

Turbulent Flame Propagation Modeling in Premixed/Stratified Combustors

Application to Flame Flashback

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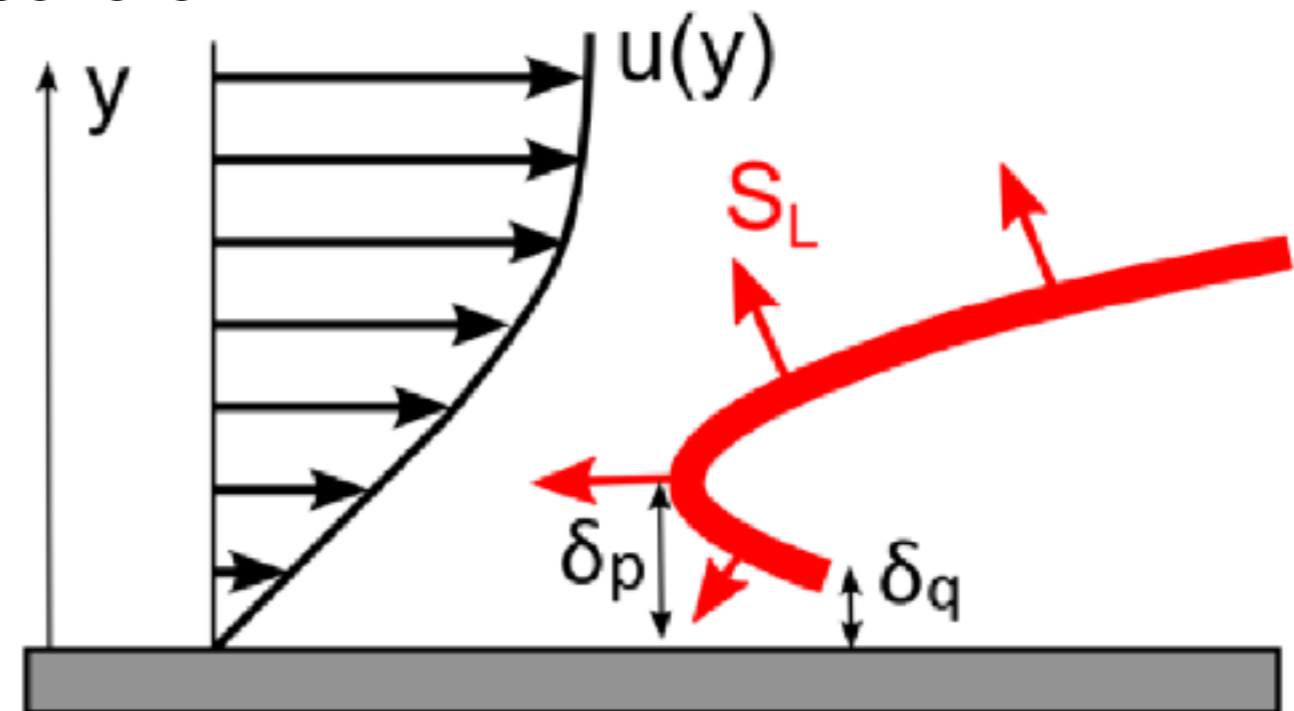
Noel Clemens

The University of Texas at Austin

Background

- **Flashback in lean premixed combustor**

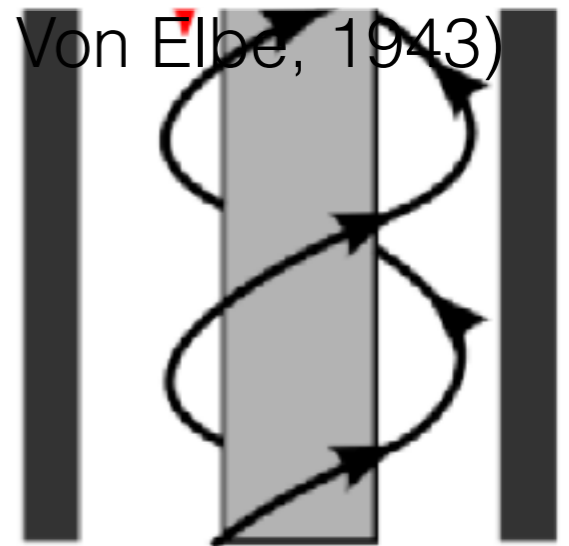
- ➔ Nature of premixed flame, lead to severe damage
- ➔ Transient and difficult to predict
 - Time scales of millisecond
- ➔ Boundary layer flashback
 - Low momentum streaks
 - Reaction vs. near-wall quenching



(Lewis and Von Elbe, 1943)

- **Challenges in practical combustion device**

- ➔ Complex geometry
- ➔ Extension to stratified flame and even partially premixed



Project Objectives

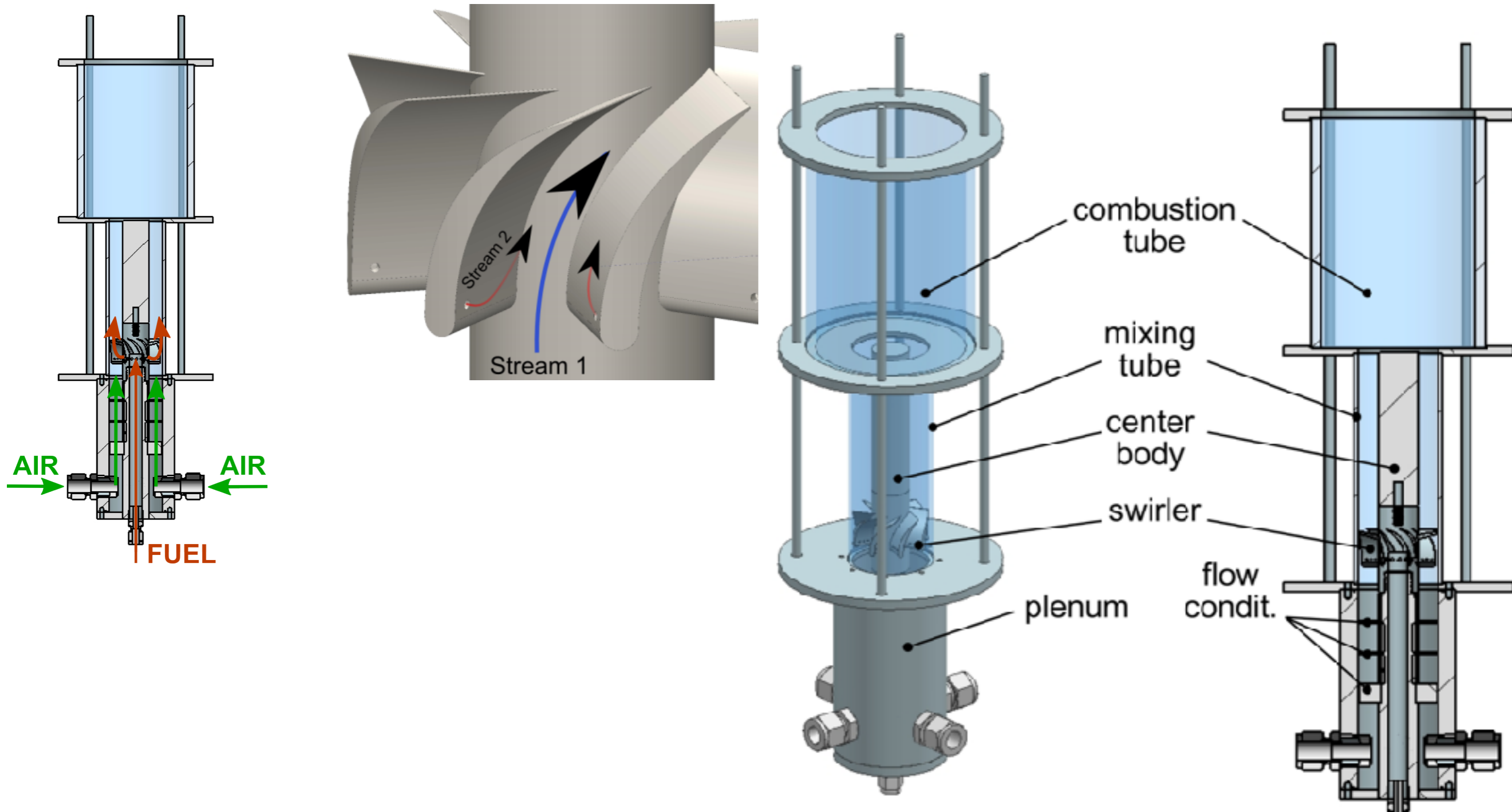
- **Goal: Understand flame structure and propagation in high pressure premixed/stratified mixtures**
 - ➔ Lean combustion in high strain conditions
 - ➔ Stratified combustion
 - ➔ Flame flashback in high hydrogen-content combustion
 - ➔ Staged combustion with hydrogen as fuel
- **Approach**
 - ➔ DNS/LES based modeling flames
 - ➔ Experiments of low and high pressure flames in stratified environments
 - Including flashback

Outline

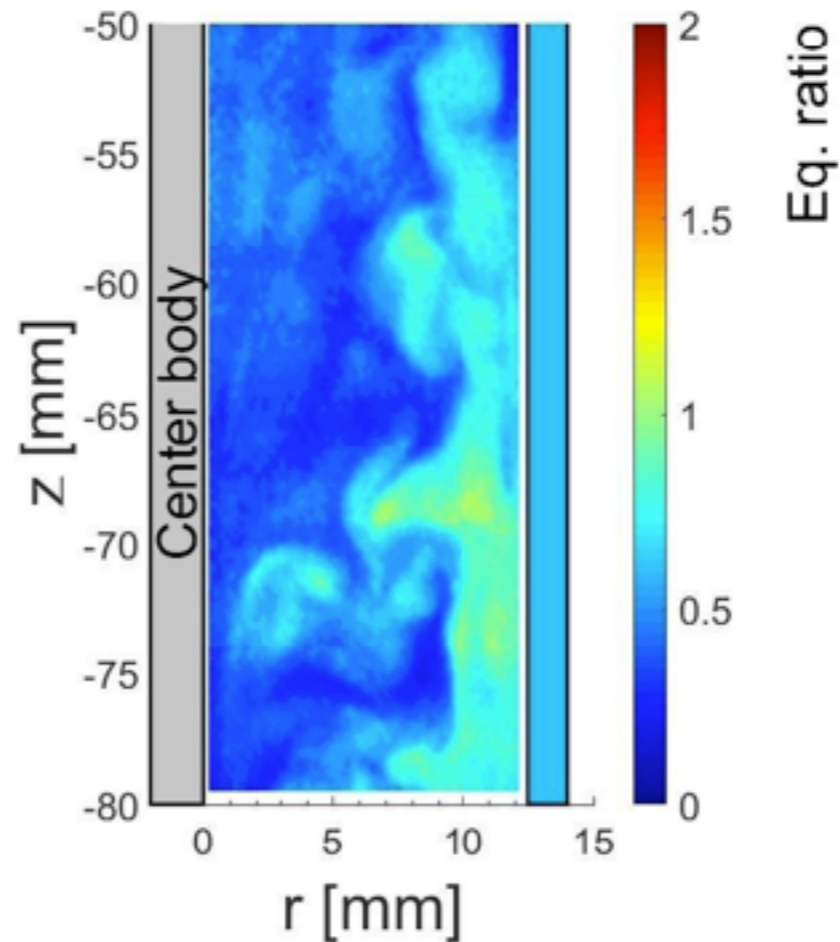
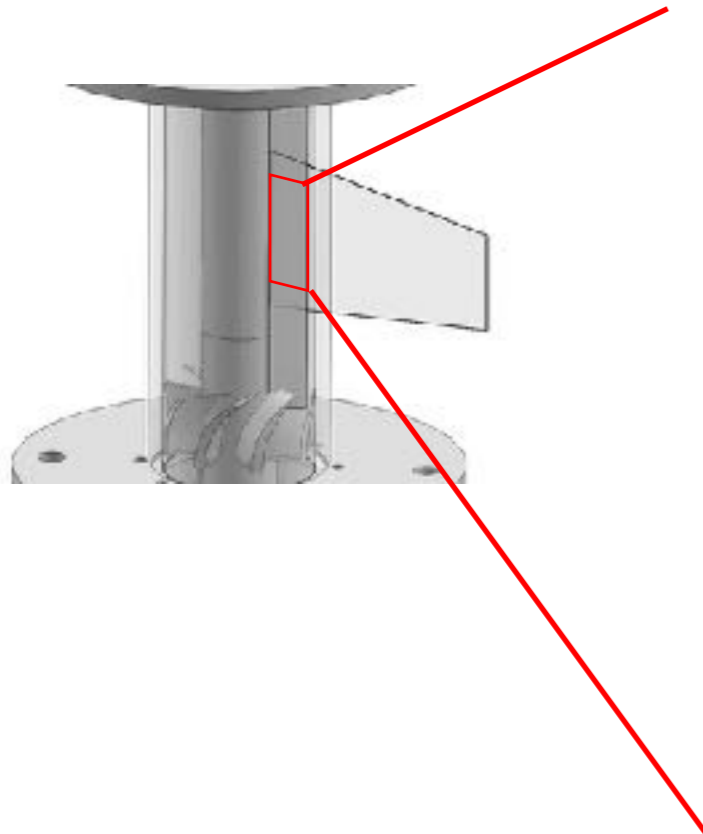
- **Experimental studies of flashback**
 - ➔ UT swirl burner
 - ➔ Low and high pressure test cases
 - ➔ Summary of findings
- **Computational modeling of premixed and stratified flames**
 - ➔ Solver development
 - ➔ Flamelet-based models
 - ➔ Validation test cases
 - ➔ Summary of findings

Stratified Flames and Flashback

- Goal is to identify physical structure of flashback
- UT Swirl Burner with Nozzle-based Injection

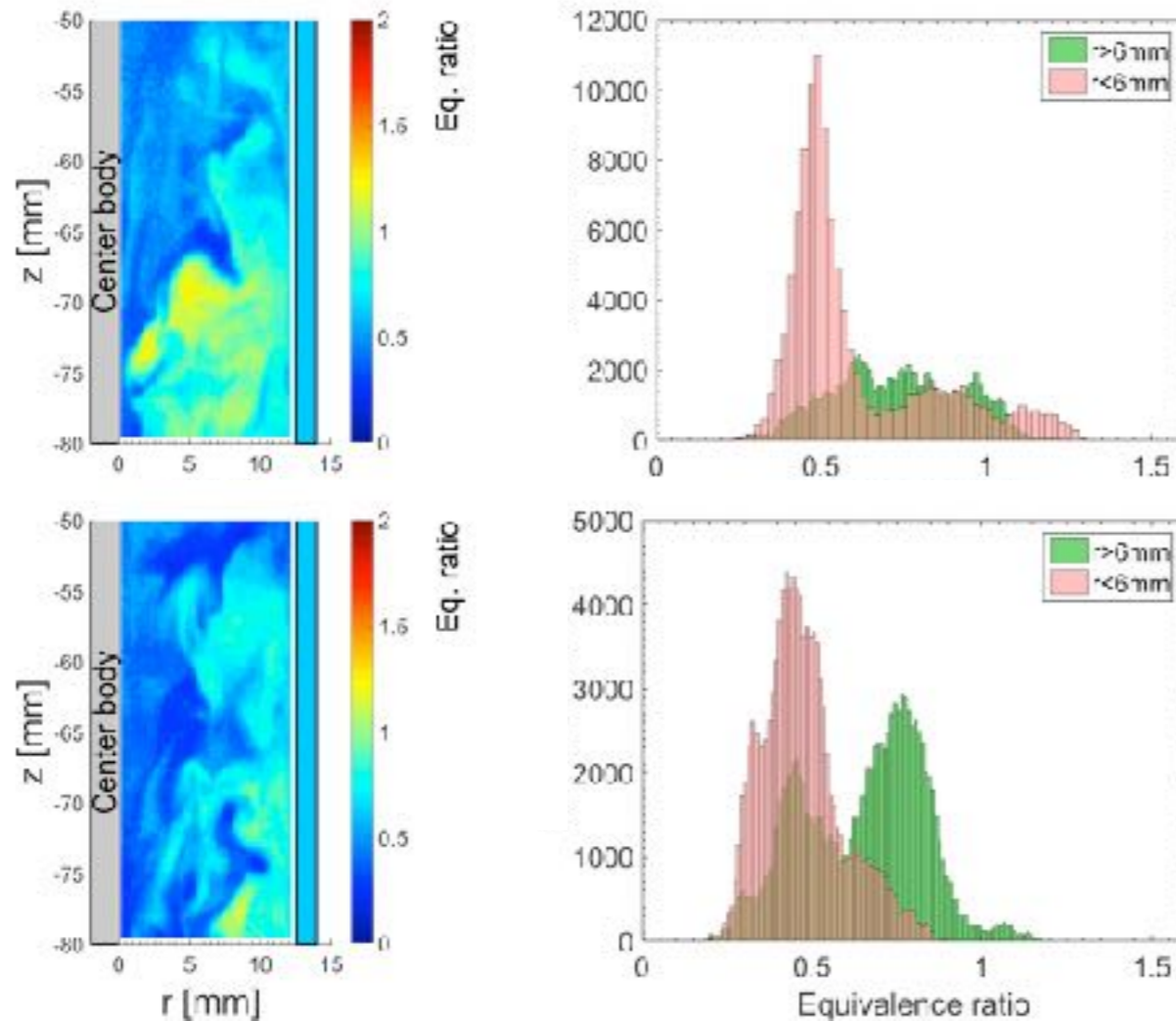


Demonstration of Stratification: Nonreacting Methane-air



- **Global equivalence ratio: 0.63**
- **$Re_h = 6100$**
- **Average axial velocity: 2.5 m/s**
- **Non-reacting flow with acetone-seeded air through the fuel-nozzles**

