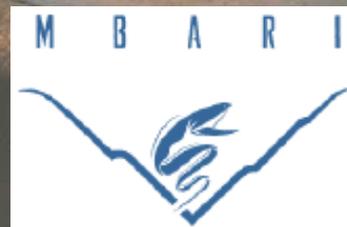


# Field Studies of CO<sub>2</sub>/Water Coflow Injection for Ocean Carbon Sequestration

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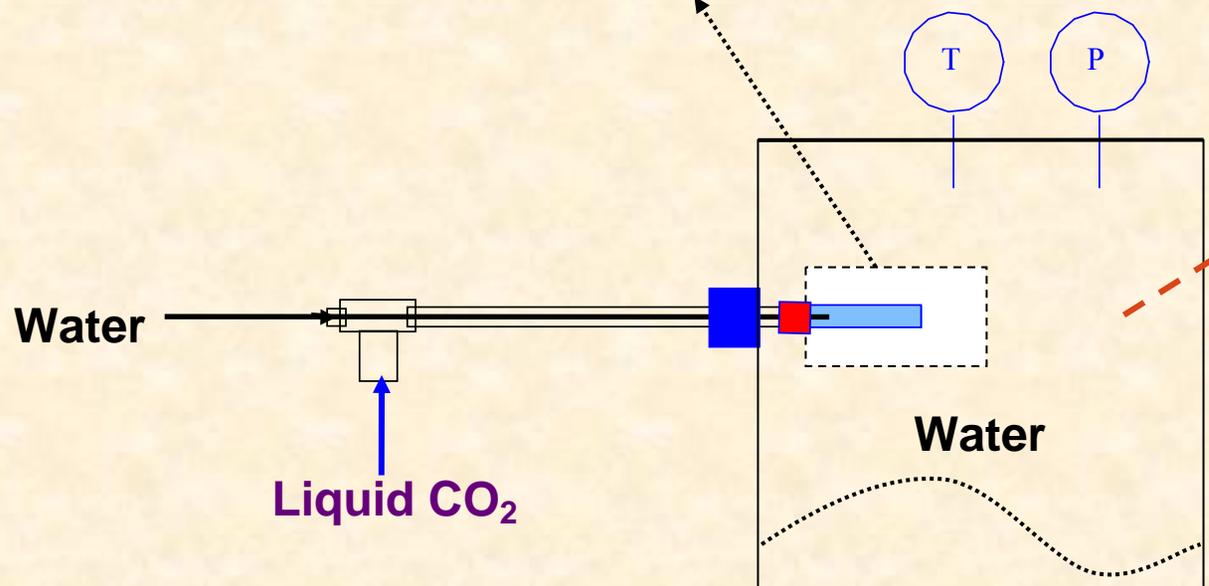
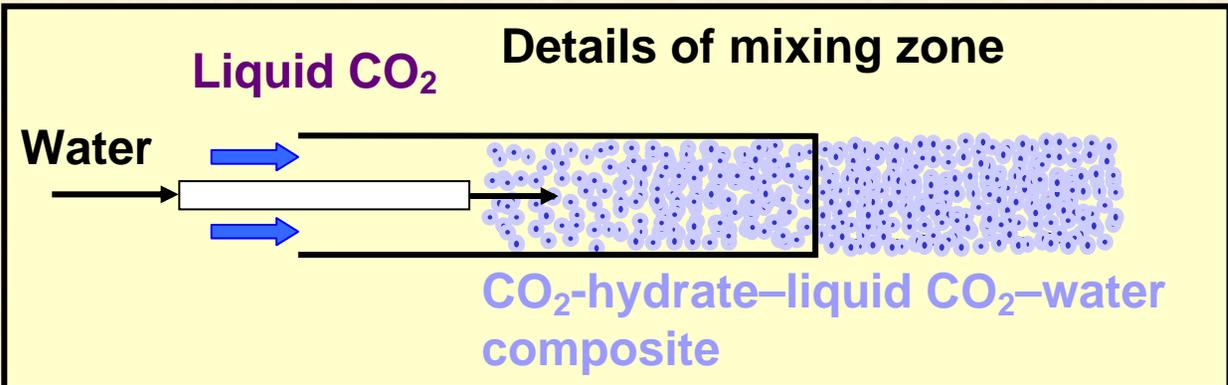


# Introduction

- Sinking CO<sub>2</sub> hydrate composite particles have been produced in the laboratory at pressures equivalent to ocean depths of 1000-1300 m.
- Field tests of a CO<sub>2</sub>/water coflow injector were conducted in Monterey Bay, CA, in 2002 and 2004 at depths of 1000-1300m.
- The objective was to demonstrate the continuous production of a sinking phase of CO<sub>2</sub> at intermediate ocean depths and observe its dissolution rate.
- A CO<sub>2</sub> hydrate dissolution model suggests that mass transfer through the hydrate layer is the rate limiting step.

