

Tunable Diode Laser Sensors to Monitor Temperature and Gas Composition in High Temperature Coal Gasifiers

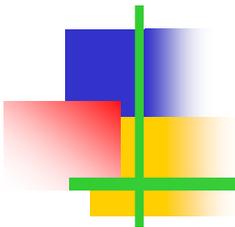
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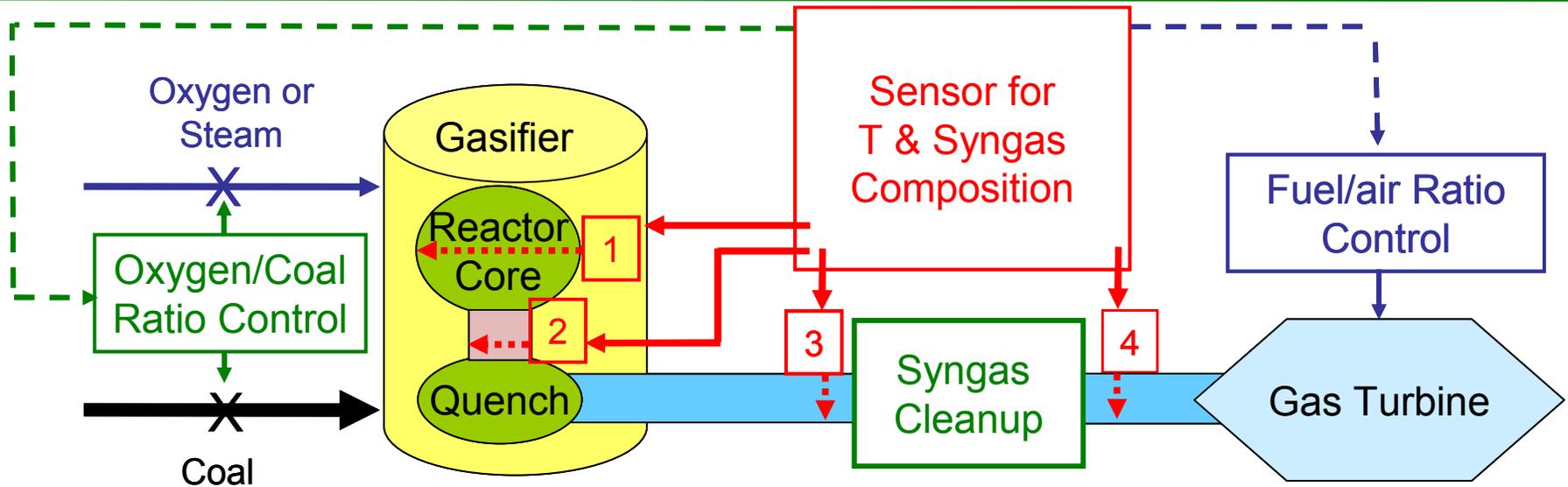
Professor Kevin J. Whitty and Randy J. Pummill

Institute for Clean and Secure Energy, The University of Utah

DoE NETL Kick-off December 16, 2009



- Vision for tunable diode laser (TDL) sensors
- Goals
- Challenges
- University of Utah sensor test bed
- Stanford sensor concept
 - TDL fundamentals
 - Prior measurements reduce risk
- Proposed work plan
- Current status



Vision: Sensor for control signals to optimize gasifier output and gas turbine input

- Goals:**
- Two control signals investigated: gas temperature and heating value
 - Measurements of CO, CH₄, CO₂, and H₂O provide heating value
 - H₂ determined by gas balance and H₂S ignored
 - Gas temperature determined by ratio of H₂O measurements
 - Four sensor locations investigated: (1) reactor core, (2) pre-quench, (3) post-quench, and (4) post-particulate clean-up
 - Locations 1 & 2 yield faster control, but have the biggest challenges

- ▶ Gasifier pressure, temperature, particulate, and slag present window difficulties
 - Successful preliminary measurements in Utah fluidized bed reactor provide guidance for next generation window design
 - Fiber-coupled lasers require modest clear aperture
 - Stanford modulation schemes can accommodate time varying window transmission
- ▶ High pressure broadens spectral features making absorption difficult
 - Prior success for high-pressure measurements in IC engines, laboratory gas cells, and behind shock waves provides design criteria for modulation schemes (reduces risk)
- ▶ Particulate scattering attenuates laser transmission making absorption difficult
 - Prior success in Utah fluidized-bed reactor provides proof-of-concept

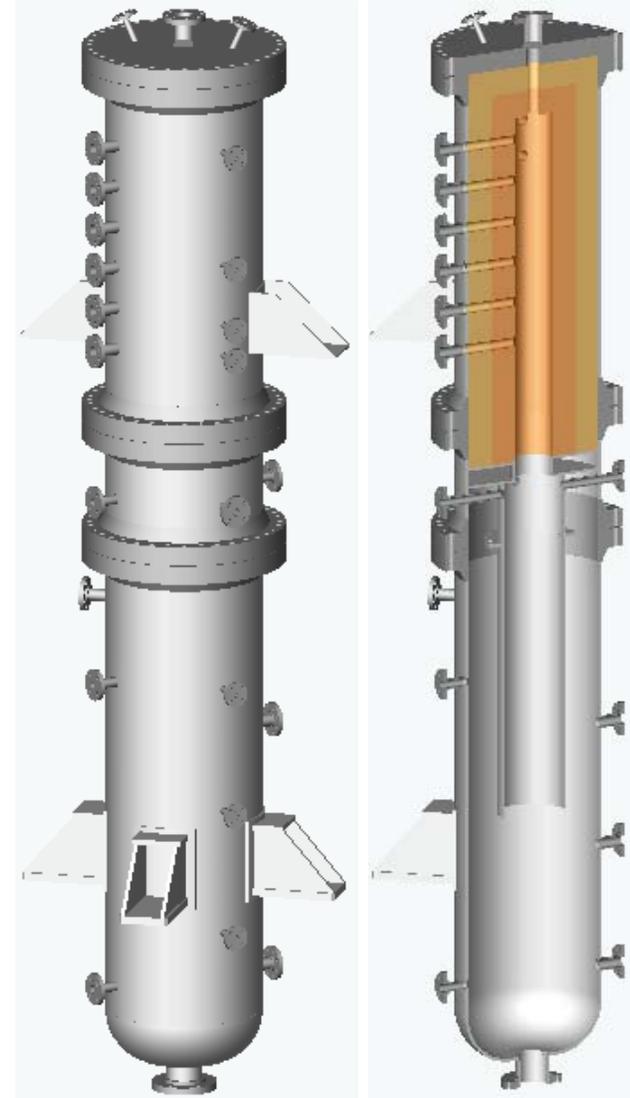
Prior work reduces risk, but gasifier has a unique environment: Hence demonstration measurements in large-scale gasifier at Utah are crucial to research effort