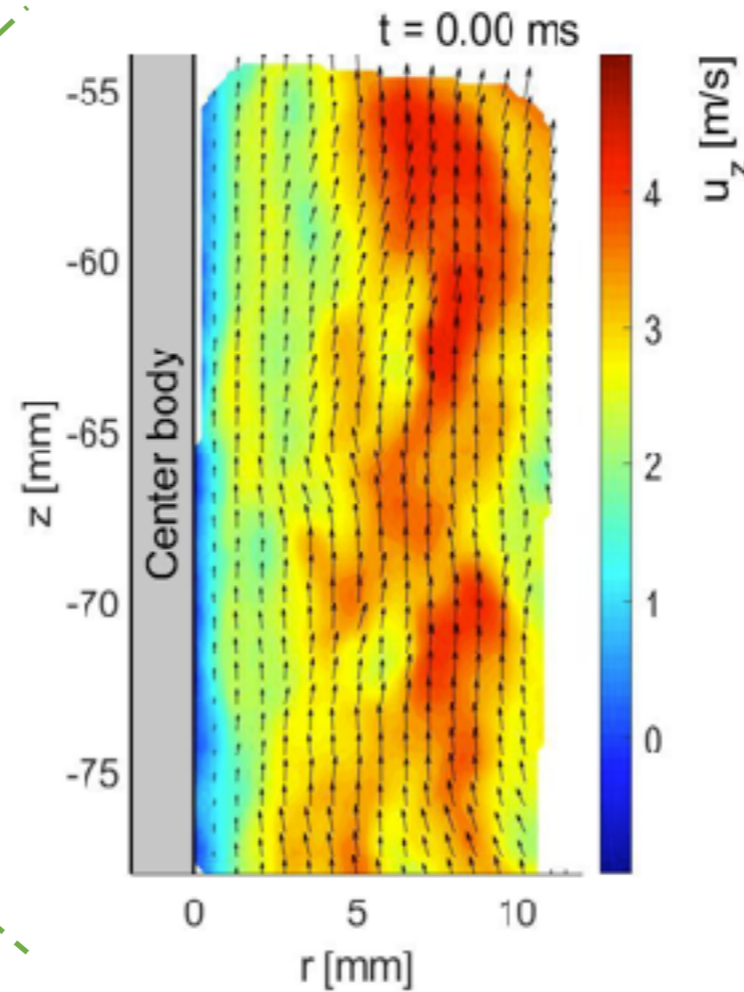
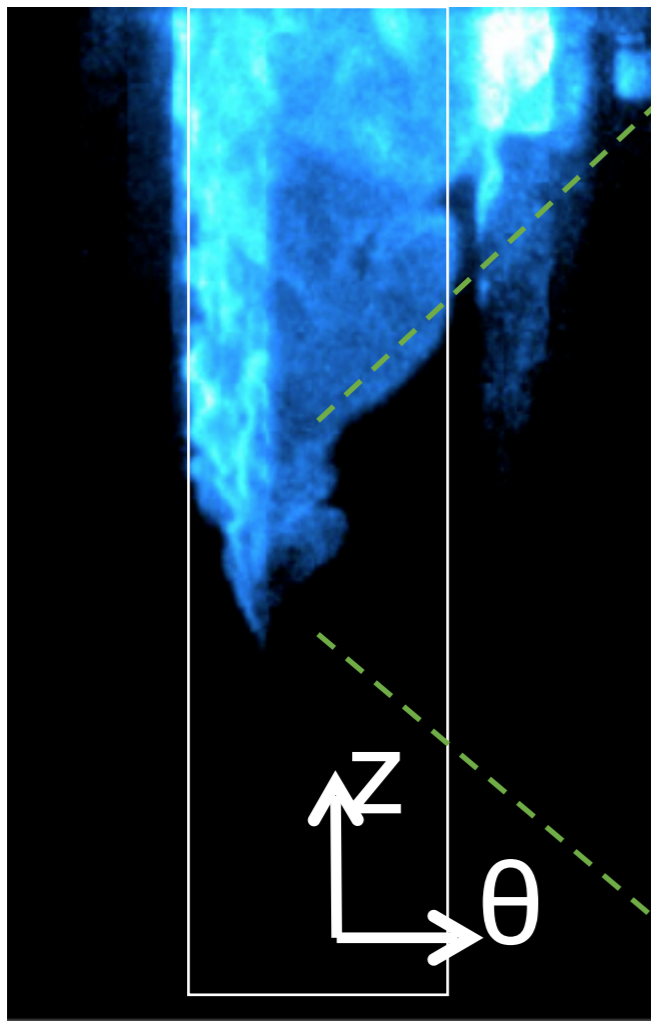
Equivalence ratio distribution snapshots



Histograms compare instantaneous equiv. ratio distribution in the inner half ($r < 6$ mm) to the outer half ($r > 6$ mm)

- Flow was found to be stratified in an average sense
- Occasional presence of fuel-rich mixtures found close to the center-body
- Swirl and turbulence in the mixing tube may bring reactive pre-mixture close to the center-body boundary layer

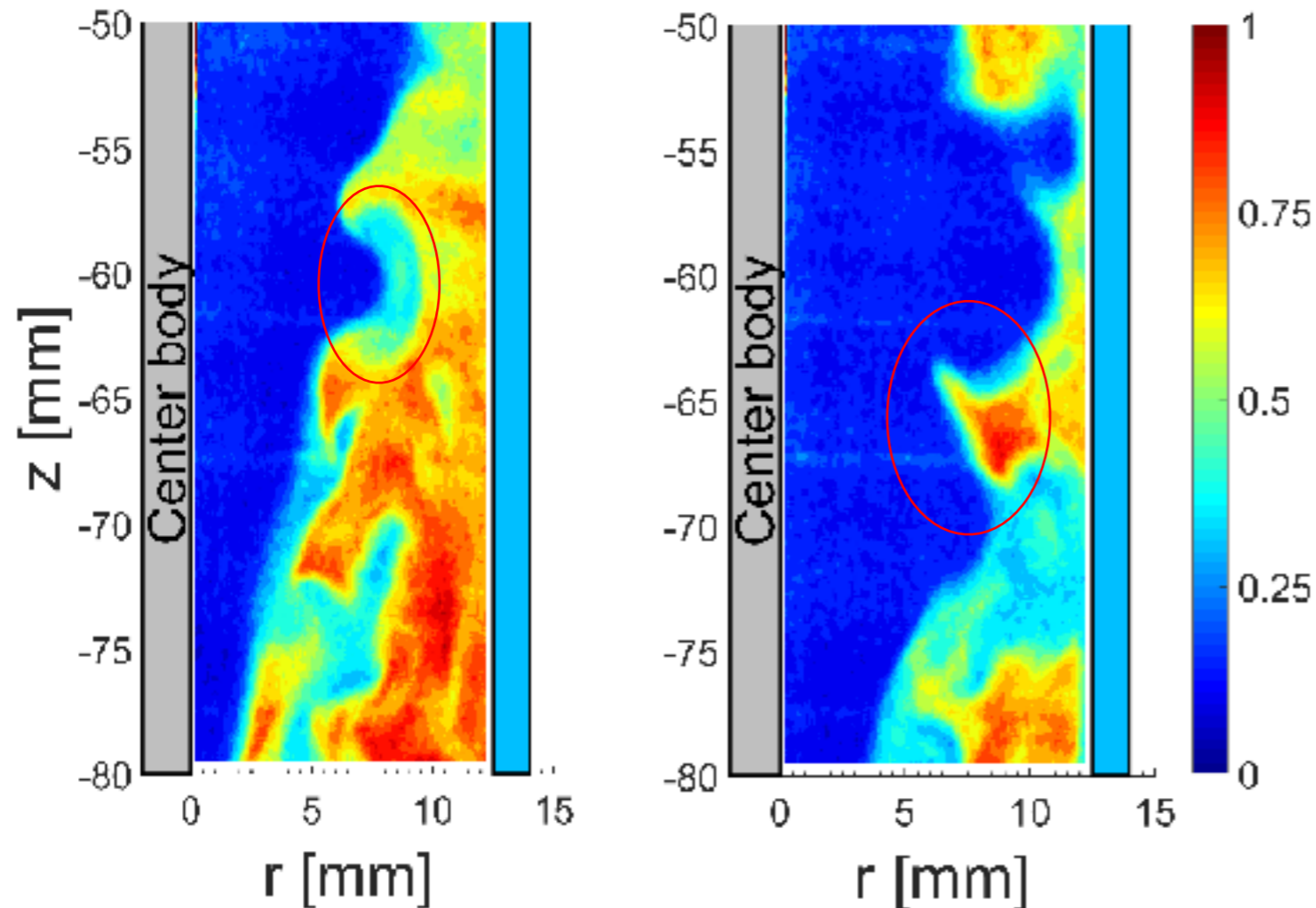
Propagation along the inner boundary layer



Luminosity image Axial velocity map

- Flame surface identified by evaporation of PIV seed particles (white region in the axial velocity map)
- Bright structures in the luminosity impose strong deflection of the approach flow
- Flame surface curvature is higher than the fully premixed flashback at same Re

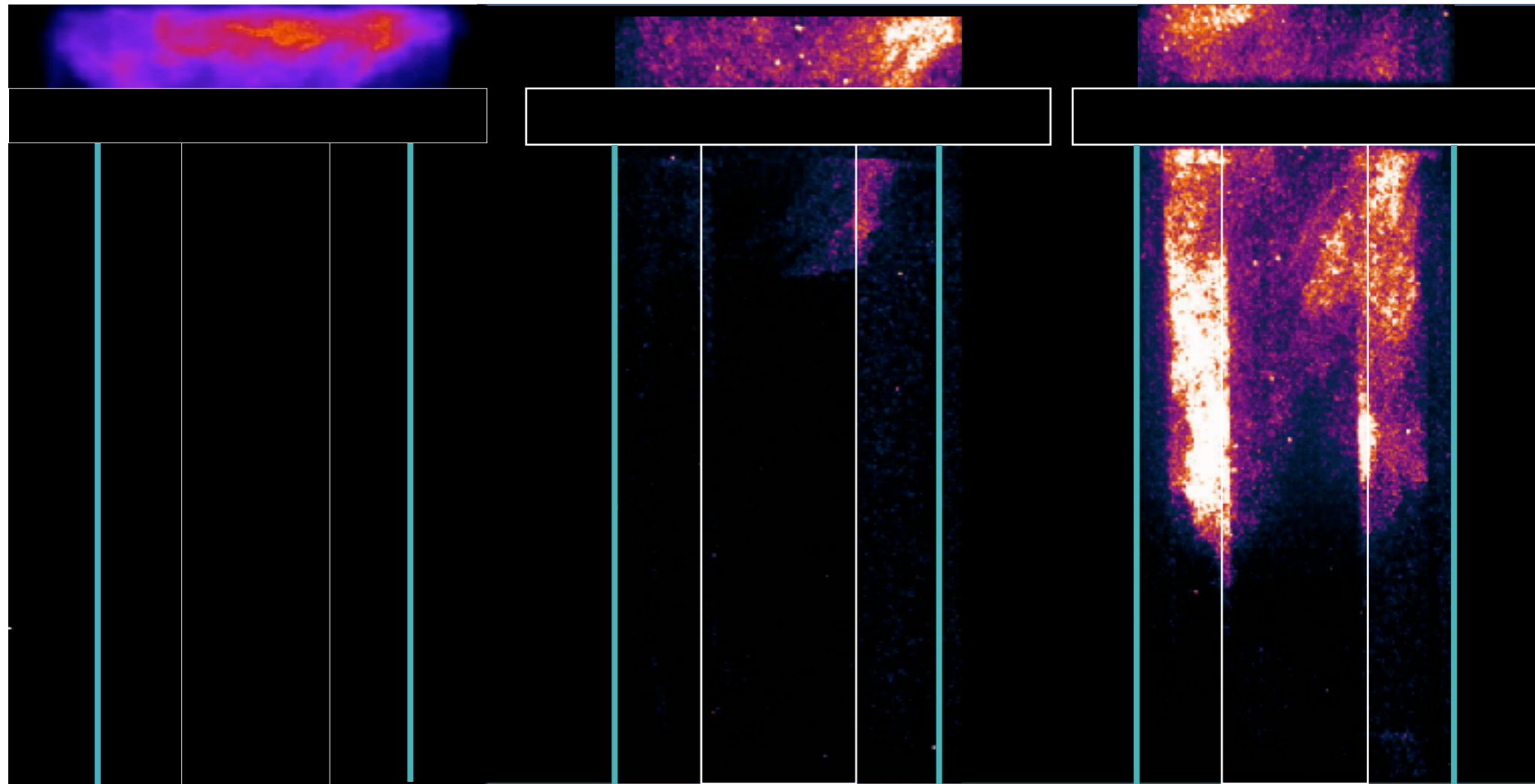
Acetone PLIF snapshots during Flashback



Normalized PLIF signal map during flashback

- **Instantaneous acetone PLIF signal maps were obtained for the reacting cases**
- **Flame curvature was found to be enhanced by the local distribution of the equivalence ratio**
- **Regions of positive and negative flame surface curvature are shown (in red circles)**

Effect of hydrogen-enrichment: Luminosity images



Methane-air

Early stage

Final stage

Hydrogen

Flame propagates along inner wall for CH₄ and H₂ early stage

At later time H₂ flame propagates on outer wall

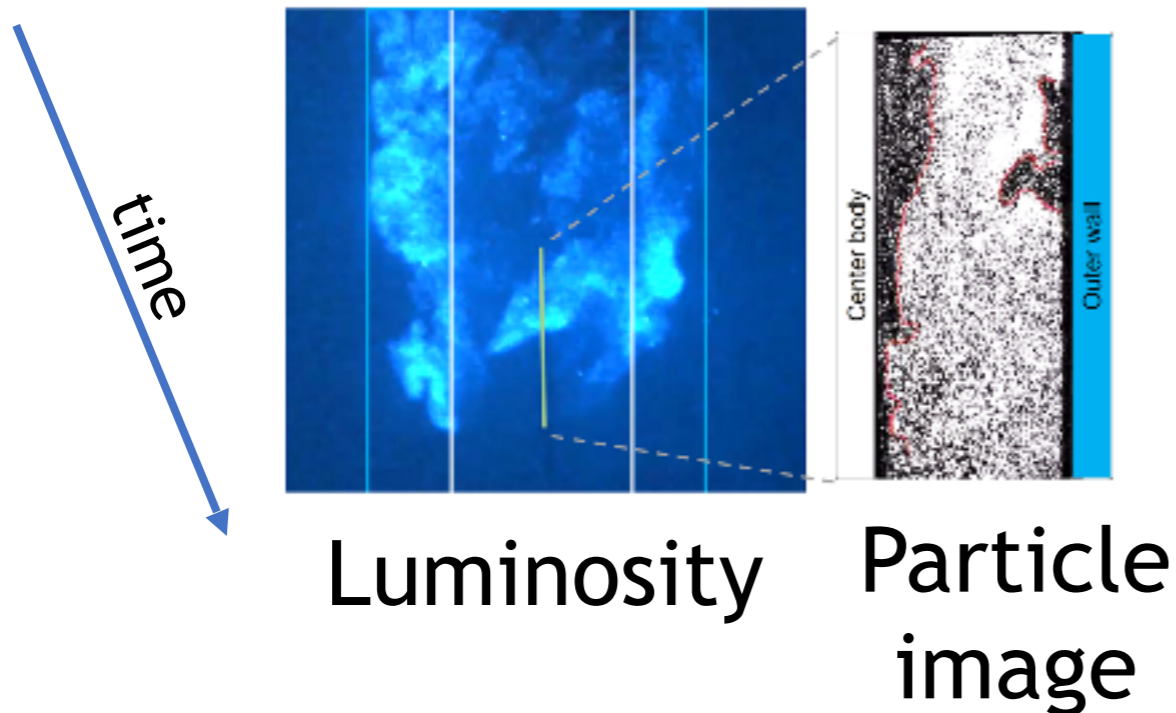
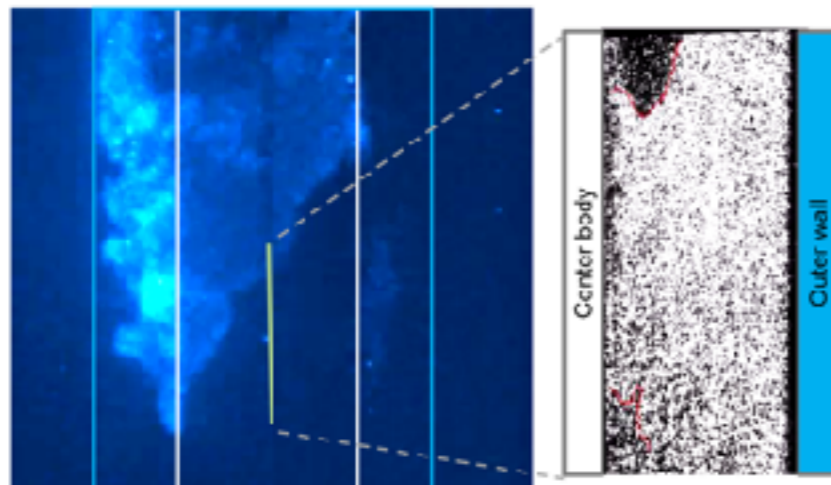
Propagation along the outer wall

- Flame starts propagating along the center-body boundary layer,

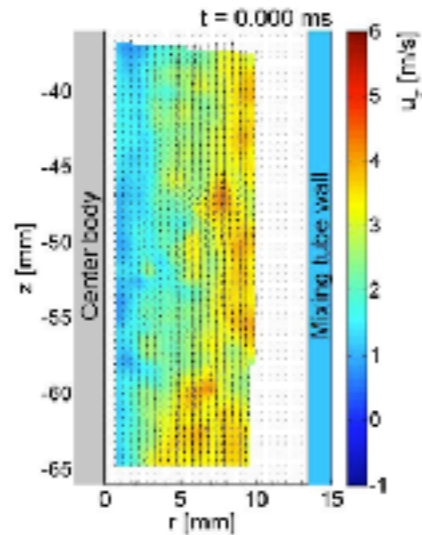
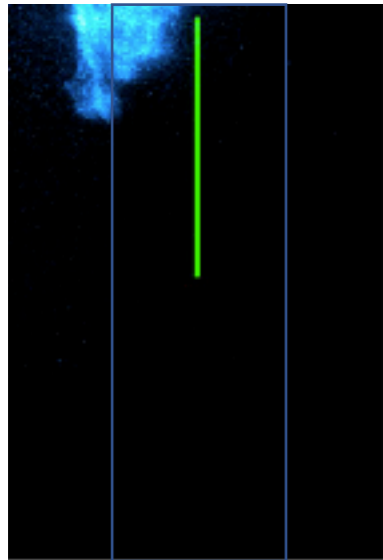
→ Switches to the outer wall after a few milliseconds

- Simultaneous Mie scattering images show the thin acute-tipped flame-strand propagating along the outer wall

- The outer wall propagation continues until the flame stabilizes itself on the fuel ports



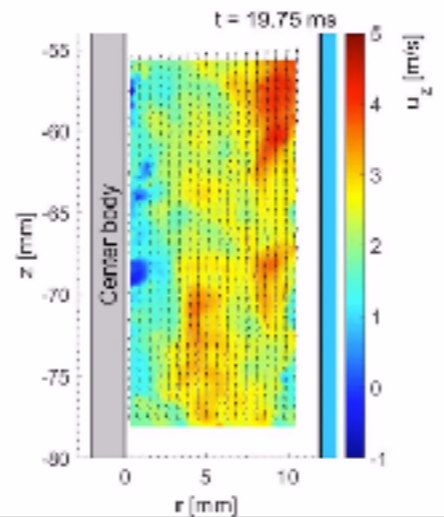
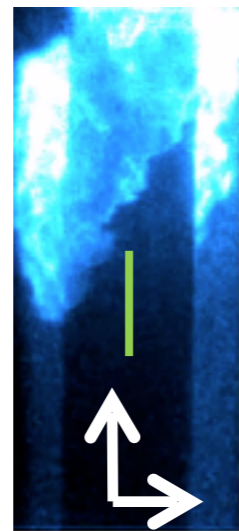
Elevated pressure flashback: Premixed vs Stratified