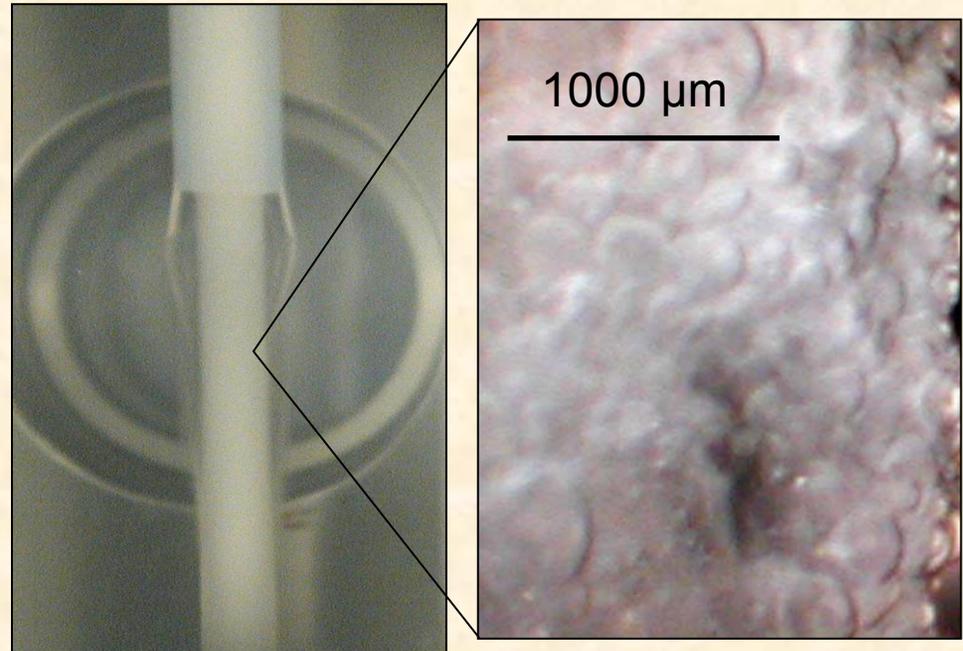
# The Continuous-Jet Hydrate Reactor

ORNL SPS  
(Seafloor Process Simulator)



(72-L high pressure vessel)

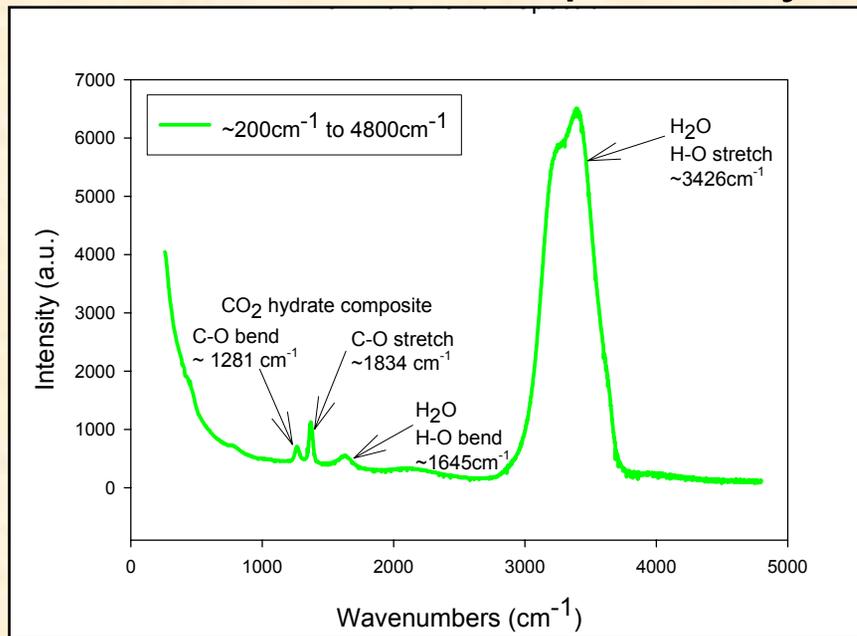
# Laboratory Results Demonstrate the Sinking CO<sub>2</sub> Phase



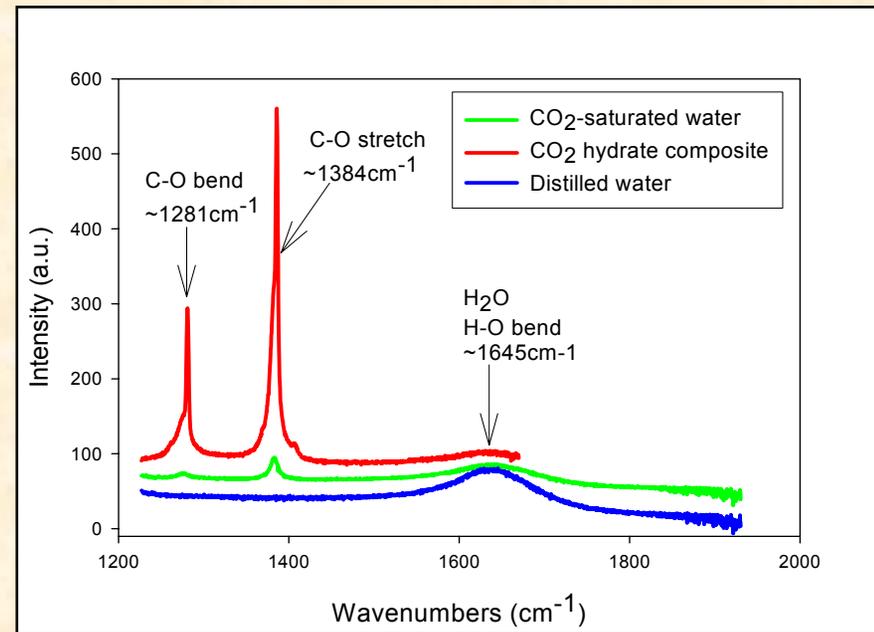
- Sinking CO<sub>2</sub> hydrate composite particles were demonstrated in the laboratory.
- Water injection capillaries used were 127 and 254 μm.
- The next step was characterization of composite, then field experiments to confirm results.

# CO<sub>2</sub> Phases Identified in Composite

- The C-O Raman shifts demonstrate the presence of CO<sub>2</sub> hydrate in the composite.
- CO<sub>2</sub> hydrate has two peaks at  $\sim 1281 \Delta\text{cm}^{-1}$  and  $\sim 1384 \Delta\text{cm}^{-1}$  for the C-O bend and C-O stretch, respectively.
- Liquid CO<sub>2</sub> peaks are shifted up-field to  $\sim 1283 \Delta\text{cm}^{-1}$  and  $\sim 1387 \Delta\text{cm}^{-1}$ , respectively.