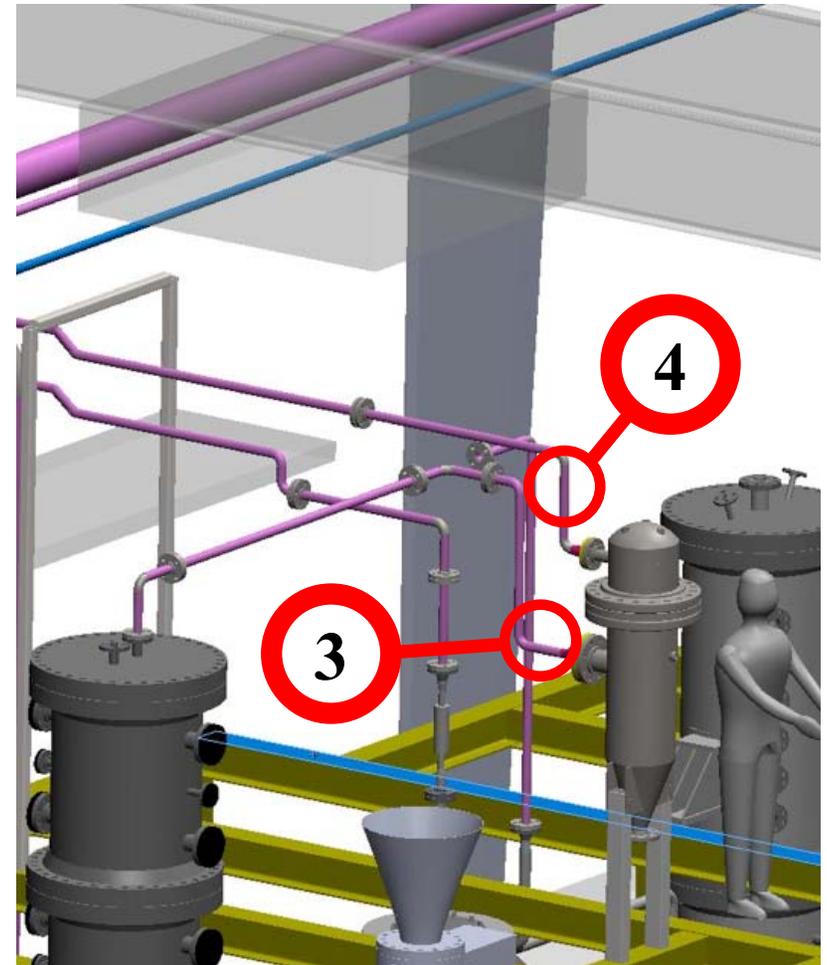
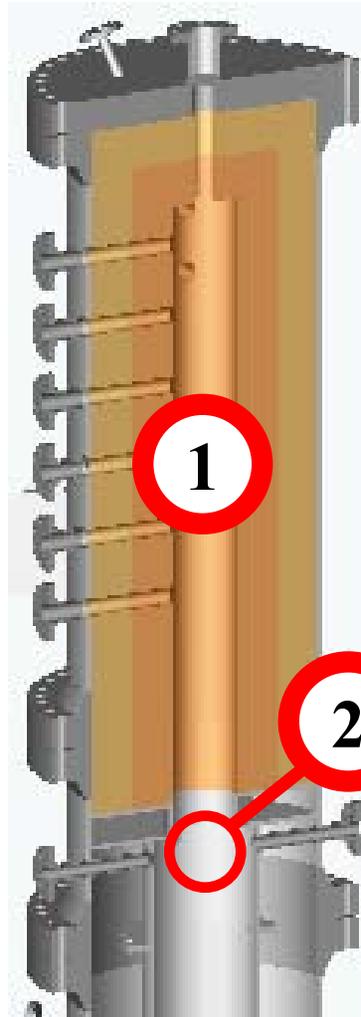
**Pressurized
Fluidized Bed
Gasifier**

**Pressurized
Entrained-Flow
Gasifier**

- Max. 450 psi
- Max. 3100 °F
- Throughput (coal)
 - 1 ton/day
 - 0.4 MW
- Overall dimensions
 - 17 feet tall
 - 30 inch vessel
- Reactor dimensions
 - 8 inch ID
 - 60 inch length
- Analytical
 - Continuous analyzer for $H_2/CO/CO_2/CH_4$
 - GC for 18 gases



- Location 1
 - Reactor “core”
 - ~2600°F / 250 psi
 - Molten slag
- Location 2
 - Pre-quench
 - ~2000°F / 250 psi
 - No slag blockage
- Location 3
 - Post-quench
 - ~250°F / 250 psi
 - Possible particles
- Location 4
 - Post filter
 - ~200°F / 250 psi
 - Particle-free



- Utilizes cheap, robust and portable TDL light sources and fiber optics
- Can yield multiple properties: species, T, P, V, & \dot{m} in real-time over wide conditions
 - T to 8000K, P to 50 atm, V to 15km/sec, multiphase flows, overcoming strong emission, scattering, vibration, and electrical interference
- Proven in harsh environments and large-scale systems:
 - Aero-engine inlets, scramjets, pulse detonation engines, IC engines, arcjets, gas turbine combustors, shock tunnels, coal-fired combustors, rocket motors,....
- Potential use in control of practical systems

IC-Engines @ Sandia NLL



Mattison et al., *Proc. Comb Symposium* **31** (2007)

SCRAMJET @ WPAFB



Rieker et al., *Applied Optics* **48** (2009)

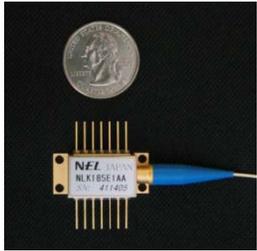
PDE at NPS



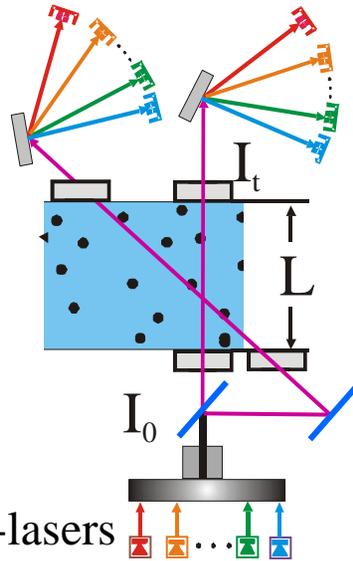
Brophy et al. *J Propulsion & Power* **22** (2006)

- TDL absorption: non-intrusive, time-resolved *line-of-sight* measurements

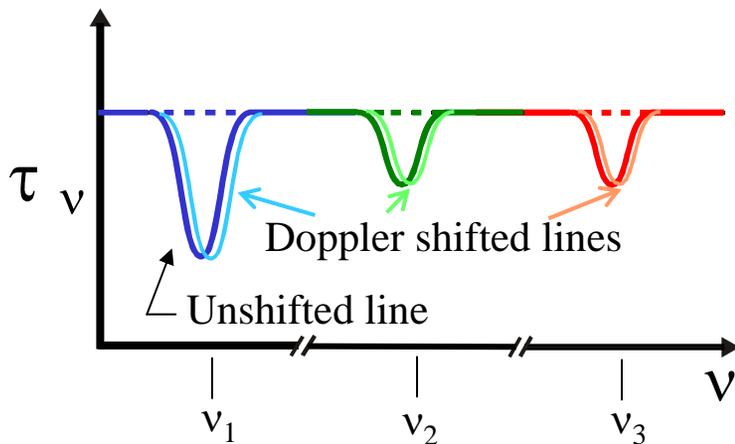
Fiber-coupled lasers are small and robust



Visible & near-IR λ 's



Multiplexed-lasers



- Beer-Lambert relation

$$\tau_v \equiv \frac{I_t}{I_o} = \exp(-\underbrace{k_v \cdot L}_{\text{absorbance}}) = \exp(-n_i \cdot \sigma_v \cdot L)$$