Premixed

Flow parameters

- Fuel: Methane
- Average axial velocity: 2.5 m/s
- Pressure: 3 atm



Stratified

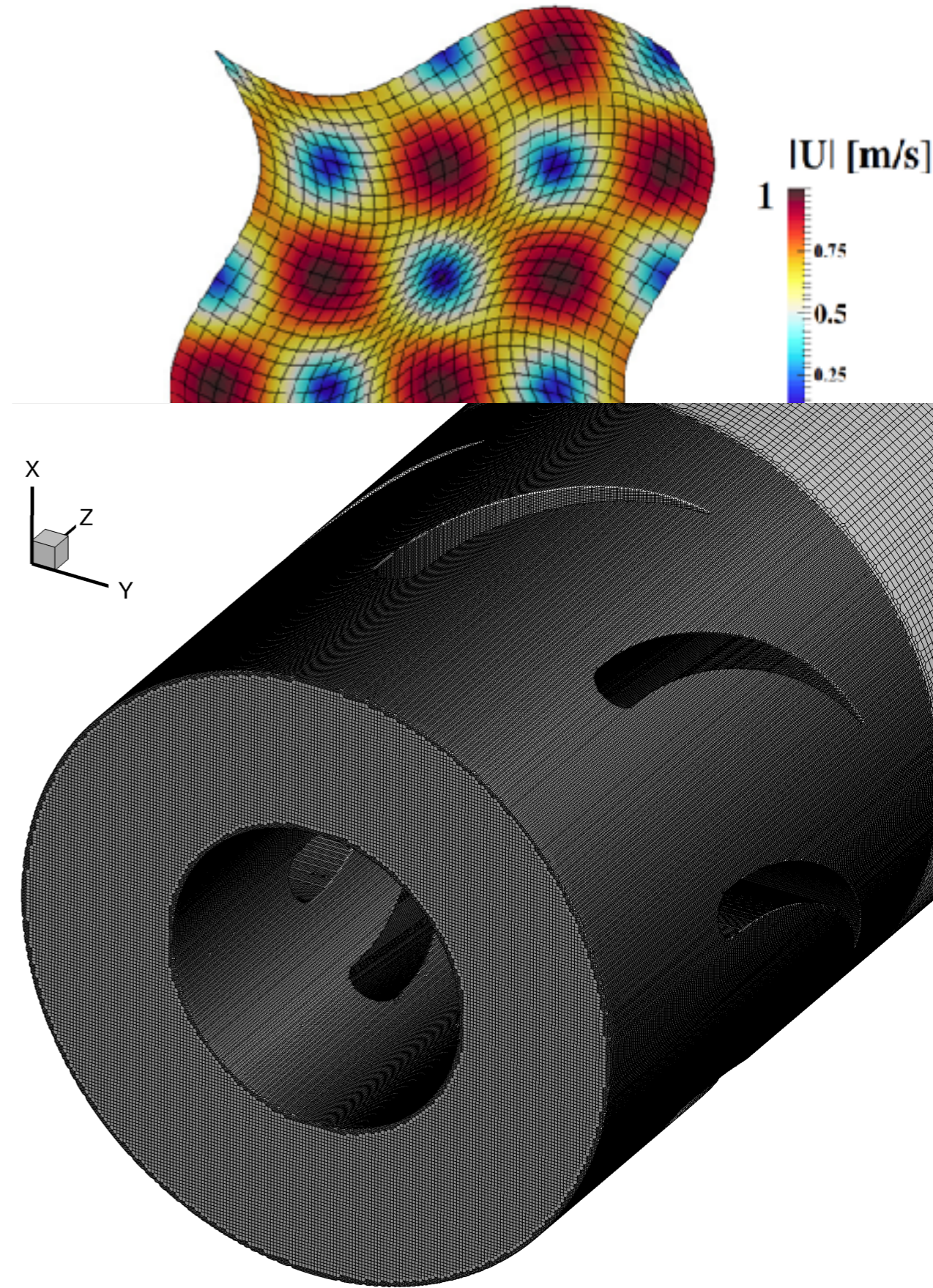
- Premixed flashback at elevated pressures exhibit very small radial spread,
- Stratified flame flashback stops at an intermediate location in the mixing tube
- The flame brush is more wrinkled and exhibits large radial spread reaching up to the outer wall

Summary of Findings

- **A methodology for initiating flashback was developed**
 - ➔ Advanced laser diagnostics used
- **Stratification leads to arresting of flame flashback**
 - ➔ As expected
 - ➔ But, hydrogen seems to get around this solution
- **At elevated pressures, flashback behavior is similar**
- **Radial spread of flame brush larger for stratified flame**
 - ➔ Flame propagation through regions with equivalence ratios outside flammability limit

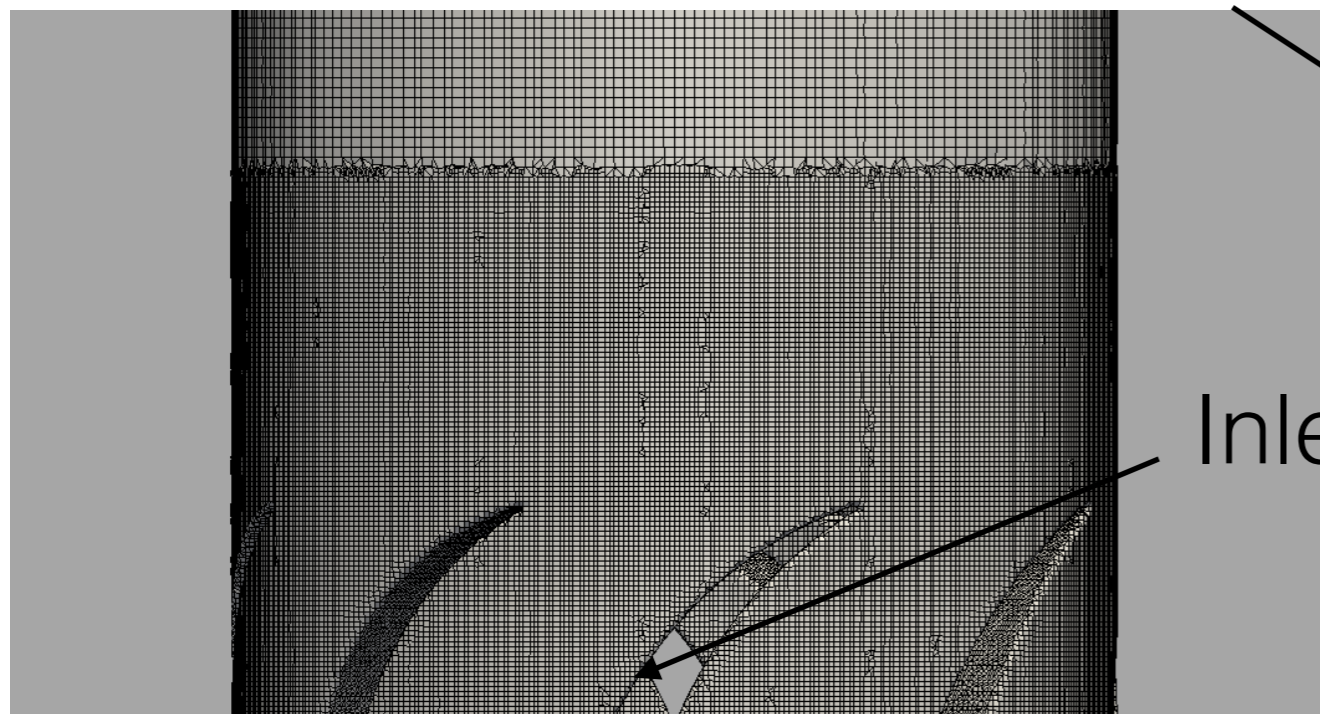
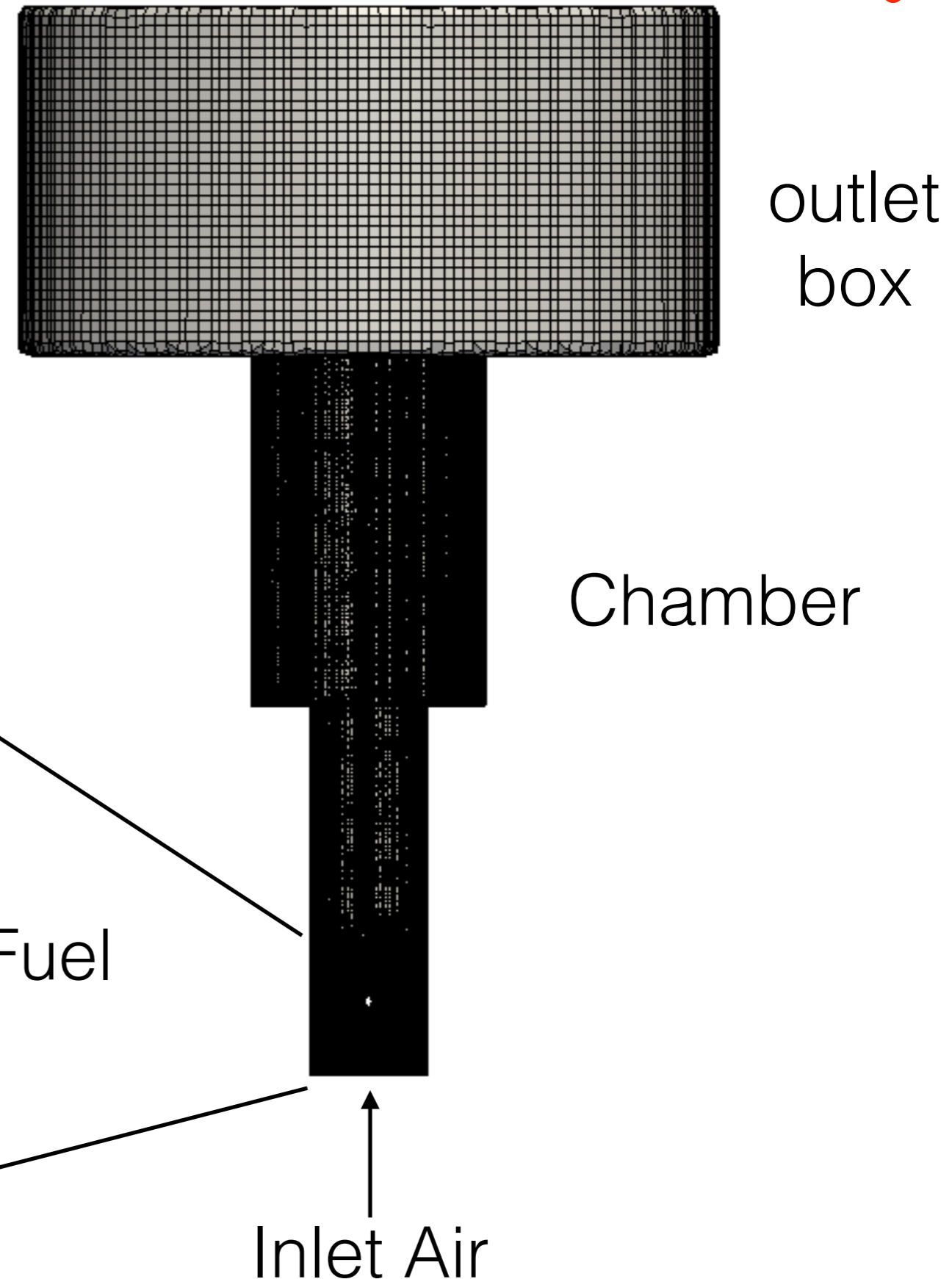
Numerical Setup

- **Variable density low Mach solver - umFlameletFoam**
 - ➔ OpenFOAM based
 - ➔ Low Mach solver
 - ➔ Minimize dissipation
- **10M hexahedral-dominant mesh**
 - ➔ Local refinement at swirler
- **Run for 10,000 core hours on 1008 processors**



Numerical details

- **9.5 million control volumes with clustering near the vanes**
- **Block-structured mesh**
 - ➔ save computational time
 - ➔ reduce numerical dissipation



Boundary conditions

- **Role of outlet box**

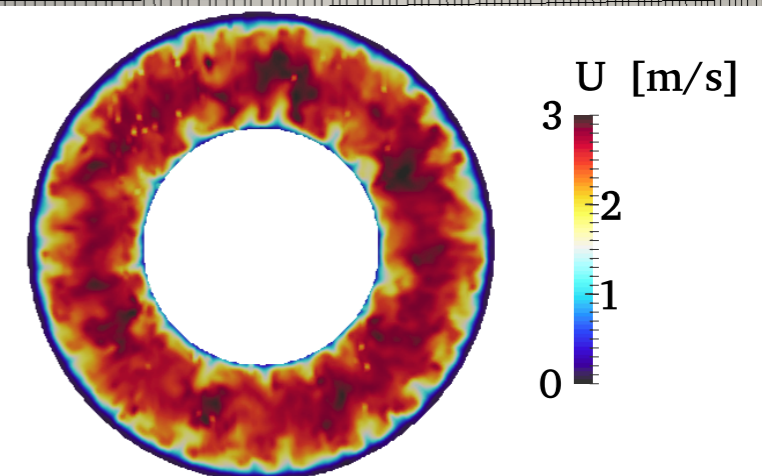
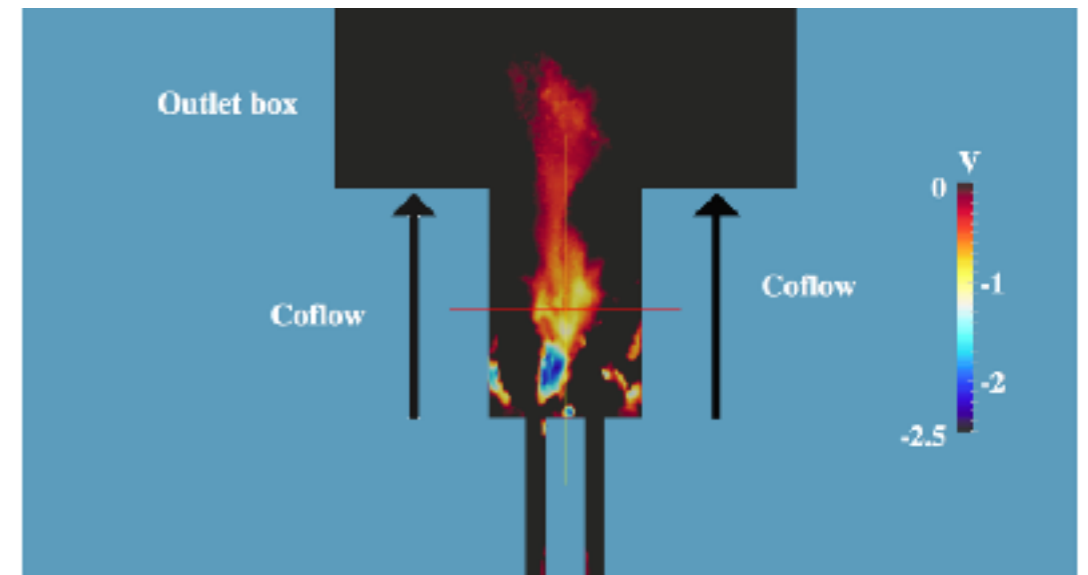
- ➔ Drive vortices outside the chamber
- ➔ Dissipate the vortices

