

# **Effects of Exhaust Gas Recirculation (EGR) on Turbulent Combustion Emissions in Advanced Gas Turbine Combustors with High Hydrogen Content (HHC) Fuels**

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## Collaborations

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## PhD students

Dong Han – CARS and PLIF

Hasti Veeraraghava Raju - CFD simulations

Jupyoung Kim – PIV

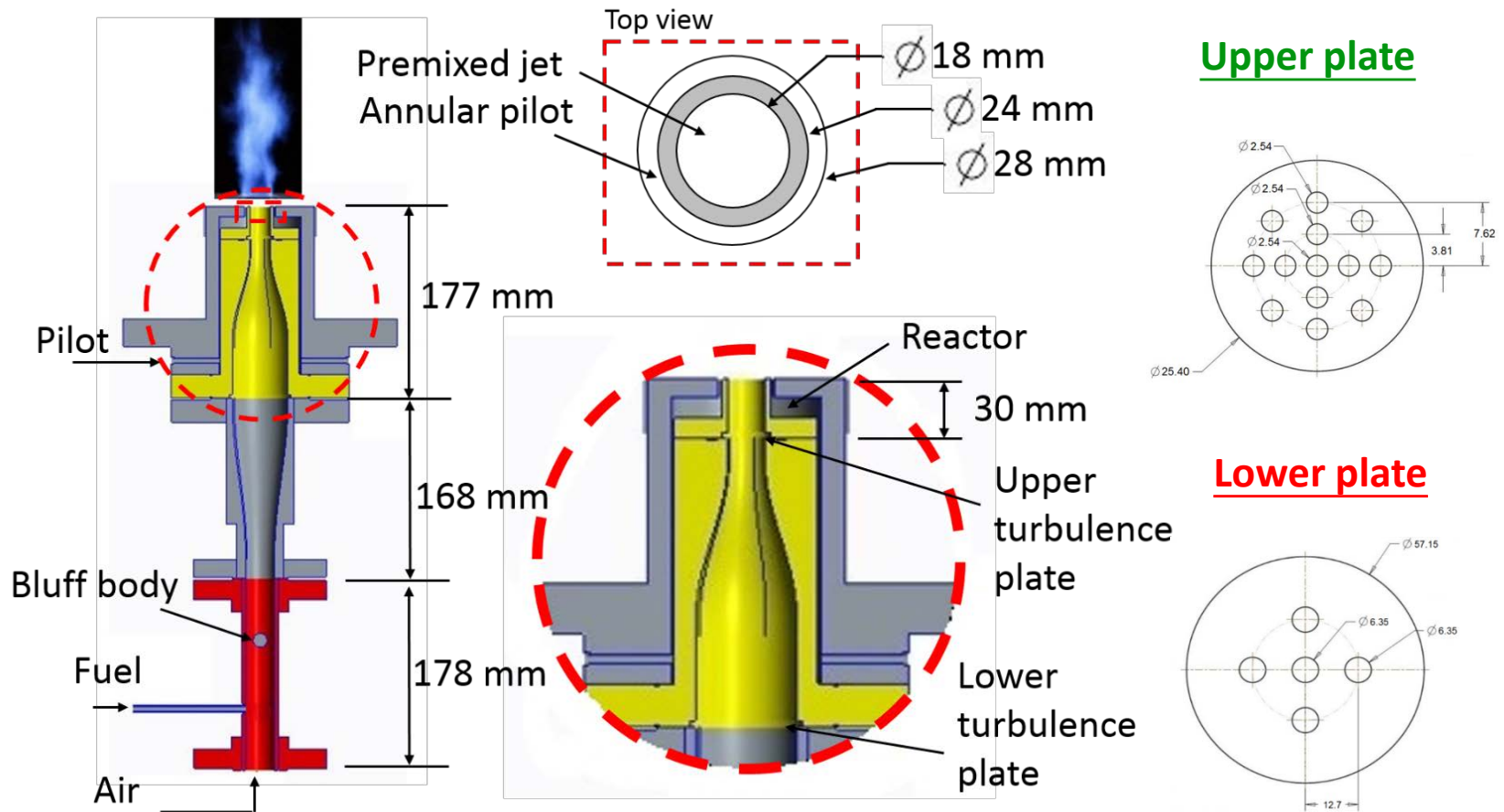
Post Doctoral Associate : Aman Satija

DOE Program Manager: Mark Freeman

# Content

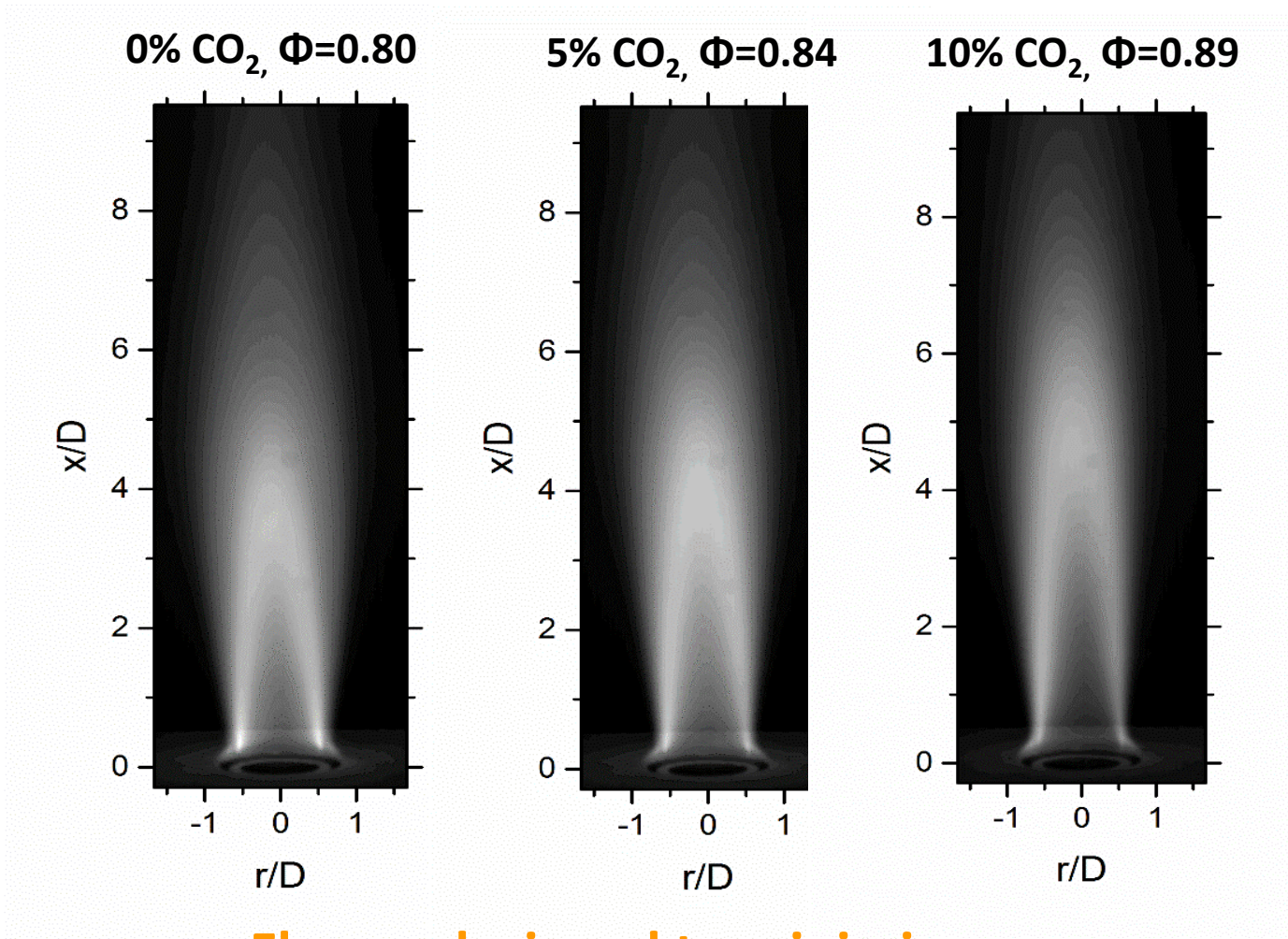
1. **Piloted Axisymmetric Reactor Assisted Turbulent (PARAT) burner development and testing under atmospheric and high-pressure conditions**
2. **Effects of CO<sub>2</sub> addition on turbulent flame structure and burning velocity**
3. **Temperature and velocity measurements in CH<sub>4</sub> /air/CO<sub>2</sub> flames with different levels of CO<sub>2</sub> addition using CARS and PIV**
4. **Development and validation of LES model for H<sub>2</sub> piloted CH<sub>4</sub> /air/CO<sub>2</sub> premixed turbulent flames**
5. **CH PLIF and IR imaging for turbulent premixed flames**

# Experimental Apparatus: PARAT Burner



# Flames with varying levels of CO<sub>2</sub> addition

Re=10,000, T<sub>ad</sub>=2030 K, Le=1, P=1 bar



Flames designed to minimize thermal and transport effects on NO<sub>x</sub>

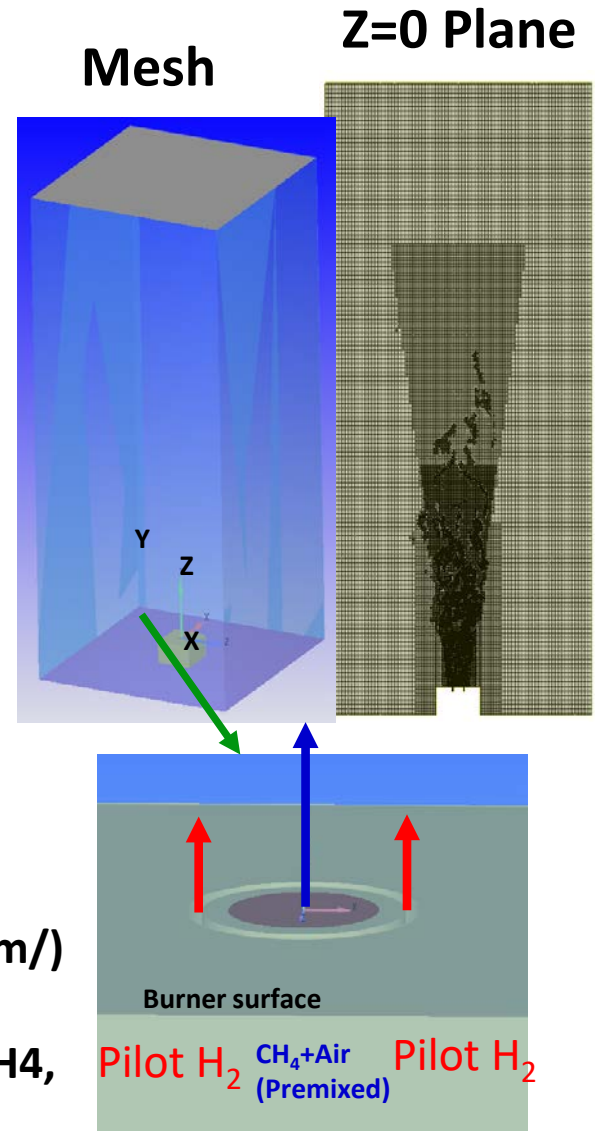
# Large Eddy Reacting Flow Simulations

## CFD Summary

- Premixing tube simulated separately and the solutions patched
- Jet Reynolds number – 10000
- Domain (D= 18 mm): 36D x 64D x 36 D
- Detailed chemistry solver with DRM19 mech. Turbulence – 1 eq. dynamic structure model
- Sensitivity study with base grid : 10 x 8 x 6 mm
- 4 Level Adaptive Mesh Refinement based on Velocity and Temperature, Max. 15 M cells
- Mesh sensitivity studied with Max. 30 M cells

## Chemistry

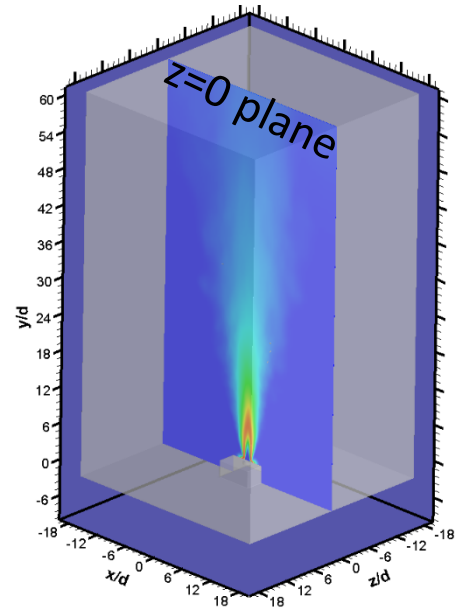
- DRM19 Mechanism: (<http://combustion.berkeley.edu/drm/>)
- Elements : O, H, C, N, AR
- Species: H<sub>2</sub>, H, O, O<sub>2</sub>, OH, H<sub>2</sub>O, HO<sub>2</sub>, CH<sub>2</sub>, CH<sub>2</sub>(S), CH<sub>3</sub>, CH<sub>4</sub>, CO, CO<sub>2</sub>, HCO, CH<sub>2</sub>O, CH<sub>3</sub>O, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>5</sub>, C<sub>2</sub>H<sub>6</sub>, N<sub>2</sub>, AR
- Number of Reactions: 84