- Spectral absorption coefficient

$$k_v = S(T) \cdot \Phi(T, P, \chi_i) \cdot \chi_i \cdot P$$

- Wavelength-multiplexing for *multi-parameters*

- Ratios of two (or more) lines yield T

- T and τ_v yield χ_i (mole fraction) or n_i or ρ

- V from Doppler shift of spectra

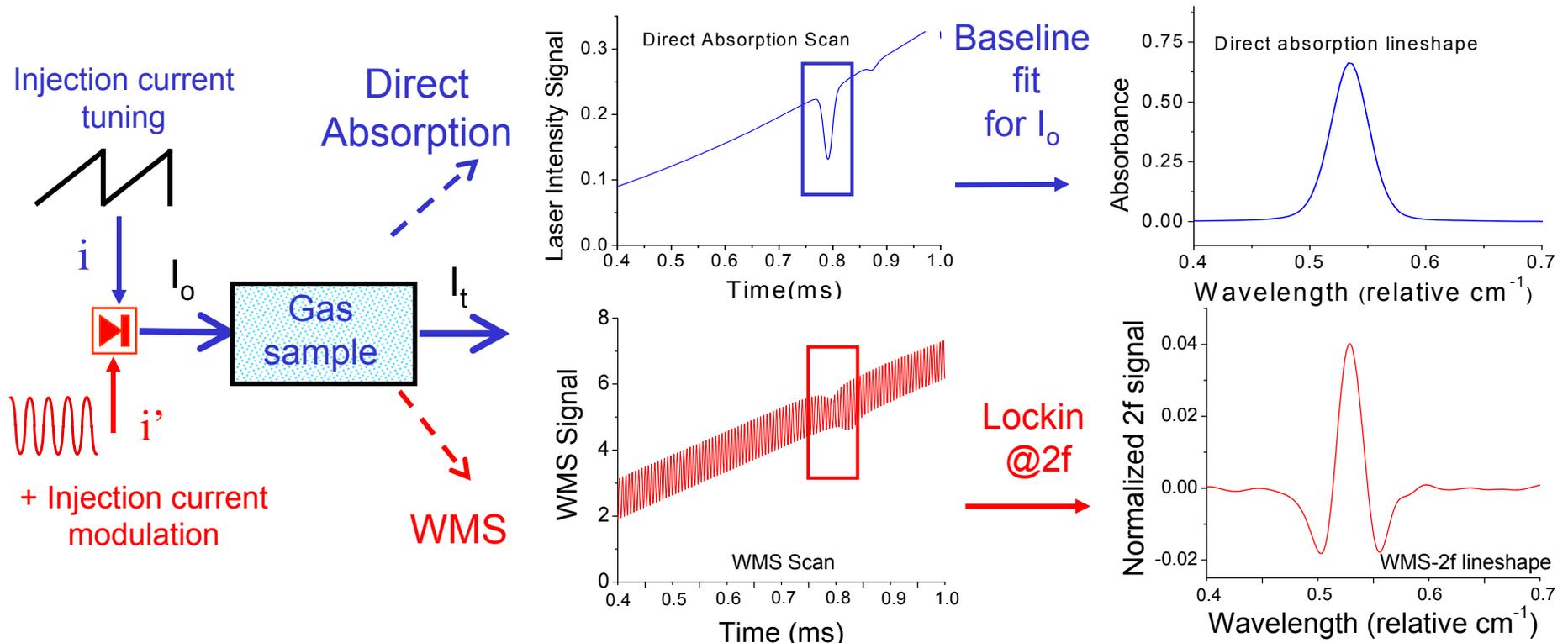
- Mass and momentum flux from ρ and V

- *Many-line* data for non-uniform $T(x)$, $X_i(x)$...

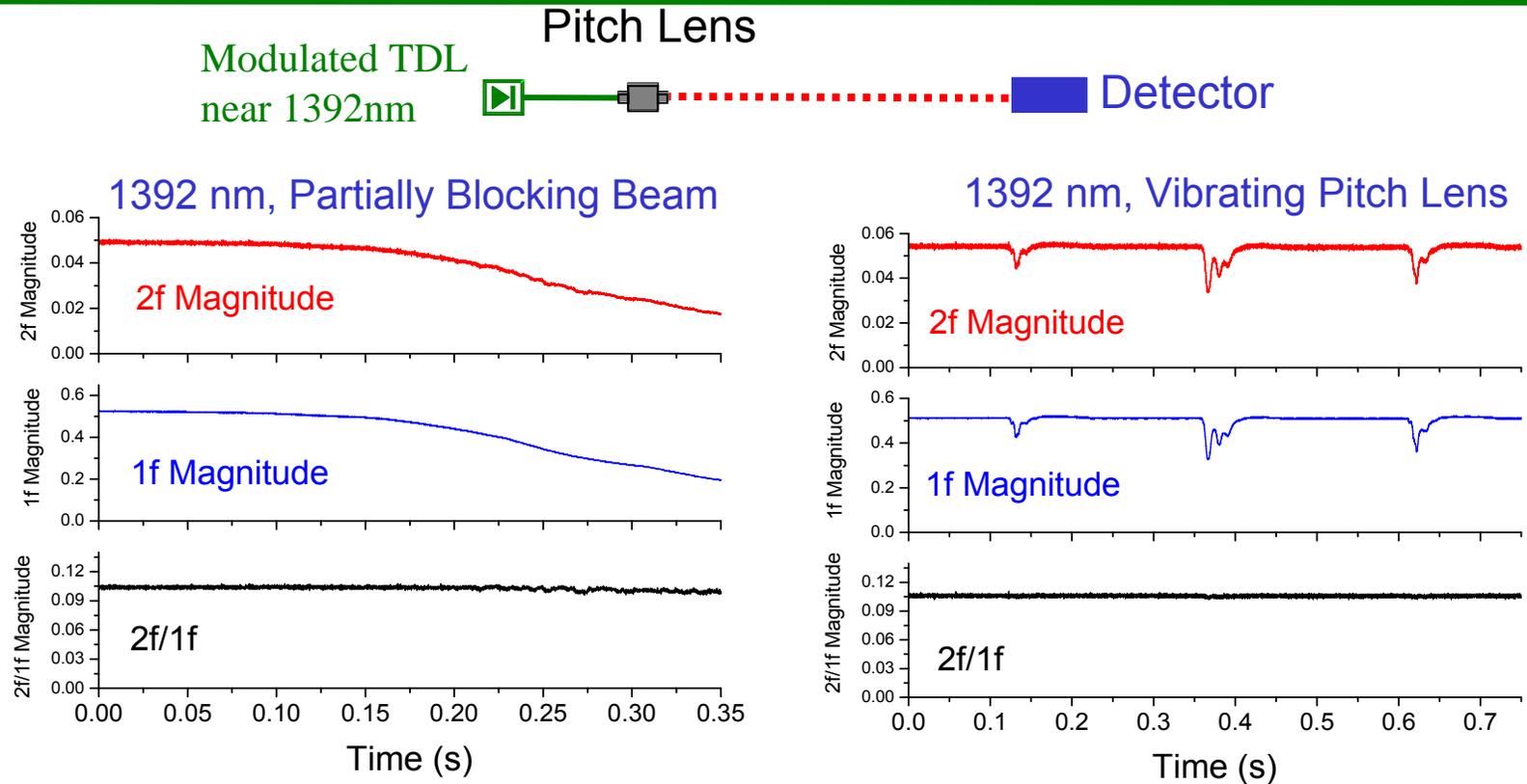
- Approaches: fixed λ and scanned λ

- Direct absorption

- WMS with harmonic detection



- Direct absorption: Simpler, if absorption is strong enough
- WMS: More sensitive (x10 or more); better noise rejection
 - WMS- $2f$ signal approximates 2nd derivative of line shape at small modulation amplitude
 - Ratio of two WMS- $2f$ signals provides T
 - Injection current FM produces intensity modulation @ $1f \rightarrow$ enables normalization