- **Fuel Inlet**

- ➔ Dirichlet BC, fixed in time
- ➔ Mass flow rate matches experiments

- **Turbulent velocity inlet**

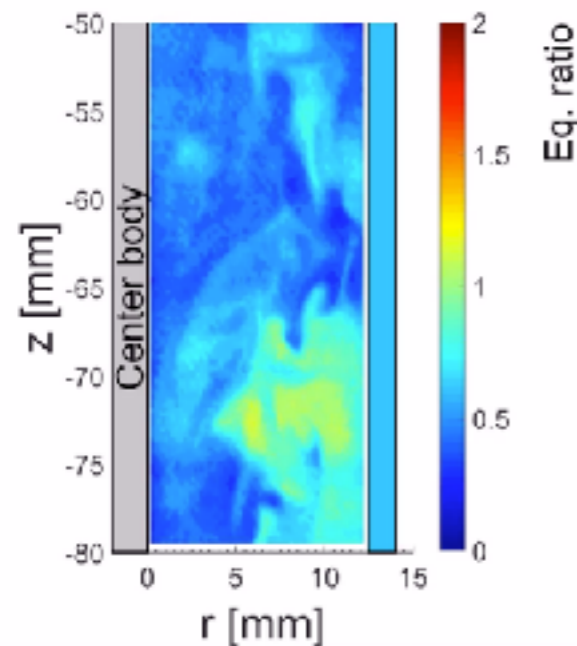
- ➔ From auxiliary annulus simulation



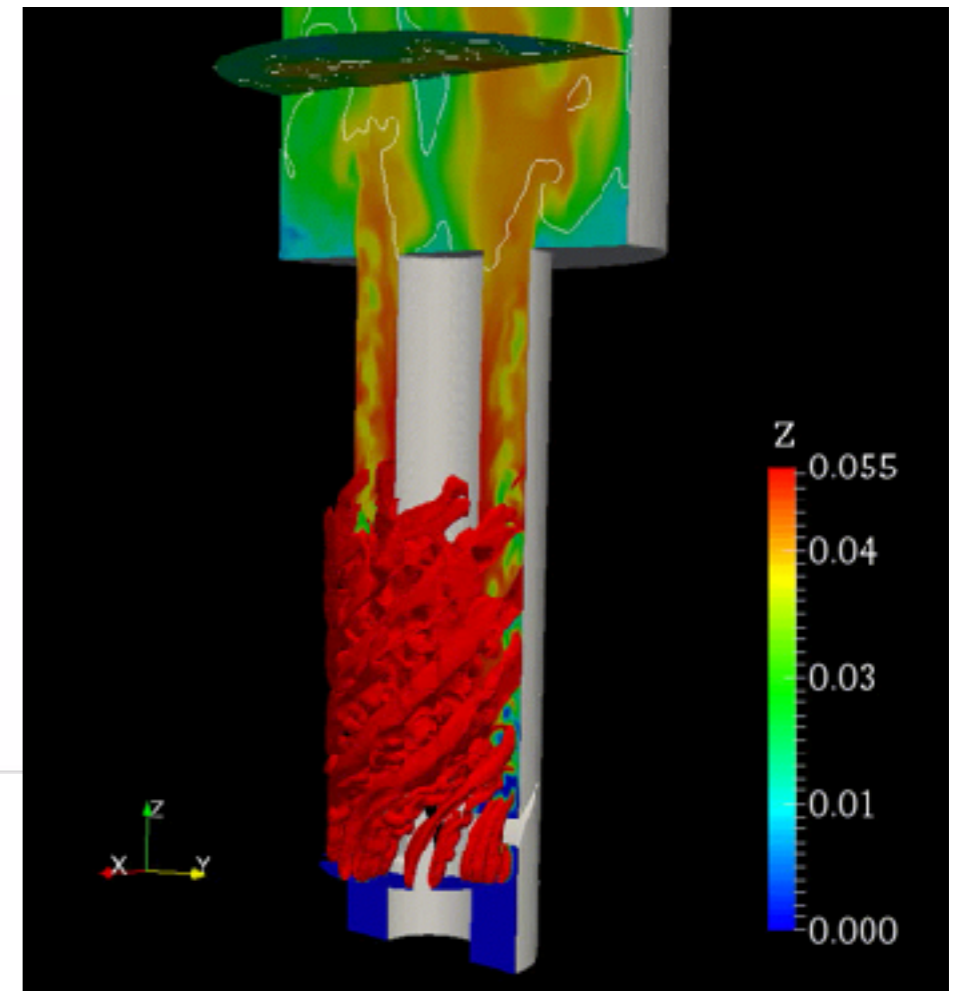
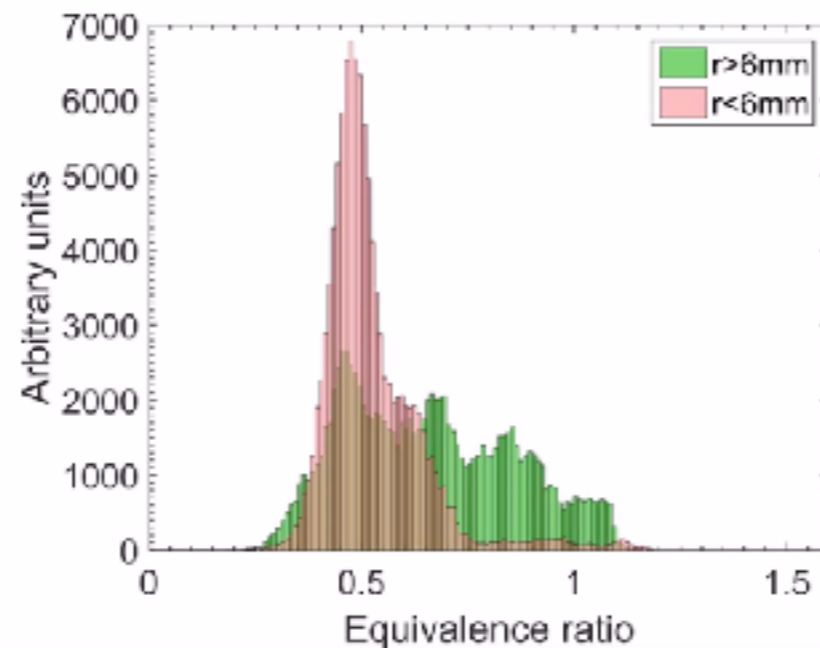
Fuel Distribution

- **Nozzle injection causes non-uniform fuel distribution in the radial direction**

ACETONE PLIF



HISTOGRAM OF FUEL CONCENTRATION

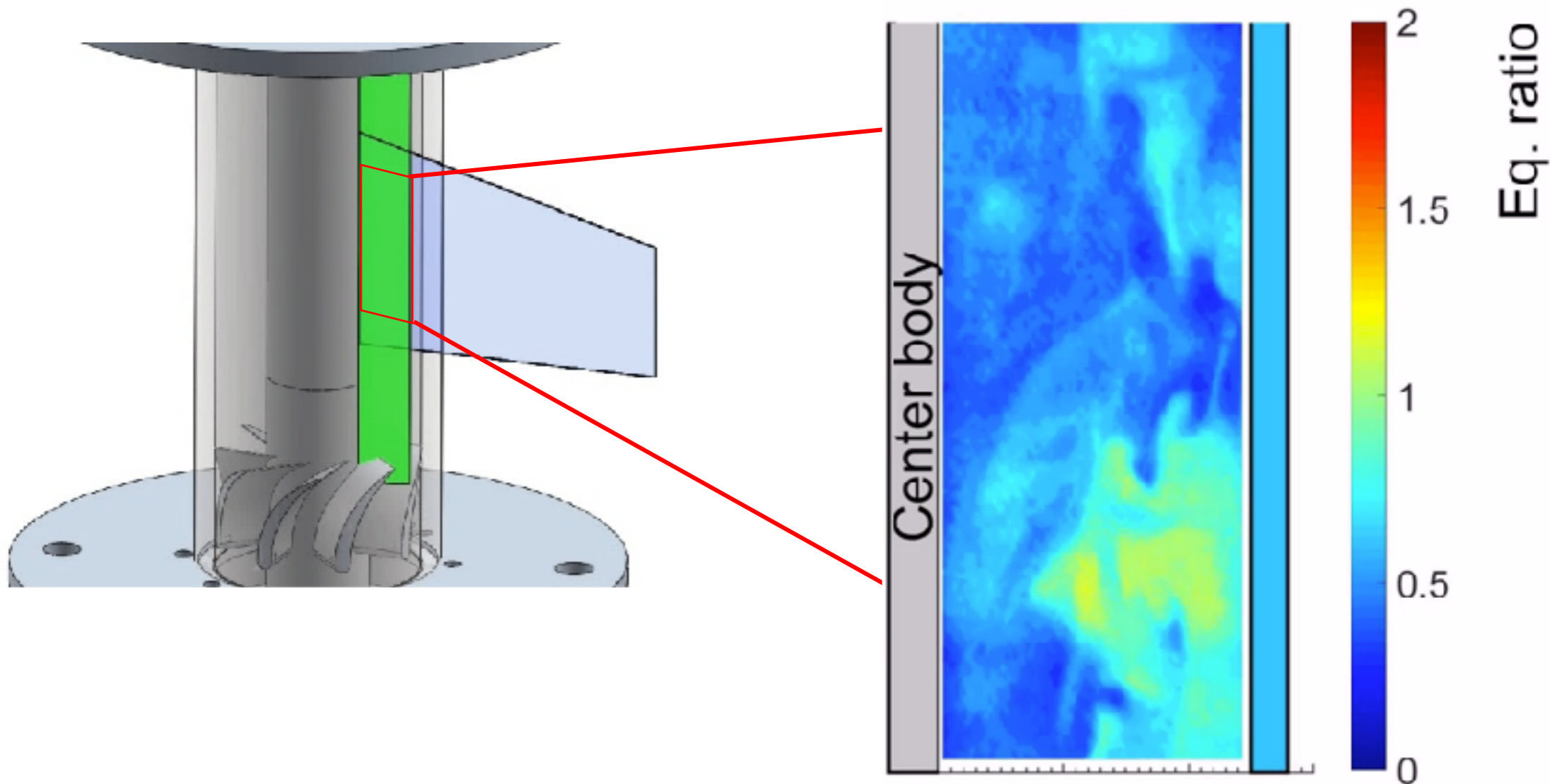


- **Richer mixtures closer to outer wall**

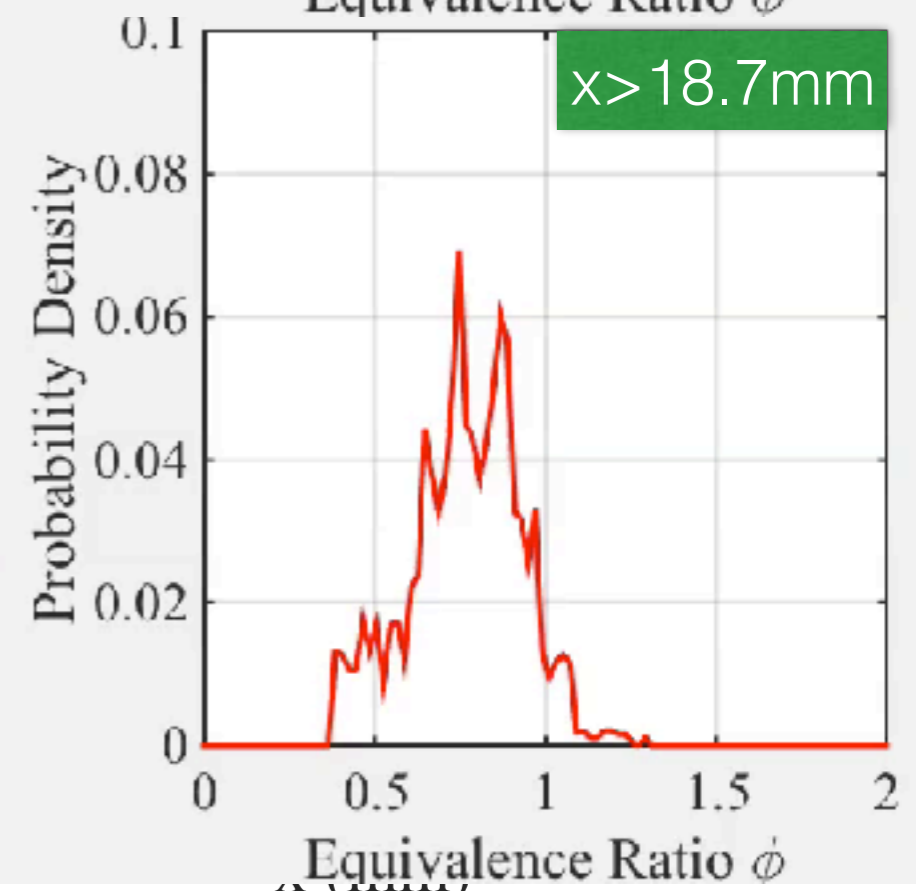
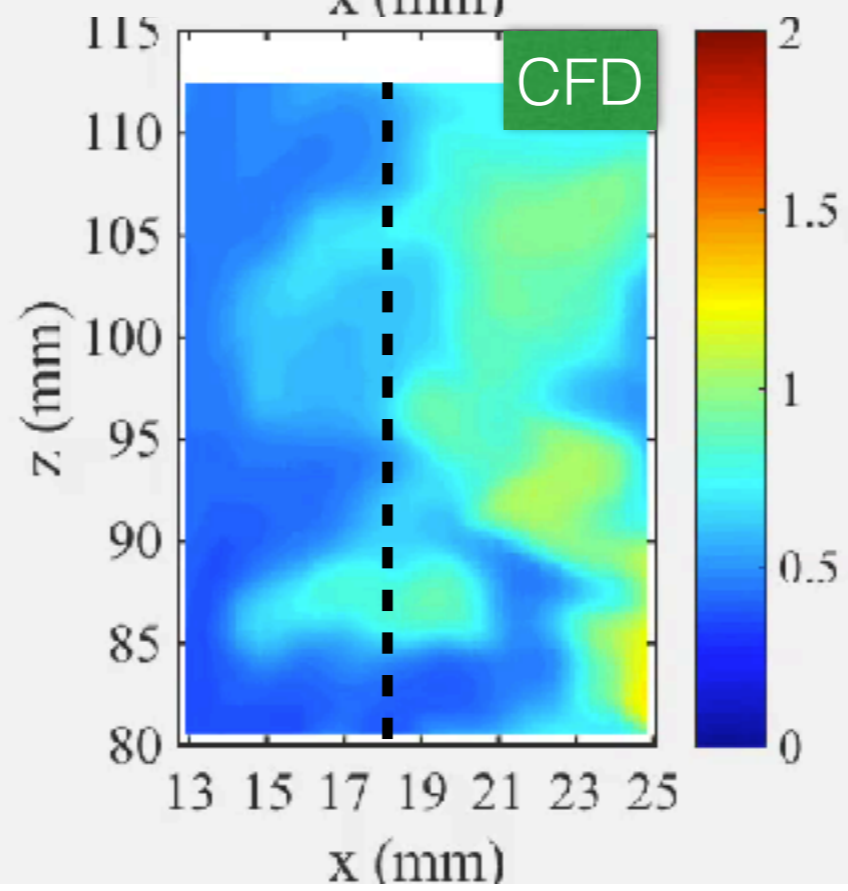
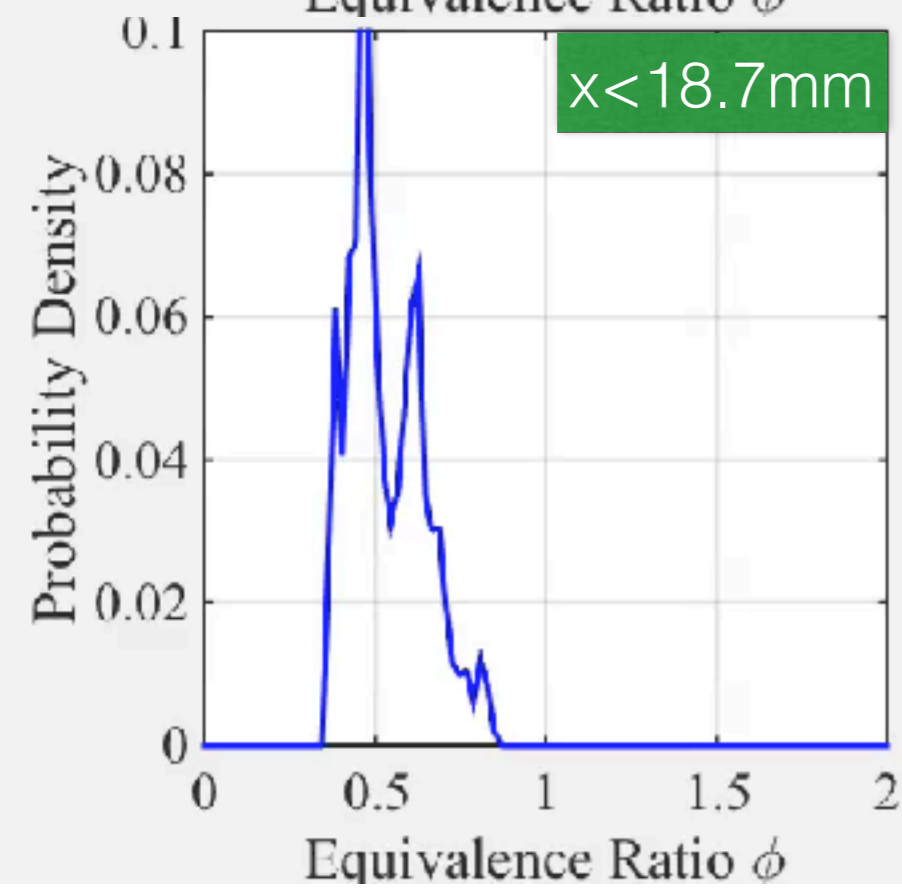
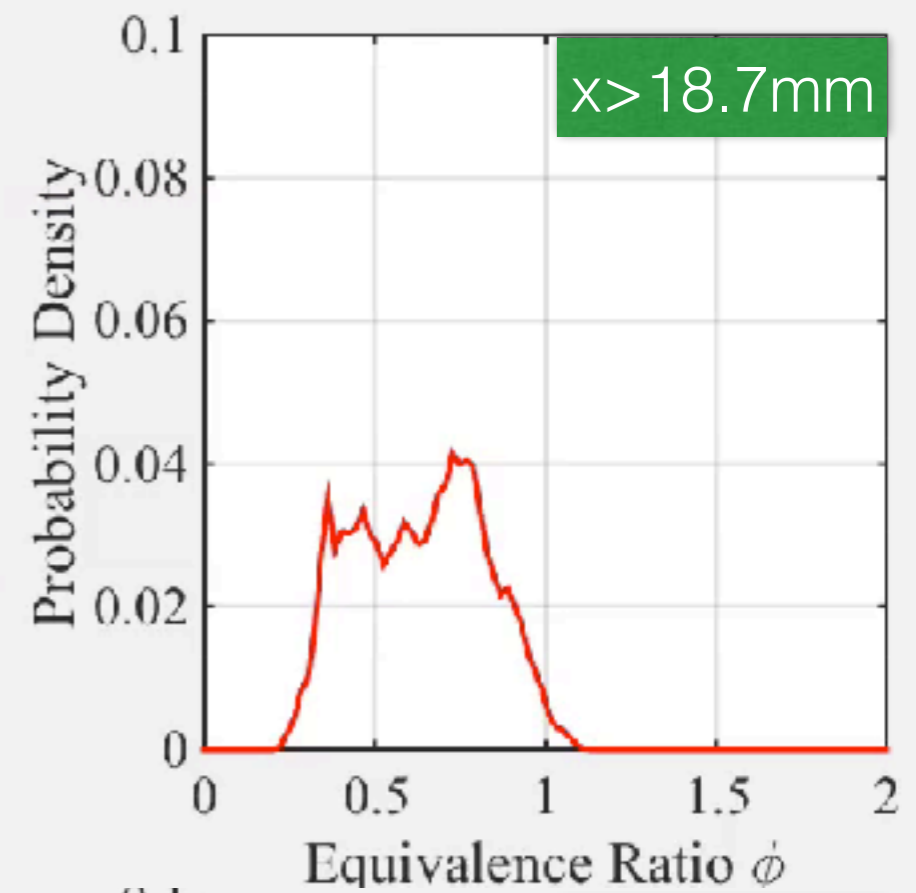
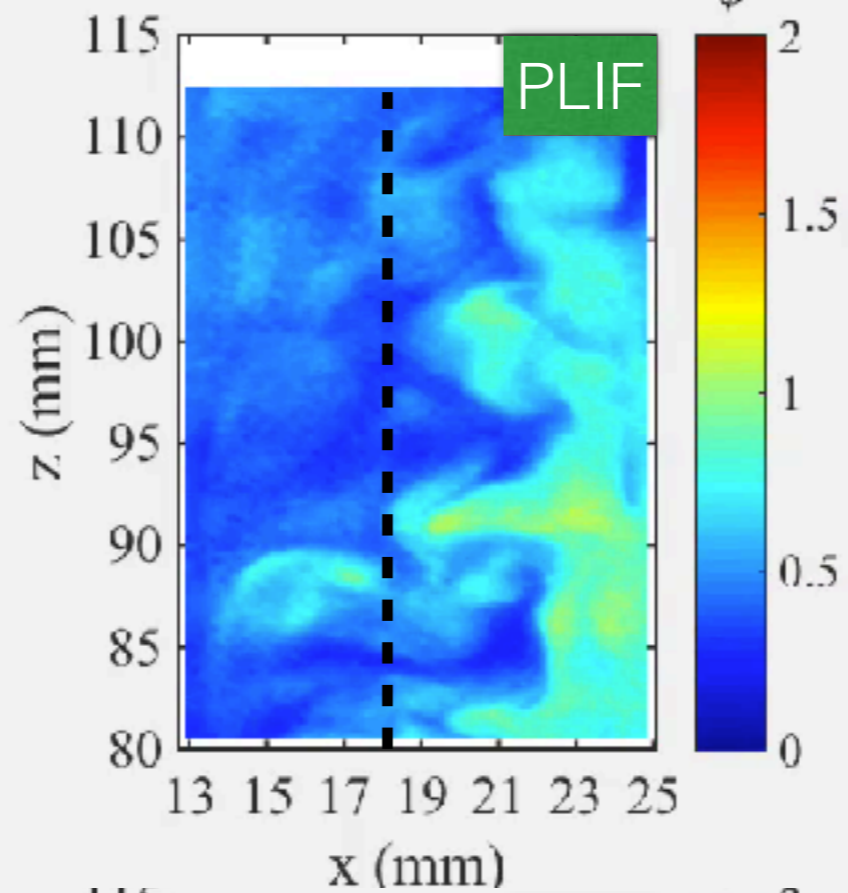
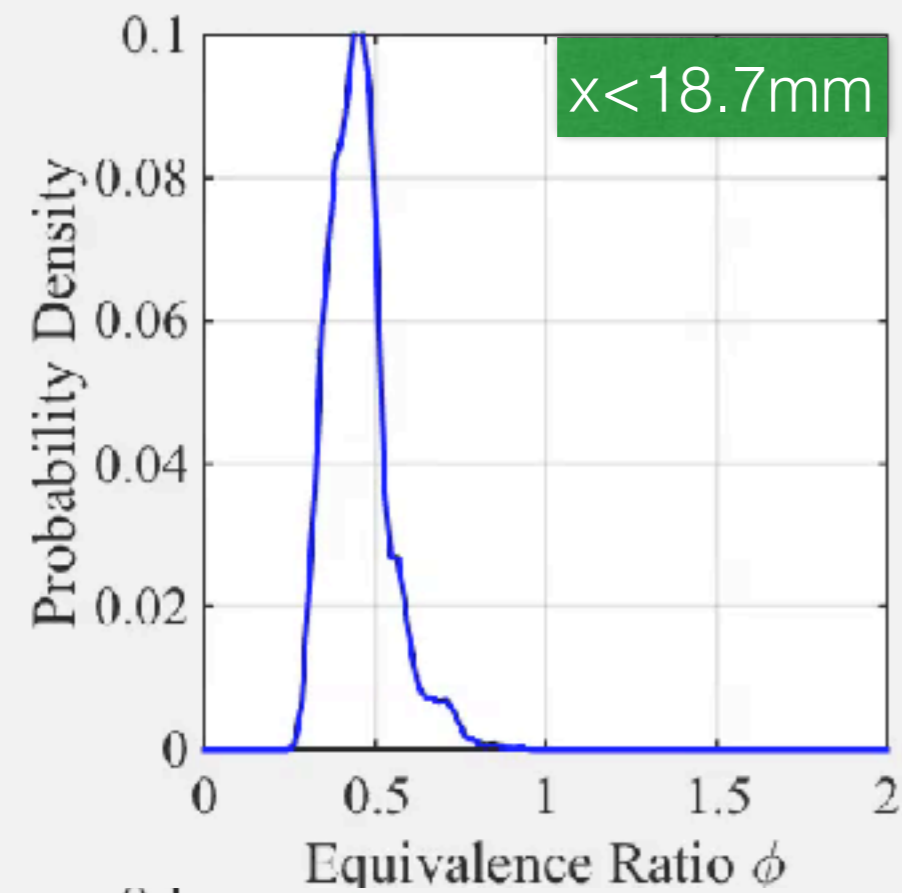
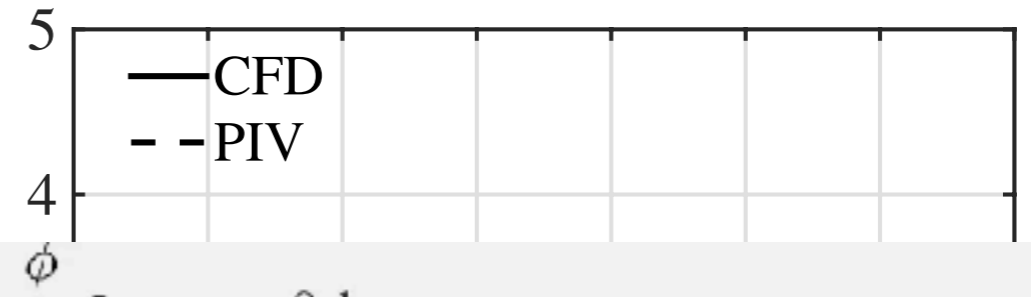
Non-reacting Case Study

