

**Joint Computational/Experimental
Study of Flashback in Hydrogen-rich
Gas Turbines**

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Challenges in Simulating Gas Turbines

- **Lack of appropriate physical models**

- Unsteady dynamics, wall-flame interactions, multiple combustion regimes

- **Less than ideal validation data**

- Diagnostic fidelity reduces with flow complexity

- High-pressure confined environment

- **Geometric complexity**

- Vanes, nozzles, etc.

- Unstructured grid systems are indispensable

- **Uncertainty**

- Boundary conditions, chemistry, operating conditions

Operating Hypotheses

- **Combined LES and RANS capabilities**
 - ➔ LES is not the solution to all problems
 - ➔ RANS has lot of unrealized potential
- **Experiments in the absence of modeling guidance is not useful for advancing predictive capability**
 - ➔ Models should capture sensitivity to parameters in a real gas turbine
 - ➔ Experiments should be designed to reproduce this sensitivity
 - Non-trivial exercise
 - Current simulation approaches cannot provide this guidance

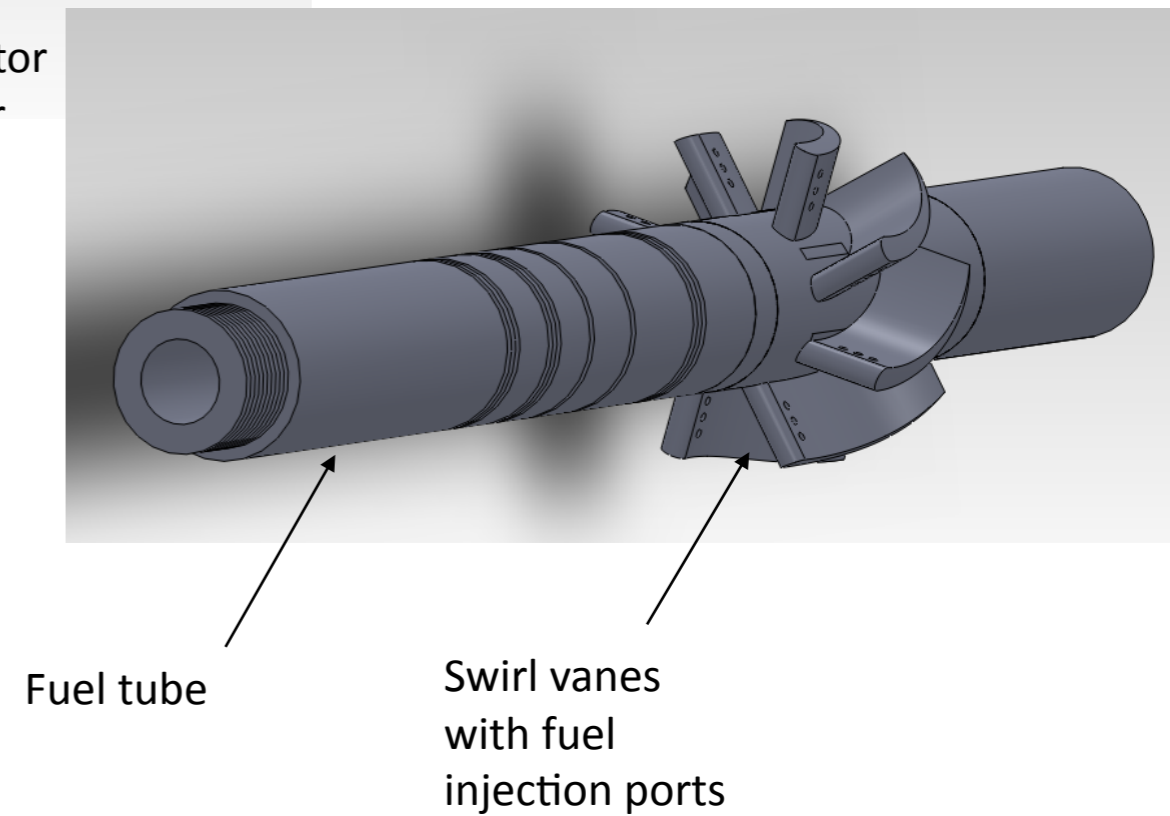
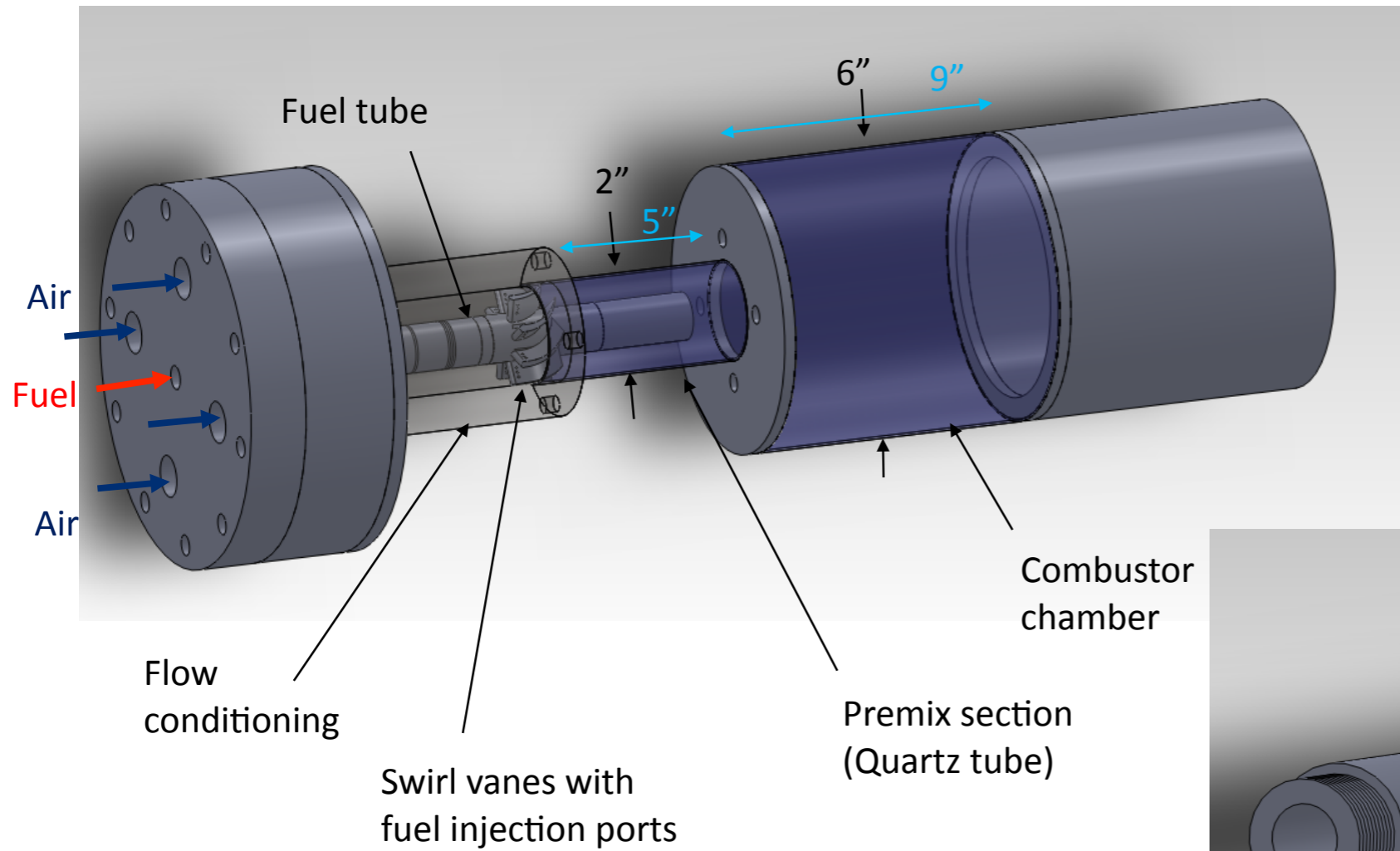
Objectives

- **Integrate high and low fidelity computational models (LES, RANS) with experiments**
 - ➔ To capture unsteady dynamics in gas turbine combustors
 - ➔ Provide **predictive** insight in the design process

- **Target-based model development**
 - ➔ UT high-pressure combustor as the overarching simulation