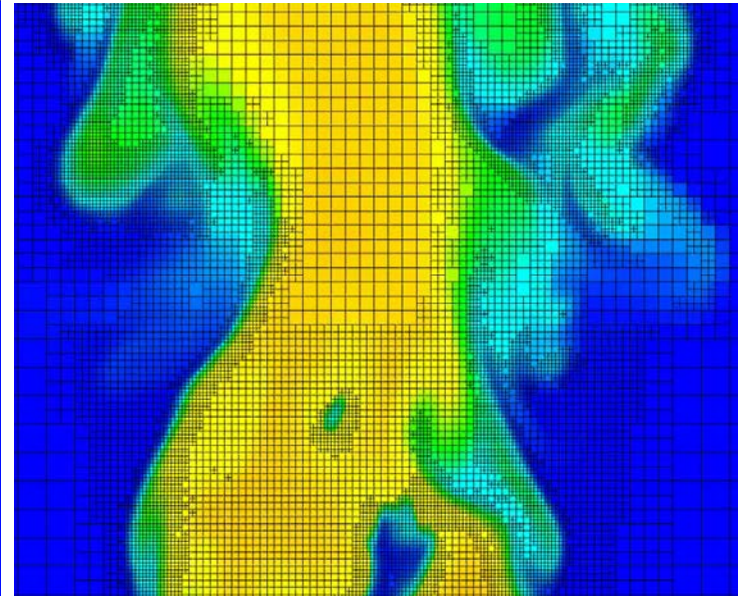
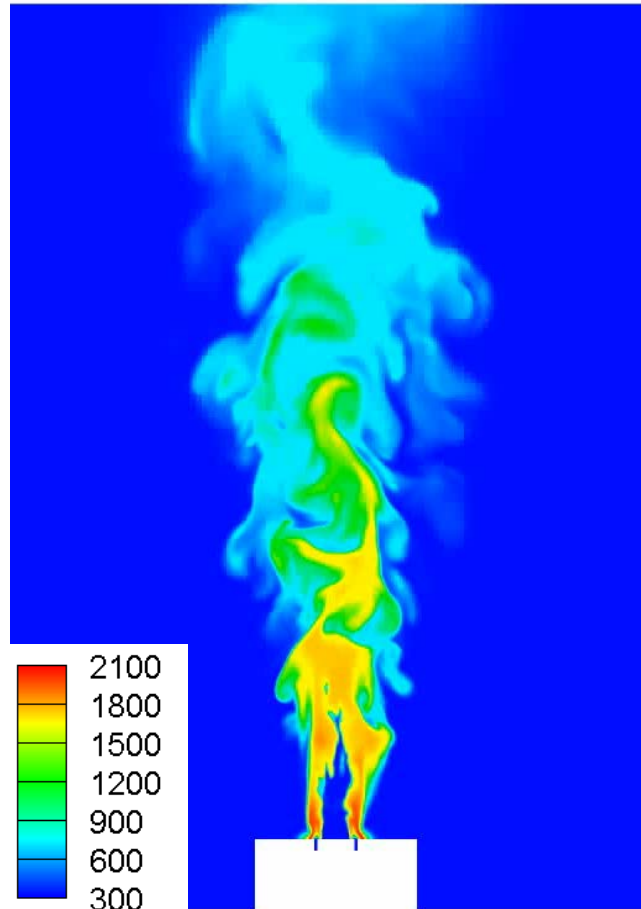
# Large Eddy Simulations

Instantaneous Temperature [K]

Computational Grid

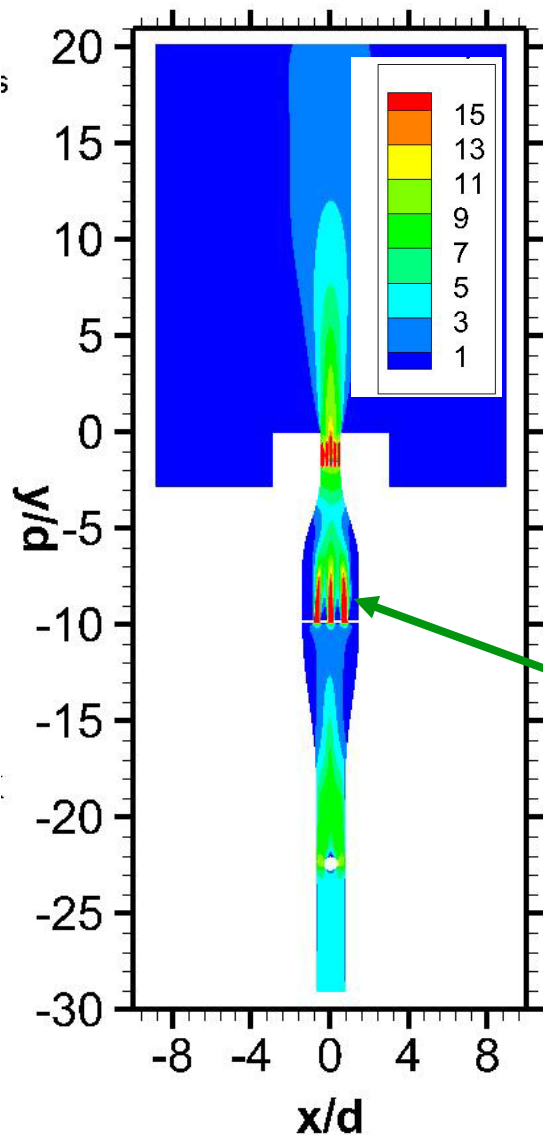


Mean Temperature [K]

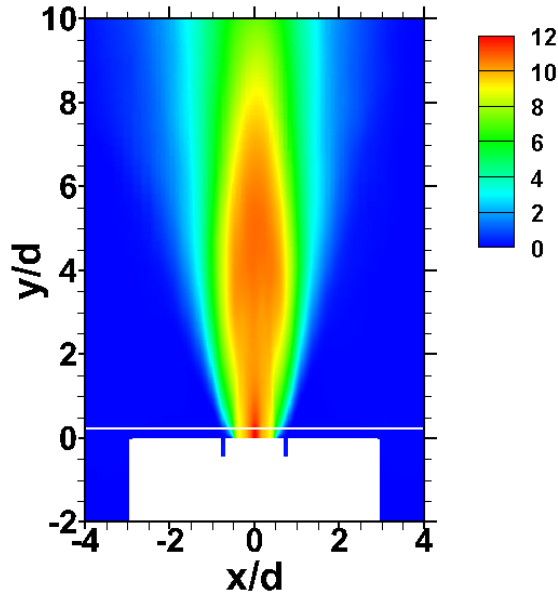


Region:  $5 < y/d < 6$

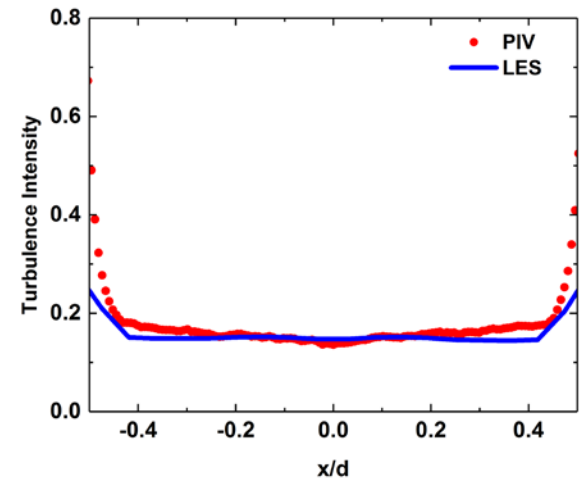
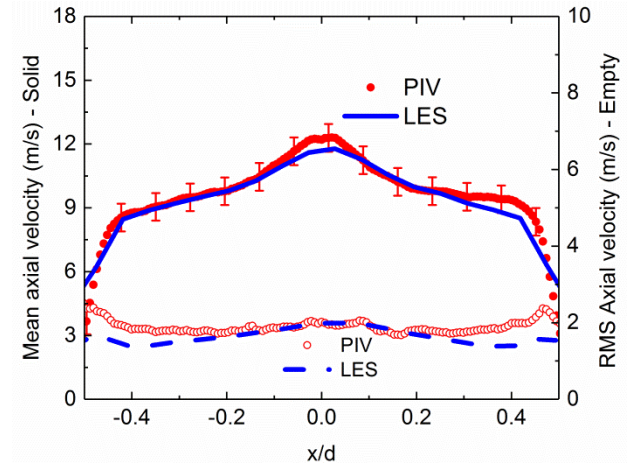
# Inlet Boundary Conditions LES Comparison with Experiments



Flame 1 velocity contour



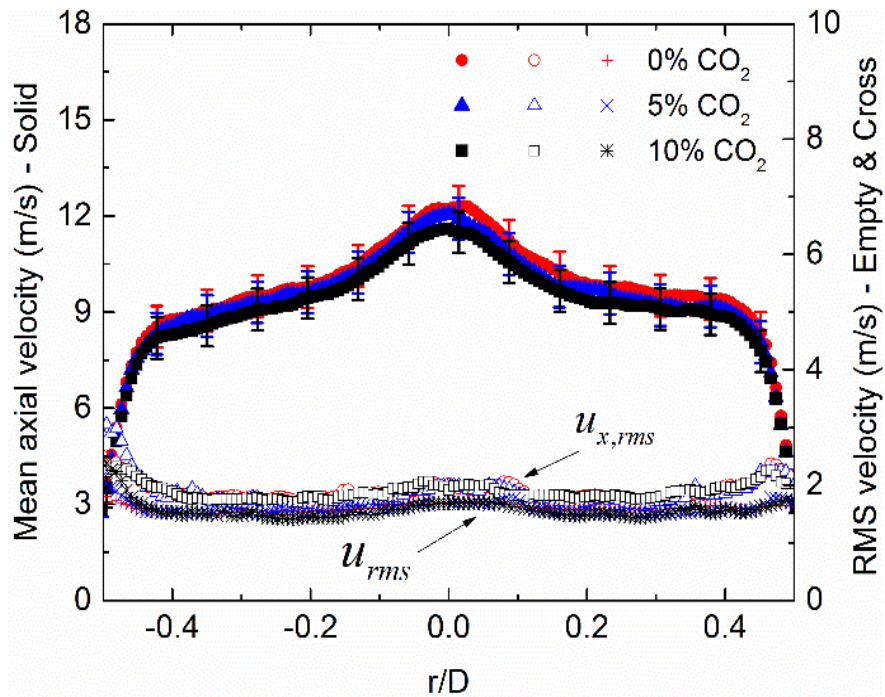
Non reacting flow simulation for jet velocity profiles at the burner exit