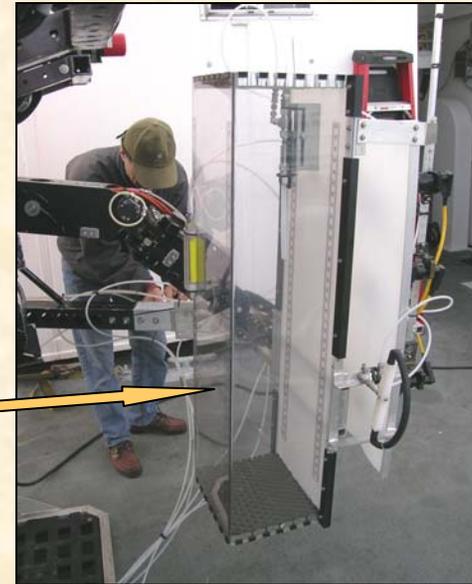
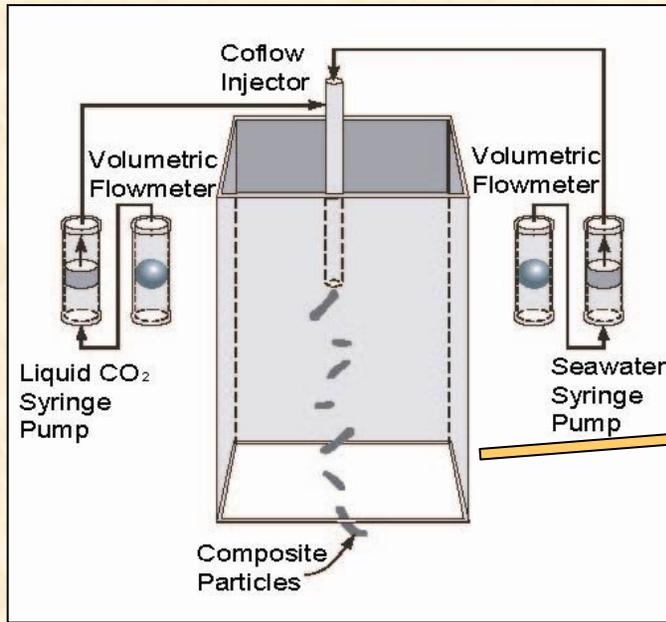