Target System

- **UT high-pressure swirl combustor**



Key Issues

- **Fuel injection, mixing, and combustion**

- ➔ Crossflow jet configuration

- ➔ Flame stabilization and mixing issues

- **Flashback dynamics**

- ➔ Flame propagation in turbulent core flow

- ➔ Flame-wall interaction and boundary layer modulation

Key Computational Issues

- **LES-based modeling**

- Combustion models in complex geometries

- Flame-wall interaction modeling

- Jet-in-crossflow anomalous behavior

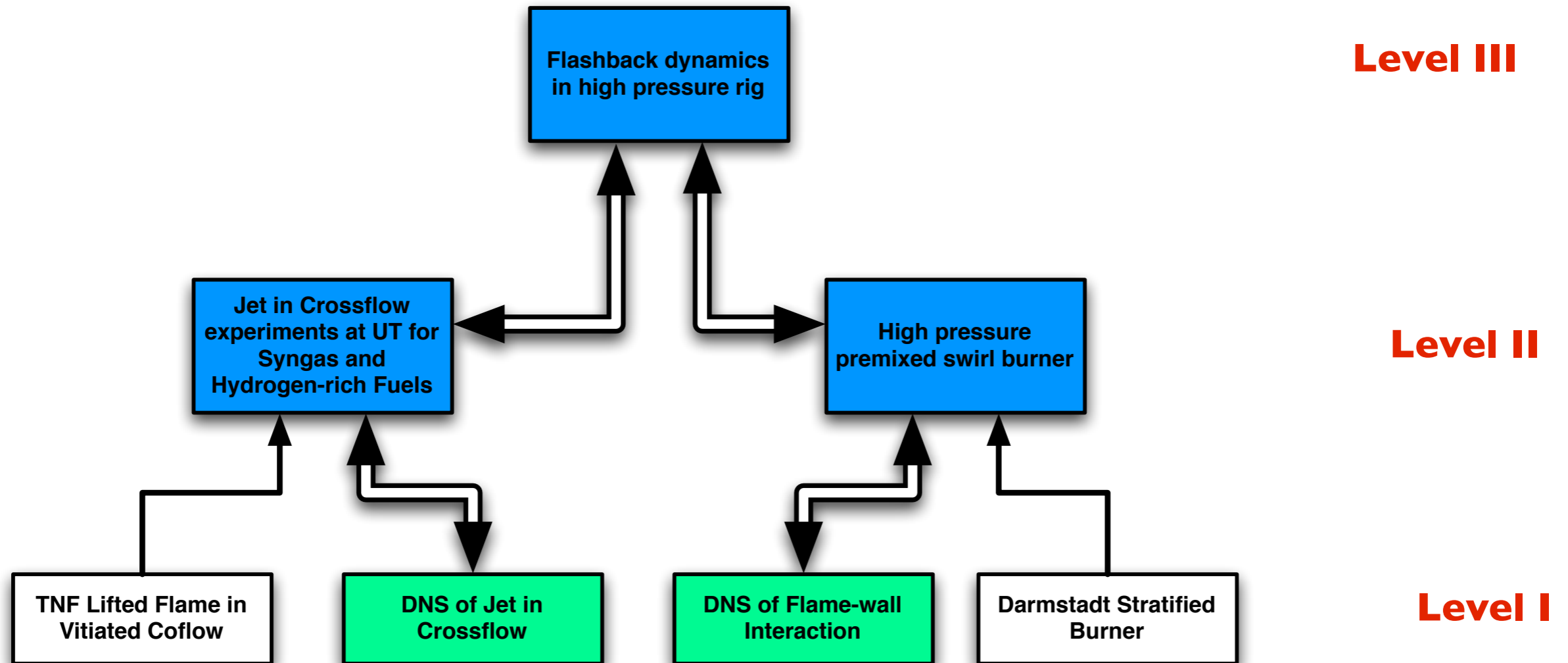
- **Predictive uncertainty in RANS**

- Highly parameter dependent turbulence models

- **Technology transfer**

- A common platform to share advances with industry

Hierarchical Validation Pyramid

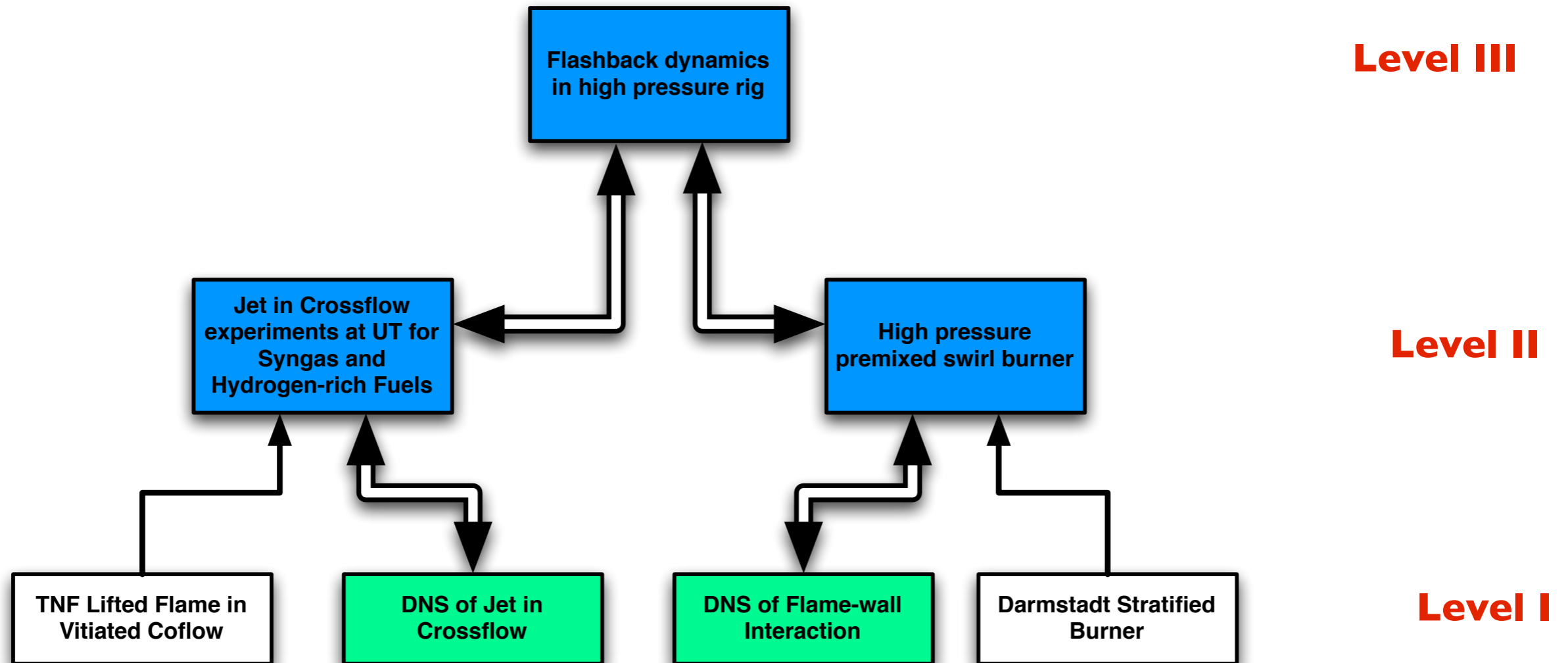


- **Level 1 - Fundamental data from legacy expts. and direct numerical simulations (DNS)**
- **Level 2 - UT re-configurable experiments designed for validation**
- **Level 3 - UT target system experiments**

Research Plan

- **UT high-pressure swirl combustor experiments**
 - ➔ Validation driven experiments
- **LES model development**
 - ➔ Eulerian probability density function (PDF) approach for complex geometries
 - ➔ Transported-equation based dissipation rate model
- **RANS accuracy improvement**
 - ➔ Calibration as a mathematical approach
 - ➔ Propagating uncertainties in chemistry and boundary conditions
- **Open source model transfer**
 - ➔ OpenFOAM based model implementation

Hierarchical Validation Pyramid



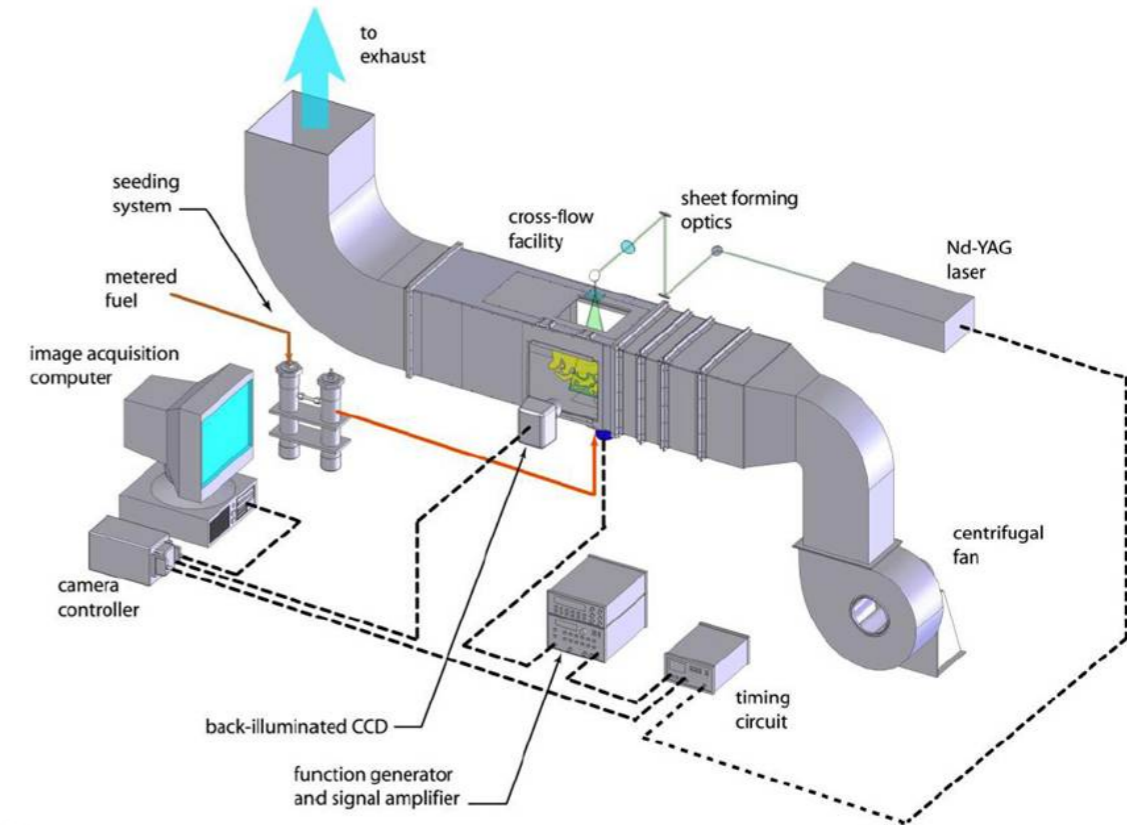
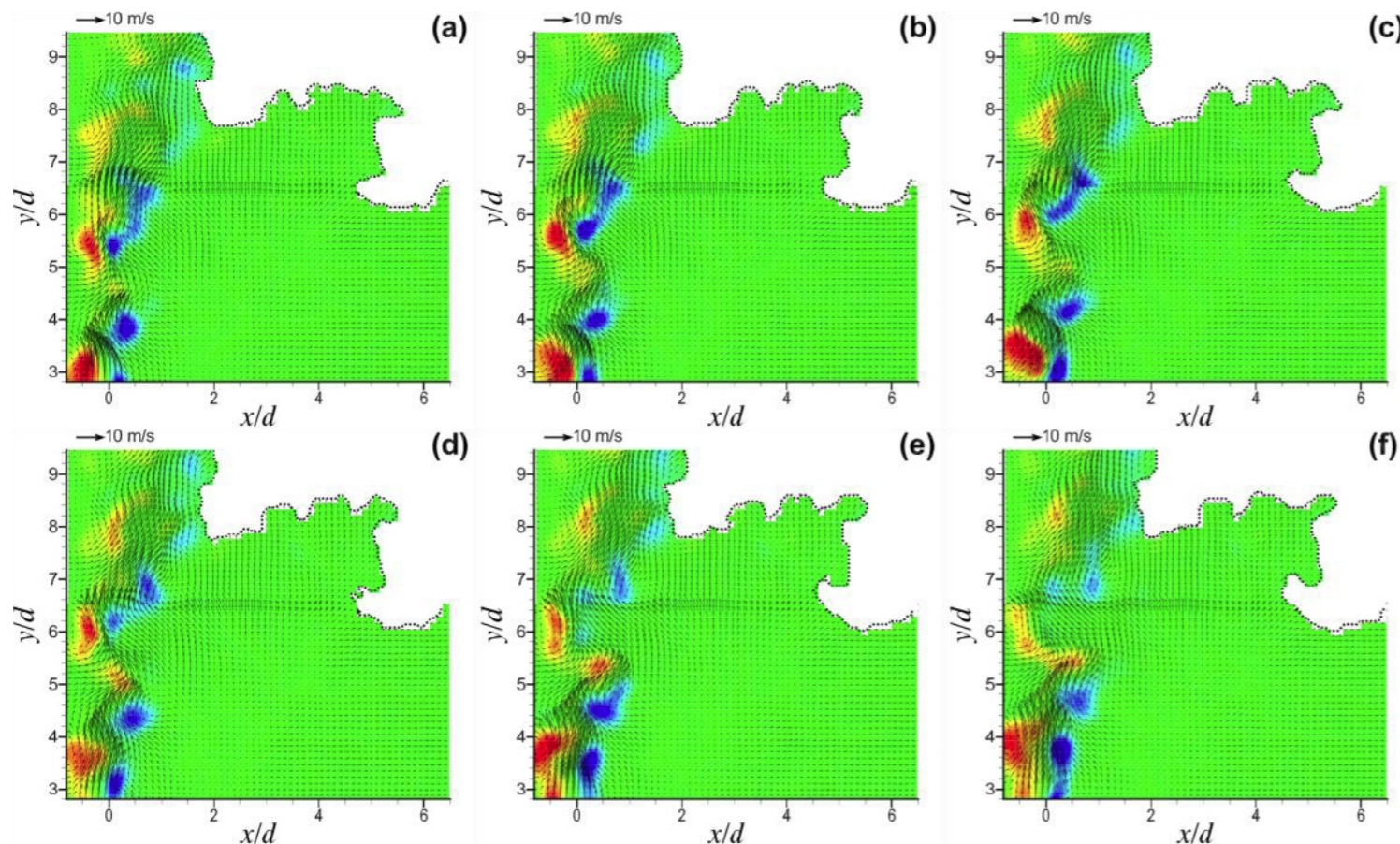
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Pitched Jets in Crossflow

