem of calculating a strike and dip of a plane from two given apparent dips, which are in fact simply two lines that lay within the plane. The rest of the spreadsheet converts the pole into a more familiar strike and true dip in quadrant form.

|  |                              |                               |            |                |                 |      |
|--|------------------------------|-------------------------------|------------|----------------|-----------------|------|
| Angular Precision:   | 2                            | Angular Field Width:          | 5          | HV Conversion: | 1,000.000       | m/km |
| Three Points with known elevations, relative bearings, and distances | Bearing                      | Distance                      | Elevation  | Inclination    | Vector attitude |      |
| Point A  | #N/A                         | #N/A                          | 3500.500   | #N/A           | #N/A            |      |
| Point B  | N 60.43 W                    | 218.030                       | 3496.000   | 1.182          | N 60.43 W 1.18  |      |
| Point C  | S 72.59 E                    | 770.490                       | 3507.000   | -0.483         | S 72.59 E -0.48 |      |
| Data Set   | Quadrant                     | Azimuth 1                     | Azimuth 2  | Plunge 1       | Plunge 2        |      |
| Joe Draw JR  | App. Dip 1<br>N 60.43 W 1.18 | App. Dip 2<br>S 72.59 E -0.48 | 299.570    | 1.180          | 107.410         |      |
| App. dip 1   | Cos(beta)                    | Cos(alpha)                    | App. dip 2 | Cos(beta)      | Theta           |      |
| -0.870   | 0.493                        | 0.021                         | 0.554      | -0.299         | Angle(radians)  |      |
| Lower Hemisphere   | Cross-product                | Cos(beta)                     | Cos(gamma) | Pole           | Strike of       |      |
| Flag   | Cos(alpha)                   | -0.059                        | 0.998      | Azimuth        | Plane           |      |
| -0.998   | -0.010                       | -0.059                        | 0.998      | 189.315        | Dip             |      |
| Hydraulic Flow   | Gradient                     |                               |            | 86.595         | N 80.68 W       |      |
| 9.32   | m/km                         | 59.498                        |            |                | 3.40            | NE   |
| Graphical Data   | Point                        | Elev.                         |            |                |                 |      |
| X  | Y                            |                               |            |                |                 |      |
| 0.000  | 0.000                        | 3500.500                      |            |                |                 |      |
| -189.632   | 107.595                      | 3496.000                      |            |                |                 |      |
| 735.192  | -230.536                     | 3507.000                      |            |                |                 |      |
| 0.000  | 0.000                        |                               |            |                |                 |      |
| -189.632   | 107.595                      |                               |            |                |                 |      |
| 25.522   | 72.302                       |                               |            |                |                 |      |
| -404.787   | 142.887                      |                               |            |                |                 |      |
|  | Strike                       | N 80.68 W 3.40 NE             |            |                |                 |      |
|  | Strike                       | N 80.68 W 3.40 NE             |            |                |                 |      |

## Symbolic block names

Symbolic names are used extensively throughout the three point solver spreadsheet to clarify calculation equations. The blue cells are where raw data is entered. Below are the definitions:

| Name           | Definition or Value   |
|----------------|---|
| AppDip1        | Apparent dip bearing and plunge of A>B vector                           |
| AppDip2        | Apparent dip bearing and plunge of A>C vector                           |
| Az_1           | Azimuth (0-360) of apparent dip 1 (A>B).                                |
| Az_2           | Azimuth of apparent dip 2 (A>C).  |
| Bearing_B      | Entered bearing (quadrant format) of vector A>B.                        |
| Bearing_C      | Entered bearing of vector A>C.  |
| CalcAppDip1    | Calculated apparent dip vector 1 (A>B).                                 |
| CalcAppDip2    | Calculated apparent dip vector 2 (A>C).                                 |
| DistB          | Entered horizontal map distance from A to B.                            |
| DistC          | Entered horizontal map distance from A to C.                            |
| Elev1          | Entered elevation at point A.   |
| Elev2          | Entered elevation at point B.   |
| Elev3          | Entered elevation at point C.   |
| fi             | Field size (characters) for reported angular values.                    |
| H_V_Conversion | Conversion factor for gradient units.                                   |
| Incline_B      | Calculated inclination (degrees) from point A to B.                     |
| Incline_C      | Calculated inclination (degrees) from point A to C.                     |
| LowerFlag      | Positive if cross product has a positive plunge angle, negative if not. |
| Ndec           | Number of decimal places for reported angular values.                   |
| Pl_1           | Plunge angle of the A>B vector.   |
| Pl_2           | Plunge angle of the A>C vector.   |
| PoleAz         | Calculated azimuth angle (degrees) of the pole (cross product) vector.  |
| PolePl         | Calculated plunge angle (degrees) of the pole (cross product) vector.   |
| Theta_S        | Calculated angle (radians) between the apparent dip vectors.            |
| X_1,Y_1,Z_1    | Directional components of apparent dip 1 (A>B).                         |
| X_2,Y_2,Z_2    | Directional components of apparent dip 2 (A>C).                         |
| X_S,Y_S,Z_S    | Directional components of the cross product solution (pole to plane).   |

Note that the geometry of the problem is depicted in graphical form in the following worksheet chart. The user should be aware that the chart will almost always use different X and Y scales by default. It will be the responsibility of the user to override the default scaling so that the X and Y scales are equivalent. If the grid on the chart appears as "squares", the X and Y scales are equivalent (or nearly so).

STEP 1: From the base map pick the higher elevation point and label it as "A". Label the intermediate and lowest elevation points "B" and "C".

Make sure that point A is the highest elevation, "B" is the intermediate, and that point "C" is the lowest elevation value.

STEP 2: Measure the relative bearings in quadrant format between "A>B" and "A>C". Also measure distances according to scale.

Note that bearings must be entered according to the precision (i.e. decimal places) setting named "Angular Precision".

For example, a bearing measured as south 9.3 degrees west would be entered as "S 09.3 W" if angular precision = 1.

STEP 3: Calculate the elevations of points A,B, and C with topographic contours or other means. Remember to convert drill depths to elevations!

The worksheet assumes that units are equivalent among distance and elevation measurements. If not, convert to a consistent unit system at this step.

STEP 4: Enter the measurements from steps 1-3 into the cells in blue color below. The attitudes of the two vectors "A>B" and "A>C" will appear below the heading "Vector Attitude".

STEP 5: Read the strike and dip of the plane containing apparent dips 1 & 2 at the lower right

of the spreadsheet. Answers appear in dark green color. Also calculated are the pole azimuth and plunge, the hydraulic flow

direction azimuth, and the gradient. The gradient horizontal vs. vertical scale conversion is controlled by the cell

right of the label "H/V conversion". Use 1000 for meters per kilometer, or 5280 for feet per mile gradient units.

NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing.

Also note that by default the cells below App. dip 1 & App. dip 2 receive the calculated vector attitudes. If you already have the apparent dip

attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event

that you need to revert back to using elevation and distance measurements.

## Accumulation Macro

The accumulation macro is designed to copy the calculated results of the current 3-point problem to the sheet named

"Accumulation". You can run the macro with the menu sequence "Tools > Macro > Macros", and then indicate the

name "AccumulateMacro" as the macro to run.

## Graphical Plot

The graphical diagram in the sheet "Map" displays a map view of the elements of the 3-point problem. The points

labelled "A", "B", and "C" correspond to the 3 control points in the problem. The line labelled "strike" indicates the

attitude of the strike line calculated by the algorithm. By default the X and Y axis are set to an "autoscale" that

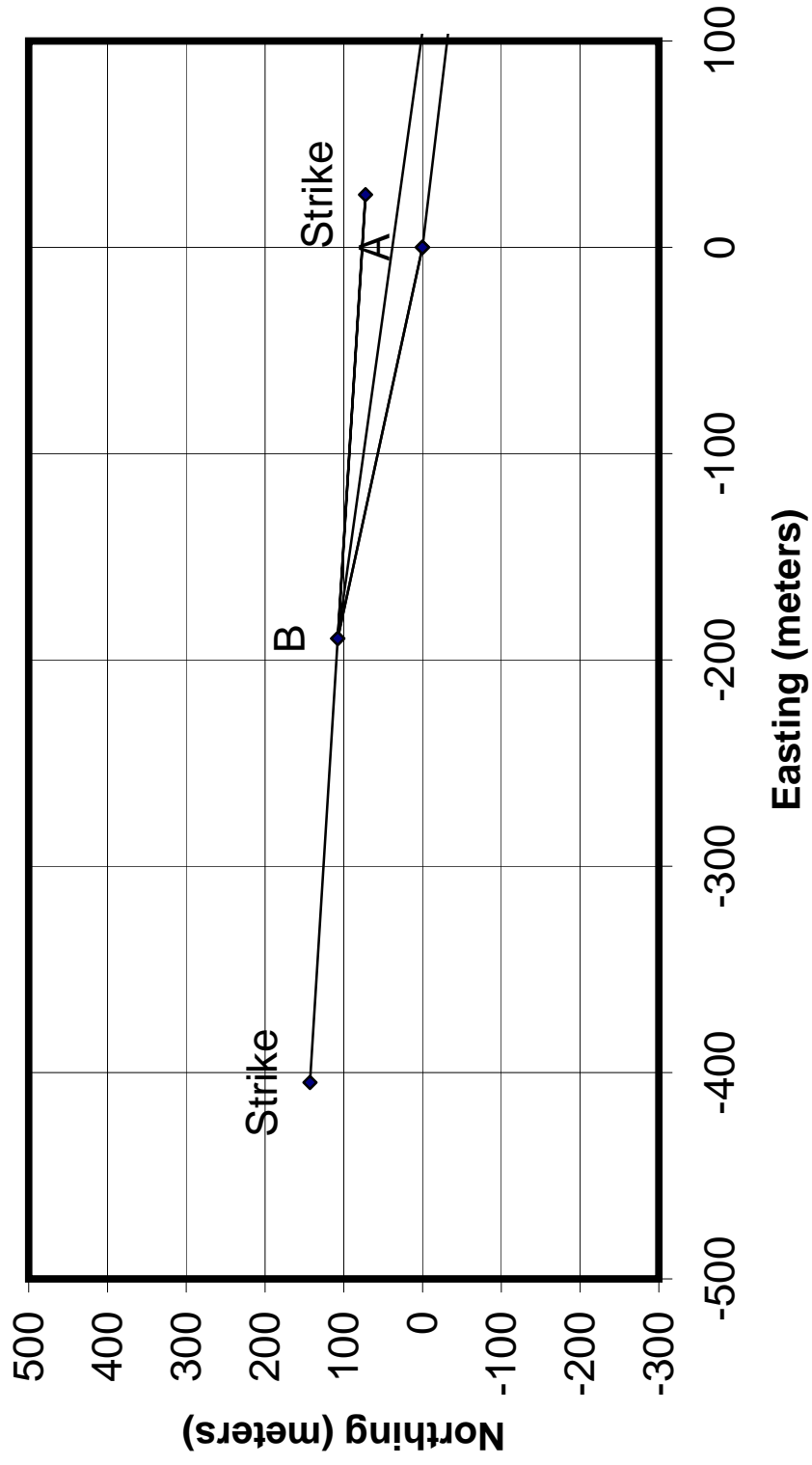
unfortunately will not generally set equivalent X and Y increments. After the elements of the problem are entered you

should edit the X and Y scale settings in "manual" mode so that the grid on the graph appears as a collection of

"squares" rather than rectangles. This means that the scaling is equivalent (or very close) on both axes, therefore,

the graph is no longer distorted.

# Three Point Problem







## Three-Point Problem Solver

### Usage

This spreadsheet calculates the strike and true dip of a structural plane given three points on the plane that have known elevation and relative bearings and distances. Normally this is the case when a planar geologic contact can be traced over irregular topography. The three elevations are determined from topographic contours whereas the bearings are measured with a protractor relative to geographic north. Distances between points are measured using the map scale. Alternatively, contours of subsurface structures may be used to measure the required parameters, however remember that this method assumes that the structure is planar! This spreadsheet may be used to determine the hydraulic flow direction below the water table, which is the true dip direction.

Detailed steps for using the below worksheet can be found in the "Documentation" sheet (next sheet)

NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typos. Also note that by default the cells below "App. dip 1" & "App. dip 2" receive the calculated vector attitudes. If you already have the vector attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event that you need to revert back to using elevation and distance measurements. The combined strike and dip attitude is displayed in green at lower right in case the solution needs to be copied to another application such as NETPROG

### Calculation Method

The method works via the cross-product of two vectors. The two vectors, defined by "A-B" and "A-C" must lie within the structural plane for which we want to know the strike and dip. The upper portion of the spreadsheet converts the raw data into the attitude of these two vectors. In the upper portion of the spreadsheet the two vectors are converted into directional cosines, and then the cross-product is taken. The cross-product yields the attitude of the vector perpendicular to the plane that contains the original two vectors. This is analogous to the problem of calculating a strike and dip of a plane from two given apparent dips, which are in fact simply two lines that lay within the plane. The rest of the spreadsheet converts the pole into a more familiar strike and true dip in quadrant form.

Angular Precision: 2 Angular Field Width: 5 HV Conversion: 1,000.000 m/km

Three Points with known elevations, relative bearings, and distances

| Bearing   | Distance | Elevation | Inclination | Vector attitude |
|-----------|----------|-----------|-------------|-----------------|
| #N/A      | #N/A     | 3515.000  | #N/A        | #N/A            |
| S 08.23 W | 83.500   | 3504.400  | 7.909       | S 08.23 W 7.91  |
| S 08.55 W | 980.920  | 3515.600  | 0.023       | S 08.55 W 0.02  |

Quadrant App. Dip 1 App. Dip 2

S 08.23 W 7.91 S 08.55 W 0.02

Azimuth 1 Azimuth 2

188.230 188.550

App. dip 2

Plunge 1 Plunge 2

7.910 0.020

Cos(alpha) Cos(beta) Cos(gamma)

-0.980 -0.138 0.040

Cos(alpha) Cos(beta) Cos(gamma)

-0.989 -0.138 0.000

Cross-product

Pole Azimuth Plunge

278.551 2.308 N 8.55 E

Hydraulic Flow

Gradient m/km

24814.627

Graphical Data

X Point Y Elev.

0.000 0.000 3516.000

-11.953 -82.640 3504.400

-145.836 -970.019 3515.600

0.000 0.000 A

-11.953 -82.640 B

-24.368 -165.212 Strike

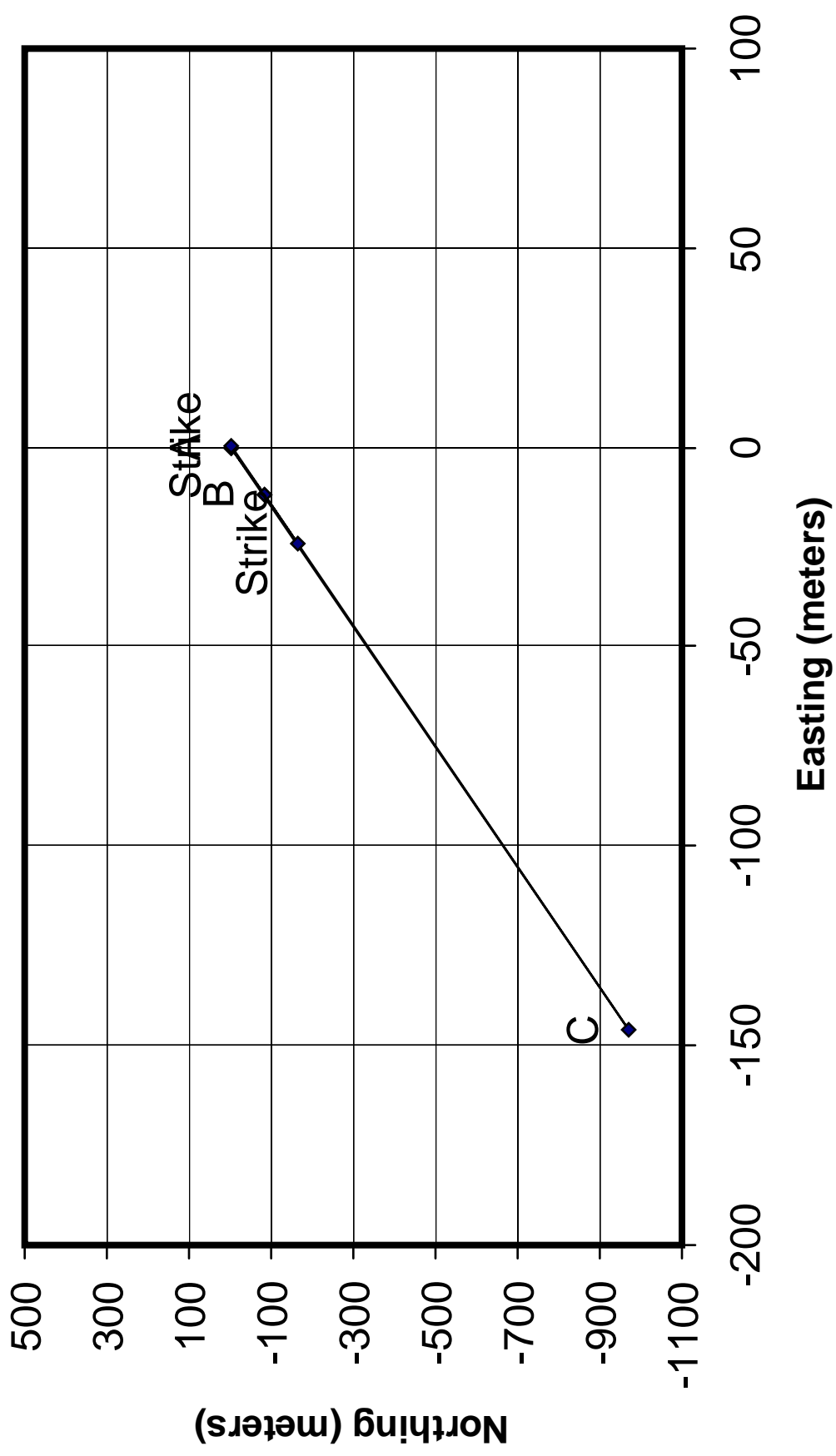
0.463 -0.068 Strike

N 8.55 E 87.69 SE

N 8.55 E 87.69 SE

| Symbolic block names   |  |
|--|--|
| Symbolic names are used extensively throughout the three point solver spreadsheet to clarify calculation equations. The blue cells are where raw data is entered. Below are the definition:  |  |
| Name   | Definition or Value  |
| AppDip1  | Apparent dip bearing and plunge of A>B vector                          |
| AppDip2  | Apparent dip bearing and plunge of A>C vector                          |
| Az_1   | Azimuth (0-360) of apparent dip 1 (A>B).                               |
| Az_2   | Azimuth of apparent dip 2 (A>C).                                       |
| Bearing_B  | Entered bearing (quadrant format) of vector A>B                        |
| Bearing_C  | Entered bearing of vector A>C  |
| CalcAppDip1  | Calculated apparent dip vector 1 (A>B).                                |
| CalcAppDip2  | Calculated apparent dip vector 2 (A>C).                                |
| DistB  | Entered horizontal map distance from A to B                            |
| DistC  | Entered horizontal map distance from A to C                            |
| Elev1  | Entered elevation at point A   |
| Elev2  | Entered elevation at point B   |
| Elev3  | Entered elevation at point C.  |
| f1   | Field size (characters) for reported angular values                    |
| H_V_Conversion   | Conversion factor for gradient units                                   |
| Incline_B  | Calculated inclination (degrees) from point A to B                     |
| Incline_C  | Calculated inclination (degrees) from point A to C                     |
| LowerFlag  | Positive if cross product has a positive plunge angle, negative if not |
| Ndec   | Number of decimal places for reported angular values                   |
| Pl_1   | Plunge angle of the A>B vector   |
| Pl_2   | Plunge angle of the A>C vector   |
| PoleAz   | Calculated azimuth angle (degrees) of the pole (cross product) vector  |
| PolePl   | Calculated plunge angle (degrees) of the pole (cross product) vector   |
| Theta_S  | Calculated angle (radians) between the apparent dip vectors            |
| X_1,Y_1,Z_1  | Directional components of apparent dip 1 (A>B)                         |
| X_2,Y_2,Z_2  | Directional components of apparent dip 2 (A>C)                         |
| X_S,Y_S,Z_S  | Directional components of the cross product solution (pole to plane)   |
| Note that the geometry of the problem is depicted in graphical form in the following worksheet chart. The user should be aware that the chart will almost always use different X and Y scales by default. It will be the responsibility of the user to override the default scaling so that the X and Y scales are equivalent. If the grid on the chart appears as "squares", the X and Y scales are equivalent (or nearly so)   |  |
| STEP 1: From the base map pick the higher elevation point and label it as "A". Label the intermediate and lowest elevation points "B" and "C". Make sure that point A is the highest elevation, "B" is the intermediate, and that point "C" is the lowest elevation value  |  |
| STEP 2: Measure the relative bearings in quadrant format between "A>B" and "A>C". Also measure distances according to scale. Note that bearings must be entered according to the precision (i.e. decimal places) setting named "Angular Precision". For example, a bearing measured as south 9.3 degrees west would be entered as "S 09.3 W" if angular precision = 1  |  |
| STEP 3: Calculate the elevations of points A, B, and C with topographic contours or other means. Remember to convert drill depths to elevation. The worksheet assumes that units are equivalent among distance and elevation measurements. If not, convert to a consistent unit system at this step  |  |
| STEP 4: Enter the measurements from steps 1-3 into the cells in blue color below. The attitudes of the two vectors "A>B" and "A>C" will appear below the heading "Vector Attitude"   |  |
| STEP 5: Read the strike and dip of the plane containing apparent dips 1 & 2 at the lower right of the spreadsheet. Answers appear in dark green color. Also calculated are the pole azimuth and plunge, the hydraulic flow direction azimuth, and the gradient. The gradient horizontal vs. vertical scale conversion is controlled by the cell to the right of the label "H/V conversion". Use 1000 for meters per kilometer, or 5280 for feet per mile gradient units  |  |
| NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing. Also note that by default the cells below App. dip 1 & App. dip 2 receive the calculated vector attitudes. If you already have the apparent dip attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event that you need to revert back to using elevation and distance measurements   |  |
| <b>Accumulation Macro</b>  |  |
| The accumulation macro is designed to copy the calculated results of the current 3-point problem to the sheet named "Accumulation". You can run the macro with the menu sequence "Tools > Macro > Macros", and then indicate the name "AccumulateMacro" as the macro to run  |  |
| <b>Graphical Plot</b>  |  |
| The graphical diagram in the sheet "Map" displays a map view of the elements of the 3-point problem. The points labelled "A", "B", and "C" correspond to the 3 control points in the problem. The line labelled "strike" indicates the attitude of the strike line calculated by the algorithm. By default the X and Y axis are set to an "autoscale" but unfortunately will not generally set equivalent X and Y increments. After the elements of the problem are entered you should edit the X and Y scale settings in "manual" mode so that the grid on the graph appears as a collection of "squares" rather than rectangles. This means that the scaling is equivalent (or very close) on both axes, therefore the graph is no longer distorted. |  |

# Three Point Problem







| Three-Point Problem Solver   |                              |                              |            |                 |                 |                  |
|--|------------------------------|------------------------------|------------|-----------------|-----------------|------------------|
| <b>Usage</b>   |                              |                              |            |                 |                 |                  |
| This spreadsheet calculates the strike and true dip of a structural plane given three points on the plane that have known elevation and relative bearings and distances. Normally this is the case when a planar geologic contact can be traced over irregular topography. The three elevations are determined from topographic contours whereas the bearings are measured with a protractor relative to geographic north. Distances between points are measured using the maps scale. Alternatively, contours of subsurface structures may be used to measure the required parameters, however, remember that this method assumes that the structure is planar! This spreadsheet may be used to determine the hydraulic flow direction below the water table, which is the true dip direction.  |                              |                              |            |                 |                 |                  |
| Detailed steps for using the below worksheet can be found in the "Documentation" sheet (next sheet).   |                              |                              |            |                 |                 |                  |
| NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing.   |                              |                              |            |                 |                 |                  |
| Also note that by default the cells below "App. dip 1" & "App. dip 2" receive the calculated vector attitudes. If you already have the apparent dip attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event that you need to revert back to using elevation and distance measurements. The combined strike and dip attitude is displayed in green at lower right in case the solution needs to be copied to another application such as NETPROG.   |                              |                              |            |                 |                 |                  |
| <b>Calculation Method</b>  |                              |                              |            |                 |                 |                  |
| The method works via the cross-product of two vectors. The two vectors defined by "A>B" and "A>C" must lie within the structural plane for which we want to know the strike and dip. The upper portion of the spreadsheet converts the raw data into the attitude of these two vectors. In the upper portion of the spreadsheet the two vectors are converted into directional cosines, and then the cross-product is taken. The cross-product yields the attitude of the vector perpendicular to the plane that contains the original two vectors. This is analogous to the problem of calculating a strike and dip of a plane from two given apparent dips, which are in fact simply two lines that lay within the plane. The rest of the spreadsheet converts the pole into a more familiar strike and true dip in quadrant format. |                              |                              |            |                 |                 |                  |
| Angular Precision:   | 2                            | Angular Field Width:         | 5          | H/V Conversion: | 1000.000        | m/km             |
| <b>Three Points with known elevations, relative bearings, and distances.</b>   |                              |                              |            |                 |                 |                  |
| Point A  | Bearing                      | Distance                     | Elevation  | Inclination     | Vector attitude |                  |
|  | #N/A                         | #N/A                         | 3520.000   | #N/A            | #N/A            |                  |
| Point B  | N 10.45 W                    | 886.410                      | 3514.000   | 0.388           | N 10.45 W 0.39  |                  |
| Point C  | N 06.64 W                    | 904.130                      | 3519.000   | 0.063           | N 06.64 W 0.06  |                  |
| Data Set   | Quadrant                     | Quadrant                     | Azimuth 1  | Plunge 1        | Azimuth 2       | Plunge 2         |
| Siltstone Aquifer  | App. Dip 1<br>N 10.45 W 0.39 | App. Dip 2<br>N 06.64 W 0.06 | 349.550    | 0.390           | 353.360         | 0.060            |
| App. dip 1   |                              |                              | App. dip 2 |                 |                 | Theta            |
| Cos(alpha)   | Cos(beta)                    | Cos(gamma)                   | Cos(alpha) | Cos(beta)       | Cos(gamma)      | Angle(radians)   |
| -0.181   | 0.983                        | 0.007                        | -0.116     | 0.993           | 0.001           | 0.067            |
| Lower Hemisphere   | Cross-product                |                              |            | Pole            | Pole            | Strike of        |
| Flag   | Cos(alpha)                   | Cos(beta)                    | Cos(gamma) | Azimuth         | Plunge          | Plane            |
| -0.996   | 0.086                        | 0.009                        | 0.996      | 84.052          | 85.044          | N 5.95 W         |
|  |                              |                              |            |                 |                 | 4.96 SW          |
| Hydraulic Flow   | Gradient                     |                              |            |                 |                 | Plane            |
| Azimuth  | m/km                         |                              |            |                 |                 | Strike & Dip     |
| 264.05   | 86.721                       |                              |            |                 |                 | N 5.95 W 4.96 SW |
| Graphical Data   |                              |                              |            |                 |                 |                  |
| X  | Y                            | Point                        | Elev.      |                 |                 |                  |
| 0.000  | 0.000                        | A                            | 3520.000   |                 |                 |                  |
| -160.775   | 871.708                      | B                            | 3514.000   |                 |                 |                  |
| -104.545   | 898.065                      | C                            | 3519.000   |                 |                 |                  |
| 0.000  | 0.000                        | A                            |            |                 |                 |                  |
| -160.775   | 871.708                      | B                            |            |                 |                 |                  |
| -252.631   | 1753.345                     | Strike                       |            |                 |                 | N 5.95 W 4.96 SW |
| -68.918  | -9.930                       | Strike                       |            |                 |                 | N 5.95 W 4.96 SW |

## Symbolic block names

Symbolic names are used extensively throughout the three point solver spreadsheet to clarify calculation equations. The blue cells are where raw data is entered. Below are the definition:

| Name           | Definition or Value  |
|----------------|--|
| AppDip1        | Apparent dip bearing and plunge of A>B vector                          |
| AppDip2        | Apparent dip bearing and plunge of A>C vector                          |
| Az_1           | Azimuth (0-360) of apparent dip 1 (A>B).                               |
| Az_2           | Azimuth of apparent dip 2 (A>C).                                       |
| Bearing_B      | Entered bearing (quadrant format) of vector A>B                        |
| Bearing_C      | Entered bearing of vector A>C  |
| CalcAppDip1    | Calculated apparent dip vector 1 (A>B).                                |
| CalcAppDip2    | Calculated apparent dip vector 2 (A>C).                                |
| DistB          | Entered horizontal map distance from A to B                            |
| DistC          | Entered horizontal map distance from A to C                            |
| Elev1          | Entered elevation at point A   |
| Elev2          | Entered elevation at point B   |
| Elev3          | Entered elevation at point C.  |
| fl             | Field size (characters) for reported angular values                    |
| H_V_Conversion | Conversion factor for gradient units.                                  |
| Incline_B      | Calculated inclination (degrees) from point A to B                     |
| Incline_C      | Calculated inclination (degrees) from point A to C                     |
| LowerFlag      | Positive if cross product has a positive plunge angle, negative if not |
| Ndec           | Number of decimal places for reported angular values                   |
| Pl_1           | Plunge angle of the A>B vector   |
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| PoleAz         | Calculated azimuth angle (degrees) of the pole (cross product) vector  |
| PolePl         | Calculated plunge angle (degrees) of the pole (cross product) vector   |
| Theta_S        | Calculated angle (radians) between the apparent dip vectors            |
| X_1_Y_1_Z_1    | Directional components of apparent dip 1 (A>B)                         |
| X_2_Y_2_Z_2    | Directional components of apparent dip 2 (A>C)                         |
| X_S_Y_S_Z_S    | Directional components of the cross product solution (pole to plane)   |

Note that the geometry of the problem is depicted in graphical form in the following worksheet chart. The user should be aware that the chart will almost always use different X and Y scales by default. It will be the responsibility of the user to override the default scaling so that the X and Y scales are equivalent. If the grid on the chart appears as "squares", the X and Y scales are equivalent (or nearly so)

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Make sure that point A is the highest elevation, "B" is the intermediate, and that point "C" is the lowest elevation value

STEP 2: Measure the relative bearings in quadrant format between "A>B" and "A>C". Also measure distances according to scale

Note that bearings must be entered according to the precision (i.e. decimal places) setting named "Angular Precision"

For example, a bearing measured as south 9.3 degrees west would be entered as "S 09.3 W" if angular precision = 1

STEP 3: Calculate the elevations of points A, B, and C with topographic contours or other means. Remember to convert drill depths to elevation

The worksheet assumes that units are equivalent among distance and elevation measurements. If not, convert to a consistent unit system at this step

STEP 4: Enter the measurements from steps 1-3 into the cells in blue color below. The attitudes of the two vectors "A>B" and "A>C"

will appear below the heading "Vector Attitude"

STEP 5: Read the strike and dip of the plane containing apparent dips 1 & 2 at the lower right

of the spreadsheet. Answers appear in dark green color. Also calculated are the pole azimuth and plunge, the hydraulic flow

direction azimuth, and the gradient. The gradient horizontal vs. vertical scale conversion is controlled by the cell

right of the label "H/V conversion". Use 1000 for meters per kilometer, or 5280 for feet per mile gradient units

NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing

Also note that by default the cells below App. dip 1 & App. dip 2 receive the calculated vector attitudes. If you already have the apparent dip

attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event

that you need to revert back to using elevation and distance measurements

## Accumulation Macro

The accumulation macro is designed to copy the calculated results of the current 3-point problem to the sheet named

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attitude of the strike line calculated by the algorithm. By default the X and Y axis are set to an "autoscale" the

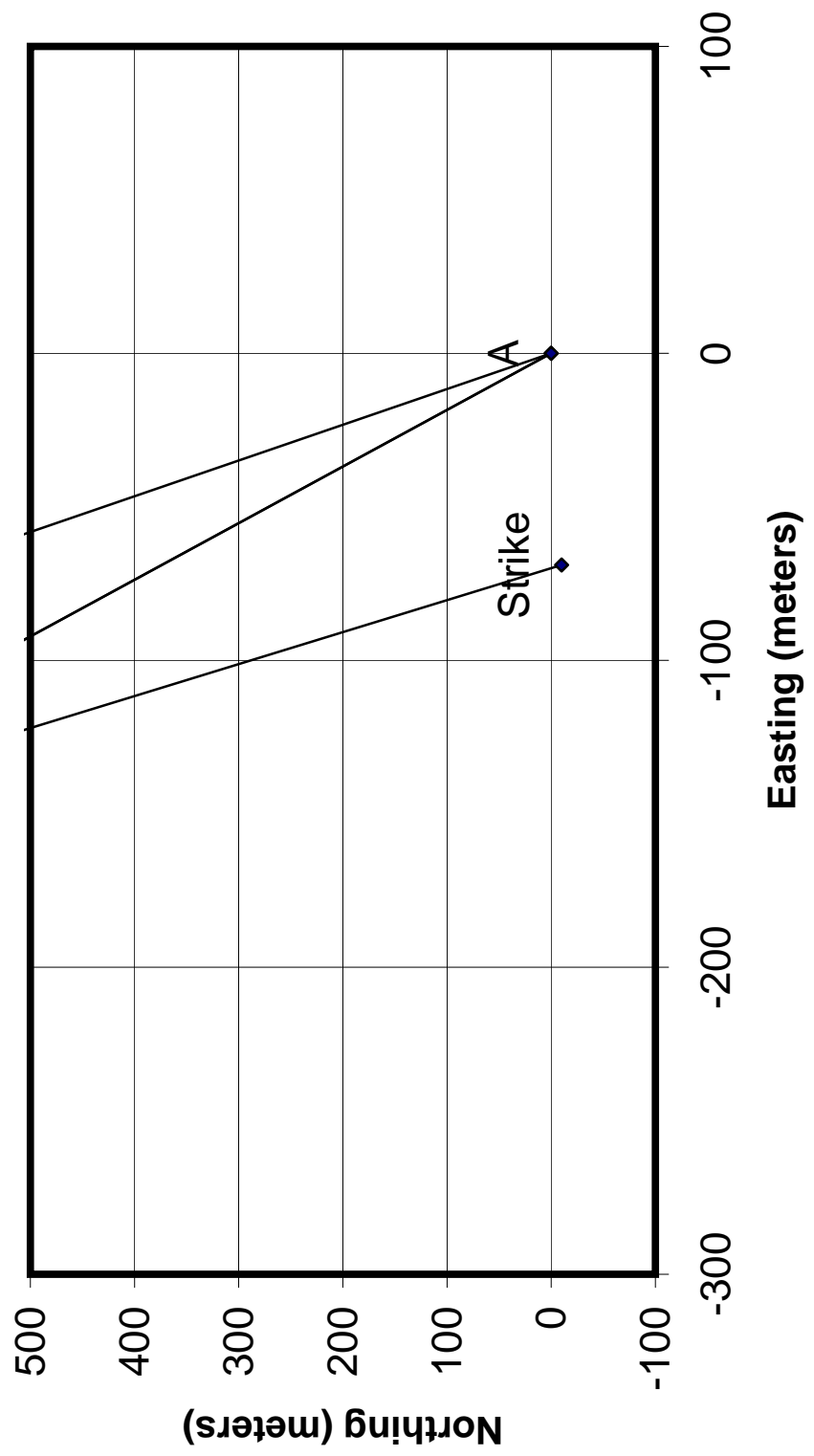
unfortunately will not generally set equivalent X and Y increments. After the elements of the problem are entered you

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"squares" rather than rectangles. This means that the scaling is equivalent (or very close) on both axes, therefore

the graph is no longer distorted.

# Three Point Problem







| Three-Point Problem Solver  |                                 |                              |                       |                     |                            |   |
|---|---------------------------------|------------------------------|-----------------------|---------------------|----------------------------|---|
| <b>Usage</b>  |                                 |                              |                       |                     |                            |   |
| This spreadsheet calculates the strike and true dip of a structural plane given three points on the plane that have known elevation and relative bearings and distances. Normally this is the case when a planar geologic contact can be traced over irregular topography. The three elevations are determined from topographic contours whereas the bearings are measured with a protractor relative to geographic north. Distances between points are measured using the map scale. Alternatively, contours of subsurface structures may be used to measure the required parameters, however remember that this method assumes that the structure is planar! This spreadsheet may be used to determine the hydraulic flow direction below the water table, which is the true dip direction.   |                                 |                              |                       |                     |                            |   |
| Detailed steps for using the below worksheet can be found in the "Documentation" sheet (next sheet)   |                                 |                              |                       |                     |                            |   |
| NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing   |                                 |                              |                       |                     |                            |   |
| Also note that by default the cells below "App. dip 1" & "App. dip 2" receive the calculated vector attitudes. If you already have the apparent dip attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event that you need to revert back to using elevation and distance measurements. The combined strike and dip attitude is displayed in green at lower right in case the solution needs to be copied to another application such as NETPROG   |                                 |                              |                       |                     |                            |   |
| <b>Calculation Method</b>   |                                 |                              |                       |                     |                            |   |
| The method works via the cross-product of two vectors. The two vectors defined by "A-B" and "A-C" must lie within the structural plane for which we want to know the strike and dip. The upper portion of the spreadsheet converts the raw data into the attitude of these two vectors. In the upper portion of the spreadsheet the two vectors are converted into directional cosines, and then the cross-product is taken. The cross-product yields the attitude of the vector perpendicular to the plane that contains the original two vectors. This is analogous to the problem of calculating a strike and dip of a plane from two given apparent dips, which are in fact simply two lines that lay within the plane. The rest of the spreadsheet converts the pole into a more familiar strike and true dip in quadrant format |                                 |                              |                       |                     |                            |   |
| Angular Precision   | 2                               | Angular Field Width:         | 5                     | H/V Conversion      | 1000.000                   | m/km  |
| Three Points with known elevations, relative bearings, and distances  |                                 |                              |                       |                     |                            |   |
| Point A   | Bearing<br>#N/A                 | Distance<br>#N/A             | Elevation<br>3576.000 | Inclinator<br>#N/A  | Vector attitude<br>#N/A    |   |
| Point B   | N 68.84 E                       | 46.280                       | 3509.000              | 55.365              | N 68.84 E 55.37            |   |
| Point C   | S 73.19 E                       | 95.590                       | 3574.000              | 1.199               | S 73.19 E 1.20             |   |
| Data Set  |                                 |                              |                       |                     |                            |   |
| Squirrel Coal Seam  | App. Dip 1<br>N 68.84 E 55.37   | App. Dip 2<br>S 73.19 E 1.20 | Azimuth 1<br>68.840   | Plunge 1<br>55.370  | Azimuth 2<br>106.810       | Plunge 2<br>1.200                           |
| App. dip 1  | Cos(beta)<br>0.530              | Cos(gamma)<br>0.823          | Cos(alpha)<br>0.957   | Cos(beta)<br>-0.289 | Cos(gamma)<br>0.021        | Theta<br>Angle(radians)<br>1.087            |
| Lower Hemisphere  | Cross-product<br>Flag<br>-0.395 | Cos(alpha)<br>-0.274         | Cos(beta)<br>-0.877   | Cos(gamma)<br>0.395 | Pole<br>Azimuth<br>197.326 | Pole<br>Plunge<br>23.258                    |
| Hydraulic Flow  | Gradient<br>Azimuth<br>17.33    | 2326.709                     |                       |                     |                            | Plane<br>Strike & Dip<br>N 72.67 W 66.74 NE |
| Graphical Data  |                                 |                              |                       |                     |                            |   |
| X   | Y                               | Point                        | Elev.                 |                     |                            |   |
| 0.000   | 0.000                           | A                            | 3576.000              |                     |                            |   |
| 43.160  | 16.706                          | B                            | 3509.000              |                     |                            |   |
| 91.505  | -27.645                         | C                            | 3574.000              |                     |                            |   |
| 0.000   | 0.000                           | A                            |                       |                     |                            |   |
| 43.160  | 16.706                          | B                            |                       |                     |                            |   |
| 87.340  | 2.923                           | Strike                       | N 72.67 W 66.74 NE    |                     |                            |   |
| -1.021  | 30.488                          | Strike                       | N 72.67 W 66.74 NE    |                     |                            |   |

## Symbolic block names

Symbolic names are used extensively throughout the three point solver spreadsheet to clarify calculation equations. The blue cells are where raw data is entered. Below are the definition:

| Name           | Definition or Value  |
|----------------|--|
| AppDip1        | Apparent dip bearing and plunge of A>B vector                          |
| AppDip2        | Apparent dip bearing and plunge of A>C vector                          |
| Az_1           | Azimuth (0-360) of apparent dip 1 (A>B).                               |
| Az_2           | Azimuth of apparent dip 2 (A>C).                                       |
| Bearing_B      | Entered bearing (quadrant format) of vector A>B                        |
| Bearing_C      | Entered bearing of vector A>C  |
| CalcAppDip1    | Calculated apparent dip vector 1 (A>B).                                |
| CalcAppDip2    | Calculated apparent dip vector 2 (A>C).                                |
| DistB          | Entered horizontal map distance from A to B                            |
| DistC          | Entered horizontal map distance from A to C                            |
| Elev1          | Entered elevation at point A   |
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| Elev3          | Entered elevation at point C.  |
| fl             | Field size (characters) for reported angular values                    |
| H_V_Conversion | Conversion factor for gradient units.                                  |
| Incline_B      | Calculated inclination (degrees) from point A to B                     |
| Incline_C      | Calculated inclination (degrees) from point A to C                     |
| LowerFlag      | Positive if cross product has a positive plunge angle, negative if not |
| Ndec           | Number of decimal places for reported angular values                   |
| Pl_1           | Plunge angle of the A>B vector   |
| Pl_2           | Plunge angle of the A>C vector.  |
| PoleAz         | Calculated azimuth angle (degrees) of the pole (cross product) vector  |
| PolePl         | Calculated plunge angle (degrees) of the pole (cross product) vector   |
| Theta_S        | Calculated angle (radians) between the apparent dip vectors            |
| X_1_Y_1_Z_1    | Directional components of apparent dip 1 (A>B)                         |
| X_2_Y_2_Z_2    | Directional components of apparent dip 2 (A>C)                         |
| X_S_Y_S_Z_S    | Directional components of the cross product solution (pole to plane)   |

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Make sure that point A is the highest elevation, "B" is the intermediate, and that point "C" is the lowest elevation value

STEP 2: Measure the relative bearings in quadrant format between "A>B" and "A>C". Also measure distances according to scale

Note that bearings must be entered according to the precision (i.e. decimal places) setting named "Angular Precision"

For example, a bearing measured as south 9.3 degrees west would be entered as "S 09.3 W" if angular precision = 1

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The worksheet assumes that units are equivalent among distance and elevation measurements. If not, convert to a consistent unit system at this step

STEP 4: Enter the measurements from steps 1-3 into the cells in blue color below. The attitudes of the two vectors "A>B" and "A>C"

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of the spreadsheet. Answers appear in dark green color. Also calculated are the pole azimuth and plunge, the hydraulic flow

direction azimuth, and the gradient. The gradient horizontal vs. vertical scale conversion is controlled by the cell

right of the label "H/V conversion". Use 1000 for meters per kilometer, or 5280 for feet per mile gradient units

NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing

Also note that by default the cells below App. dip 1 & App. dip 2 receive the calculated vector attitudes. If you already have the apparent dip

attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event

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name "AccumulateMacro" as the macro to run

## Graphical Plot

The graphical diagram in the sheet "Map" displays a map view of the elements of the 3-point problem. The point

labelled "A", "B", and "C" correspond to the 3 control points in the problem. The line labelled "strike" indicates the

attitude of the strike line calculated by the algorithm. By default the X and Y axis are set to an "autoscale" the

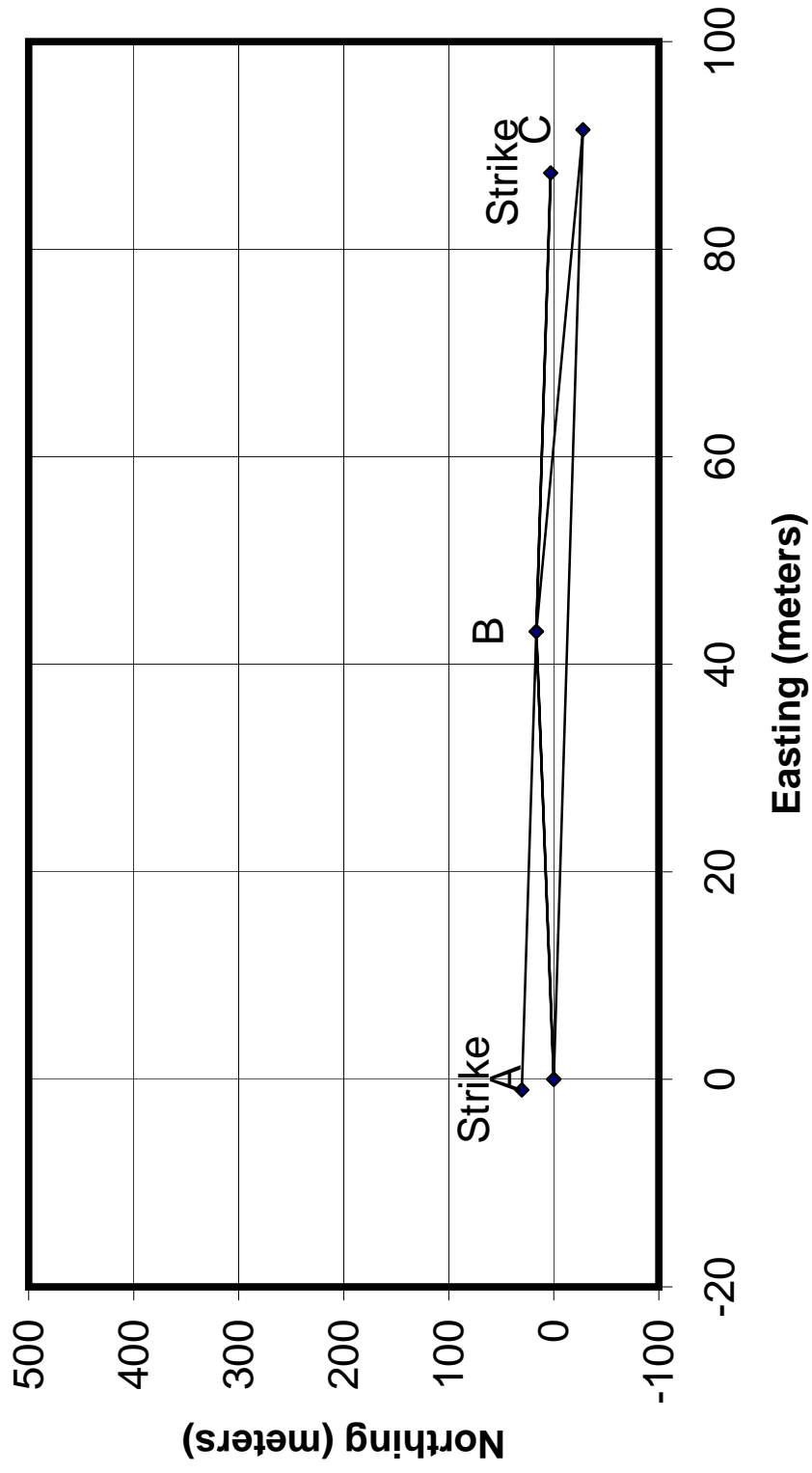
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"squares" rather than rectangles. This means that the scaling is equivalent (or very close) on both axes, therefore

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# Three Point Problem





**Accumulated 3-point problem solutions**

| Data Set  | Quadrant<br>App. Dip. 1 | Quadrant<br>App. Dip. 2 | Azimuth 1<br>Plunge 1 | Azimuth 2<br>Plunge 2 | Avg. dip. 1<br>Cos(alpha) | Cos(beta) | Cos(gamma) | Avg. dip. 2<br>Cos(alpha) | Cos(beta) | Cos(gamma) | Theia<br>Angle(ract) | Cross-product<br>Cos(alpha) | Cos(beta) | Cos(gamma) | Pole<br>Plunge | Pole<br>Strike & Dip |
|---|-------------------------|-------------------------|-----------------------|-----------------------|---------------------------|-----------|------------|---------------------------|-----------|------------|----------------------|-----------------------------|-----------|------------|----------------|----------------------|
|   |                         |                         |                       |                       |                           |           |            |                           |           |            |                      |                             |           |            |                |                      |
| <b>Note:</b> This calculation was performed for the Squirrel Coal Seam proximal to the Lori reservoir using data obtained at PD #1, PD #2, and PD #3. |                         |                         |                       |                       |                           |           |            |                           |           |            |                      |                             |           |            |                |                      |

| Three-Point Problem Solver   |                |                      |                   |                 |                 |                   |
|--|----------------|----------------------|-------------------|-----------------|-----------------|-------------------|
| <b>Usage</b>   |                |                      |                   |                 |                 |                   |
| This spreadsheet calculates the strike and true dip of a structural plane given three points on the plane that have known elevation and relative bearings and distances. Normally this is the case when a planar geologic contact can be traced over irregular topography. The three elevations are determined from topographic contours whereas the bearings are measured with a protractor relative to geographic north. Distances between points are measured using the map scale. Alternatively, contours of subsurface structures may be used to measure the required parameters, however, remember that this method assumes that the structure is planar! This spreadsheet may be used to determine the hydraulic flow direction below the water table, which is the true dip direction.                                       |                |                      |                   |                 |                 |                   |
| Detailed steps for using the below worksheet can be found in the "Documentation" sheet (next sheet).   |                |                      |                   |                 |                 |                   |
| NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing.   |                |                      |                   |                 |                 |                   |
| Also note that by default the cells below "App. dip 1" & "App. dip 2" receive the calculated vector attitudes. If you already have the apparent attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event that you need to revert back to using elevation and distance measurements. The combined strike and dip attitude is displayed in green at the bottom in case the solution needs to be copied to another application such as NETPROC.  |                |                      |                   |                 |                 |                   |
| <b>Calculation Method</b>  |                |                      |                   |                 |                 |                   |
| The method works via the cross-product of two vectors. The two vectors defined by "A-B" and "A-C" must lie within the structural plane for which we want to know the strike and dip. The upper portion of the spreadsheet converts the raw data into the attitude of these two vectors. In the upper portion of the spreadsheet the two vectors are converted into directional cosines, and then the cross-product is taken. The cross-product yields the attitude of the vector perpendicular to the plane that contains the original two vectors. This is analogous to the problem of calculating a strike and dip of a plane from two given apparent dips, which are in fact simply two lines that lay within the plane. The rest of the spreadsheet converts the pole into a more familiar strike and true dip in quadrant form: |                |                      |                   |                 |                 |                   |
| Angular Precision  | 2              | Angular Field Width: | 5                 | H/V Conversion: | 1000.000        | m/km              |
| Three Points with known elevations, relative bearings, and distance  |                |                      |                   |                 |                 |                   |
|  | Bearing        | Distance             | Elevation         | Inclination     | Vector attitude |                   |
| Point A  | #N/A           | #N/A                 | 3598.100          | #N/A            | #N/A            |                   |
| Point B  | N 67.44 E      | 765.890              | 3558.000          | 2.997           | N 67.44 E 3.00  |                   |
| Point C  | N 58.34 E      | 1267.390             | 3560.000          | 1.722           | N 58.34 E 1.72  |                   |
|  | Quadrant       | Quadrant             |                   |                 |                 |                   |
| Data Set   | App. Dip 1     | App. Dip 2           | Azimuth 1         | Plunge 1        | Azimuth 2       | Plunge 2          |
| Upper Roland Coal  | N 67.44 E 3.00 | N 58.34 E 1.72       | 67.440            | 3.000           | 58.340          | 1.720             |
| App. dip 1   |                |                      | App. dip 2        |                 |                 | Theta             |
| Cos(alpha)   | Cos(beta)      | Cos(gamma)           | Cos(alpha)        | Cos(beta)       | Cos(gamma)      | Angle(radians)    |
| 0.922  | 0.383          | 0.052                | 0.851             | 0.525           | 0.030           | 0.160             |
| Lower Hemisphere   | Cross-product  |                      |                   | Pole            | Pole            | Strike of         |
| Flag   | Cos(alpha)     | Cos(beta)            | Cos(gamma)        | Azimuth         | Plunge          | Plane             |
| 0.989  | -0.100         | 0.106                | 0.989             | 316.552         | 81.638          | N 46.55 E         |
|  |                |                      |                   |                 |                 | 8.36 SE           |
| Hydraulic Flow   | Gradient       |                      |                   |                 |                 | Plane             |
| Azimuth  | m/km           |                      |                   |                 |                 | Strike & Dip      |
| 136.55   | 146.988        |                      |                   |                 |                 | N 46.55 E 8.36 SE |
| Graphical Data   |                |                      |                   |                 |                 |                   |
| X  | Y              | Point                | Elev.             |                 |                 |                   |
| 0.000  | 0.000          | A                    | 3598.100          |                 |                 |                   |
| 707.283  | 293.834        | B                    | 3558.000          |                 |                 |                   |
| 1078.774   | 665.225        | C                    | 3560.000          |                 |                 |                   |
| 0.000  | 0.000          | A                    |                   |                 |                 |                   |
| 707.283  | 293.834        | B                    |                   |                 |                 |                   |
| 151.249  | -232.867       | Strike               | N 46.55 E 8.36 SE |                 |                 |                   |
| 1263.317   | 820.535        | Strike               | N 46.55 E 8.36 SE |                 |                 |                   |