Wide range spectrum of CO<sub>2</sub> hydrate composite



Comparison of CO<sub>2</sub> spectra in hydrate and in water

# Ocean Injections in Monterey Bay, Ca



“Bubble box” for particle injection

Plexiglass bubble box mounted on the ROV *Ventana*

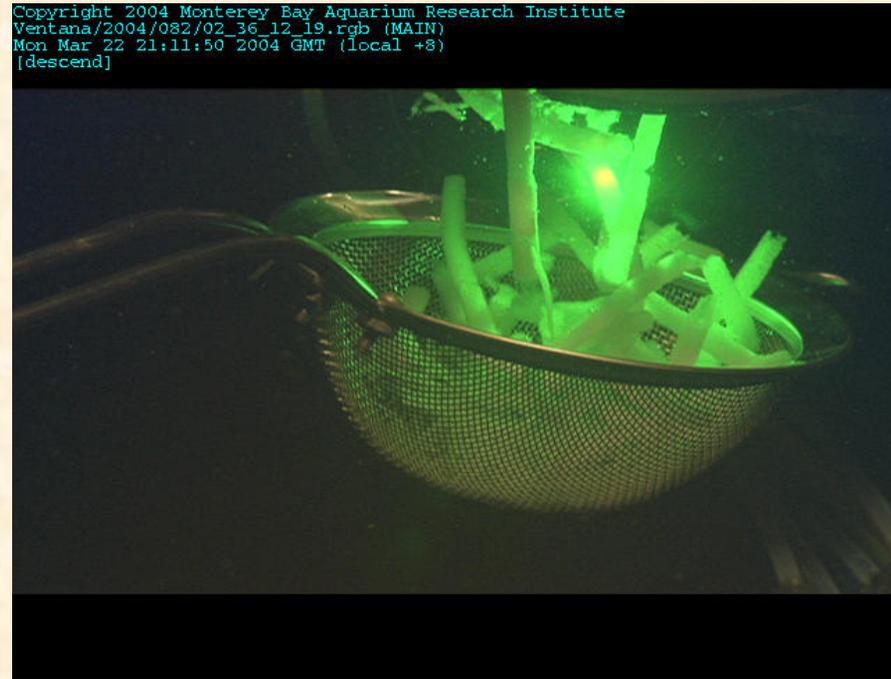


MBARI R/V Point Lobos



ROV Ventana

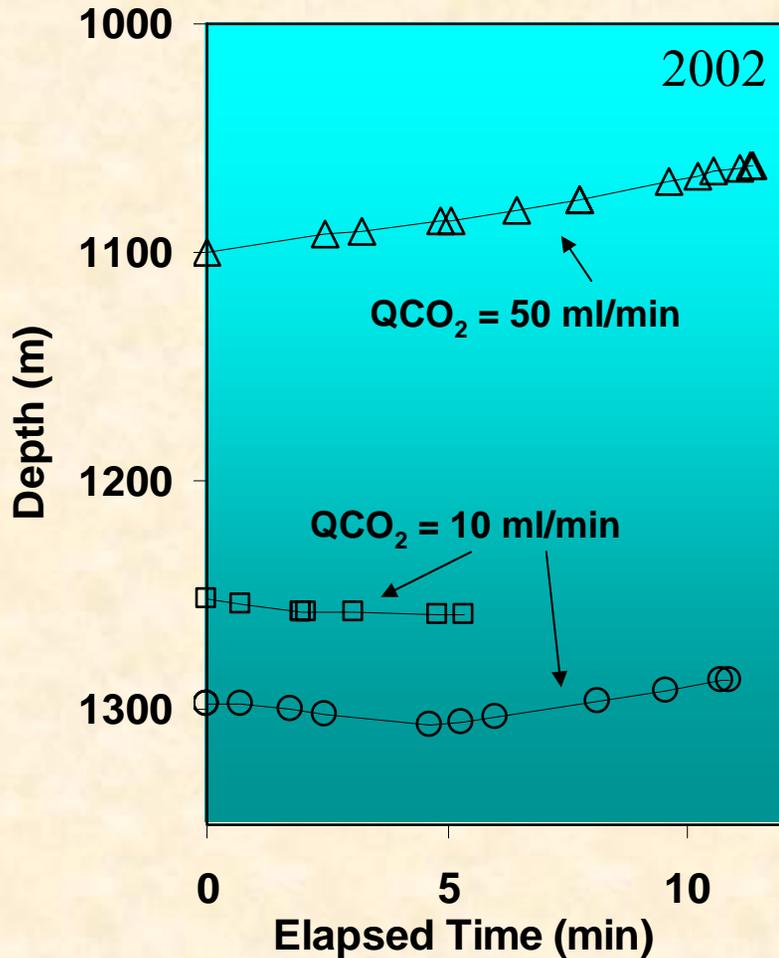
# 2004 Ocean Injection Results



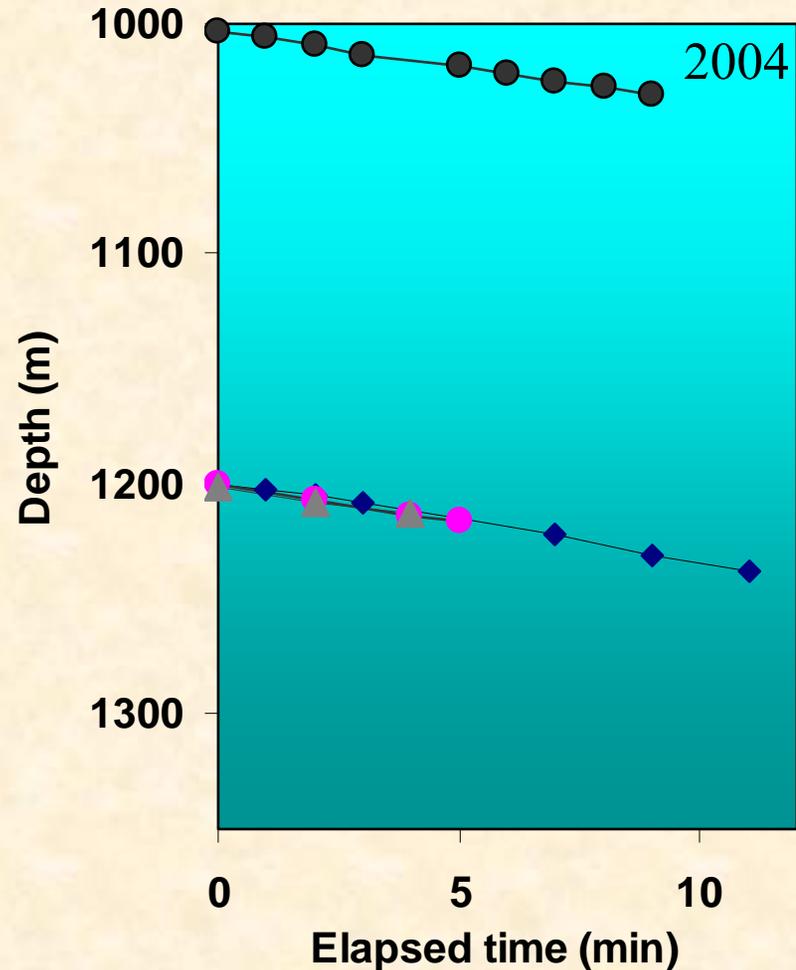
Copyright 2004 Monterey Bay Aquarium Research Institute  
Ventana/2004/082/02\_36\_12\_19.rgb (MAIN)  
Mon Mar 22 21:11:50 2004 GMT (local +8)  
[descend]

- A 381  $\mu\text{m}$  capillary was used to inject water at 140 ml/min.
- $\text{CO}_2$  was injected at 26-36 ml/min.
- Hydrate composite particles were injected at 1000m and at 1200m.