- Variations in jet angle, fuel composition



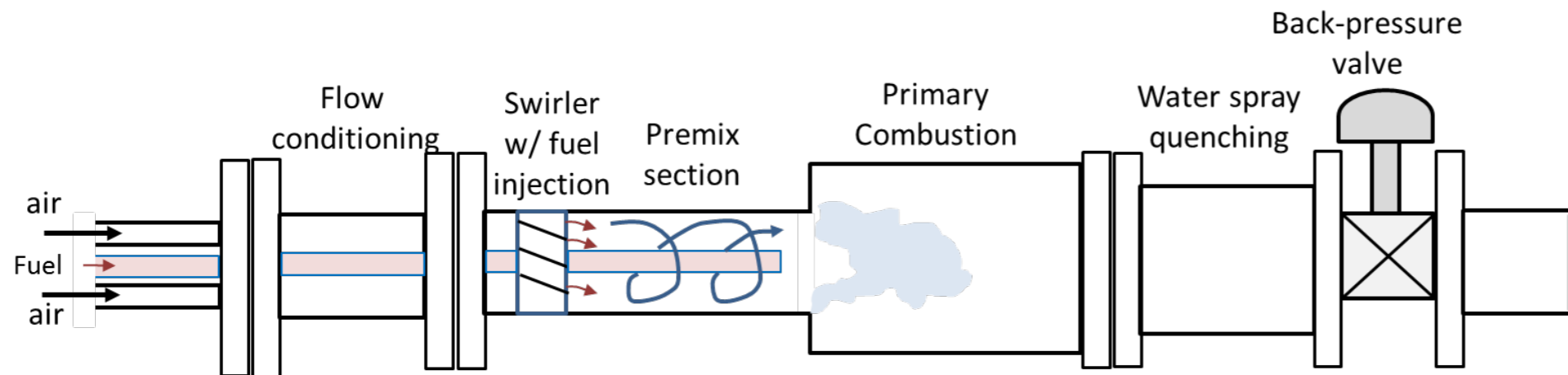
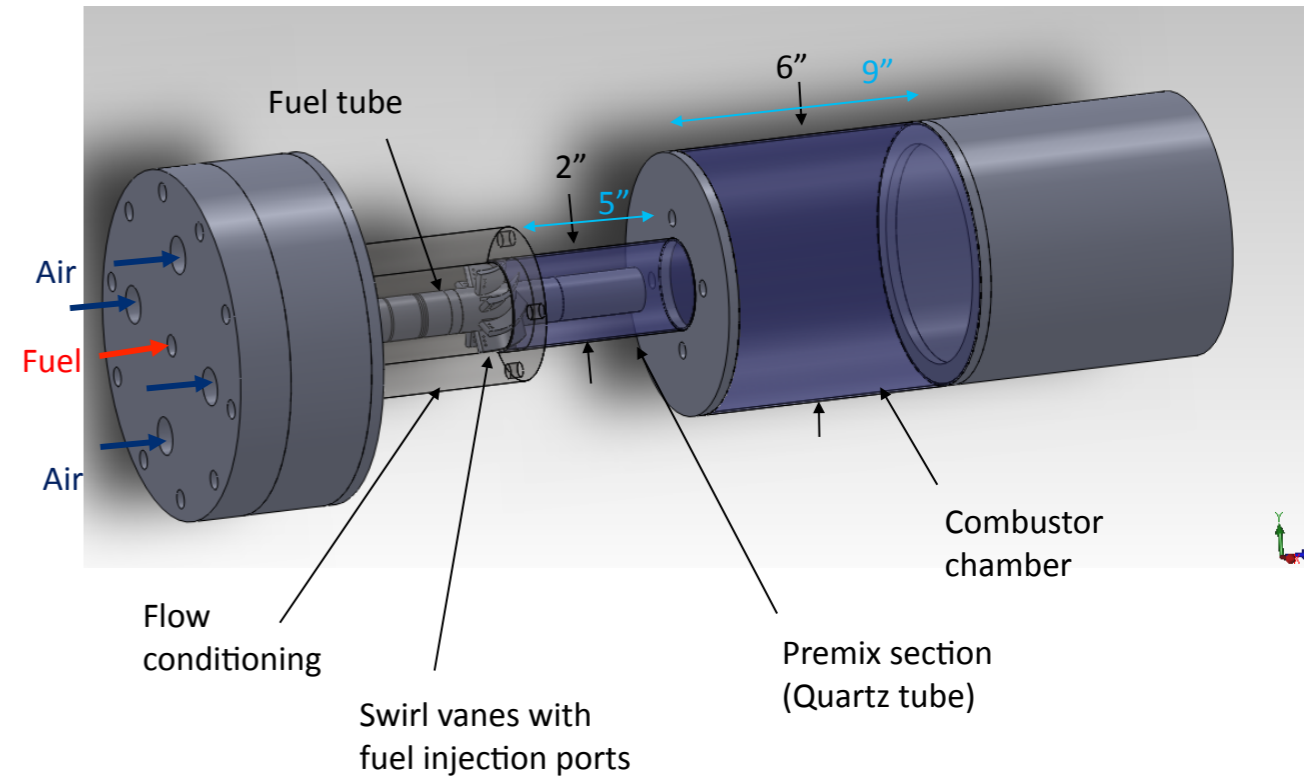
Figure 12: Jet flames in crossflow with different levels of premixing. The fuel is 70% CH₄ + 30% H₂. (a) non-premixed, (b) jet fluid diluted by 25% (volume basis) with air, and (c) jet fluid diluted by 50% with air.



Simultaneous PLIF + PIV

Flashback Dynamics

- Fuel injection through swirl vanes
- Flashback induced through back-pressure valve
- Optical access for simultaneous velocity/scalar measurements



Modeling Approach

- **Probability density function (PDF) approach**

→ Solve a high-dimensional transport equation for joint-PDF of gas phase scalars

- **In LES calculations, the filtered moments of the composition vector are required**

$$\tilde{\phi} = \int \mathcal{G}(\zeta) P_{\xi}(\zeta; \mathbf{x}, t) d\zeta$$

- **PDF transport equation**

$$\frac{\partial P}{\partial t} + \frac{\partial}{\partial x_j} \left[P \widetilde{u_j} | \zeta \right] = - \underbrace{\frac{\partial}{\partial \zeta_{\alpha}} \left[P \widetilde{\mathcal{M}_{\alpha}} | \zeta \right]}_{\text{Conditional Diffusion}} - \frac{\partial}{\partial \zeta_{\alpha}} \left[P S_{\alpha} \right]_{\text{Chemical Source}}$$

→ Condition diffusion requires a model for scalar dissipation rate

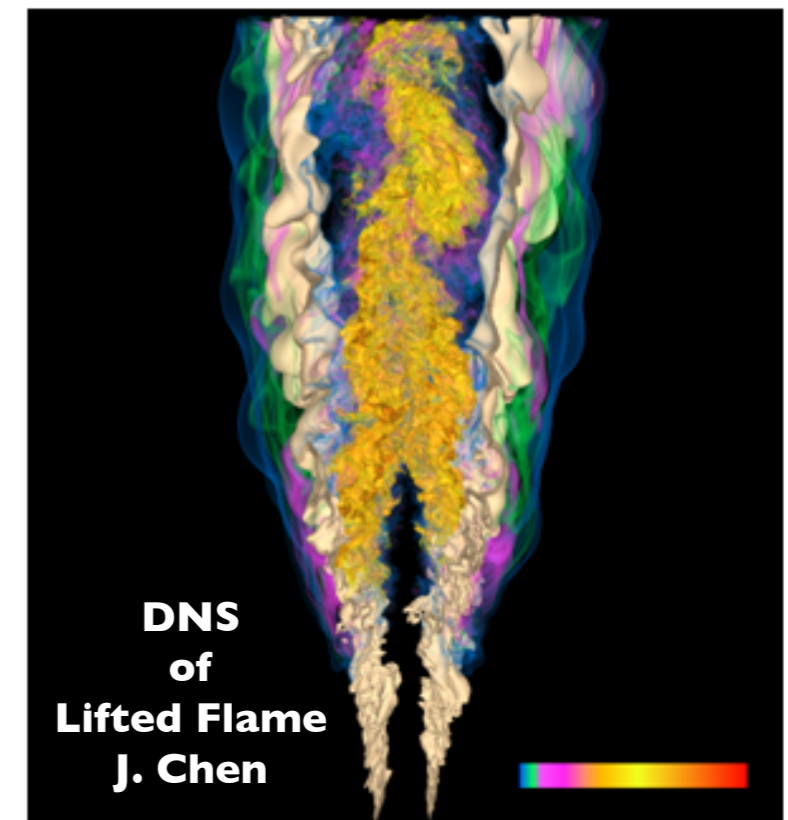
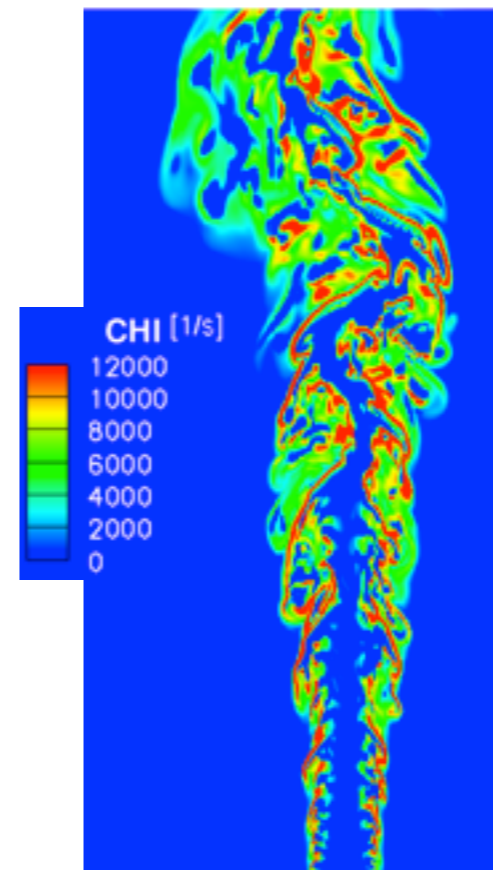
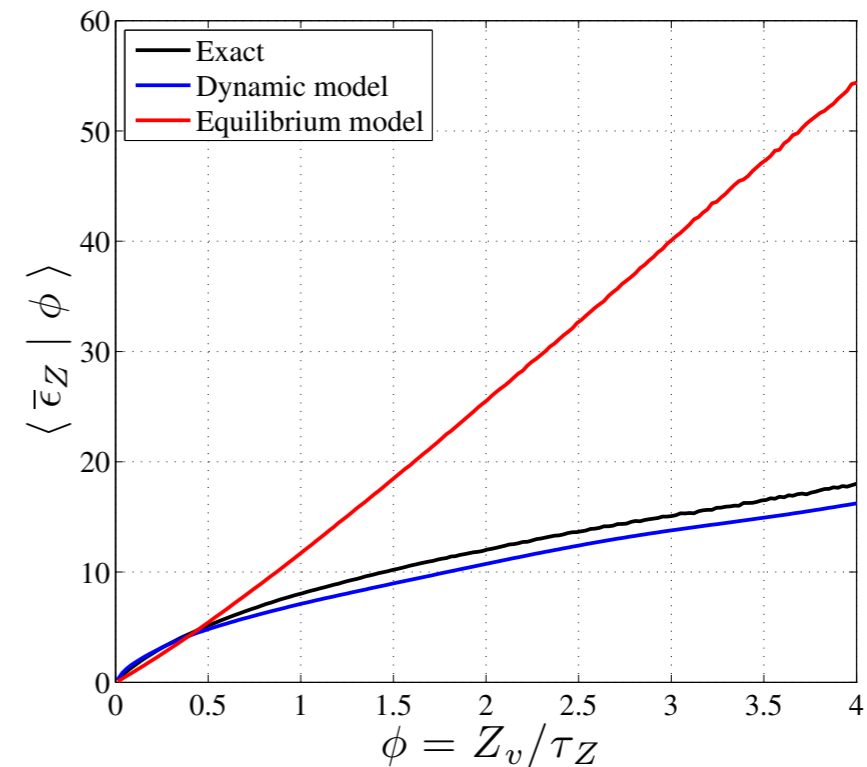
Nonequilibrium Dissipation Rate Model