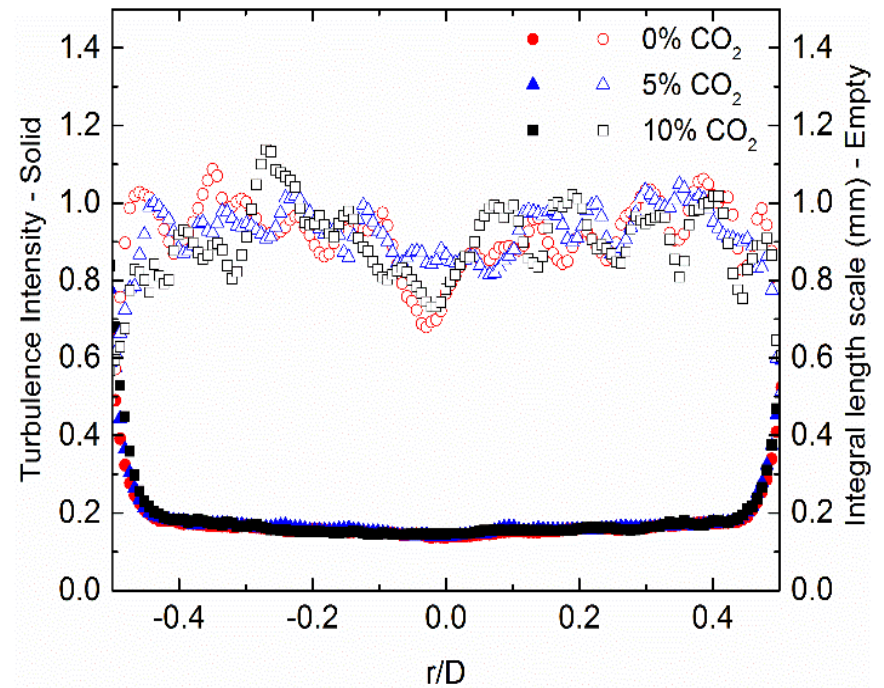


# Boundary Condition & Turbulence Intensity at $x/D=0.2$

## Mean & RMS velocity profiles



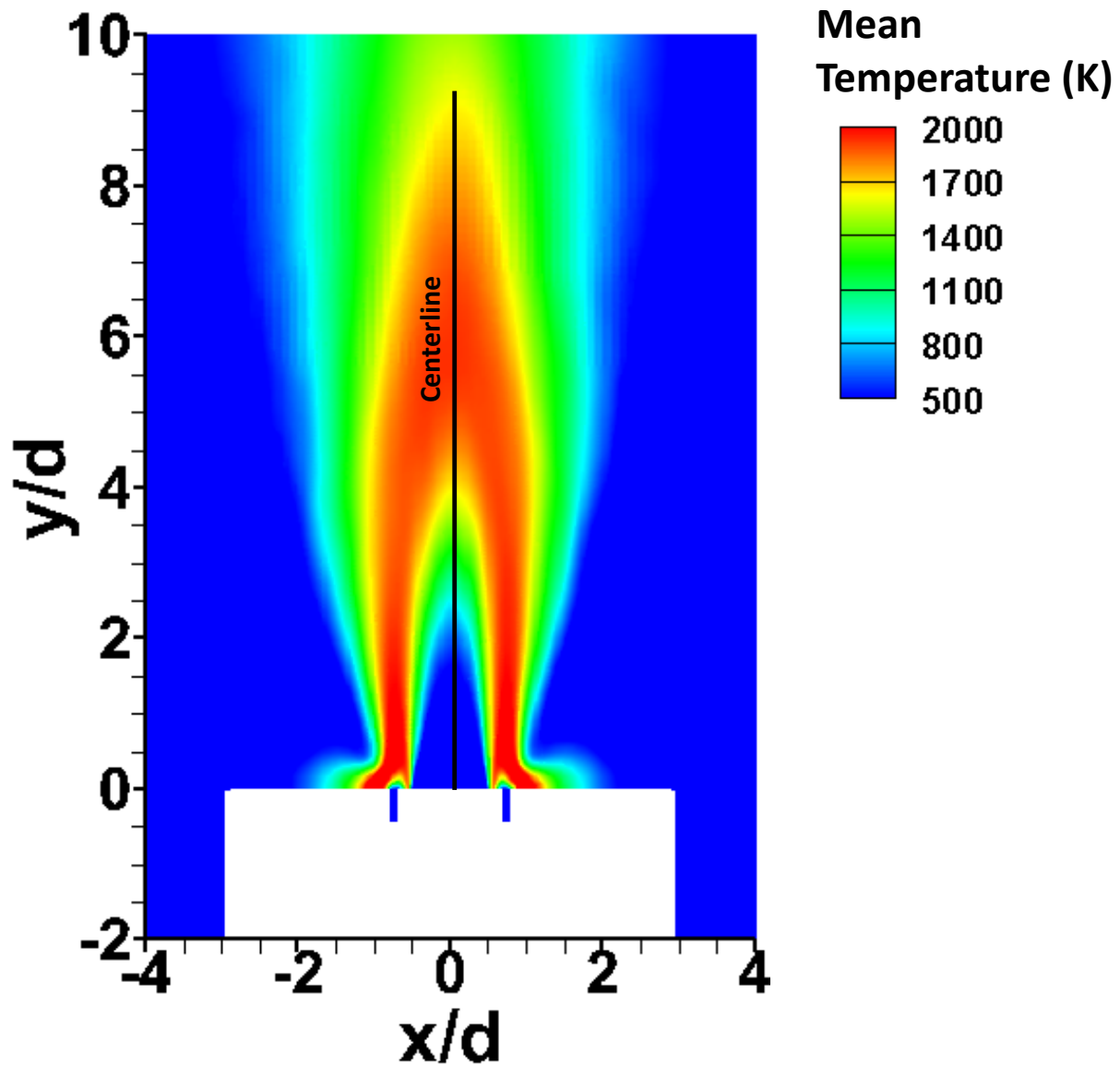
## Integral length scale & turbulence intensity



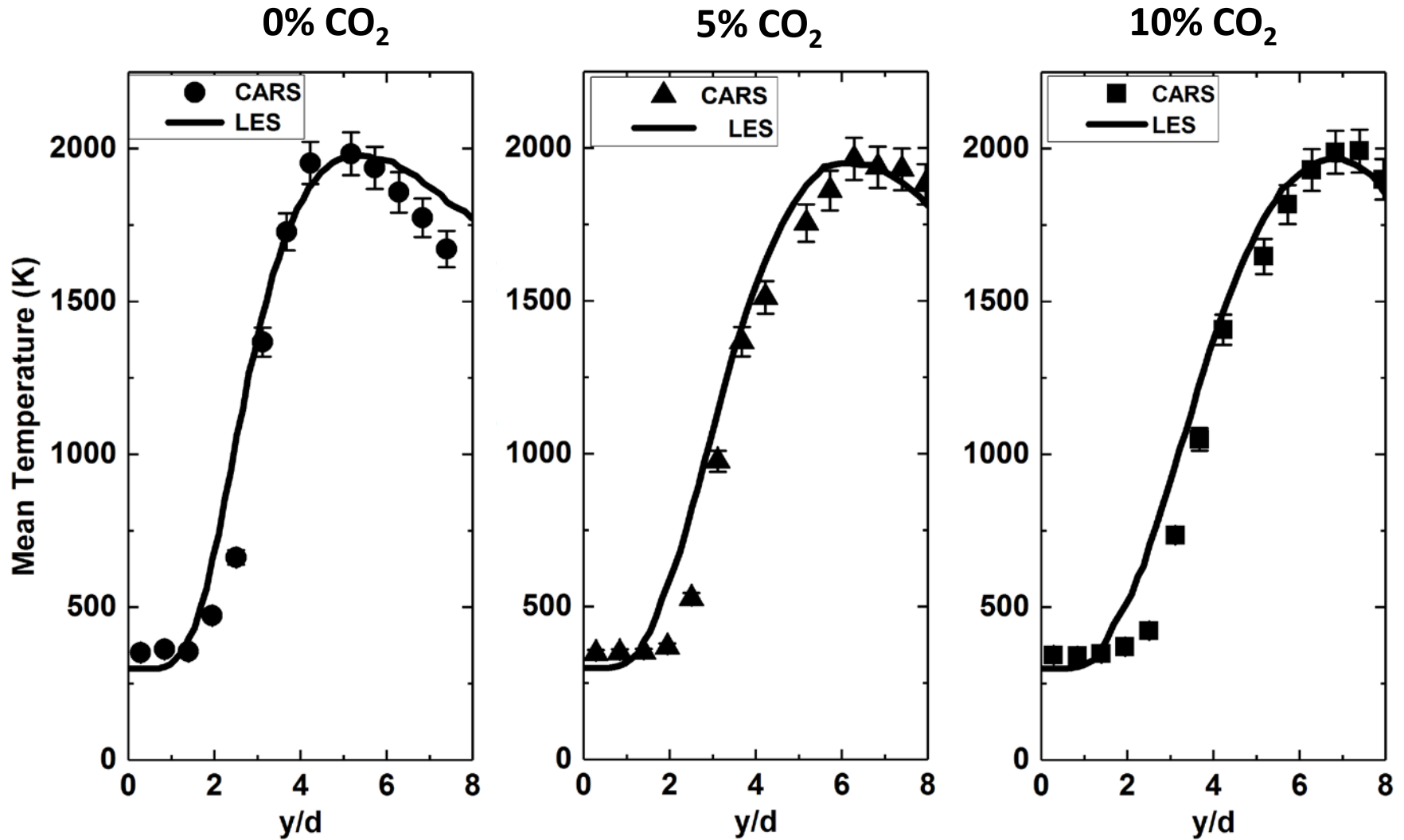
## Integral length scale

$$l(r) = \int_0^{\infty} \rho(r, r^*) dr^* \quad \rho(r, \Delta r) = \frac{\overline{u'_x(r)u'_x(r + \Delta r)}}{u'^2_x(r)}; \Delta r = |r - r^*| \quad T.I. = \frac{u_{rms}}{u_{mean}}$$

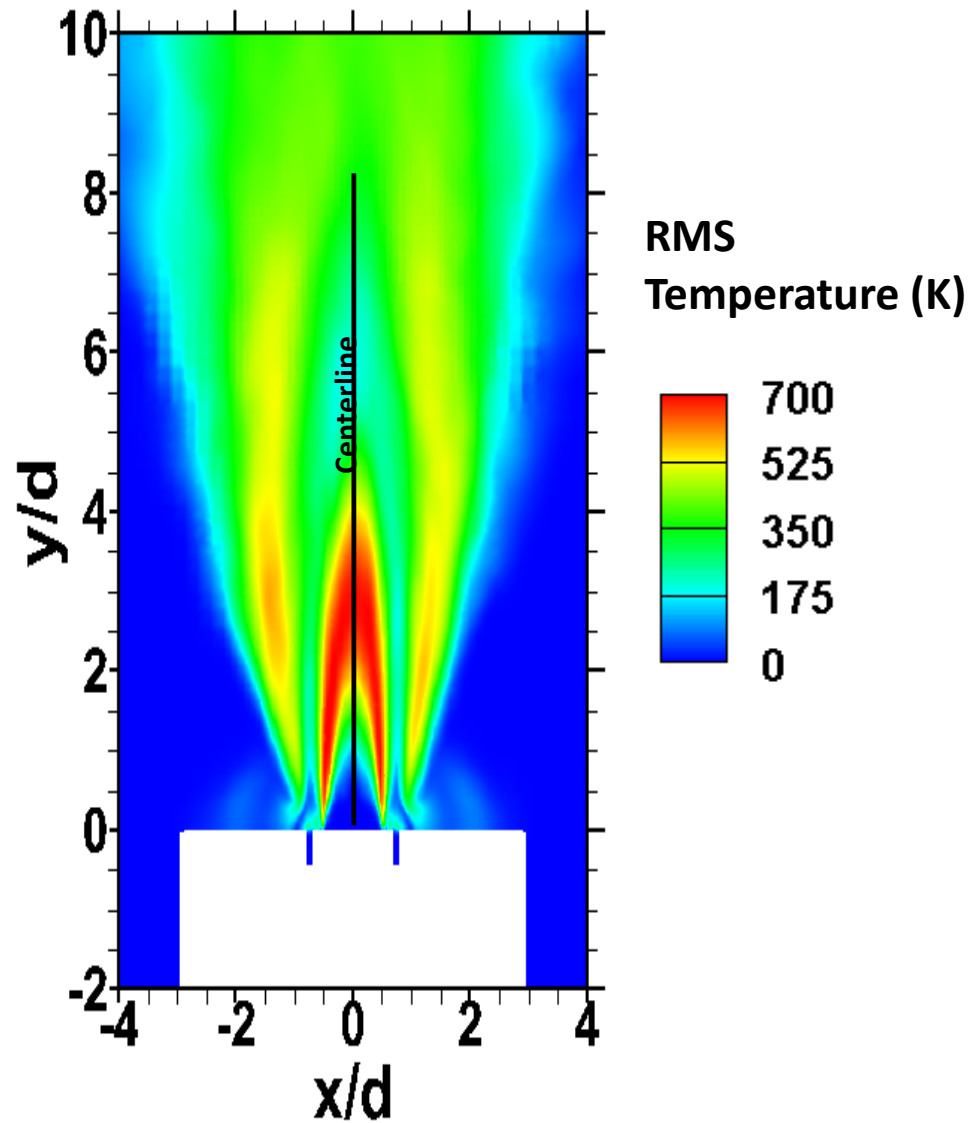
# LES Mean Temperature Contours on Z=0 Plane