# 2004 Particles Sank Consistently

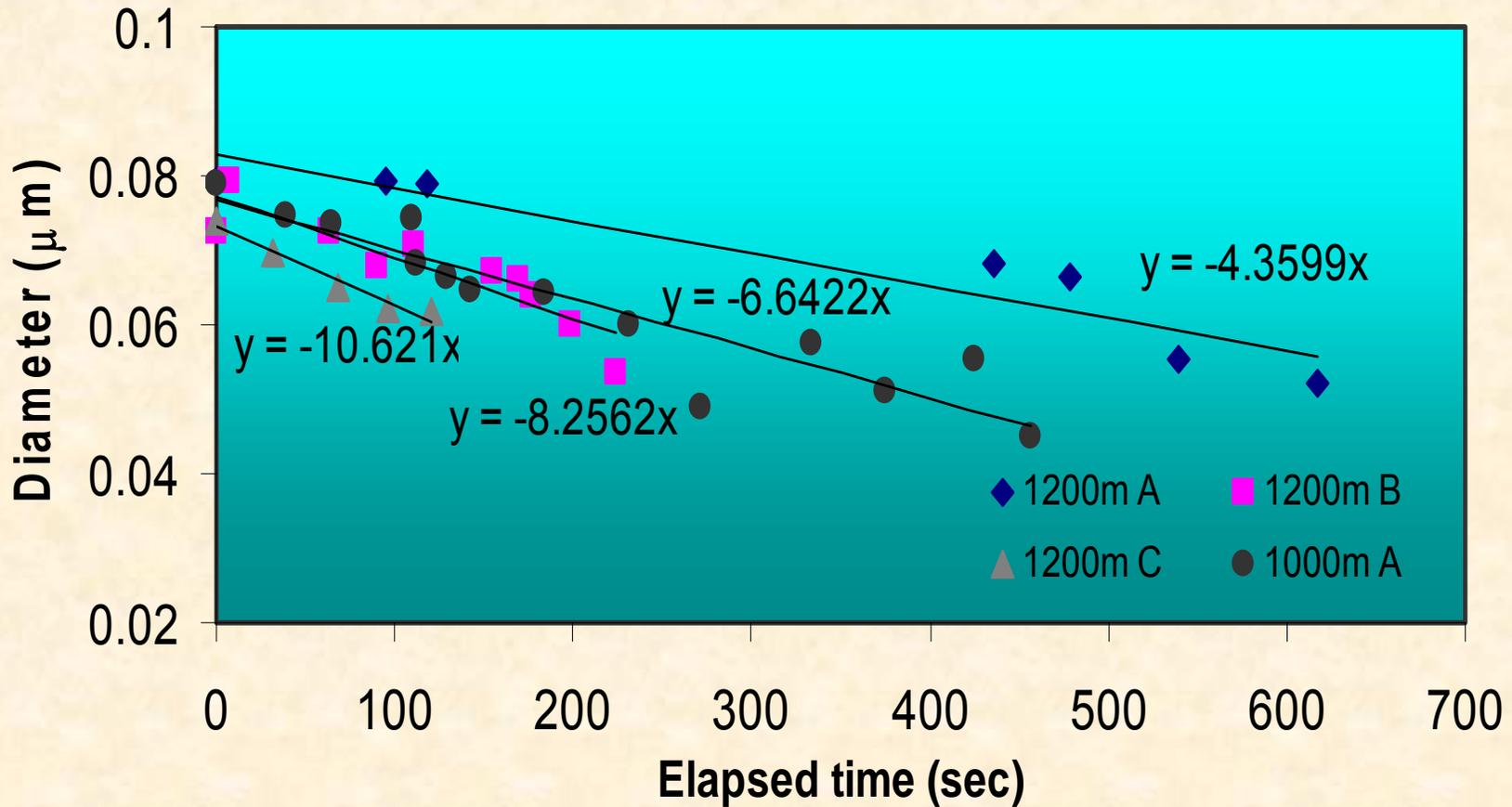


water capillary i.d. = 254  $\mu\text{m}$   
outer tube i.d. = 6 mm  
 $H_2O$  flow rate = 50 ml/min  
 $CO_2$  flow rates = 10-50 ml/min



water capillary i.d. = 381  $\mu\text{m}$   
outer tube i.d. = 9 mm  
 $H_2O$  flow rate = 140 ml/min  
 $CO_2$  flow rates = 26-36 ml/min

# 2004 Ocean Injection Results



- Composite particles shrank at 4.4-10.6  $\mu\text{m/s}$ .
- Rehder et al. (2004) reported a pure  $\text{CO}_2$  hydrate dissolution rate of 0.94-1.20  $\mu\text{m/sec}$  at 1028m depth.

# Comparison of 2002 and 2004 Particles

	2004 Injections		2002 Injections		
depth (m)	1200 (A)	1000 (A)	1100	1250	1300
behavior	Sink	sink	float	sink	neutral
sinking rate (m/min)	3.5	3.1	-3.6 (float)	1.2	0
est. composite density (g/cm <sup>3</sup> )	1.04(8)	1.04(6)	1.02(1)	1.04(5)	1.03(4)
est. composite conversion (x)	0.25	0.26	0.12	0.19	0.16
Composite shrink rt. (μm/sec)	4.4	6.6	5.3	7.4	4.1
CO <sub>2</sub> DR (μmol/cm <sup>2</sup> s)	0.76	1.29	2.97	1.38	0.76

- 2004 particles appear to have more CO<sub>2</sub> converted to hydrate.
- Rehder et al. (2004) report pure CO<sub>2</sub> hydrate dissolution rate of 0.36 0.46 μmol/cm<sup>2</sup>s and Brewer et al. (2002) report the dissolution rate of a rising CO<sub>2</sub> droplet as 3 μmol/cm<sup>2</sup>s.

Rehder et al. *Geochim. Cosmochim. Acta* **2004**, 68, 285-292.

Brewer et al. *Environ. Sci. Technol.* **2002**, 36, 5441-5446.

# Uncertainty on Hydrate Conversion: Future Experiments

Variables	Values	Est. Hydrate Conversion
Particle Drag Coefficient	0.33	0.25
	1	0.46
	4	1.09
CO <sub>2</sub> Hydrate Density (g/cm <sup>3</sup> )	1.143 <sup>a</sup>	0.25
	1.12 <sup>b</sup>	0.30
	1.10 <sup>c</sup>	0.37
CO <sub>2</sub> /H <sub>2</sub> O in Particle	0.19	0.25
	0.46	0.21

- Drag Coefficient:  
Particles may act more like rigid cylinders  $\approx$  higher drag
- Hydrate Density:  
Precise value of CO<sub>2</sub> hydrate density still unknown
- CO<sub>2</sub>/H<sub>2</sub>O in particle:  
There may be significant water loss during injection

<sup>a</sup> Circone et al. *J. Phys. Chem. B*, 2003

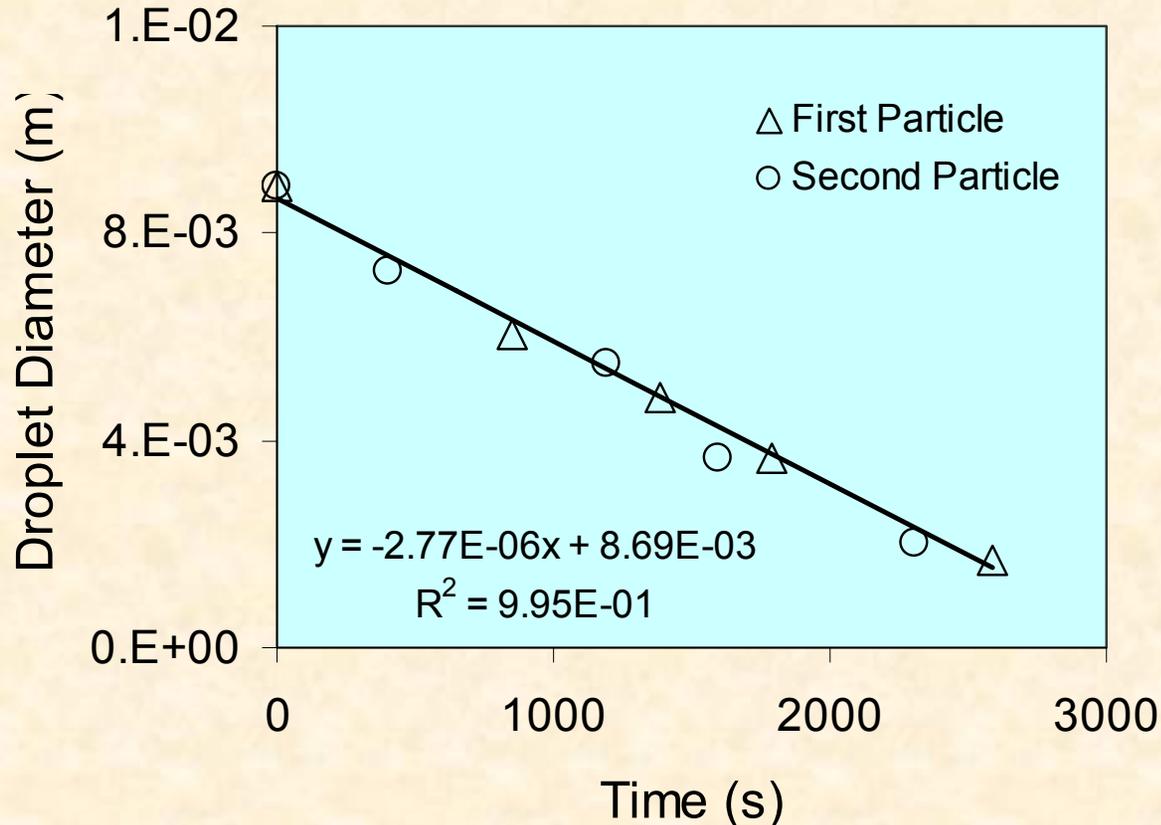
<sup>b</sup> Holder et al. *Environ. Sci. Technol.* 1995