- **Currently used dissipation rate models rely on equilibrium assumption**

- ➔ Highly restrictive
- ➔ Invalid even in homogeneous isotropic turbulence

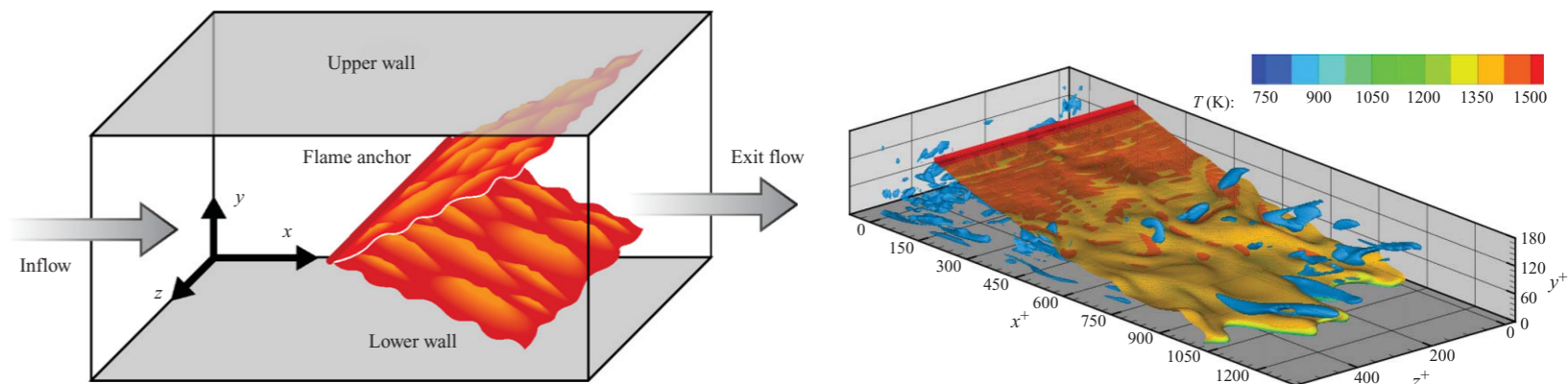
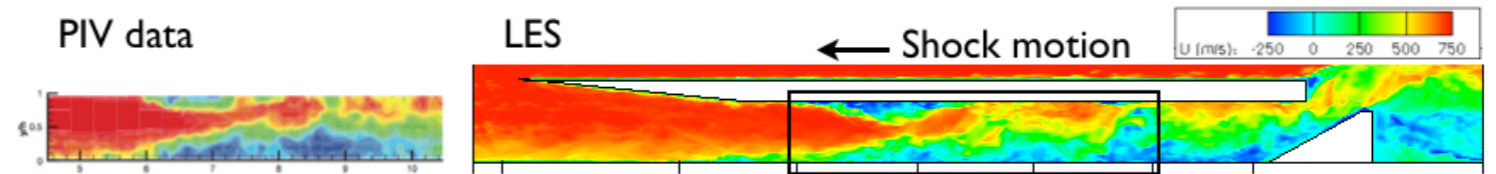
- **Transport-equation based dissipation model**

- ➔ Incorporates spatial transport of scalar energy
- ➔ Allows scalar and turbulence scales to be decoupled



Flame-Wall Interaction

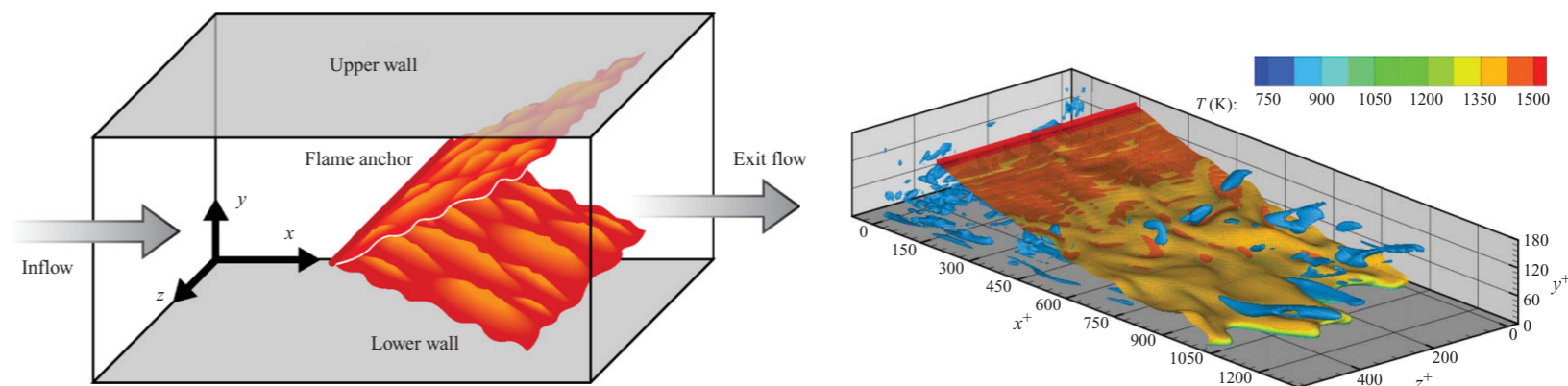
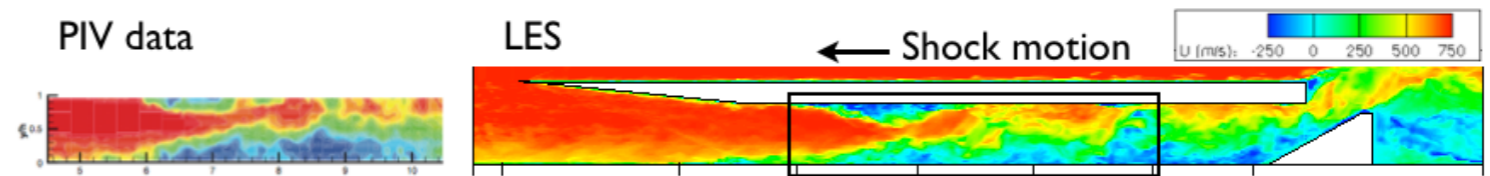
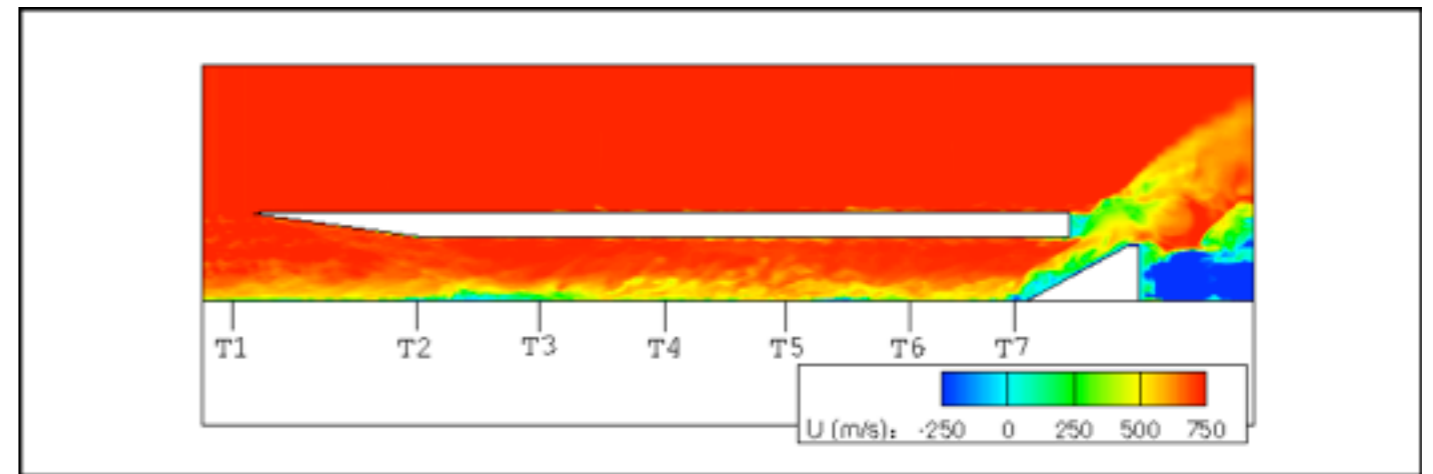
- Propagation of flames in a boundary layer
 - ➔ Modulates the turbulent boundary layer
 - ➔ Alters turbulent energy transport and dissipation
- Similar to unstart propagation in scramjets
 - ➔ Propagation of density/pressure fronts through a separated boundary layer
- DNS-based analysis of turbulent flux models



DNS of J. Chen (Sandia)

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DNS of J. Chen (Sandia)

Modeling PDF Transport Equation

- **PDF transport equation**

$$\frac{\partial P}{\partial t} + \frac{\partial}{\partial x_j} \left[P \widetilde{u_j} | \zeta \right] = - \frac{\partial}{\partial \zeta_\alpha} \left[P \widetilde{\mathcal{M}_\alpha} | \zeta \right] - \frac{\partial}{\partial \zeta_\alpha} [P S_\alpha]$$