# Axial Temperature Profiles with CO<sub>2</sub> Addition

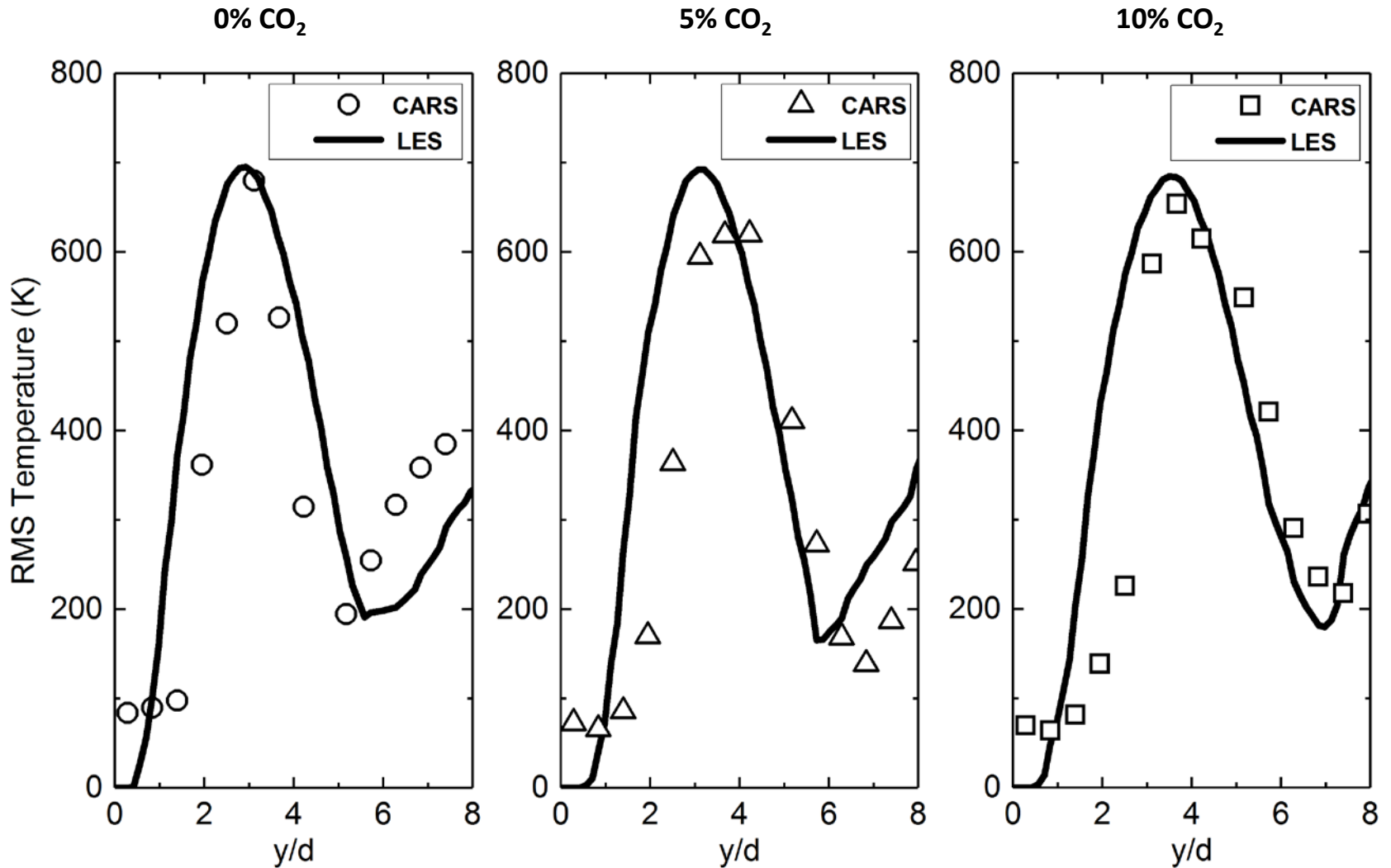


# LES RMS Temperature on Z=0 plane

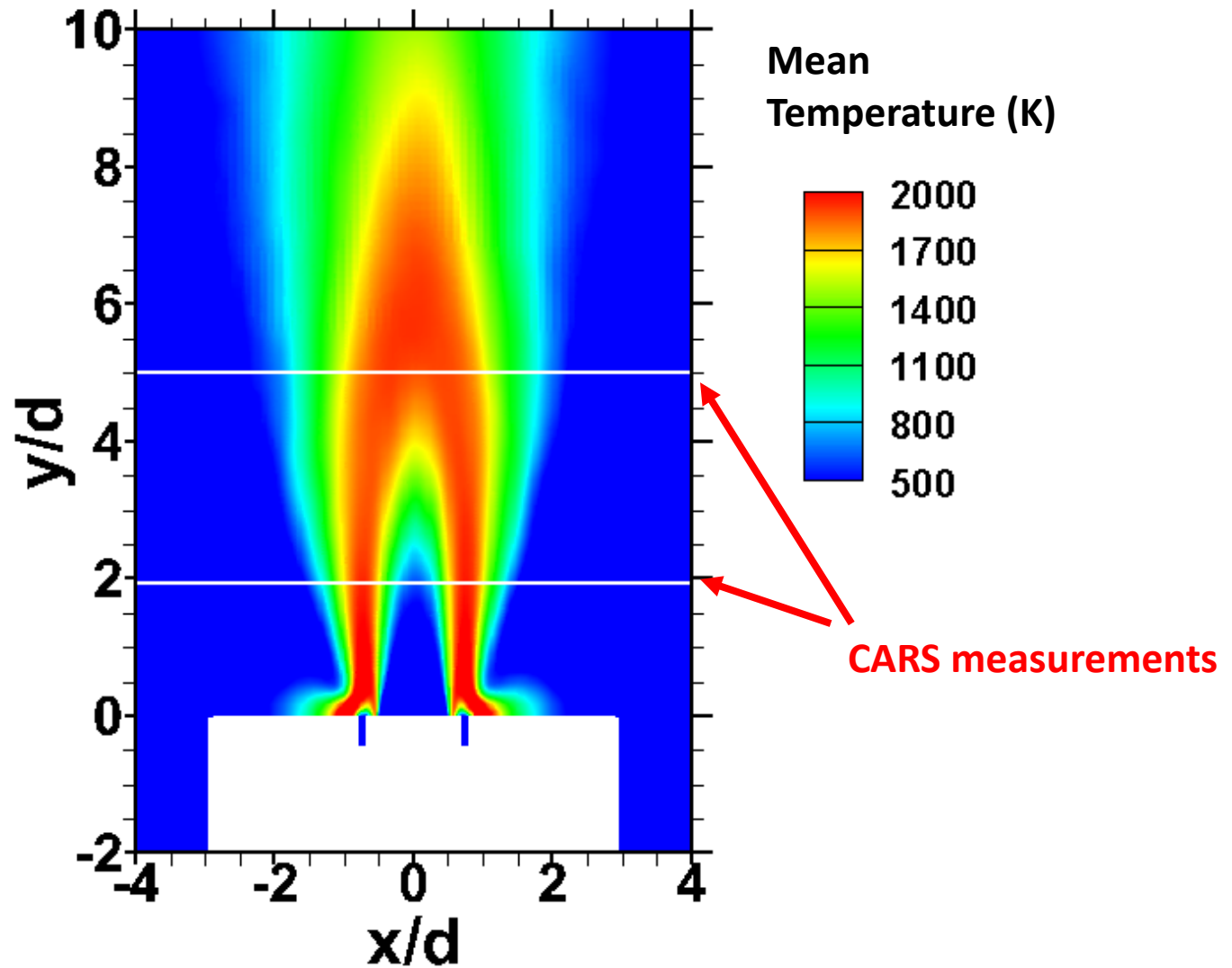


# T RMS comparison between CARS and LES

Centerline RMS temperature



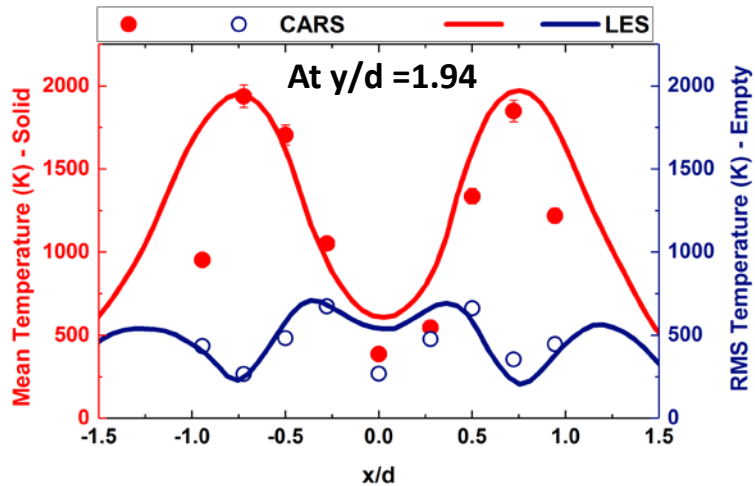
# Temperature comparison between CARS and LES



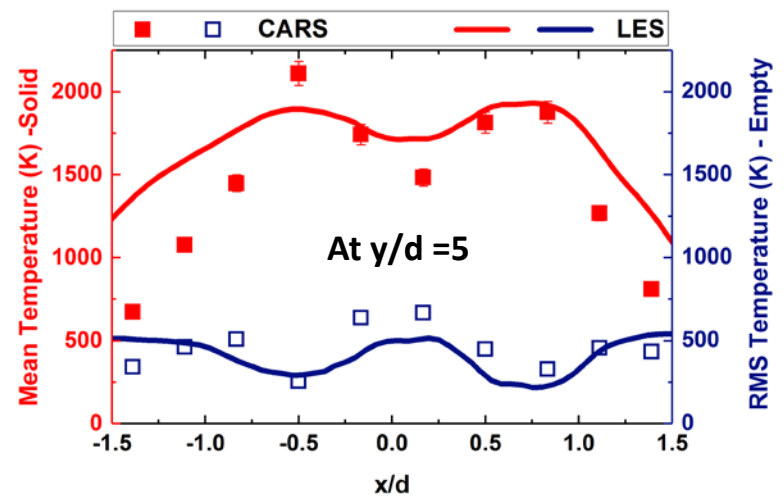
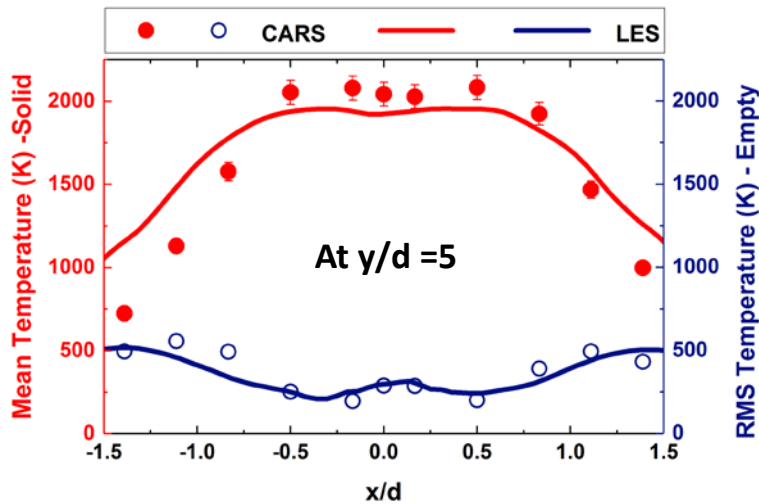
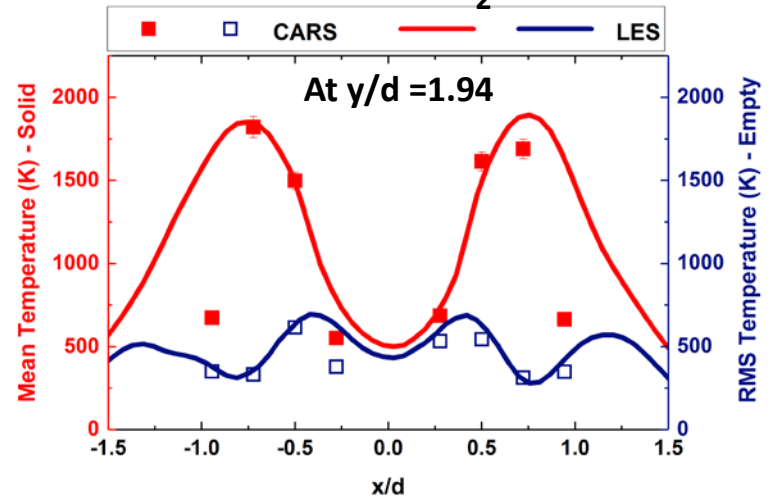
# Temperature comparison between CARS and LES

Radial mean and RMS temperature

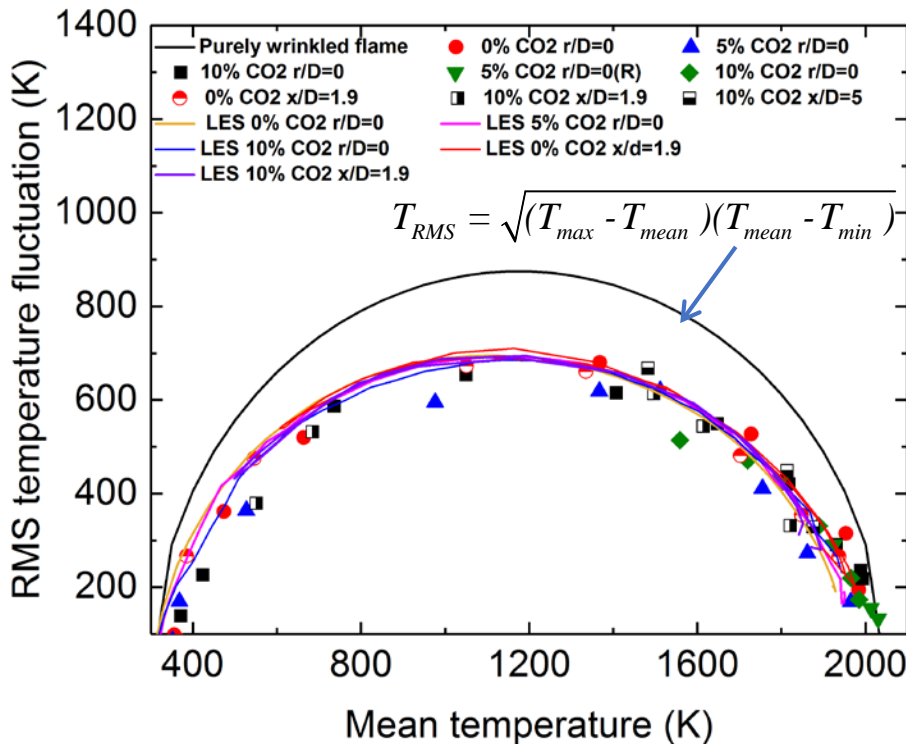
0% CO<sub>2</sub>



10% CO<sub>2</sub>



# Thin or Purely Wrinkled Flame Assumption is not adequate!



$$\lambda = \frac{D_u}{S_L^0} \quad \eta = \left( \frac{v^3}{\varepsilon} \right)^{1/4}$$