<sup>c</sup> Aya et al. *Energy* 1997

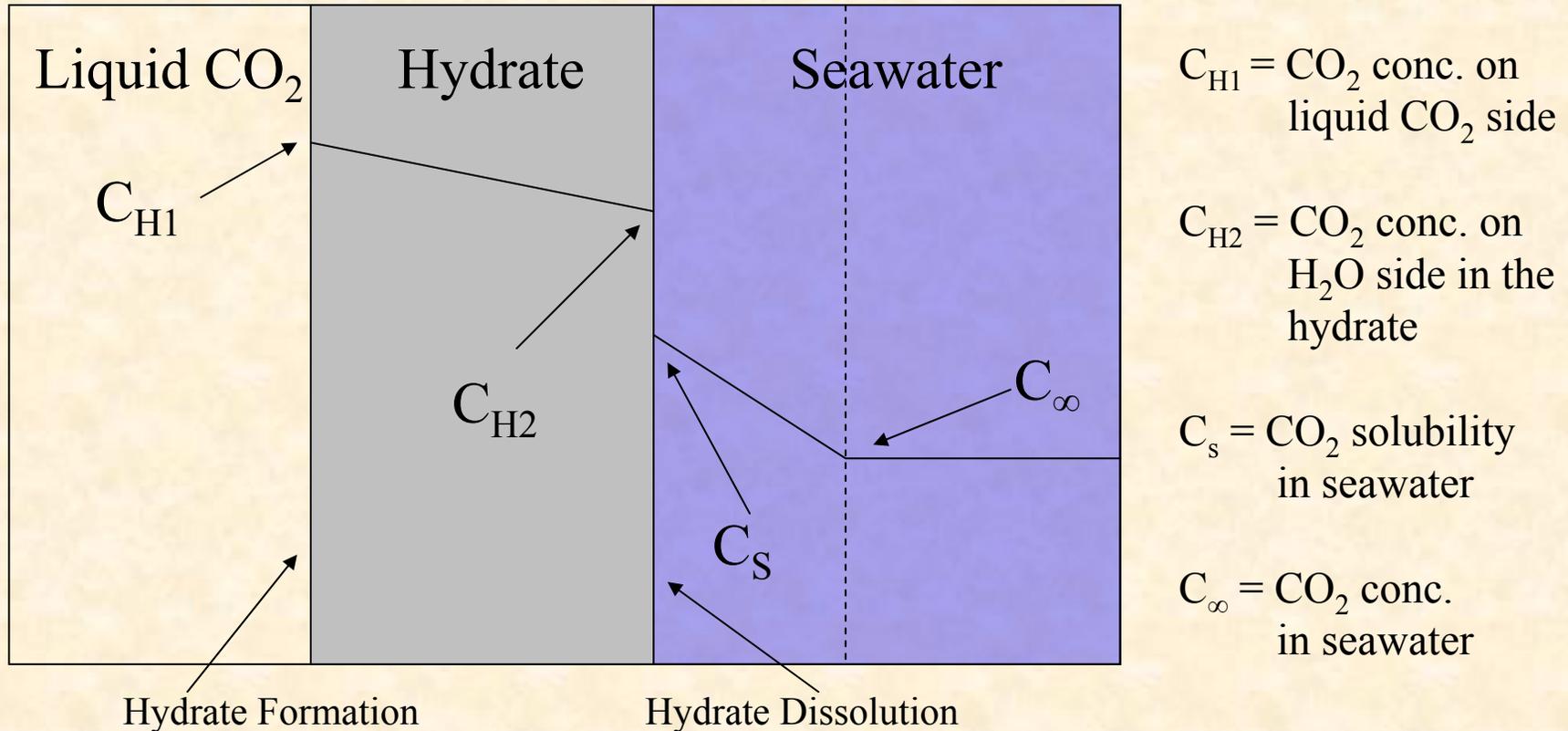
# Dissolution Mechanism of Hydrate Covered CO<sub>2</sub> Droplets

Modeling CO<sub>2</sub> dissolution in rising droplets of hydrate-covered CO<sub>2</sub> droplets released by Brewer et al. (ES&T, 2002).

Focus of study is on the controlling step in CO<sub>2</sub> dissolution.