## Symbolic block names

Symbolic names are used extensively throughout the three point solver spreadsheet to clarify calculation equations. The blue cells are where raw data is entered. Below are the definition:

| Name           | Definition or Value  |
|----------------|--|
| AppDip1        | Apparent dip bearing and plunge of A>B vector                          |
| AppDip2        | Apparent dip bearing and plunge of A>C vector                          |
| Az_1           | Azimuth (0-360) of apparent dip 1 (A>B).                               |
| Az_2           | Azimuth of apparent dip 2 (A>C).                                       |
| Bearing_B      | Entered bearing (quadrant format) of vector A>B                        |
| Bearing_C      | Entered bearing of vector A>C  |
| CalcAppDip1    | Calculated apparent dip vector 1 (A>B).                                |
| CalcAppDip2    | Calculated apparent dip vector 2 (A>C).                                |
| DistB          | Entered horizontal map distance from A to B                            |
| DistC          | Entered horizontal map distance from A to C                            |
| Elev1          | Entered elevation at point A   |
| Elev2          | Entered elevation at point B   |
| Elev3          | Entered elevation at point C.  |
| fl             | Field size (characters) for reported angular values                    |
| H_V_Conversion | Conversion factor for gradient units.                                  |
| Incline_B      | Calculated inclination (degrees) from point A to B                     |
| Incline_C      | Calculated inclination (degrees) from point A to C                     |
| LowerFlag      | Positive if cross product has a positive plunge angle, negative if not |
| Ndec           | Number of decimal places for reported angular values                   |
| Pl_1           | Plunge angle of the A>B vector   |
| Pl_2           | Plunge angle of the A>C vector.  |
| PoleAz         | Calculated azimuth angle (degrees) of the pole (cross product) vector  |
| PolePl         | Calculated plunge angle (degrees) of the pole (cross product) vector   |
| Theta_S        | Calculated angle (radians) between the apparent dip vectors            |
| X_1_Y_1_Z_1    | Directional components of apparent dip 1 (A>B)                         |
| X_2_Y_2_Z_2    | Directional components of apparent dip 2 (A>C)                         |
| X_S_Y_S_Z_S    | Directional components of the cross product solution (pole to plane)   |

Note that the geometry of the problem is depicted in graphical form in the following worksheet chart. The user should be aware that the chart will almost always use different X and Y scales by default. It will be the responsibility of the user to override the default scaling so that the X and Y scales are equivalent. If the grid on the chart appears as "squares", the X and Y scales are equivalent (or nearly so)

STEP 1: From the base map pick the higher elevation point and label it as "A". Label the intermediate and lowest elevation points "B" and "C"

Make sure that point A is the highest elevation, "B" is the intermediate, and that point "C" is the lowest elevation value

STEP 2: Measure the relative bearings in quadrant format between "A>B" and "A>C". Also measure distances according to scale

Note that bearings must be entered according to the precision (i.e. decimal places) setting named "Angular Precision"

For example, a bearing measured as south 9.3 degrees west would be entered as "S 09.3 W" if angular precision = 1

STEP 3: Calculate the elevations of points A, B, and C with topographic contours or other means. Remember to convert drill depths to elevation

The worksheet assumes that units are equivalent among distance and elevation measurements. If not, convert to a consistent unit system at this step

STEP 4: Enter the measurements from steps 1-3 into the cells in blue color below. The attitudes of the two vectors "A>B" and "A>C"

will appear below the heading "Vector Attitude"

STEP 5: Read the strike and dip of the plane containing apparent dips 1 & 2 at the lower right

of the spreadsheet. Answers appear in dark green color. Also calculated are the pole azimuth and plunge, the hydraulic flow

direction azimuth, and the gradient. The gradient horizontal vs. vertical scale conversion is controlled by the cell

right of the label "H/V conversion". Use 1000 for meters per kilometer, or 5280 for feet per mile gradient units

NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing

Also note that by default the cells below App. dip 1 & App. dip 2 receive the calculated vector attitudes. If you already have the apparent dip

attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event

that you need to revert back to using elevation and distance measurements

## Accumulation Macro

The accumulation macro is designed to copy the calculated results of the current 3-point problem to the sheet named

"Accumulation". You can run the macro with the menu sequence "Tools > Macro > Macros", and then indicate the

name "AccumulateMacro" as the macro to run

## Graphical Plot

The graphical diagram in the sheet "Map" displays a map view of the elements of the 3-point problem. The point

labelled "A", "B", and "C" correspond to the 3 control points in the problem. The line labelled "strike" indicates the

attitude of the strike line calculated by the algorithm. By default the X and Y axis are set to an "autoscale" the

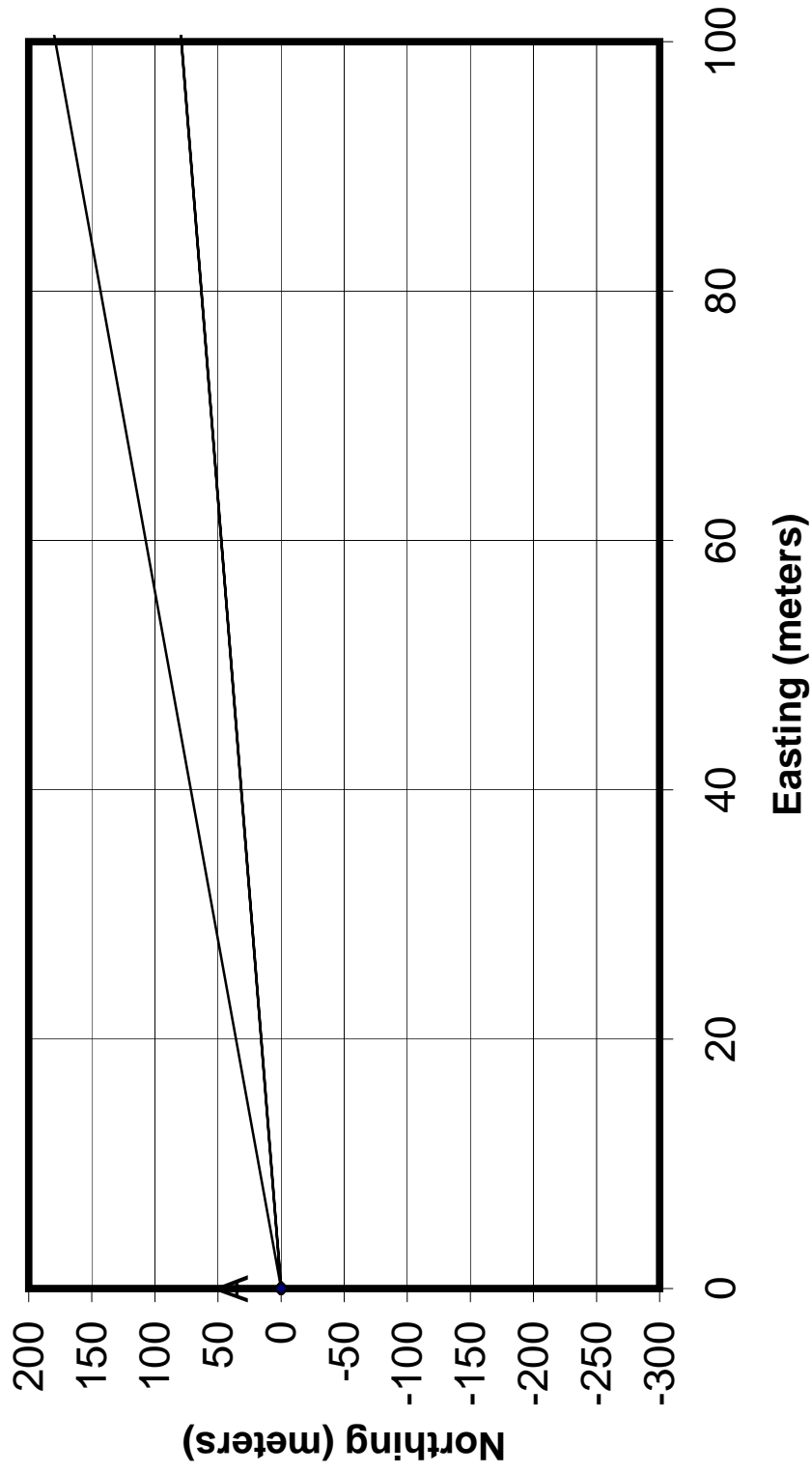
unfortunately will not generally set equivalent X and Y increments. After the elements of the problem are entered you

should edit the X and Y scale settings in "manual" mode so that the grid on the graph appears as a collection of

"squares" rather than rectangles. This means that the scaling is equivalent (or very close) on both axes, therefore

the graph is no longer distorted.

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|                                       |          |            |           |           |           |          |            |            |           |            |            |            |           |            |            |            |           |            |            |            |           |            |       |               |            |           |            |               |        |            |              |           |  |            |  |      |  |        |  |       |  |              |  |
|---------------------------------------|----------|------------|-----------|-----------|-----------|----------|------------|------------|-----------|------------|------------|------------|-----------|------------|------------|------------|-----------|------------|------------|------------|-----------|------------|-------|---------------|------------|-----------|------------|---------------|--------|------------|--------------|-----------|--|------------|--|------|--|--------|--|-------|--|--------------|--|
| Accumulated 3-point problem solutions |          | Quadrant   |           | Azimuth 1 |           | Plunge 1 |            | Azimuth 2  |           | Plunge 2   |            | App. dip 1 |           | Cos(beta)  |            | Cos(gamma) |           | App. dip 2 |            | Cos(alpha) |           | Cos(beta)  |       | Cos(gamma)    |            | Theia     |            | Cross-product |        | Cos(alpha) |              | Cos(beta) |  | Cos(gamma) |  | Pole |  | Plunge |  | Plane |  | Strike & Dip |  |
| Data Set                              | Quadrant | App. Dip 1 | Azimuth 1 | Plunge 1  | Azimuth 2 | Plunge 2 | App. dip 1 | Cos(alpha) | Cos(beta) | Cos(gamma) | App. dip 2 | Cos(alpha) | Cos(beta) | Cos(gamma) | App. dip 1 | Cos(alpha) | Cos(beta) | Cos(gamma) | App. dip 2 | Cos(alpha) | Cos(beta) | Cos(gamma) | Theia | Cross-product | Cos(alpha) | Cos(beta) | Cos(gamma) | Pole          | Plunge | Plane      | Strike & Dip |           |  |            |  |      |  |        |  |       |  |              |  |

| Three-Point Problem Solver   |                |                      |            |                 |                 |                   |
|--|----------------|----------------------|------------|-----------------|-----------------|-------------------|
| <b>Usage</b>   |                |                      |            |                 |                 |                   |
| This spreadsheet calculates the strike and true dip of a structural plane given three points on the plane that have known elevation and relative bearings and distances. Normally this is the case when a planar geologic contact can be traced over irregular topography. The three elevations are determined from topographic contours whereas the bearings are measured with a protractor relative to geographic north. Distances between points are measured using the map scale. Alternatively, contours of subsurface structures may be used to measure the required parameters, however remember that this method assumes that the structure is planar! This spreadsheet may be used to determine the hydraulic flow direction below the water table, which is the true dip direction.  |                |                      |            |                 |                 |                   |
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| <b>Calculation Method</b>  |                |                      |            |                 |                 |                   |
| The method works via the cross-product of two vectors. The two vectors defined by "A-B" and "A-C" must lie within the structural plane for which we want to know the strike and dip. The upper portion of the spreadsheet converts the raw data into the attitude of these two vectors. In the upper portion of the spreadsheet the two vectors are converted into directional cosines, and then the cross-product is taken. The cross-product yields the attitude of the vector perpendicular to the plane that contains the original two vectors. This is analogous to the problem of calculating a strike and dip of a plane from two given apparent dips, which are in fact simply two lines that lay within the plane. The rest of the spreadsheet converts the pole into a more familiar strike and true dip in quadrant form: |                |                      |            |                 |                 |                   |
| Angular Precision  | 2              | Angular Field Width: | 5          | H/V Conversion: | 1000.000        | m/km              |
| <b>Three Points with known elevations, relative bearings, and distance</b>   |                |                      |            |                 |                 |                   |
|  | Bearing        | Distance             | Elevation  | Inclination     | Vector attitude |                   |
| Point A  | #N/A           | #N/A                 | 3768.000   | #N/A            | #N/A            |                   |
| Point B  | S 61.48 W      | 587.490              | 3764.000   | 0.390           | S 61.48 W 0.39  |                   |
| Point C  | S 72.12 W      | 602.110              | 3769.000   | -0.095          | S 72.12 W -0.10 |                   |
|  | Quadrant       | Quadrant             |            |                 |                 |                   |
| Data Set   | App. Dip 1     | App. Dip 2           | Azimuth 1  | Plunge 1        | Azimuth 2       | Plunge 2          |
| Termo  | S 61.48 W 0.39 | S 72.12 W -0.10      | 241.480    | 0.390           | 252.120         | -0.100            |
| App. dip 1   |                |                      | App. dip 2 |                 |                 | Theta             |
| Cos(alpha)   | Cos(beta)      | Cos(gamma)           | Cos(alpha) | Cos(beta)       | Cos(gamma)      | Angle(radians)    |
| -0.879   | -0.477         | 0.007                | -0.952     | -0.307          | -0.002          | 0.186             |
| Lower Hemisphere   | Cross-product  |                      |            | Pole            | Pole            | Strike of         |
| Flag   | Cos(alpha)     | Cos(beta)            | Cos(gamma) | Azimuth         | Plunge          | Plane             |
| -0.999   | -0.016         | 0.043                | 0.999      | 339.954         | 87.355          | N 69.95 E         |
|  |                |                      |            |                 |                 | 2.64 SE           |
| Hydraulic Flow   | Gradient       |                      |            |                 |                 | Plane             |
| Azimuth  | m/km           |                      |            |                 |                 | Strike & Dip      |
| 159.95   | 46.189         |                      |            |                 |                 | N 69.95 E 2.64 SE |
| Graphical Data   |                |                      |            |                 |                 |                   |
| X  | Y              | Point                | Elev.      |                 |                 |                   |
| 0.000  | 0.000          | A                    | 3768.000   |                 |                 |                   |
| -516.198   | -280.506       | B                    | 3764.000   |                 |                 |                   |
| -573.029   | -184.862       | C                    | 3769.000   |                 |                 |                   |
| 0.000  | 0.000          | A                    |            |                 |                 |                   |
| -516.198   | -280.506       | B                    |            |                 |                 |                   |
| -1068.099  | -481.878       | Strike               |            |                 |                 | N 69.95 E 2.64 SE |
| 35.702   | -79.134        | Strike               |            |                 |                 | N 69.95 E 2.64 SE |

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| Bearing_B      | Entered bearing (quadrant format) of vector A>B                        |
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| CalcAppDip1    | Calculated apparent dip vector 1 (A>B).                                |
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| DistB          | Entered horizontal map distance from A to B                            |
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| Elev1          | Entered elevation at point A   |
| Elev2          | Entered elevation at point B   |
| Elev3          | Entered elevation at point C.  |
| fl             | Field size (characters) for reported angular values                    |
| H_V_Conversion | Conversion factor for gradient units.                                  |
| Incline_B      | Calculated inclination (degrees) from point A to B                     |
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| LowerFlag      | Positive if cross product has a positive plunge angle, negative if not |
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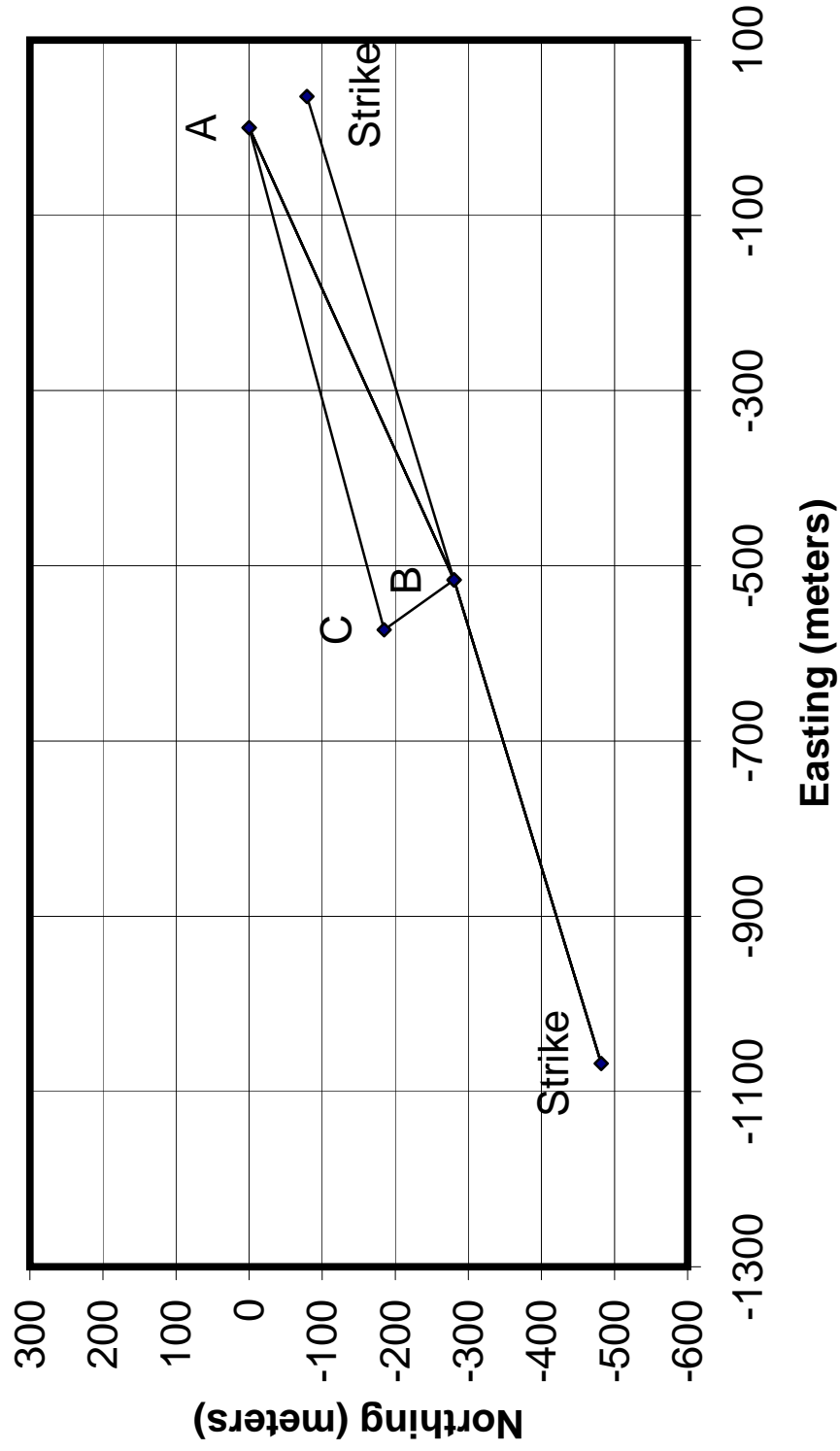
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| Angular Precision  | 2              | Angular Field Width: | 5                  | H/V Conversion: | 1000.000        | m/km               |
| <b>Three Points with known elevations, relative bearings, and distance</b>   |                |                      |                    |                 |                 |                    |
|  | Bearing        | Distance             | Elevation          | Inclination     | Vector attitude |                    |
| Point A  | #N/A           | #N/A                 | 1200.000           | #N/A            | #N/A            |                    |
| Point B  | N 83.00 W      | 4148.000             | 950.000            | 3.449           | N 83.00 W 3.45  |                    |
| Point C  | N 46.00 W      | 2143.000             | 550.000            | 16.873          | N 46.00 W 16.87 |                    |
|  | Quadrant       | Quadrant             |                    |                 |                 |                    |
| Data Set   | App. Dip 1     | App. Dip 2           | Azimuth 1          | Plunge 1        | Azimuth 2       | Plunge 2           |
| South Drive  | N 83.00 W 3.45 | N 46.00 W 16.87      | 277.000            | 3.450           | 314.000         | 16.870             |
| App. dip 1   |                |                      | App. dip 2         |                 |                 | Theta              |
| Cos(alpha)   | Cos(beta)      | Cos(gamma)           | Cos(alpha)         | Cos(beta)       | Cos(gamma)      | Angle(radians)     |
| -0.991   | 0.122          | 0.060                | -0.688             | 0.665           | 0.290           | 0.676              |
| Lower Hemisphere   | Cross-product  |                      |                    | Pole            | Pole            | Strike of          |
| Flag   | Cos(alpha)     | Cos(beta)            | Cos(gamma)         | Azimuth         | Plunge          | Plane              |
| -0.919   | 0.008          | -0.394               | 0.919              | 178.906         | 66.821          | N 88.91 E          |
|  |                |                      |                    |                 |                 | 23.18 NW           |
| Hydraulic Flow   | Gradient       |                      |                    |                 |                 | Plane              |
| Azimuth  | m/km           |                      |                    |                 |                 | Strike & Dip       |
| 358.91   | 428.157        |                      |                    |                 |                 | N 88.91 E 23.18 NW |
| Graphical Data   |                |                      |                    |                 |                 |                    |
| X  | Y              | Point                | Elev.              |                 |                 |                    |
| 0.000  | 0.000          | A                    | 1200.000           |                 |                 |                    |
| -4117.081  | 505.514        | B                    | 950.000            |                 |                 |                    |
| -1541.545  | 1488.653       | C                    | 550.000            |                 |                 |                    |
| 0.000  | 0.000          | A                    |                    |                 |                 |                    |
| -4117.081  | 505.514        | B                    |                    |                 |                 |                    |
| 30.162   | 584.743        | Strike               | N 88.91 E 23.18 NW |                 |                 |                    |
| -8264.325  | 426.285        | Strike               | N 88.91 E 23.18 NW |                 |                 |                    |

## Symbolic block names

Symbolic names are used extensively throughout the three point solver spreadsheet to clarify calculation equations. The blue cells are where raw data is entered. Below are the definition:

| Name           | Definition or Value  |
|----------------|--|
| AppDip1        | Apparent dip bearing and plunge of A>B vector                          |
| AppDip2        | Apparent dip bearing and plunge of A>C vector                          |
| Az_1           | Azimuth (0-360) of apparent dip 1 (A>B).                               |
| Az_2           | Azimuth of apparent dip 2 (A>C).                                       |
| Bearing_B      | Entered bearing (quadrant format) of vector A>B                        |
| Bearing_C      | Entered bearing of vector A>C  |
| CalcAppDip1    | Calculated apparent dip vector 1 (A>B).                                |
| CalcAppDip2    | Calculated apparent dip vector 2 (A>C).                                |
| DistB          | Entered horizontal map distance from A to B                            |
| DistC          | Entered horizontal map distance from A to C                            |
| Elev1          | Entered elevation at point A   |
| Elev2          | Entered elevation at point B   |
| Elev3          | Entered elevation at point C.  |
| fl             | Field size (characters) for reported angular values                    |
| H_V_Conversion | Conversion factor for gradient units.                                  |
| Incline_B      | Calculated inclination (degrees) from point A to B                     |
| Incline_C      | Calculated inclination (degrees) from point A to C                     |
| LowerFlag      | Positive if cross product has a positive plunge angle, negative if not |
| Ndec           | Number of decimal places for reported angular values                   |
| Pl_1           | Plunge angle of the A>B vector   |
| Pl_2           | Plunge angle of the A>C vector.  |
| PoleAz         | Calculated azimuth angle (degrees) of the pole (cross product) vector  |
| PolePl         | Calculated plunge angle (degrees) of the pole (cross product) vector   |
| Theta_S        | Calculated angle (radians) between the apparent dip vectors            |
| X_1_Y_1_Z_1    | Directional components of apparent dip 1 (A>B)                         |
| X_2_Y_2_Z_2    | Directional components of apparent dip 2 (A>C)                         |
| X_S_Y_S_Z_S    | Directional components of the cross product solution (pole to plane)   |

Note that the geometry of the problem is depicted in graphical form in the following worksheet chart. The user should be aware that the chart will almost always use different X and Y scales by default. It will be the responsibility of the user to override the default scaling so that the X and Y scales are equivalent. If the grid on the chart appears as "squares", the X and Y scales are equivalent (or nearly so)

STEP 1: From the base map pick the higher elevation point and label it as "A". Label the intermediate and lowest elevation points "B" and "C"

Make sure that point A is the highest elevation, "B" is the intermediate, and that point "C" is the lowest elevation value

STEP 2: Measure the relative bearings in quadrant format between "A>B" and "A>C". Also measure distances according to scale

Note that bearings must be entered according to the precision (i.e. decimal places) setting named "Angular Precision"

For example, a bearing measured as south 9.3 degrees west would be entered as "S 09.3 W" if angular precision = 1

STEP 3: Calculate the elevations of points A, B, and C with topographic contours or other means. Remember to convert drill depths to elevation

The worksheet assumes that units are equivalent among distance and elevation measurements. If not, convert to a consistent unit system at this step

STEP 4: Enter the measurements from steps 1-3 into the cells in blue color below. The attitudes of the two vectors "A>B" and "A>C"

will appear below the heading "Vector Attitude"

STEP 5: Read the strike and dip of the plane containing apparent dips 1 & 2 at the lower right

of the spreadsheet. Answers appear in dark green color. Also calculated are the pole azimuth and plunge, the hydraulic flow

direction azimuth, and the gradient. The gradient horizontal vs. vertical scale conversion is controlled by the cell

right of the label "H/V conversion". Use 1000 for meters per kilometer, or 5280 for feet per mile gradient units

NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing

Also note that by default the cells below App. dip 1 & App. dip 2 receive the calculated vector attitudes. If you already have the apparent dip

attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event

that you need to revert back to using elevation and distance measurements

## Accumulation Macro

The accumulation macro is designed to copy the calculated results of the current 3-point problem to the sheet named

"Accumulation". You can run the macro with the menu sequence "Tools > Macro > Macros", and then indicate the

name "AccumulateMacro" as the macro to run

## Graphical Plot

The graphical diagram in the sheet "Map" displays a map view of the elements of the 3-point problem. The point

labelled "A", "B", and "C" correspond to the 3 control points in the problem. The line labelled "strike" indicates the

attitude of the strike line calculated by the algorithm. By default the X and Y axis are set to an "autoscale" the

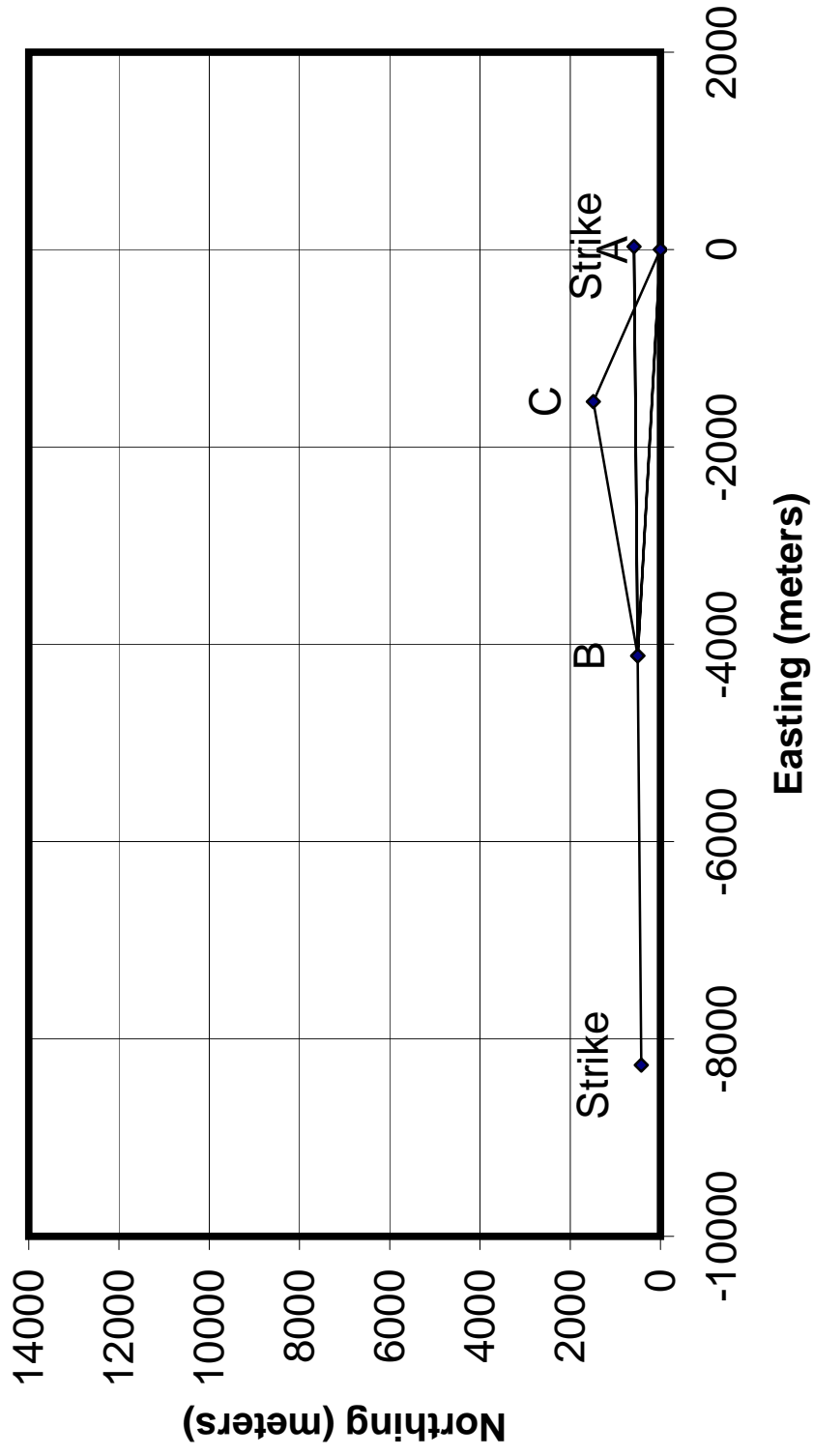
unfortunately will not generally set equivalent X and Y increments. After the elements of the problem are entered you

should edit the X and Y scale settings in "manual" mode so that the grid on the graph appears as a collection of

"squares" rather than rectangles. This means that the scaling is equivalent (or very close) on both axes, therefore

the graph is no longer distorted.

# Three Point Problem





Accumulated 3-point problem solutions

| Data Set    | Quadrant       |                 | Plunge 1  |          | Plunge 2  |          | App. dip 1 |          | App. dip 2 |          | Theila Angle(rad.) |           | Cross-product |           | Pole    |        | Plane   |        |                    |
|-------------|----------------|-----------------|-----------|----------|-----------|----------|------------|----------|------------|----------|--------------------|-----------|---------------|-----------|---------|--------|---------|--------|--------------------|
|             | N              | W               | Azimuth 1 | Plunge 1 | Azimuth 2 | Plunge 2 | Azimuth 1  | Plunge 1 | Azimuth 2  | Plunge 2 | Cos(alpha)         | Cos(beta) | Cos(alpha)    | Cos(beta) | Azimuth | Plunge | Strike  | Dip    |                    |
| South Drive | N 83.00 W 3.45 | N 46.00 W 16.87 | 277.000   | 3.450    | 314.000   | 16.870   | -0.991     | 0.122    | 0.060      | -0.688   | 0.665              | 0.290     | 0.576         | 0.008     | -0.394  | 0.919  | 178.906 | 66.821 | N 88.91 E 23.18 NW |

| Three-Point Problem Solver  |                |                      |            |                |                 |                    |
|---|----------------|----------------------|------------|----------------|-----------------|--------------------|
| <b>Usage</b>  |                |                      |            |                |                 |                    |
| This spreadsheet calculates the strike and true dip of a structural plane given three points on the plane that have known elevation and relative bearings and distances. Normally this is the case when a planar geologic contact can be traced over irregular topography. The three elevations are determined from topographic contours whereas the bearings are measured with a protractor relative to geographic north. Distances between points are measured using the map scale. Alternatively, contours of subsurface structures may be used to measure the required parameters, however remember that this method assumes that the structure is planar! This spreadsheet may be used to determine the hydraulic flow direction below the water table, which is the true dip direction.   |                |                      |            |                |                 |                    |
| Detailed steps for using the below worksheet can be found in the "Documentation" sheet (next sheet)   |                |                      |            |                |                 |                    |
| NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing   |                |                      |            |                |                 |                    |
| Also note that by default the cells below "App. dip 1" & "App. dip 2" receive the calculated vector attitudes. If you already have the apparent dip attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event that you need to revert back to using elevation and distance measurements. The combined strike and dip attitude is displayed in green at lower right in case the solution needs to be copied to another application such as NETPROG   |                |                      |            |                |                 |                    |
| <b>Calculation Method</b>   |                |                      |            |                |                 |                    |
| The method works via the cross-product of two vectors. The two vectors defined by "A-B" and "A-C" must lie within the structural plane for which we want to know the strike and dip. The upper portion of the spreadsheet converts the raw data into the attitude of these two vectors. In the upper portion of the spreadsheet the two vectors are converted into directional cosines, and then the cross-product is taken. The cross-product yields the attitude of the vector perpendicular to the plane that contains the original two vectors. This is analogous to the problem of calculating a strike and dip of a plane from two given apparent dips, which are in fact simply two lines that lay within the plane. The rest of the spreadsheet converts the pole into a more familiar strike and true dip in quadrant format |                |                      |            |                |                 |                    |
| Angular Precision   | 2              | Angular Field Width: | 5          | H/V Conversion | 1000.000        | m/km               |
| Three Points with known elevations, relative bearings, and distances  |                |                      |            |                |                 |                    |
|   | Bearing        | Distance             | Elevation  | Inclinator     | Vector attitude |                    |
| Point A   | #N/A           | #N/A                 | 3717.000   | #N/A           | #N/A            |                    |
| Point B   | N 79.41 W      | 569.640              | 3689.000   | 2.814          | N 79.41 W 2.81  |                    |
| Point C   | S 89.33 W      | 555.230              | 3716.000   | 0.103          | S 89.33 W 0.10  |                    |
|   | Quadrant       | Quadrant             |            |                |                 |                    |
| Data Set  | App. Dip 1     | App. Dip 2           | Azimuth 1  | Plunge 1       | Azimuth 2       | Plunge 2           |
| WayLon  | N 79.41 W 2.81 | S 89.33 W 0.10       | 280.590    | 2.810          | 269.330         | 0.100              |
| App. dip 1  |                |                      | App. dip 2 |                |                 | Theta              |
| Cos(alpha)  | Cos(beta)      | Cos(gamma)           | Cos(alpha) | Cos(beta)      | Cos(gamma)      | Angle(radians)     |
| -0.982  | 0.184          | 0.049                | -1.000     | -0.012         | 0.002           | 0.202              |
| Lower Hemisphere  | Cross-product  |                      |            | Pole           | Pole            | Strike of Plane    |
| Flag  | Cos(alpha)     | Cos(beta)            | Cos(gamma) | Azimuth        | Plunge          | True Dip           |
| 0.972   | 0.004          | -0.236               | 0.972      | 178.918        | 76.363          | N 88.92 E 13.64 NW |
| Hydraulic Flow  | Gradient       |                      |            |                |                 | Plane              |
| Azimuth   | m/km           |                      |            |                |                 | Strike & Dip       |
| 358.92  | 242.611        |                      |            |                |                 | N 88.92 E 13.64 NW |
| Graphical Data  |                |                      |            |                |                 |                    |
| X   | Y              | Point                | Elev.      |                |                 |                    |
| 0.000   | 0.000          | A                    | 3717.000   |                |                 |                    |
| -559.938  | 104.688        | B                    | 3689.000   |                |                 |                    |
| -555.192  | -6.493         | C                    | 3716.000   |                |                 |                    |
| 0.000   | 0.000          | A                    |            |                |                 |                    |
| -559.938  | 104.688        | B                    |            |                |                 |                    |
| 9.601   | 115.447        | Strike               |            |                |                 | N 88.92 E 13.64 NW |
| -1129.476   | 93.930         | Strike               |            |                |                 | N 88.92 E 13.64 NW |

## Symbolic block names

Symbolic names are used extensively throughout the three point solver spreadsheet to clarify calculation equations. The blue cells are where raw data is entered. Below are the definition:

| Name           | Definition or Value  |
|----------------|--|
| AppDip1        | Apparent dip bearing and plunge of A>B vector                          |
| AppDip2        | Apparent dip bearing and plunge of A>C vector                          |
| Az_1           | Azimuth (0-360) of apparent dip 1 (A>B).                               |
| Az_2           | Azimuth of apparent dip 2 (A>C).                                       |
| Bearing_B      | Entered bearing (quadrant format) of vector A>B                        |
| Bearing_C      | Entered bearing of vector A>C  |
| CalcAppDip1    | Calculated apparent dip vector 1 (A>B).                                |
| CalcAppDip2    | Calculated apparent dip vector 2 (A>C).                                |
| DistB          | Entered horizontal map distance from A to B                            |
| DistC          | Entered horizontal map distance from A to C                            |
| Elev1          | Entered elevation at point A   |
| Elev2          | Entered elevation at point B   |
| Elev3          | Entered elevation at point C.  |
| fl             | Field size (characters) for reported angular values                    |
| H_V_Conversion | Conversion factor for gradient units.                                  |
| Incline_B      | Calculated inclination (degrees) from point A to B                     |
| Incline_C      | Calculated inclination (degrees) from point A to C                     |
| LowerFlag      | Positive if cross product has a positive plunge angle, negative if not |
| Ndec           | Number of decimal places for reported angular values                   |
| Pl_1           | Plunge angle of the A>B vector   |
| Pl_2           | Plunge angle of the A>C vector.  |
| PoleAz         | Calculated azimuth angle (degrees) of the pole (cross product) vector  |
| PolePl         | Calculated plunge angle (degrees) of the pole (cross product) vector   |
| Theta_S        | Calculated angle (radians) between the apparent dip vectors            |
| X_1_Y_1_Z_1    | Directional components of apparent dip 1 (A>B)                         |
| X_2_Y_2_Z_2    | Directional components of apparent dip 2 (A>C)                         |
| X_S_Y_S_Z_S    | Directional components of the cross product solution (pole to plane)   |

Note that the geometry of the problem is depicted in graphical form in the following worksheet chart. The user should be aware that the chart will almost always use different X and Y scales by default. It will be the responsibility of the user to override the default scaling so that the X and Y scales are equivalent. If the grid on the chart appears as "squares", the X and Y scales are equivalent (or nearly so)

STEP 1: From the base map pick the higher elevation point and label it as "A". Label the intermediate and lowest elevation points "B" and "C"

Make sure that point A is the highest elevation, "B" is the intermediate, and that point "C" is the lowest elevation value

STEP 2: Measure the relative bearings in quadrant format between "A>B" and "A>C". Also measure distances according to scale

Note that bearings must be entered according to the precision (i.e. decimal places) setting named "Angular Precision"

For example, a bearing measured as south 9.3 degrees west would be entered as "S 09.3 W" if angular precision = 1

STEP 3: Calculate the elevations of points A, B, and C with topographic contours or other means. Remember to convert drill depths to elevation

The worksheet assumes that units are equivalent among distance and elevation measurements. If not, convert to a consistent unit system at this step

STEP 4: Enter the measurements from steps 1-3 into the cells in blue color below. The attitudes of the two vectors "A>B" and "A>C"

will appear below the heading "Vector Attitude"

STEP 5: Read the strike and dip of the plane containing apparent dips 1 & 2 at the lower right

of the spreadsheet. Answers appear in dark green color. Also calculated are the pole azimuth and plunge, the hydraulic flow

direction azimuth, and the gradient. The gradient horizontal vs. vertical scale conversion is controlled by the cell

right of the label "H/V conversion". Use 1000 for meters per kilometer, or 5280 for feet per mile gradient units

NOTE: Magenta and green cells contain formulae, therefore, they are by default "protected" so they are not accidentally corrupted from inadvertent typing

Also note that by default the cells below App. dip 1 & App. dip 2 receive the calculated vector attitudes. If you already have the apparent dip

attitudes you should over-type the formulae, however, make sure that you keep a copy of the original worksheet in the event

that you need to revert back to using elevation and distance measurements

## Accumulation Macro

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name "AccumulateMacro" as the macro to run

## Graphical Plot

The graphical diagram in the sheet "Map" displays a map view of the elements of the 3-point problem. The point

labelled "A", "B", and "C" correspond to the 3 control points in the problem. The line labelled "strike" indicates the

attitude of the strike line calculated by the algorithm. By default the X and Y axis are set to an "autoscale" the

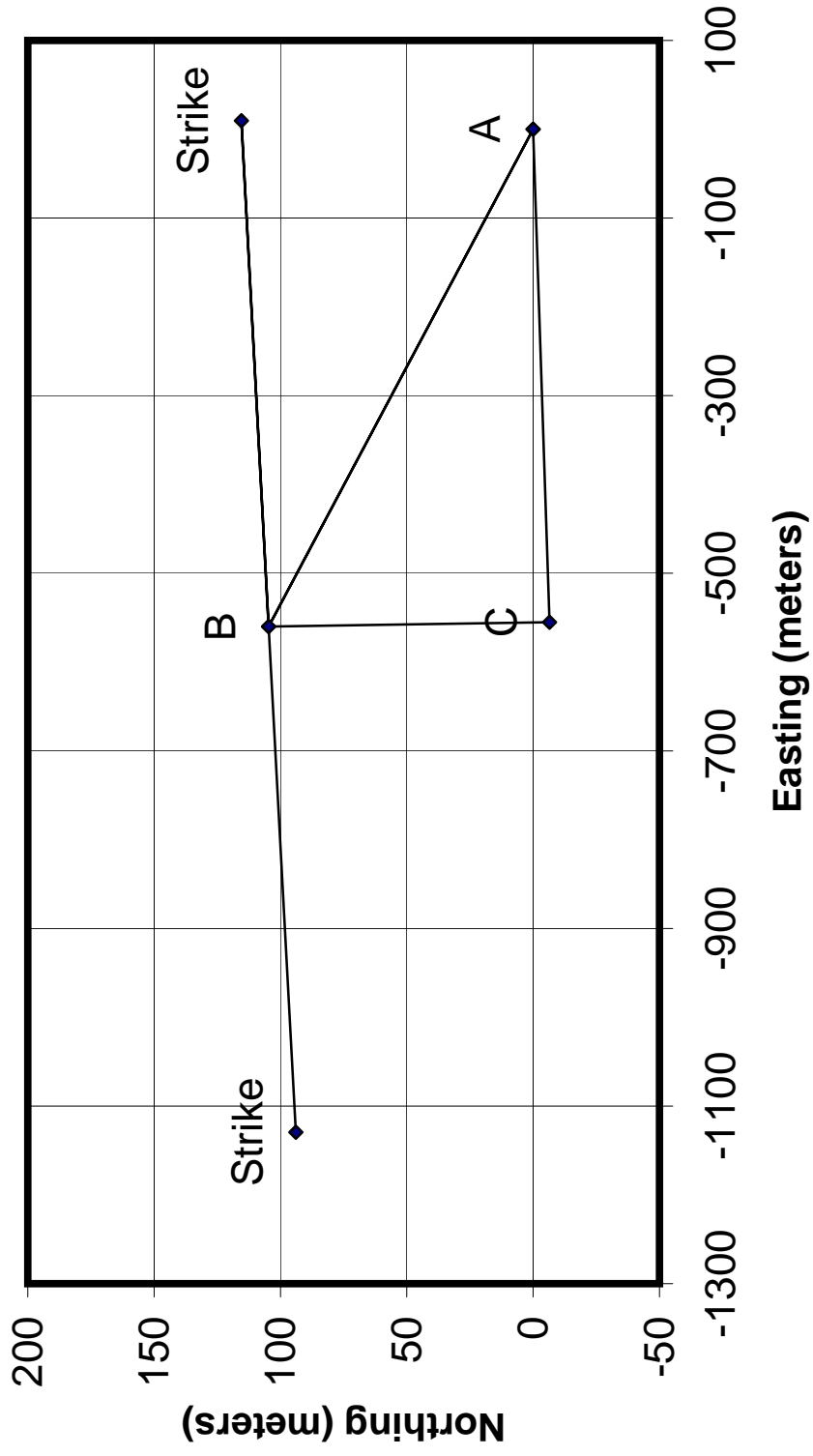
unfortunately will not generally set equivalent X and Y increments. After the elements of the problem are entered you

should edit the X and Y scale settings in "manual" mode so that the grid on the graph appears as a collection of

"squares" rather than rectangles. This means that the scaling is equivalent (or very close) on both axes, therefore

the graph is no longer distorted.

# Three Point Problem







**APPENDIX E**  
**GROUNDWATER DISCUSSION**

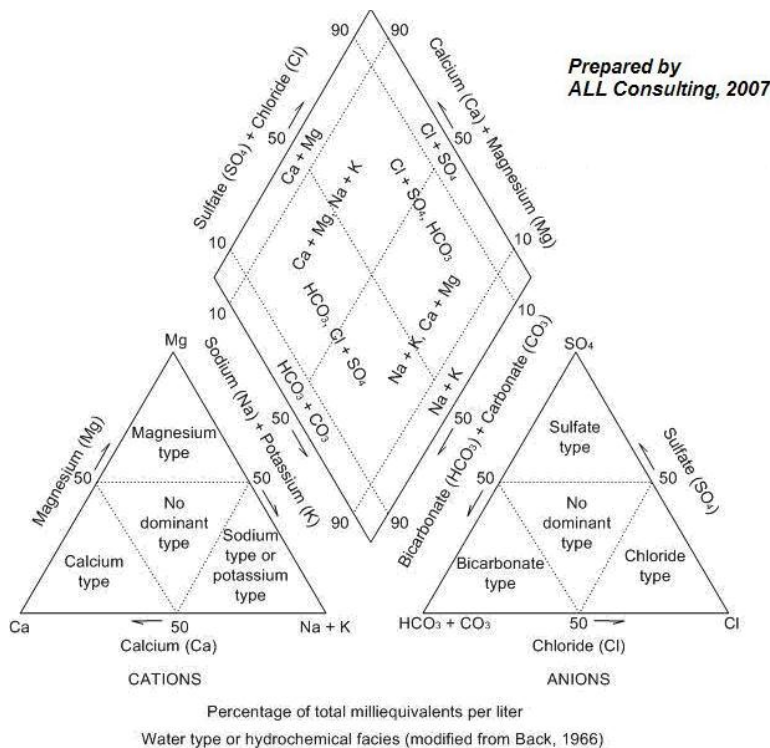
# Observed Impacts to Groundwater Resulting from the Operation of CBNG Impoundments

## ANALYSIS OF OBSERVED GROUNDWATER IMPACTS

Analysis of the groundwater chemistry of aquifers and of CBNG produced waters can be performed by evaluating posted analytical plots of a variety of chemical constituents present in the water. The analysis of total dissolved solids (TDS) and sodium adsorption ration (SAR) are commonly utilized to evaluate CBNG waters as a measure of suitability for agricultural uses including both livestock watering and for land application/irrigation. Other analysis performed to determine compliance with state required monitoring may focus on common and trace metals present in the waters for comparison to guidance levels. In terms of water origin analysis and evaluating water bedrock interactions, analysis is focused on the major dissolved ionic constituents including the cations of sodium, potassium, calcium, magnesium, and the anions of bicarbonate, chloride, sulfate, and carbonate.

Piper diagrams can be used to analyze the composition of most natural waters in the

**Figure 5-1: Generalized Piper Plot for Water Samples**



terms of the major cation and anion species (Hem, 1985). Figure 5-1 shows the basic layout of the Piper diagram separated into its respective water quality zones. For the groundwater analysis performed in this research, the geochemical analysis focused on evaluating water chemistry data

in terms of the major cation and anion data as depicted on a Piper diagrams as well as the evaluation of TDS and SAR data for the samples.

Piper diagrams have long been used to study water chemistry. The two triangles at the bottom of the diagrams correspond to cations and anions, with each vertex representing 100 percent of a particular ion or groups of ions. Water quality is established by the diamond shaped area in which the two points plotted in the triangles are projected into the diamond and are plotted as a single point. Figure 5-1 shows how water quality characteristics are separated into the components of the Piper diagram. Interpretations of water quality can be made from the single point projected into the diamond. The piper plots allow for a visual comparison and thus an analysis of the quality of two or more groundwater samples. The piper plot does not however provide analysis for changes in concentrations of the major ions, other analytical methods are used to assess changes in overall ionic concentration including TDS analysis and ion plots.

### **Analysis of Geochemical Data from Impoundments located over Alluvial Aquifers along the Powder River of Wyoming**

During the discussion of anticipated impacts associated with the infiltration of CBNG impoundment water one of the major conditions that was identified as influencing the changes in chemistry as the water infiltrates was the local geology. In an effort to in part account for this condition in this research the data analysis has been separated by aquifer type. This section presents the results of geochemical monitoring data gathered at infiltration impoundments which were sited and completed at locations over alluvial aquifers. The sites include the Jeff 3, Jeff 5, Jeff 6, Jeff 7, Arvada Phil's Pond, Arvada Cottonwood 8, Arvada Santiago, and Arvada Tietjen impoundments.

#### **Marathon Impoundment Jeff 3 – East Arvada**

CBNG produced water was initially discharged into the Jeff 3 impoundment after November 2001 and prior to January 2002. Before CBNG produced water was discharged into the impoundment, five monitoring wells were installed. The locations of these wells are shown in Figure 4-3. Background groundwater samples were collected in these well during July and November 2001 with samples from MW-1 collected in July and samples for MW-2, MW-3, MW-4, and MW-5 being collected in November. There

were twenty-eight sampling events at MW-1 and a total of twenty-six sampling events occurring for the other four monitoring wells. These water quality samples represent background water quality for the shallow alluvial aquifer prior to any CBNG produced water had been discharge to the impoundment. Analysis of major ion groundwater chemistry is depicted per sampling event for each monitoring well in Figure 5-2 (Appendix G). For comparison purposes, the quality of the CBNG produced water discharged into the impoundment is also presented on Figure 5-2.

Figure 5-2 shows that the data for the Jeff 3 MW-1 and MW-2 plots between the data for Jeff MW-3, MW-4 and MW-5 toward that of CBNG produced water quality. The groundwater samples for MW-1 and MW-2 wells indicate a trend from a water with a mixed calcium/sodium cations and sulfate anion dominance to a water with a more sodium/bicarbonate dominance. This trend can be seen more clearly when the samples from the individual monitoring wells are plotted, (See Figure 5-3 and Figure 5-4, Appendix G).

The data in Figure 5-2 shows that the initial background water quality sample for MW-1 (top black circle) collected in 2001 is representative of the natural water chemistry present in an alluvial aquifer with a sodium/sulfate dominant water. Figure 5-2 also shows the quality of CBNG produced water that was discharged into the impoundment (green square); the sample was collected in April 2002 and represents typical CBNG produced water that is typically a sodium/bicarbonate water. Additionally Figure 5-2 shows plots for several simple mixing increments in which 25%, 50%, and 75% groundwater is mixed with the corresponding percentage of CBNG produced water. Groundwater quality data from Jeff 3 MW-1 collected after the initial background sample show a migration of anions away from the background sulfate dominated waters to a more carbonate dominant water. The plot of cations for these data in Figure 5-2 shows a trend which migrates away from the mixed calcium/sodium background values to a sodium dominant water.

The data in Figure 5-3 shows that the water quality samples for MW-2 collected in 2001 and 2002 are representative of the water chemistry present in an alluvial aquifer with

sodium/sulfate dominant waters. Figure 5-3 also shows that the quality of the CBNG produced water that was discharged into the impoundment (green square) was a sodium/bicarbonate water. Additionally, Figure 5-3 shows plots for several simple mixing increments in which 25%, 50%, and 75% groundwater is mixed with the corresponding percentage of CBNG produced water. Groundwater quality data from Jeff 3 MW-2 collected after 2002 show a definite migration of anions away from the background sulfate dominated waters to a more carbonate dominant water. The plot of cations for these data in Figure 5-3 shows a trend which migrates from the mixed calcium/sodium background to sodium dominant water.

### ***Jeff 3 Monitoring Well #1 Mixing – Figures 5-4 through 5-6***

An evaluation of the time step sample data from the Jeff 3 MW-1 shows a mixing trend that beginning around October 2001 shifts the chemistry of the water away from the background water quality toward CBNG produced water quality. The transition mixing trend continues until around the August 2002 sampling event shown in yellow on Figure 5-4. Sampling events occurring after this date begin to reverse in direction away from the produced water quality.