Chemical Source

**Conditional
Diffusion**

- **PDF equation is high-dimensional**

➔ If N species present in chemistry, N+5 dimensions

- **Lagrangian Monte-Carlo approach typically used**

➔ Stochastic in nature

➔ Numerical stability is highly flow dependent

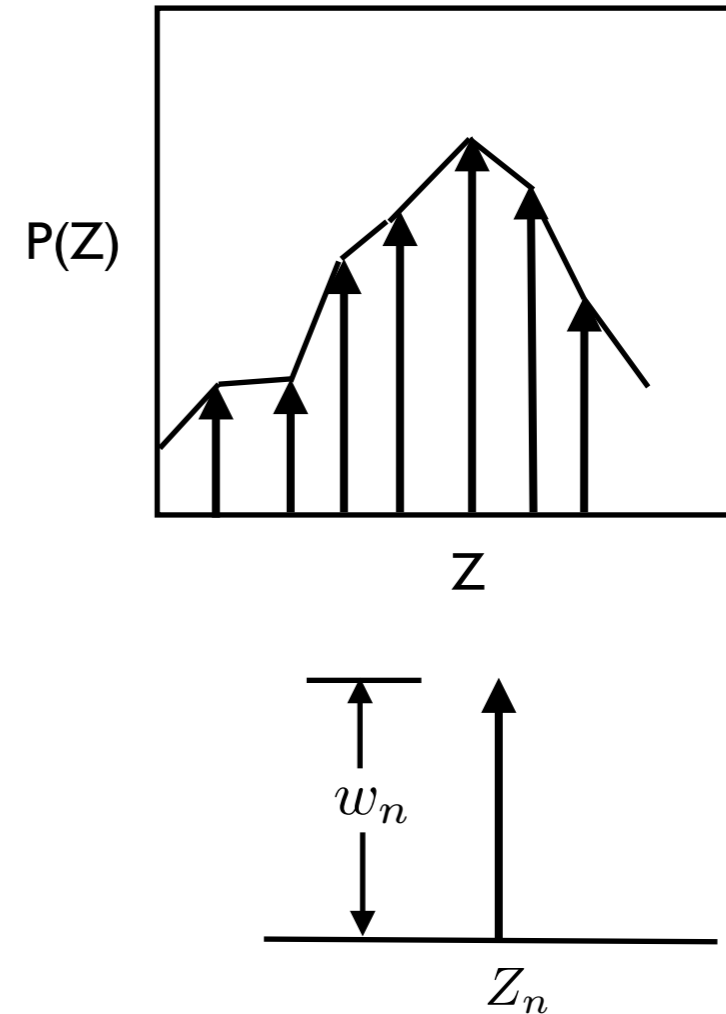
➔ Difficult to maintain numerical accuracy in complex geometries

➔ Highly expensive for realistic flow configurations

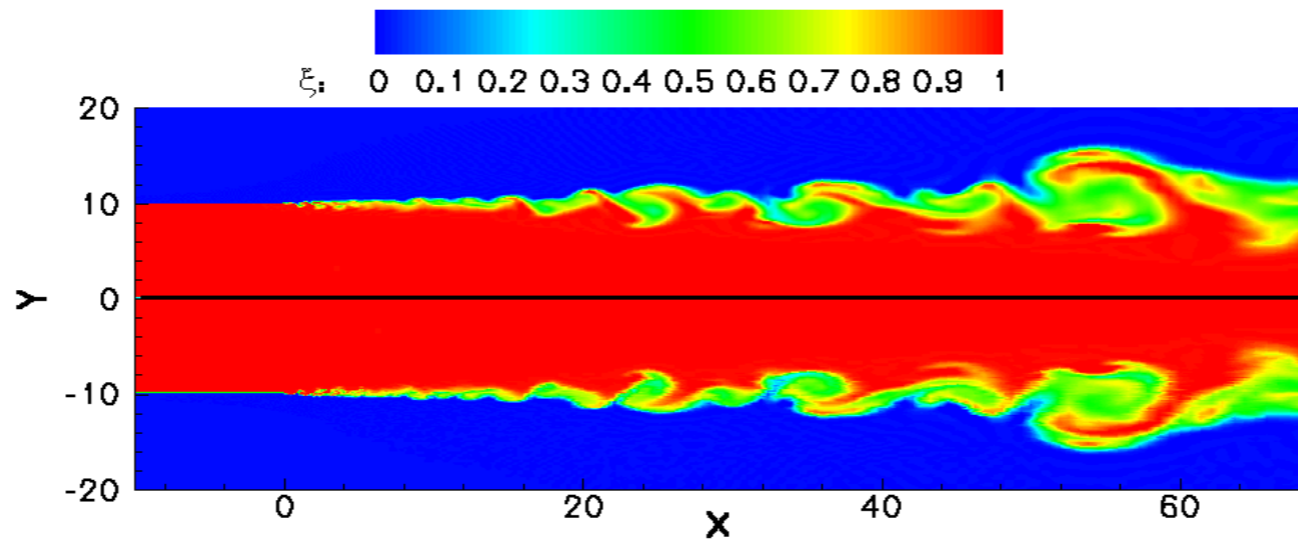
Direct-Quadrature Method of Moments (DQMOM)

- DQMOM uses dirac-delta functions to discretize the PDF
- Each delta-function characterized by a weight and abscissa
 - ➔ Transport equations for these two variables can be formulated
- Similar in structure to scalar transport equations

$$\frac{\partial w_n}{\partial t} + \overline{U}_i \frac{\partial w_n}{\partial x_i} = \frac{\partial}{\partial x_i} \left(\Gamma \frac{\partial w_n}{\partial x_i} \right) + a_n$$



Test case : 2-D shear layer



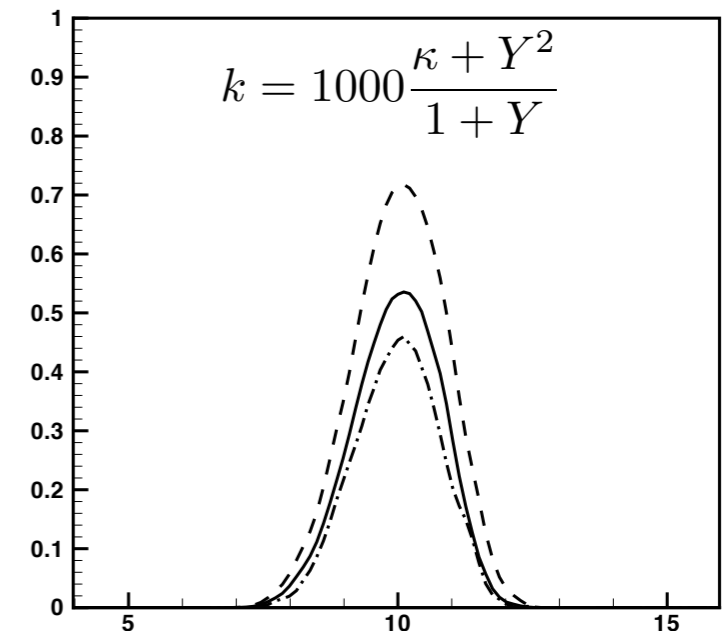
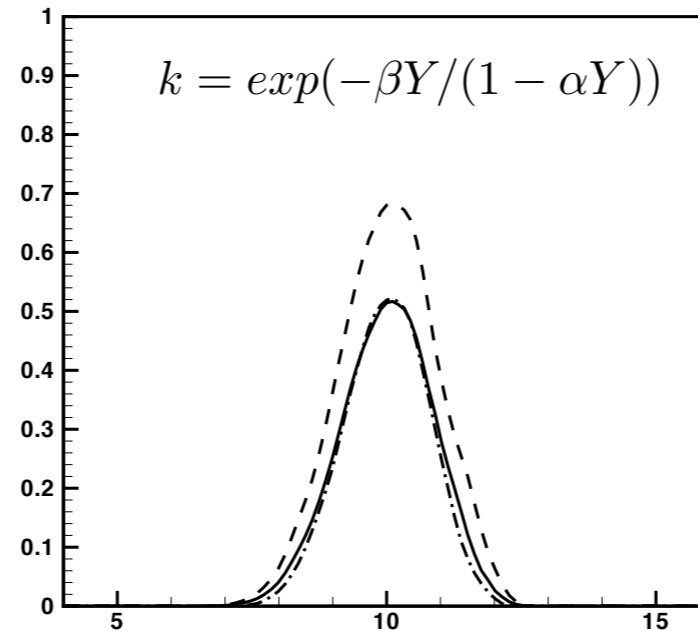
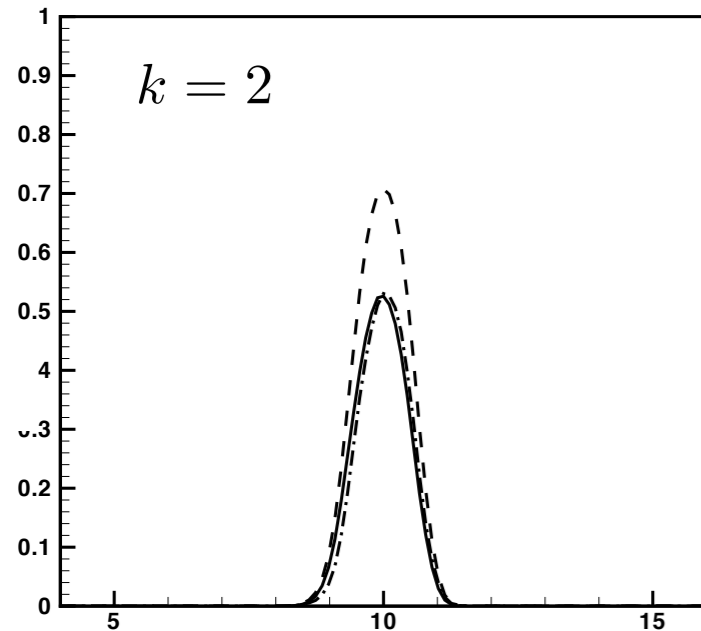
- Flow conditions similar to the experiment of Mungal and Dimotakis (1984)
- Two streams at velocity of 8.8 m/s and 22 m/s
- Single step chemistry formulated using progress-variable and mixture fraction

$$S(Y, Z) = k \left(\frac{Z}{Z_{st}} - Y \right) \left(\frac{1 - Z}{1 - Z_{st}} - Y \right)$$