- **Fuel stream replaced by acetone seeded air**
- **PLIF measurement of equivalence ratio**

Operating Condition
Temperature : 300K
Pressure : 1atm
Global equivalence ratio: 0.5
Bulk velocity : 2.5m/s

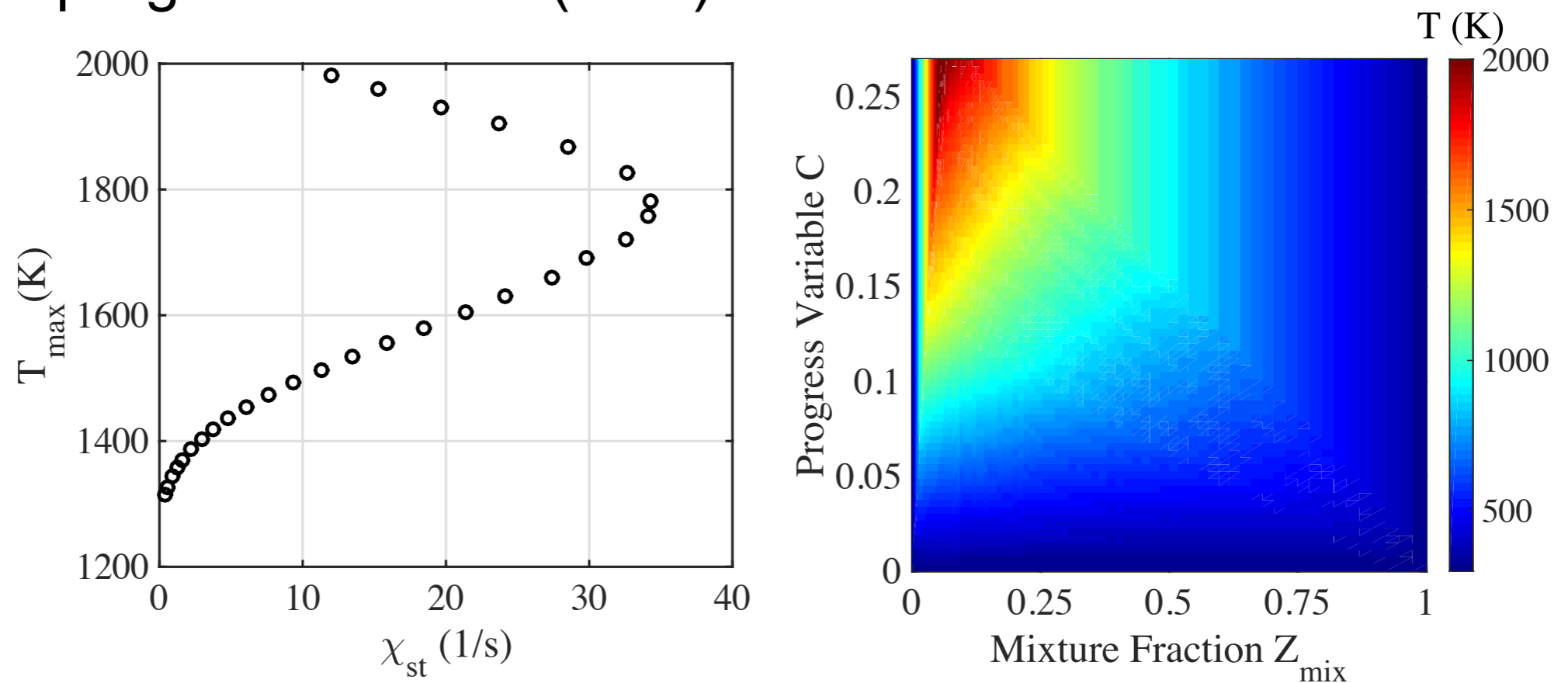


Non-reacting Case Study



Modeling Approach

- Based on large eddy simulation(LES)/flamelet approach
- Stratified mixtures
 - ➔ Mixture fraction and progress variable required
 - ➔ Flamelet progress variable (FPV) method



- **Heat loss**

- ➔ Additional coordinate for enthalpy defect

Heat Loss Modeling

- **Introducing heat loss into flamelet**

➔ Modify flamelet equations to account for heat loss

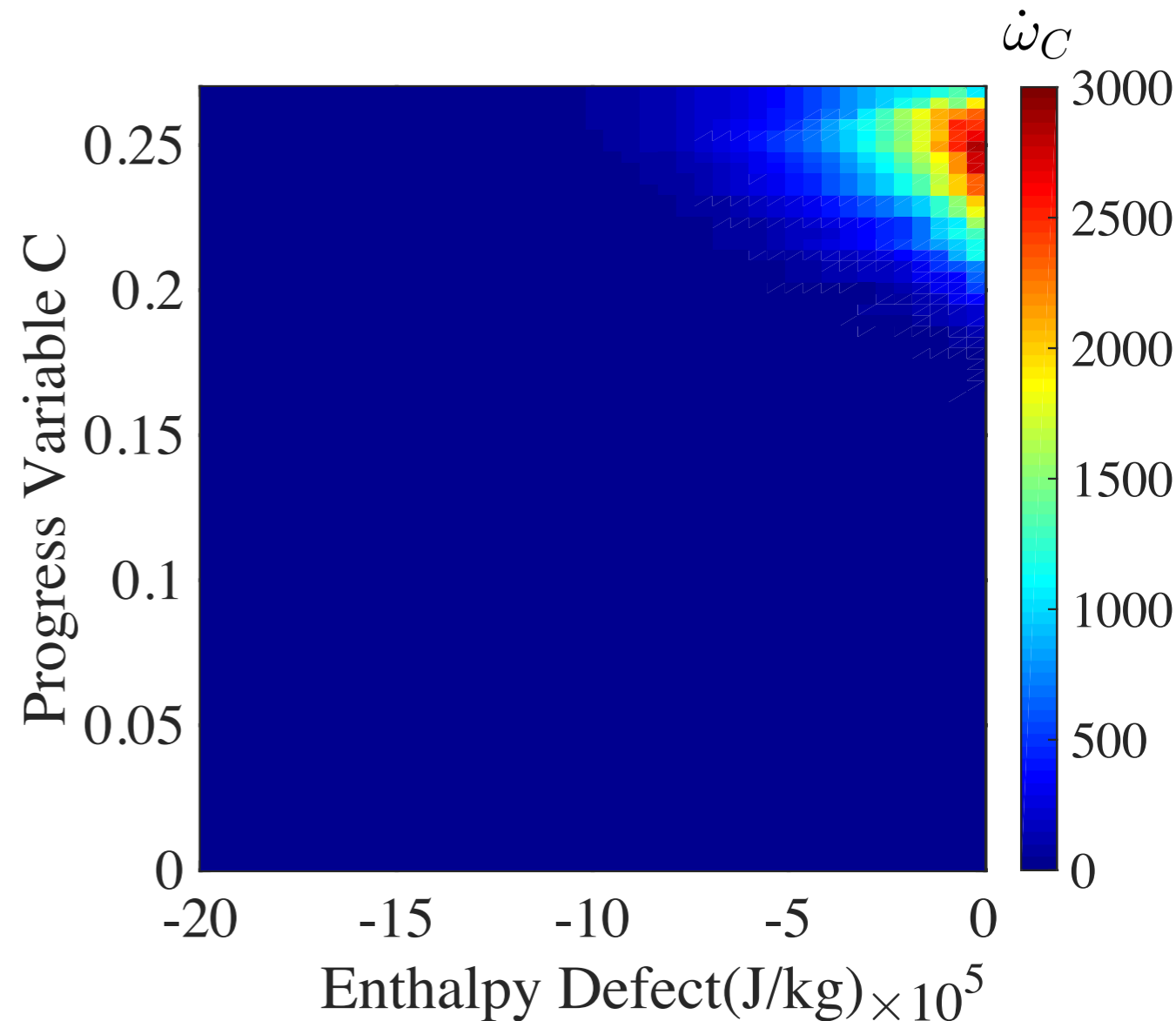
$$\frac{\rho C_p \chi}{2} \frac{\partial^2 T}{\partial Z^2} = \dot{\omega}_h - \lambda \frac{T(Z) - T_w}{\delta}$$

➔ Fourier heat loss term, varied based on δ

- **Transport equation of enthalpy defect**

$$H = h_{tot} - h_{tot,Ad}$$

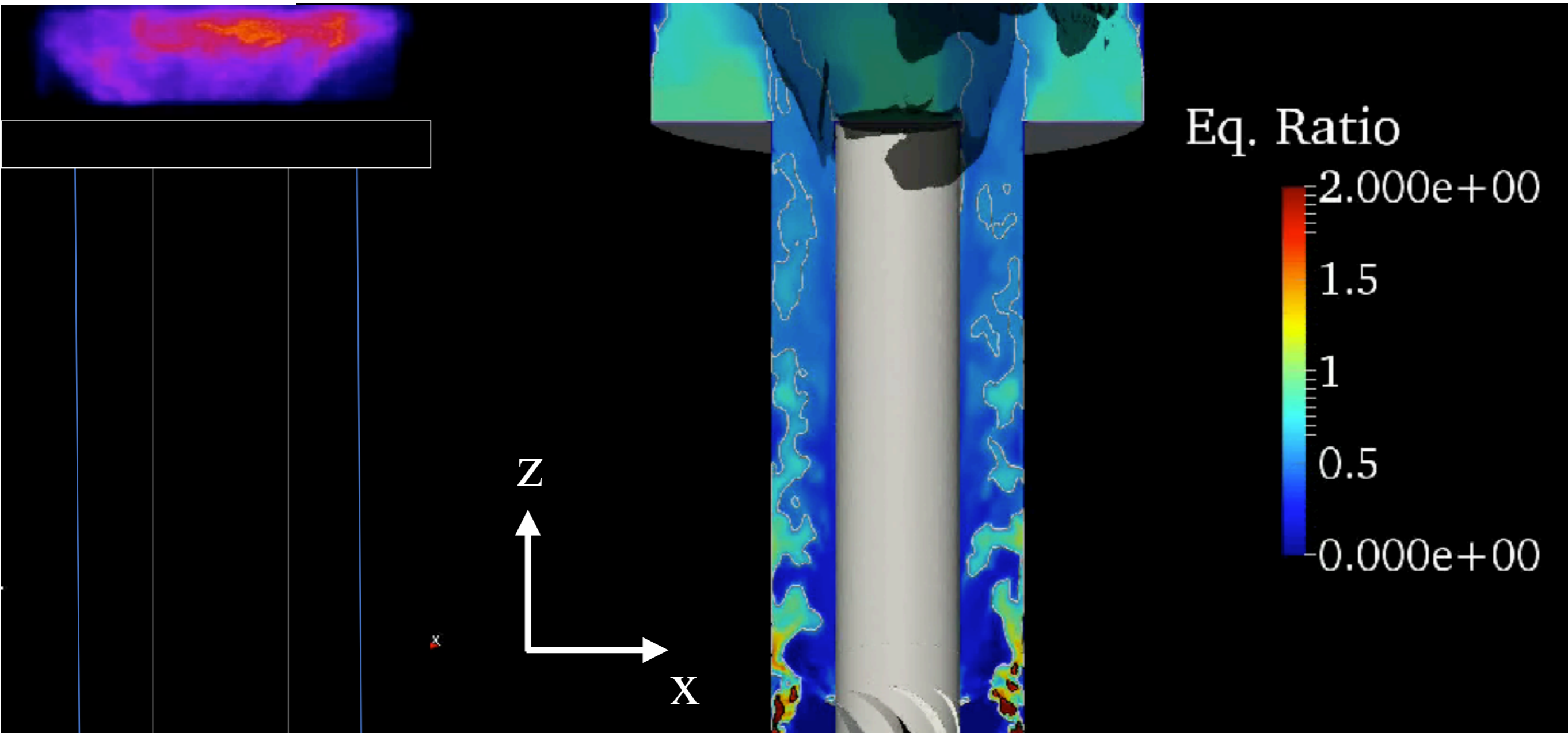
$$\frac{\partial \bar{\rho} \tilde{H}}{\partial t} + \nabla \cdot (\bar{\rho} \tilde{v} \tilde{H}) = \nabla \cdot \left(\frac{\mu_T}{Pr} \nabla \tilde{H} \right) + \nabla \cdot (\lambda \nabla T) - \nabla \cdot (\lambda_{Ad} \nabla T_{Ad})$$