Figure 5-5 shows the progression of water quality in MW-3 from January 2003 to the final sample taken in October 2004. Data collected in 2001 is also shown on the Figure 5-5 to illustrate the background water quality sampling results. The two plots (Figure 5-4 and Figure 5-5) appears to indicate that the mixing of infiltrated CBNG water with the native alluvial aquifer waters to be the factor causing the change in the MW-1 water quality samples over time.

Figure 5-6 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-1 over time. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. The TDS line shows a drop of more than 3,500 mg/L in total dissolved solids between the first two sampling events. The plot shows that the mixing of the infiltrating CBNG water decreases the TDS of the alluvial groundwater by nearly 80% nearly instantly, while there is nearly a 50% increase in the SAR of the alluvial water that is drawn out over several years. The groundwater data from the Jeff 3 MW-1 indicates



that CBNG produced water dominated the mixing that occurred within the alluvial aquifer near the Jeff 3 impoundment over the short term, but that the alluvial water quality started to recover in a relatively short time frame (<5 years).

Additional plots of the major cations and anions from the MW-1 samples are presented in Figures 5-7 and 5-8 (Appendix G). Figure 5-7 shows that sulfate and chloride decrease in a trend similar to that observed in the TDS concentrations. Sulfate decreased from more than 54 meq/L to a low of <5 meq/L over the duration of the sampling. The chloride concentrations over the same period decreased from 25 meq/L to a low of <2 meq/L. The smaller fluctuations that are observed in Figure 5-6 for TDS are also mimicked in the anion data for both sulfate and chloride. Conversely, the bicarbonate data shows an increase of approximately 50% occurs over the duration of sampling increasing from approximately 15 meq/L to more than 23 meq/L.

The concentrations of the three major cations (Calcium, Magnesium and Sodium) show a similar initial trend to that seen in TDS with a large decrease in all three ions (see Figure 5-8, Appendix G). Sodium decreased from 42 meq/L in the background sample to approximately 20 meq/L. Calcium decreased from 25 meq/L in the background sample to <5 meq/L, while the magnesium concentration decreased from 13.5 meq/L in the background sample to <3 meq/L. In each case there was some fluctuation in the concentration across the duration the sampling events (Figure 5-8). A comparison of the cation plots with the SAR data plotted in Figure 5-6 shows that the corresponding fluctuations in SAR are primarily a reflection of the changes in the sodium concentrations and fluctuations in sodium which occur over time. The increases in SAR seen during 2002 and 2003 are a result of decreases in calcium and magnesium while there are corresponding increases in sodium over the same time intervals (Figure 5-8, Appendix G). This data indicates that in addition to simple mixing of the existing alluvial groundwater and the infiltrating CBNG produced water, there appears to be an influx of fresh or meteoric water with sodium concentrations lower than the CBNG produced water.

### ***Jeff 3 Monitoring Well #2 Mixing***

An evaluation of the time step sample data from Jeff 3 MW-2 shows a mixing trend beginning around December 2001 which continues to shift the chemistry of the water away from the background level toward that of CBNG produced water quality. The transitional mixing trend continues until around the August 2002 sampling event shown in yellow on Figure 5-9. Figure 5-9 illustrates a mixing trend for MW-2 that does not become as dominant with respect to CBNG produced water with the water quality data staying above the 25% mixing point.

Figure 5-10 shows the progression of water quality samples from January 2003 to the final sample in October 2004. Data collected in 2001 is also shown in the plot to represent a background water quality value. The MW-2 sample data for this period show a similar mixing of infiltrated water with the alluvial aquifer as was seen at MW-1, however the MW-2 data shows the mixing to be less CBNG infiltrated water dominant and there is a more complete return of the groundwater chemistry toward background concentrations, see Figure 5-10. The groundwater data from the Jeff 3 MW-2 further illustrates that although mixing is occurring within the shallow groundwater the changes to water quality can return to background levels in a relatively short time frame (<5 years).

Figure 5-11 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-1 over time. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. A decrease in TDS of more than 1,000 mg/L occurs within the first year after the start of infiltration. The plot shows that the mixing of the infiltrating CBNG water decreases the TDS of the alluvial groundwater by more than 50% in a relatively short time frame, while the approximate 40% increase in the SAR of the alluvial water is drawn out over several years.

Additional plots of the major cations and anions from the MW-2 samples are presented in Figures 5-12 and 5-13 (Appendix G). Figure 5-12 shows that sulfate and chloride concentrations have a trend similar to that observed in the TDS concentrations. Sulfate decreased from more than 35 meq/L to a low of <10 meq/L then increased to more than

25 meq/L over the duration of the sampling. The chloride concentrations decreased from 12 meq/L to a low of <3 meq/L then increased to more than 8 meq/L over the duration of the sampling. The fluctuations that are observed in Figure 5-11 for TDS are also mimicked in the anion data for sulfate and chloride. Conversely, the bicarbonate data shows an increase of approximately 75% or 8 meq/L occurs over the duration of sampling increasing from approximately 11 meq/L to more than 18.5 meq/L.

Two of the three major cations (calcium, and magnesium) concentrations showed a similar initial trend to TDS with the large decrease in all three ions (Figure 5-13). Sodium decreased from 22.5 meq/L in the background sample to approximately 18 meq/L with some variation in calcium over the sample record. Calcium decreased from 15 meq/L in the background sample to <7 meq/L over the duration of the sampling events; there is some variation of approximately 3 to 4 meq/L after the April 2002 sampling events. Magnesium decreased from 10 meq/L in the background sample to <5 meq/L over the duration of the sampling events; there is some variation of approximately 2 to 3 meq/L. A comparison of the cation plots with the SAR data plotted in Figure 5-11 shows that the corresponding fluctuations in SAR are primarily a reflection of the changes in the sodium concentrations and the fluctuations in sodium which occur over time. This data indicates that in addition to simple mixing of the existing alluvial groundwater with infiltrating CBNG produced water, there also appears to be mixing of fresh or meteoric water with sodium concentrations lower than that of the CBNG produced water.

### ***Monitoring Wells #3, 4, & 5***

The three additional monitoring wells were installed and sampled at the Jeff 3 impoundment. None of these three monitoring wells show the same signs of mixing as was seen in MW-1 and MW-2. Sampling occurred at MW-3, MW-4, and MW-5 from 2001 to 2004 (Figure 5-14, 5-15, and 5-16). Review of the water quality for the wells MW-3 (Figure 5-14) and MW-5 (Figure 5-16) show little variation in the groundwater quality occurred over the course of the sampling events.

Data from MW-3 (Figure 5-14) is representative of a cross-gradient well which has not been influenced by the infiltrating impoundment water; the well is located cross-gradient

approximately 390 feet from the impoundment. Groundwater quality represented by MW-3 is representative of the groundwater in the alluvium bordering the Powder River and shows a sodium/potassium sulfate water.

Data from MW-4 (Figure 5-15) is representative of a cross-gradient well which appears to be on the margin of influence by the infiltrating impoundment water. The well is located cross-gradient approximately 380 feet from the impoundment.

Data from MW-5 (Figure 5-16) is representative of a background well which should not be influenced by the infiltrating impoundment water because it is located up-gradient approximately 550 feet from the impoundment. Background groundwater quality represented by MW-5 shows a sodium/potassium sulfate water.

Figure 5-17 is plot of the SAR and TDS values for monitoring wells MW-3, MW-4, and MW-5. Groundwater quality represented by MW-4 appears to show a marginal mixing (up to approximately 25% CBNG infiltrated water) representative of the groundwater in the alluvium on the margins of the infiltrating water plume but still shows a sodium/potassium sulfate water. Figure 5-17 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-3, MW-4, and MW-5 over time. A decrease in TDS of more than 2,400 mg/L occurs in the last year of sampling at MW-4. The TDS data for monitoring well MW-3 increases by as much as 1,700 mg/L during 2002 then decreases to the levels shown in 2001. The TDS data for MW-5 shows approximately 600 mg/L of total variation over the sampling period. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. The initial TDS values for MW-3, MW-4, and MW-5 are all greater than that of the CBNG water being discharged into the impoundment, therefore mixing of these two fluids should result in decreased TDS concentrations over time. Mixing of alluvial water and infiltrating water was indicated on the plots of data from MW-1 and MW-2, and showed decreases in TDS over time. The TDS data for MW-4 appears to show that mixing was occurring in the groundwater near this well in 2003 and 2004 as indicated by the approximate 50% decrease in TDS. The

SAR plots shown in Figure 5-17 for the three monitoring wells show little change occurs in the ratio of the three cations over the sampling interval.

Additional plots of the major cations and anions from the MW-3, MW-4, and MW-5 samples are presented in Figure 5-18 through 5-23 (Appendix G). The anion figures for each of the monitoring wells show that anion concentrations reflect similar trends to that observed in the TDS concentrations. Similarly, the fluctuations and changes in the TDS concentrations are also reflected in the cation plots presented in Appendix G.

### **Marathon Impoundment Jeff 5 – East Arvada**

CBNG produced water was originally discharged into the Marathon Jeff 5 impoundment after November 2001 and prior to January 2002. Background groundwater samples were collected in July 2001 for MW-1 and November 2001 for MW-2, MW-3, MW-4, and MW-5. Before discharge of produced water from the impoundment took place, five monitoring wells were installed as shown in Figure 5-24. Initial groundwater sampling events took place in July 2001 for MW-1 and November 2001 for MW-2, MW-3, MW-4, and MW-5. Thirteen sampling events occurred between 2001 and November 2004. Water quality samples collected in 2001 represent background water quality in the shallow alluvial aquifer prior to any produced water discharge. Analysis of major ion groundwater chemistry is depicted per sampling event for each monitoring well in Figure 5-24. For comparison purposes, the quality of the CBNG produced water discharged into the impoundment is also presented on Figure 5-24.

Figure 5-24 shows the data for the Jeff 5 MW-1 plots between the data for Jeff 5 MW-2, MW-3, MW-4 and MW-5 toward that of CBNG produced water quality. The groundwater samples for the MW-1 well indicate a trend from water with a mixed Calcium/Sodium cation, Sulfate anion dominance to water with no dominant cation or anion. This trend can be seen more clearly when the samples from the individual monitoring wells are plotted, as indicated in Figure 5-25.

### ***Monitoring Well # 1 Mixing***

An evaluation of the time step sample data from Jeff 5 MW-1 shows a mixing trend beginning around October 2001 which continues to shift the chemistry of the water away



from the background alluvial water quality toward CBNG produced water quality. The downward transition mixing trend continues until the October 2002 sampling event shown in yellow on Figure 5-26. Sampling events occurring after this date begin to reverse in direction away from the produced water quality. Figure 5-26 shows the beginning of the mixing trend in 2001 to water samples continuing the trend in 2002.

Figure 5-27 shows the progression of water quality from January 2003 to the final sample in October 2004. Data collected in 2001 is also shown on the Figure 5-27 to show the background water quality sampling results. The two plots (Figure 5-26 and Figure 5-27) appear to indicate the mixing of infiltrated CBNG water with the alluvial aquifer to be the factor causing the change in the MW-1 water quality samples. Figure 5-28 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-1 over time. The TDS line fluctuates over time varying as much as 1,000 mg/L over all the sampling events. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. The plot shows that the mixing of the infiltrating CBNG water decreases the TDS of the alluvial groundwater by as much as 25%, while there is more than a 200% increase in the SAR of the alluvial water. The groundwater data from the Jeff 5 MW-1 indicates that CBNG produced water mixing occurred within the alluvial aquifer with the Jeff 5 impoundment over the short term, but that the alluvial water quality has recovered to more than 75% groundwater in a relatively short time frame (<5 years).

Additional plots of the major cations and anions from the MW-1 samples are presented in Figures 5-30 and 5-31 (Appendix G). Figure 5-30 shows that the sulfate concentration fluctuates in a trend similar to that observed in the TDS concentrations. Sulfate decreased from approximately 25 meq/L to a low of 10 meq/L then increased to over 30 meq/L over the duration of the sampling. The chloride concentrations decreased slightly from 5 meq/L to a low of <2 meq/L then increased back to 5 meq/L over the duration of the sampling. Conversely, the bicarbonate data shows an increase of approximately 300% or 15 meq/L occurs over the duration of sampling with values increasing from approximately 5 meq/L to more than 20 meq/L before returning to approximately 10 meq/L at the last sampling event.

Two of the three major cations (Calcium and Magnesium) concentrations showed a similar initial trend to TDS with variations seen reflected in the plots for the two ions (Figure 5-31, Appendix G). Sodium increased from 13 meq/L in the background sample to approximately 25 meq/L before decreasing to 17 meq/L with some variation in sodium data over the sample record. Calcium started at 12 meq/L in the background sample and decreased to <8 meq/L before returning to 12 meq/L. Magnesium started at 5 meq/L in the background sample and decreased to <3 meq/L before returning to 5 meq/L over the duration of the sampling events there is some variation of approximately 2 meq/L. A comparison of the cation plots with the SAR data plotted in Figure 5-29 shows that the corresponding fluctuations in SAR are primarily a reflection of the changes in the sodium concentrations and the fluctuations in sodium which occur over time. The increases in SAR seen during 2002 and 2003 are a result of decreases in calcium and magnesium while there are corresponding increases in Sodium over the same time intervals (see plots in Appendix D). This data indicates that in addition to simple mixing of the existing alluvial groundwater and the infiltrating CBNG produced water, there also appears to be mixing of fresh or meteoric water with sodium concentrations lower than CBNG produced water.

### ***Monitoring Wells #2, 3, 4, & 5***

The four additional monitoring wells drilled at the Jeff 5 impoundment are MW-2 (Figure 5-32), MW-3 (Figure 5-33), MW-4 (Figure 5-34), and MW-5 (Figure 5-35), which were sampled between 2001 to 2004 in a manner similar to MW-1. The data from these four monitoring wells did not show signs of mixing between infiltrating CNNG produced water and alluvial groundwater. The data for each of the monitoring wells does show some variation from sample to sample, but the overall data seems to be indicative of a pattern with little migration in water character.

Figure 5-36 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-2, MW-3, MW-4, and MW-5 over time. A decrease in TDS of more than 1,200 mg/L occurs at MW-2, while the TDS data for monitoring well MW-3 shows increases by as much as 400 mg/L. The TDS data for both MW-4 and MW-5 shows approximately 500 mg/L of total variation over the sampling period. The

bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. The initial TDS values for MW-2, MW-3, MW-4, and MW-5 are all greater than that of the CBNG water being discharged into the impoundment, therefore mixing of these two fluids should result in decreased TDS concentrations over time. The TDS and SAR plots shown in Figure 5-36 for the four monitoring wells at the Jeff 5 impoundment show only minor changes in the water chemistry over the sampling interval, with less than one unit of SAR variation in three of the wells (MW-3, MW-4, and MW-5), and approximately two units of SAR variation in the other well.

Additional plots of the major cations and anions from the MW-2, MW-3, MW-4, and MW-5 samples are presented in Figures 5-37 through 5-44 (Appendix G). The anion figures for each of the monitoring wells show that anion concentrations reflect similar trends to that observed in the TDS concentrations. Similarly, the fluctuations and changes in the TDS concentrations are also reflected in the cation plots presented in Appendix G.

#### **Marathon Impoundment Jeff 6 – East Arvada**

CBNG produced water was originally discharged into the Marathon Jeff 6 impoundment after October 2001 and prior to January 2002. Background groundwater samples were collected in July 2001 for MW-1. The monitoring well Jeff 6 MW-1 was installed the previous summer in 2001, with the first groundwater sampling event occurring in July 2001. Groundwater monitoring data has been collected from Jeff 6 MW-1 from July 2001 to November 2004 with thirteen sampling events occurring over that timeframe. Water quality samples collected in 2001 represent background water quality in the shallow alluvial aquifer prior to any produced water discharge. Analysis of major ion groundwater chemistry is depicted per sampling event for each monitoring well in Figure 5-45. For comparison purposes, the quality of the CBNG produced water discharged into the impoundment is also presented on Figure 5-45.

Figure 5-45 shows the background water quality to represent a sodium/potassium sulfate water type. Figure 5-45 shows that the CBNG produced water (green square) that is

discharged into the impoundment is representative of sodium bicarbonate water. The data from Jeff 6 MW-1 presented in Figure 5-45 shows the change in shallow alluvial groundwater quality that occurred over the sampling interval. Figure 5-45 shows the mixing transition over time as the infiltrating CBNG water mixes with the shallow alluvium water. Figure 5-45 shows the anion migration from sulfate dominated waters in the background sample to a mixed sulfate/carbonate water type.

The downward mixing trend shown on Figure 5-46 occurs from July 2001 to May 2003; around the May 2003 sampling event, the trend appears to reverse as subsequent samples become more sulfate rich. Figure 5-47 shows the evolution of water quality from July 2003 to the date of the final sample in November 2004. The transition from July 2003 to November 2004 could be the result of decreasing infiltration or an influx of alluvial water. The groundwater data from the Jeff 6 MW-1 monitoring well shows that mixing was occurring within the shallow groundwater but the water quality started to recover in a relatively short time frame (<5 years).

Figure 5-48 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-1 over time. A decrease in TDS of more than 2000 mg/L occurs at MW-1 between July 2001 and January 2002. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. The TDS values for MW-1 from the January 2002 sample until sampling ended in 2004 are all within 500 mg/L of the CBNG water discharged to the impoundment; this low TDS concentration could be indicative of the mixing of two waters with CBNG water dominating the volume of water being mixed. The SAR plots shown in Figure 5-48 show a similar CBNG water dominance in the mixing as is reflected by the increased SAR values in the samples collected after January 2002.

Additional plots of the major cations and anions from the MW-1 samples are presented in Figure 5-49 and 5-50 (Appendix D). Figure 5-49 shows that sulfate exhibits a trend similar to that observed in the TDS concentrations. Sulfate levels decreased from a high of approximately 57 meq/L to a low of 8 meq/L then fluctuated around 5 meq/L over the duration of the sampling. The chloride concentrations seemed to be constant at about 1

meq/L with less than 0.5 meq/L of variation over the duration of the sampling. Conversely, the bicarbonate data shows an increase of approximately 200% or 13 meq/L occurs over the duration of sampling increasing from approximately 6 meq/L to approximately 20 meq/L before returning to approximately 18 meq/L at the last sampling event.

The three major cations (Calcium, Magnesium, and Sodium) concentrations showed an initial trend similar to TDS with variations reflected in the plots for the two ions (Figure 5-50, Appendix G). Sodium decreased from 33 meq/L in the background sample to approximately 20 meq/L before increasing to 22 meq/L with some fluctuation in sodium data over the sample record. Calcium started at 12 meq/L in the background sample and decreased to < 3 meq/L with minor fluctuation of approximately 1 meq/L for the remainder of the sampling events. Magnesium started at 8 meq/L in the background sample and decreased to <3 meq/L; for the duration of the sampling events there is some variation of approximately 0.5 meq/L. A comparison of the cation plots with the SAR data plotted in Figure 5-48 shows that the corresponding fluctuations in SAR are primarily a reflection of the changes in the sodium concentrations and the fluctuations in sodium which occur over time. The increases in SAR seen during 2002 and 2003 appear to result from decreases in calcium and magnesium while there are corresponding increases in sodium over the same time intervals (Appendix G). This data indicates that in addition to simple mixing of the existing alluvial groundwater and the infiltrating CBNG produced water, there also appears to be mixing of fresh or meteoric water with sodium concentrations lower than CBNG produced water.

#### **Marathon Impoundment Jeff 7 – East Arvada**

CBNG produced water was originally discharged into the Marathon Jeff 7 impoundment between November 2001 and January 2002. Before discharge of produced water from the impoundment took place, four monitoring wells were installed (see Figure 4-3). Initial groundwater sampling events took place in July 2001 for MW-1 and November 2001 for MW-2 with a total of twenty-seven sampling events and during November 2001 for MW-3, and MW-4, with twenty-six sampling events occurring. Water quality samples collected in 2001 represent background water quality for the shallow alluvial



aquifer prior to any produced water discharge. The Piper diagram shown in Figure 5-51 exhibits sampling results for each of the monitoring wells and the CBNG produced water discharged into the impoundment.

The data for the Jeff 7 MW-4, plotted on Figure 5-52, shows the start of a mixing trend toward that of CBNG produced water quality similar to trends seen in previously discussed impoundments. The data shows that background water quality samples (black circles) were collected in 2001 and represent the water quality of alluvial groundwater. The groundwater data shows background groundwater quality to be representative of sodium/potassium sulfate water. Sampling of the CBNG produced water quality (green square) occurred in April 2002 and is a sodium bicarbonate water type. Migration of anions of the background sulfate dominance to a water with a more sodium/bicarbonate dominance is apparent in Figure 5-52. This trend can be seen more clearly when the samples from MW-4 are plotted separately, see Figure 5-53 and 5-54. Figure 5-52 also shows several simple mixing increments in which 25%, 50%, and 75% groundwater is mixed with the corresponding percentage of CBNG produced water. Samples of groundwater from Jeff 7 MW-4 collected after the initial background sample show a migration of anions away from the background sulfate dominated waters to a more carbonate dominant water. The plot also shows a migration trend of cations away from the mixed calcium/sodium background toward a sodium water.

#### ***Monitoring Well #4 Mixing***

An evaluation of the time step sample data from Jeff 7 MW-4 shows a mixing trend beginning around October 2001 which continues to shift the chemistry of the water away from the background alluvial water quality toward CBNG produced water quality. Figure 5-54 shows the beginning of the mixing trend in 2003 with water samples continuing the trend through the last sampling event in 2004. Figure 5-55 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples collected from MW-4 over time. The TDS line shows little migration from November 2001 until the June 2003 the sampling event. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the

impoundment. The plot shows that the mixing of the infiltrating CBNG water decreases the TDS of the alluvial groundwater by as much as 50%.

Additional plots of the major cations and anions from the MW-4 samples are presented in Figures 5-56 and 5-57 (Appendix G). Figure 5-56 shows that the sulfate concentrations trend in the same observed pattern as the TDS concentrations. Sulfate levels decreased from approximately 55 meq/L to a low of 20 meq/L over the duration of the sampling. The chloride concentrations seemed to be similar to sulfate but at a reduced scale over the duration of the sampling. Conversely, the bicarbonate data shows an increase of approximately 100% or 10 meq/L occurs over the duration of sampling increasing from approximately 11 meq/L to approximately 21 meq/L at the last sampling event.

The three major cations (Calcium, Magnesium, and Sodium) concentrations showed a similar initial trend to TDS with variations seen in the plots for the three ions (Figure 5-57, Appendix G). Sodium levels decreased from 33 meq/L in the background sample to approximately 22 meq/L with fluctuation in sodium data over the sample record. Calcium concentrations started at 27 meq/L in the background sample and decreased to 13 meq/L with fluctuations of approximately 4 meq/L over the course of the sample record. The initial Magnesium concentration was at 15 meq/L in the background sample and decreased to <8 meq/L, during the duration of the sampling events with some variation of approximately 1.5 meq/L. A comparison of the cation plot (Figure 5-57) with the SAR data plotted in Figure 5-55 shows the corresponding fluctuations in cation concentrations are also displayed in the SAR plot. The fluctuations seen in SAR's data points during the duration of the sampling rounds are corresponding to changes seen in all three cations over the same time intervals.

### ***Jeff 7 MW-1, MW-2, and MW-3***

The three additional monitoring wells drilled at the Jeff 7 impoundment did not show signs of mixing. Sampling for MW-1, MW-2, and MW-3 occurred from 2001 to 2004, and was similar to that for MW-4 (Figures 5-58, 5-59, and 5-60). Water quality for the three remaining wells did not present the same downward trend which could mean infiltrating water from the impoundment has not migrated laterally into the alluvial aquifer. Data shows background groundwater quality to represent sodium/potassium

sulfate water. Data collected in the subsequent years did not show the infiltrating impoundment CBNG produced water to be affecting groundwater in any significant way, as can be seen by the grouping of the data for these wells on the appropriate Piper diagram. Figures 5-58, 5-59, and 5-60 show the Piper diagrams for the Jeff 7 MW-1, MW-2 and MW-3, respectively.

Figure 5-61 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-1, MW-2, and MW-3 over time. The TDS data for MW-1 shows approximately 700 mg/L of total variation over the sampling period. A decrease in TDS of more than 1,200 mg/L occurs at MW-2. The TDS data for monitoring well MW-3 increases by as much as 1,200 mg/L. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. The initial TDS values for MW-1, MW-2, and MW-3 were all greater than that of the CBNG water being discharged into the impoundment, therefore mixing of these two fluids should result in decreased TDS concentrations over time. The TDS and SAR plots presented in Figure 5-61 for the three monitoring wells at the Jeff 7 impoundment show minor changes in the water chemistry occurred over the sampling interval. The plot shows there was less than two units of SAR variation at the three monitoring wells (MW-1, MW-2, and MW-3).

Additional plots of the major cations and anions from the MW-1, MW-2, and MW-3 samples are presented in Figures 5-62 through 5-67 (Appendix G). The anion figures for each of the monitoring wells show that anion concentrations reflect similar trends to that observed in the TDS concentrations. Similarly, the fluctuations and changes in the SAR concentrations are also reflected in the cation plots presented in Appendix G.

#### **Marathon Impoundment Phil's Pond – West Arvada**

CBNG produced water was originally discharged into the Marathon Phil's Pond impoundment after November 2001 and prior to January 2002. Before CBNG produced water was discharged into the impoundment, one groundwater monitoring well was installed. Background groundwater samples were collected in April 2001 and October 2001. Water quality samples collected in 2001 represent background water quality in the

shallow alluvial aquifer prior to any produced water discharge. Samples of the monitoring well were taken from April 2001 to November 2004, with a total of fifteen sampling events. The Piper diagram showing sampling events for each well and the CBNG produced water discharged into the impoundment is shown in Figure 5-68.

### ***Monitoring Well #1 Mixing***

An evaluation of the time step sample data from Phil's Pond MW-1 shows a mixing trend beginning around December 2001 which continues to shift the chemistry of the water away from the background water quality toward that of CBNG produced water quality. As shown on Figure 5-68 the transition mixing trend continues for the entire sampling record. This plot also shows that the mixing trend at MW-1 does not become as CBNG produced water dominant as some of the previously analyzed impoundments, with the sample data staying above the 50% mixing point. The mixing trend is not as readily apparent in the early years of discharge to the impoundment in comparison to the data from the other impoundments such as the Jeff 3 or Jeff 6 data. Figure 5-69 shows the 2001-2002 data for MW-1, with a trend which appears to be reflective of the scatter seen on some of the background wells. A slight shift away from the dominant sulfate to bicarbonate anion can be observed from the diagram. However, the geochemical change shown in Figure 5-69 does not appear to reflect mixing with a water of a different chemical signature such as that reflected in the CBNG produced water data point. It is not until the data from the 2003-2004 sampling events is plotted and reviewed, Figure 5-70, that the mixing trend in the alluvial water under Phil's Pond is apparent. The Phil's Pond data does not appear to show the end point of the mixing timeline, additional sampling would be needed to determine if additional mixing is occurring or if the alluvial groundwater will return to its background chemistry. Based on the data collected for the Phil's Pond MW-1, it is not possible to determine if the aquifer would recover to background quality in a relatively short time frame (<5 years), as has been observed for the other impoundments in the area.

Figure 5-71 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-1 over time. The TDS data plotted shows a 1,600 mg/L decrease over the duration of the sampling events. The bottom boundary line on the plot

represents the TDS concentration of the CBNG water that was discharged into the impoundment. The plot shows that the mixing of the infiltrating CBNG water decreases the TDS and increases the SAR of the alluvial groundwater.

Additional plots of the major cations and anions from the MW-1 samples are presented in Figures 5-72 and 5-73 (Appendix G). Figure 5-72 shows that sulfate concentration trends dominate the observed pattern seen in the TDS concentrations. Sulfate levels decreased from approximately 55 meq/L to a low of 20 meq/L over the duration of the sampling. The chloride concentrations seemed to be relatively consistent at approximately 1 meq/L over the duration of the sampling. Conversely, the bicarbonate data shows an increase of approximately 100% or 9 meq/L occurs over the duration of sampling increasing from approximately 9 meq/L to approximately 18 meq/L at the last sampling event.

The three major cations (Calcium, Magnesium, and Sodium) concentrations showed a similar initial trend then diverged in 2002 with variations seen in the plots for the three ions (Figure 5-73, Appendix G). Sodium increased from 23 meq/L in the background sample to approximately 29 meq/L with fluctuation in sodium data over the sample record. Calcium concentrations started at 25.5 meq/L in the background sample and decreased to 19 meq/L with fluctuations of approximately 5 meq/L over the course of the sample record. The initial magnesium concentration was 24 meq/L in the background sample and decreased to 17 meq/L during the duration of the sampling events with some variation of approximately 5 meq/L. A comparison of the cation plots with the SAR data plotted in Figure 5-71 shows the corresponding fluctuations and changes in the sodium concentrations are reflected in the SAR's data. The increases seen in SAR during the duration of the sampling rounds are corresponding to changes seen in all three cations over the same time intervals (see plots in Appendix G).

### **Marathon Impoundment Candida 2 – West Arvada**

CBNG produced water was initially discharged into the Candida 2 impoundment after June 2001 and prior to October 2001. Before CBNG produced water was discharged into the impoundment, one monitoring well was installed. Background groundwater samples were collected in April and June 2001 for MW-1. There were a total of 15 sampling



events at MW-1. The water quality samples collected in 2001 represent background water quality for the shallow alluvial aquifer prior to any CBNG produced water being discharge. Analysis of major ion groundwater chemistry is depicted per sampling event for each monitoring well at the Candida 2 site in Figure 5-74. For comparison purposes, the water chemistry of the CBNG produced water discharged into the impoundment is also presented on Figure 5-74.

### ***Monitoring Well #1 Mixing***

An evaluation of the time step sample data from Candida 2 MW-1 shows a mixing trend beginning in early 2001 which resulted in a shifting of the chemistry of the water away from that of background groundwater quality toward the quality of the CBNG produced water discharged into the impoundment. The mixing trend appears to continue for the entire sampling record, see Figure 5-74. Figure 5-75 shows that the mixing trend at MW-1 is nearly 50% CBNG produced water by the October 2001 sampling event, the first sample after produced water was discharged to the impoundment. The 2001-2002 data for MW-1 shows the mixing transition from 50% to approximately 75% CBNG water chemistry. Figure 5-76 reflects the further migration toward CBNG infiltration water chemistry with greater than 80% CBNG water chemistry present in the 2004 samples.

The Candida 2 data does not appear to show the end point of the mixing timeline. Additional sampling would be needed to determine if additional mixing is occurring or if the alluvial groundwater will return to its background chemistry. Based on the data collected for the Candida 2 MW-1, it is not possible to determine if the aquifer would recover to background quality in a relatively short time frame (<5 years), as has been observed for the other impoundments in the area.

Figure 5-77 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-1 over time. The TDS data plotted shows a 2,000 mg/L decrease over the duration of the sampling events, with TDS levels below the level of the CBNG water discharged into the impoundment during two of the sampling events. The 1,810 mg/L plotted on the chart that represents the TDS concentration of the CBNG water that was discharged into the impoundment. The plot shows that the mixing of the infiltrating CBNG water decreases the TDS. The SAR data plotted on Figure 5-77 shows

that the mixing of the CBNG water resulted in a 100% increase of SAR values for the alluvial groundwater.

Additional plots of the major cations and anions from the MW-1 samples are presented in Figures 5-78 and 5-79 (Appendix G). Figure 5-78 shows that sulfate concentration trends dominate the observed pattern seen in the TDS concentrations. Sulfate levels decreased from approximately 39 meq/L to a low of <5 meq/L over the duration of the sampling. The chloride concentrations seemed to decrease from approximately 9 meq/L to less than 2 meq/L over the duration of the sampling. Conversely, the bicarbonate data shows an increase of approximately 300% or 19 meq/L occurs over the duration of sampling increasing from approximately 7 meq/L to approximately 26 meq/L at the last sampling event. There appears to be some mixing with meteoric water as the TDS concentrations of the mixed waters decrease below TDS concentrations for CBNG produced water in 2004.

The combined trends of the three major cations (Calcium, Magnesium, and Sodium) concentrations can be seen in the TDS data (Figure 5-79, Appendix G). Sodium fluctuated from 18 meq/L to approximately 33 meq/L with fluctuations in sodium data over the sample record trending in a similar pattern to TDS. Calcium concentrations started at 17 meq/L in the background sample and decreased to 5 meq/L with fluctuations of approximately 0.5 meq/L over the course of the sample record. The initial Magnesium concentration was at 8 meq/L in the background sample and decreased to 3 meq/L for the duration of the sampling events with some variations of approximately 0.5 meq/L. A comparison of the cation plots with the SAR data plotted in Figure 5-77 shows the corresponding fluctuations in the sodium concentrations are reflected in the SAR's data. The increases and decreases seen in SAR during the duration of the sampling rounds correspond to changes seen in all three cations over the same time intervals (see plots in Appendix G).

### **Marathon Impoundment Santiago 3 – West Arvada**

CBNG produced water was initially discharged into the Santiago 3 impoundment after June 2001 and prior to October 2001. Before CBNG produced water was discharged into

the impoundment, one monitoring well was installed. As shown in Figure 5-80 background groundwater samples were collected in April and June 2001 for MW-1. There were a total of 15 sampling events at MW-1. The water quality samples collected in 2001 represent background water quality for the shallow alluvial aquifer prior to any CBNG produced water being discharge. Analysis of major ion groundwater chemistry is depicted per sampling event for each monitoring well in Figure 5-80. For comparison purposes, the water chemistry of the CBNG produced water discharged into the impoundment is also presented on Figure 5-80.

### ***Monitoring Well #1 Mixing***

An evaluation of the time step sample data from Santiago 3 MW-1 shows a mixing trend beginning in early 2001 which resulted in a shifting of the chemistry of the water away from that of background water quality toward the quality of the CBNG produced water discharged into the impoundment. The mixing trend appears to continue into 2003, see Figure 5-81. Figure 5-81 shows that the mixing trend at MW-1 is less than 75% alluvial water by the October 2001 sampling event, the first sample taken after produced water was discharged to the impoundment. Figure 5-81 also shows the 2001-2002 data for MW-1, which shows the mixing transition from 75% alluvial water to approximately 50% alluvial water chemistry. Figure 5-82 reflects the further migration toward the CBNG infiltration water chemistry with less than 25% alluvial water chemistry present in the July 2003 sample. The data in Figure 5-82 does show the start of the recovery of the alluvial water beginning with the late 2003 and 2004 data. In these sampling events the water chemistry is observed to be changing from less than 25% alluvial water to more than 50% alluvial water by the time of the last sample.

Figure 5-83 shows the changes that occur to the TDS and SAR concentrations in the groundwater samples from MW-1 over time. The TDS data plotted shows a 3,000 mg/L decrease over the duration of the sampling events. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. The plot shows that the mixing of the infiltrating CBNG water decreased the TDS. The SAR data plotted on Figure 5-83 shows that the mixing of the CBNG water resulted in a 3 unit increase of SAR in the alluvial groundwater.

Additional plots of the major cations and anions from the MW-1 samples are presented in Figures 5-84 and 5-85 (Appendix G). Figure 5-84 shows that sulfate concentration trends dominate the observed pattern seen in the TDS concentrations. Sulfate level decreased from approximately 78 meq/L to a low of 14 meq/L before increasing to 38 meq/L at the final sampling event. The chloride concentrations decreased from approximately 4 meq/L to less than 2 meq/L over the duration of the sampling. Conversely, the bicarbonate data shows an increase of approximately 200% or 17 meq/L occurs over the duration of sampling increasing from approximately 12 meq/L to approximately 29 meq/L at the last sampling event.

The combined trends of the three major cations (Calcium, Magnesium, and Sodium) concentrations can be seen in the TDS data (Figure 5-85, Appendix G). Sodium fluctuated from 33 meq/L to approximately 27 meq/L with fluctuations in sodium data over the sample record trending in a similar pattern to TDS. Calcium concentrations started at 22 meq/L in the background sample and decreased to 8 meq/L with fluctuations over the course of the sample record. Magnesium concentrations started at 27 meq/L in the background sample and decreased to 7 meq/L for the duration of the sampling events with some variation in concentrations. A comparison of the cation plots with the SAR's data plotted in Figure 5-83 shows the corresponding fluctuations in the sodium concentrations are reflected in the SAR data. The increases and decreases seen in SAR during the duration of the sampling rounds correspond to changes seen in all three cations over the same time intervals (see plots in Appendix G).

### **Marathon Impoundment Cottonwood 8 – West Arvada**

CBNG produced water was initially discharged into the Cottonwood 8 impoundment after June 2001 and prior to October 2001. Before CBNG produced water was discharged into the impoundment, one monitoring well was installed as shown in Figure 5-86. Background groundwater samples were collected in April and June 2001 for MW-1. There were a total of fourteen sampling events at MW-1. The water quality samples collected in 2001 represent background water quality for the shallow alluvial aquifer prior to any CBNG produced water being discharge. Analysis of major ion groundwater chemistry is depicted per sampling event for each monitoring well in Figure 5-86. For

comparison purposes, the water chemistry of the CBNG produced water discharged into the impoundment is also presented on Figure 5-86.

Figure 5-87 shows the TDS and SAR concentrations in the groundwater samples from MW-1 over time. The TDS data plotted shows a 900 mg/L decrease over the duration of the sampling events. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. The plot does not show evidence of mixing of infiltrating CBNG water in the TDS data. The SAR data plotted on Figure 5-87 shows only a 1.5 unit variation in SAR in the alluvial groundwater over the sample events.

Additional plots of the major cations and anions from the MW-1 samples are presented in Figure 5-88 and 5-89 (Appendix G). Figure shows that sulfate concentration trends dominate the observed pattern seen in the TDS concentrations. Sulfate decreased from approximately 95 meq/L to a low of 84 meq/L before increasing to 88 meq/L at the final sampling event. The chloride concentrations decreased from approximately 4 meq/L to less than 2 meq/L over the duration of the sampling. Conversely, the bicarbonate data shows a constant concentration of approximately 8 meq/L over the duration of the sampling.

The combined trends of the three major cations (Calcium, Magnesium, and Sodium) concentrations can be seen in the TDS data (Figure 5-89, Appendix G). Sodium fluctuated from 33 meq/L to approximately 42 meq/L. Calcium began at 22 meq/L in the background sample and fluctuated around 20 meq/L over the course of the sample record. Magnesium started at 30 meq/L in the background sample and fluctuated around 30 meq/L over the course of the sample record. A comparison of the cation plots with the SAR's data plotted in Figure 5-87 shows the corresponding fluctuations in the sodium concentrations were not reflected in the SAR data (see plots in Appendix G).

### **Marathon Impoundment Tietjen – West Arvada**

CBNG produced water was initially discharged into the Tietjen impoundment after June 2001 and prior to October 2001. Before CBNG produced water was discharged into the impoundment, two monitoring wells were installed as shown in Figure 4-3. Background

groundwater samples were collected in April and June 2001 for MW-1 and MW-2. There were a total of sixteen sampling events at MW-1 and MW-2. The water quality samples collected in 2001 represent background water quality for the shallow alluvial aquifer prior to any CBNG produced water having been discharge. Analysis of major ion groundwater chemistry is depicted per sampling event for each monitoring well in Figure 5-90 and 5-91. For comparison purposes, the quality of the CBNG produced water discharged into the impoundment is also presented on Figure 5-90 and 5-91.

### ***Tietjen MW-1, and MW-2***

The two monitoring wells drilled at the Tietjen impoundment did not show signs of mixing. Sampling for MW-1 and MW-2 occurred from April 2001 to November 2004. Water quality for the two wells did not present the mixing trend which has been seen at other alluvial impoundments; this could mean infiltrating water from the impoundment has not migrated laterally into the alluvial aquifer near these wells. Data shows background groundwater quality to represent sodium/potassium sulfate water. As can be seen by the grouping of data points on Figures 5-90 and 5-91 data collected in the subsequent years did not show that CBNG produced water infiltrating from this impoundment had affected groundwater in any significant way.

Figure 5-92 shows the TDS and SAR concentrations in the groundwater samples from MW-1 and MW-2 over time. The TDS data plotted shows a 5,000 mg/L increase over the duration of the sampling events for MW-1. The bottom boundary line on the plot represents the TDS concentration of the CBNG water that was discharged into the impoundment. The plot does not show evidence of mixing of infiltrating CBNG water in the TDS data; MW-1 shows a trend opposite what would be expected of simple mixing between the two waters. The SAR data plotted on Figure 5-92 mirrors the increase in TDS that is seen over the record of sampling events. The increase in SAR is the result of a 125% increase in Sodium between the first sampling event (896 mg/L) and the final sample (2,040). The increase in SAR does not reflect the complete increase in Sodium as there was also an 85% increase Magnesium noted between the first sampling event (336 mg/L) and the final sample (622 mg/L). There was also a 50% increase in both Sulfate,



which increased from 4,060 mg/L to 6,790 mg/L, and in Bicarbonate which saw an increase from 506 mg/L to 762 mg/L.

Figure 5-92 also presents the sampling results from Tietjen MW-2. The MW-2 sample data shows only minor variation over the duration of the sampling event. The TDS data from MW-2 varies by 800 mg/L and shows a steady rise over the duration of the sampling interval. A similar trend can be seen in the SAR data for the same period with a total of 1.4 units of variation between all of the samples, see Figure 5-92.

### **Analysis of Geochemistry Data from Impoundments over Non-Alluvial Aquifers along the Powder River of Wyoming**

During the discussion of anticipated impacts associated with the infiltration of CBNG impoundment water one of the major conditions that were identified as influencing the changes in chemistry as the water infiltrates was the local geology. This section presents the results of monitoring chemical data for impoundments which were completed over non-alluvial aquifers. The lithologic composition of the materials present below these impoundments is described in the geology discussion in Section 4.3 of this document.

#### **JM Huber Impoundment Lori – Prairie Dog Creek**

CBNG produced water was initially discharged into the Lori impoundment in 2001. Since CBNG produced water was discharged into the impoundment, four monitoring wells were installed. Groundwater chemistry, as shown in the piper diagram in Figure 5-93, shows the Lori PD#1, Lori MW-1, and Lori MW-4 waters to be characterized as sodium/sulfate waters. The groundwater sample from the Lori MW-3 is characterized as sodium/carbonate and bicarbonate water. Water chemistry representing average CBNG produced water quality is also plotted in Figure 5-93 for comparison, and is characterized as having a predominant sodium/carbonate and bicarbonate chemical signature. Groundwater was encountered in the Lori MW-3 in a coal stringer formation at an approximate elevation of 3,504.4 feet amsl. Groundwater collected from Lori MW-4 was interpreted to be from the same coal stringer, where it was encountered at an approximate elevation of 3,515.6 amsl. The proximal distance and structural similarities between the subsurface materials in the boreholes of MW-3 and MW-4 would indicate these two wells are producing water from a similar water bearing zone while chemical analysis

shows these two wells to have differing chemistries. Based on the simple mixing data shown on Figure 5-93 and the geographic location of PD-1, MW-3 and MW-4 it is possible that the chemistry of the water in coal stringer aquifer screened in MW-3 and MW-4 is being altered by infiltration of CBNG water from the Lori impoundment. Lori PD-1 and MW-1 contained groundwater originating in a siltstone aquifer. Lori MW-3 and MW-4 contained groundwater originating a coal stringer aquifer.

Figure 5-94 presents the major cation and anion composition of the wells installed near the Lori impoundment on a stiff diagram. A comparison of the major cation and anion chemistry shown on the stiff diagram in Figure 5-94 to the general formation quality data shown in Figure 2-5 shows the influence of CBNG infiltration water at Lori MW-3. The migration/influence of the CBNG infiltration water for the sodium and magnesium/sulfate water in Lori PD-1, to the sodium/bicarbonate water of Lori MW-3 and MW-4 is also apparent on Figure 5-94.

### **JM Huber Impoundment Sandy – Prairie Dog Creek**

CBNG produced water was initially discharged into the Sandy impoundment in 2001. Since CBNG produced water was discharged into the impoundment, three monitoring wells were installed. Groundwater chemistry, as shown in the Piper diagram in Figure 5-95, shows the Sandy MW-1 and Sandy MW-2 waters to be characterized as sodium/sulfate waters, and water samples from the Sandy MW-3 to be characterized as calcium and sodium/sulfate water. Water chemistry representing average CBNG produced water quality is also plotted in Figure 5-95 for comparison, and is characterized as having a predominant sodium/carbonate and bicarbonate chemical signature. Groundwater was encountered in the Sandy MW-1 and MW-2 in Upper Roland Coal aquifer. Groundwater collected from Sandy MW-3 was interpreted to be from shallow alluvial zone and was encountered at an elevation of 3,614 ft amsl. The alluvial aquifer sampled in MW-3, however, contained water enriched in calcium and magnesium, suggesting an influence from gypsum within that particular alluvium. The water chemistry analysis indicates that none of these monitoring wells are positioned structurally down-gradient from the impoundment or are not being influenced by infiltrating CBNG water.

Figure 5-96 presents the major cation and anion composition of the wells installed near the Sandy impoundment on a stiff diagram. A comparison of the major cation and anion chemistry shown on the stiff diagram in Figure 5-96 to the general formation quality data shown in Figure 2-5 shows that none the wells exhibit water of similar to the average CBNG water quality observed elsewhere in the PRB. Figure 5-96 appears to show the lack of influence of the CBNG infiltration water for the sodium and magnesium/sulfate water in Lori PD-1, to the sodium/bicarbonate water of Lori MW-3 and MW-4.

### **JM Huber Impoundment Joe Draw Jr. – Prairie Dog Creek**

CBNG produced water was initially discharged into the Joe Draw Jr. impoundment in 2000. Since CBNG produced water was discharged into the impoundment, three monitoring wells were installed. Groundwater chemistry, as shown in the Piper diagram in Figure 5-97, shows the Joe Draw Jr. MW-1, MW-2, and MW-3 waters to be characterized sodium/bicarbonate water. Water chemistry representing average CBNG produced water quality is also plotted in Figure 5-97 for comparison, and is characterized as having a predominant sodium/bicarbonate chemical signature. Groundwater that was encountered in the three Joe Draw Jr. monitor wells plots very closely to that of CBNG produced water on the Piper Diagrams. The water chemistry analysis appears to indicate that the three Joe Draw Jr. monitoring wells are all affected by CBNG infiltration, or are completed in an aquifer of similar quality to that of CBNG produced water. The lack of returns during the drilling of these three boreholes makes the interpretation of the geologic nature of the water producing formation more difficult, however, based on the returns that were seen, it appears to be a siltstone between two coal seams.

Figure 5-98 presents the major cation and anion composition of the wells installed near the Joe Draw Jr. impoundment plotted on a stiff diagram. A comparison of the major cation and anion chemistry shown on the stiff diagram in Figure 5-98 to the general formation quality data shown in Figure 2-5 shows that none the wells exhibit water of a quality similar to average CBNG produced water in the PRB.

**Yates Impoundment Yates State – LX Bar Creek**

CBNG produced water was initially discharged into the Yates State impoundment in 2001. Since CBNG produced water was discharged into the impoundment, two monitoring wells were installed. Groundwater chemistry, as shown in the Piper diagram in Figure 5-99, shows the water samples from the Yates State MW-1 to be characterized as calcium, magnesium/sulfate waters and while waters from MW-2 to be characterized as calcium, magnesium, sodium/bicarbonate water. Water chemistry representing average CBNG produced water quality is also plotted in Figure 5-99 for comparison, and is characterized as having a predominant sodium/bicarbonate chemical signature. The MW-1 well is screened in a sandy silt. MW-2 is screened in the Anderson Coal seam aquifer. The MW-2 sample is comparatively rich in sodium and bicarbonate while the MW-1 sample is richer in calcium, magnesium, and sulfate. It is unclear whether the difference in water chemistry is caused by the difference in lithology of the aquifers or infiltration from the impoundment.

The stiff diagram shown in Figure 5-100 presents the major cation and anion composition of the wells installed near the Yates State impoundment. A comparison of the major cation and anion chemistry shown on this diagram to the general formation quality data shown in Figure 2-5 shows that MW-1 data exhibits water of a quality similar to average Wasatch Formation water quality. Figure 5-100 also shows that the water quality shown at MW-2 appears to be influenced by CBNG produced water quality.

Additionally, it is unknown the extent the two aquifers sampled by the two monitoring wells are connected. The shallow sandy silt aquifer has limited head and may be a perched aquifer of very limited extent. This perched aquifer may outcrop beneath the impoundment if it extends that far, although the direction of water flow within the aquifer is unknown. Communication between the perched aquifer and the impoundment is likely; however, it is unknown whether flow is into the aquifer or into the impoundment.

On the other hand, the Anderson Coal aquifer, seen in MW-2, is extensive over much of the area. Water in the Anderson Coal aquifer is likely to drain both to the west, into the buttes, and to the east, toward the creek, following the dip of the coal seam. The

Anderson Coal may outcrop in the LX Bar Creek or in the alluvium under the creek to the north-east of the impoundment. The bottom of the impoundment is likely to be more than 40 feet above the Anderson, suggesting that infiltration into this aquifer is not probable.

#### **Yates Impoundment Bounty Hunter – LX Bar Creek**

CBNG produced water was initially discharged into the Bounty Hunter impoundment in 2001. Since CBNG produced water was discharged into the impoundment, three monitoring wells were installed. Groundwater chemistry, as shown in the Piper diagram in Figure 5-101, shows that the Bounty Hunter MW-1 contains a sodium-calcium-magnesium bicarbonate water, MW-2 contains a sodium-calcium-magnesium bicarbonate sulfate water, and MW-3 contains a magnesium-sodium-sulfate-bicarbonate water. Water chemistry representing average CBNG produced water quality is also plotted in Figure 5-101 for comparison and is characterized as having a predominant sodium/bicarbonate chemical signature. Anderson coal aquifer sampled at MW-1 contains a sodium-calcium-magnesium bicarbonate water. Alluvial water in MW-2 is similar to the coal aquifer but is enriched in sulfate. Alluvial water from MW-3 is similar to MW-2 water but is more enriched with sulfate ion. No indication of infiltration out of the impoundment into the alluvial aquifers is apparent from the sampling data.

Figure 5-102 presents the major cation and anion composition of the wells installed near the Bounty Hunter impoundment as plotted on a stiff diagram. A comparison of the major cation and anion chemistry shown on this diagram to the general formation quality data shown in Figure 2-5 indicates an apparent chemical change occurring from the water in MW-1 to MW-2 and MW-3. That change being a gradual decline in the sulfate concentration.

#### **Termo Impoundment Termo – LX Bar Creek**

CBNG produced water was initially discharged into the Termo impoundment in 2002. Since CBNG produced water was discharged into the impoundment, three monitoring wells were installed. Groundwater chemistry, as shown in the Piper diagram in Figure 5-103, shows the Termo MW-1, MW-2, and MW-3 contain a calcium-magnesium-sodium

sulfate water. Water chemistry representing average CBNG produced water quality is also plotted in Figure 5-103 for comparison, and is characterized as having a predominant sodium/bicarbonate chemical signature. MW-1 was screened through the Anderson Coal and overlying sandy siltstone. MW-2 was screened through the Anderson Coal and overlying silty clays. MW-3 is screened through the Anderson Coal and overlying sand. Water samples from these wells are approximately the same and no indication is seen for the occurrence of infiltration out of the impoundment into the alluvial aquifers.

Figure 5-104 presents the major cation and anion composition of the wells installed near the Termo impoundment as plotted on a stiff diagram. A comparison of the major cation and anion chemistry shown on the stiff diagram in Figure 5-104 to the general formation quality data shown in Figure 2-5 shows the quality of water to differ from the average water quality of the shallow aquifers in the PRB.

#### **Yates Impoundment Waylon – LX Bar Creek**

CBNG produced water was initially discharged into the Waylon impoundment in 2002. Since CBNG produced water was discharged into the impoundment, three monitoring wells were installed. Groundwater chemistry, as shown in the Piper diagram in Figure 5-105, shows the Waylon MW-1, MW-2, and MW-3 contains calcium-magnesium-sodium sulfate water. Water chemistry representing average CBNG produced water quality is also plotted in Figure 5-105 for comparison, and is characterized as having a predominant sodium/bicarbonate chemical signature. MW-1 is screened in the Lower Cook Coal and an overlying silt. MW-2 is screened in a silty sand below the Lower Cook Coal. MW-3 is screened in the Lower Cook Coal aquifer. MW-3 is structurally down-gradient while MW-1 and MW-2 are up-gradient of the impoundment. It appears that the Lower Cook becomes only slightly enriched in magnesium and sulfate ions, suggesting that the aquifer is less influenced by CBNG water. If MW-1 and MW-3 are screened in the same aquifer, then there seems to be no evidence of infiltration out of the impoundment. All three of the water samples appear to be surface water related, not influenced by CBNG water.