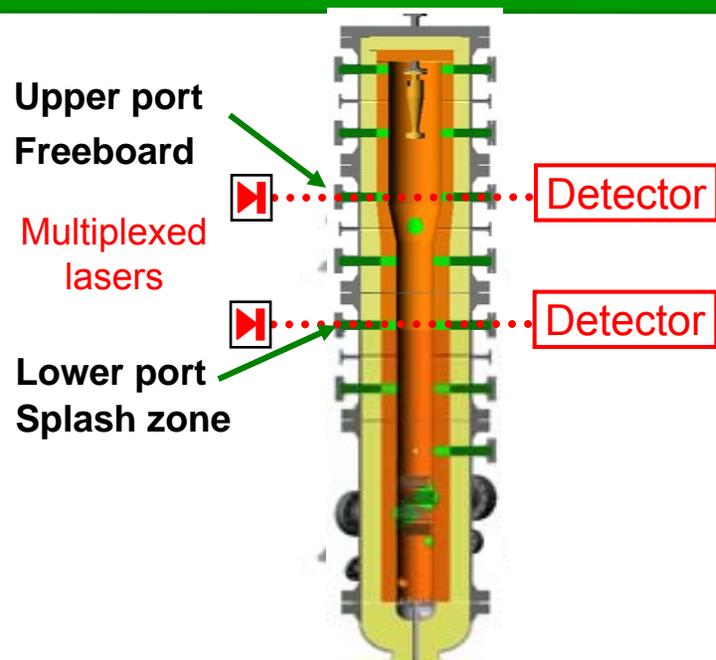


- Measure ambient H₂O (T=296 K, 60% RH, L=29.5 cm, ~6% absorbance)
- Attenuate the beam by partial blocking: Normalized $2f/1f$ signal constant
- Attenuate the beam by mechanical vibration: Normalized signal constant
- Expect strategy to provide immunity from window fouling and particulate loading

Examples of Stanford TDL Sensing in Harsh, High-P, High-T Environments

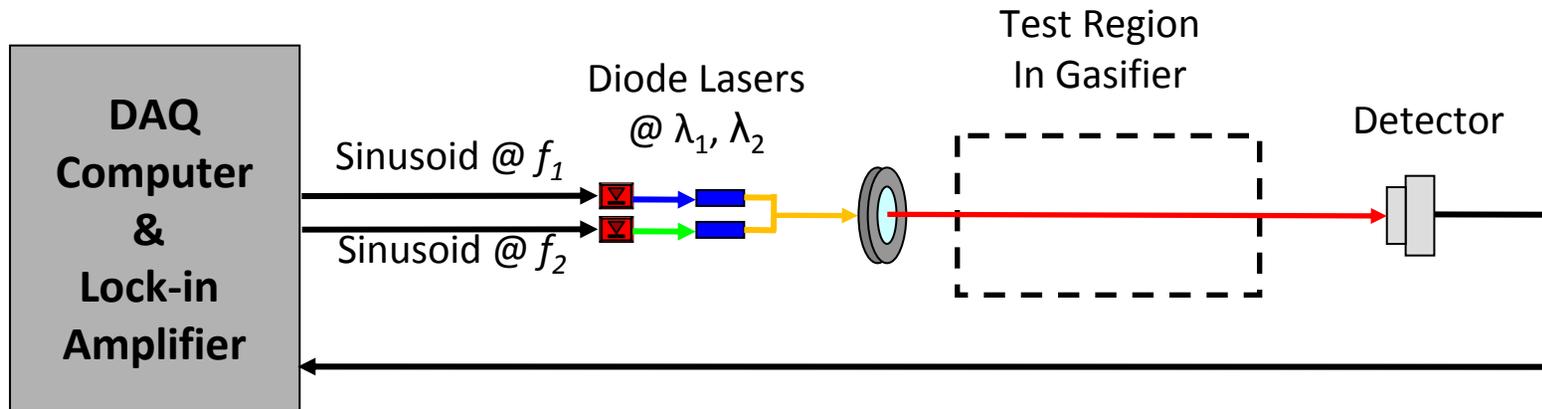
- IC-Engines
 - Crank-angle-resolved measurements of temperature and EGR
 - T-sensing for HCCI research with Sandia National Labs
 - Development of WMS-based T-sensor for production engines
 - Crank-angle-resolved measurements of gasoline

- Fluidized-bed gasification of black liquor (funded by EPRI)
 - TDL absorption measurements in the presence of particulate
 - Successful measurements with 92% beam attenuation
 - Provides proof-of-concept for gasification application
 - TDL in the Utah fluidized-bed rig discussed below



- Measurements in two ports investigated different types of particulate interference for the laser-absorption measurements
 - Lower port views the “splash zone” where optical transmission experiences time-varying interference as bed particulate ($\sim 200\mu\text{m}$) splashes up and down in the beam
 - Upper port views the gasifier products where transmission is obscured by char particulate ($\sim 10\mu\text{m}$)

Two-color TDL sensor for T and X_{H_2O}



- Two lasers (λ_1 & λ_2) wavelength-modulated at 40 and 60 kHz respectively
- Signals detected @ 2f and 1f for each laser scanned at 2 kHz across H_2O absorption line
- Normalization of 2f by the 1f signal corrects each laser for scattering losses
- Temperature from the ratio of 2f/1f signals @ λ_1 & λ_2
- Concept tested with EPRI support in U Utah fluidized-bed gasifier

Lasers and electronics

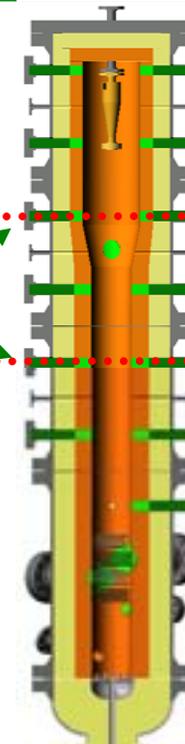


*Stanford student Andrew Fahrland
in gasifier control room*

Fiber launch of laser beam



*Optical fiber
30m long*



Fiber collection transmitted light



Remote detector

- Fiber-coupled lasers and electronics located in the control room
 - Transmitted light collected onto a fiber to allow remote location of detector
- Two different diode laser detection strategies tested
 - Wavelength-scanned direct absorption
 - Normalized (1f) wavelength-modulation spectroscopy with 2f detection (WMS-2f/1f)

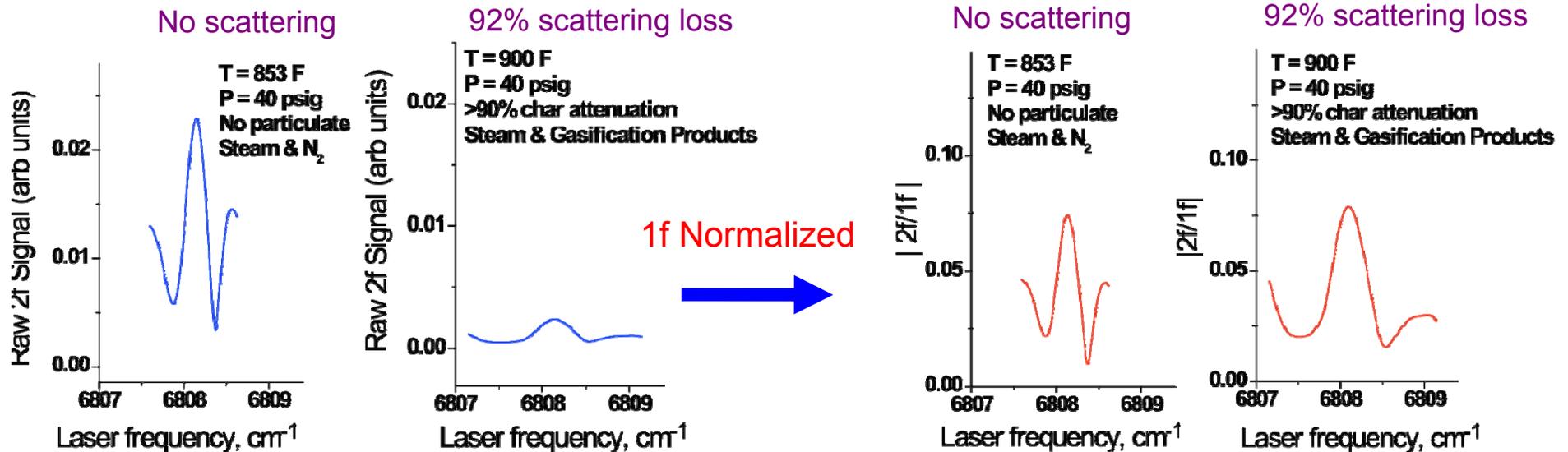
Just looking at the raw signals shows potential of TDL sensing