# Heterogeneous Dissolution Model to Account for Multiple Phases\*



- Hydrate layer may be impermeable (diffusion limited) or contain permeable capillaries\*

\* proposed by Mori and Mochizuki (Energy Conv. Manage., 1998)

# Determination of the Limiting Step in Hydrate Dissolution

Overall dissolution ( $\mathbf{k}_T$ ) is a function of hydrate layer mass transfer ( $\mathbf{k}_H$ ) and CO<sub>2</sub> dissolution mass transfer ( $\mathbf{k}_D$ )\*

$$J = \mathbf{k}_T (C_{H1} - C_{\infty}) A_p$$

$J$  = molar flow of CO<sub>2</sub>

$C_{H1}$  = CO<sub>2</sub> conc. on CO<sub>2</sub> side

$C_{\infty}$  = CO<sub>2</sub> conc. in seawater

$A_p$  = reaction surface area

where  $\mathbf{k}_T = s k_H k_D / (k_H + s k_D$

$s$  = constant defined by  $C_{H2} = s C_s$

$C_{H2}$  = CO<sub>2</sub> conc. on H<sub>2</sub>O side in the hydrate

$C_s$  = CO<sub>2</sub> solubility in seawater

to determine  $\mathbf{k}_D$ :  $Sh = 2 + 0.6 Re^{0.5} Sc^{0.333}$  \*\*

$Sh$  = Sherwood Number =  $\mathbf{k}_D d_p / D$ ,  $d_p$  = droplet diameter,  $D$  = CO<sub>2</sub> diffusivity

$Re$  = Reynolds Number =  $v d_p \rho / \nu$ ,  $\nu$  = seawater kinematic viscosity

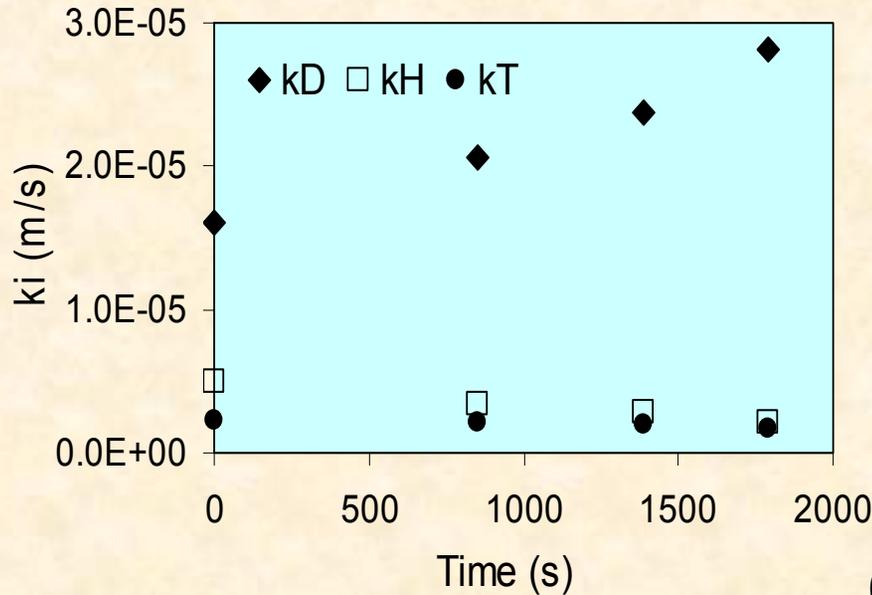
$Sc$  = Schmidt Number =  $\nu / D$

↳ use values for  $\mathbf{k}_T$  and  $\mathbf{k}_D$  to solve for  $\mathbf{k}_H$

\* from Ogasawara et al., (Energy and Fuels, 2001)

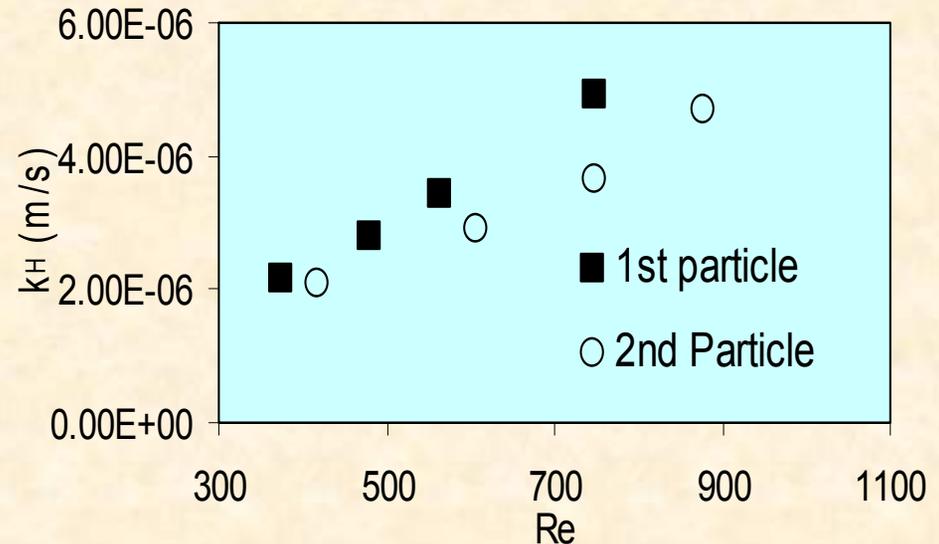
\*\* from Hirai et al. (Energy, 1997)

# Mass Transfer through the Hydrate Layer is the Limiting Dissolution Step

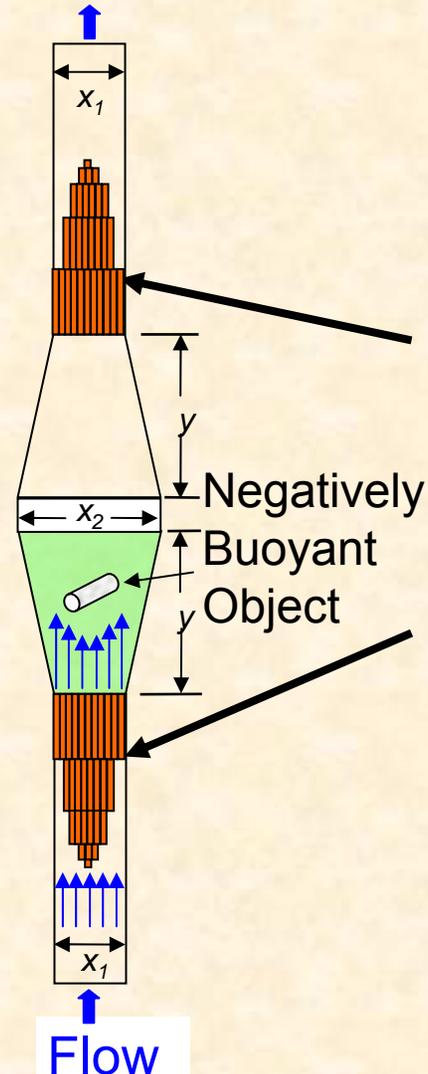


$k_H$  appears to be the controlling step in mass transfer of  $\text{CO}_2$

A positive relationship between  $k_H$  and the droplet Reynolds Number suggests the existence of capillaries in hydrate