Figure 5-106 presents the major cation and anion composition of the wells installed near the Waylon impoundment as plotted on a stiff diagram. A comparison of the major



cation and anion chemistry shown on the stiff diagram in Figure 5-106 to the general formation quality data shown in Figure 2-5 shows there appears to be a chemical change occurring from the water in MW-1 to MW-3 as a gradual decline in the magnesium and sulfate concentration occurs.

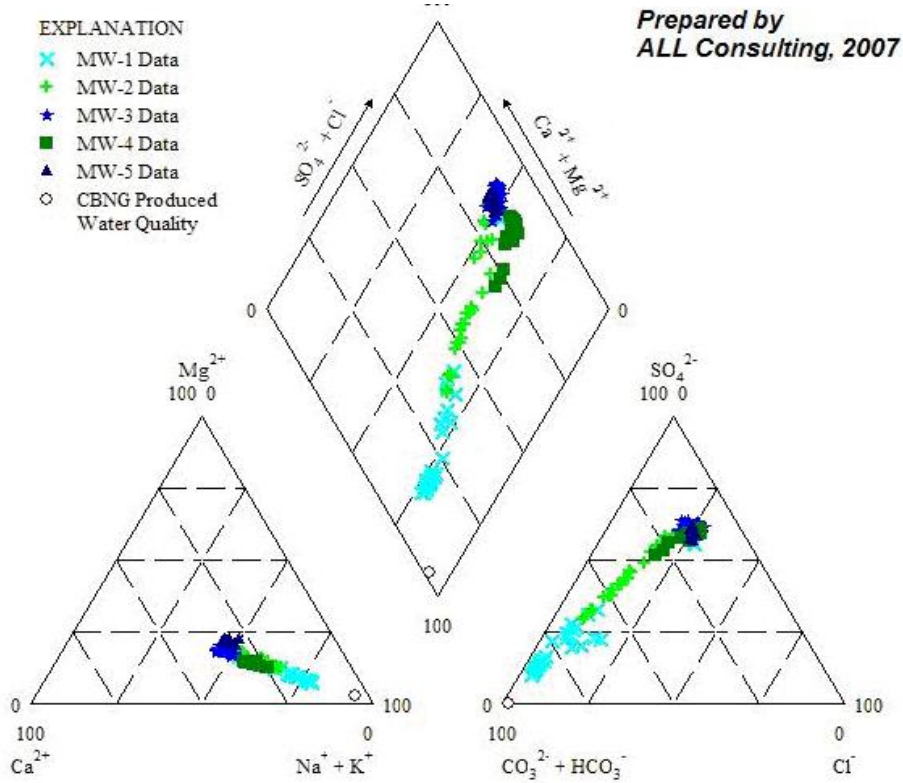
### **J.M. Huber Impoundment Golden Eagle – LX Bar Creek**

CBNG produced water was initially discharged into the Golden Eagle impoundment in 2000. Since CBNG produced water was discharged into the impoundment, three monitoring wells were installed. Groundwater chemistry, as shown in the Piper diagram in Figure 5-107, shows the Waylon MW-1, MW-2, and MW-3 contains calcium-magnesium-sodium sulfate water. All three samples are mixed ion sulfate waters that are similar to each other and are similar to alluvial water seen elsewhere. These samples do not appear to have been impacted by infiltration of CBNG water. No up-gradient alluvial aquifer sample point appears to be available at this reservoir. MW-2 and MW-3 appear to be free of impact from infiltrate coming from the impoundment. Water chemistry representing average CBNG produced water quality is also plotted in Figure 5-107 for comparison, and is characterized as having a predominant sodium/bicarbonate chemical signature. MW-1 is screened in Felix Coal and underlying bedrock. MW-2 and MW-3 are screened in shallow alluvium below the impoundment. Water samples are approximately the same and no indication is seen for the occurrence of infiltration out of the impoundment into the alluvial aquifers.

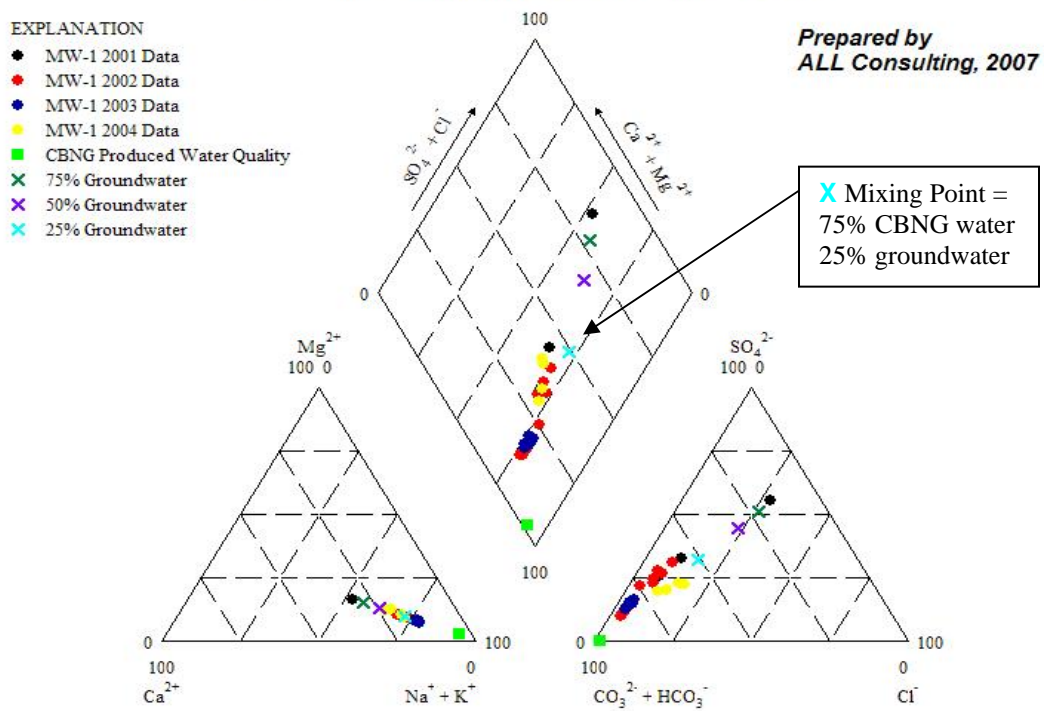
Figure 5-108 presents the major cation and anion composition of the wells installed near the Golden Eagle impoundment on a stiff diagram. A comparison of the major cation and anion chemistry shown on the stiff diagram in Figure 5-108 to the general formation quality data shown in Figure 2-5 shows there appears to be a chemical change occurring to the cations from MW-1 to MW-3 as a gradual increase in magnesium concentration occurs.

**APPENDIX F**  
**FIGURES**

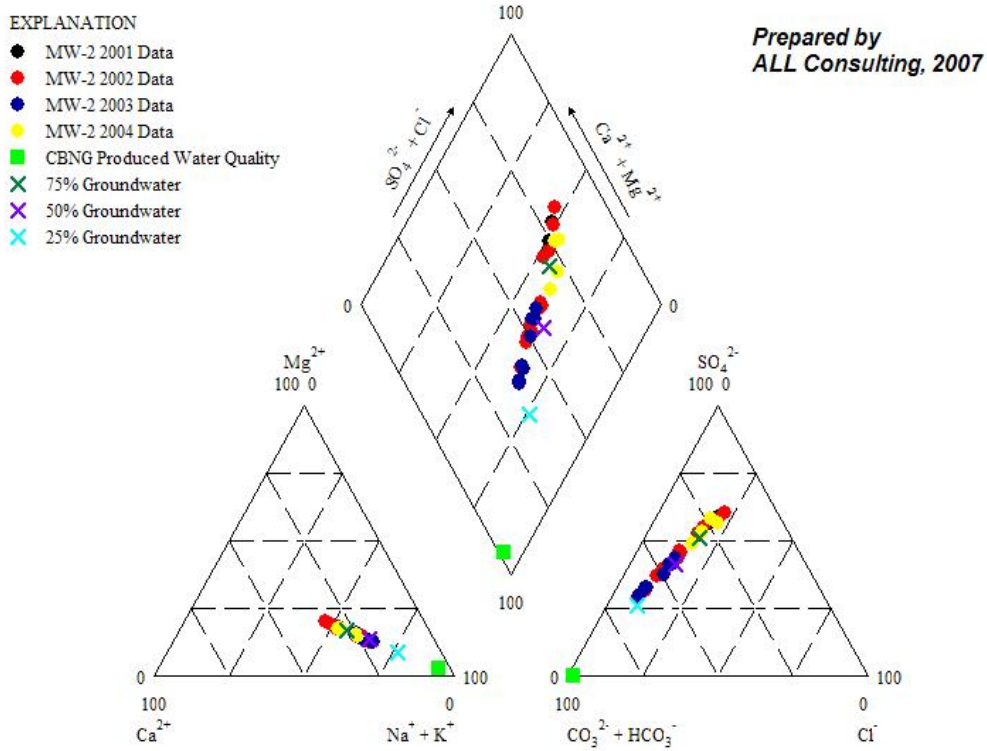
**Figure 5-1: Piper Plot for Water Samples Collected from the Jeff 3 Impoundment Monitoring Wells**



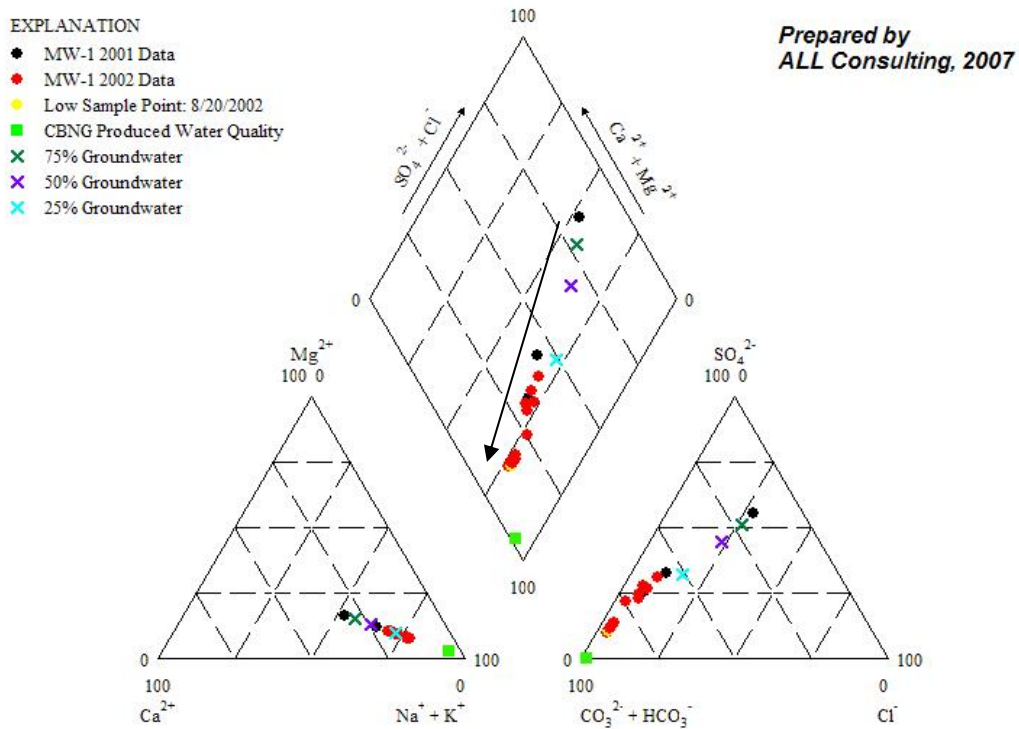
**Figure 5-2: Piper Plot for Jeff 3 MW-1**



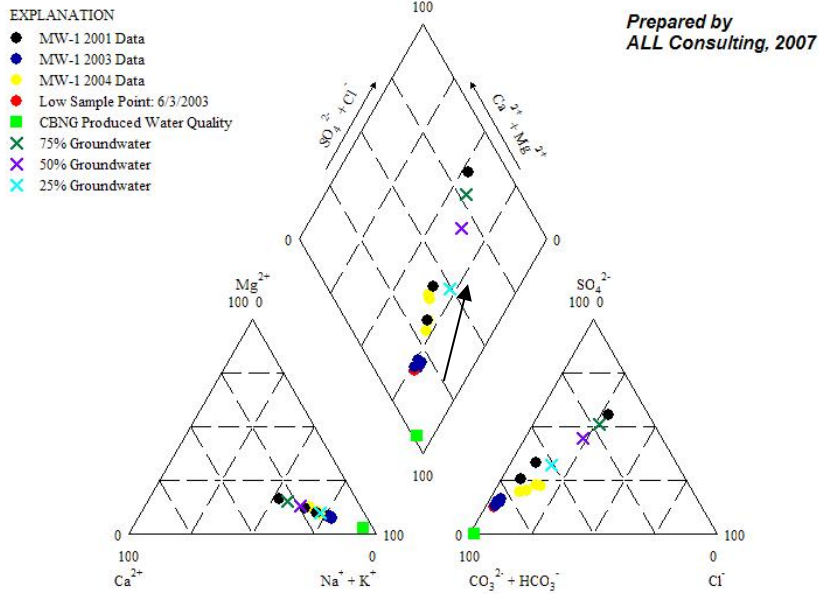
**Figure 5-3: Piper Plot for Jeff 3 MW-2**



**Figure 5-4: Piper Plot for Jeff 3 MW-1 Years 2001-2002**

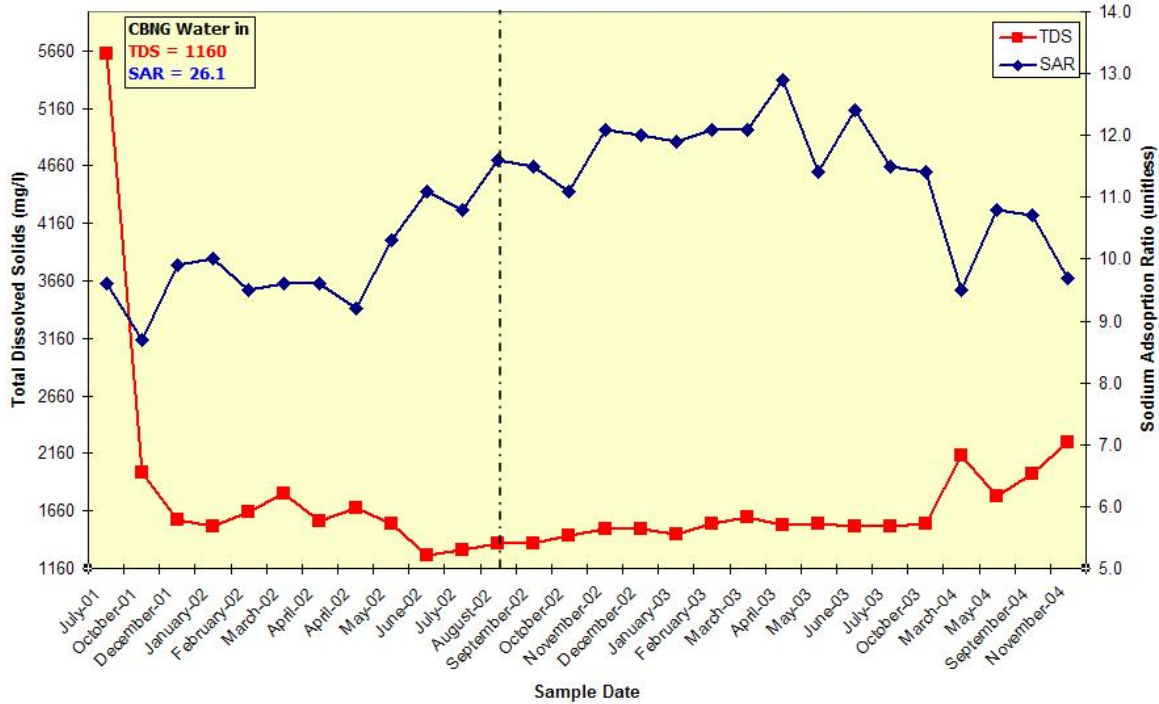


**Figure 5-5: Piper Plot for Jeff 3 MW-1 Years 2003-2004**



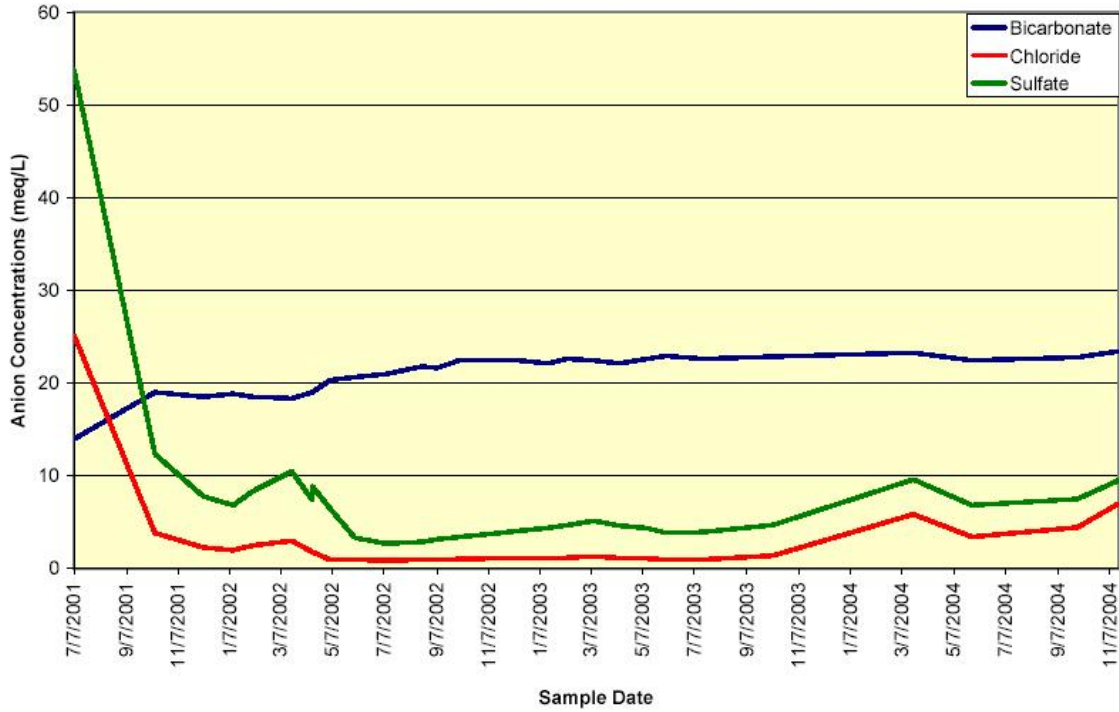
**Figure 5-6: SAR and TDS Trends for Jeff 3 MW-1**

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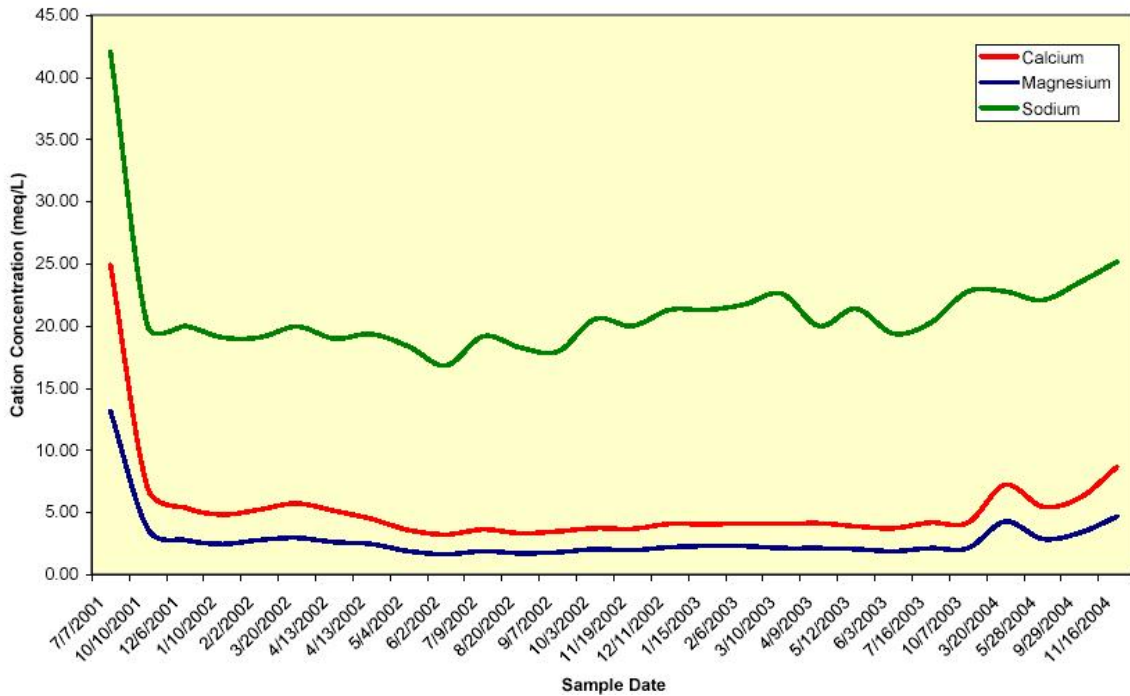
**Figure 5-7: Anion Trend Data for the Jeff 3 MW-1**

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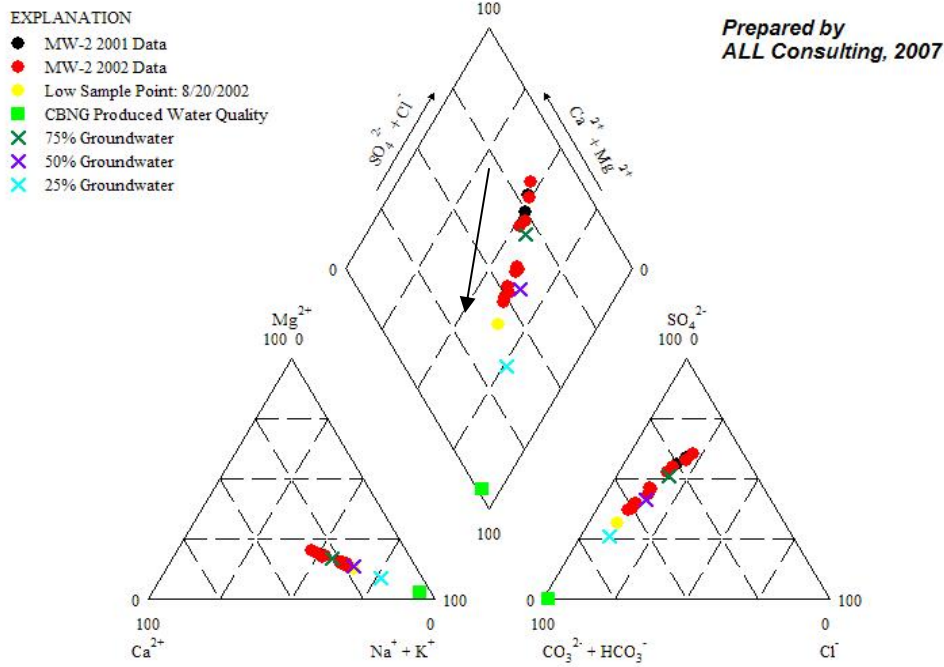
**Figure 5-8: Cation Trend Data for the Jeff 3 MW-1**

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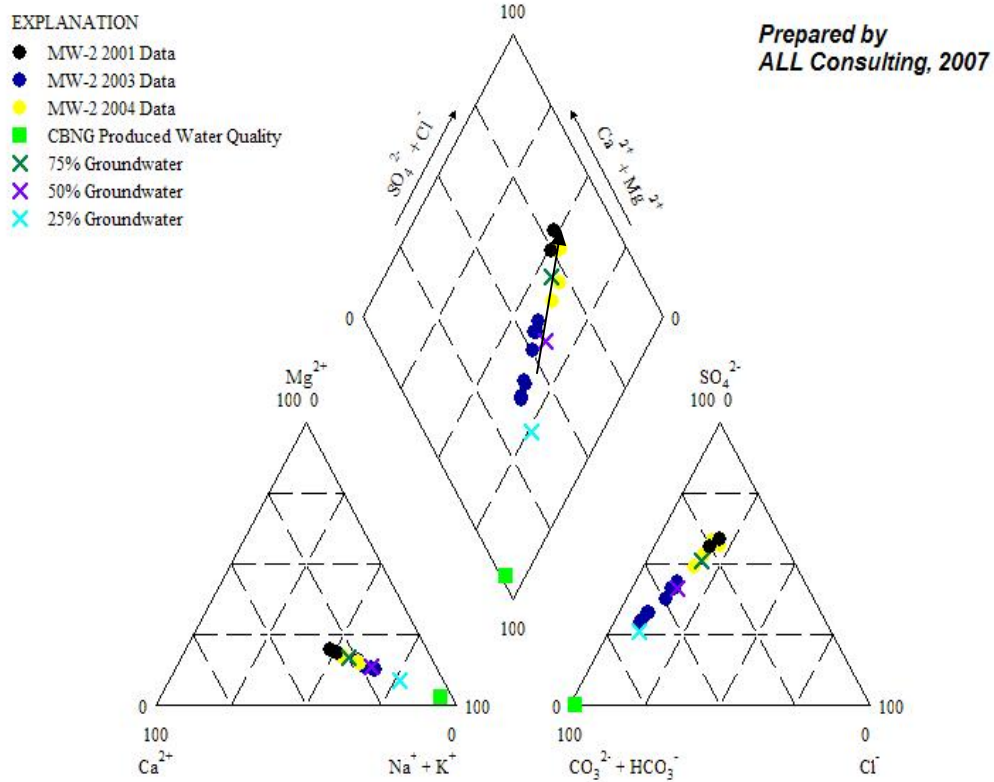




**Figure 5-9: Piper Plot for Jeff 3 MW-2 Years 2001-2002**

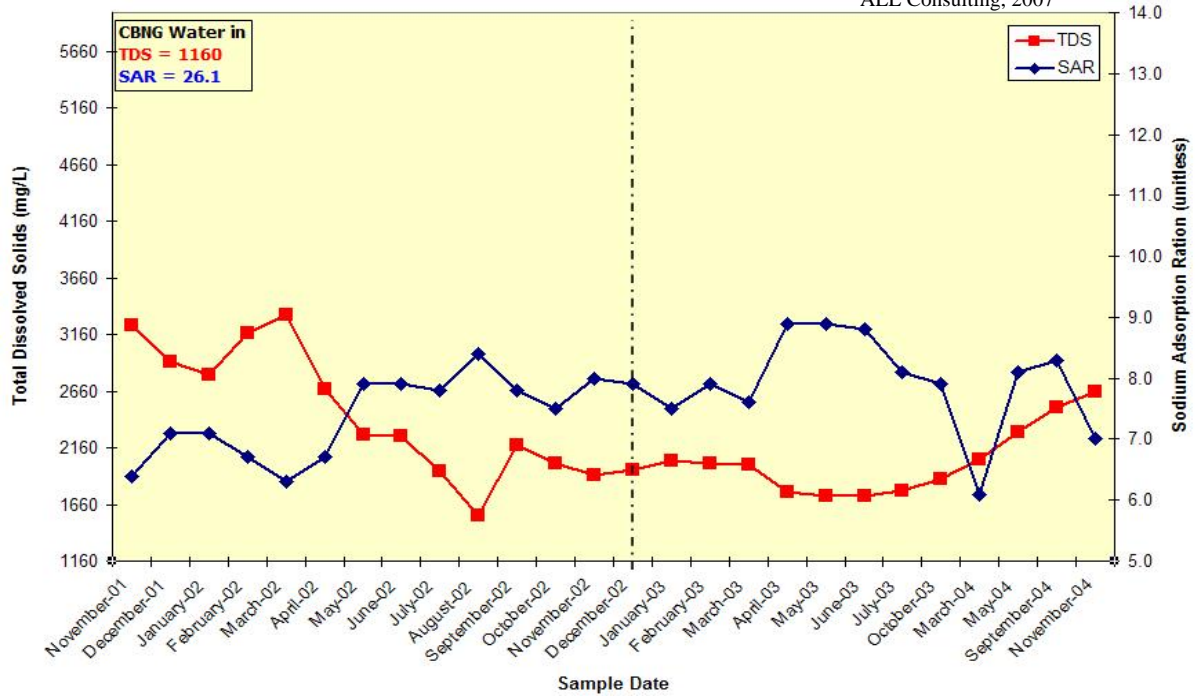


**Figure 5-10: Piper Plot for Jeff 3 MW-2 Years 2003-2004**



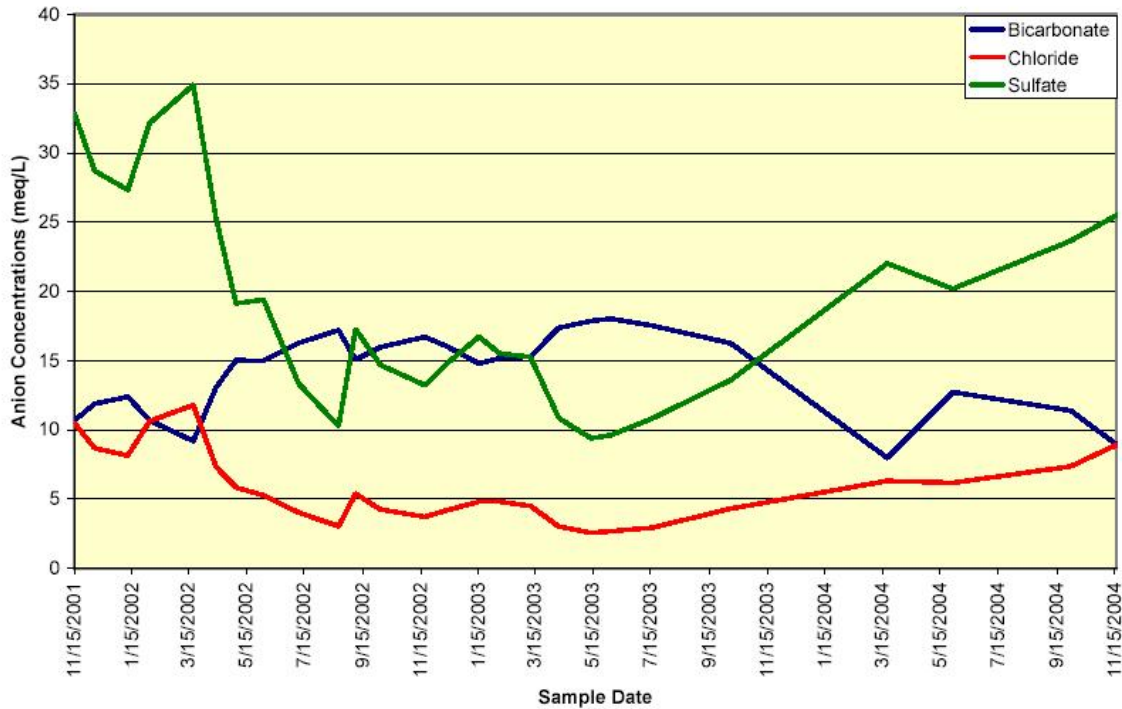
**Figure 5-11: SAR and TDS Trends for Jeff 3 MW-2**

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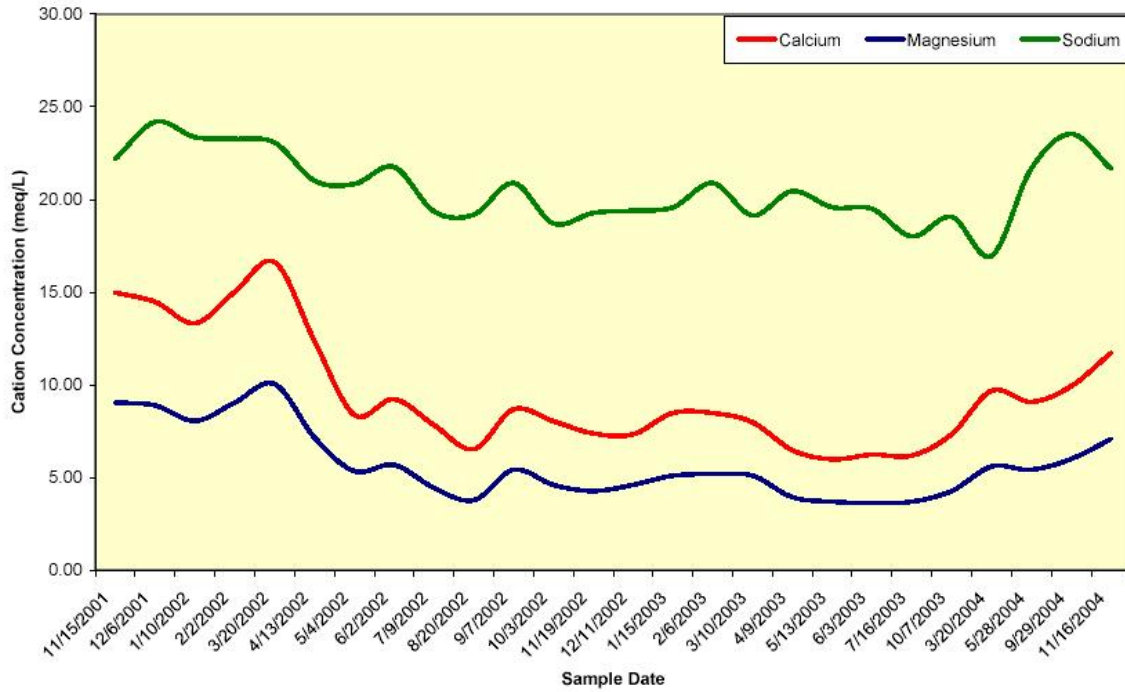
**Figure 5-12: Anion Trend Data for the Jeff 3 MW-2**

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**Figure 5-13: Cation Trend Data for the Jeff 3 MW-2**

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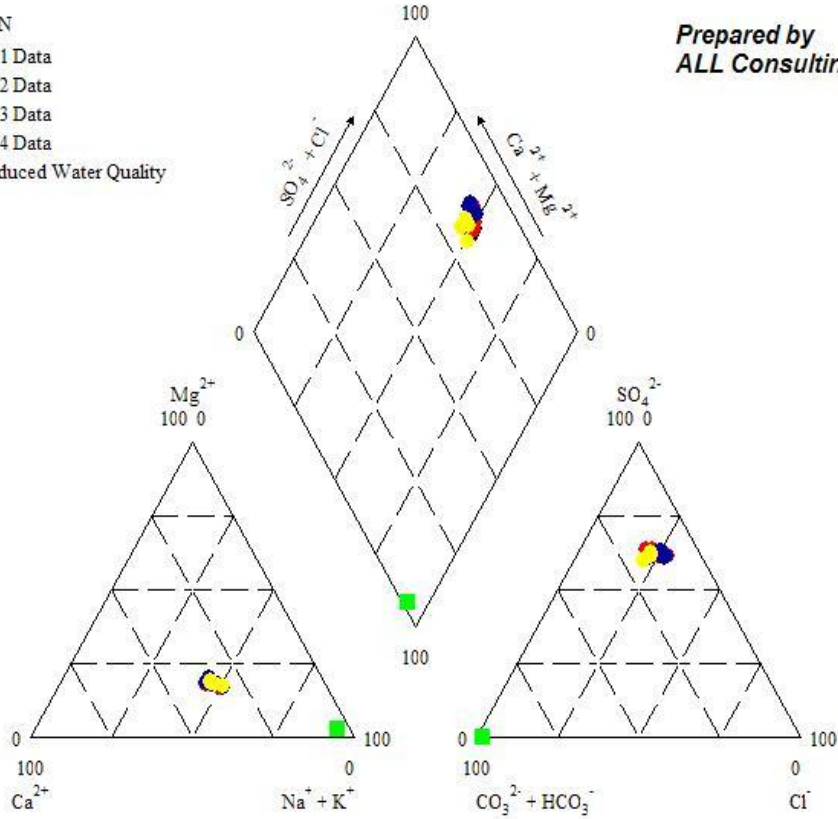


**Figure 5-14: Piper Diagram of Water Samples Collected from Jeff 3 MW-3**

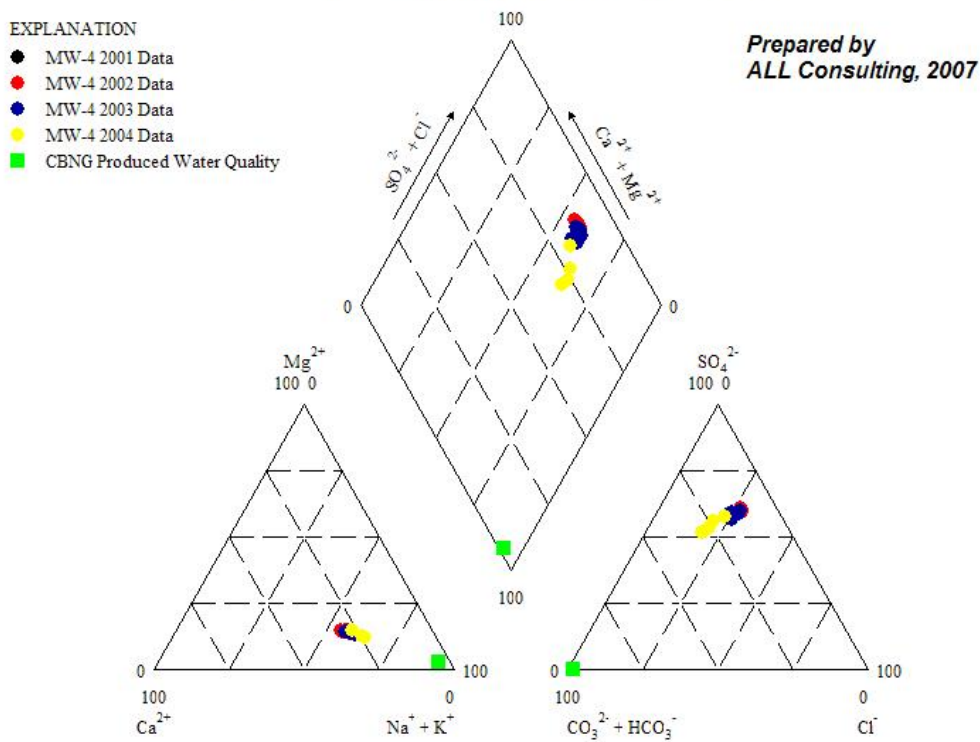
**EXPLANATION**

- MW-3 2001 Data
- MW-3 2002 Data
- MW-3 2003 Data
- MW-3 2004 Data
- CBNG Produced Water Quality

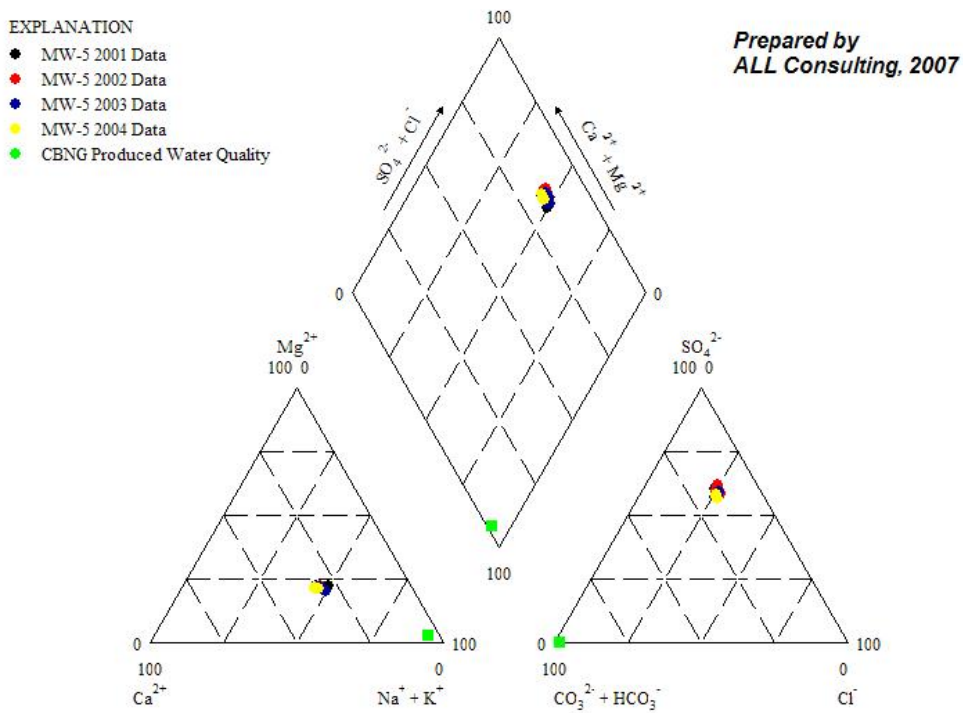
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ALL Consulting, 2007



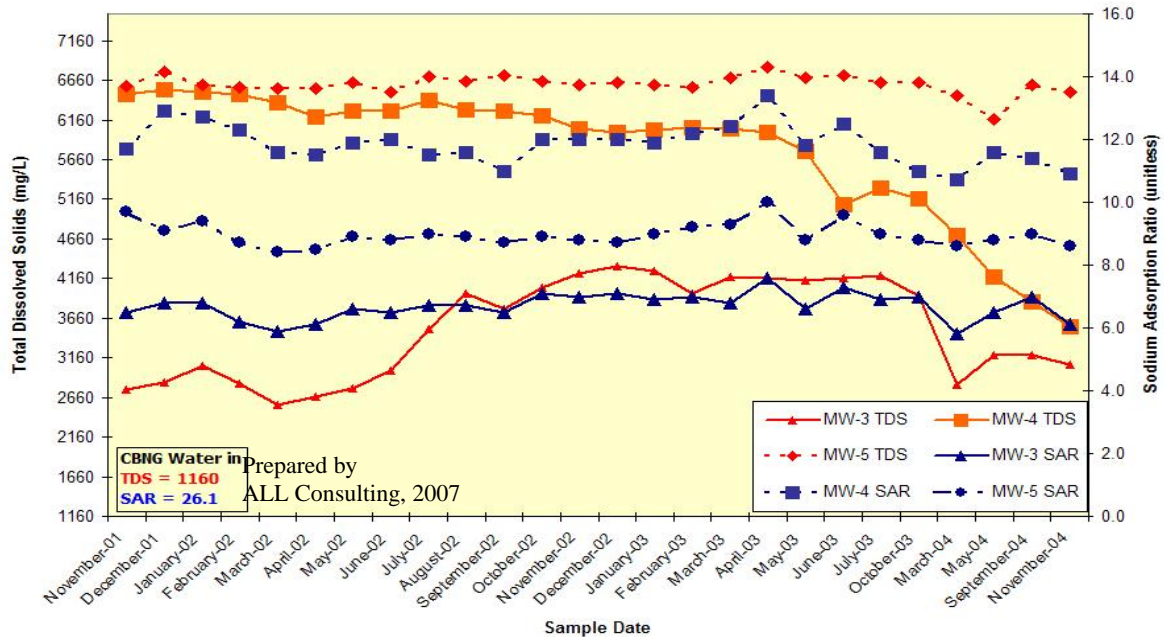
**Figure 5-15: Piper Diagram of Water Samples Collected from Jeff 3 MW-4**



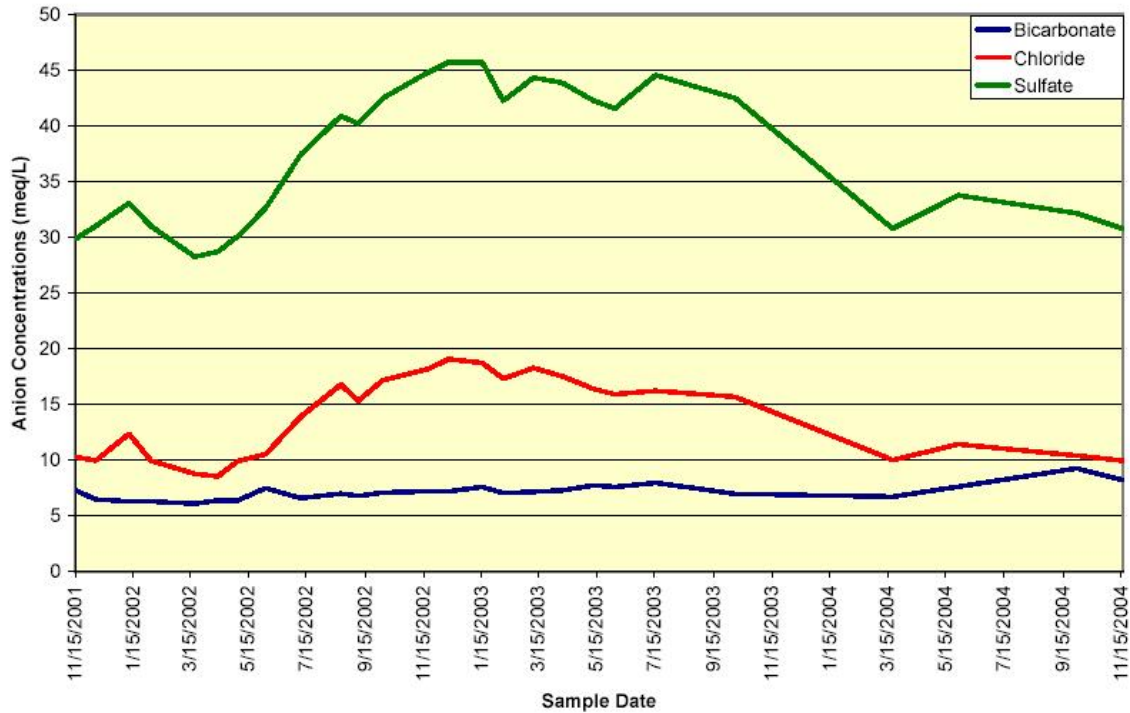
**Figure 5-16: Piper Diagram of Water Samples Collected from Jeff 3 MW-5**



**Figure 5-17: SAR and TDS Trends for Jeff 3 MW-3, MW-4, and MW-5**

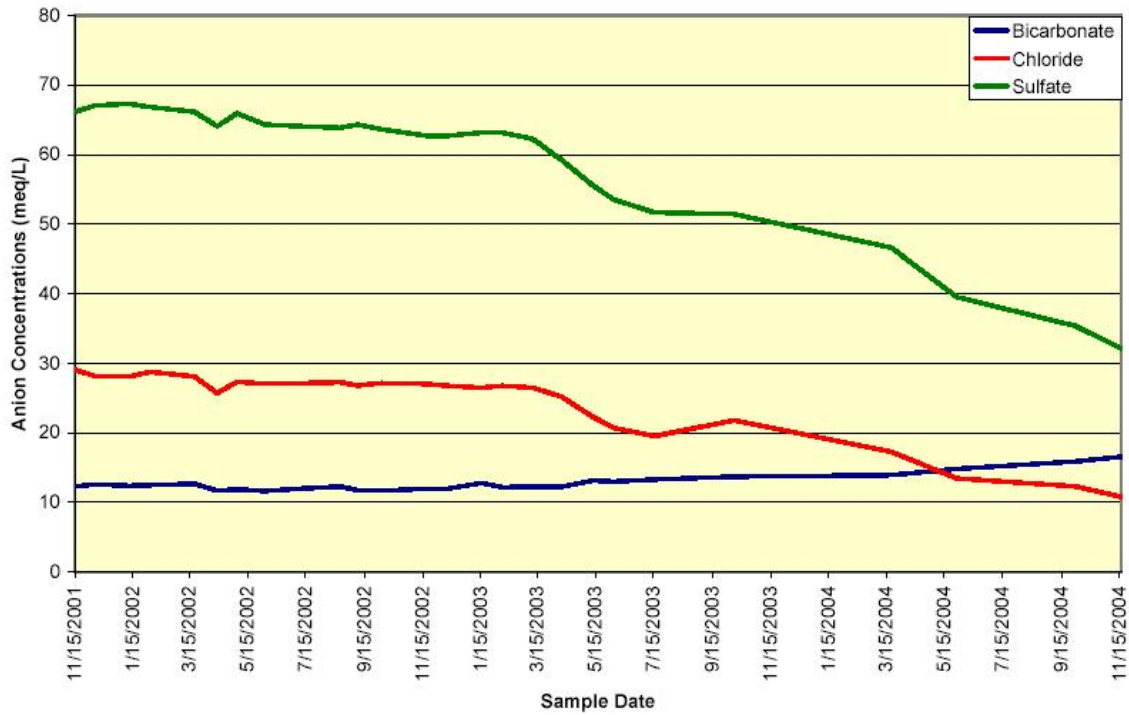


**Figure 5-18: Anion Trend Data for the Jeff 3 MW-3**

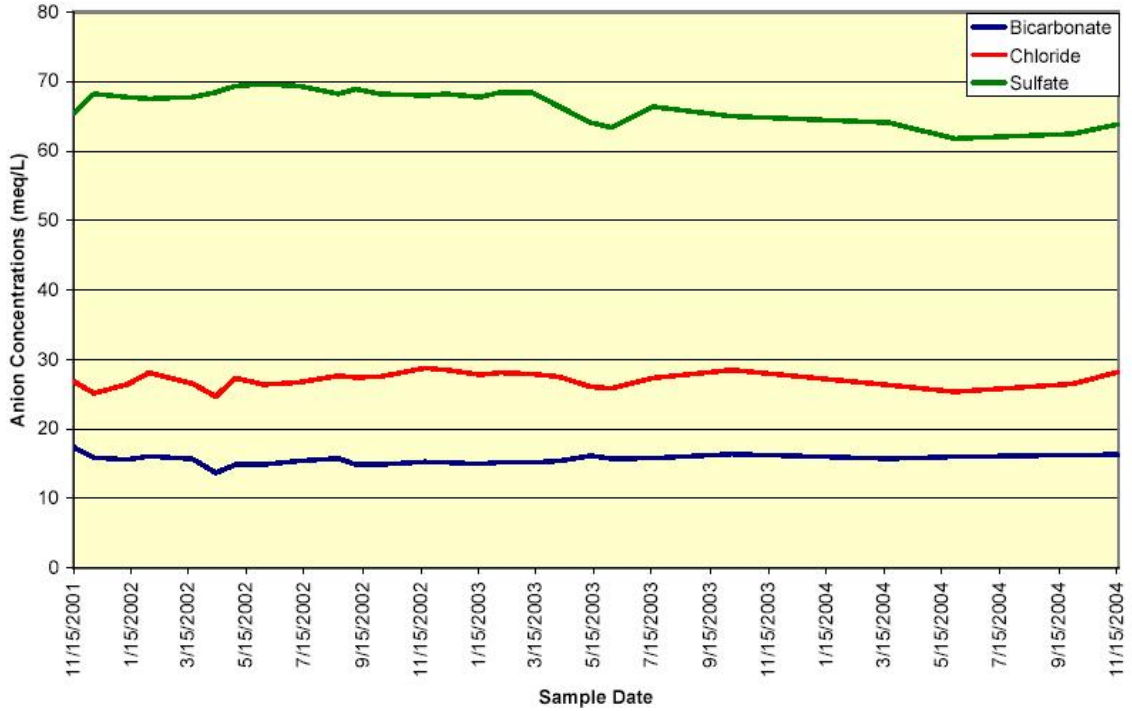




**Figure 5-19: Anion Trend Data for the Jeff 3 MW-4**

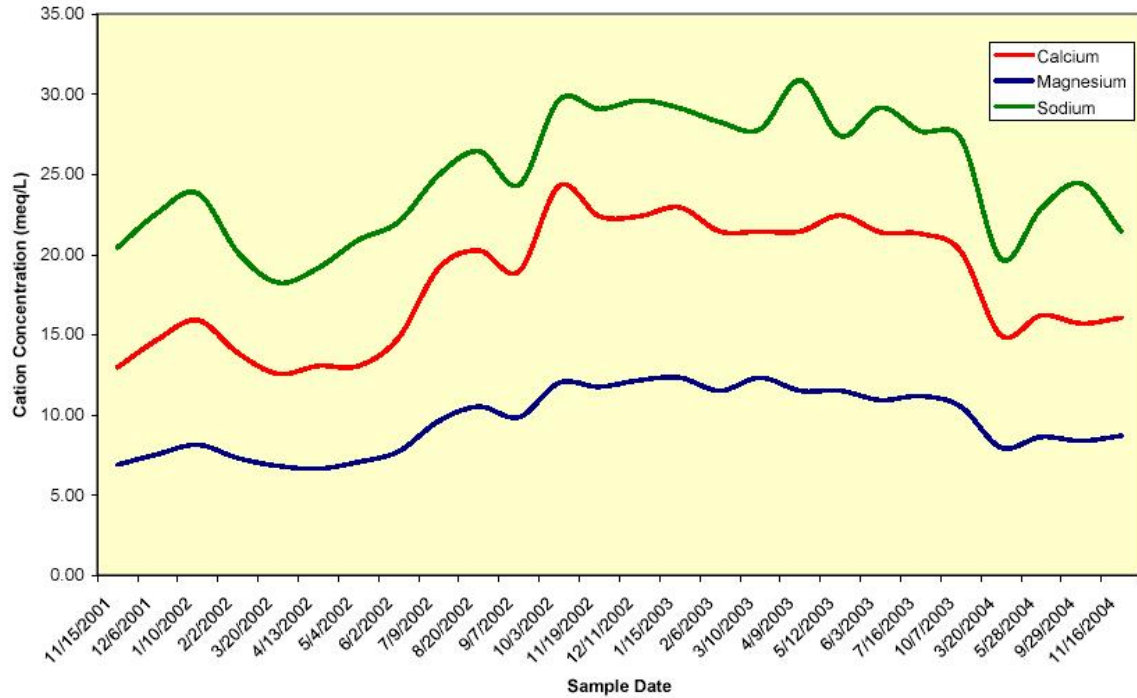


**Figure 5-20: Anion Trend Data for the Jeff 3 MW-5**

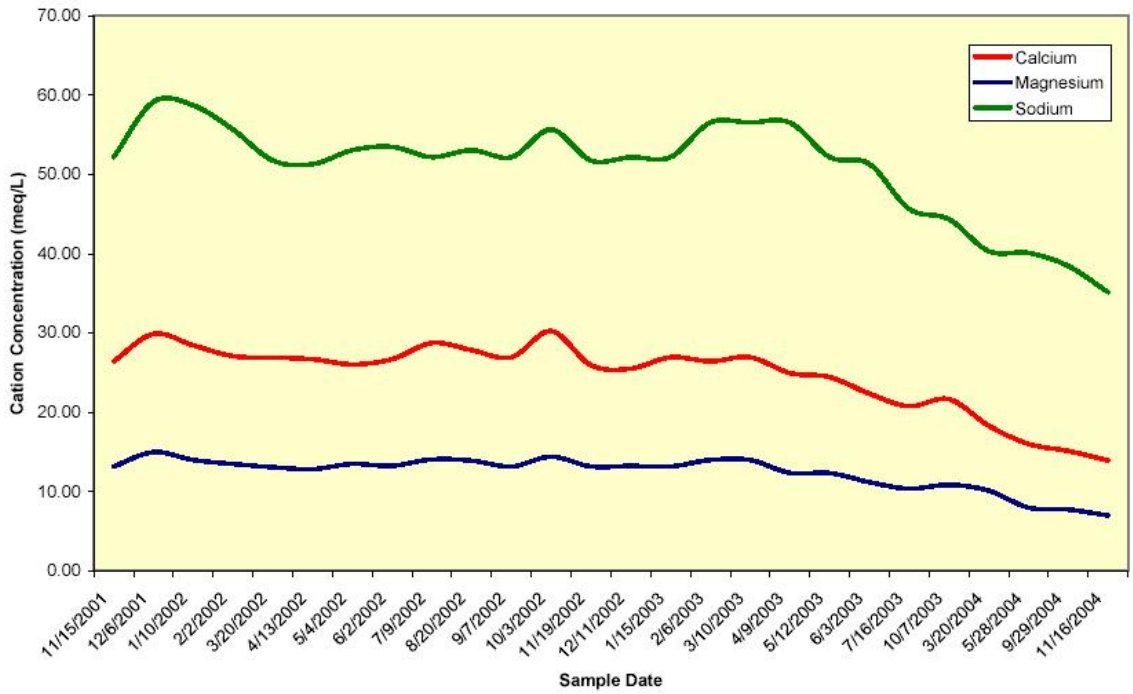




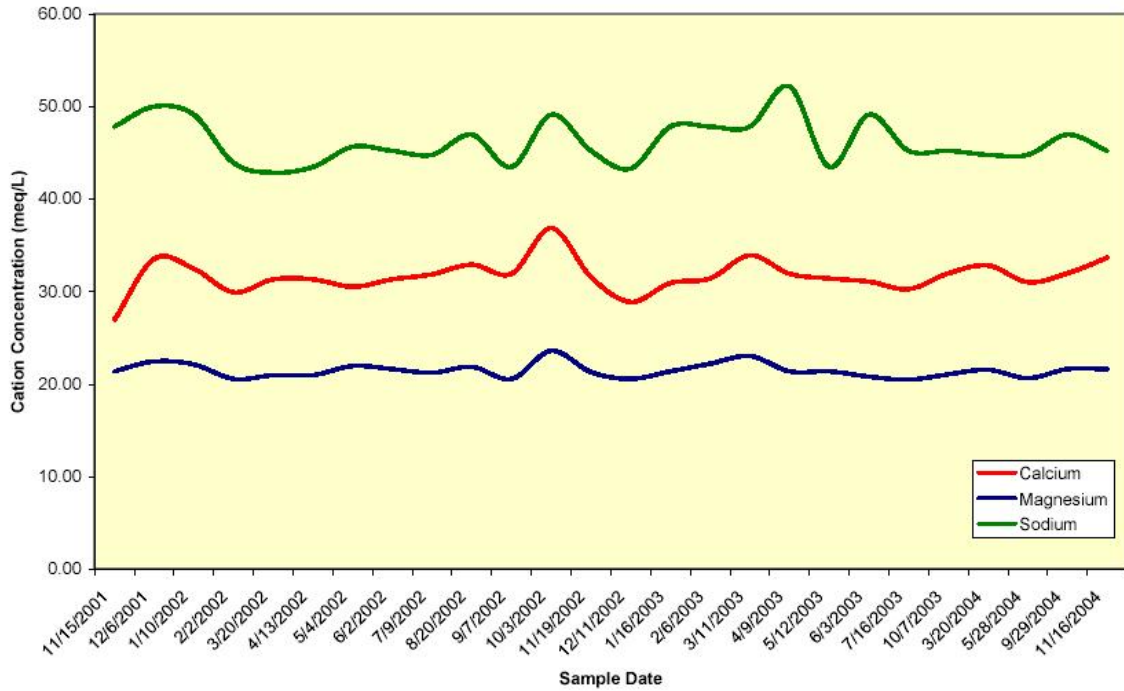
**Figure 5-21: Cation Trend Data for the Jeff 3 MW-3**