Adiabatic Reacting Case Study

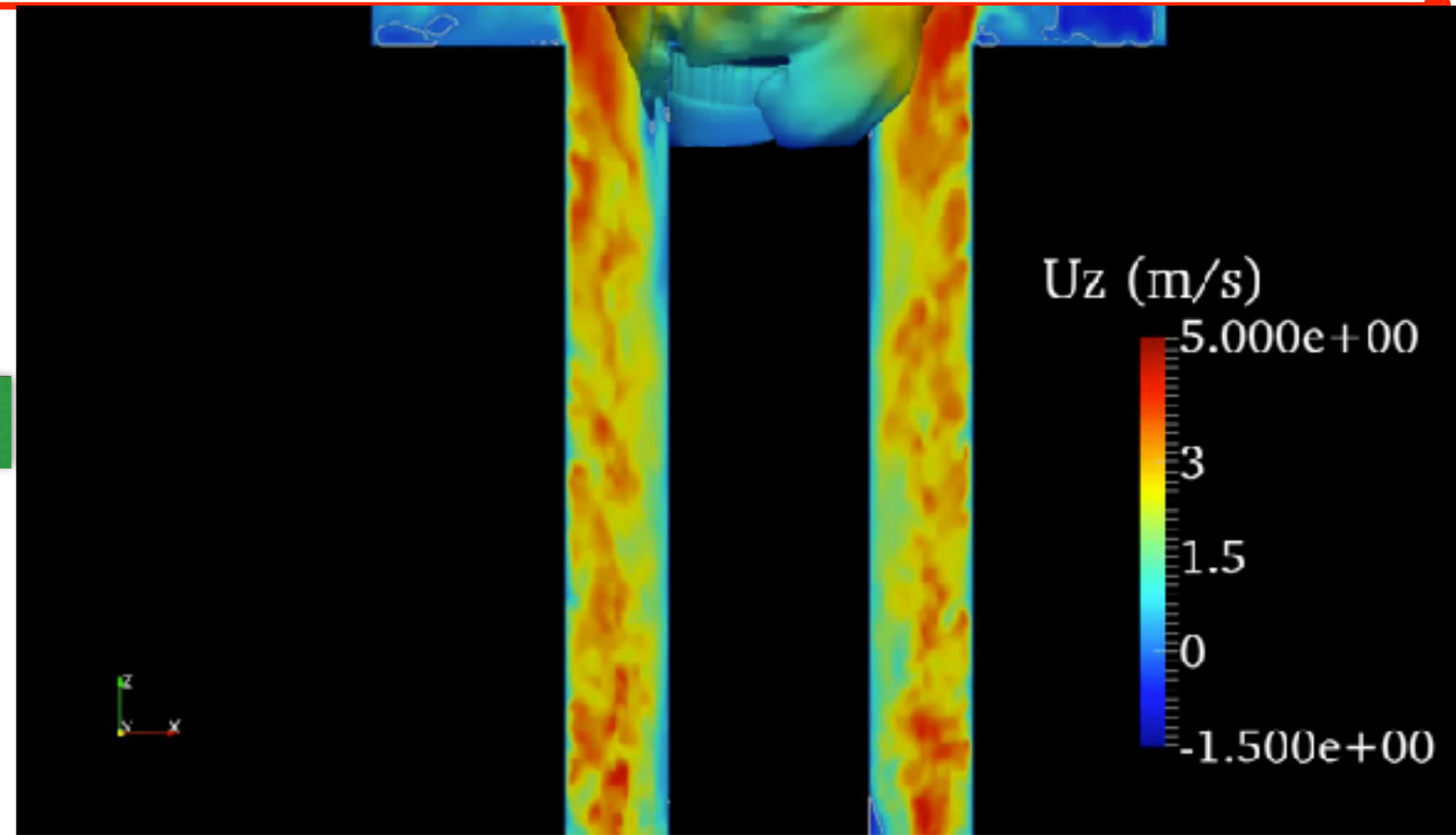
Chemiluminescence

CFD

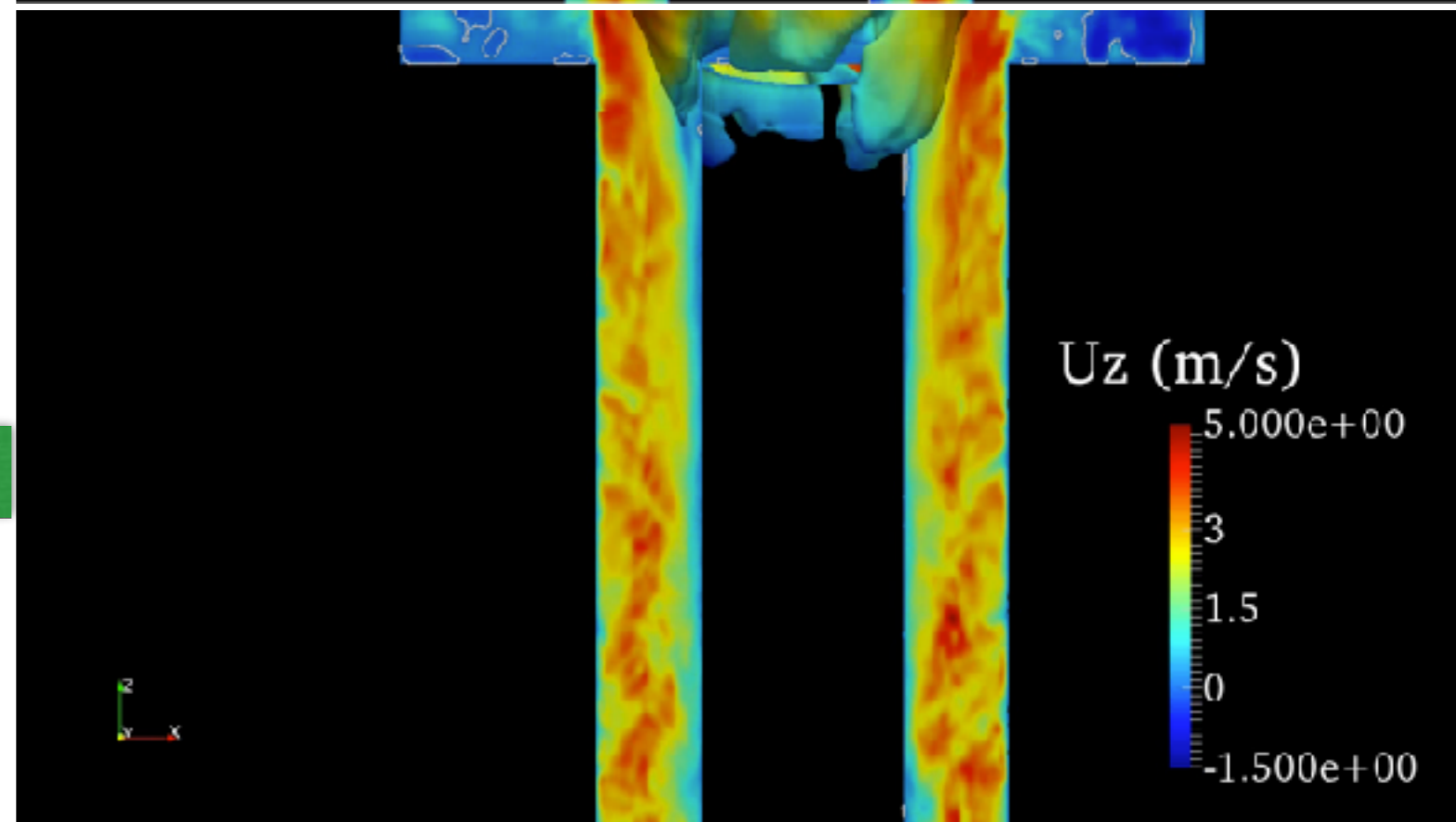


Non-adiabatic Reacting Case Study

Adiabatic
(1/50 real time speed)



Non-adiabatic
(1/50 real time speed)

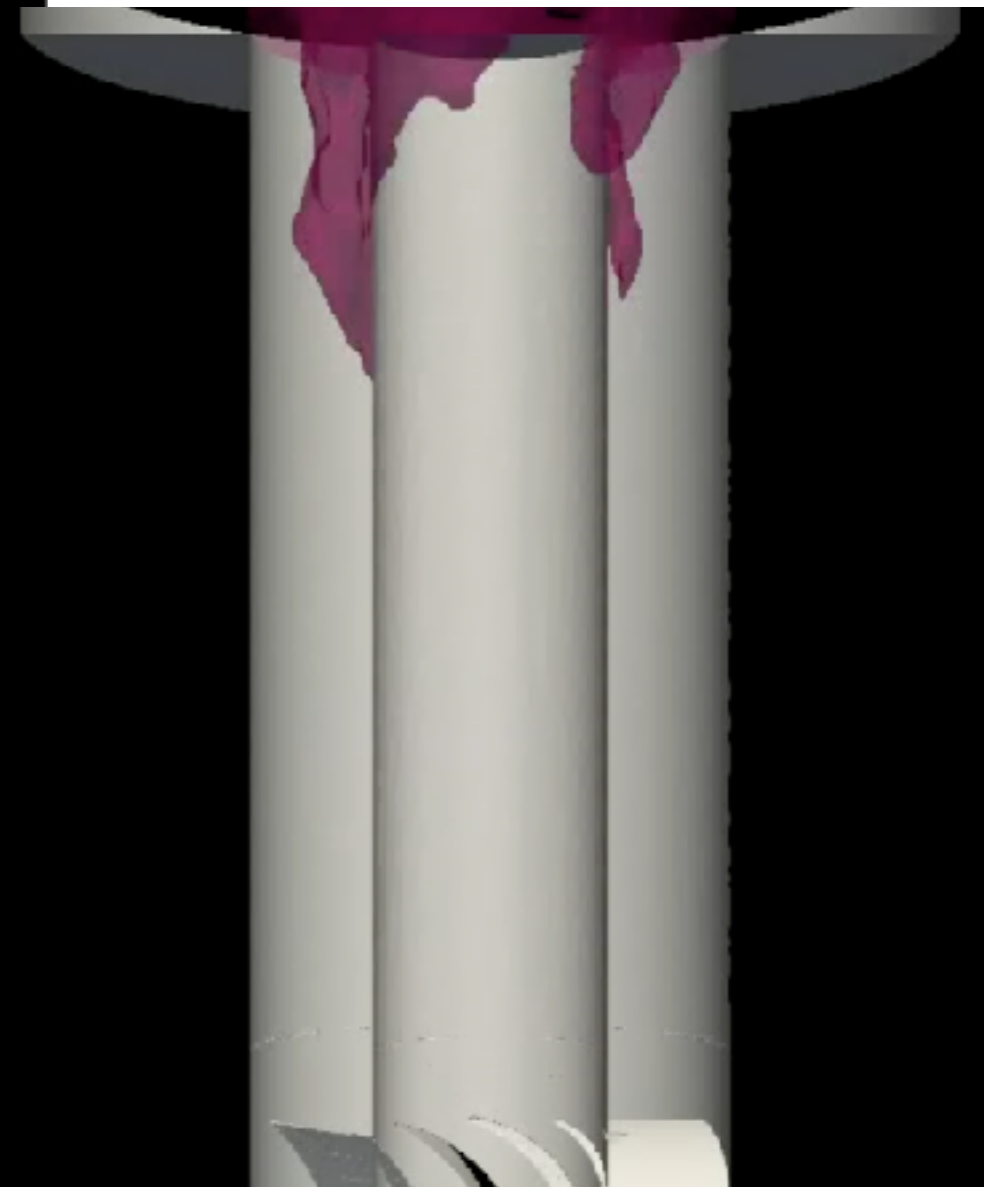
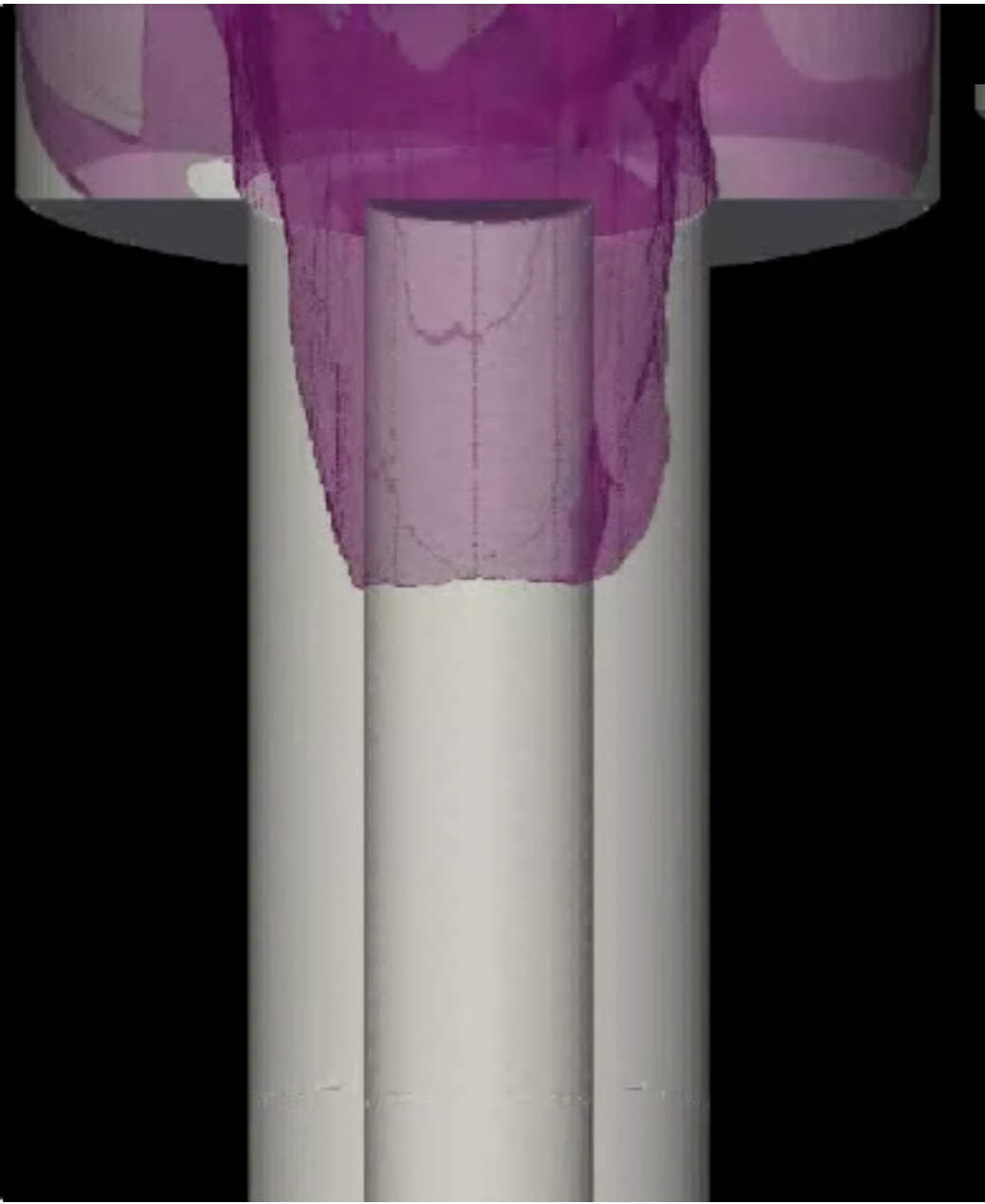
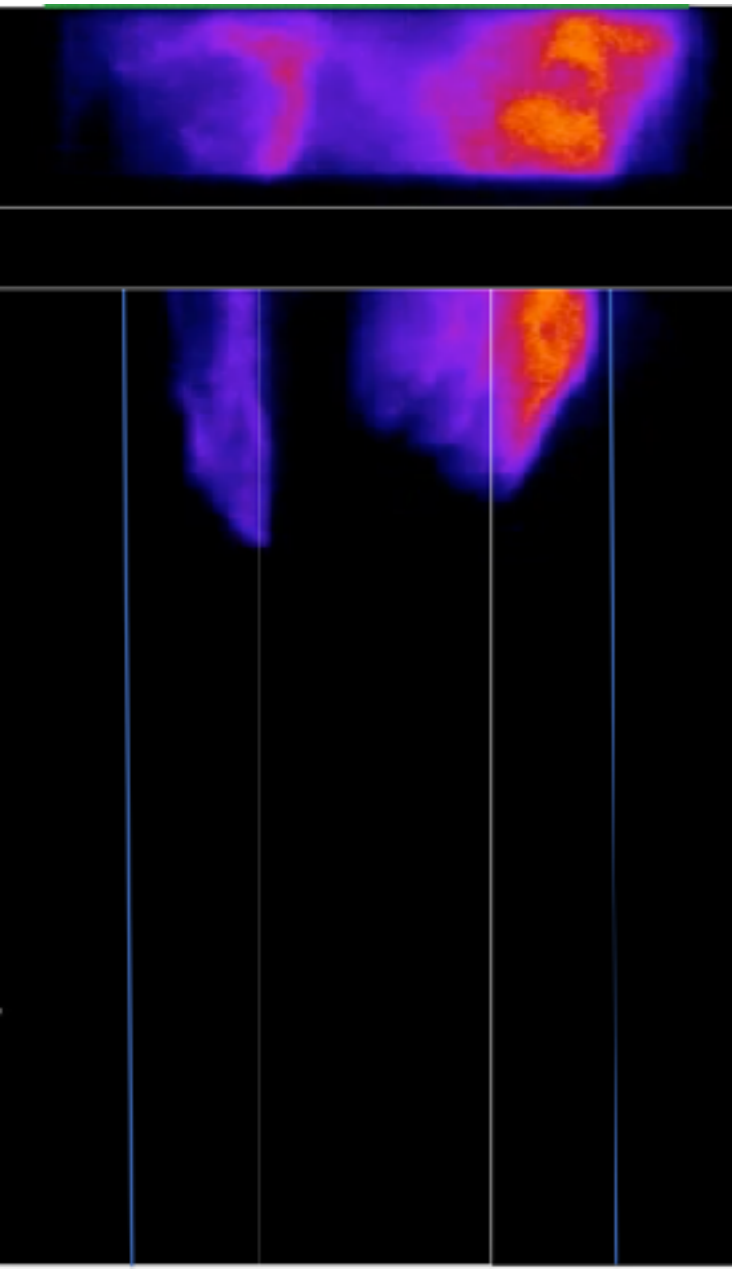