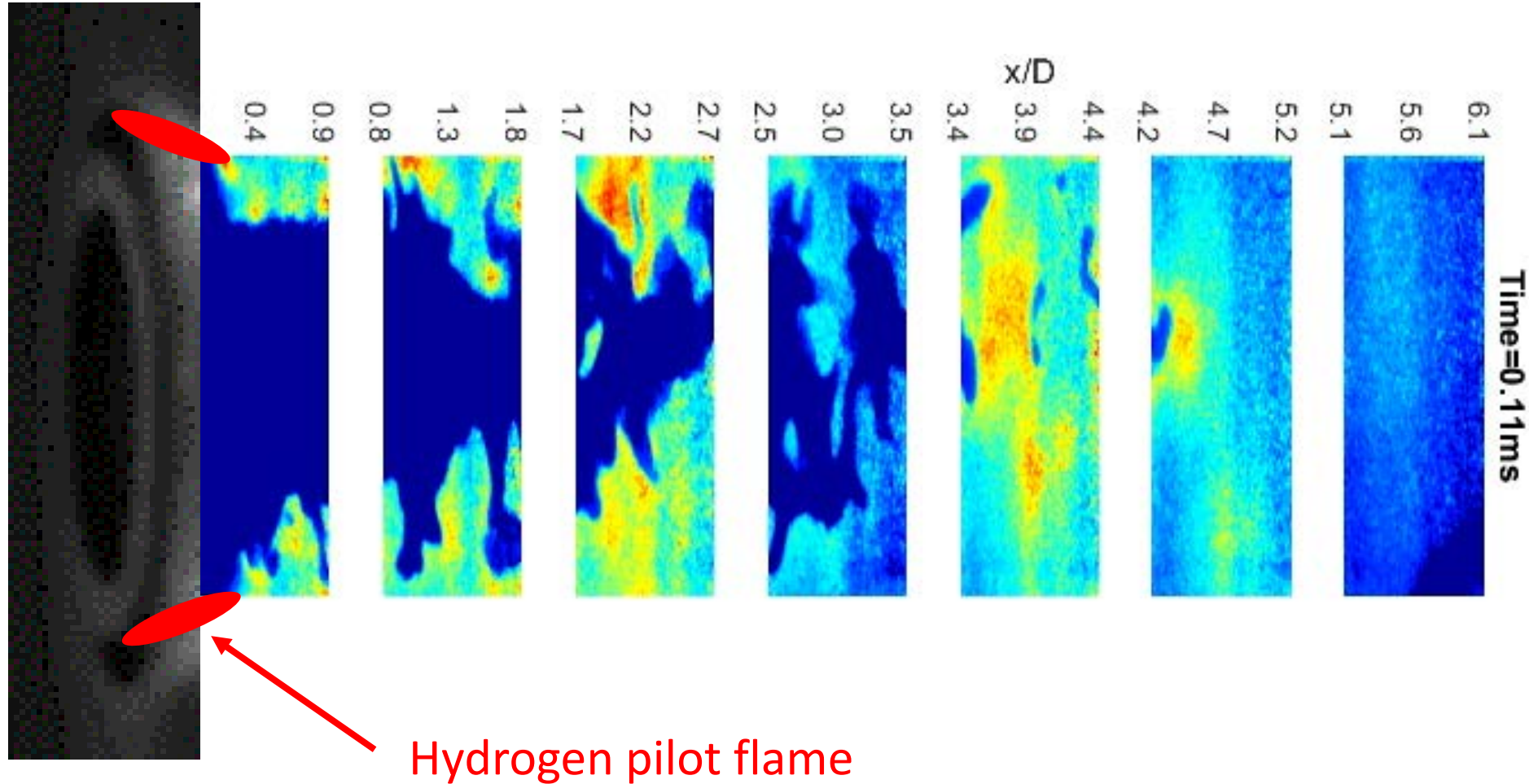
CO <sub>2</sub> levels	Characteristic flame thickness, $\lambda$ ( $\mu\text{m}$ )	Kolmogorov length scale $\eta$ , ( $\mu\text{m}$ )
0%	70	50
5%	80	52
10%	90	55

**Effect of CO<sub>2</sub> on the chemistry of turbulent flames with EGR are captured in the present computations!**



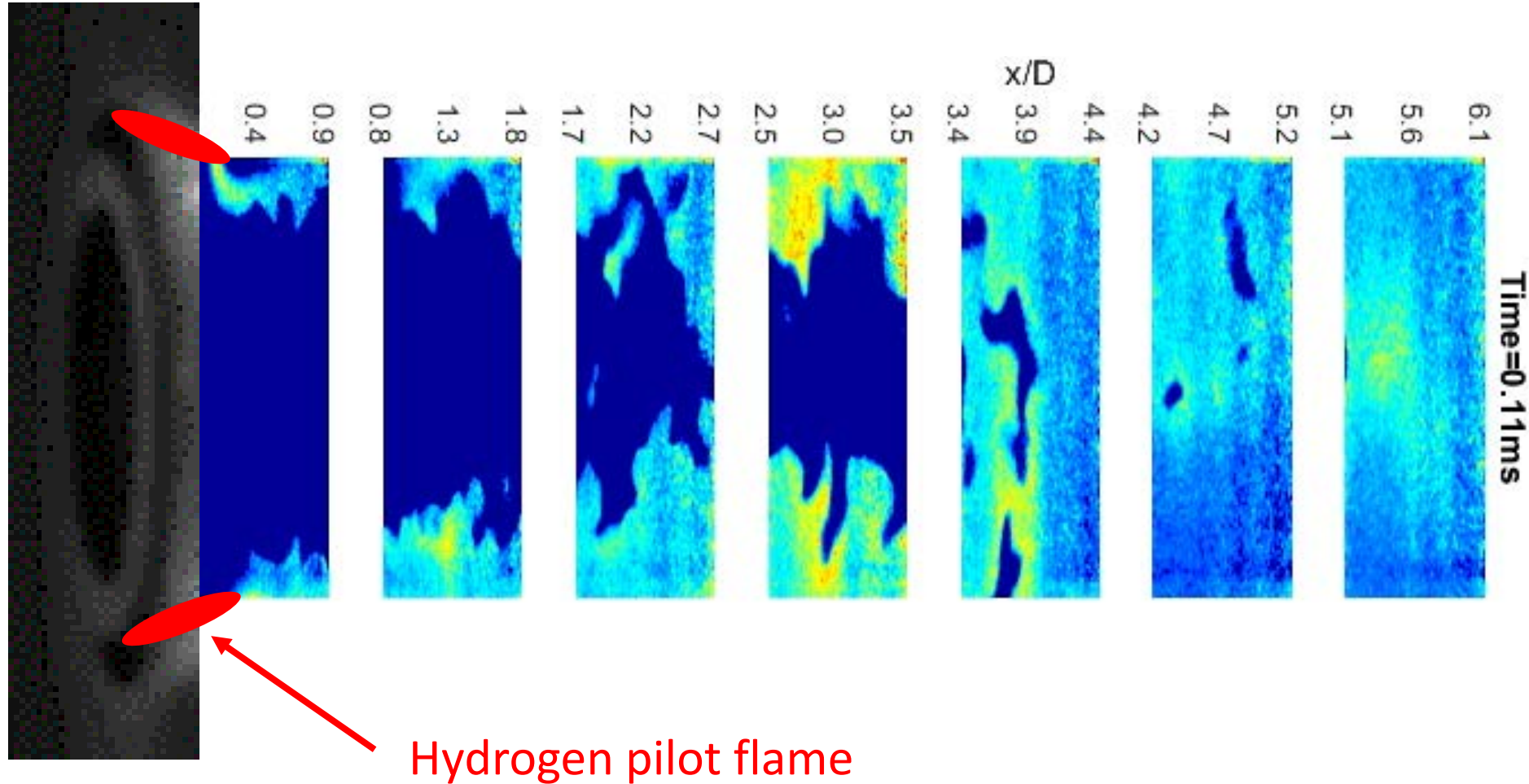
# OH PLIF video for flame with 0% CO<sub>2</sub> addition

$\Phi=0.8$ ,  $Re=10000$



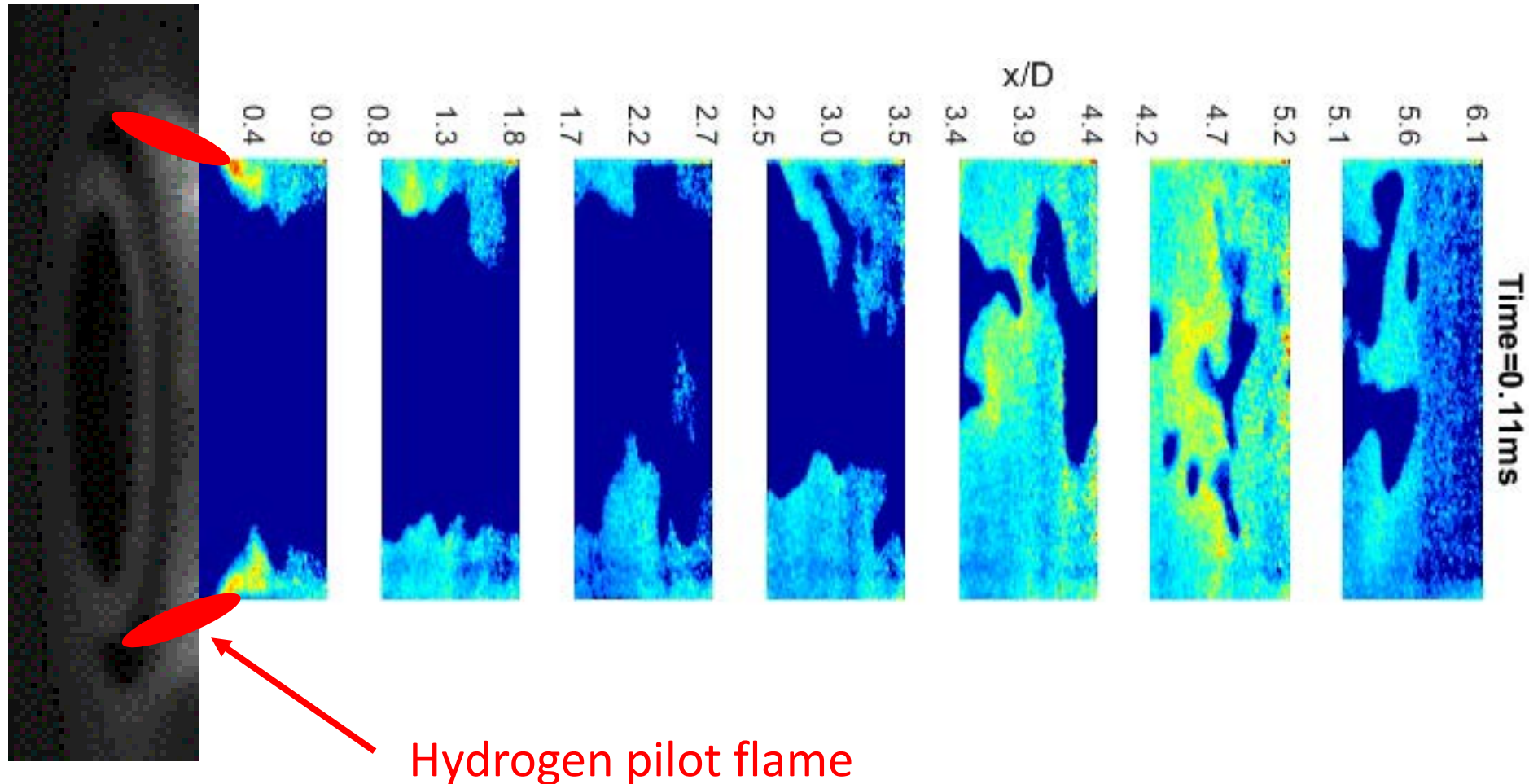
# OH PLIF video for flame with 5% CO<sub>2</sub> addition