Measurements in reactor core to test influence of char particle scattering on WMS

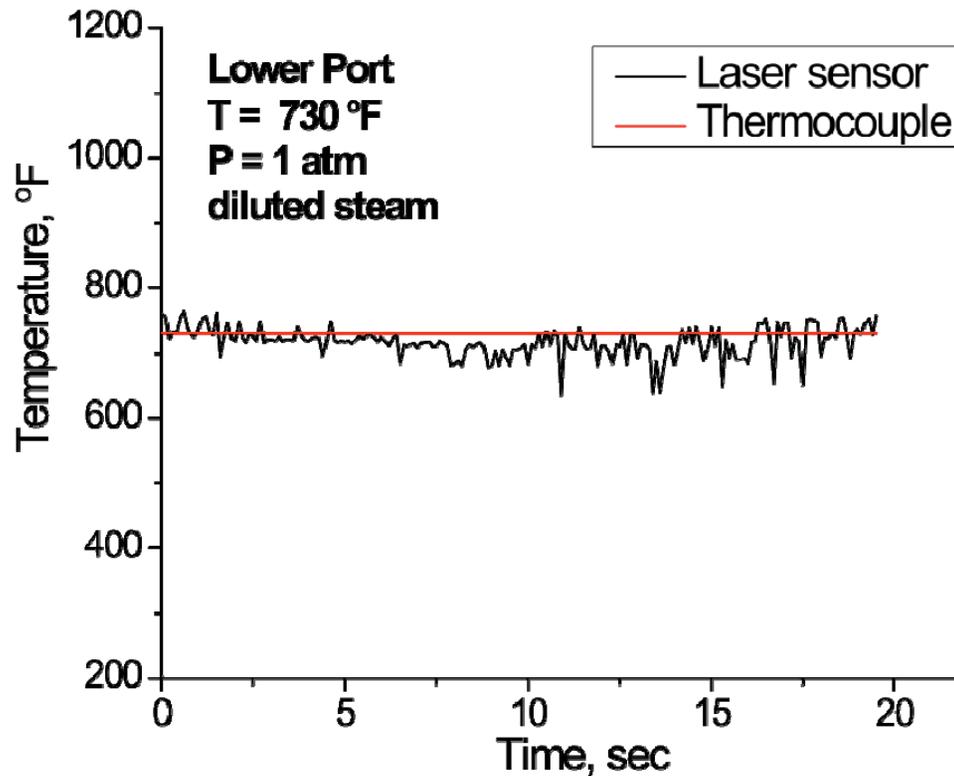
Single-scan data at 2kHz (measurement time = 0.5ms)

Raw 2f signals

1f Normalized 2f signals



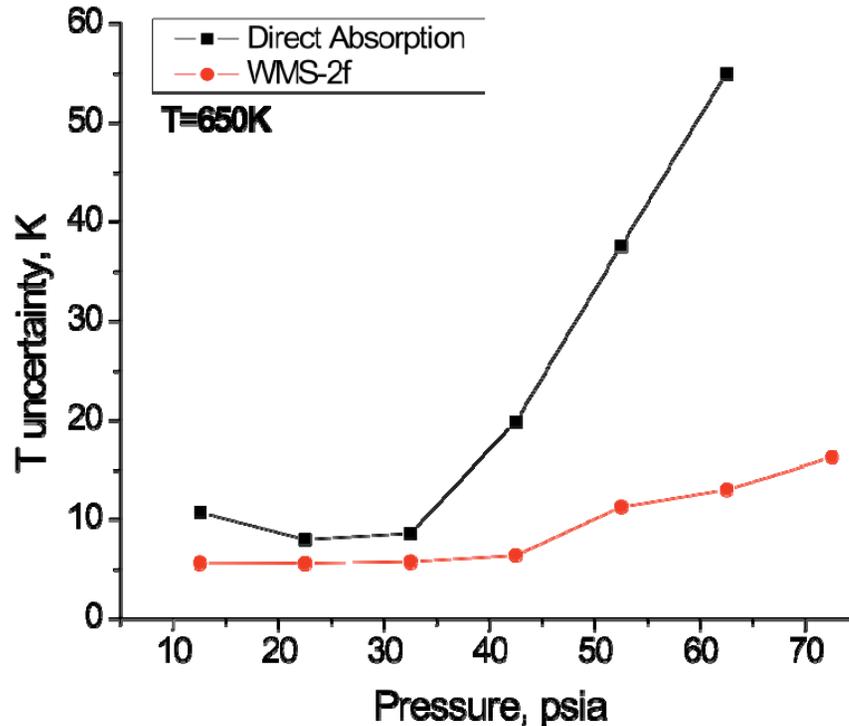
- Char particles made during gasification attenuate the transmitted signals by 92%
- Normalization of 2f by 1f signals recovers a quantitative WMS-2f signal
- Excellent SNR provides proof-of-concept for TDL sensing in highly scattering reactor environments



TDL measurements on lower port without bed in nitrogen-diluted steam

Single-scan data at 2kHz (measurement time = 0.5ms)

- Time record of temperature agrees well with facility thermocouple
- Statistical temperature uncertainty used to characterize precision of sensor



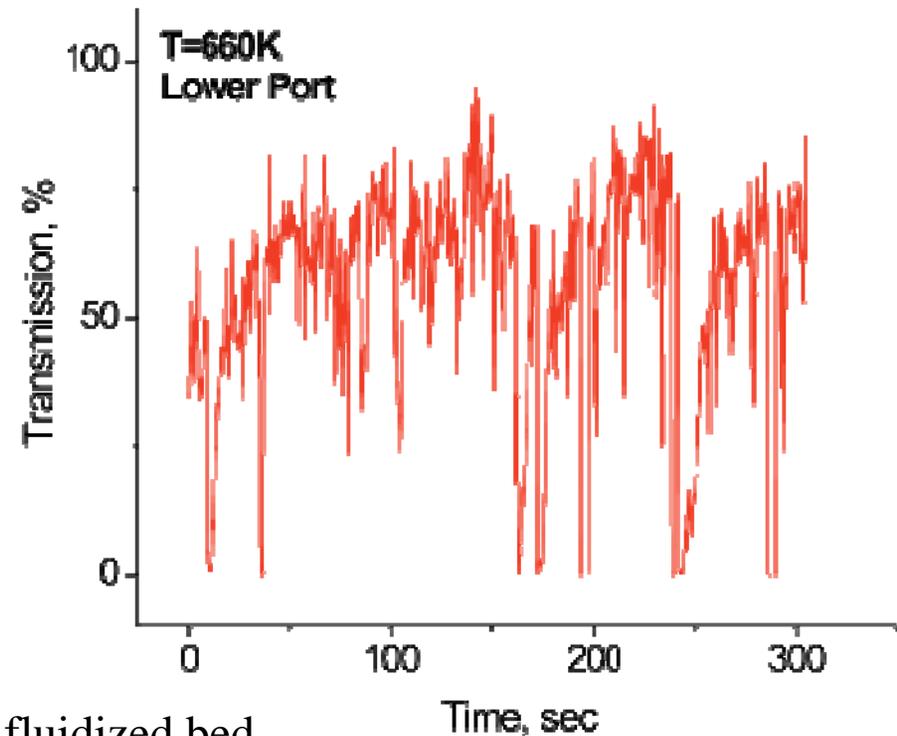
TDL measurements on lower port without bed in nitrogen-diluted steam