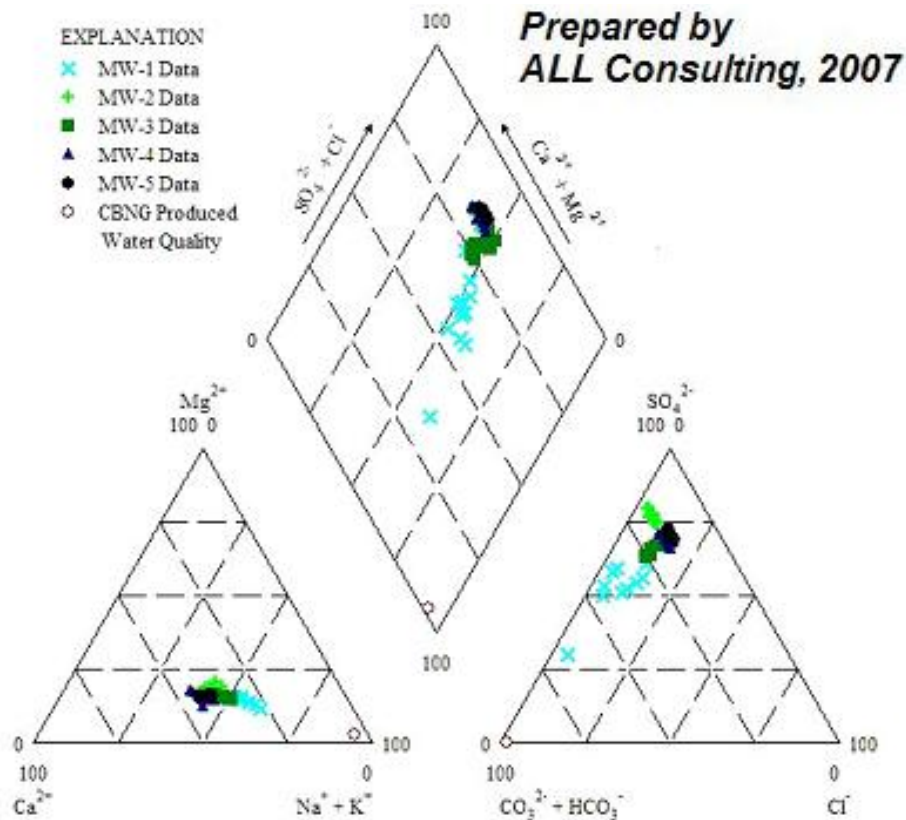
**Figure 5-22: Cation Trend Data for the Jeff 3 MW-4**



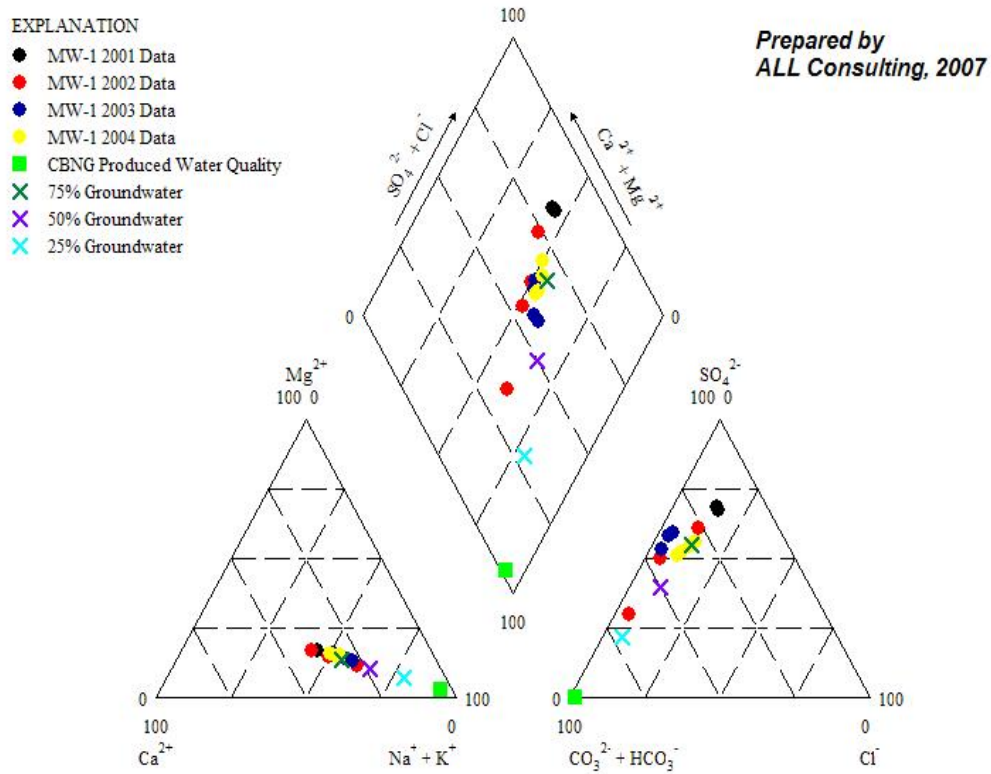
**Figure 5-23: Cation Trend Data for the Jeff 3 MW-5**



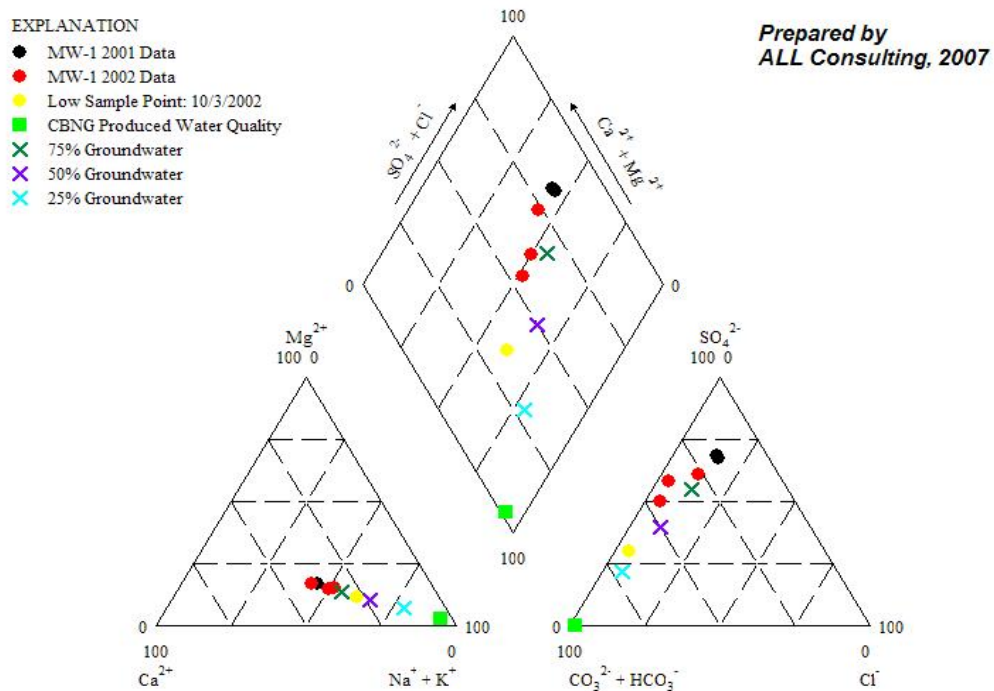
**Figure 5-24: Piper Plot for Water Samples Collected from the Jeff 5 Impoundment Monitoring Wells**



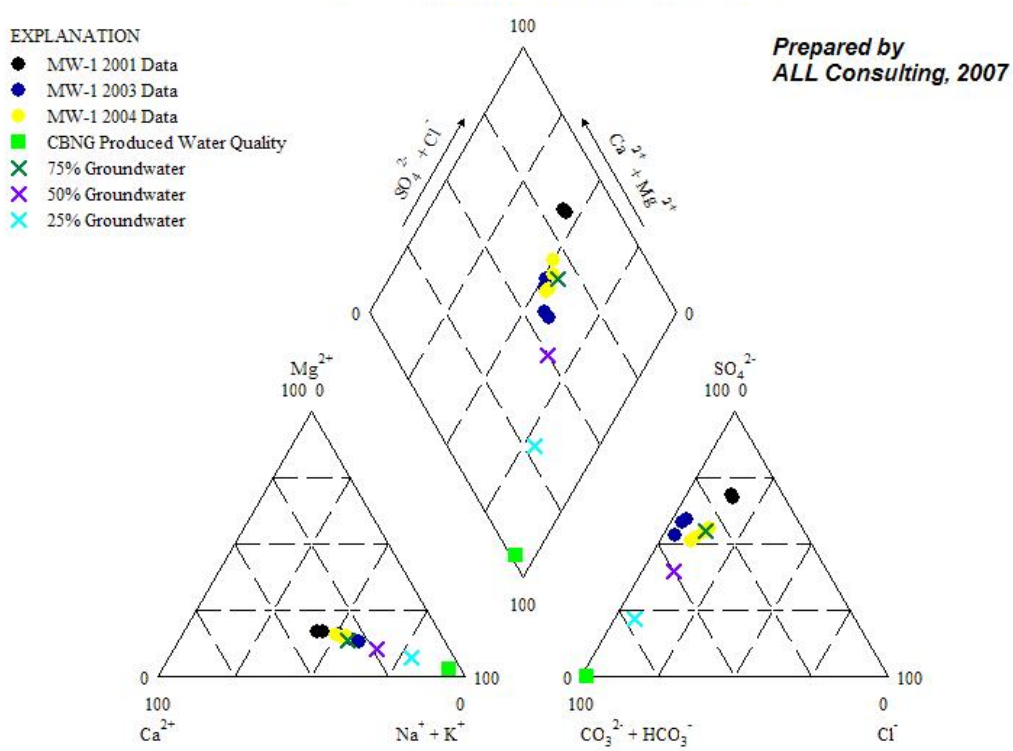
**Figure 5-25: Piper Plot for Jeff 5 MW-1**



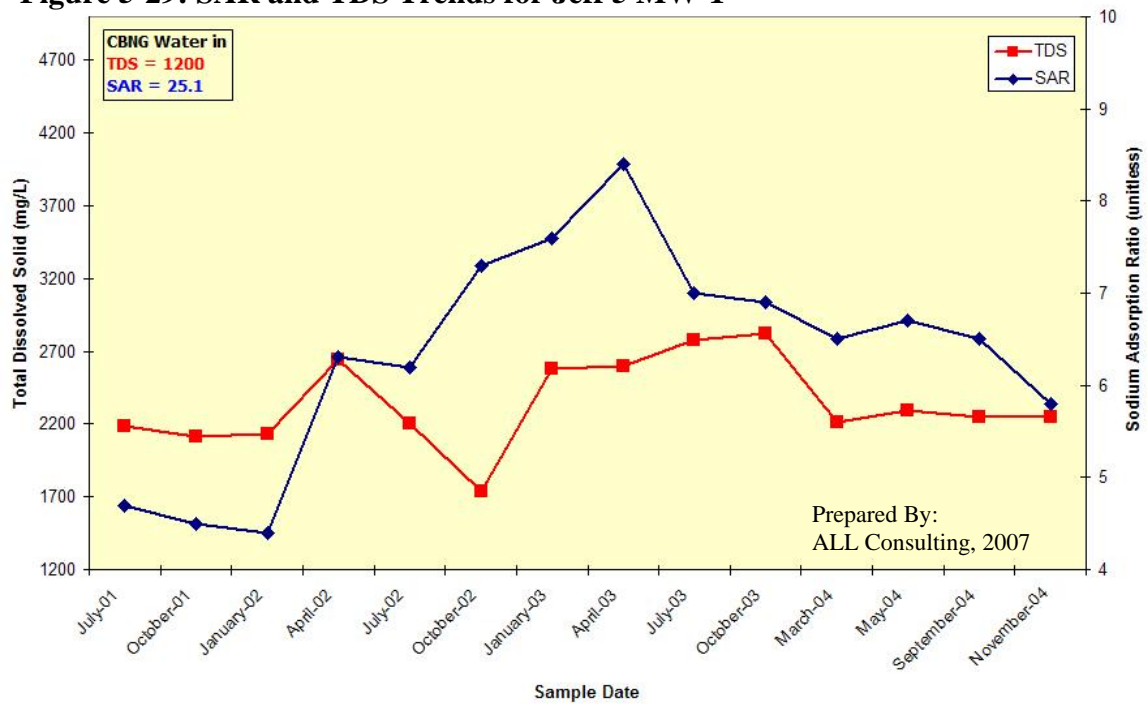
**Figure 5-26: Piper Plot for Jeff 5 MW-1 Years 2001-2002**



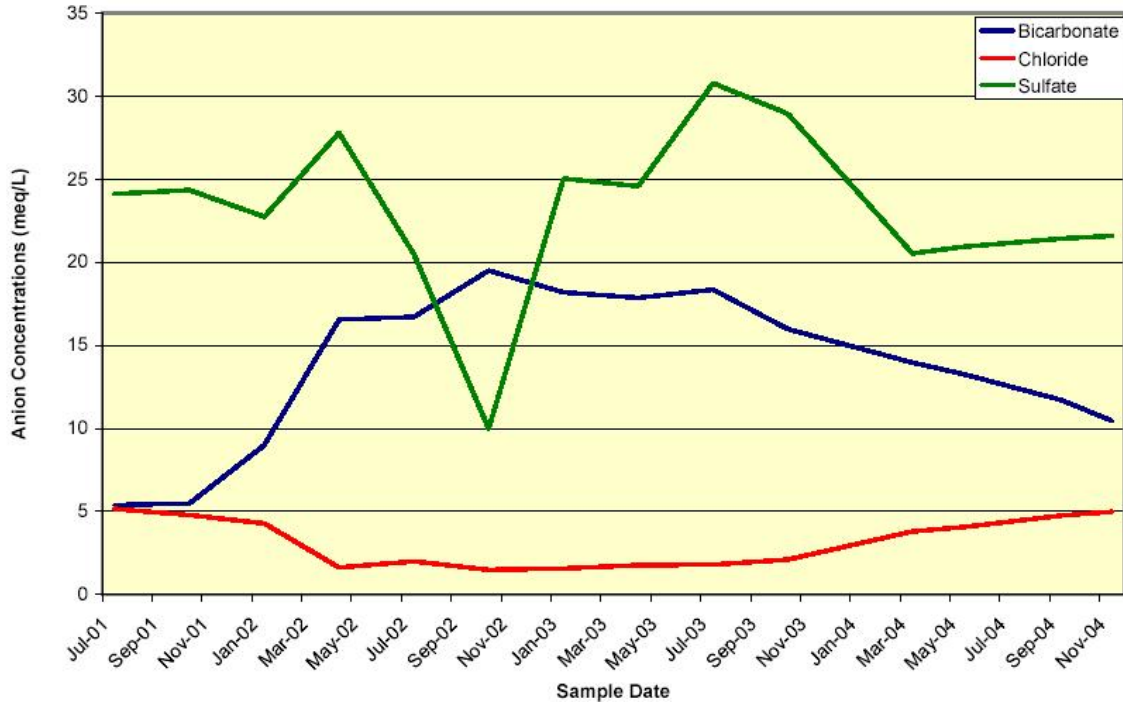
**Figure 5-28: Piper Plot for Jeff 5 MW-1 Years 2003-2004**



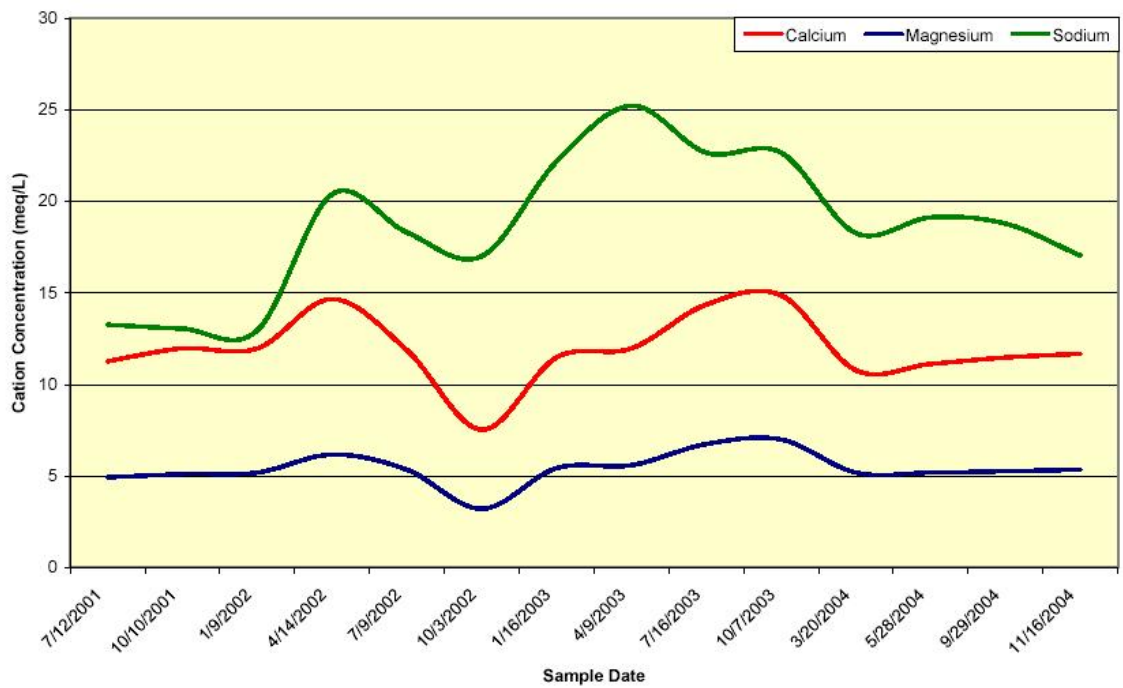
**Figure 5-29: SAR and TDS Trends for Jeff 5 MW-1**



**Figure 5-30: Anion Trend Data for the Jeff 5 MW-1**

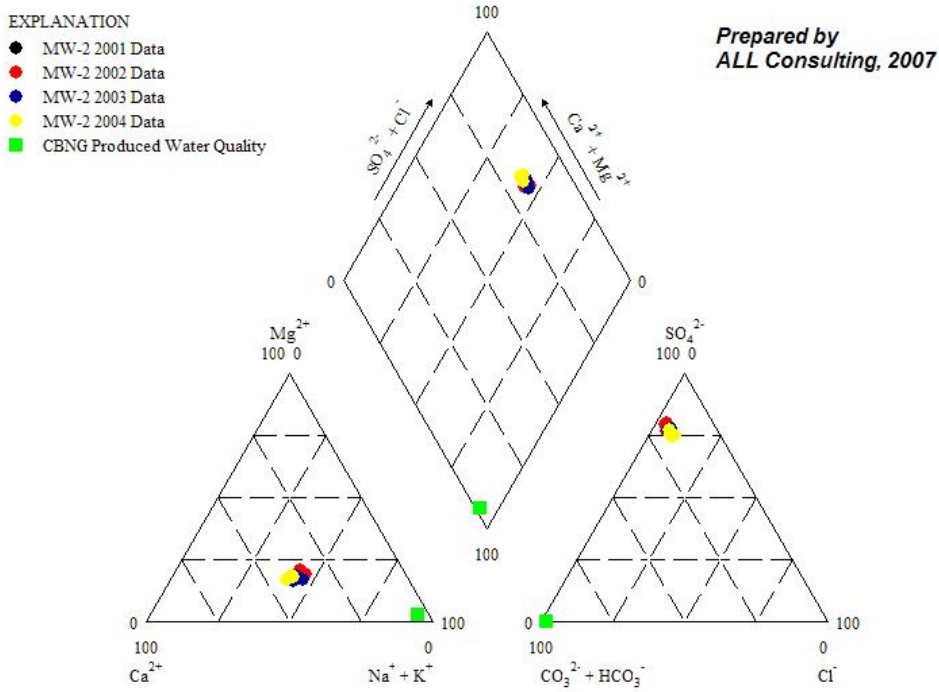


**Figure 5-31: Cation Trend Data for the Jeff 5 MW-1**

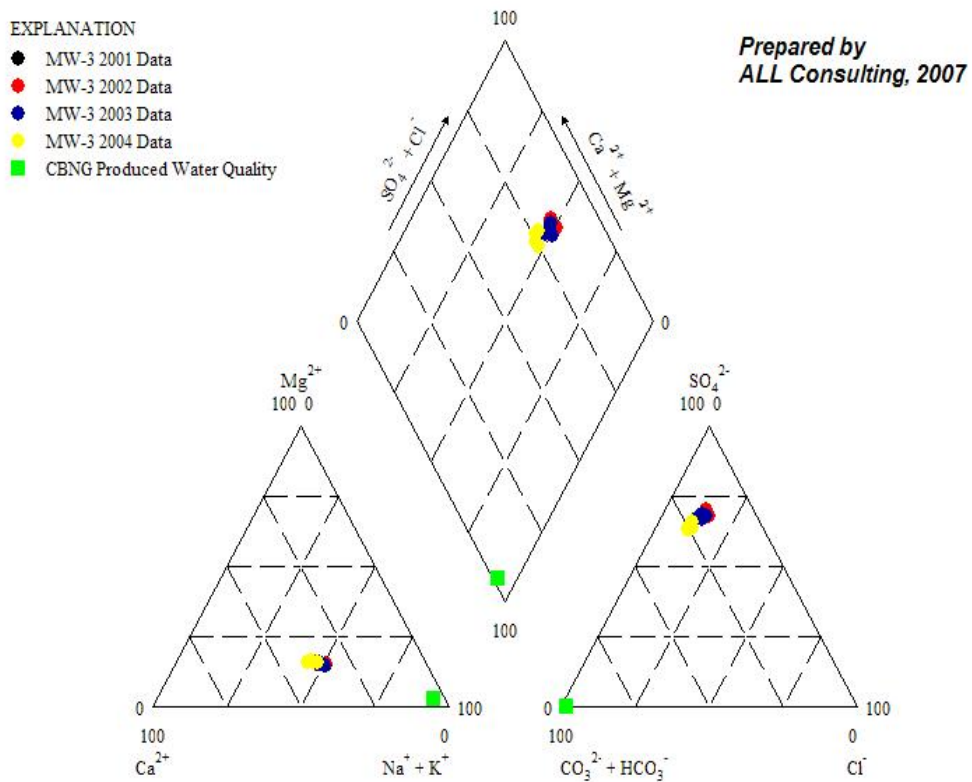




**Figure 5-32: Piper Plot of Water Samples Collected from Jeff 5 MW-2**

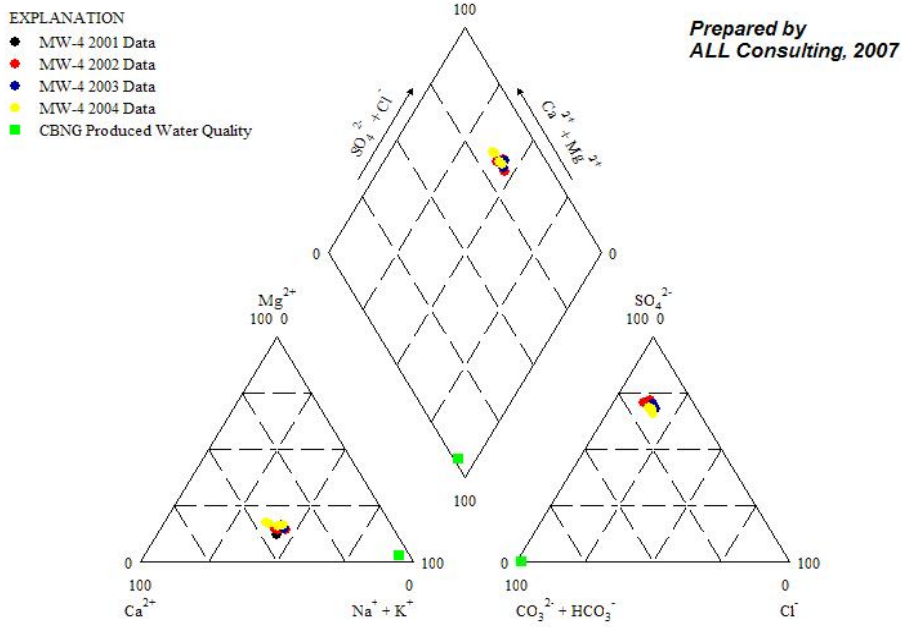


**Figure 5-33: Piper Plot of Water Samples Collected from Jeff 5 MW-3**

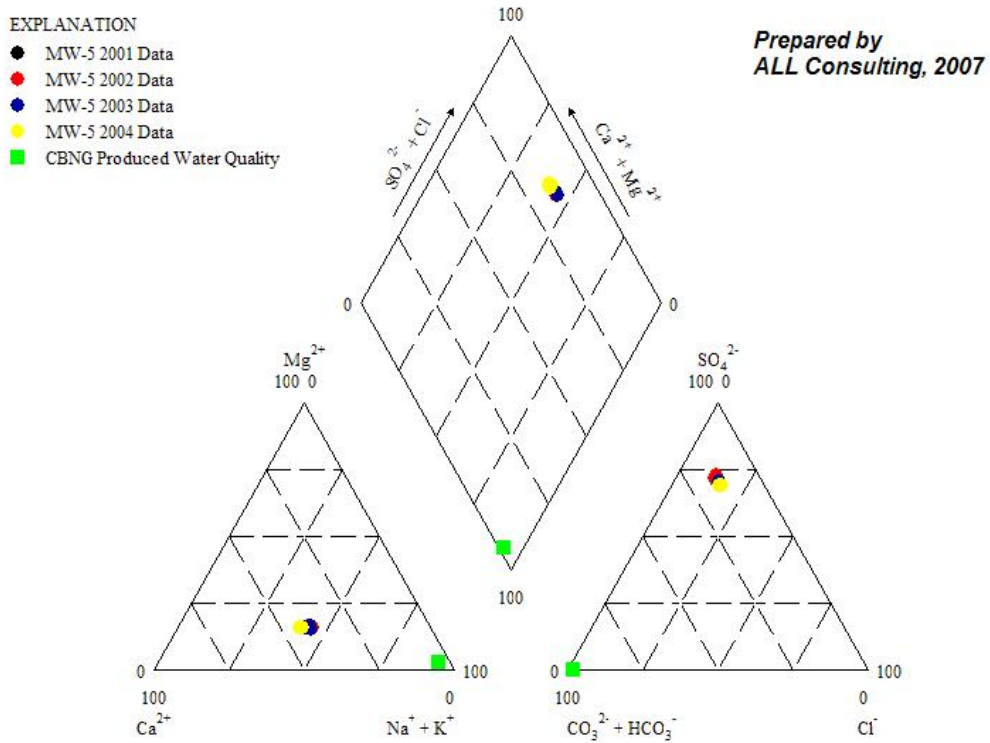




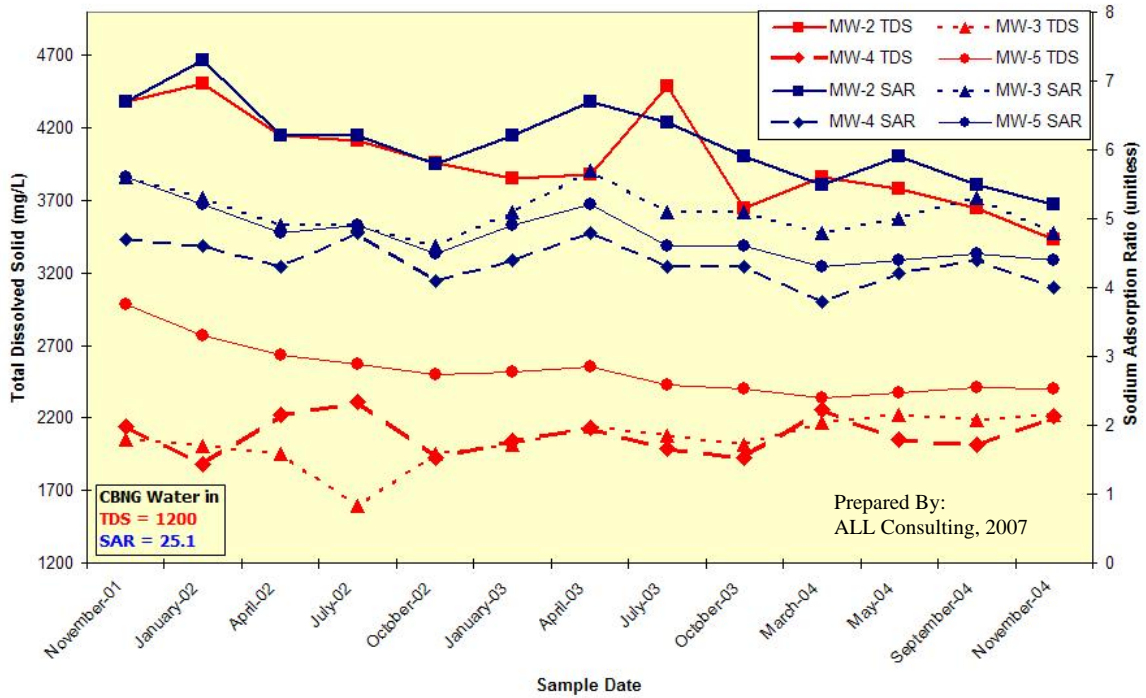
**Figure 5-34: Piper Plot of Water Samples Collected from Jeff 5 MW-4**



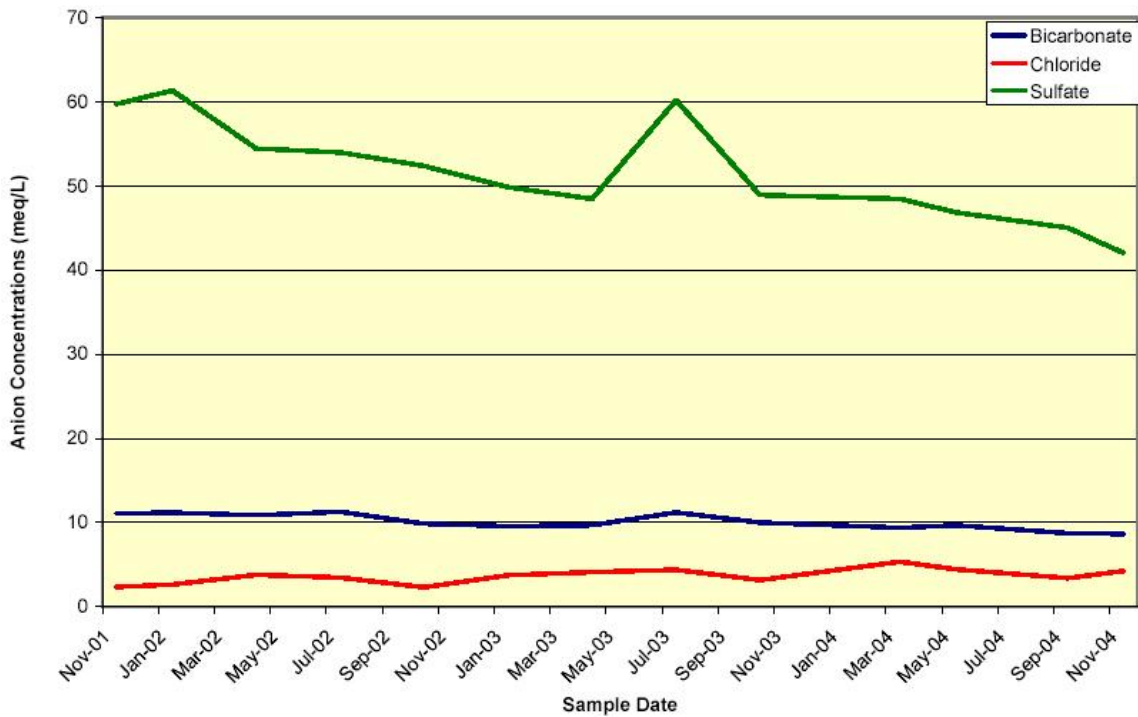
**Figure 5-35: Piper Plot of Water Samples Collected from Jeff 5 MW-5**



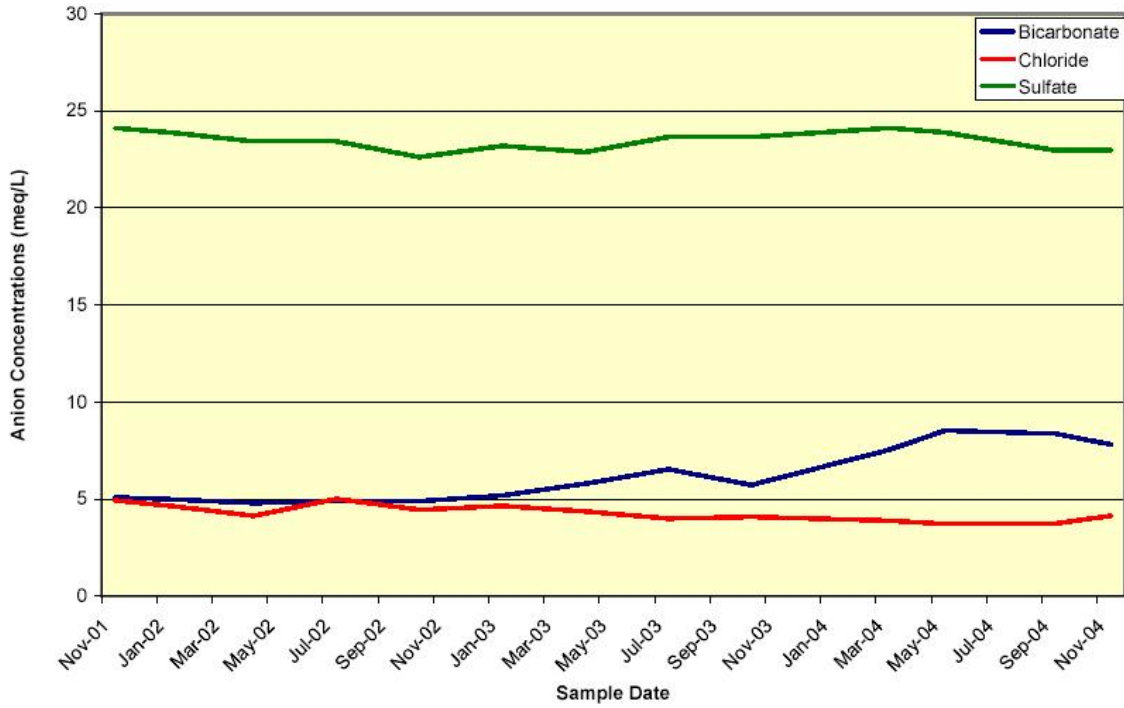
**Figure 5-36: SAR and TDS Trends for Jeff 5 MW-2, MW-3, MW-4, and MW-5**



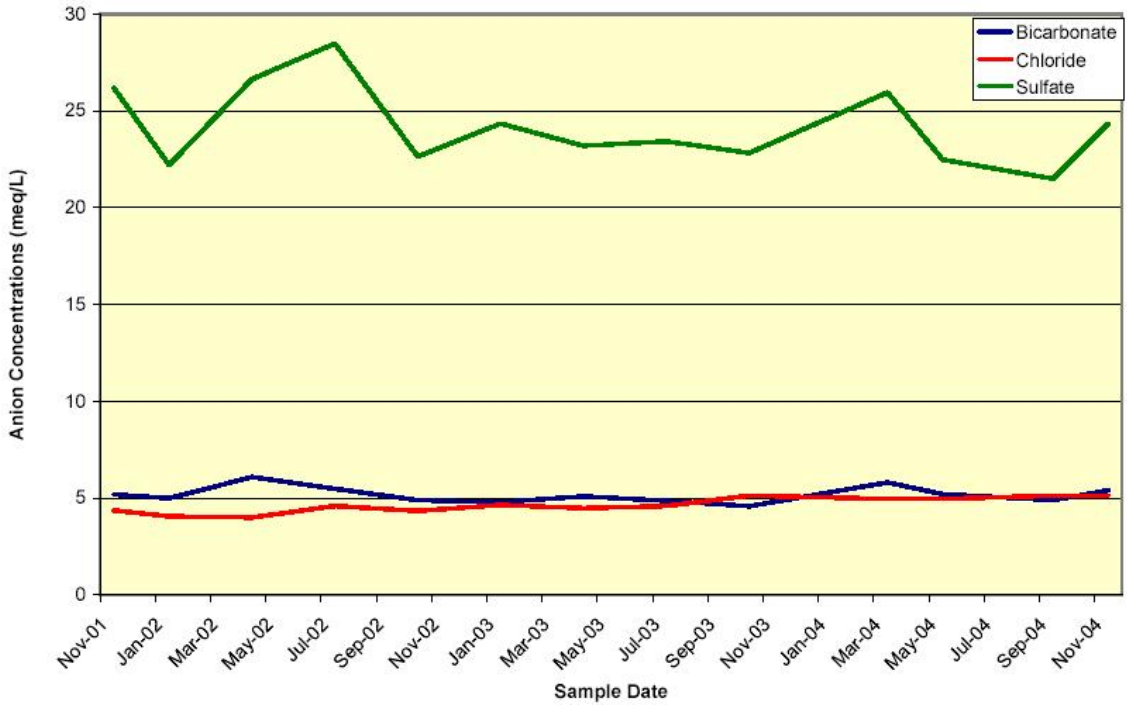
**Figure 5-37: Anion Trend Data for the Jeff 5 MW-2**



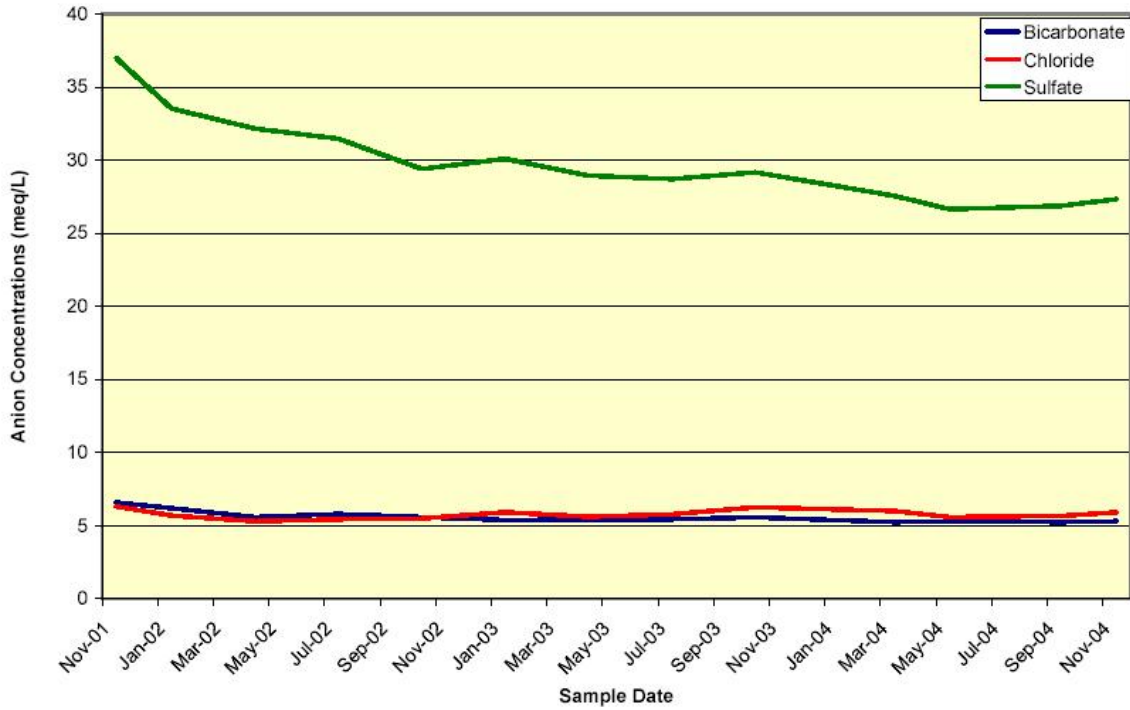
**Figure 5-38: Anion Trend Data for the Jeff 5 MW-3**



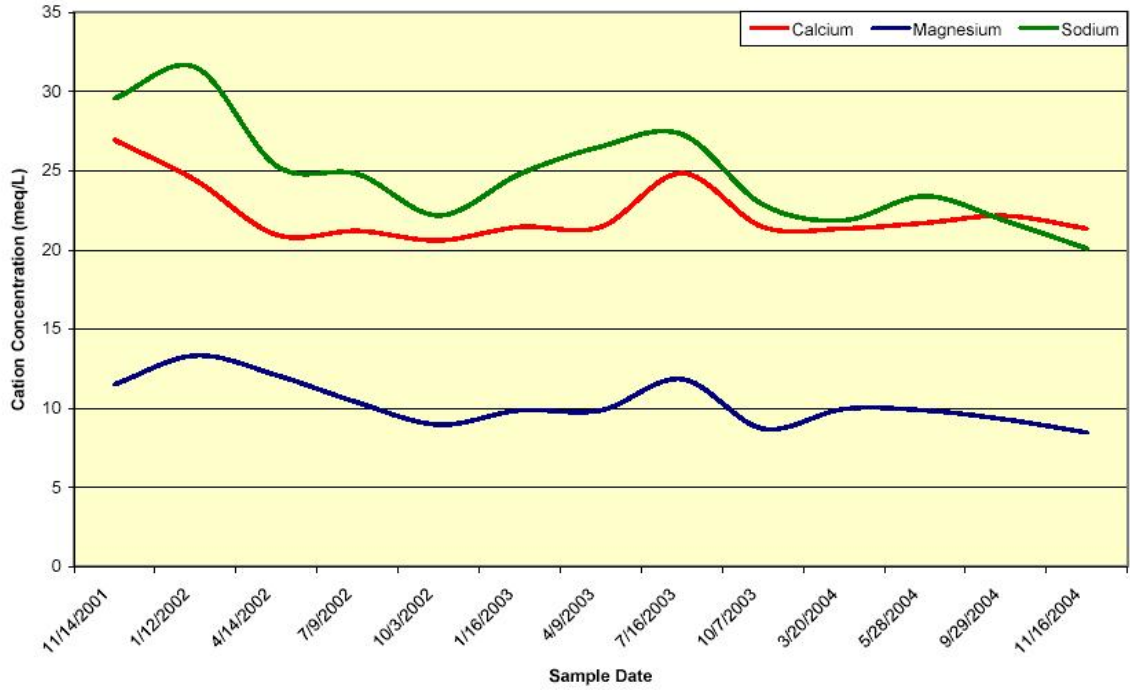
**Figure 5-39: Anion Trend Data for the Jeff 5 MW-4**



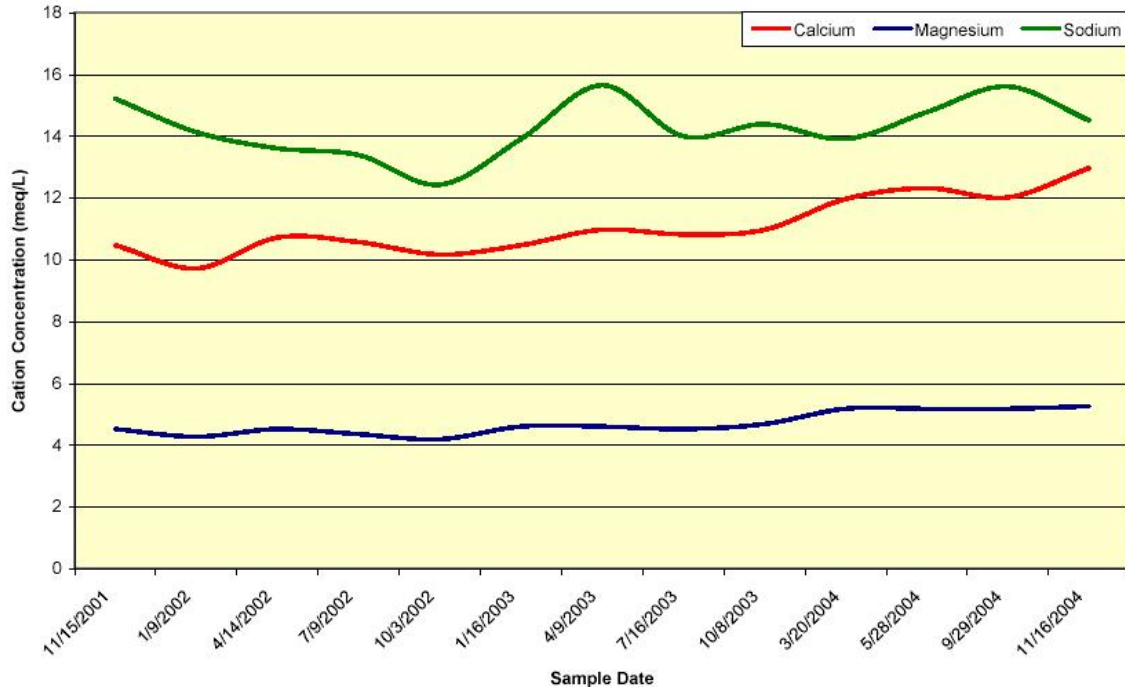
**Figure 5-40: Anion Trend Data for the Jeff 5 MW-5**



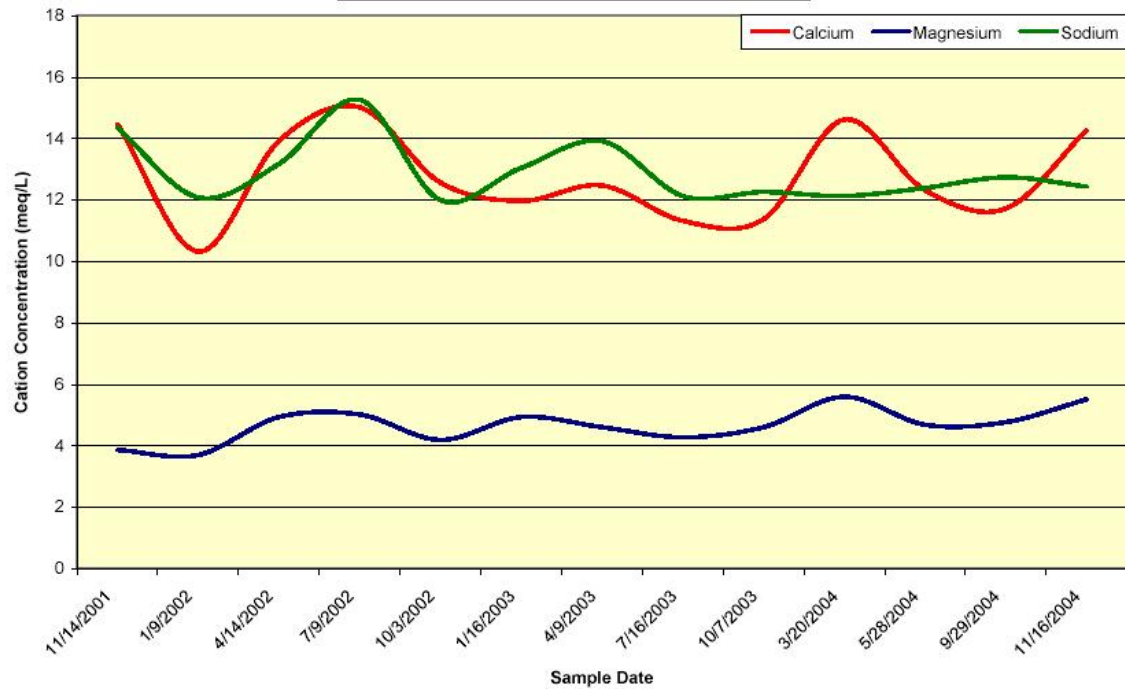
**Figure 5-41: Cation Trend Data for the Jeff 5 MW-2**