$\Phi=0.84$ ,  $Re=10000$

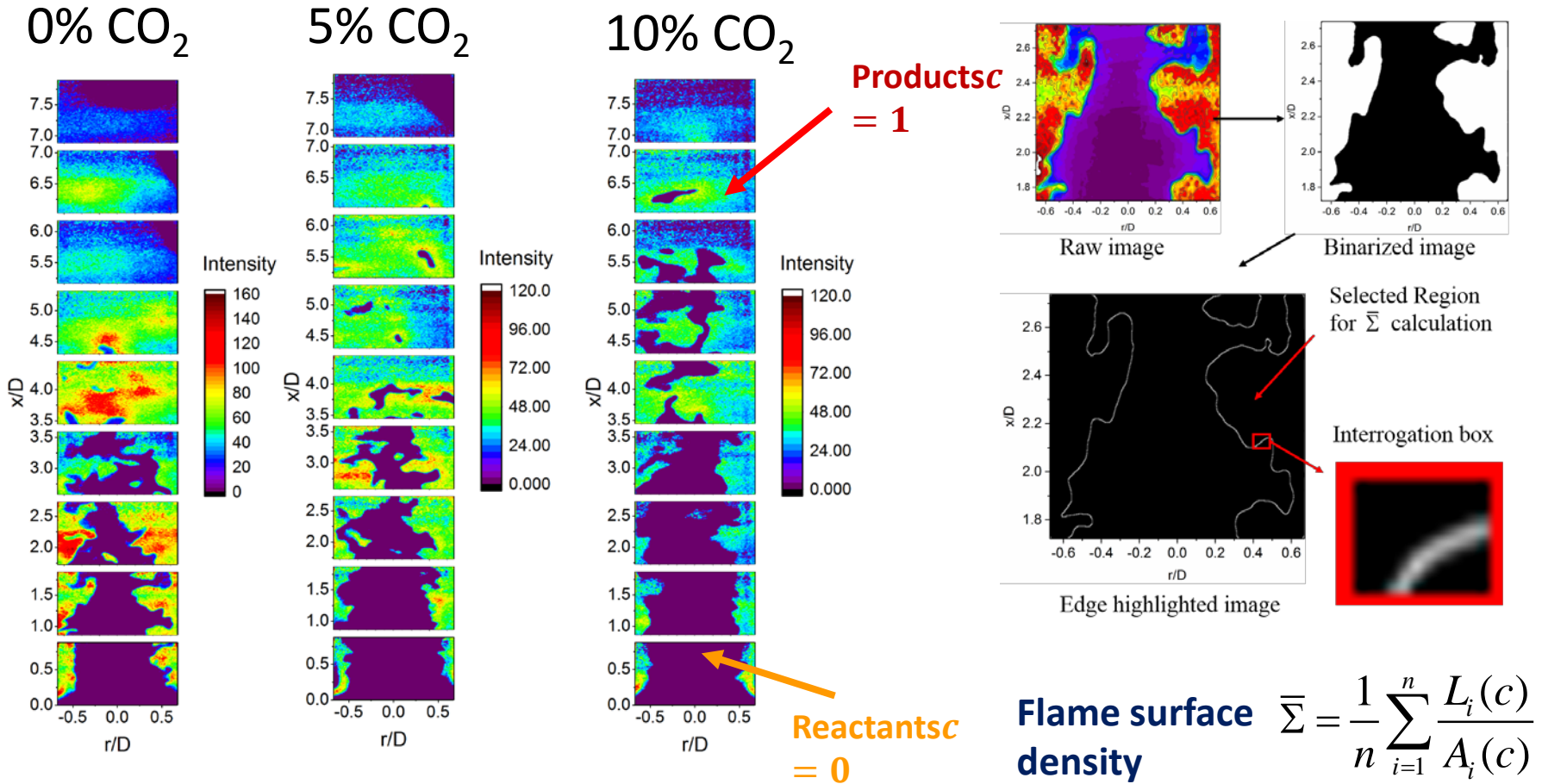


# OH PLIF video for flame with 10% CO<sub>2</sub> addition

$\Phi=0.89$ ,  $Re=10000$



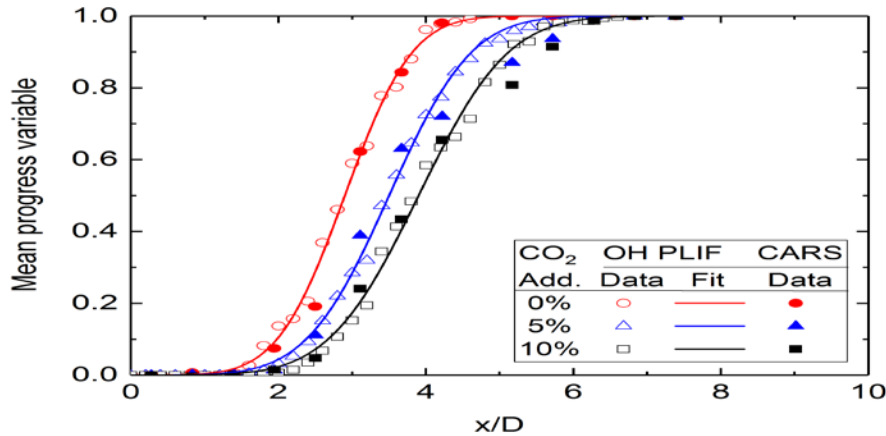
# OH PLIF Images & Data Processing



# Mean Reaction Progress

**Axial direction**

**Flame brush development & Taylor's theory**



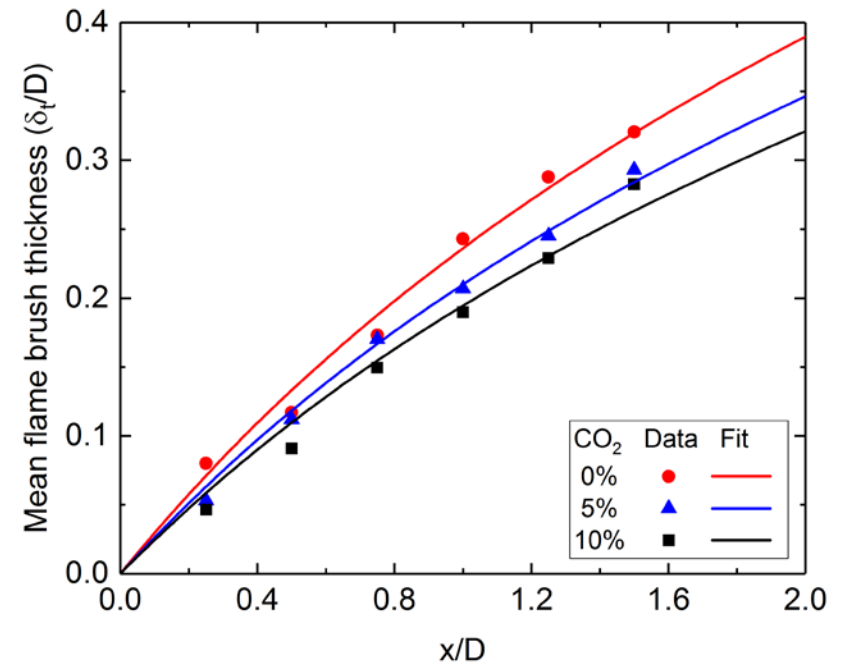
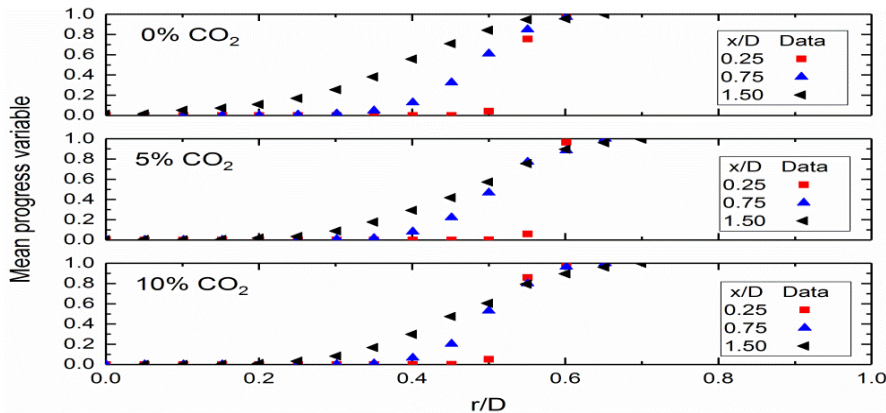
**Data**

$$\delta_{T,r} = \max^{-1} \left( \frac{d\bar{c}}{dr} \right)$$

**Fit**

$$\delta_{T,r} = \alpha (2u'l\tau)^{1/2} \left\{ 1 - \frac{l}{u'\tau} \left[ 1 - \exp\left(-\frac{\tau u'}{l}\right) \right] \right\}^{1/2}$$

**Radial direction**



**Mean progress variable**

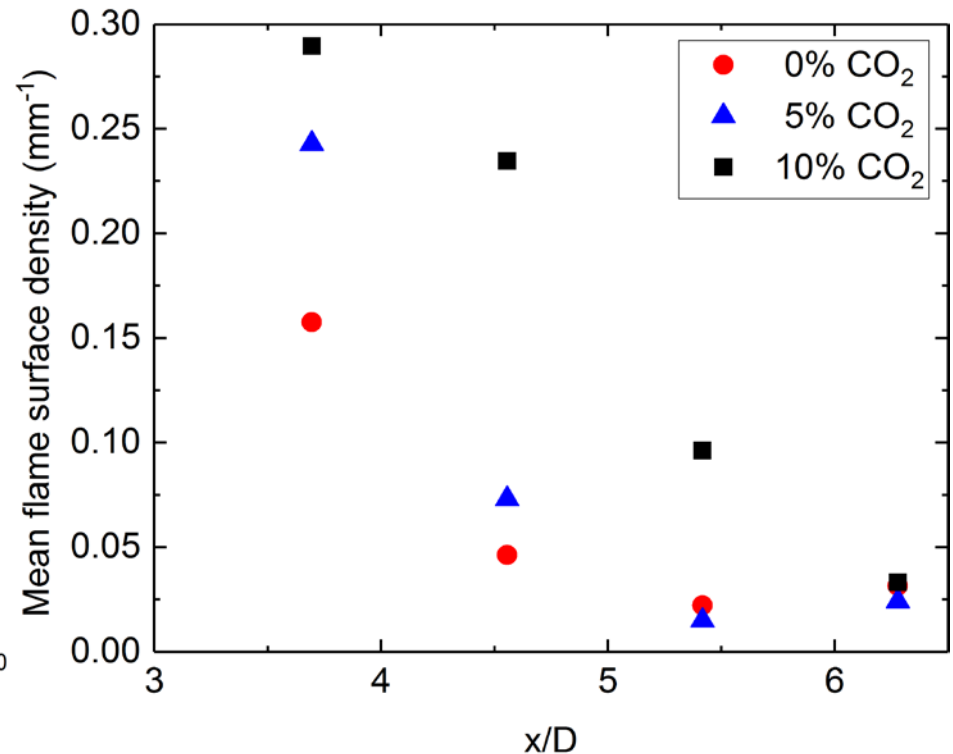
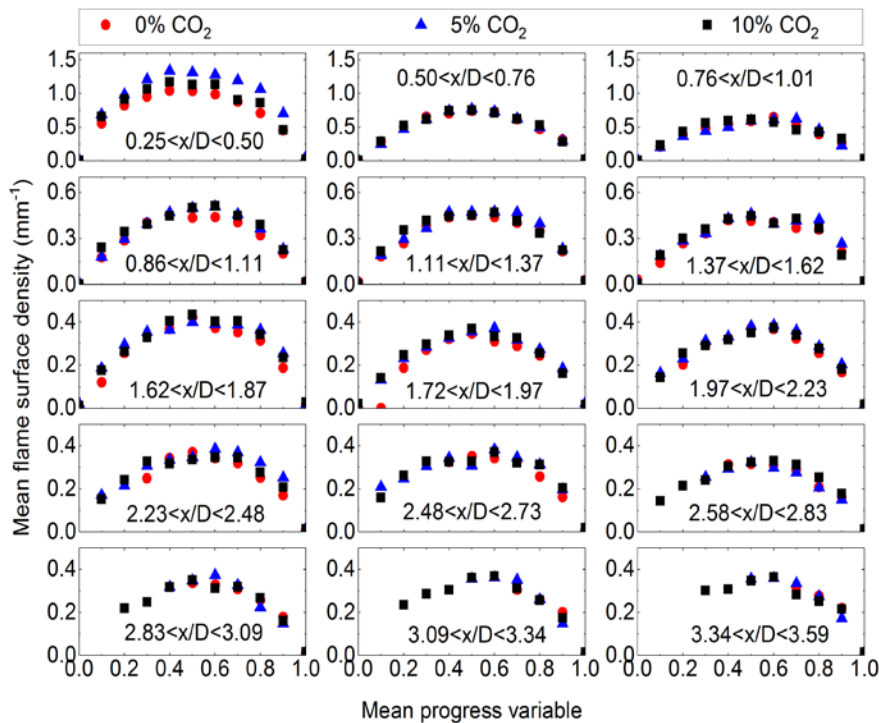
$$\bar{c}(x,r) = \frac{1}{n} \sum_{i=1}^n c_i(x,r)$$

# Flame Surface Density

Radial flame brush development   Axial flame brush development

$0 < x/D < 3.6$

$3.6 < x/D < 6.5$

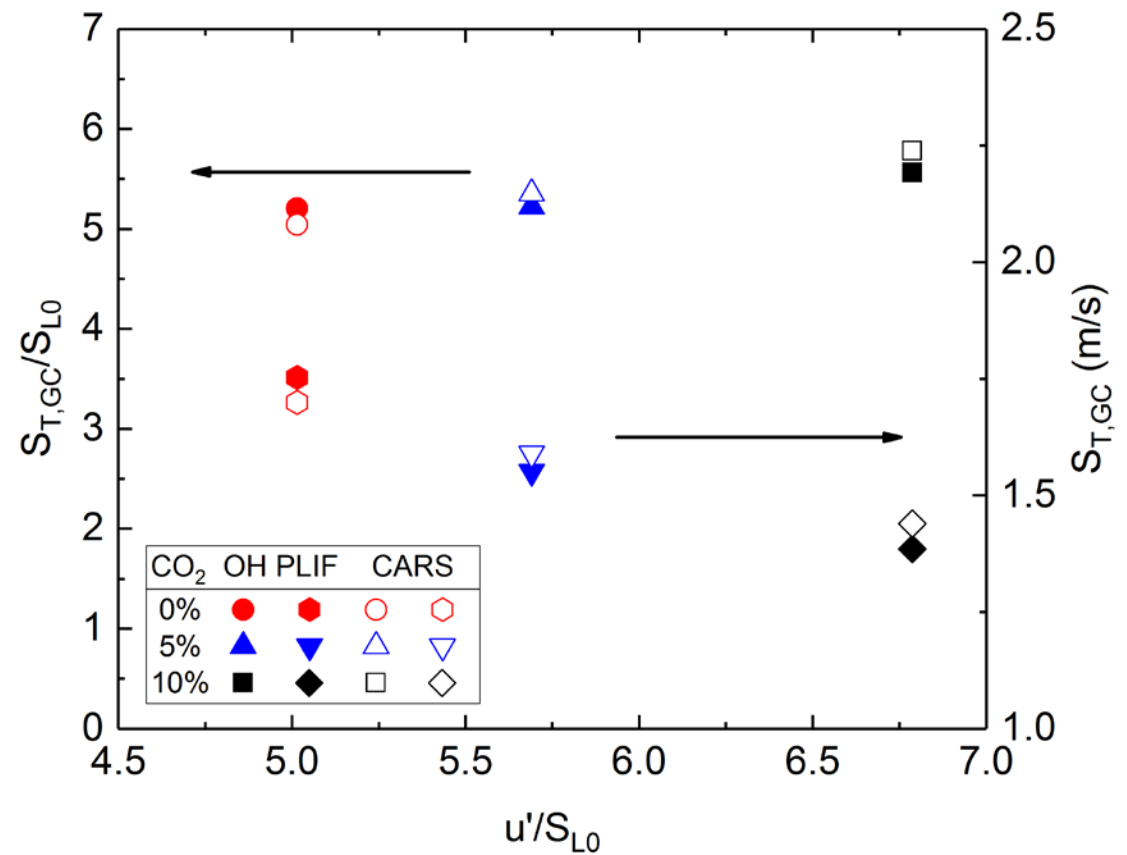
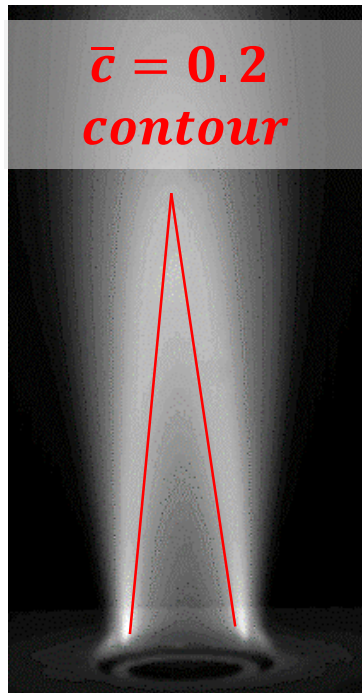