Single-scan data at 2kHz (measurement time = 0.5ms)

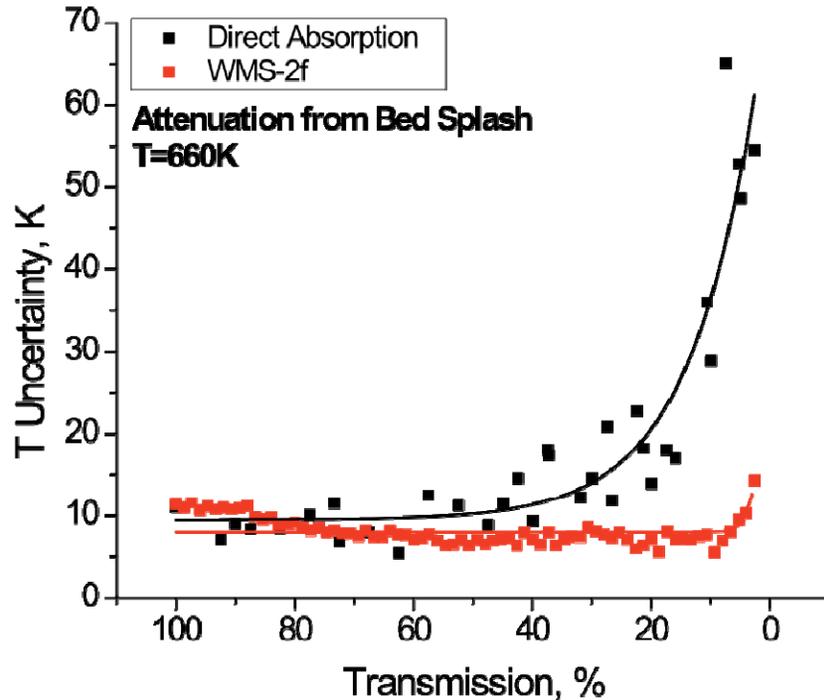
- Temperature uncertainty increases with pressure for direct absorption
 - Less than 15K uncertainty at 2kHz for all pressures available with WMS-2f/1f
 - Wavelength modulation signal significantly less sensitive to pressure increase
- Potential to further increase signal-to-noise ratio by averaging (reducing bandwidth)



Laser Transmission vs Time in Splash Zone



- Picture/movie shows cold flow model of fluidized bed
 - Large bed particles ($200\ \mu\text{m}$) are splashing in the bed of the reactor
- This particulate bounces up and down through the beam, sometimes completely blocking the beam
- TDL data taken in actual fluidized bed reactor and 300 seconds of data is binned by transmission for analysis of T vs transmission



Splash Zone

TDL measurements on lower port with bed fluidized by steam flow

Beam attenuated by scattering from bed particle splash

Single-scan data at 2kHz
(measurement time = 0.5ms)

- Bed particle splash produces time-varying transmission (2kHz data rate)
- **Wavelength modulation less sensitive to signal attenuation**
- Signal binned by transmission, analyzed for temperature uncertainty
- **Less than 15K uncertainty at 2kHz for >5% transmission with WMS-2f/1f**
- Illustrates potential for WMS-2f/1f strategy for DoE gasifier measurements

- 2010
 - Design TDL sensors for H₂O and CO (SU)
 - Design and fabricate optical access for pre-quench, post-quench, clean output (Utah)
 - Validate H₂O and CO spectroscopic database (SU)
 - Controlled environment sensor tests (SU)
 - Field measurements at Utah with SU sensor for H₂O and CO (SU & Utah)
 - Designs to extend the TDL sensor for methane and carbon dioxide begin (SU)
- 2011
 - Validate CO₂ and CH₄ spectroscopic database (SU)
 - Laboratory tests of gas composition (H₂O, CO, CO₂, and CH₄) (SU)
 - Optical access for the reactor core will be designed and tested (Utah)
 - The water and temperature sensor design will be finalized (SU)
 - Initial field measurements for gas composition (H₂O, CO, CH₄, CO₂) (SU & Utah)
- 2012
 - Optical access to the reactor core will be completed (Utah)
 - Sensor design will be finalized (SU)
 - Final field measurements of gas composition (heating value) & T (SU & Utah)

location	1. Reactor	2. Pre-quench	3. Post-quench	4. Output
T	1500K	1200K	500K	500K
P	7-18 atm	7-18 atm	7-18 atm	6-17 atm
Path Length	20 cm	34 cm	5 cm	5 cm
CO	34%	34%	44%	44%
CH ₄	1.6%	1.6%	2%	2%
H ₂	20%	20%	26%	26%
H ₂ S	1.3%	1.3%	1.6%	1.6%
CO ₂	17%	17%	21%	21%
H ₂ O	26%	26%	6%	6%

Estimate gas composition, temperature, pressure and pathlength @ Utah

- Use this data to estimate relative contributions to lower heating value
- Use this data to simulate absorption spectra for sensor design

Progress & Current Status: Contributions to Lower Heating Value

Test locations 1 & 2

Species	LHV (MJ/kg _{mixture})	Percent
CH ₄	0.556	7.7%
H ₂ O	0	0%
CO ₂	0	0%
CO	4.247	58.6%
H ₂	2.162	29.8%
H ₂ S	0.288	3.9%