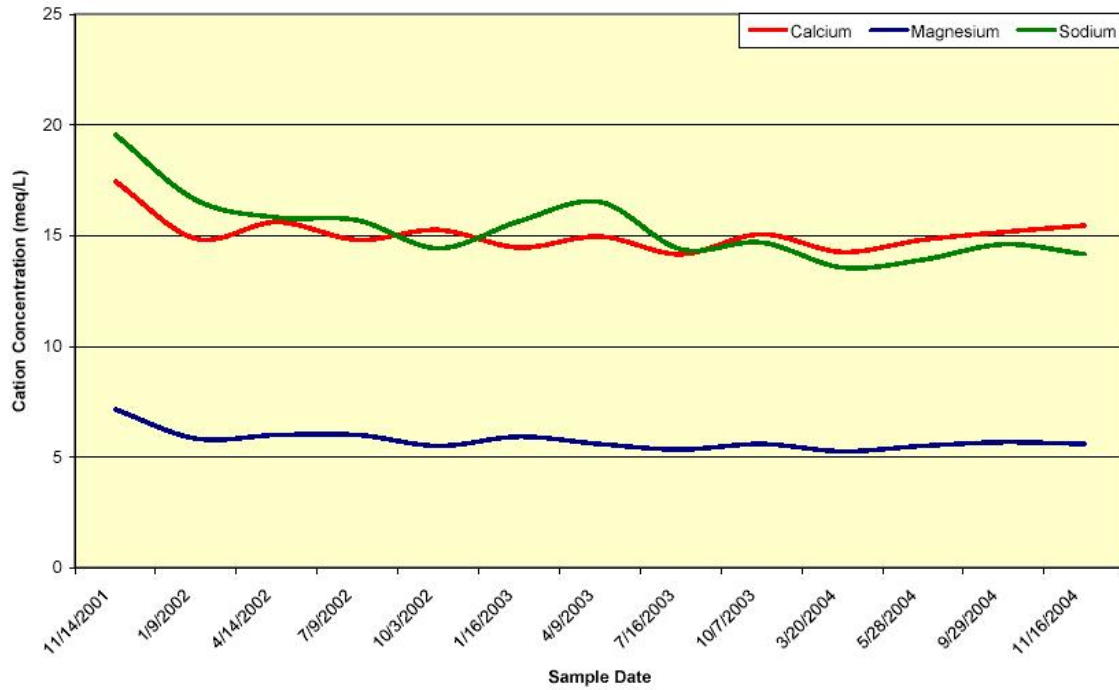
**Figure 5-42: Cation Trend Data for the Jeff 5 MW-3**



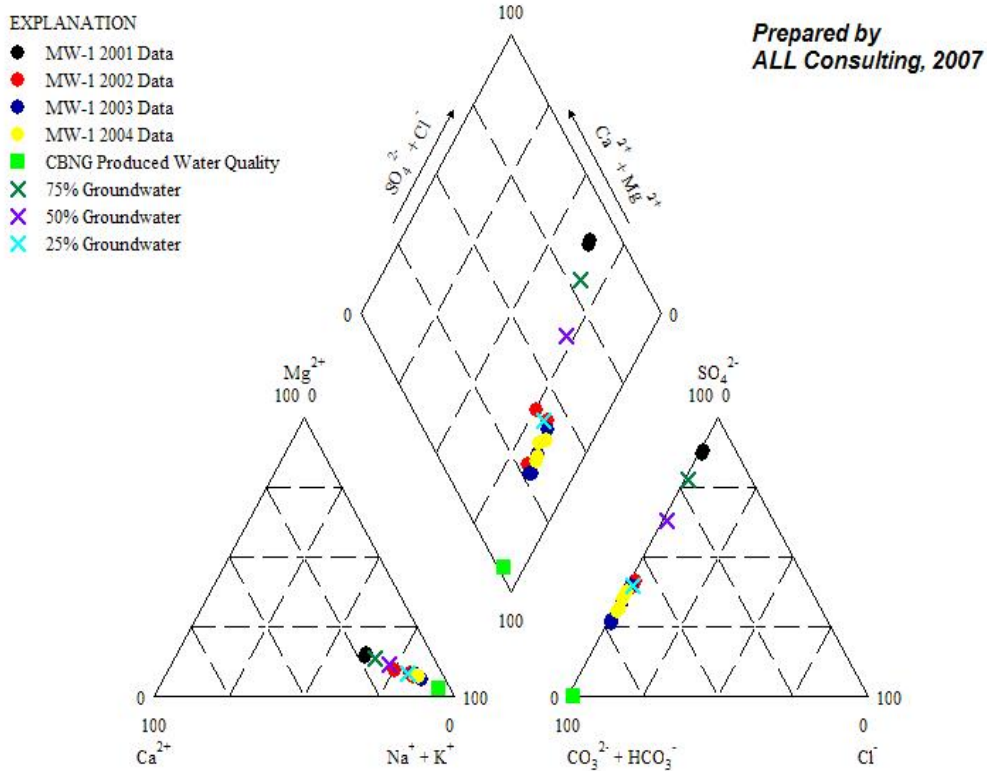
**Figure 5-43: Cation Trend Data for the Jeff 5 MW-4**



**Figure 5-44: Cation Trend Data for the Jeff 5 MW-5**

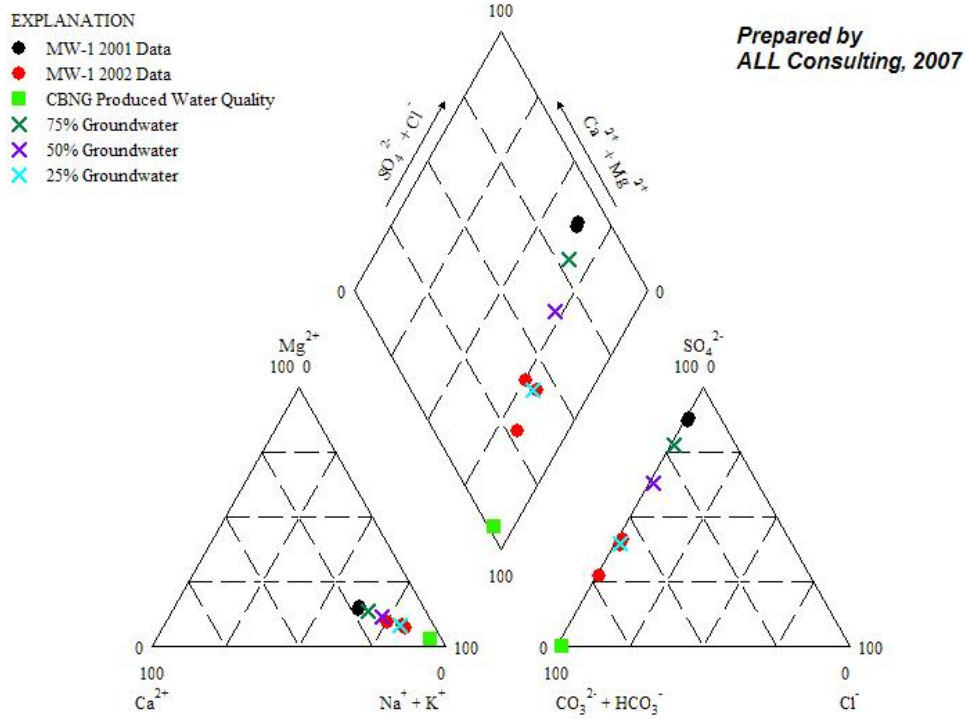


**Figure 5-45: Piper Plot of Water Samples Collected from Jeff 6 MW-1**

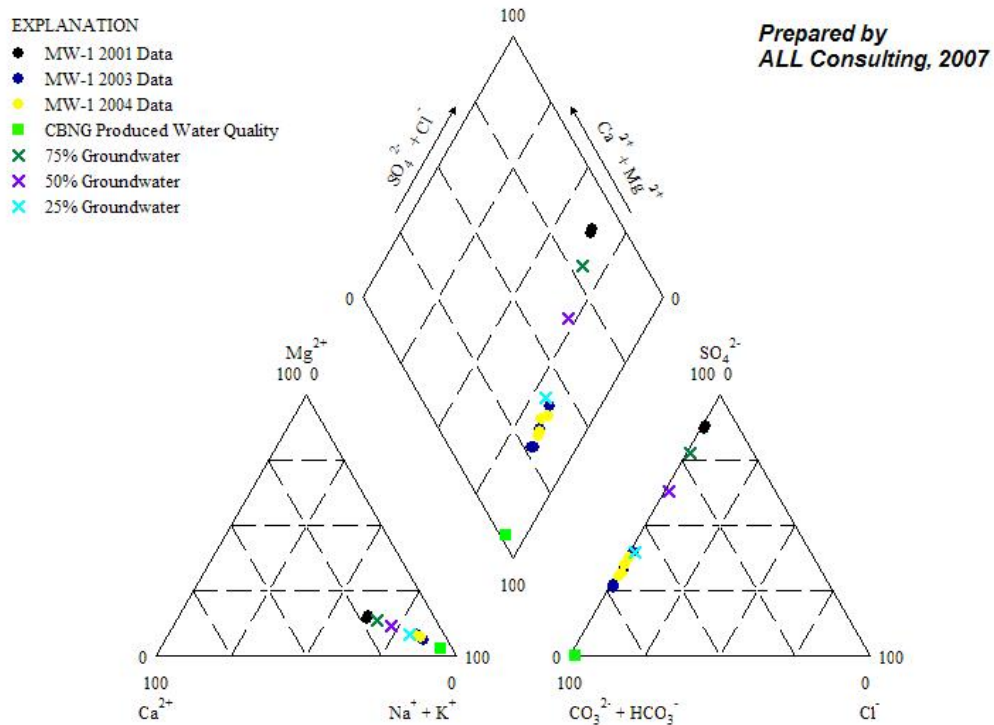




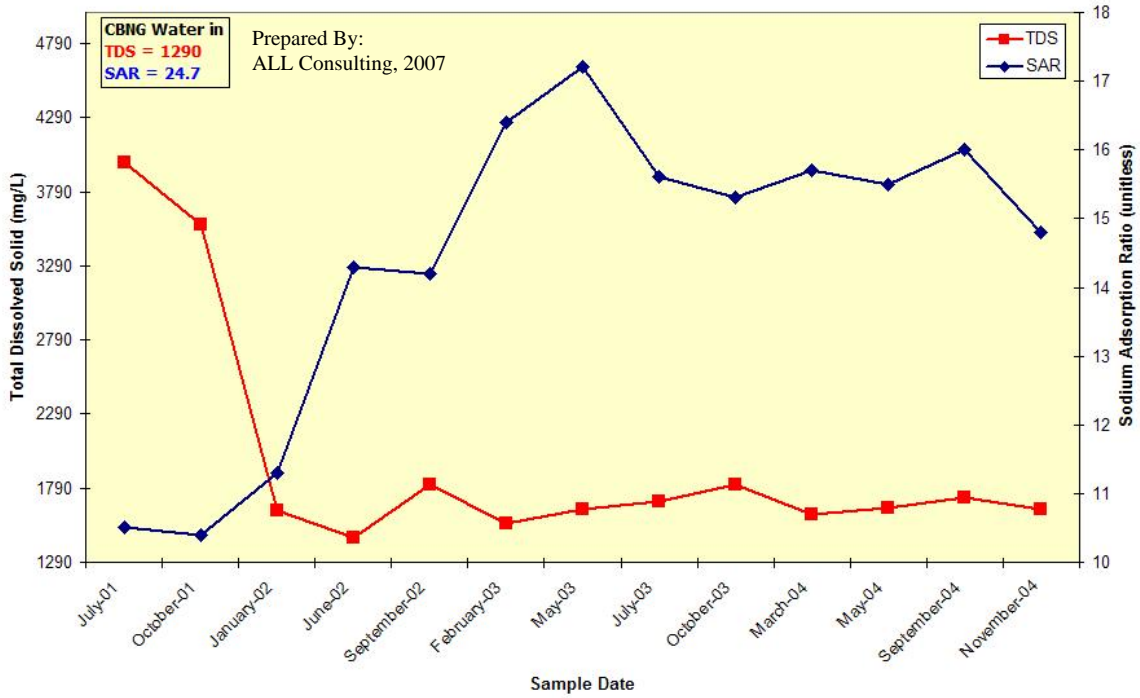
**Figure 5-46: Piper Plot for Jeff 6 MW-1 Years 2001-2002**



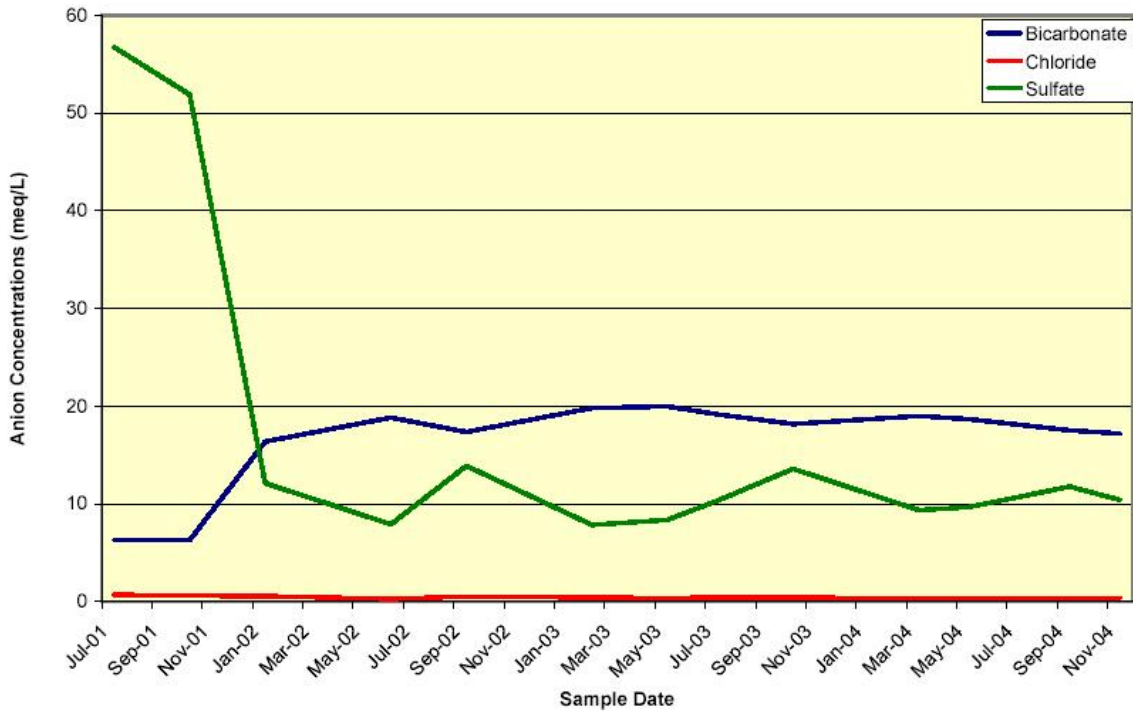
**Figure 5-47: Piper Plot for Jeff 6 MW-1 Years 2003-2004**



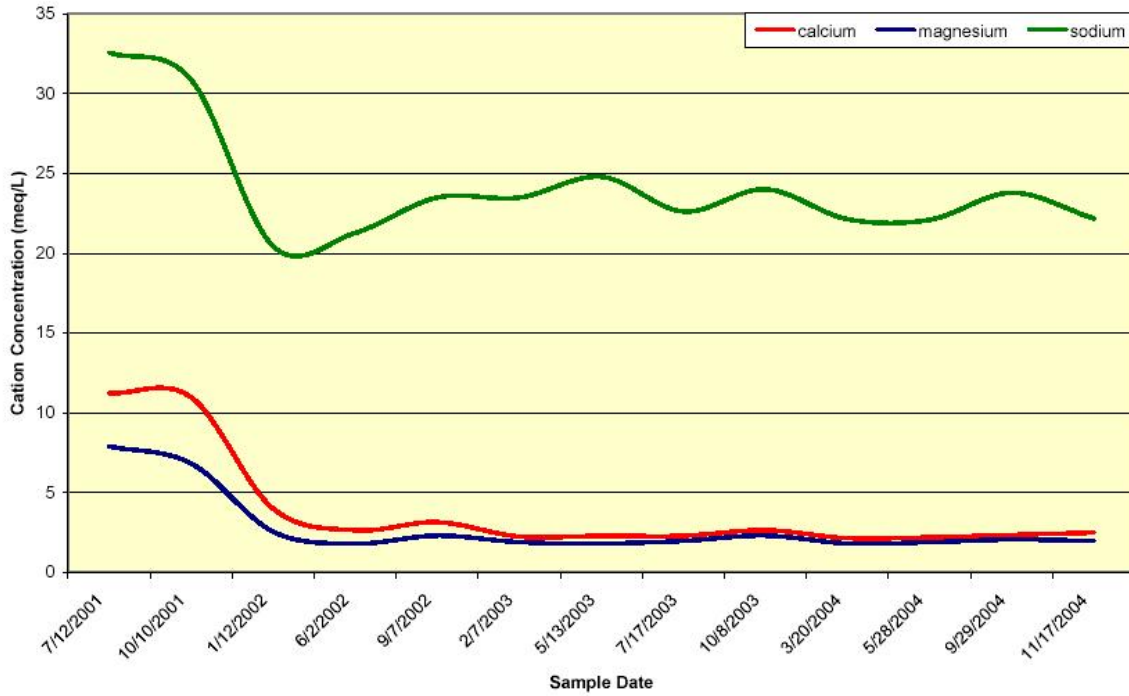
**Figure 5-48: SAR and TDS Trends for Jeff 6 MW-1**



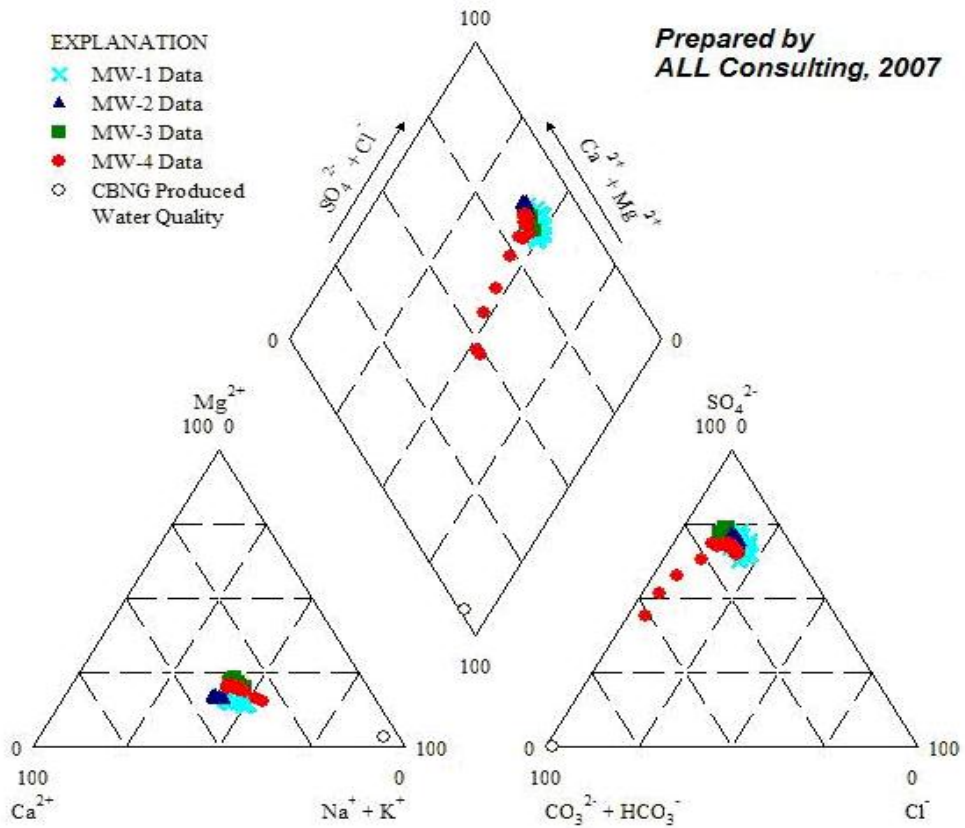
**Figure 5-49: Anion Trend Data for the Jeff 6 MW-1**



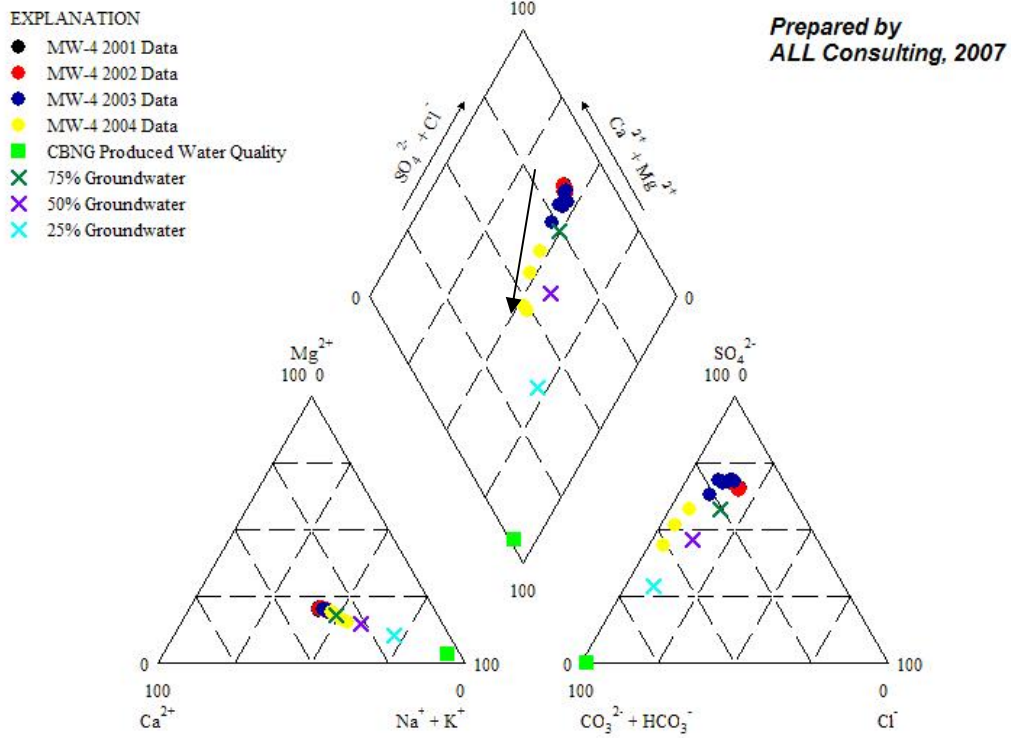
**Figure 5-50: Cation Trend Data for the Jeff 6 MW-1**



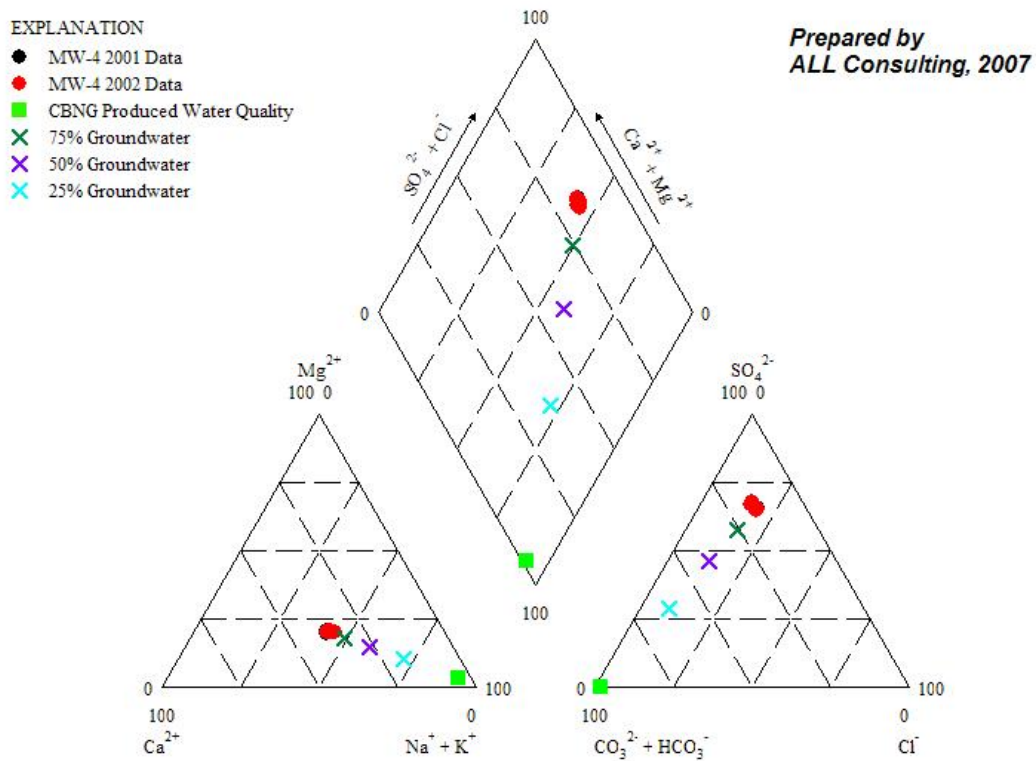
**Figure 5-51: Piper Plot of Water Samples Collected from Jeff 7 Monitoring Wells**



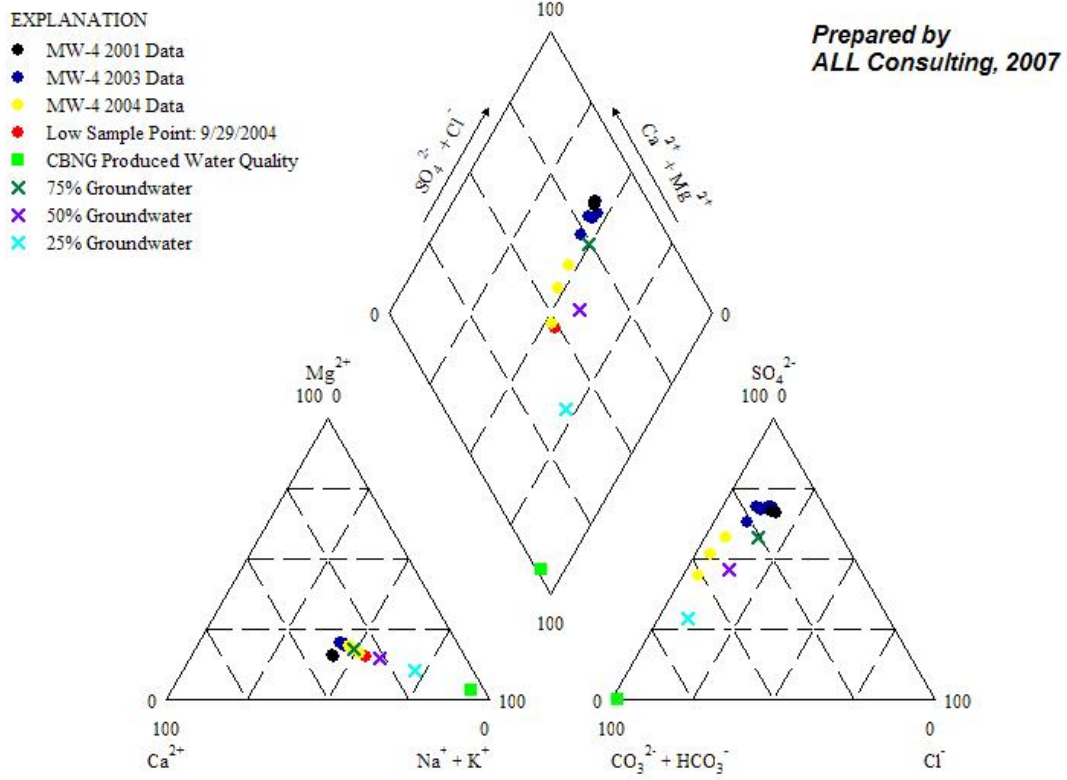
**Figure 5-52: Piper Plot for Jeff 7 MW-4**



**Figure 5-53: Piper Plot for Jeff 7 MW-4 Years 2001-2002**

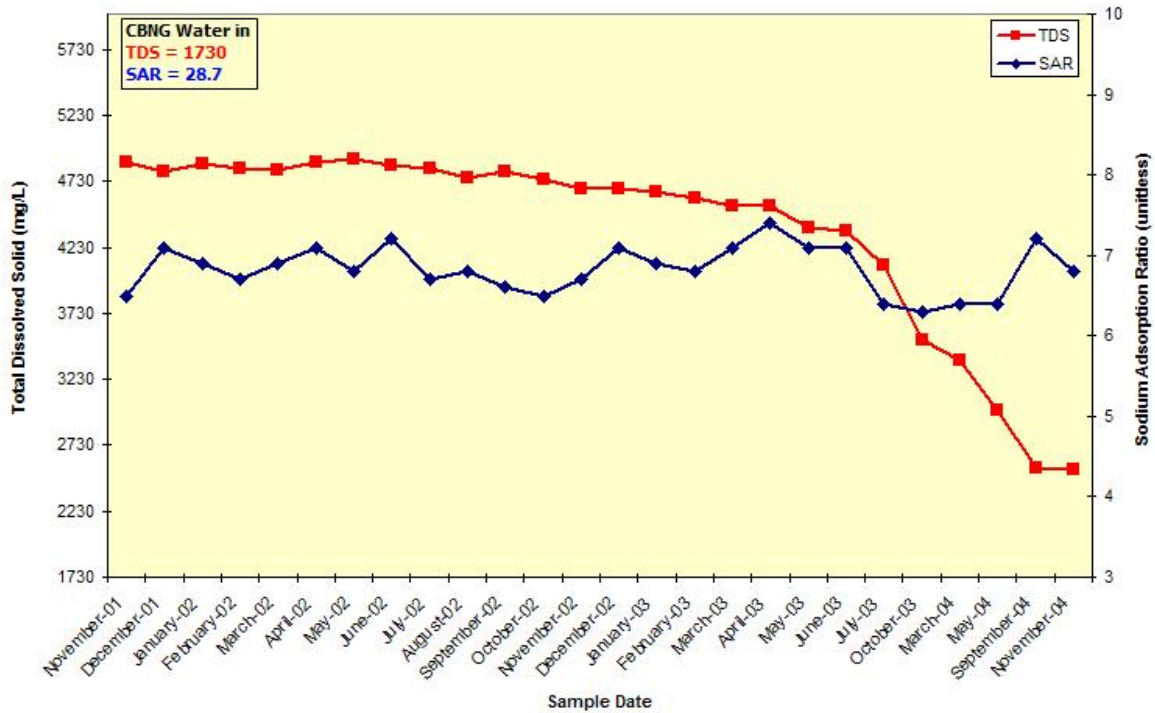


**Figure 5-54: Piper Plot for Jeff 7 MW-4 Years 2003-2004**



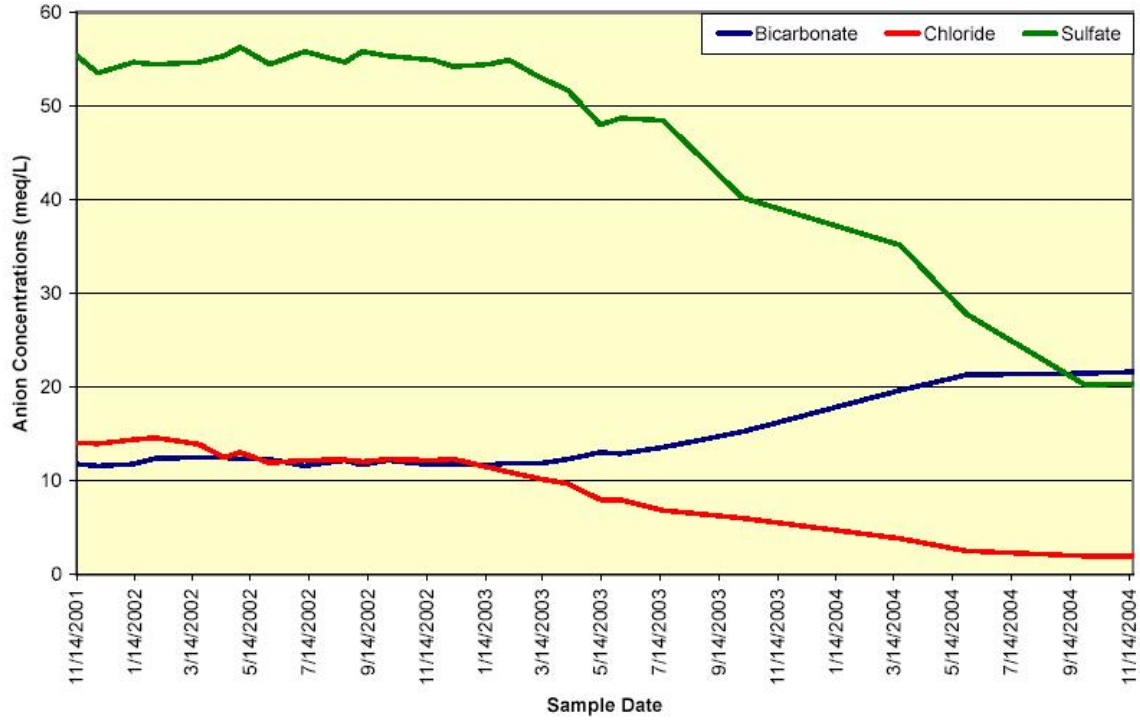
**Figure 5-55: SAR and TDS Trends for Jeff 7 MW-4**

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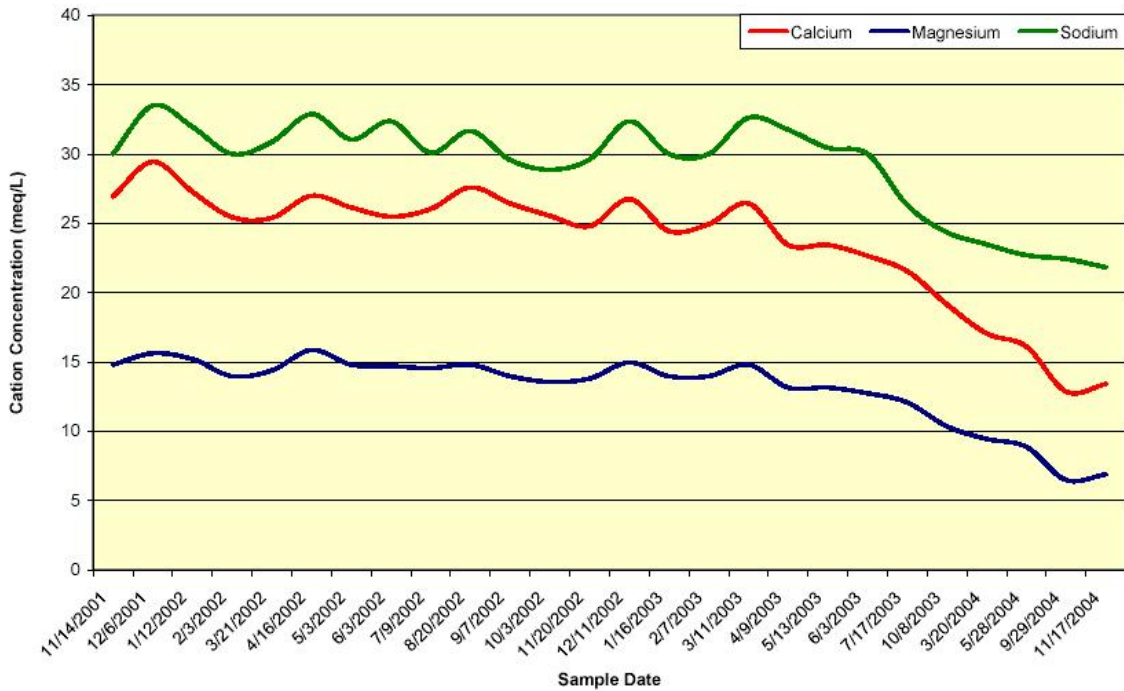




**Figure 5-56: Anion Trend Data for the Jeff 7 MW-4**

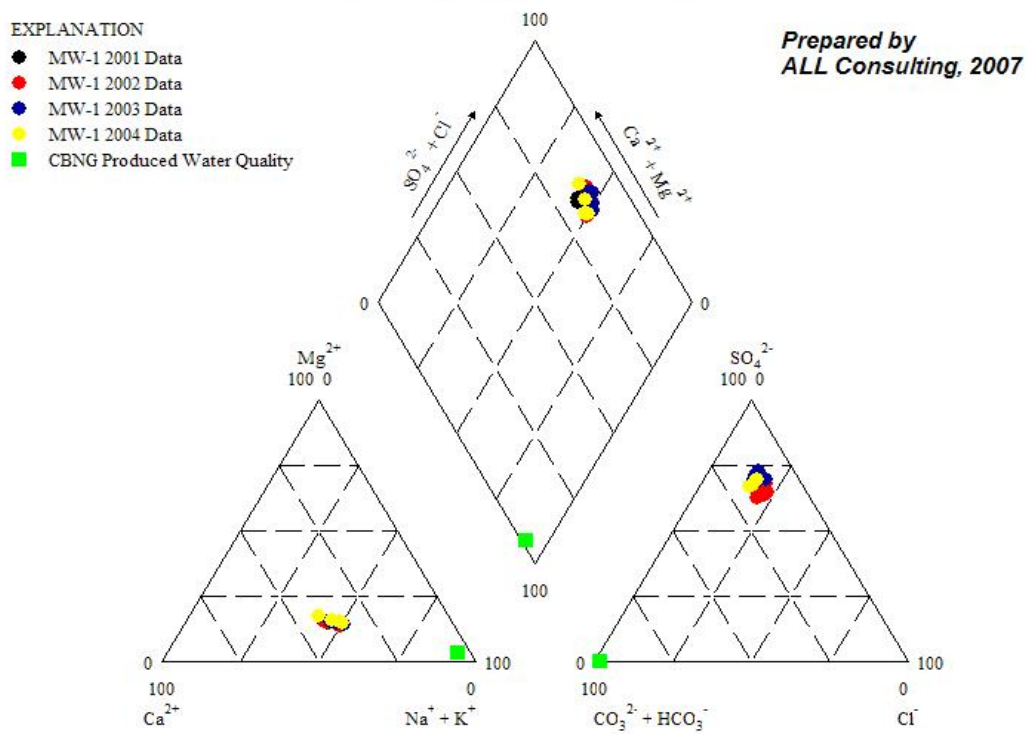


**Figure 5-57: Cation Trend Data for the Jeff 7 MW-4**

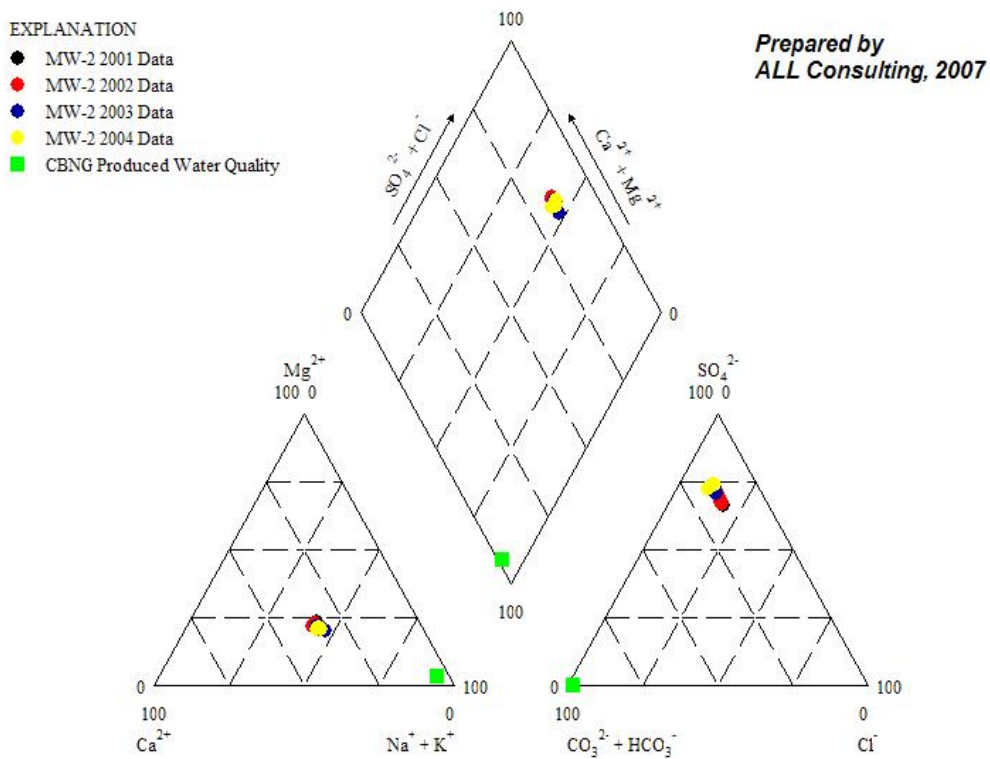




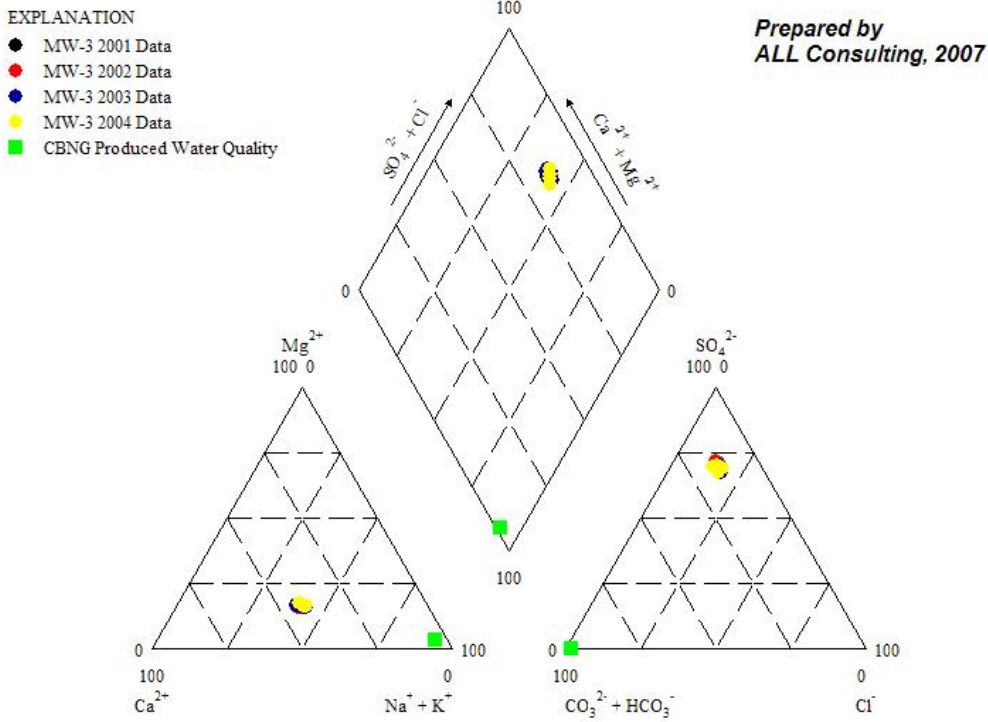
**Figure 5-58: Piper Plot for Jeff 7 MW-1**



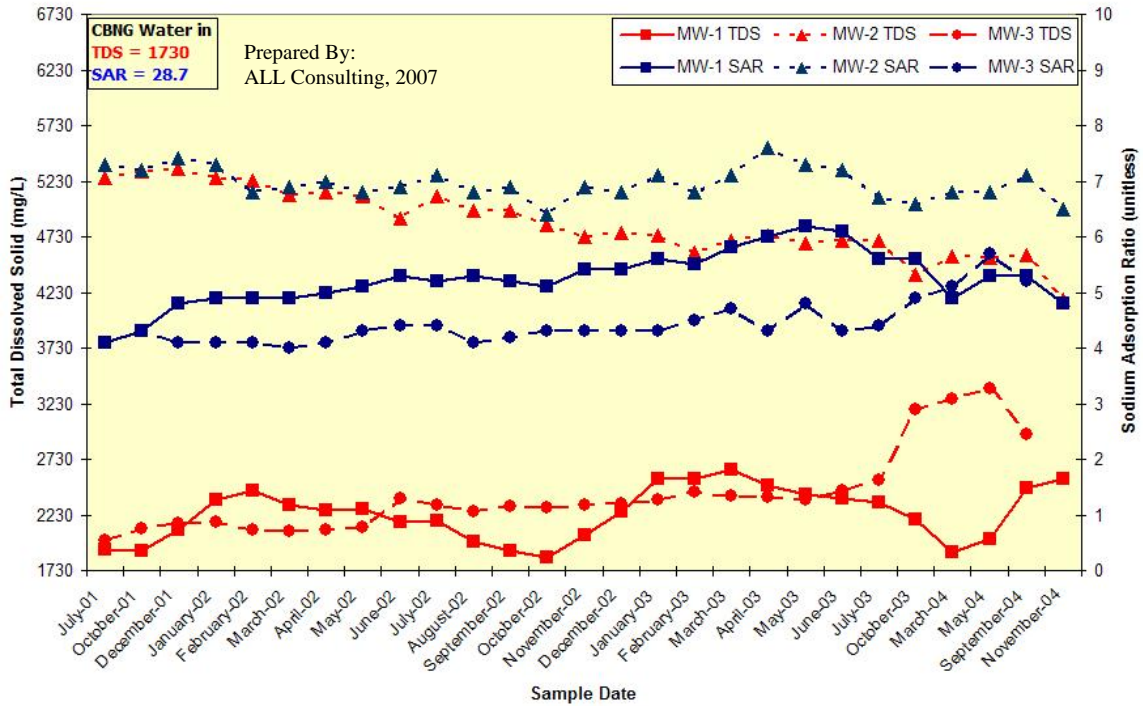
**Figure 5-59: Piper Plot for Jeff 7 MW-2**



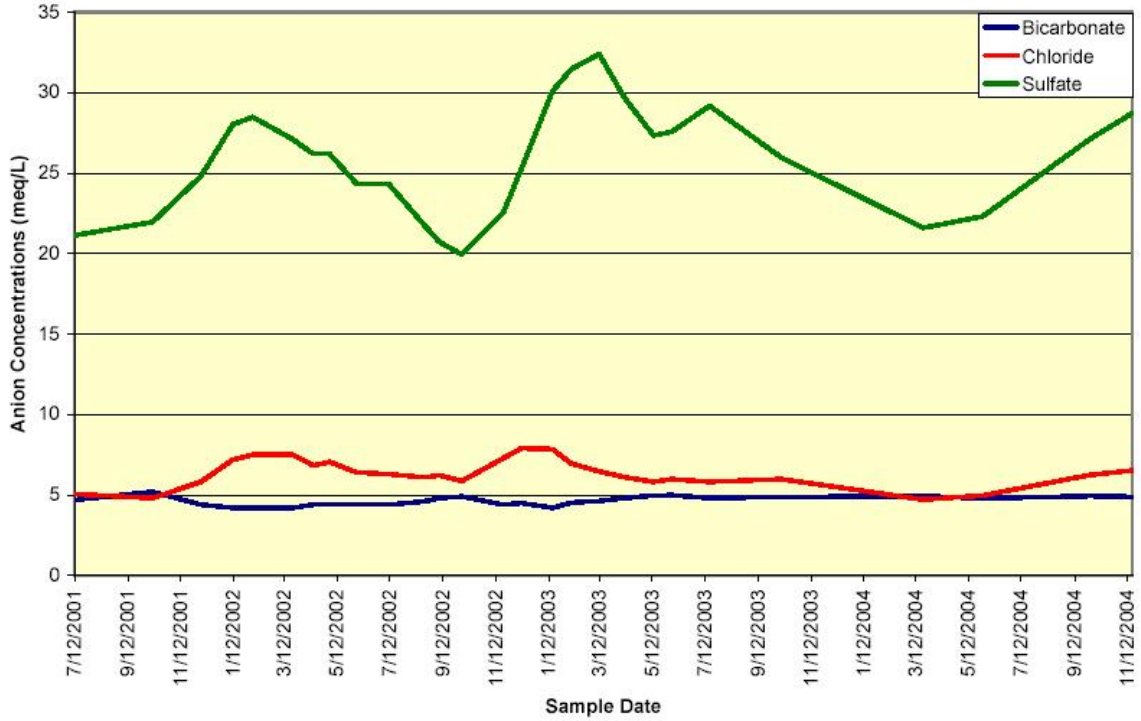
**Figure 5-60: Piper Plot for Jeff 7 MW-3**



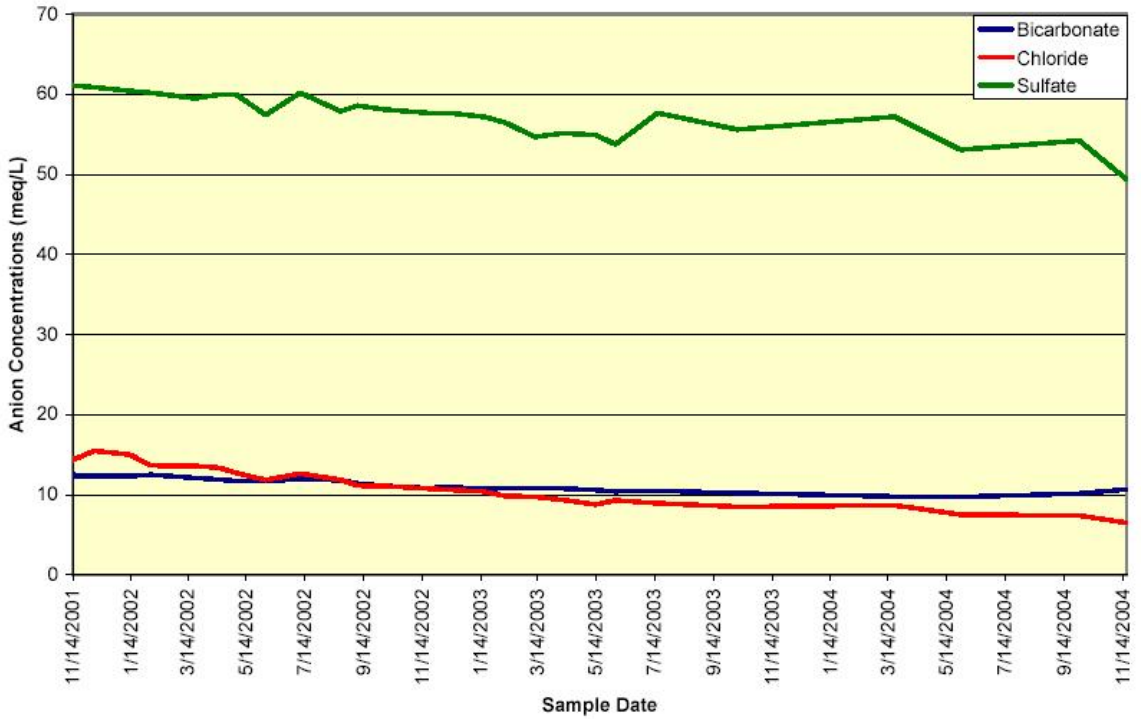
**Figure 5-61: SAR and TDS Trends for Jeff 7 MW-1, MW-2, and MW-3**



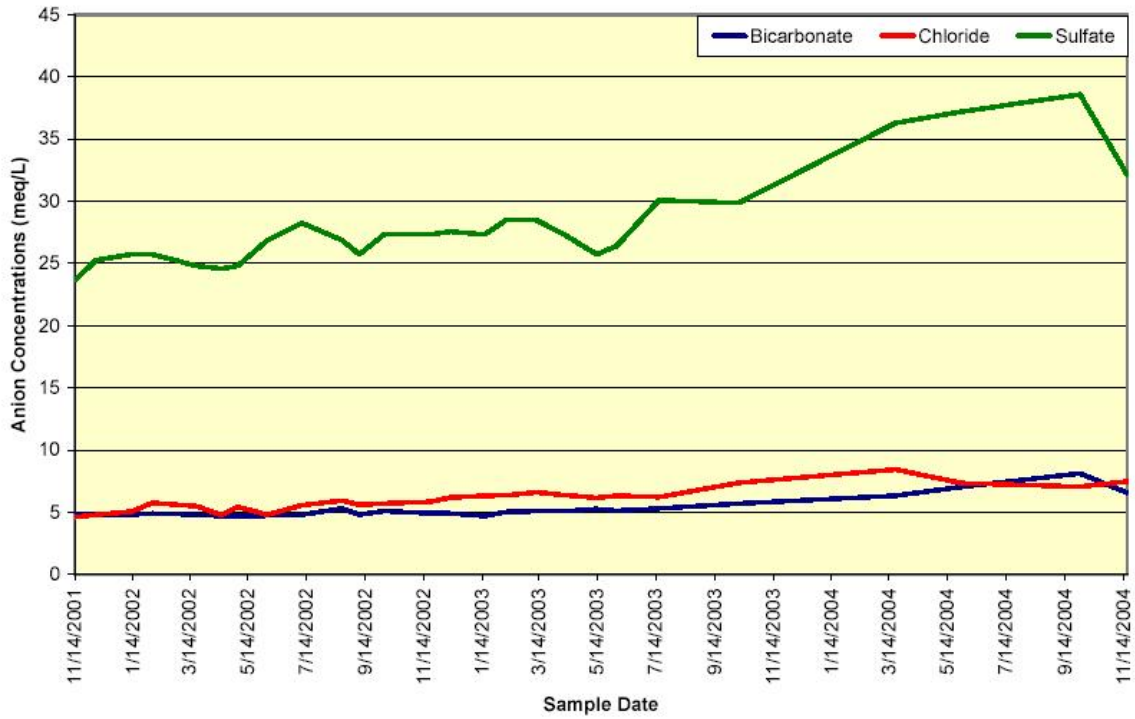
**Figure 5-62: Anion Trend Data for the Jeff 7 MW-1**