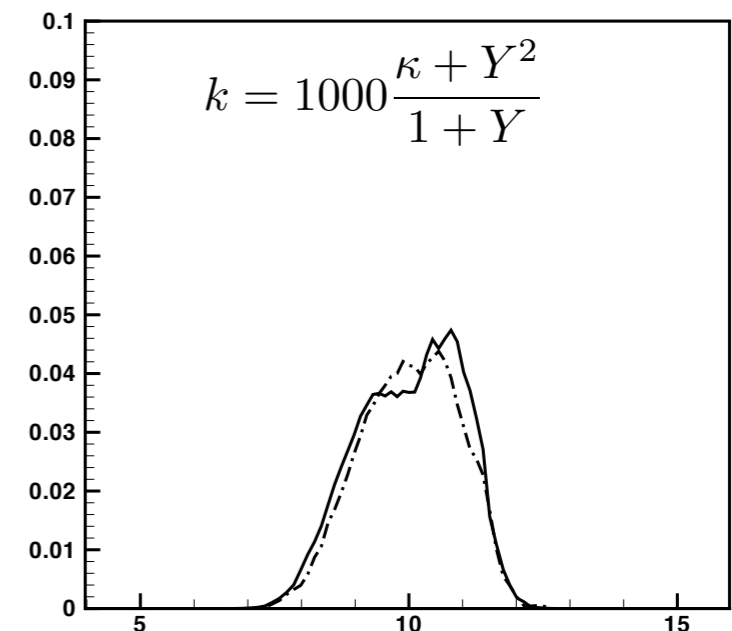
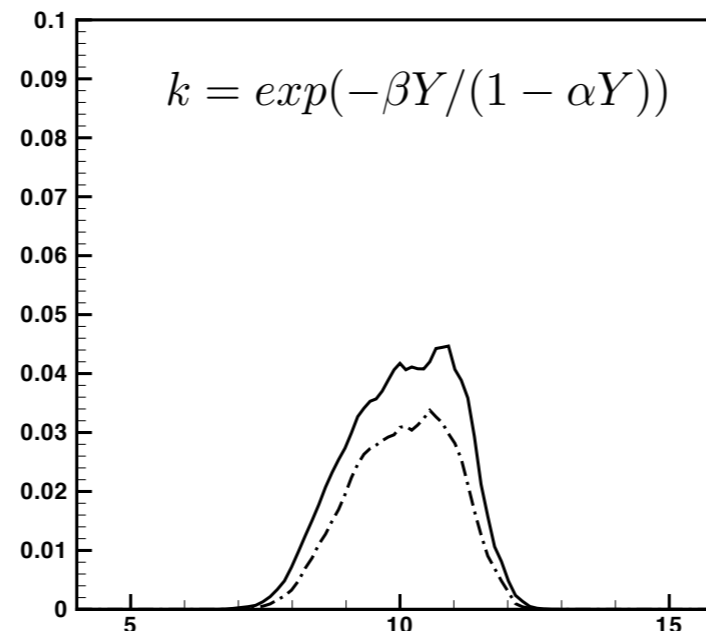
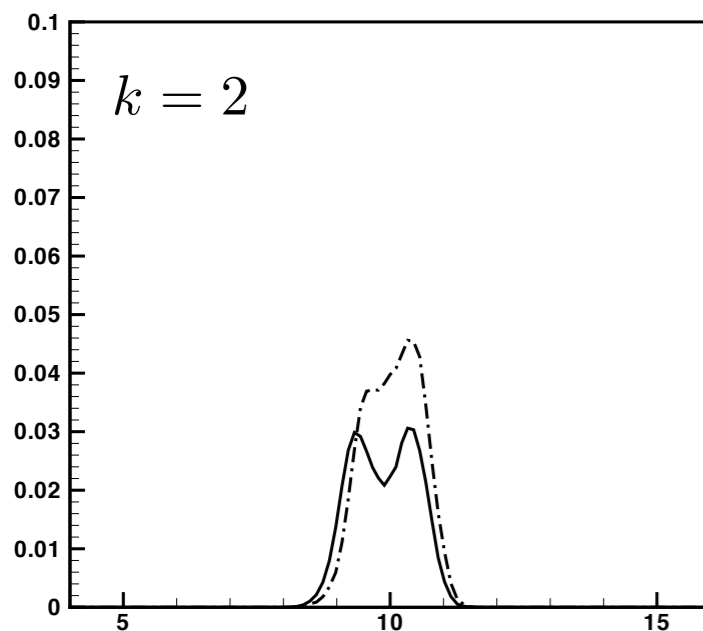
- Test cases performed
 - ➔ LES simulation of first moment of Y, Z and second moment of Z
 - ➔ Lagrangian simulations with IEM mixing model
 - ➔ DQMOM simulation with IEM mixing model and 2-peak formulation
 - ➔ Different functional form for rate constants

Test results

Progress variable mean



Progress variable variance



Solid - DQMOM : Dash-dotted - Lagrangian : Dashed - No subgrid model

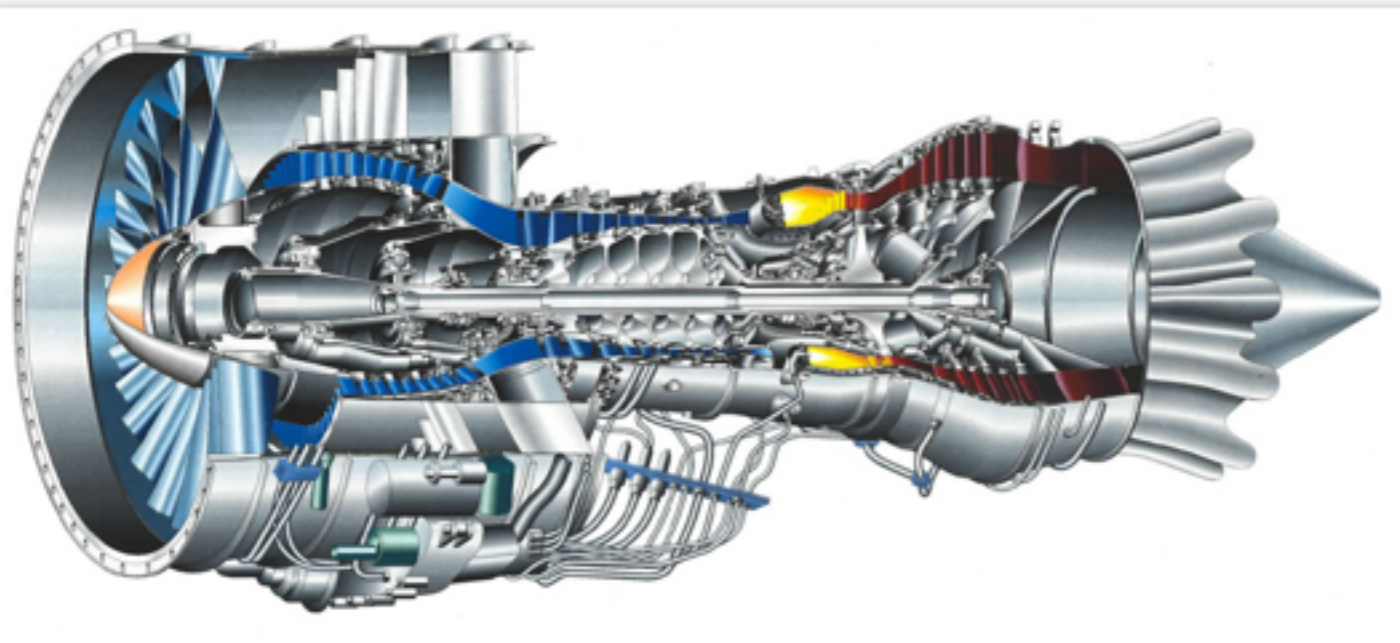
Decision Making, Risks, and CFD

- **CFD is a vital tool for understanding practical engineering devices**
- **CFD models are also highly unreliable**
 - ➔ Modeling is as much an art as science
- **Can we rely on CFD results to make critical decisions?**