Mean flame surface density

$$\bar{\Sigma} = \frac{1}{n} \sum_{i=1}^n \frac{L_i(c)}{A_i(c)}$$

# Global Consumption Speed

$$S_{T,GC} = \sqrt{\frac{U^2}{1 + [2x(\bar{c} = 0.2) / D]^2}}$$



# Local Consumption Speed

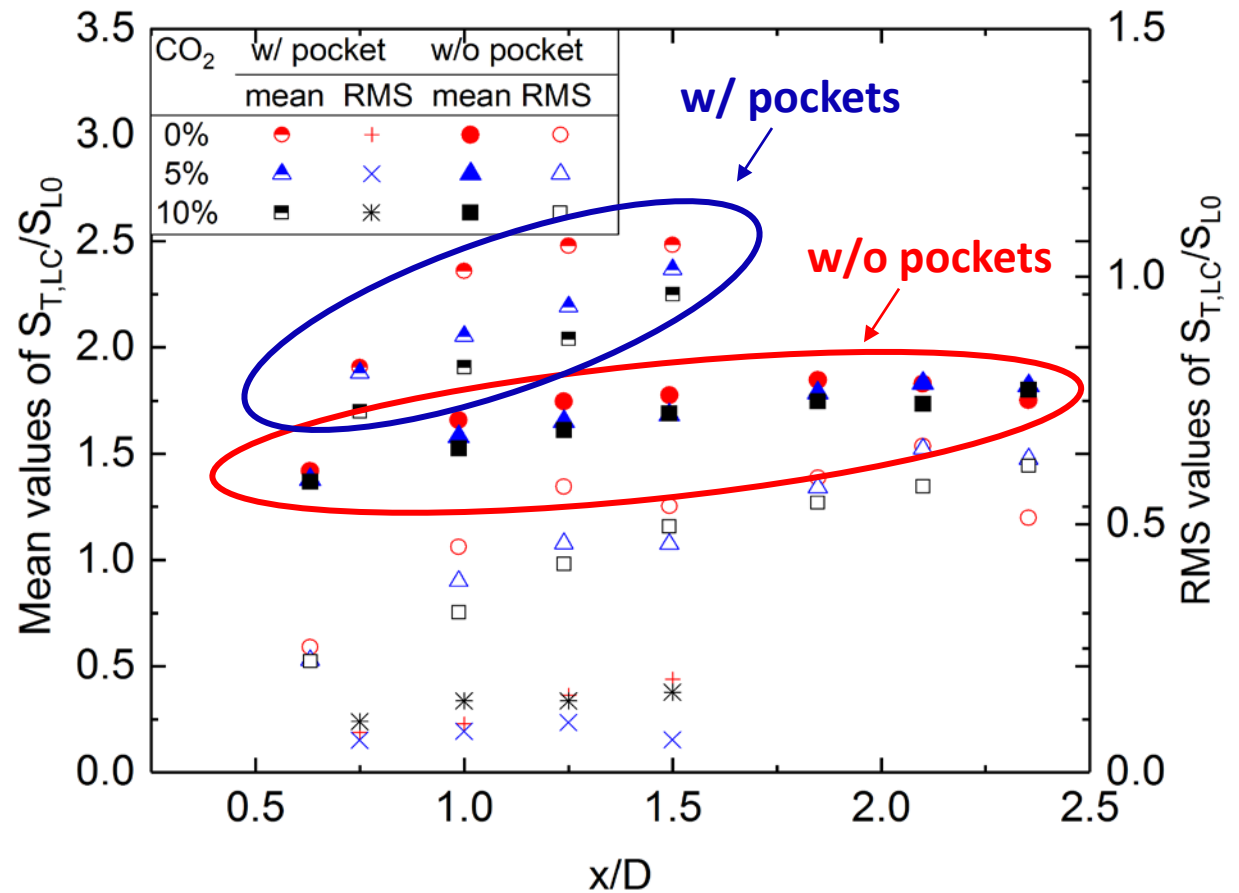
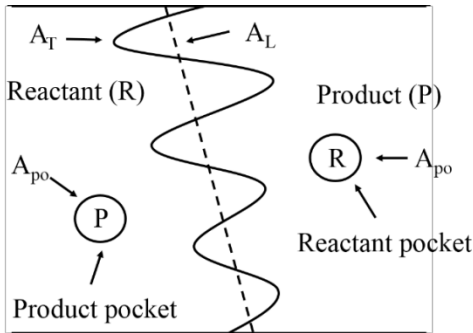
- w/o pockets

$$S_{T,LC} = S_{L0} I_0 \frac{A_T}{A_L}$$

- w/ pockets

$$S_{T,LC} = S_{L0} I_0 \sum_{\max} \delta_T$$

- pockets



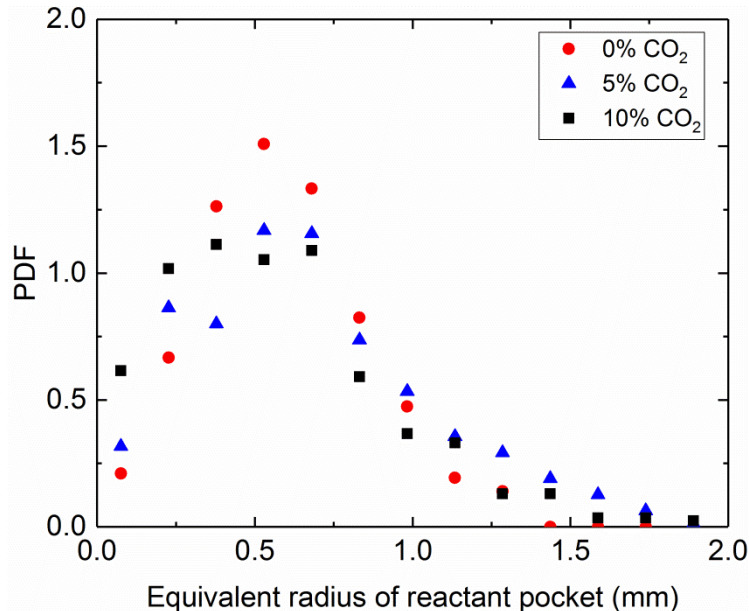


# Fine-scale Unburned Pocket Consumption

Fine-scale pocket size

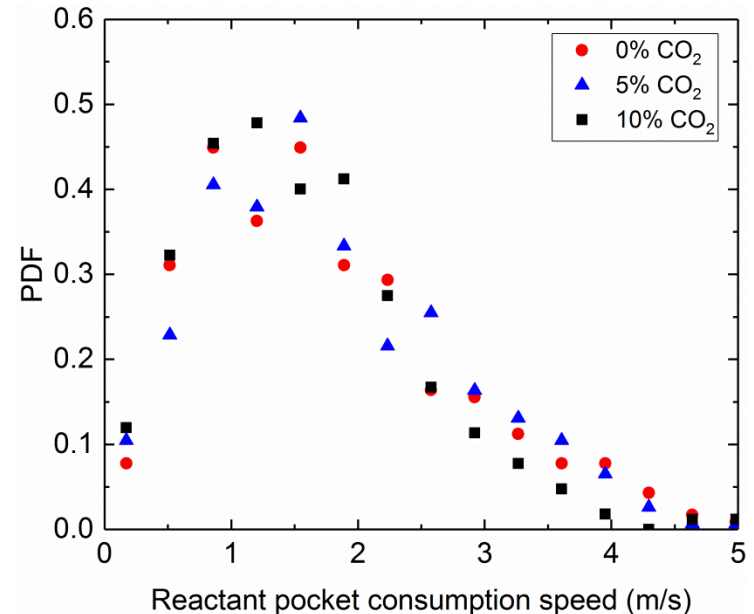
$$R_e = \sqrt{\frac{A_{up}}{\pi}}$$

$A_{up}$  Unburned pocket area  
 $\Delta t$  Time step



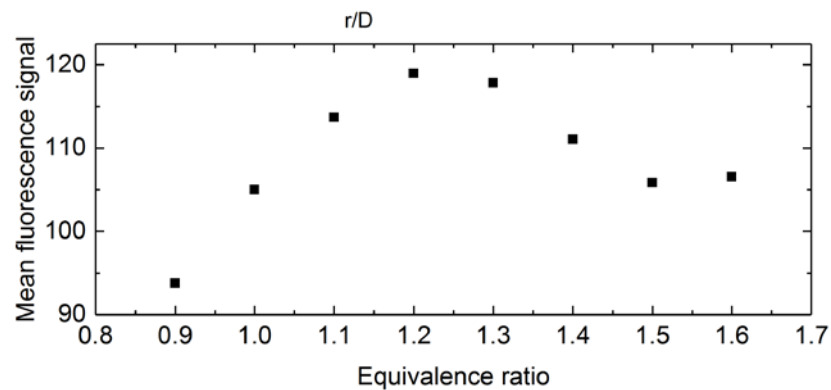
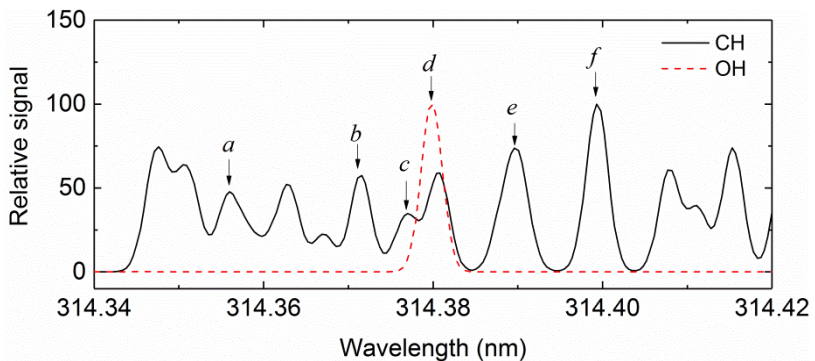
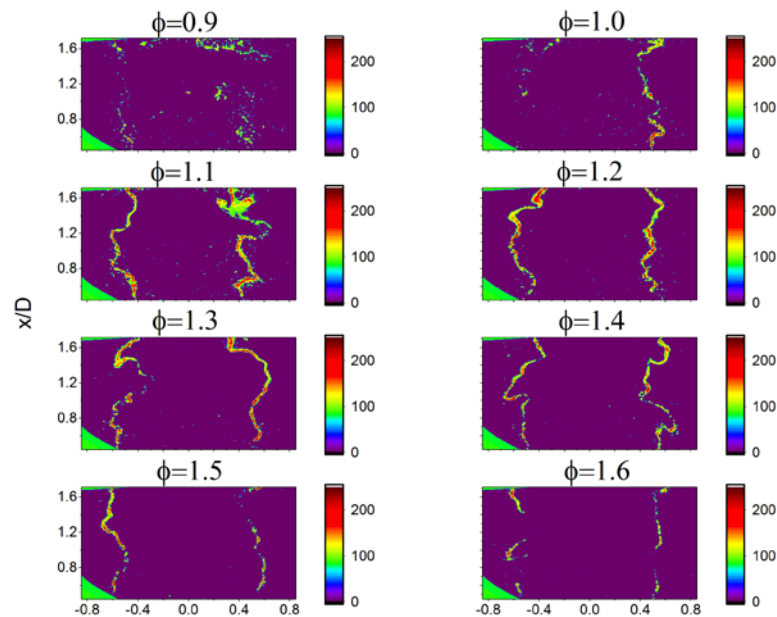
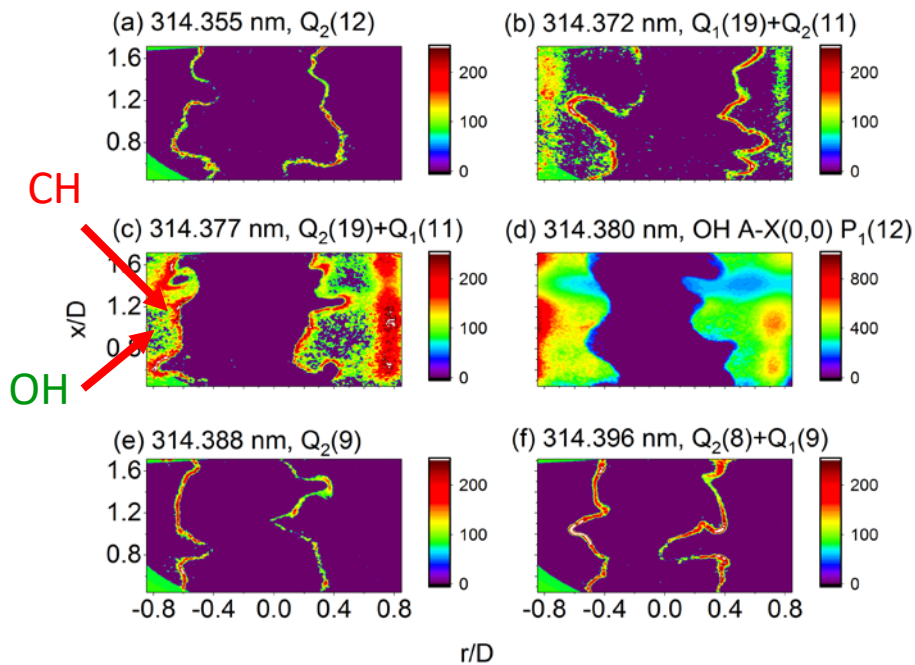
Consumption speed

$$S_{T,LCP} = \frac{\Delta A_{up}}{2\pi R_e \Delta t}$$



Fine-scale pocket: a pocket does not break up into smaller ones with flame-flame interaction