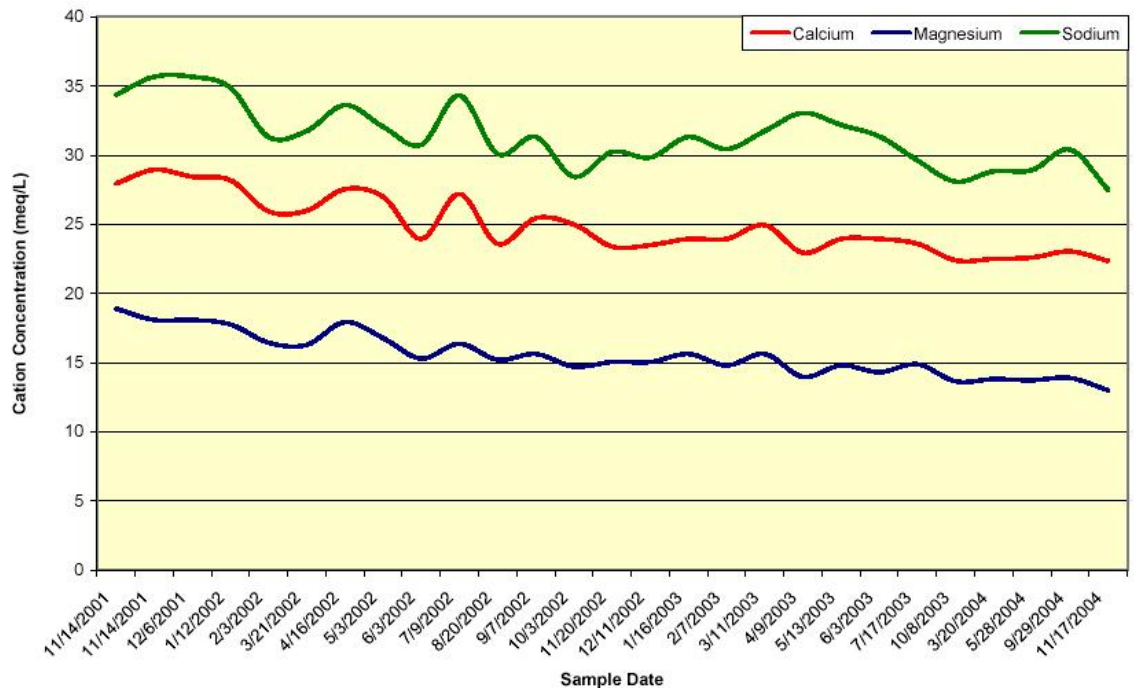
**Figure 5-63: Anion Trend Data for the Jeff 7 MW-2**



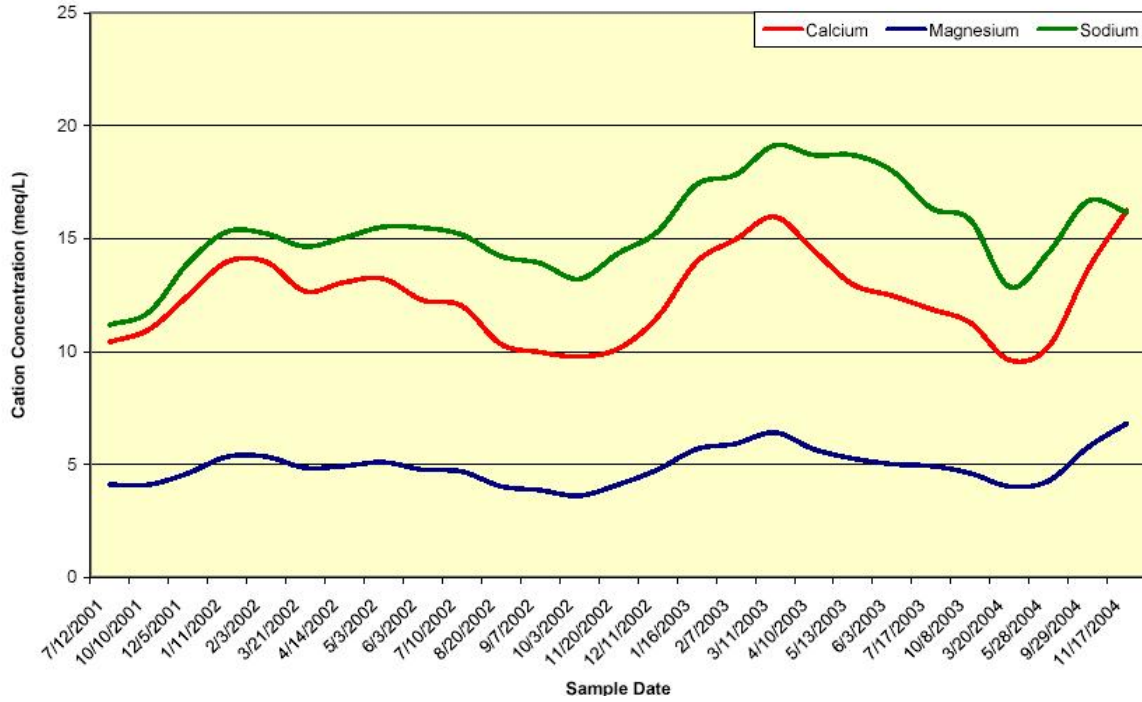
**Figure 5-64: Anion Trend Data for the Jeff 7 MW-3**



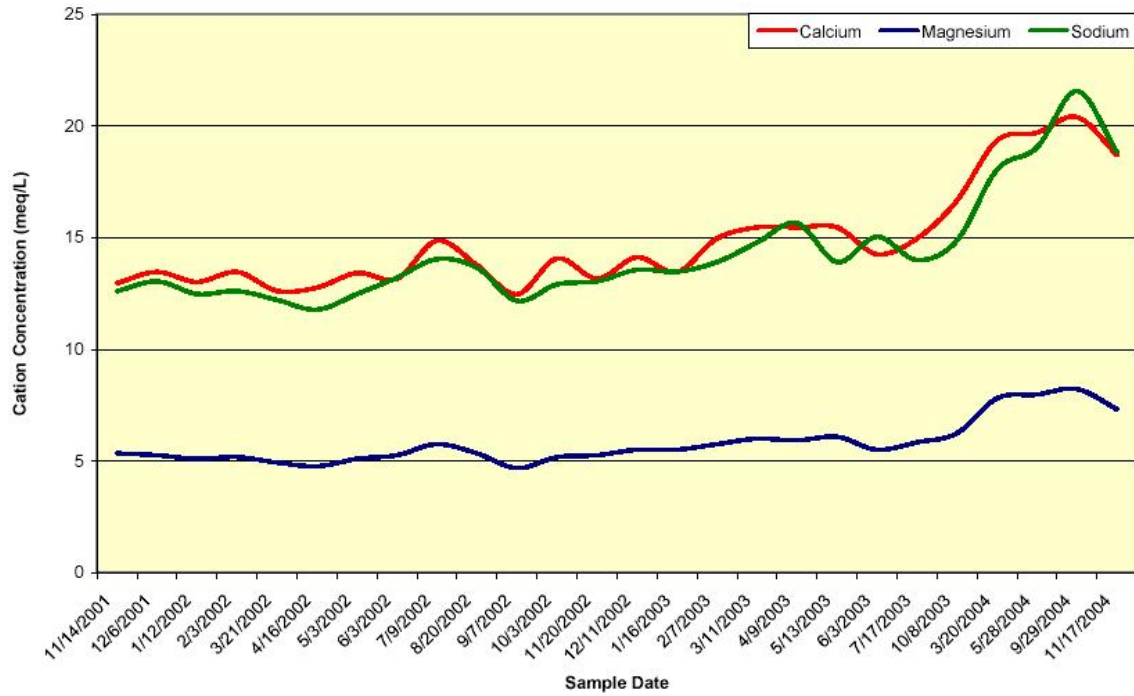
**Figure 5-65: Cation Trend Data for the Jeff 7 MW-1**



**Figure 5-66: Cation Trend Data for the Jeff 7 MW-2**

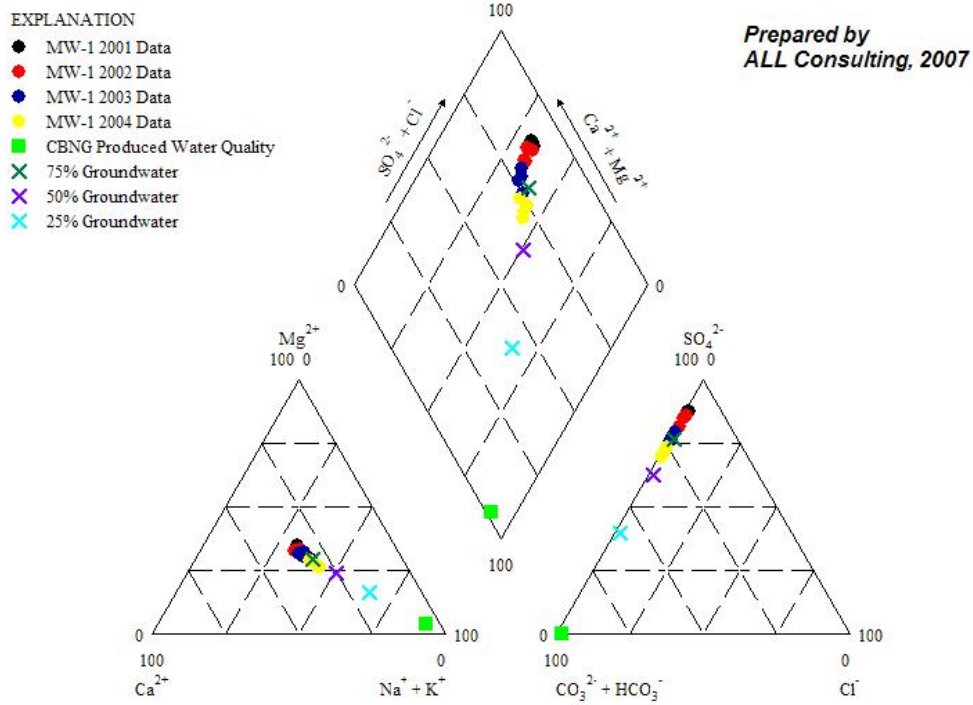


**Figure 5-67: Cation Trend Data for the Jeff 7 MW-3**

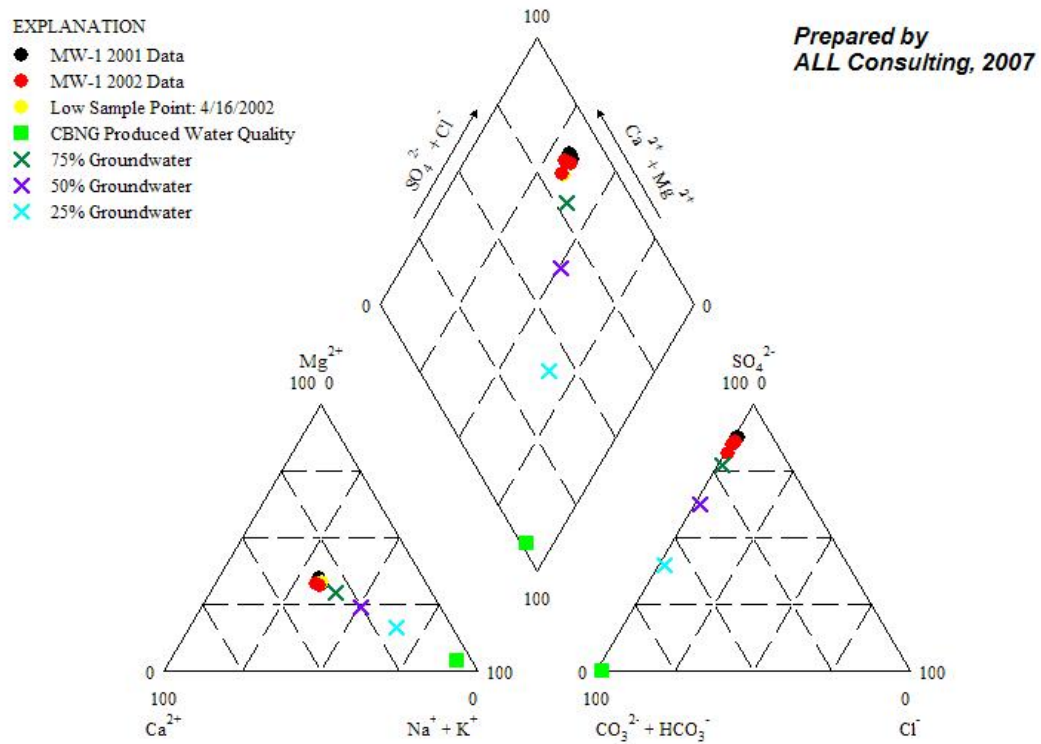




**Figure 5-68: Piper Diagram of Water Samples Collected from the Phil's Pond MW-1**

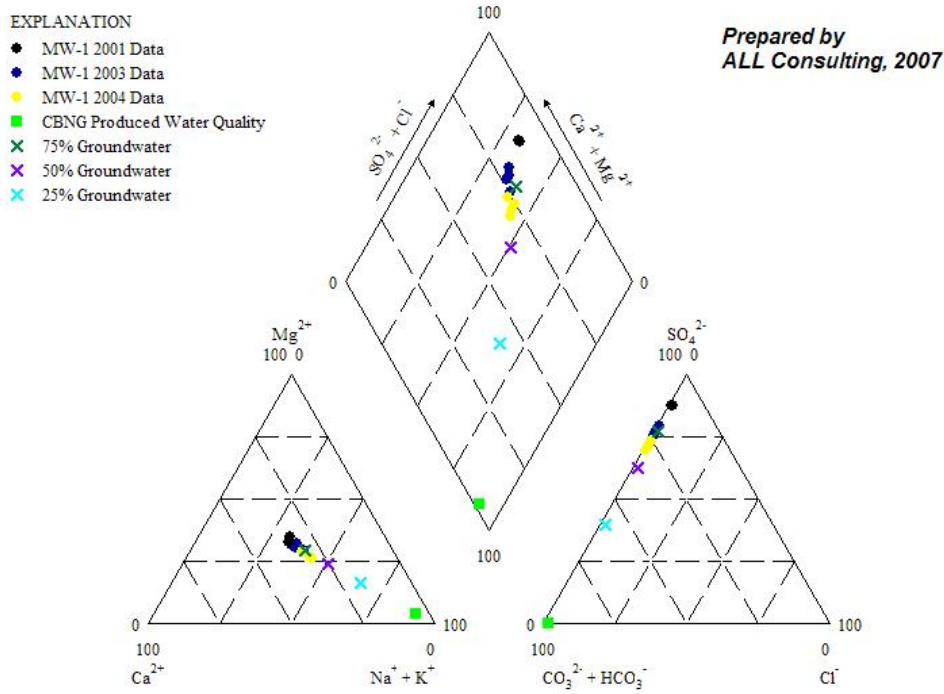


**Figure 5-69: Piper Plot for Phil's Pond MW-1 Year 2001-2002**

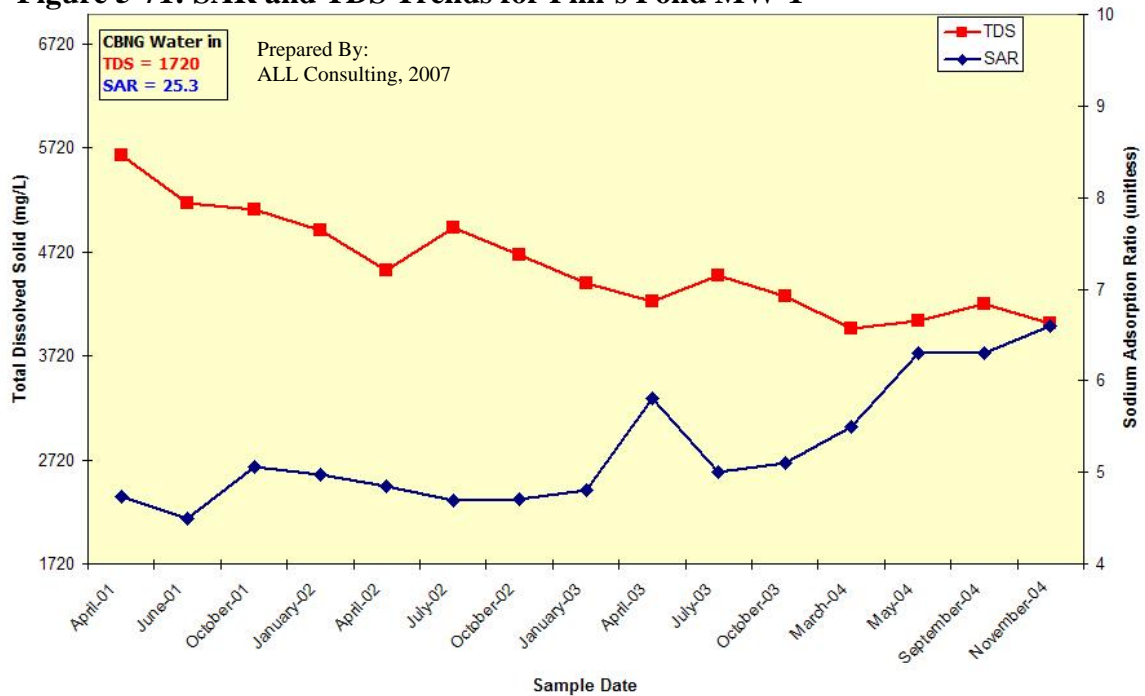




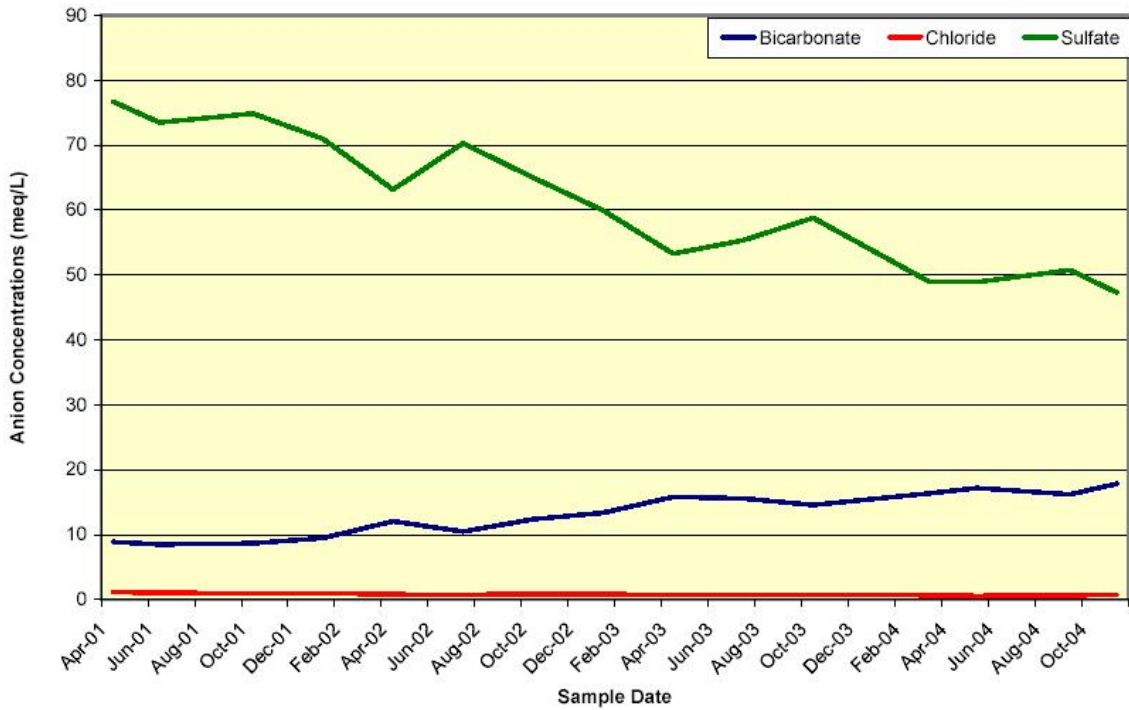
**Figure 5-70: Piper Plot for Phil's Pond MW-1 Year 2003-2004**



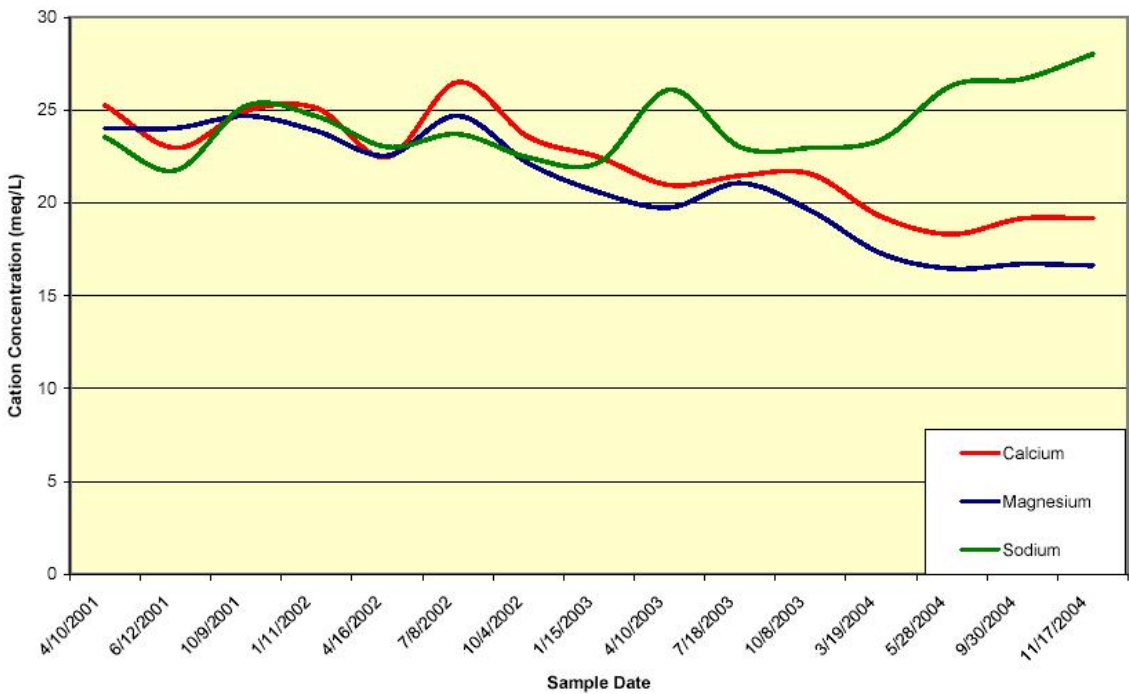
**Figure 5-71: SAR and TDS Trends for Phil's Pond MW-1**



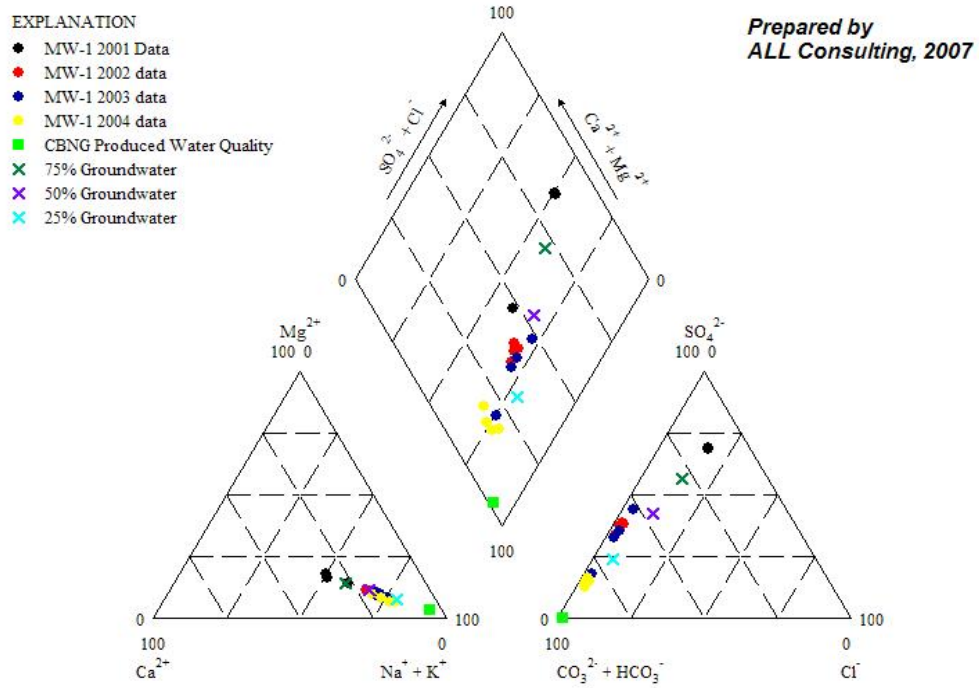
**Figure 5-72: Anion Trend Data for the Phils Pond MW-1**



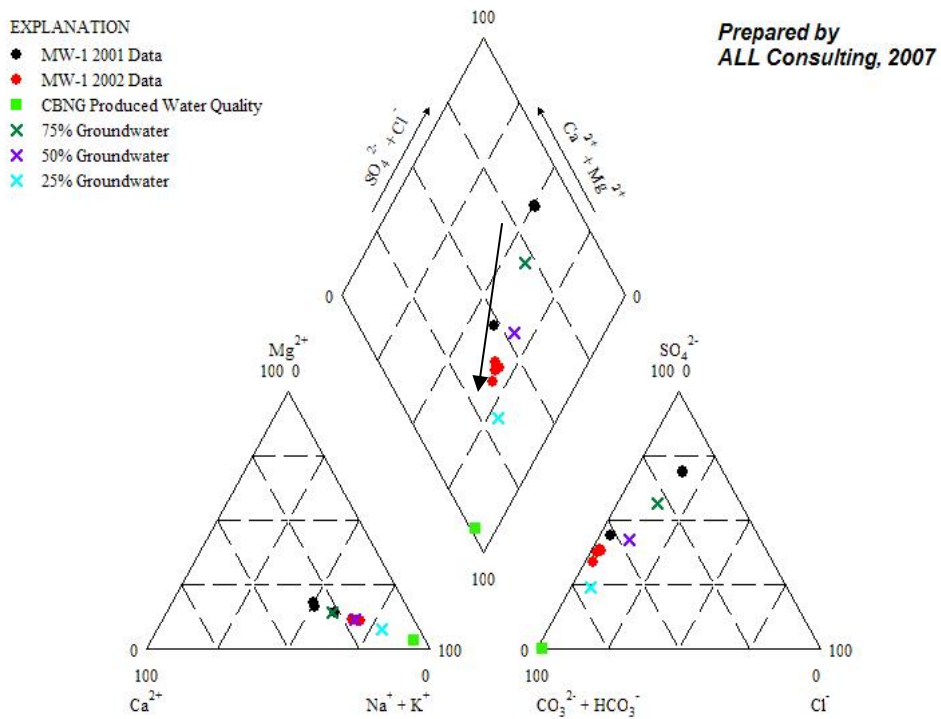
**Figure 5-73: Cation Trend Data for the Phils Pond MW-1**



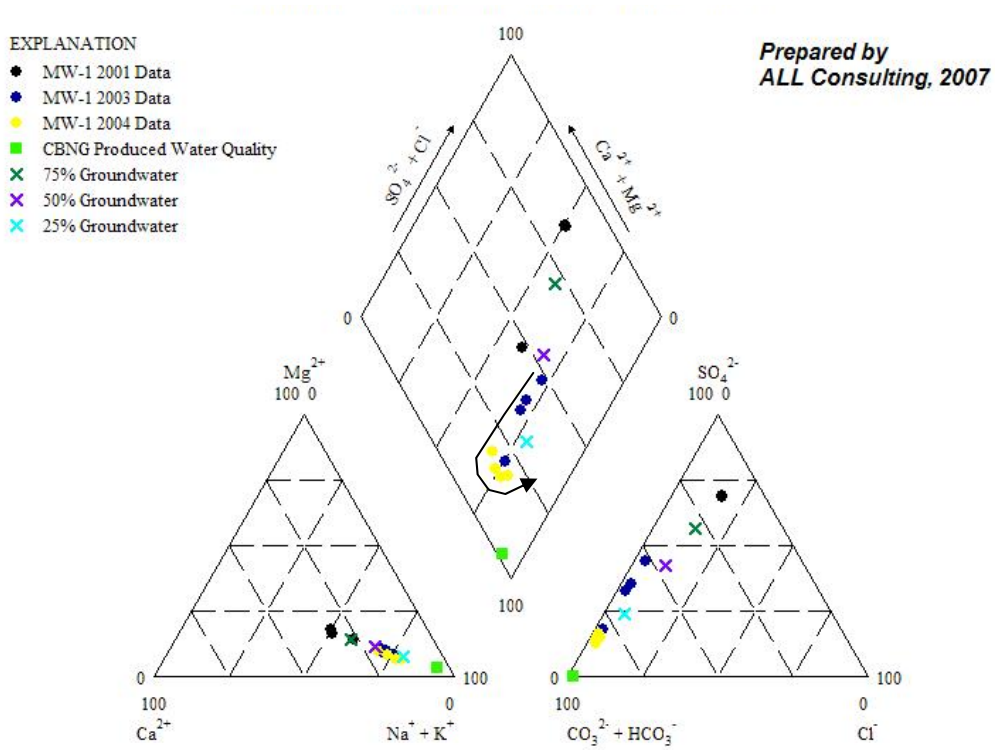
**Figure 5-74: Piper Plot Diagram of Water Samples Collected from the Candida 2 MW-1**



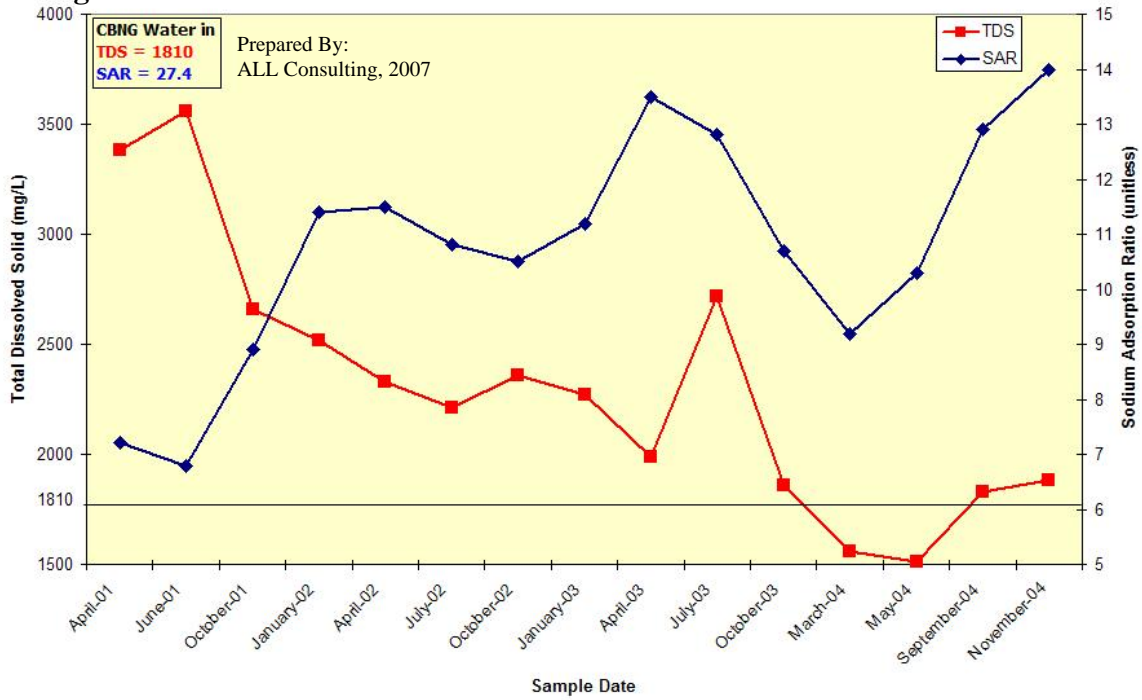
**Figure 5-75: Piper Plot for Candida 2 MW-1 Years 2001-2002**



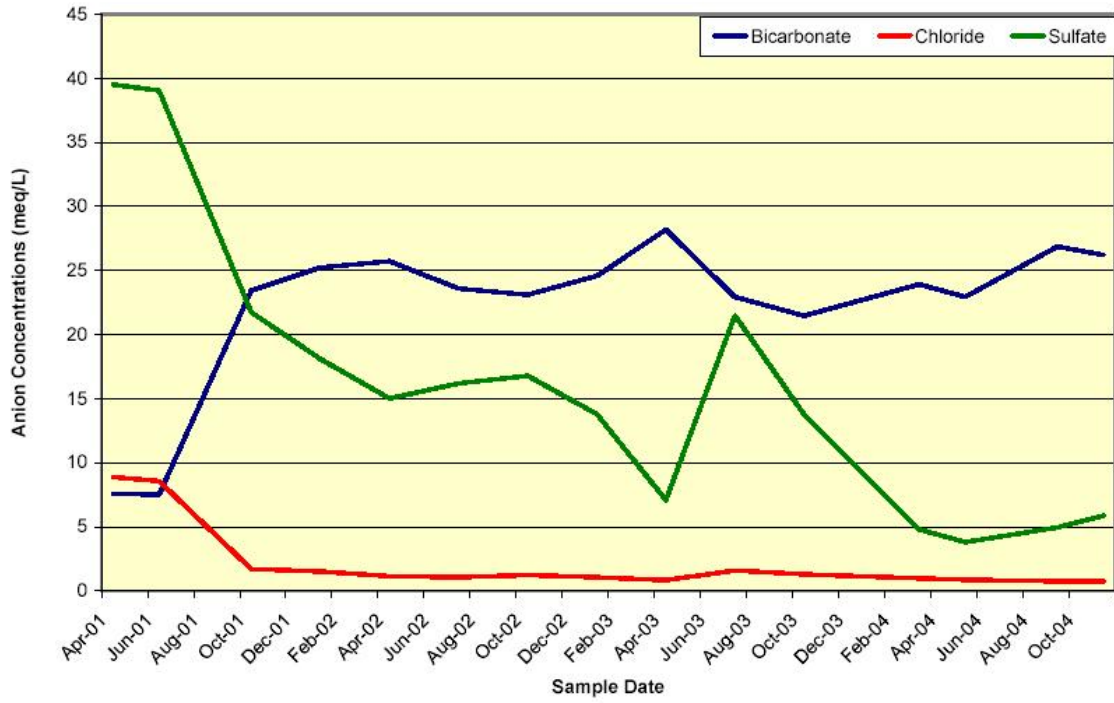
**Figure 5-76: Piper Plot for Candida 2 MW-1 Years 2003-2004**



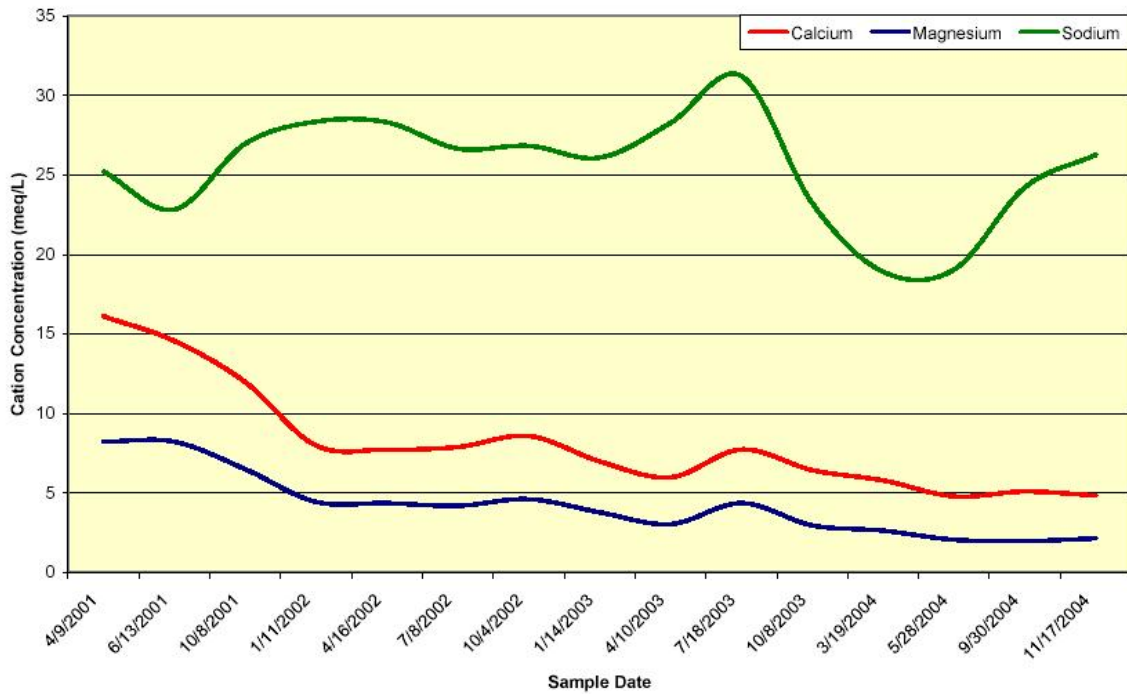
**Figure 5-77: SAR and TDS Trends for Candida 2 MW-1**



**Figure 5-78: Anion Trend Data for the Candida 2 MW-1**

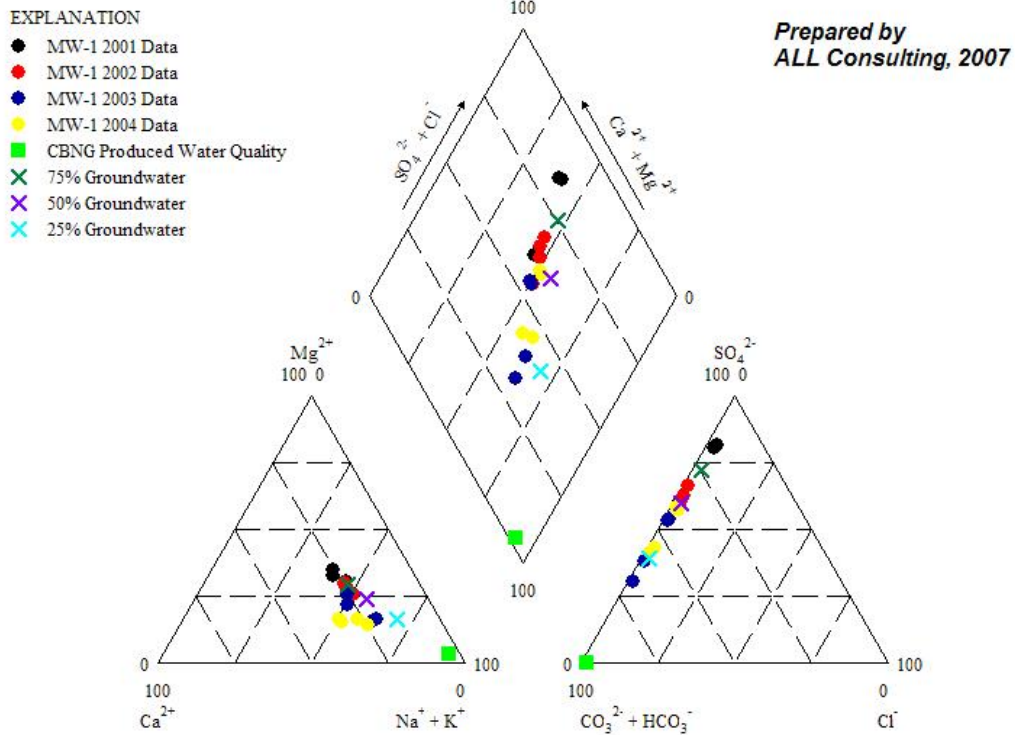


**Figure 5-79: Cation Trend Data for the Candida 2 MW-1**

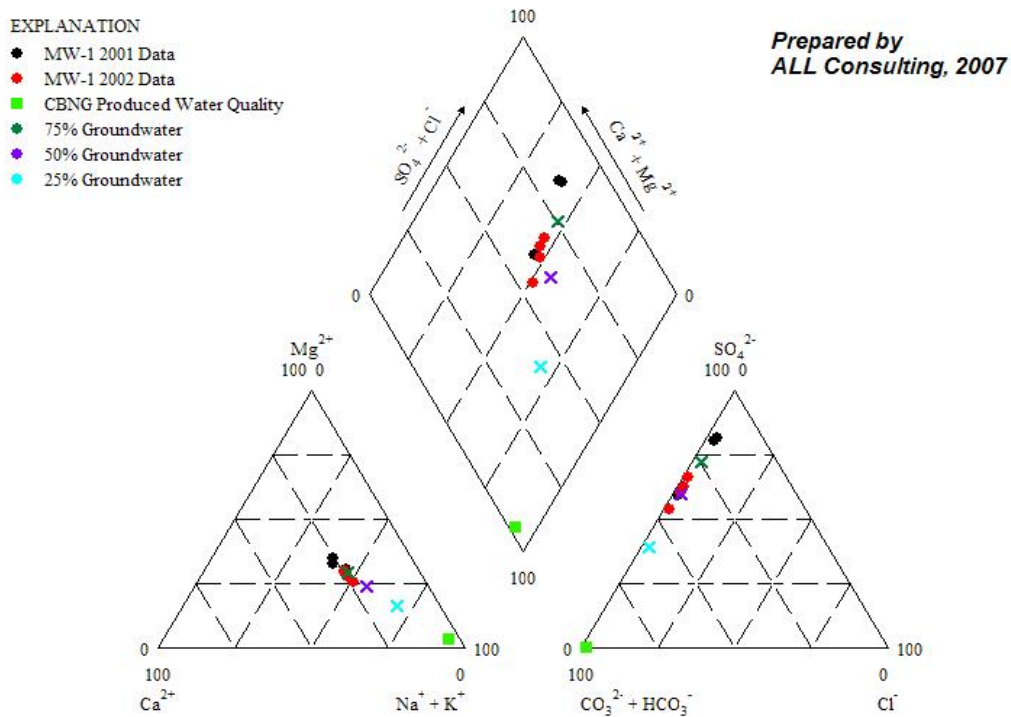




**Figure 5-80: Piper Plot for Water Samples Collected from the Santiago 3 Impoundment Monitoring Wells**

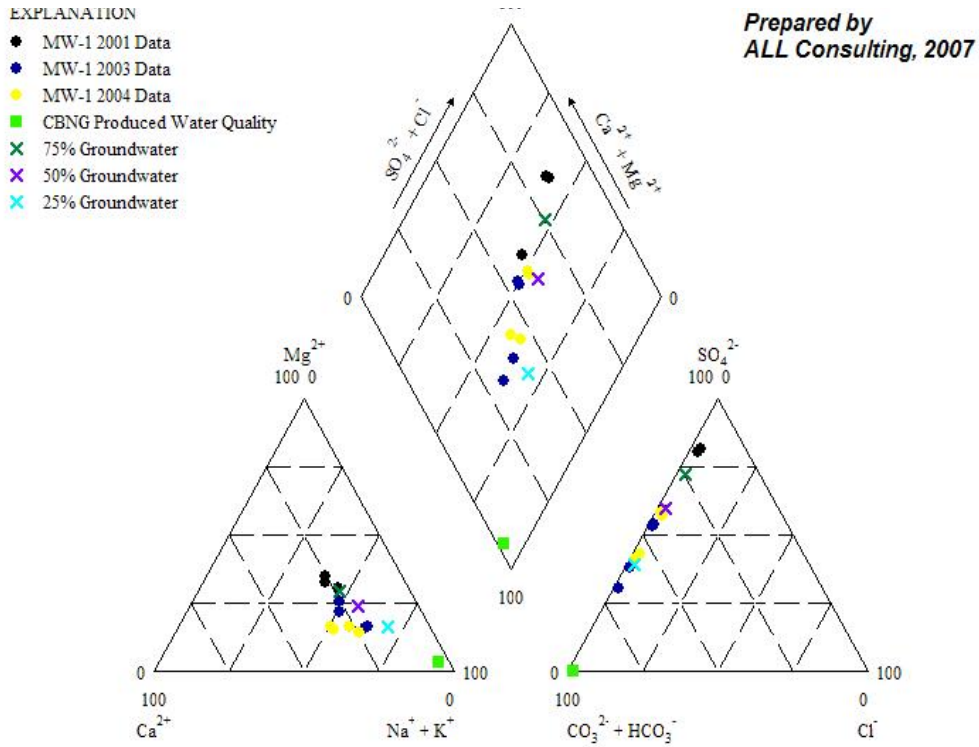


**Figure 5-81: Piper Plot for Santiago 3 MW-1 Years 2001-2002**

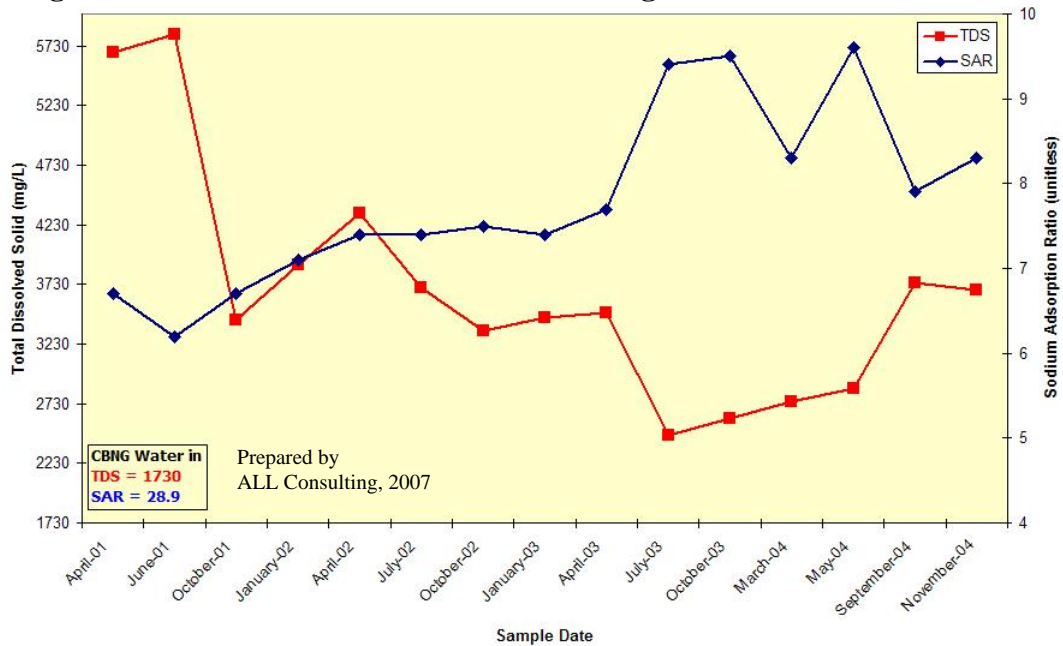




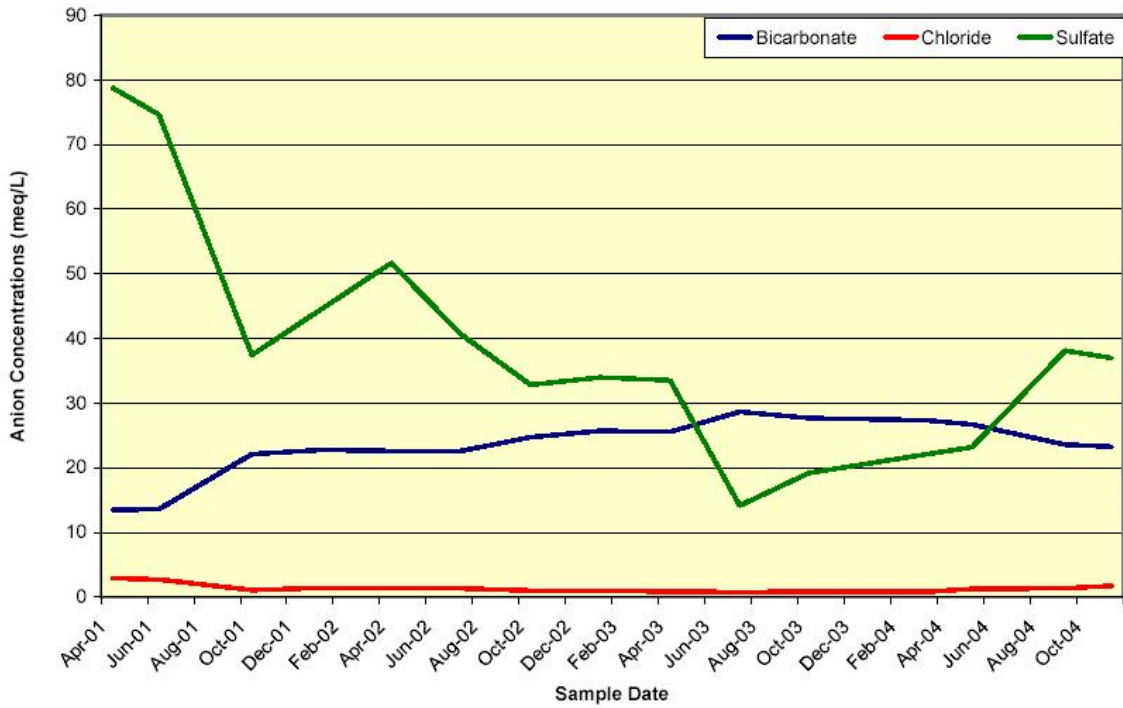
**Figure 5-82: Piper Plot for Santiago 3 MW-1 Years 2003-2004**



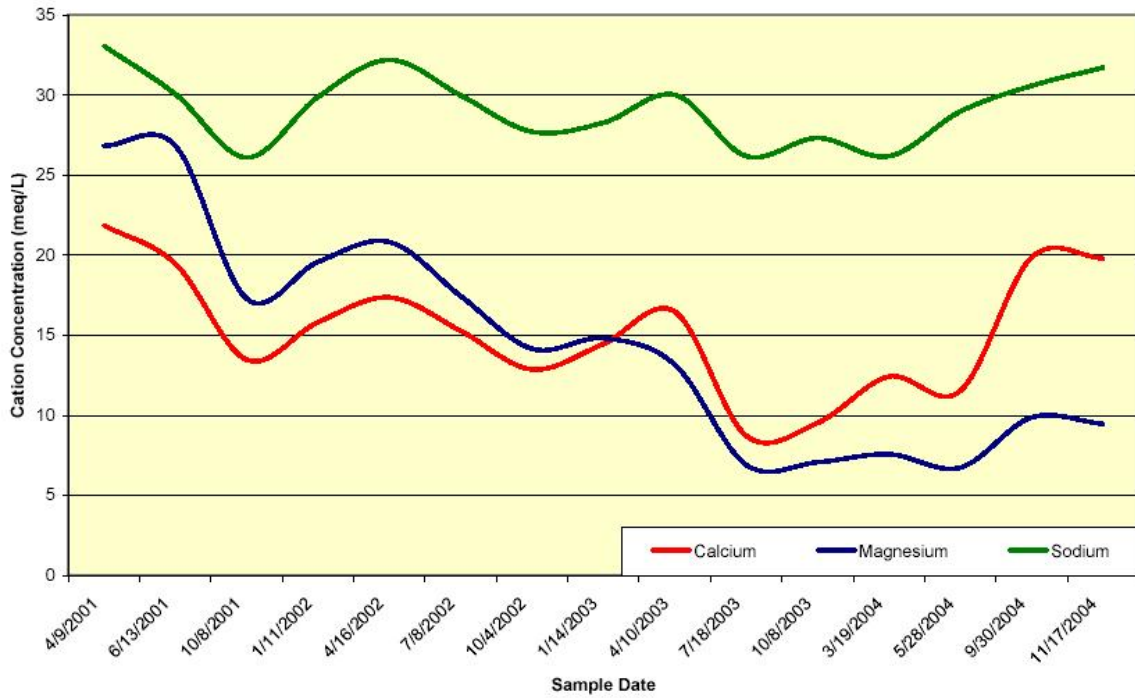
**Figure 5-83: SAR and TDS Trends for Santiago 3 MW-1**