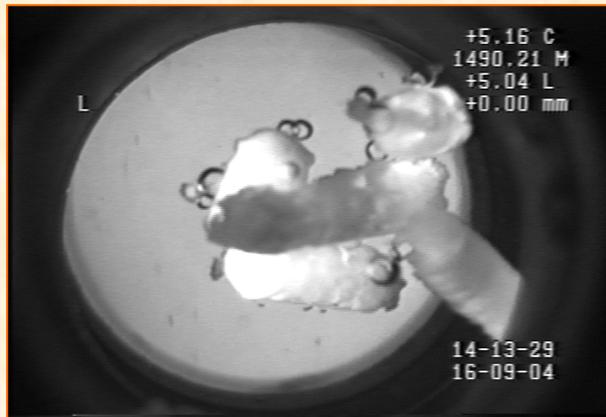


# Collaborative Work with Dr. Warzinski of NETL Using the High-Pressure Water Tunnel Facility

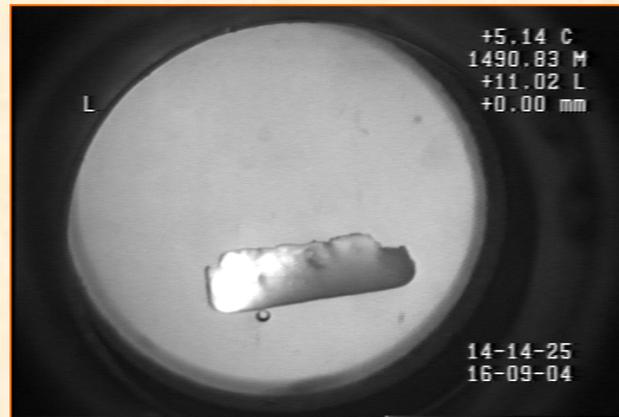


Flow Conditioning Elements

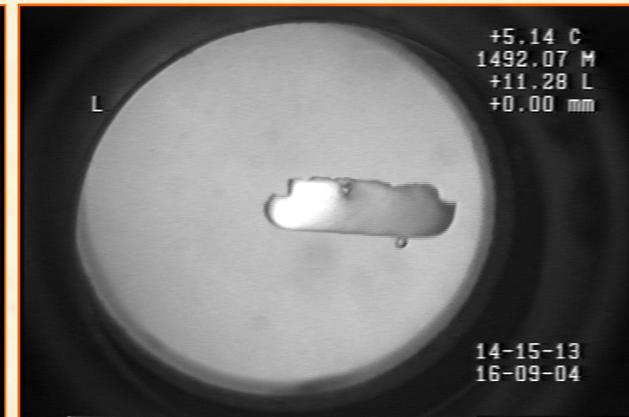
# Particle Measurements in the HWTf



Elapsed Time = 103 s



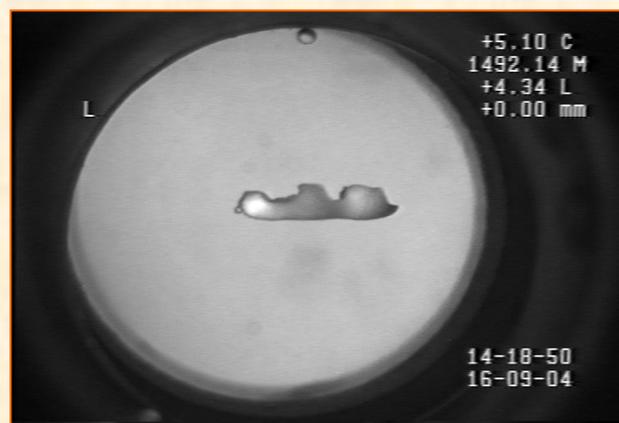
Elapsed Time = 157 s



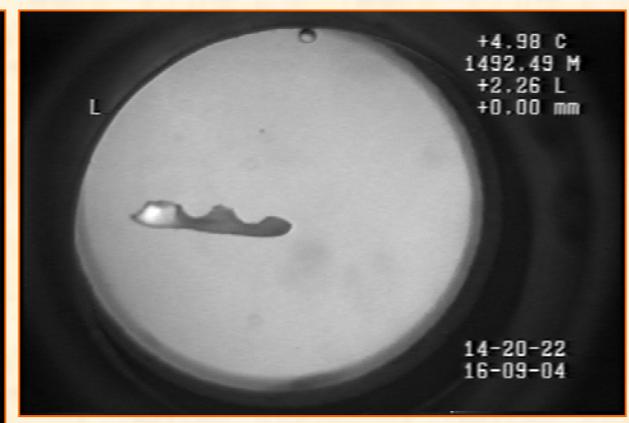
Elapsed Time = 205 s



Elapsed Time = 322 s



Elapsed Time = 422 s

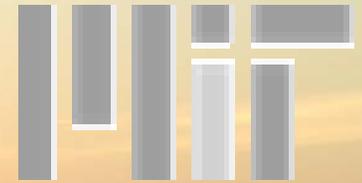


Elapsed Time = 514 s

**For more details on this work, see poster #85**



# Summary



- Ocean injections have demonstrated the formation of composite solid particles containing CO<sub>2</sub> hydrate, water, and liquid CO<sub>2</sub> at intermediate depths from the co-flow injection of ambient seawater and liquid CO<sub>2</sub>
- Particles made by the larger injector in 2004 sank at a rate of 3 m/min which should carry CO<sub>2</sub> to deeper waters and lead to longer sequestration.
- Mass transfer modeling suggests that mass transfer through the hydrate layer is the controlling step in hydrate dissolution.

## Acknowledgment



Ocean Carbon Sequestration Program, OBER  
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