DOE interest

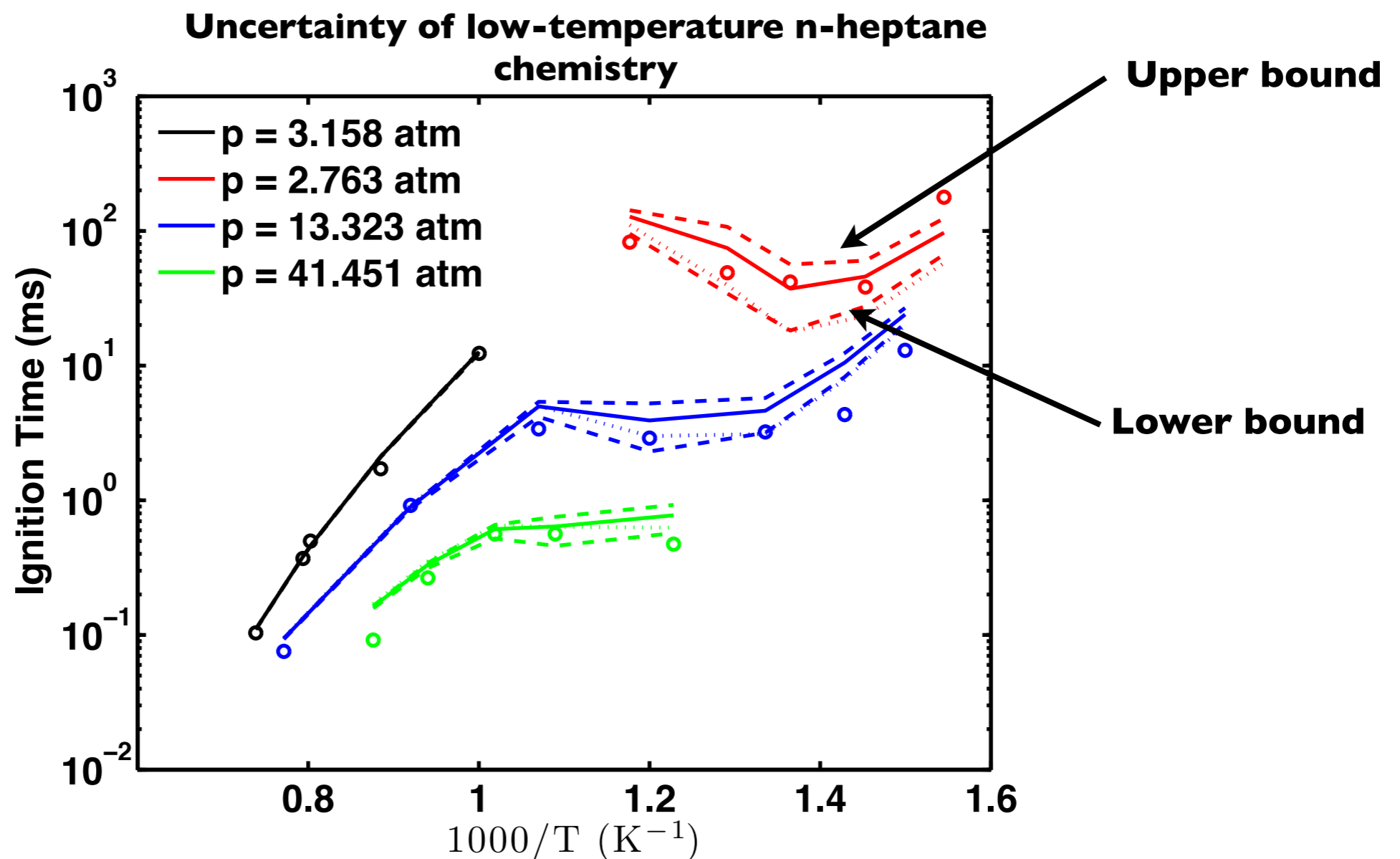


Our interest



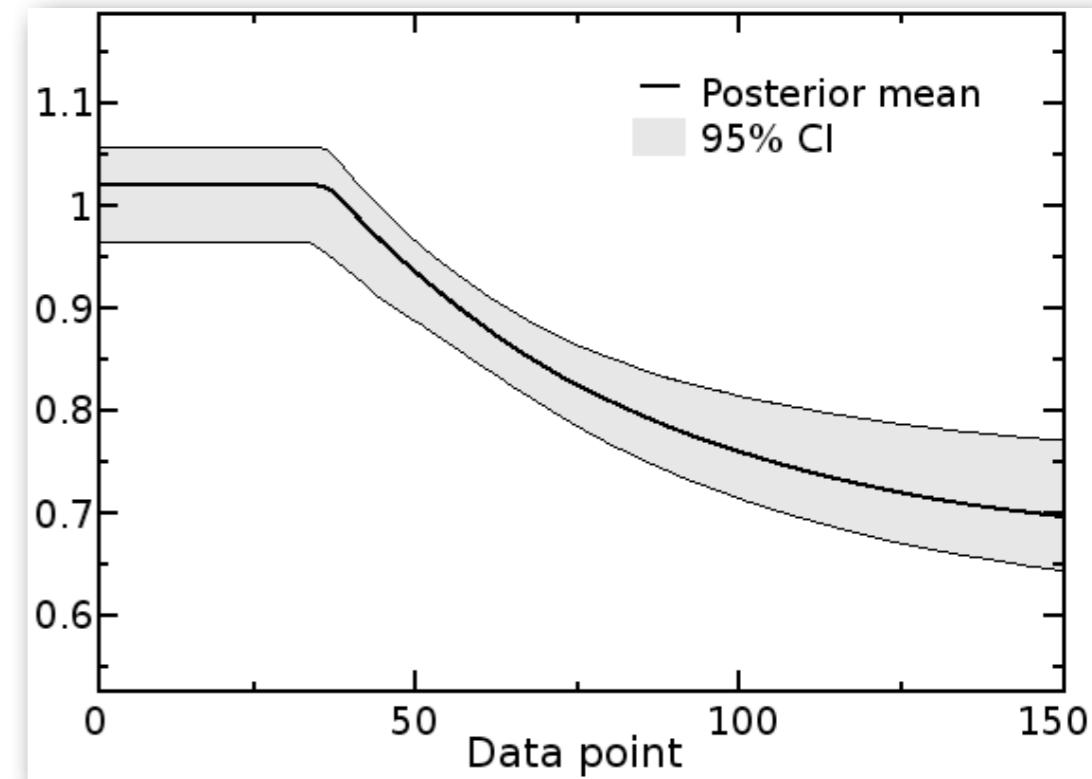
DOE Predictive Science Academic Alliance Program

- PECOS Center at UT Austin focuses on estimating uncertainties
- Quantifying uncertainties
 - ➔ Use experiments and models to determine simulation error bars



Uncertainty Quantification (UQ)

- **Since models will always incur errors, the best strategy is to quantify the errors**
 - ➔ In a simple sense, compute error bars for the solution
 - ➔ More broadly, CFD results are no longer deterministic “plots” but probabilistic distributions
- **The quantifiable error in the computations is termed uncertainty**
 - ➔ Expressed in terms of confidence in results, which are also computed



RANS Models for Scalar Flux

- **RANS scalar transport equation**

$$\frac{\partial \bar{\rho} \tilde{\phi}}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j \tilde{\phi}}{\partial x_j} - \frac{\partial}{\partial x_j} \left(\bar{\rho} D \frac{\partial \tilde{\phi}}{\partial x_j} \right) = - \frac{\partial \bar{\rho} \widetilde{u'_j \phi'}}{\partial x_j} + \widetilde{S(\phi)}$$

Scalar flux **Chemical source term**

→ Closures for the scalar flux needed

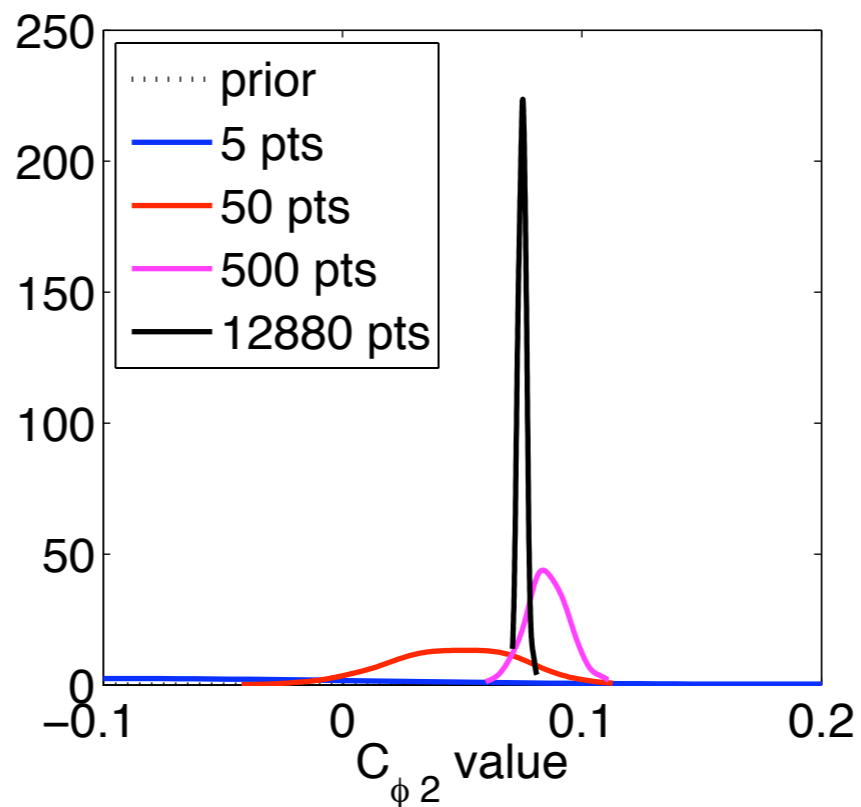
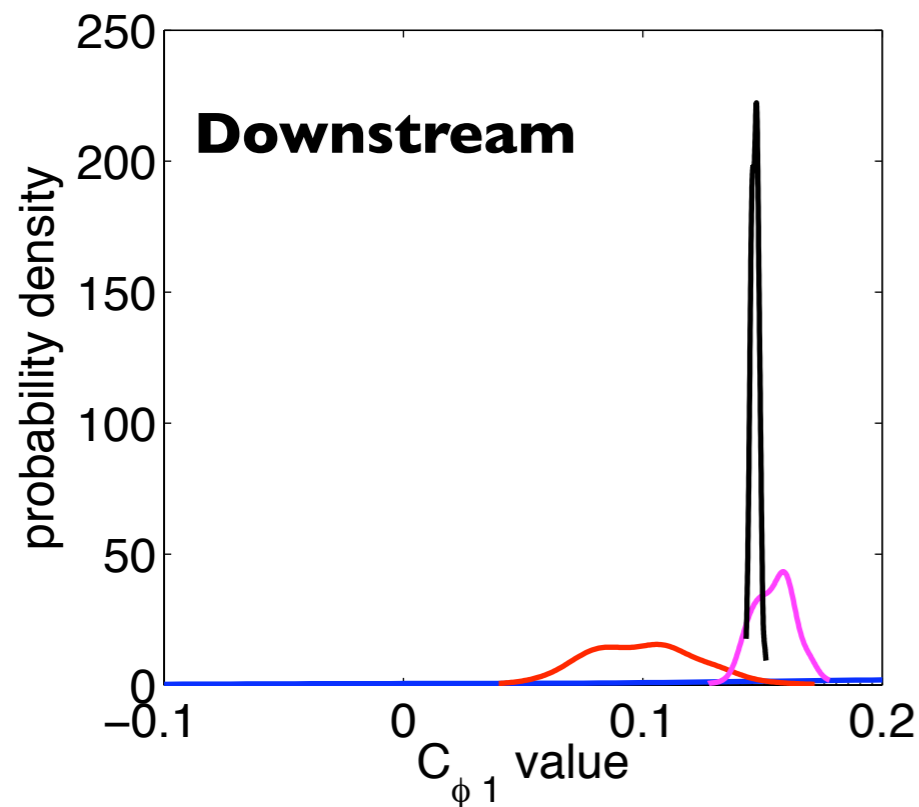
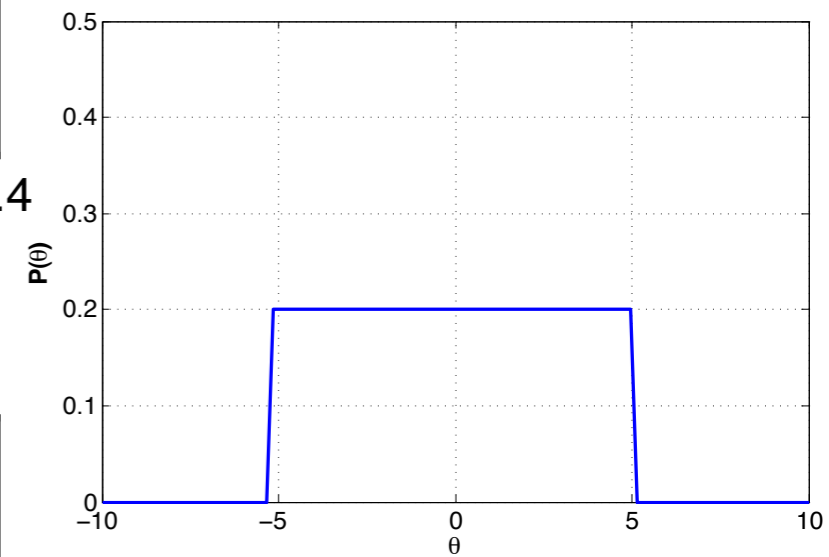
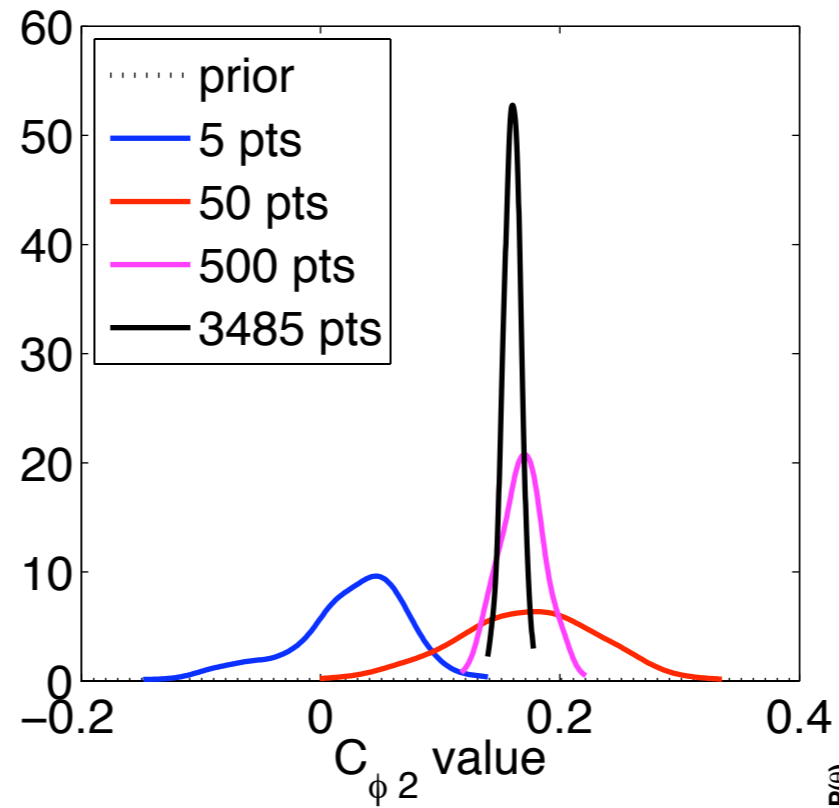
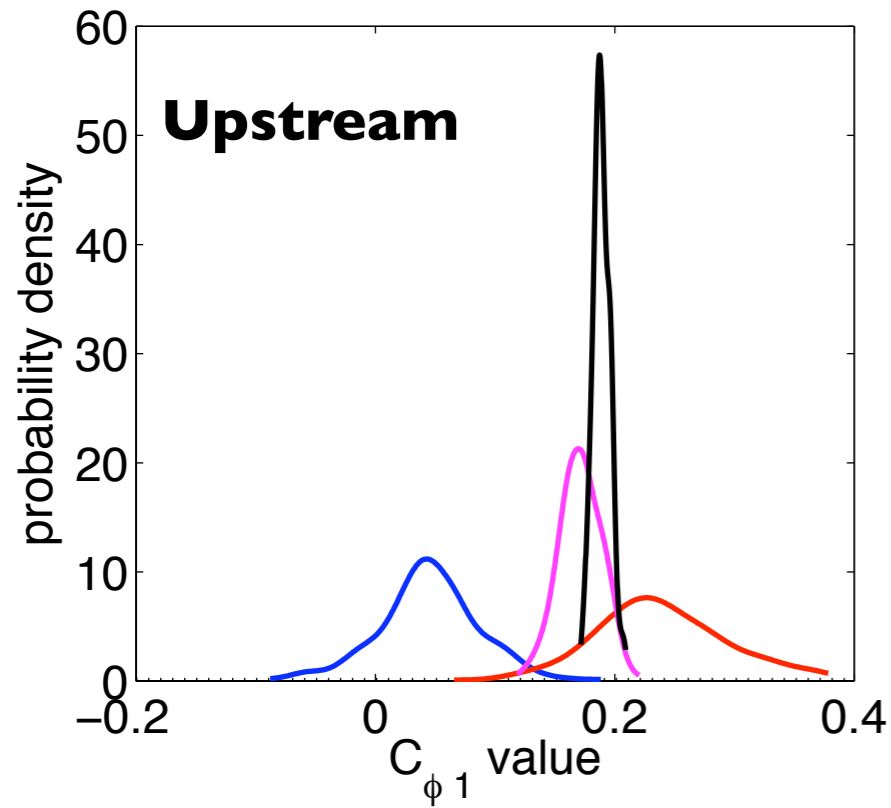
- **Several models considered**