Non-adiabatic Reacting Case Study

Chemiluminescence

Adiabatic

Non-adiabatic



Lean Premixed Combustion at High Pressures

- **MILD combustion conditions**

- High recirculation rate to maintain combustion

- **Asymmetric nozzles**

- Recirculation predominantly k the nozzles

- Very high jet velocities

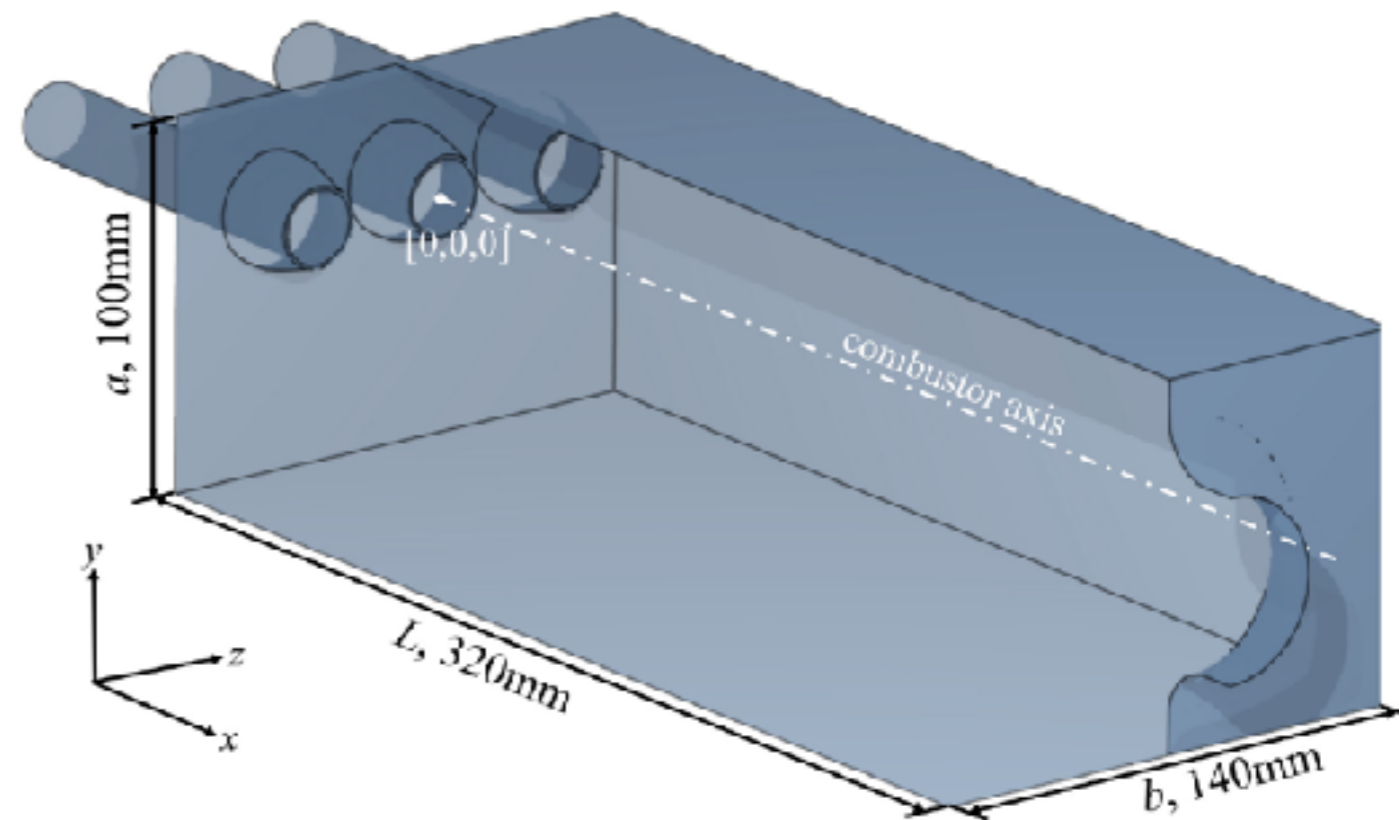
- **Broad reaction zones**

- Strain influenced

- Large heat loss to walls

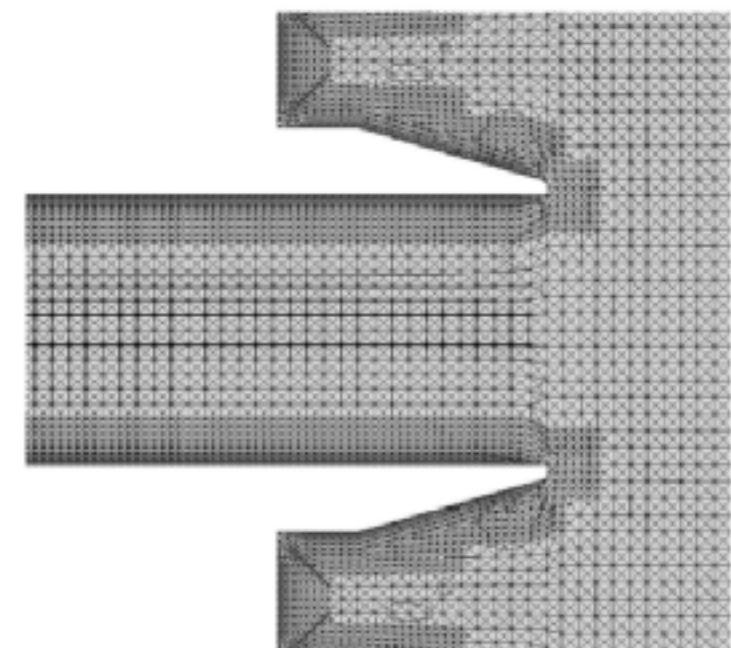
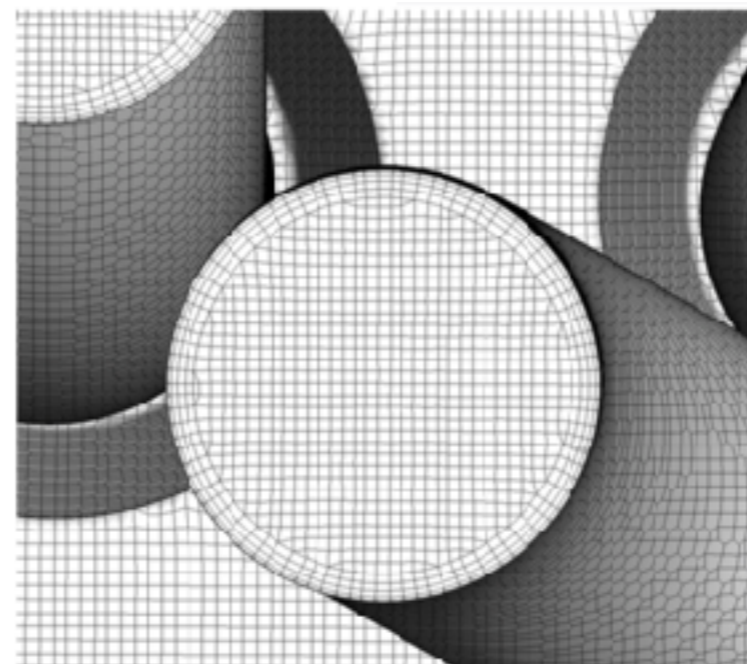
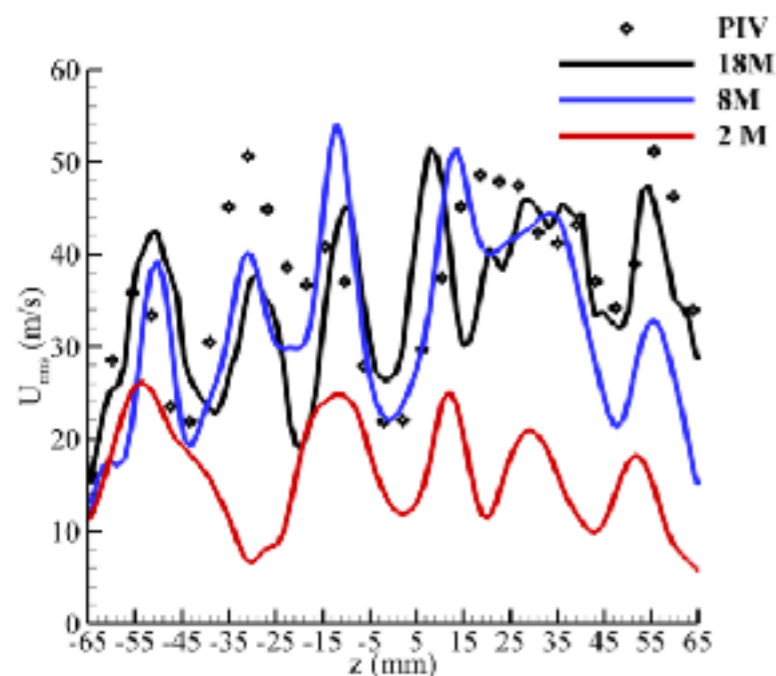
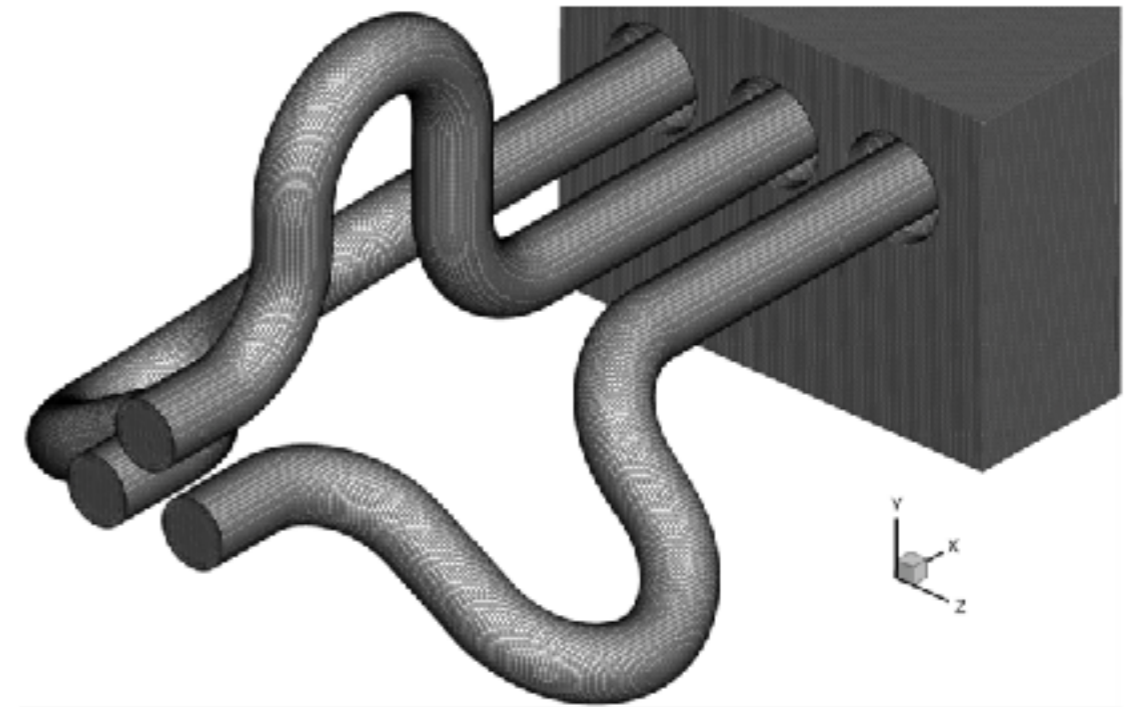
- **Methane or hydrogen as fuel**

- **Experimental data from DLR**



DLR 3-jet Case: Numerical details

- 8 M grid points in the flow
DNS limit
- Dirichlet BC for velocity
and progress variable
- Extended pipes at the inlet
to generate turbulence
- Inlet velocity 120 m/s



DLR 3-Jet Case - Heat Loss Effect

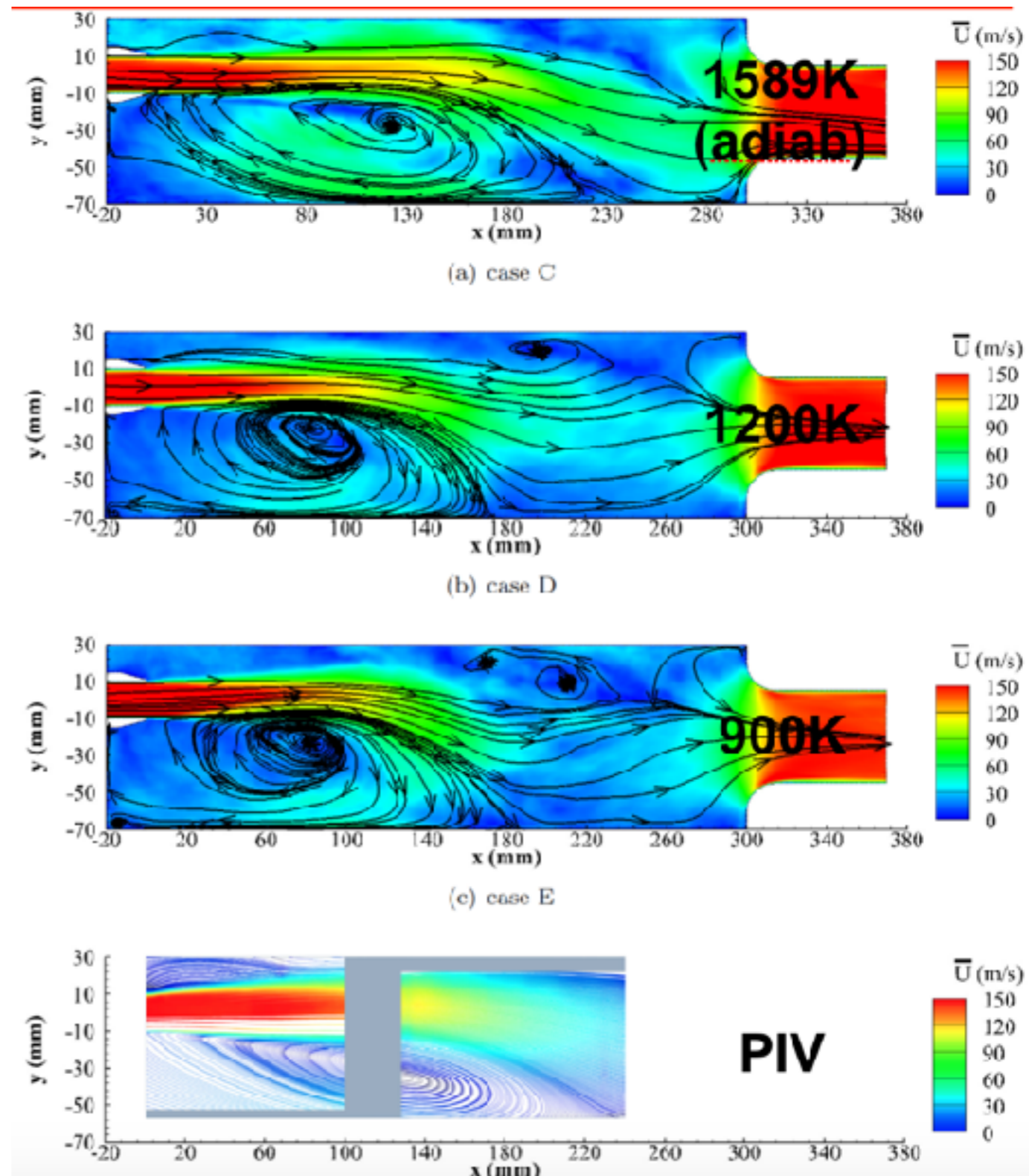
- **Wall temperature has significant effect on flow structure**