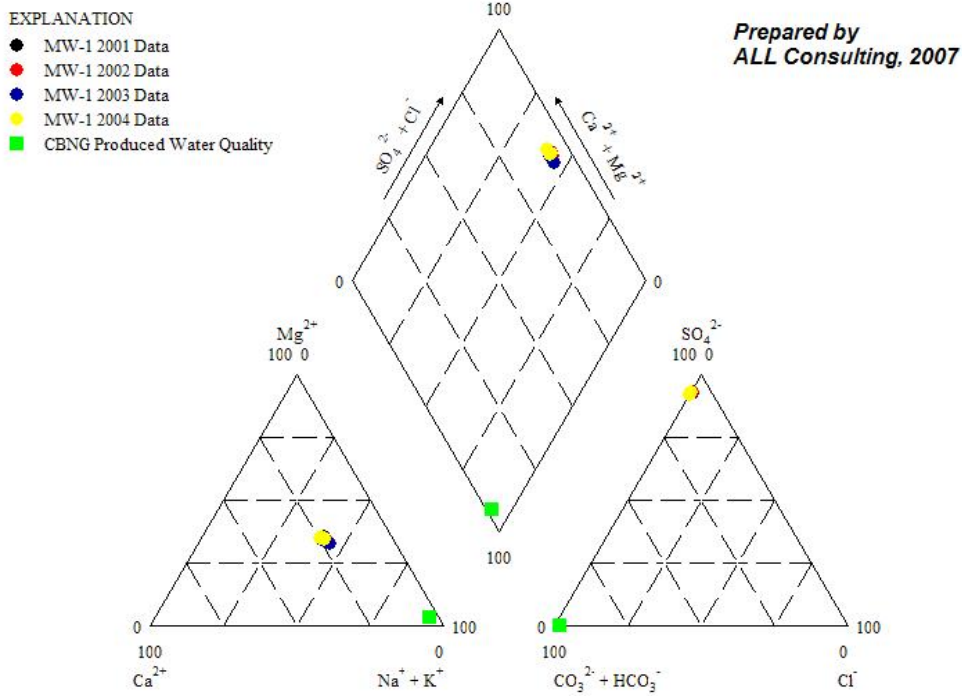
**Figure 5-84: Anion Trend Data for the Santiago 3 MW-1**



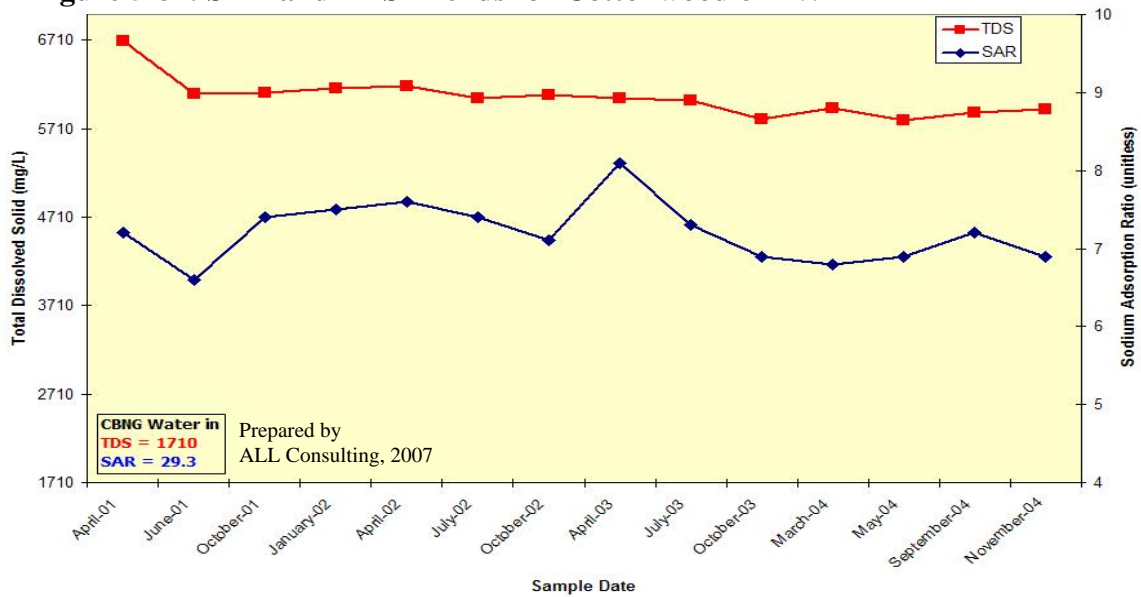
**Figure 5-85: Cation Trend Data for the Santiago 3 MW-1**



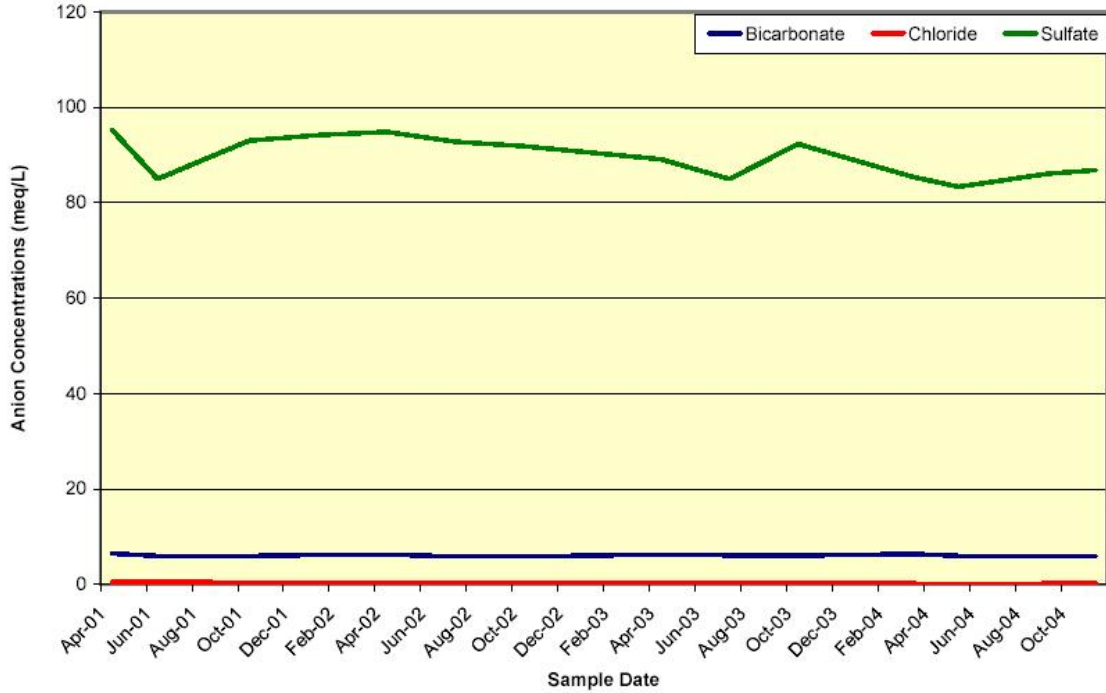
**Figure 5-86: Piper Diagram of Water Samples Collected from the Cottonwood 8 MW-1**



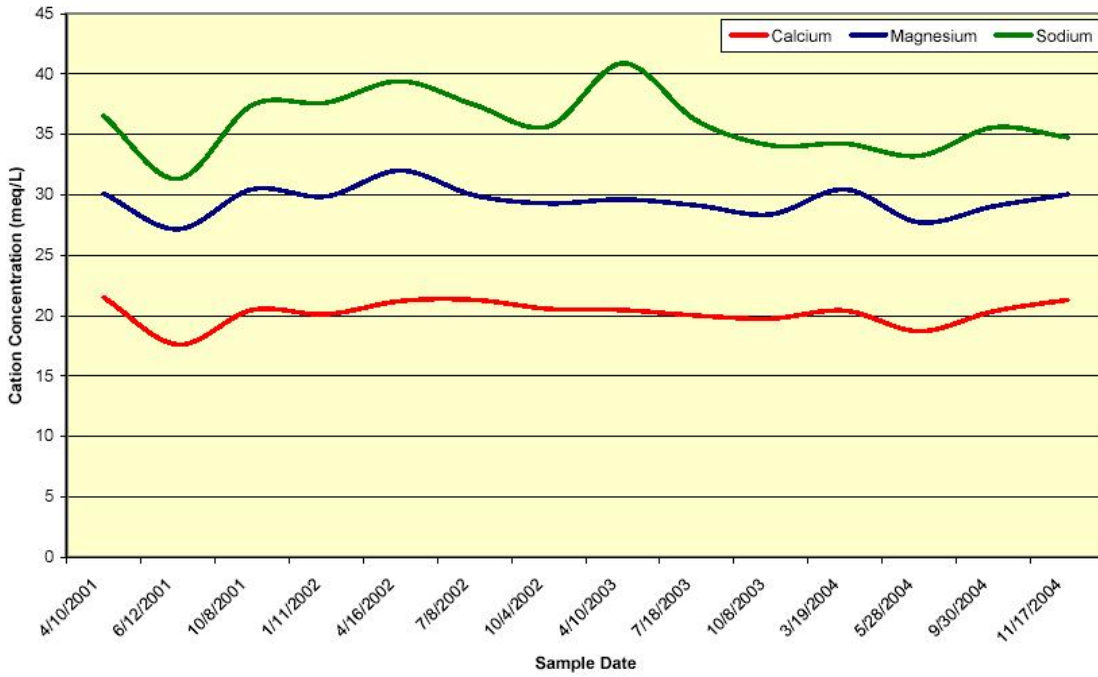
**Figure 5-87: SAR and TDS Trends for Cottonwood 8 MW-1**



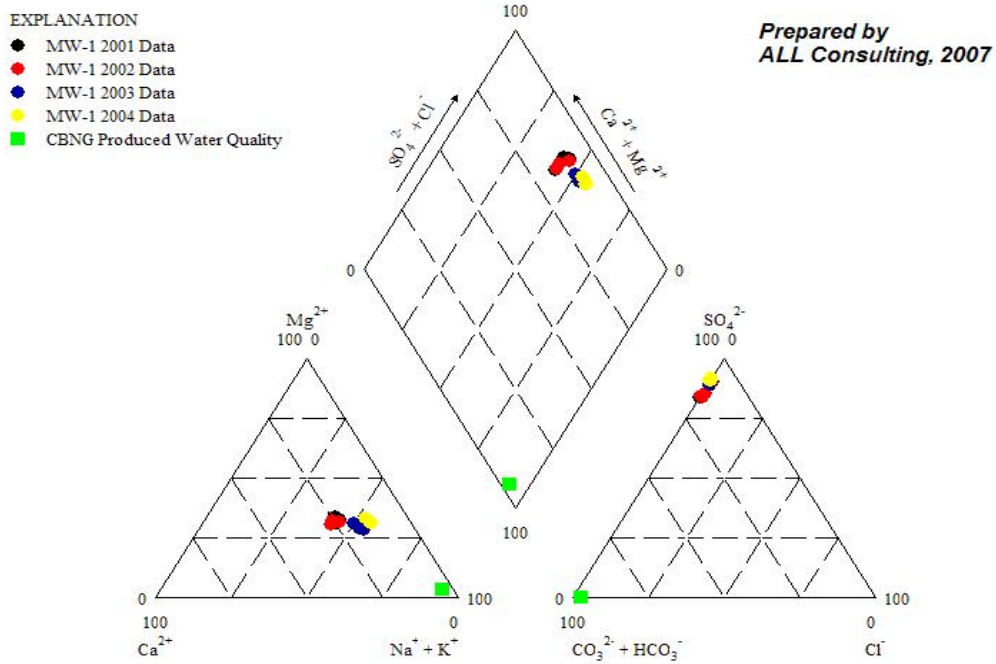
**Figure 5-88: Anion Trend Data for the Cottonwood 8 MW-1**



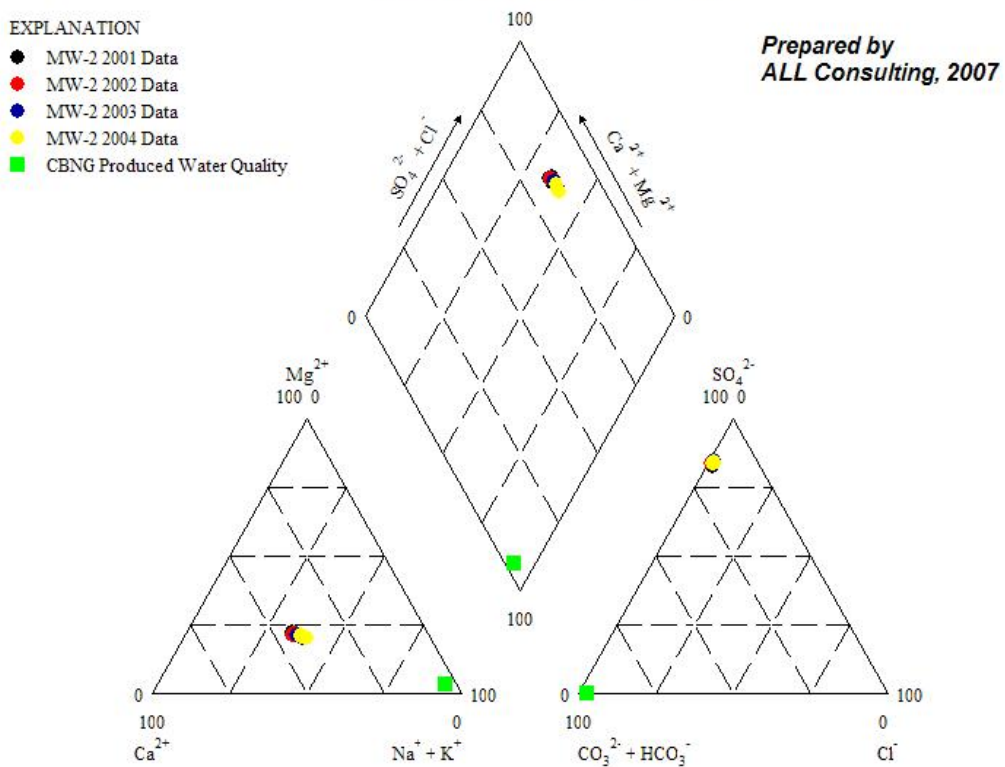
**Figure 5-89: Cation Trend Data for the Cottonwood 8 MW-1**



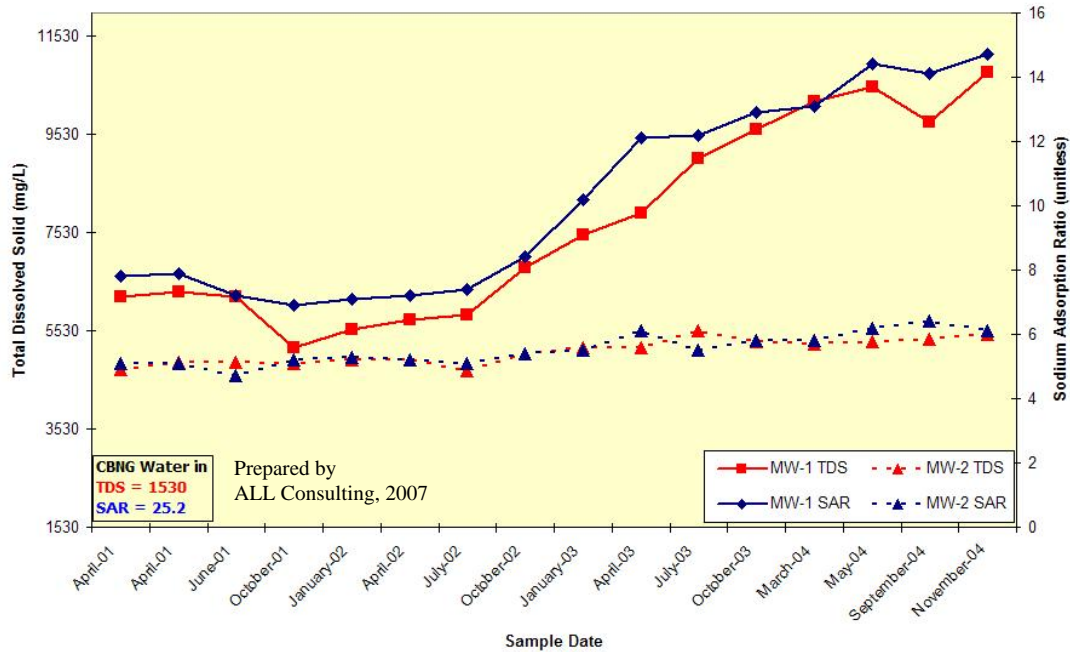
**Figure 5-90: Piper Diagram of Water Samples Collected from the Tietjen Impoundment MW-1**



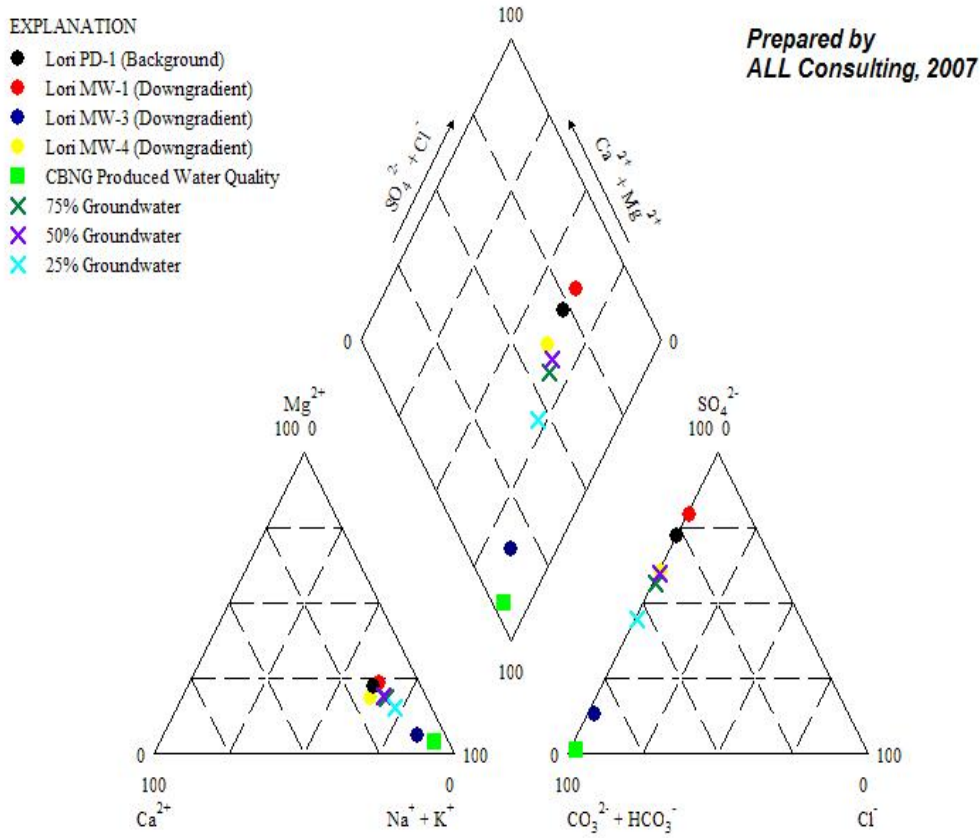
**Figure 5-91: Piper Diagram of Water Samples Collected from the Tietjen Impoundment MW-2**



**Figure 5-92: SAR and TDS Trends for Tietjen MW-1 and MW-2**

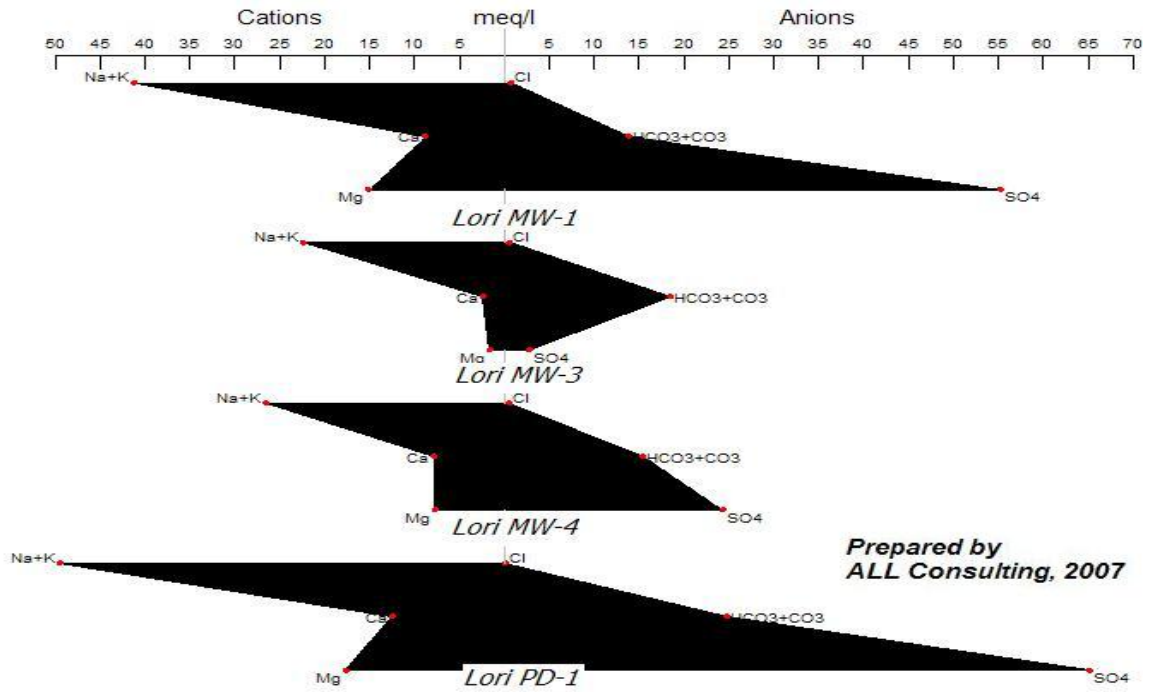


**Figure 5-93: Piper Diagram of Water Samples Collected from the Lori Impoundment Monitoring Wells**



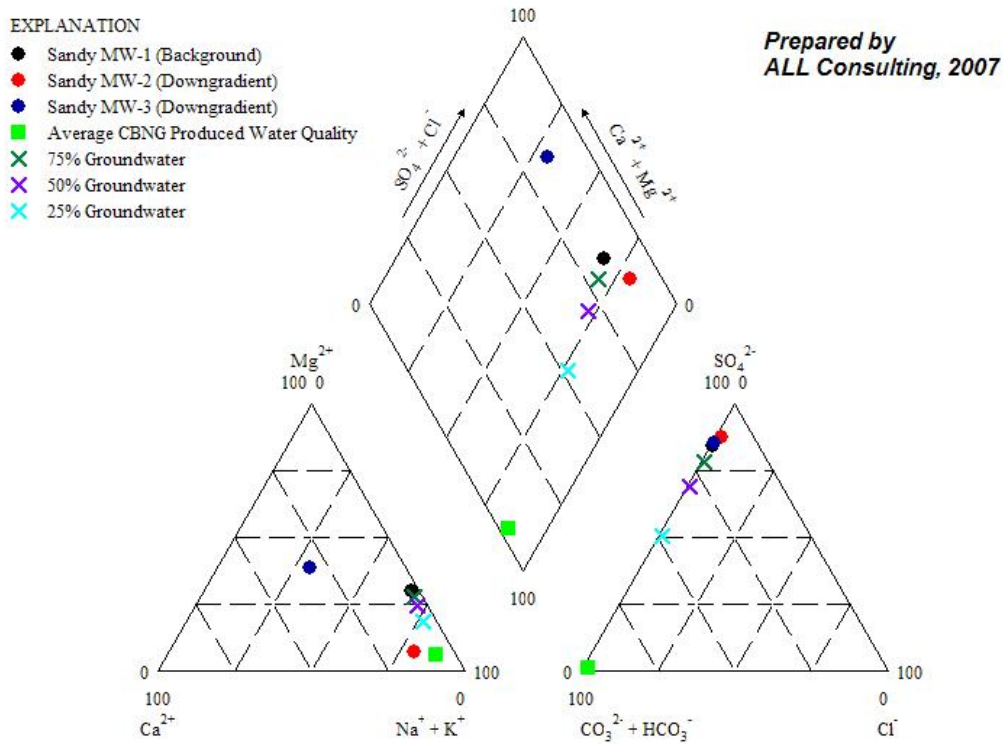


**Figure 5-94: A Stiff Diagram Displaying Water Quality for the Lori impoundment**

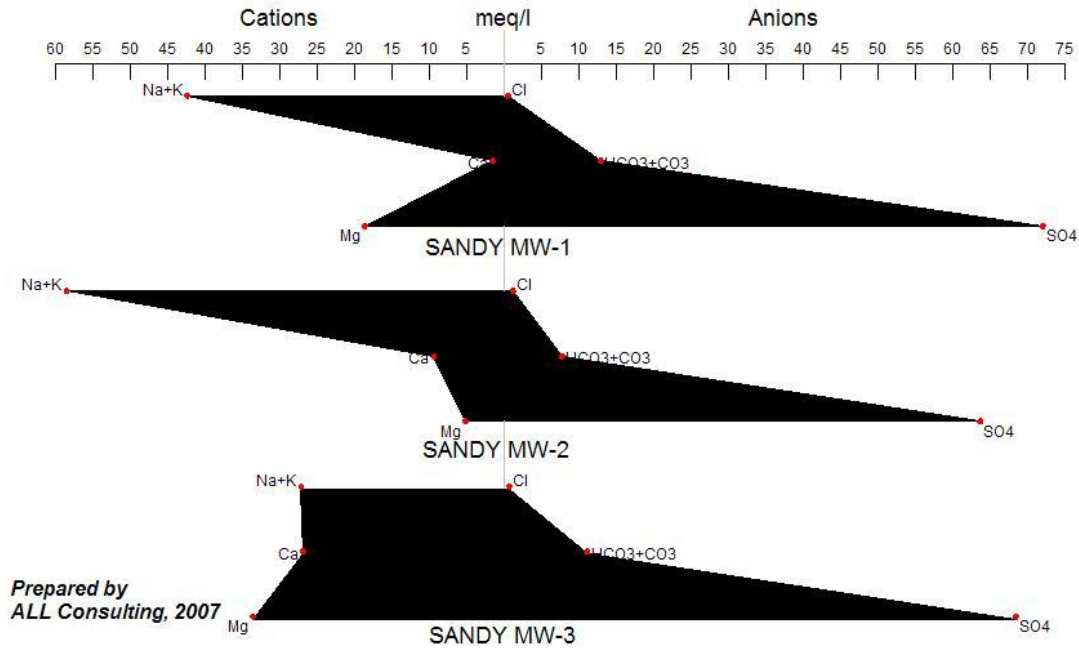


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**Figure 5-95: Piper Diagram of Water Samples Collected from the Sandy Impoundment Monitoring Wells**

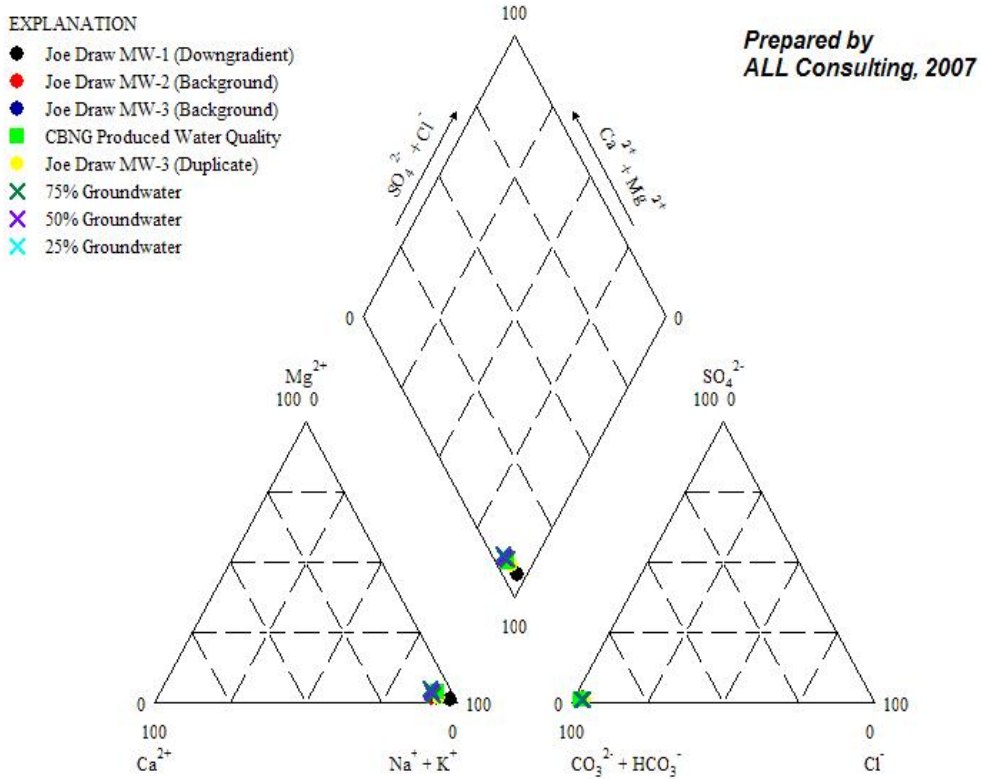


**Figure 5-96: A Stiff Diagram Displaying Water Quality for the Sandy impoundment**



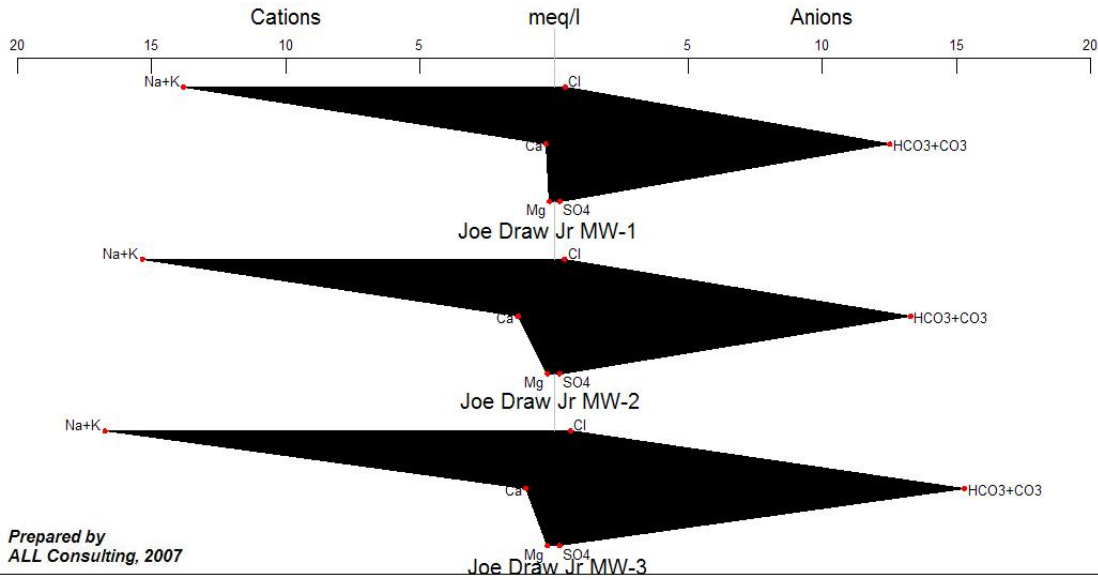
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ALL Consulting, 2007

**Figure 5-97: Piper Diagram of Water Samples Collected from the Joe Draw Jr. Impoundment Monitoring Wells**

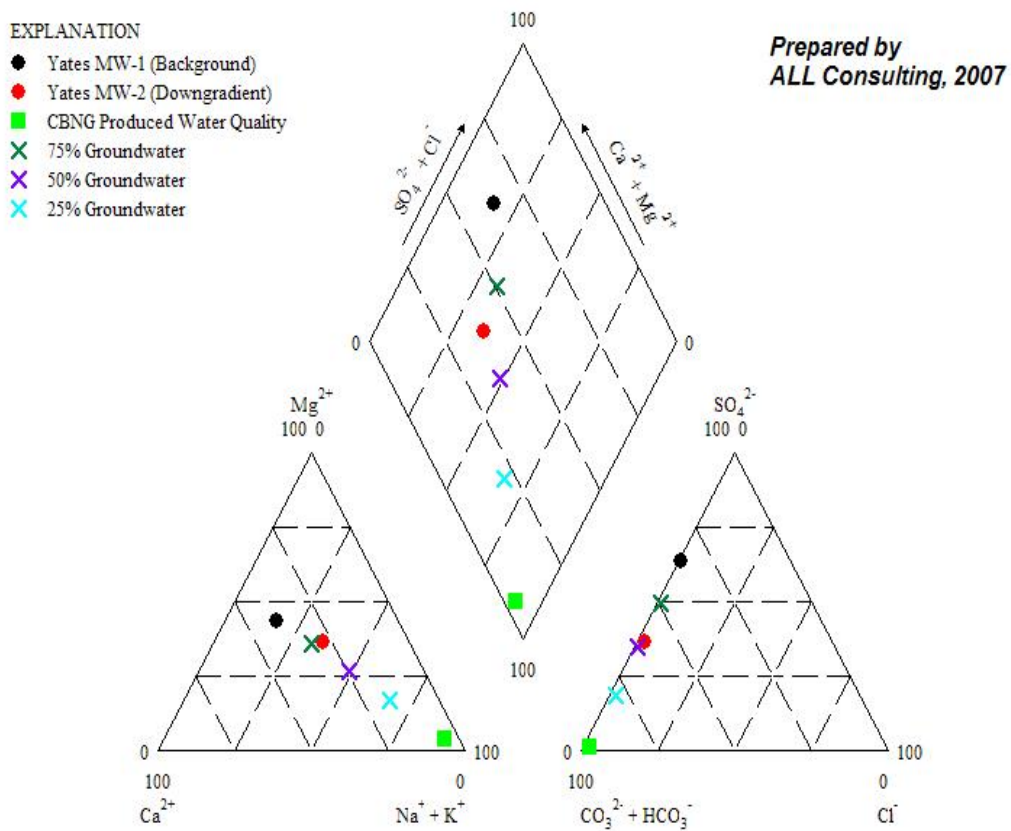


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ALL Consulting, 2007

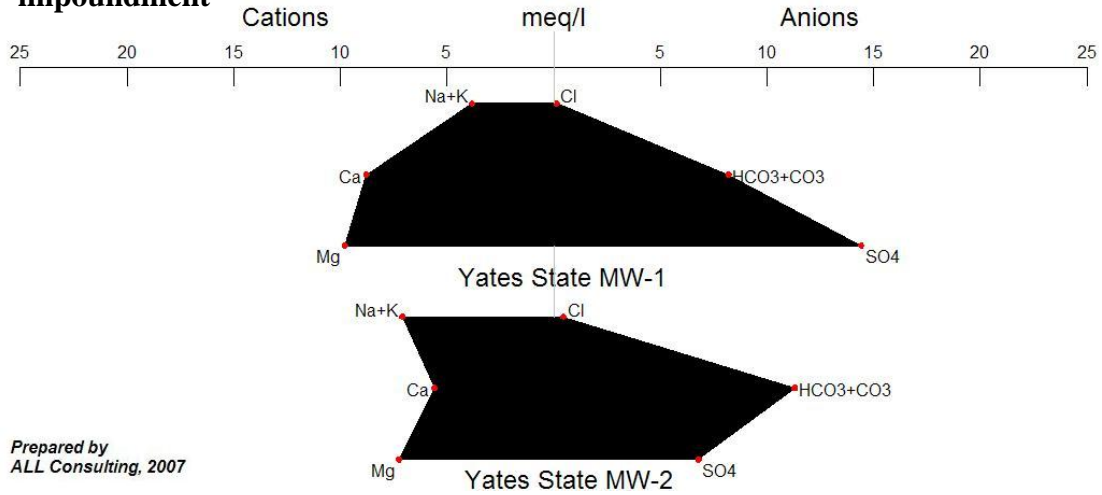
**Figure 5-98: A Stiff Diagram Displaying Water Quality for the Joe Draw Jr. impoundment**



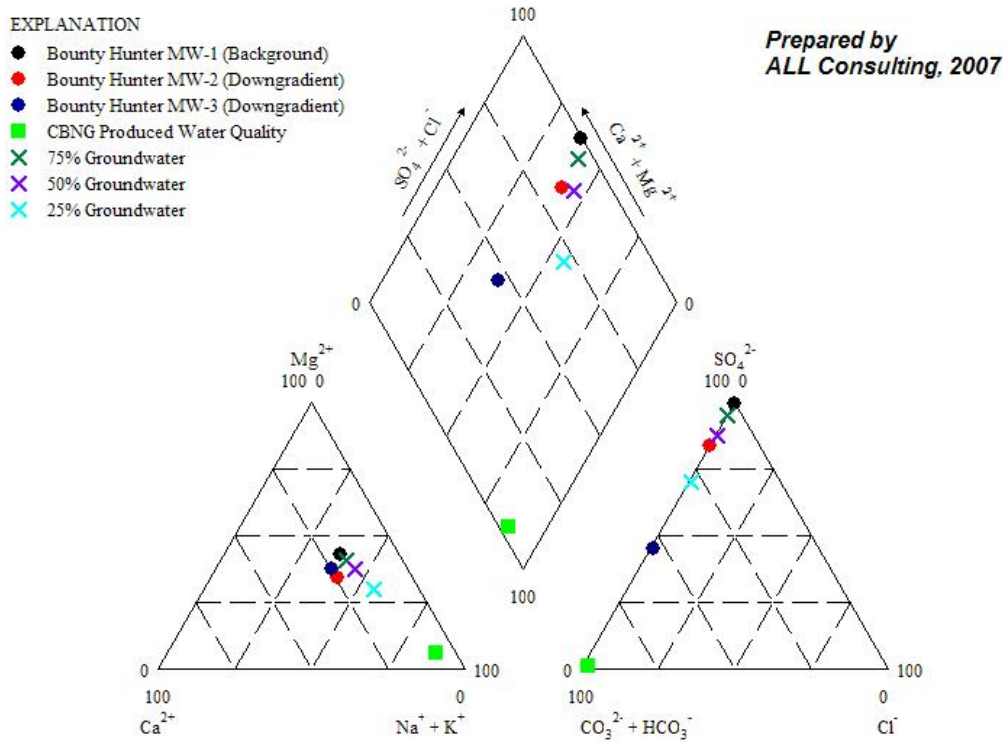
**Figure 5-99: Piper Diagram of Water Samples Collected from the Yates State Impoundment Monitoring Wells**



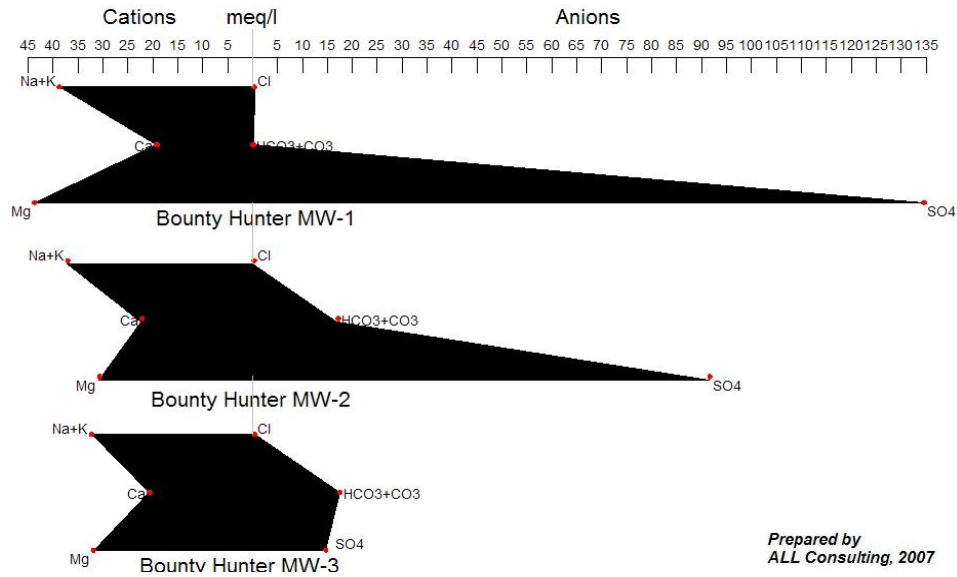
**Figure 5-100: A Stiff Diagram Displaying Water Quality for the Yates State impoundment**



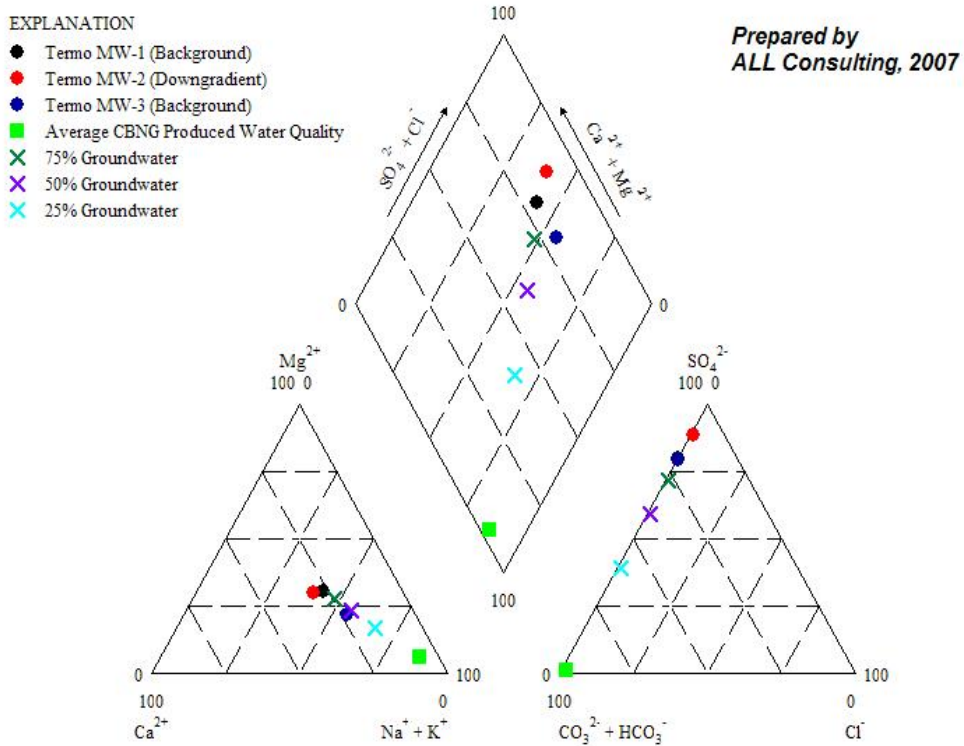
**Figure 5-101: Piper Diagram of Water Samples Collected from the Bounty Hunter Impoundment Monitoring Wells**



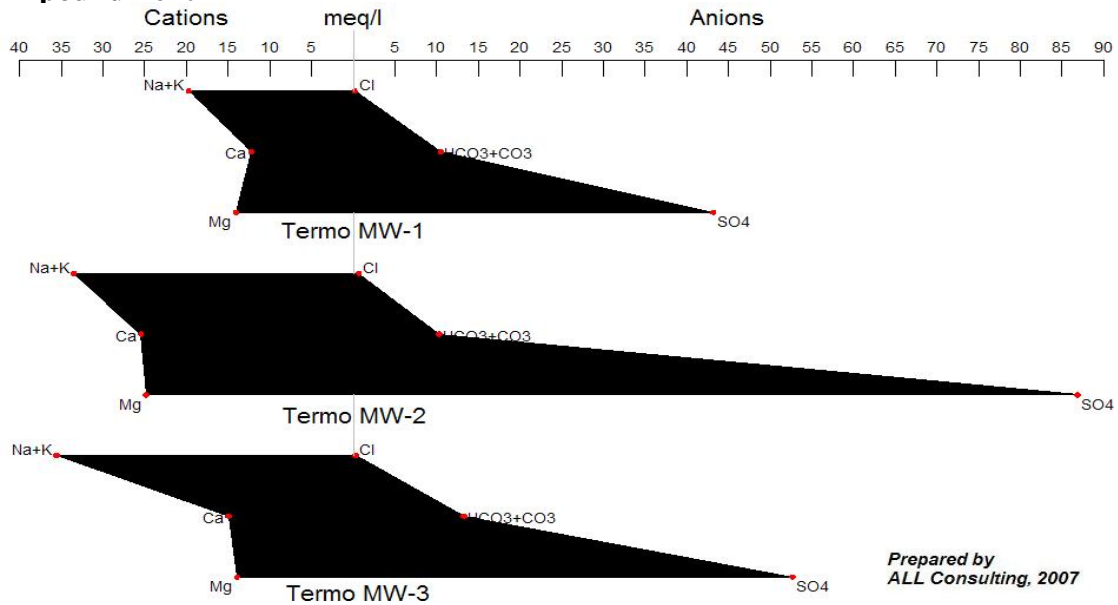
**Figure 5-102: A Stiff Diagram Displaying Water Quality for the Bounty Hunter impoundment**



**Figure 5-103: Piper Diagram of Water Samples Collected from the Termo Impoundment Monitoring Wells**

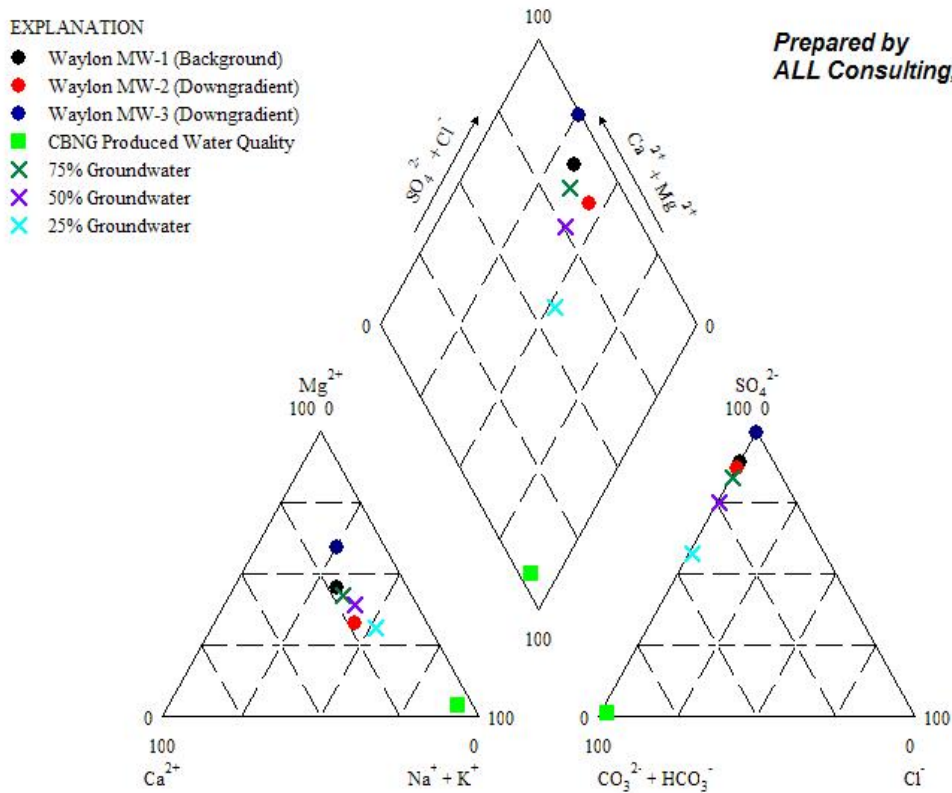


**Figure 5-104: A Stiff Diagram Displaying Water Quality for the Termo impoundment**



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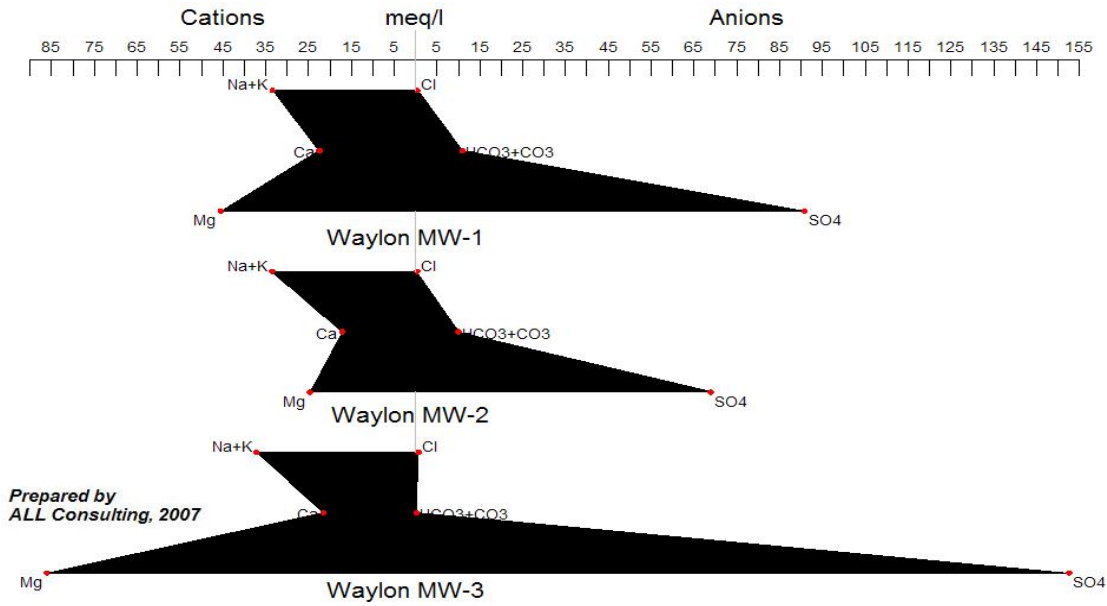
**Figure 5-105. Piper Diagram of Water Samples Collected from the Waylon Impoundment Monitoring Wells**



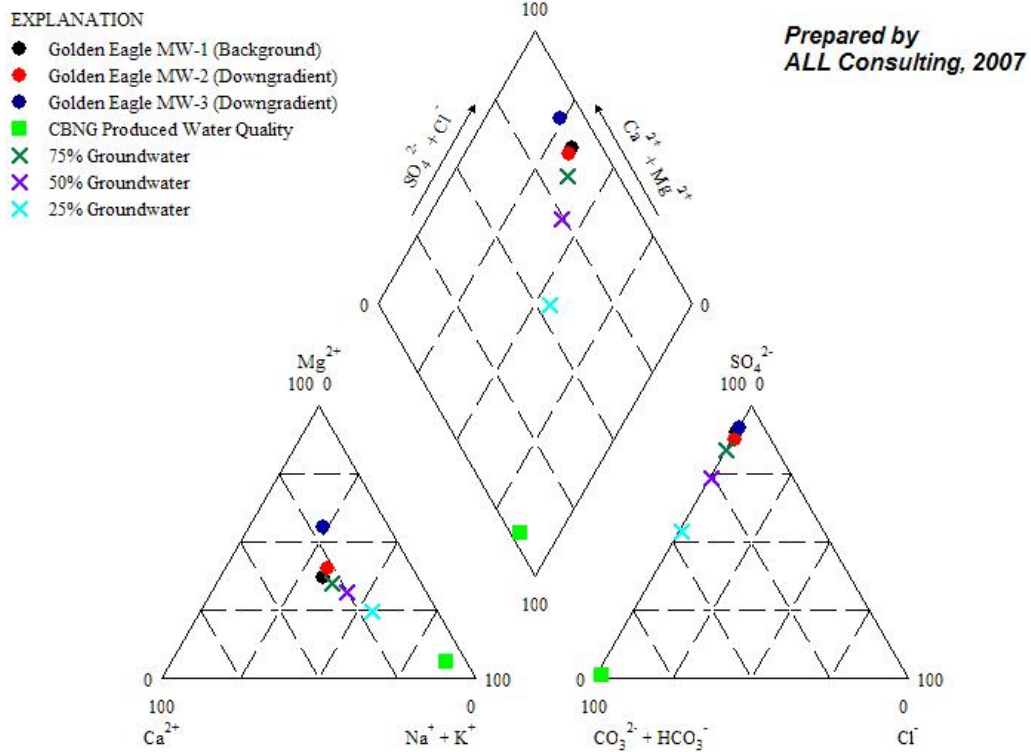
Prepared by  
ALL Consulting, 2007



**Figure 5-106: A Stiff Diagram Displaying Water Quality for the Waylon impoundment**



**Figure 5-107. Piper Diagram of Water Samples Collected from the Golden Eagle Impoundment Monitoring Wells**



**Figure 5-108: A Stiff Diagram Displaying Water Quality for the Golden Eagle impoundment**