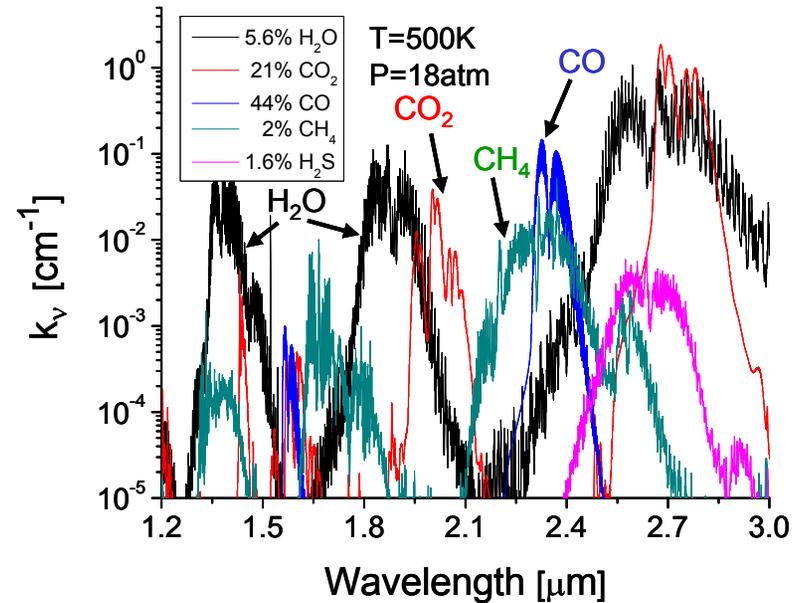
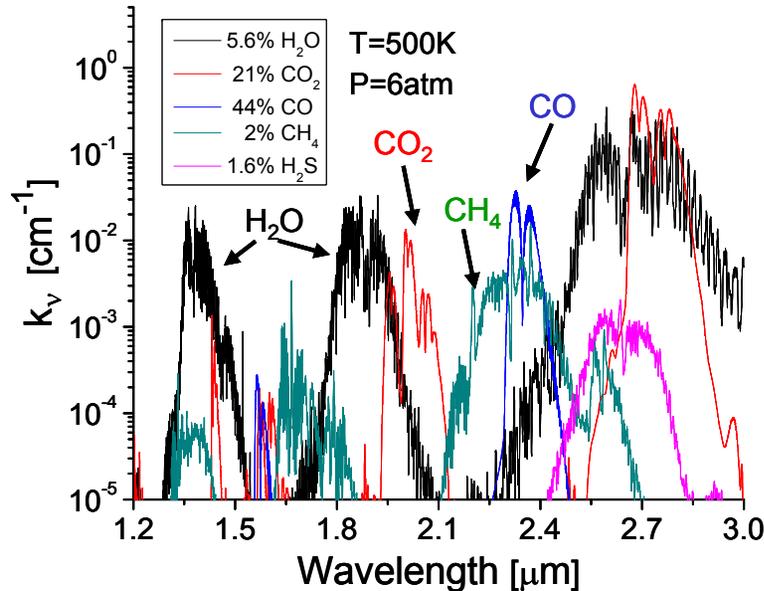
Test locations 3 & 4

Species	LHV (MJ/kg _{mixture})	Percent
CH ₄	0.673	7.7%
H ₂ O	0	0%
CO ₂	0	0%
CO	5.140	58.6%
H ₂	2.616	29.8%
H ₂ S	0.350	3.9%

Mixture LHV(MJ/kg): 7.253MJ/kg

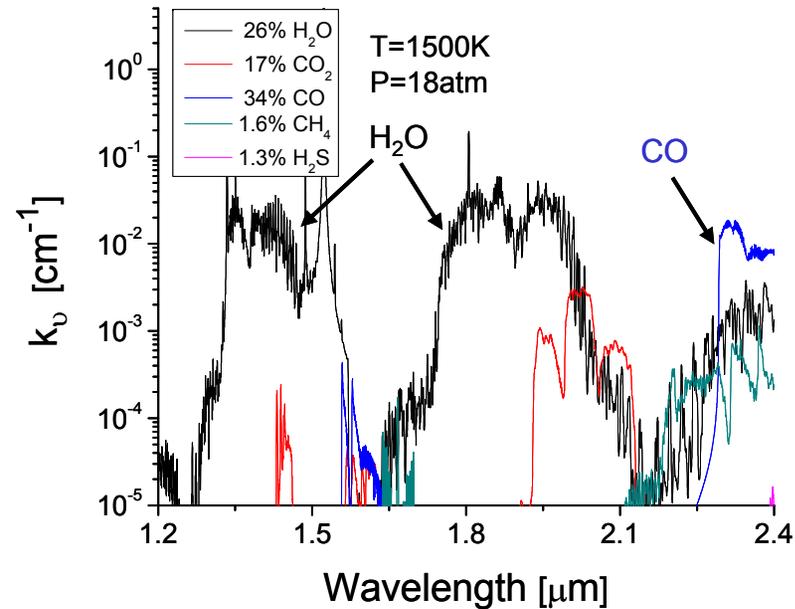
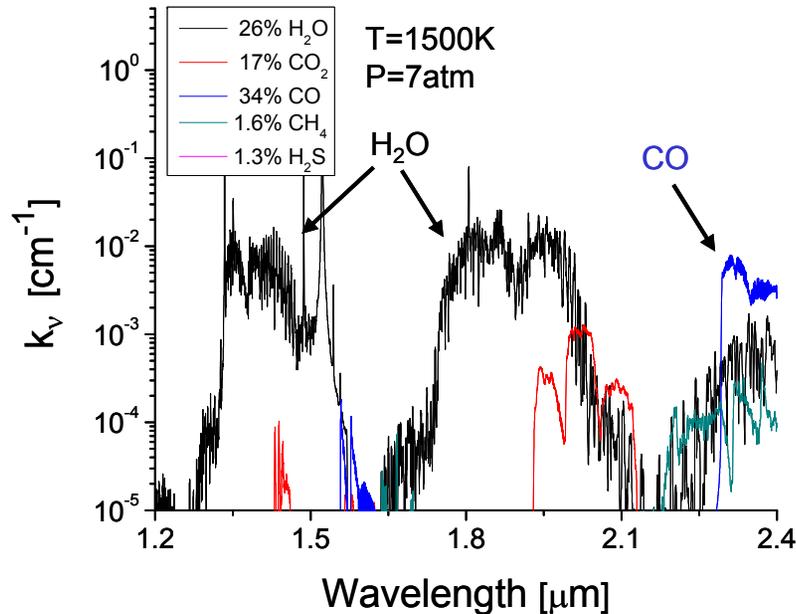
- TDL sensor measures CH₄, H₂O, CO₂, and CO and assumes that H₂ is the balance of the gas (ignoring H₂S and N₂)
 - Although H₂S has 4% of the LHV assuming “balance” as H₂ results in an error for the gas mixture of only 0.3%
 - If N₂ is approximately known, similar errors in the LHV result
- Model calculations show that heating value can be monitored with TDL measurements of CH₄, H₂O, CO₂, and CO

- Use HITRAN database to simulate the expected absorption signals



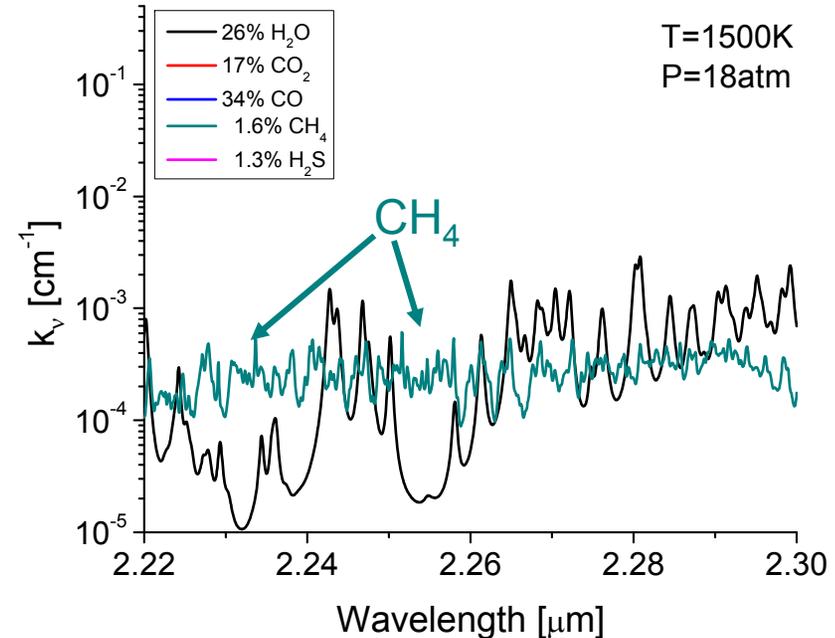
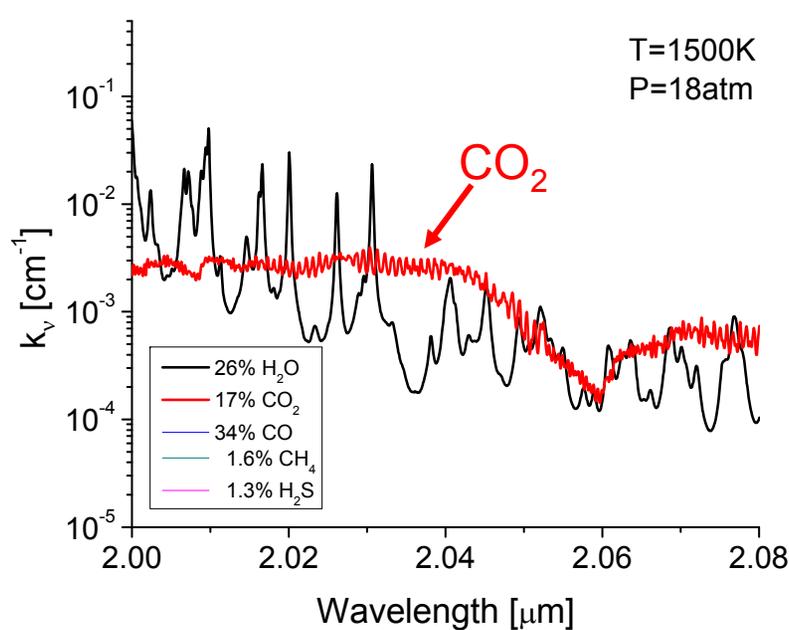
- At 500K there are many laser wavelengths where H₂O, CO, CO₂, and CH₄ can be detected with minimal interference
- Increase in pressure broadens the transitions, but still good separation between the different species