➔ Higher heat loss leads to smaller recirculation zone

- **Simulations capture flow structure reasonably well**

➔ Lack of adequate experimental data

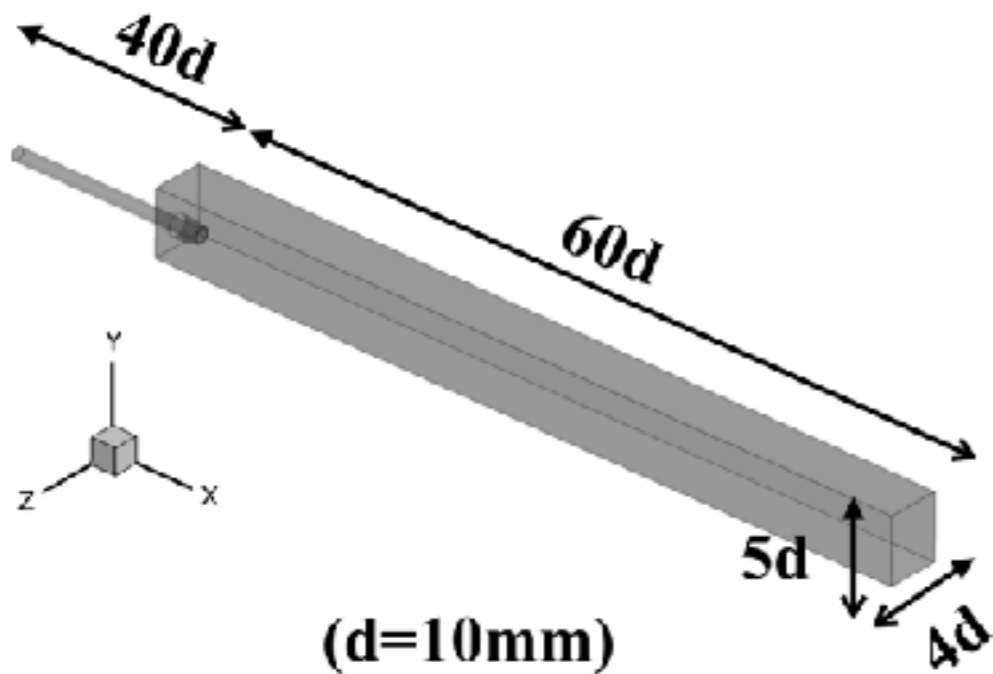
➔ Some issues with measurements noted



Validation - DLR 1-Jet Case

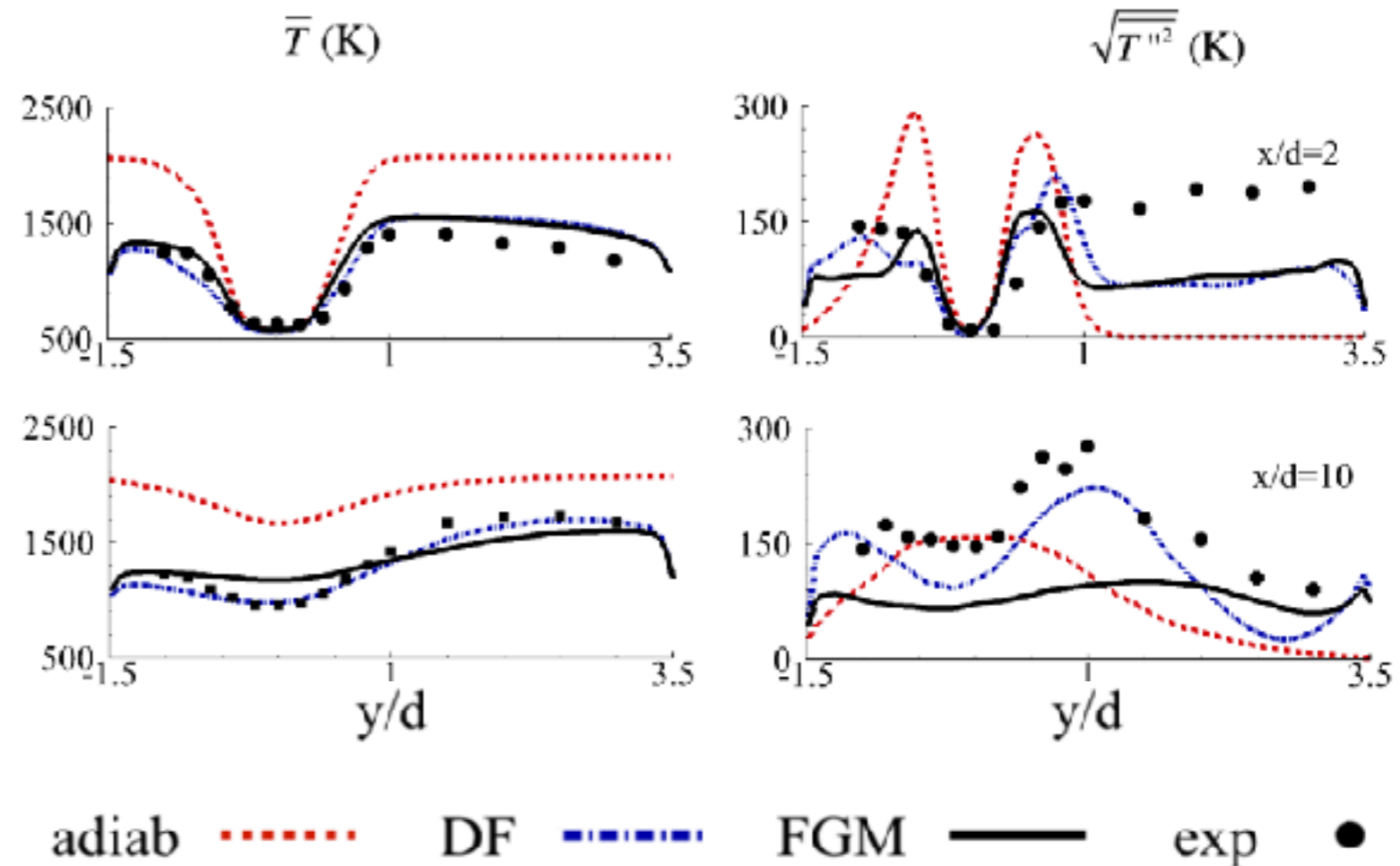
- **Modification of the 3-Jet case**

➔ Single nozzle inflow



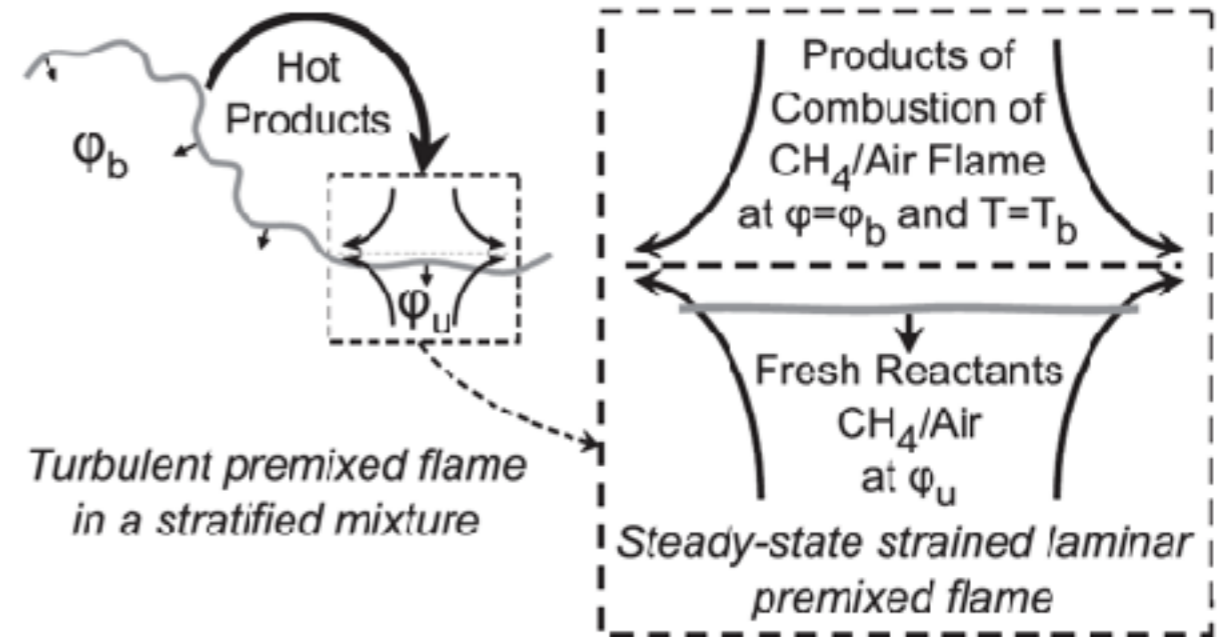
(d=10mm)

Preheat premixed methane-air:
Operating pressure: 1atm
Jet bulk velocity: 90m/s
Wall temp: 1000K
Equivalence ratio: 0.67



Effect of Strain

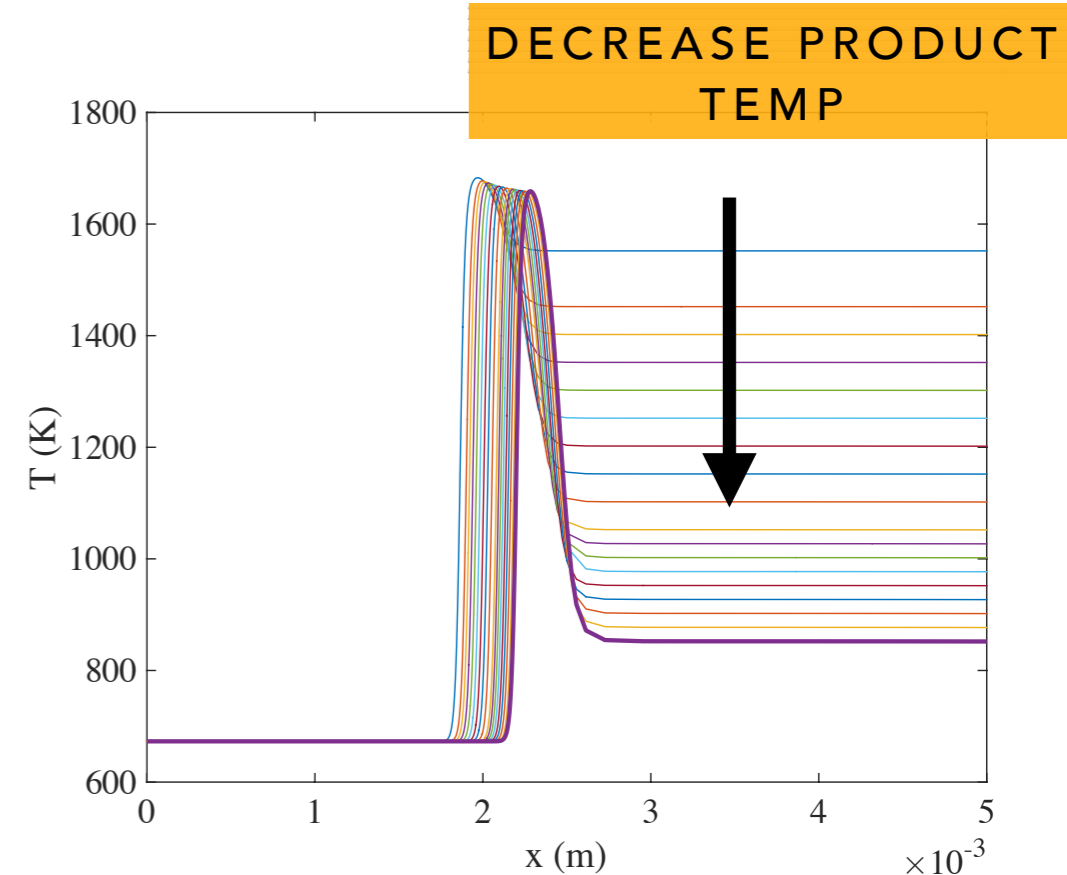
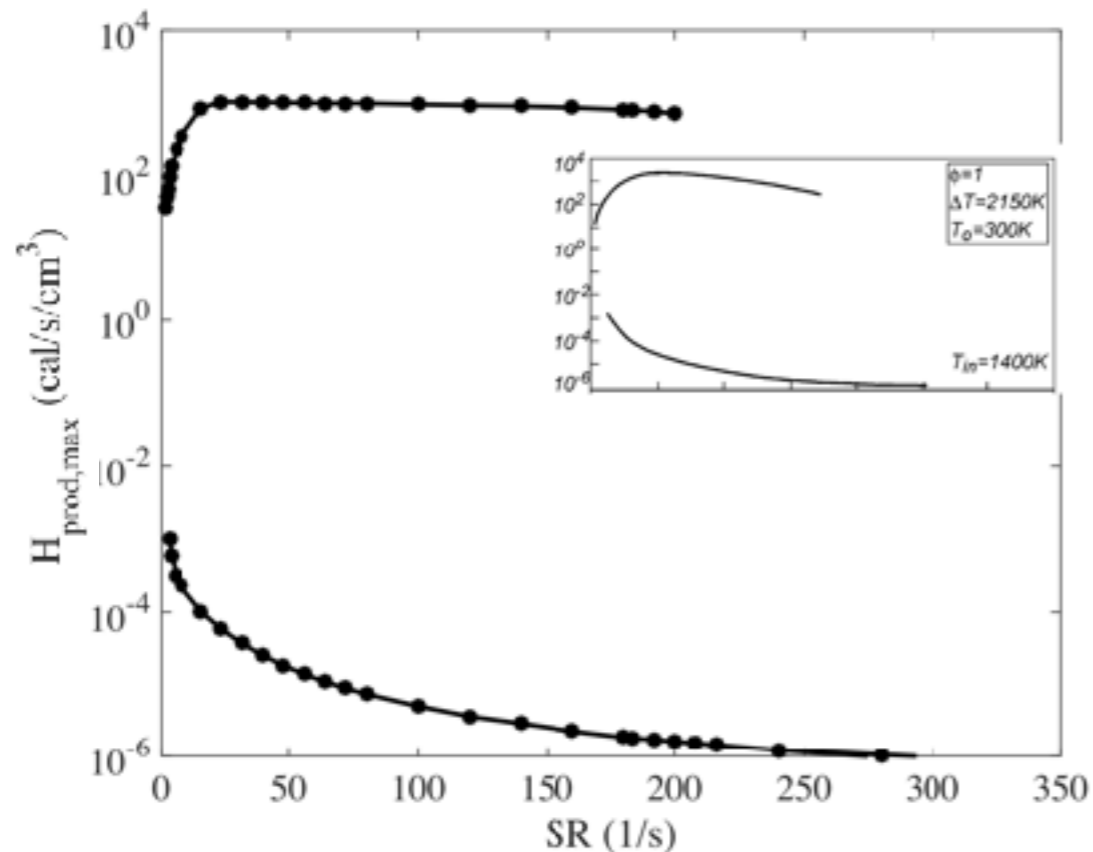
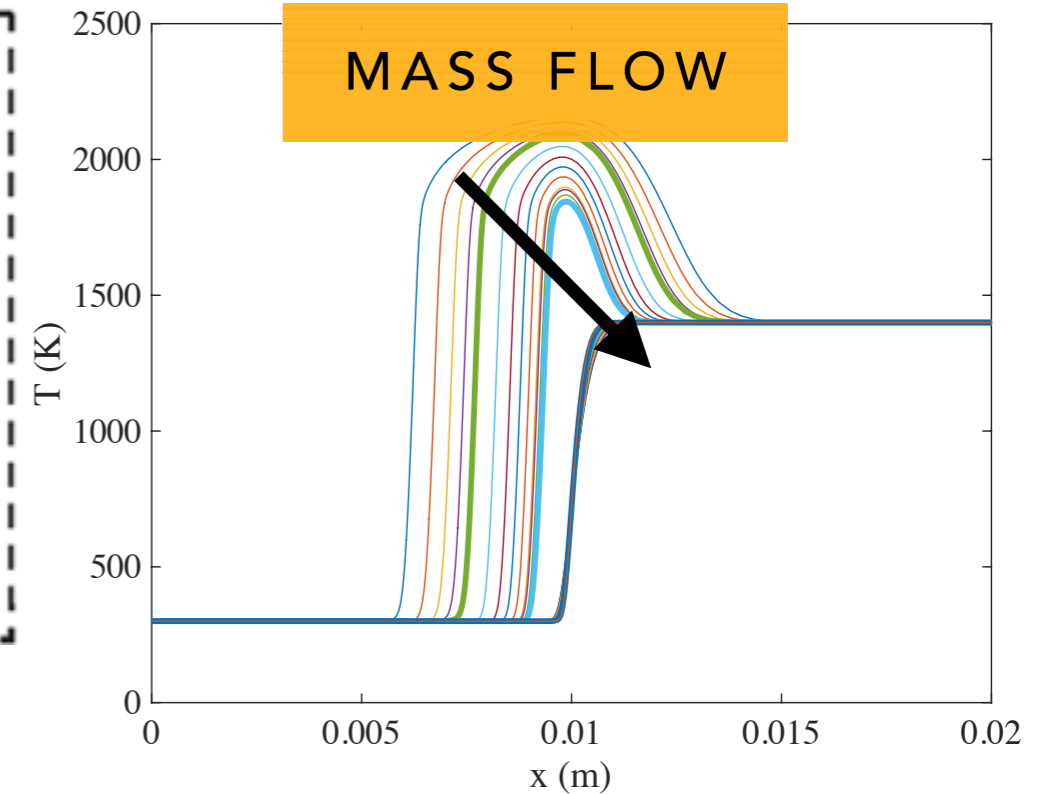
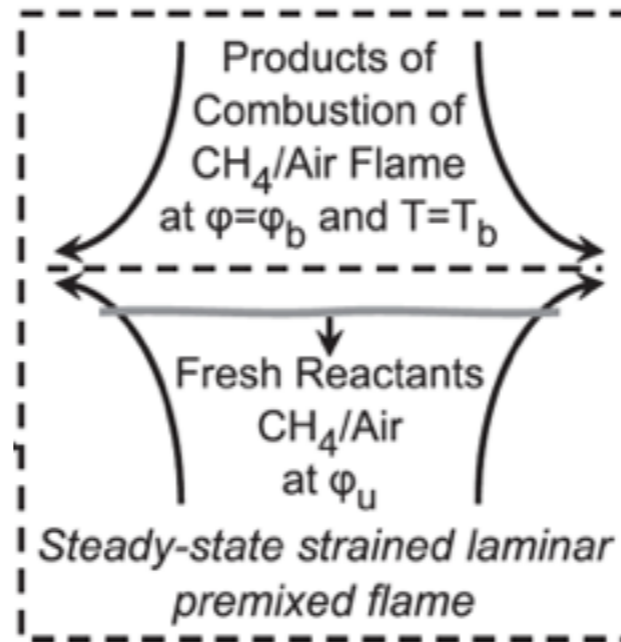
- **1D unstrained model based tabulation**
 - ➔ Overpredicts flame speeds even with heat loss
 - ➔ Combustion pushed towards thin reaction zone
- **Approach: Incorporate strain effects**
 - ➔ Consider opposed premixed flames
- **Strain effects can lead to varying mappings**



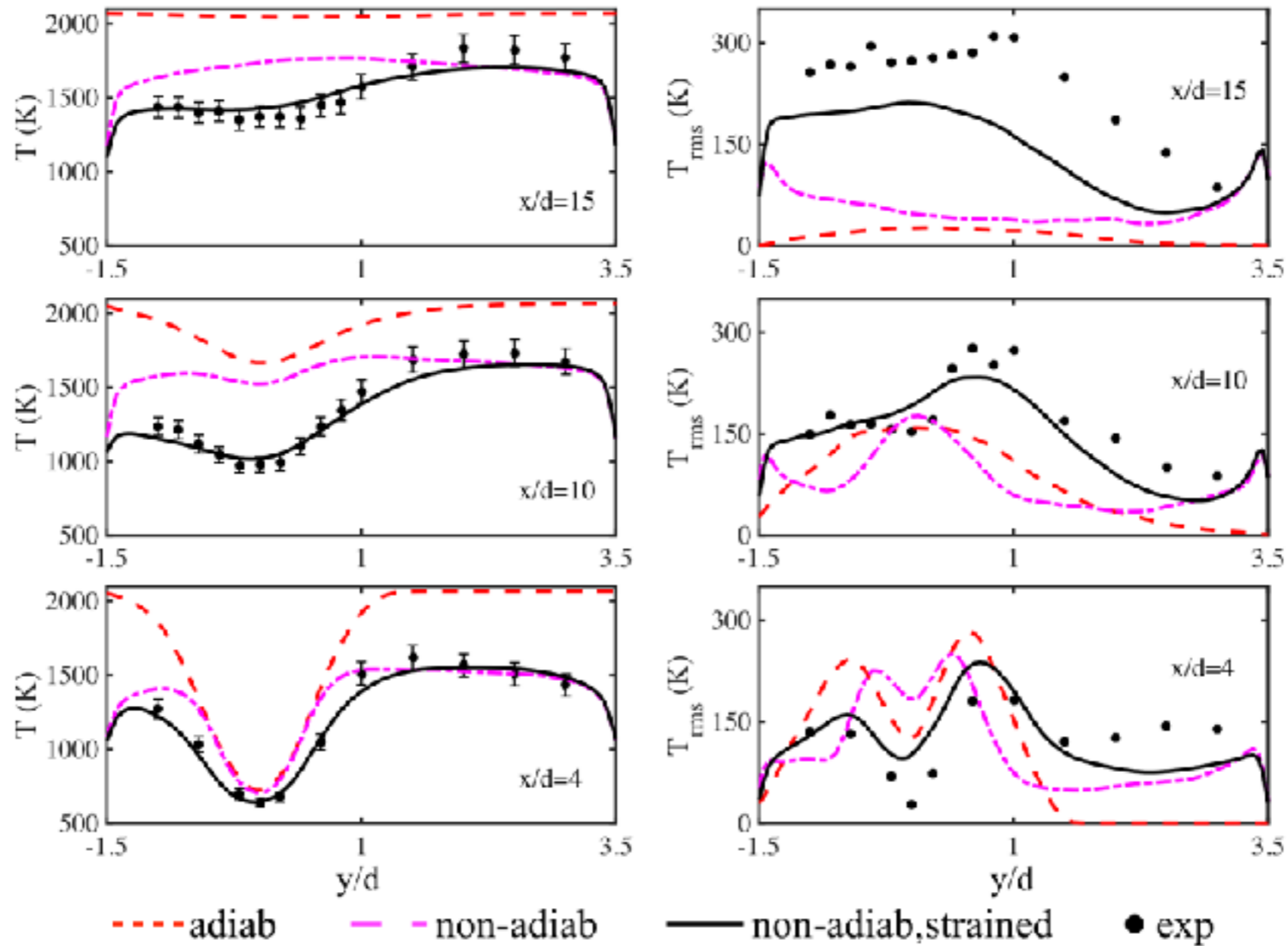
Obtained from B. Coriton, M. Smooke, A. Gomez (2016)

Counterflow Premixed Flame Tabulation

- Flow solution known to have hysteresis effect
- Two control variables
 - ➔ Mass flow (strain)
 - ➔ Product temperature (enthalpy)



Comparisons with Experimental Data



- **New flameout description highly accurate**

➔ Captures temperature profiles throughout combustor

Summary of Findings

- **LES with modified flamelet closures**
 - ➔ Accurately predicts flashback processes
 - ➔ Captures MILD combustion processes
- **Solver plays a key role**
 - ➔ Non-dissipative numerics key to recovering turbulence characteristics
- **Strain rate seen as key parameter for modeling low equivalence ratio MILD combustion devices**
 - ➔ Non-adiabatic formulations necessary where heat loss to walls is important

Products of Research

- **Experimental database on boundary layer flashback**
 - ➔ Variety of fuels, equivalence ratios, pressures
 - ➔ Time-series of velocity and flame front data
- **General purpose LES solver for premixed and stratified flames**
 - ➔ OpenFOAM code base
 - ➔ All solvers available cooperative release
 - Already used by 6 universities and industrial partners
 - Models included in low-Mach number version of solvers
- **4 PhDs (2 still in progress) + several journal articles**