→ E.g., Combination generalized gradient diffusion model

$$\widetilde{u'_i \phi'} = -\tau_T \left(C_{\phi 1} \widetilde{u'_i u'_j} + C_{\phi 2} \frac{\widetilde{u'_i u'_k} \widetilde{u'_k u'_j}}{k} \right) \frac{\partial \tilde{\phi}}{\partial x_j}$$

→ Model coefficients $(C_{\phi 1}, C_{\phi 2})$ need to be determined

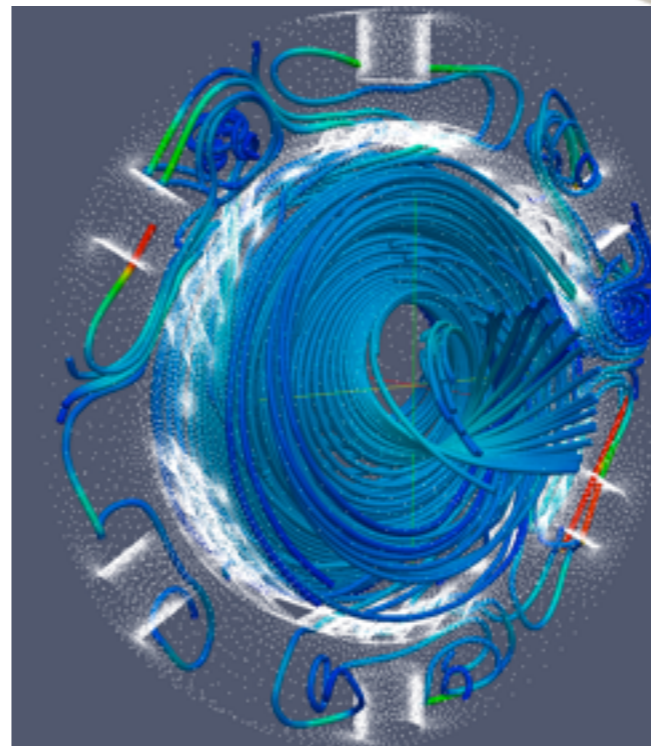
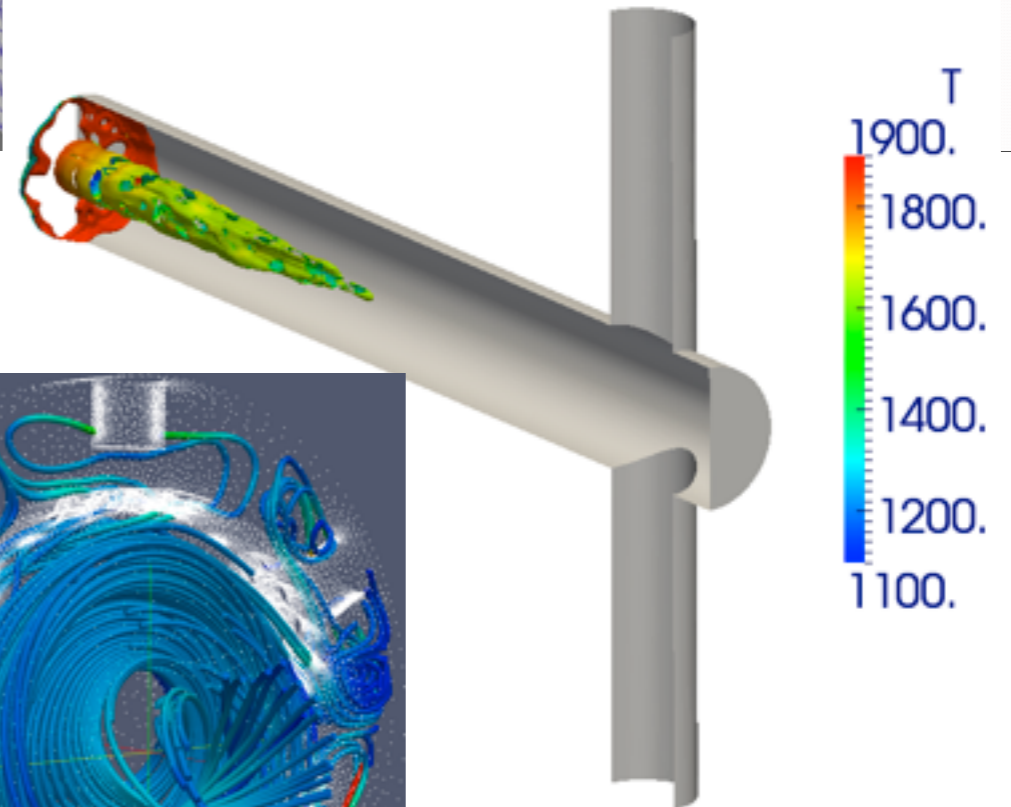
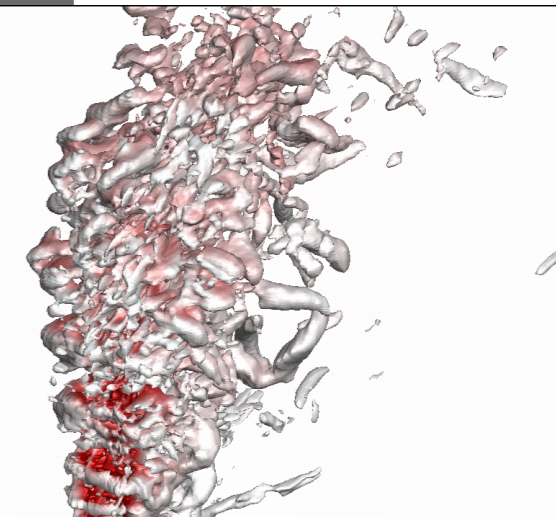
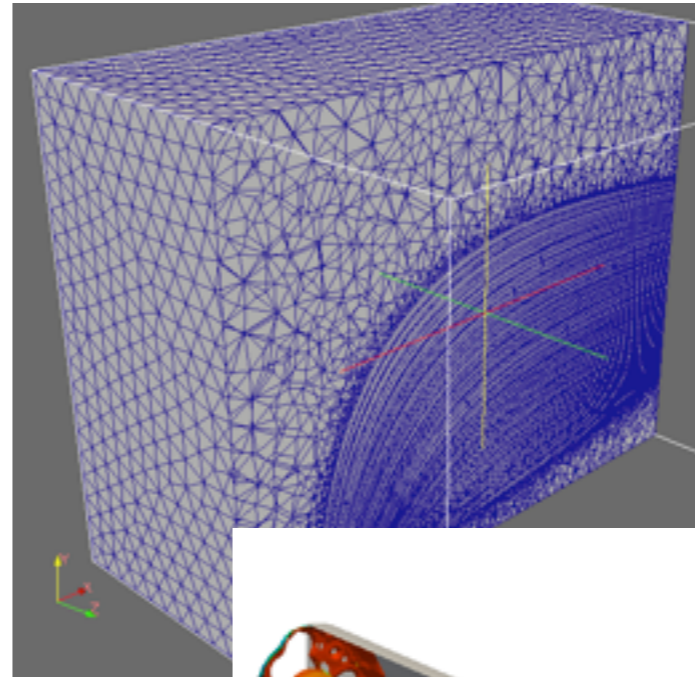
Probabilistic Description of RANS Model Constants



Prior

Technology Transfer Using OpenFOAM

- **Open source software**
- **Large-scale code modification**
 - ➔ Numerics changed to accommodate LES computations
 - ➔ New flow solvers for turbulent combustion problems
 - ➔ Arbitrary chemistry inclusion with chemkin-compatible interface



UT Gas Turbine Program

- **LES/RANS combined modeling approach**
 - ➔ LES for unsteady dynamics
 - ➔ Calibration-based RANS for parametric studies
- **Well-characterized experimental setup**
 - ➔ Simultaneous PIV/PLIF measurements under high pressure conditions
 - ➔ Pitched jets in crossflow with varying fuel compositions
- **Open source technology transfer**
 - ➔ OpenFOAM based transfer of models