- Use HITRAN database to simulate the expected absorption signals

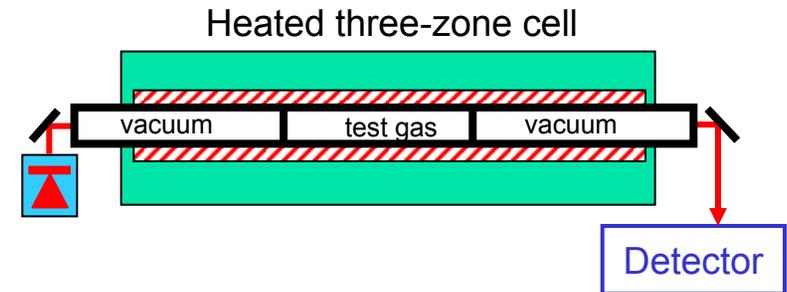
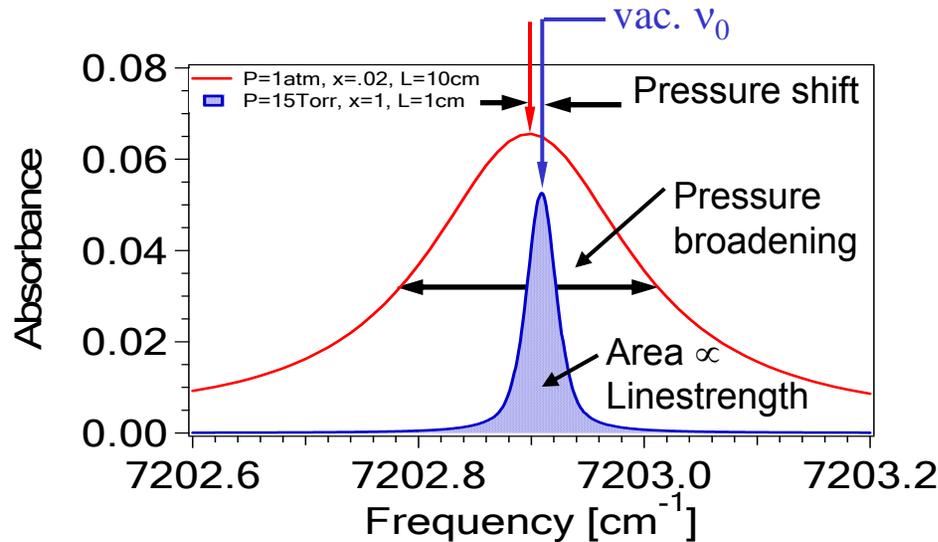


- At 1500K, H_2O and CO can be detected with minimal interference
 - H_2O in the bands near $1.4 \mu\text{m}$ and the bands near $1.8 \mu\text{m}$
 - CO in the first overtone band near $2.3 \mu\text{m}$
- Selection of laser wavelength for CO_2 and CH_4 must carefully avoid interferences

- Use HITRAN database to simulate the expected absorption signals

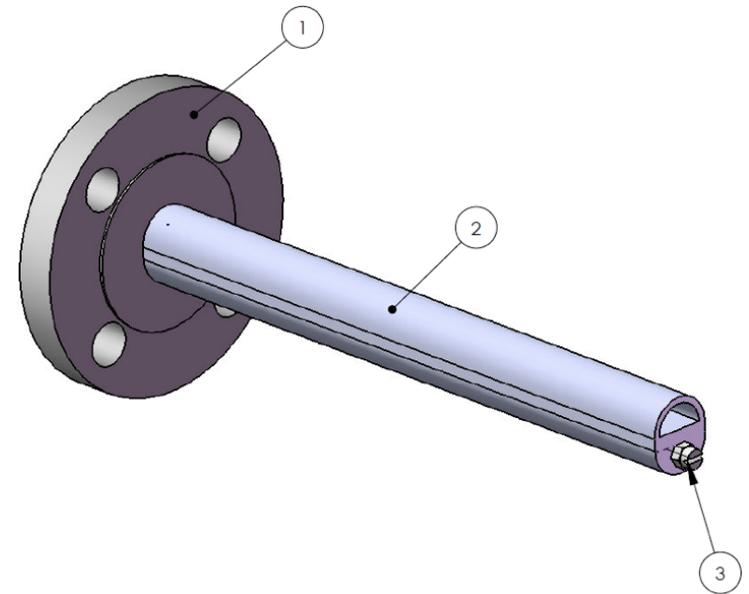


- Simulations show, H₂O is the major interference species
- There are gaps or “windows” in the H₂O where CO₂ and CH₄ detection should be possible
- Careful validation of the spectroscopic database is required (especially for H₂O in the region for CO₂ and CH₄ detection)



- Laboratory measurements to validate spectral database
 - Three-zone furnace with quartz cell for measurements to 1500K
 - Measurements versus pressure (at low values) to determine spectral data
- Current status:
 - Lasers for H₂O and CO purchased and on-hand
 - Initial line selection for CH₄ and CO₂ complete

- Sensor locations 3 and 4 (post-quench in piping)
 - Assessing optimum optical pathlength
 - Either “tee” (across pipe) or along length of pipe
 - Nitrogen purged sapphire window
 - Purge provides air curtain to avoid fouling
 - Developed technology – minimum fabrication time
- Sensor location 2 (pre-quench below reactor)
 - Use existing quench spray ports (two opposing)
 - Axially split spray lance to allow optical access in upper half and quench spray in bottom half
 - Optical pathlength (14” or 35.5cm)
 - Requires fabrication and testing
- Sensor location 1 (gasification reactor)
 - Modeling work planned to assess options to keep slag layer from blocking windows (fiber technology can minimize needed aperture)
 - Plan reactor modifications for opposing ports on the completion of the window design
 - Required for Year 3 experiments



Field measurements using Stanford sensor technology in Utah gasifier facilities

- 2010: Field measurements for H₂O and CO concentrations
- 2011: Initial field measurements for gas composition (H₂O, CO, CH₄, CO₂)
- 2012: Final field measurements of gas composition (heating value) & T