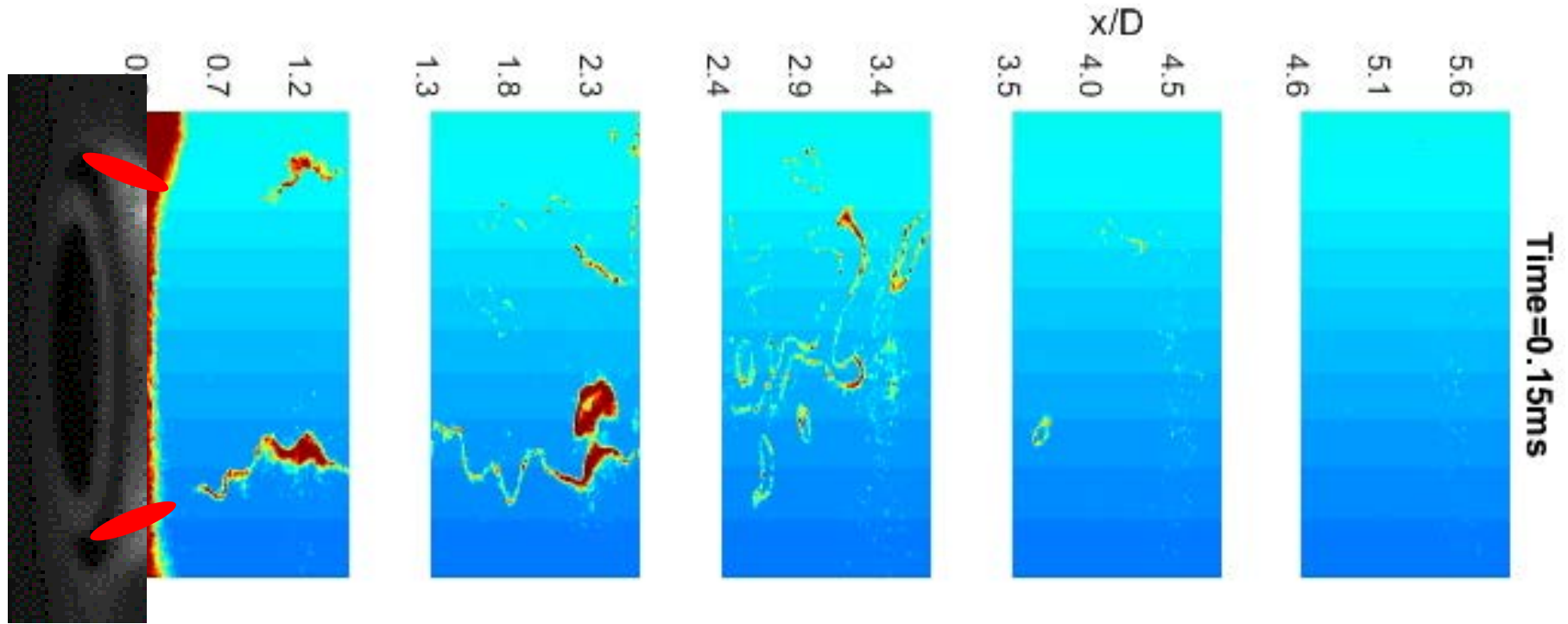
# CH PLIF: Wavelength & Signal Strength



Simulation using LIFBASE

# CH PLIF video for flame with 0% CO<sub>2</sub> addition

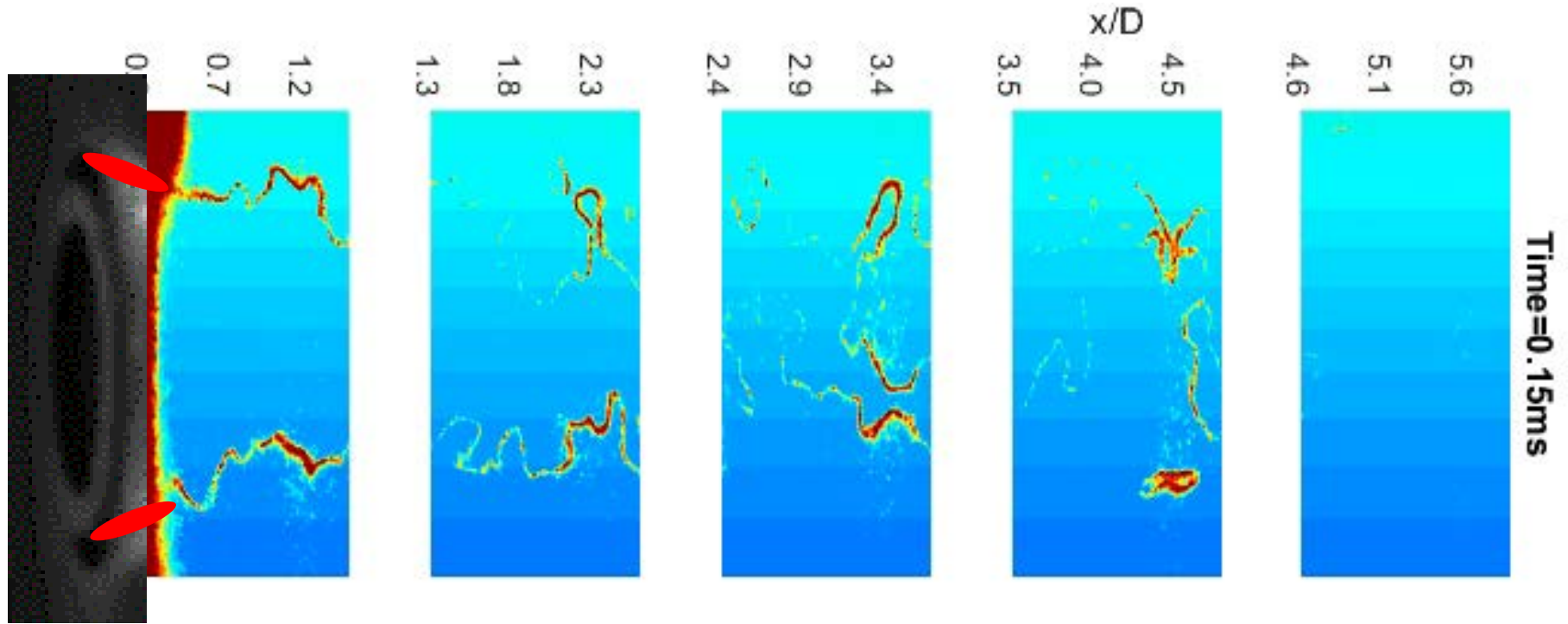
$\Phi=1$ ,  $Re=10000$



Hydrogen pilot flame

# CH PLIF video for flame with 5% CO<sub>2</sub> addition

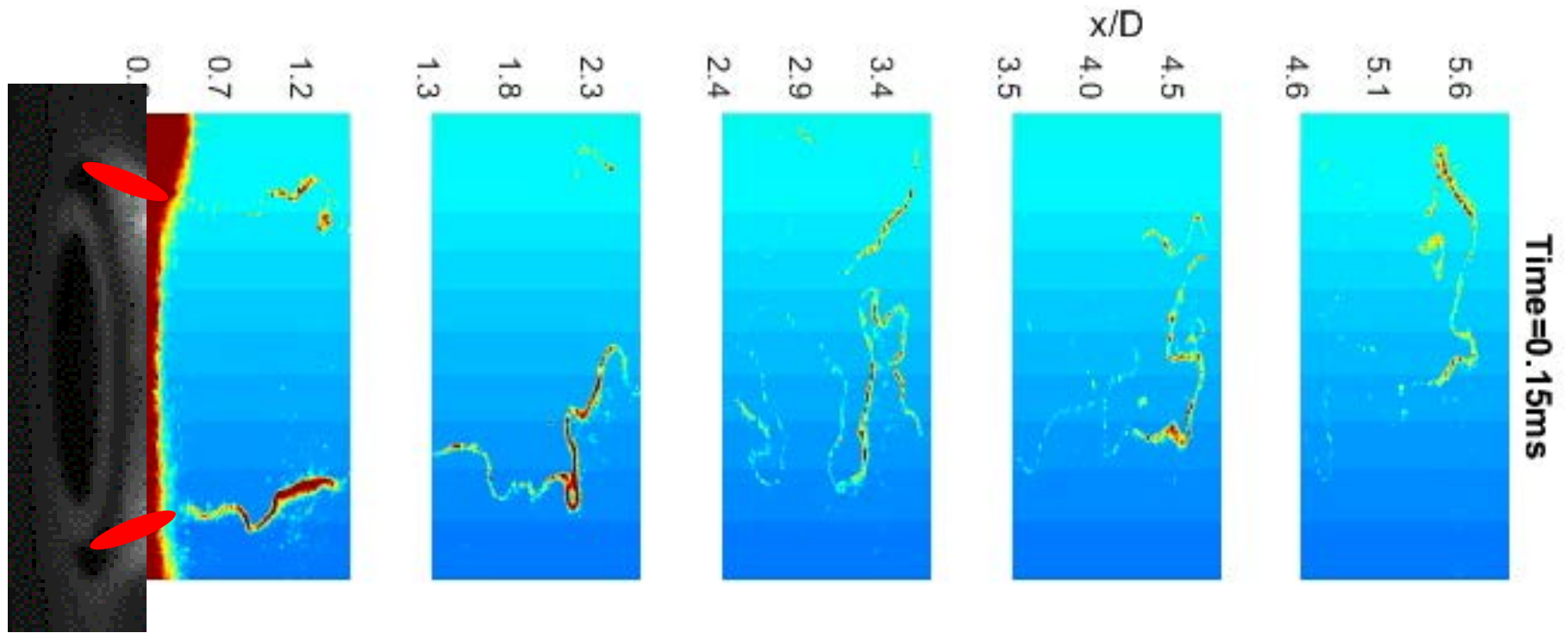
$\Phi=1$ ,  $Re=10000$



Hydrogen pilot flame

# CH PLIF video for flame with 10% CO<sub>2</sub> addition

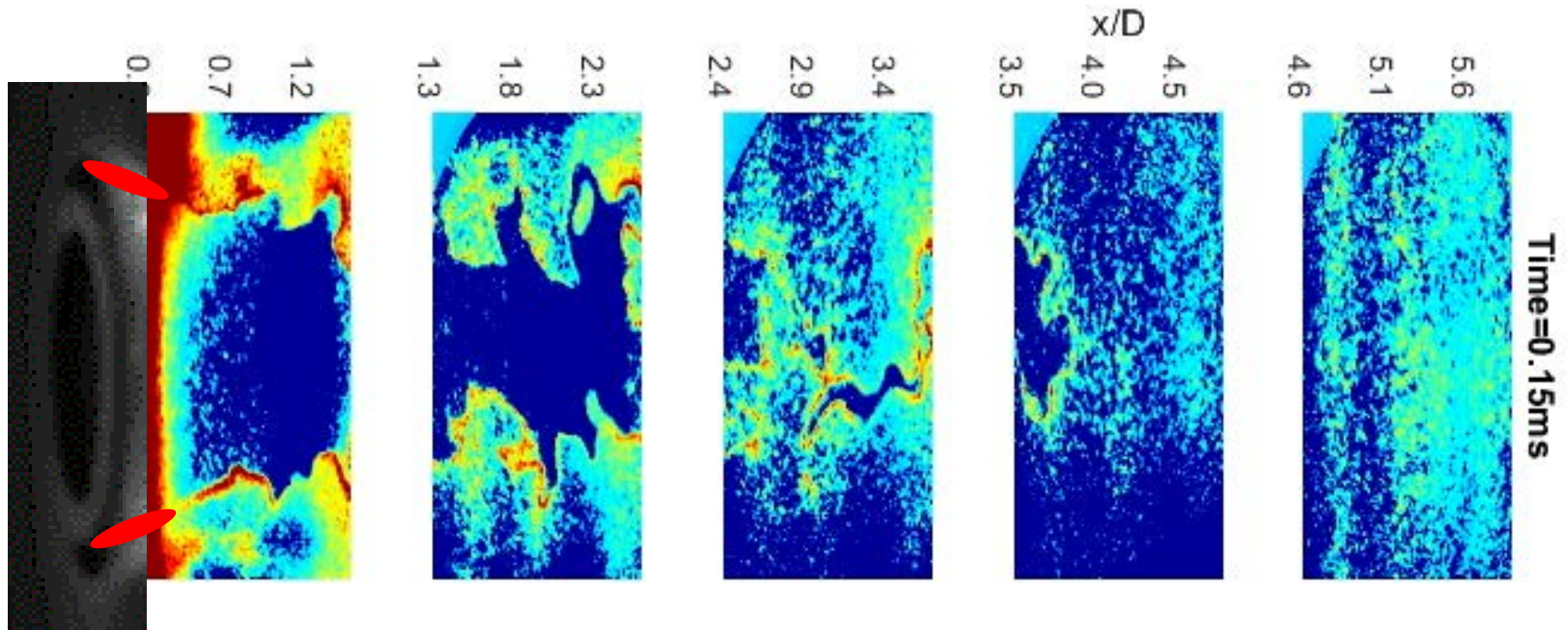
$\Phi=1, Re=10000$



Hydrogen pilot flame

# CH-OH PLIF video for flame with 0% CO<sub>2</sub> addition

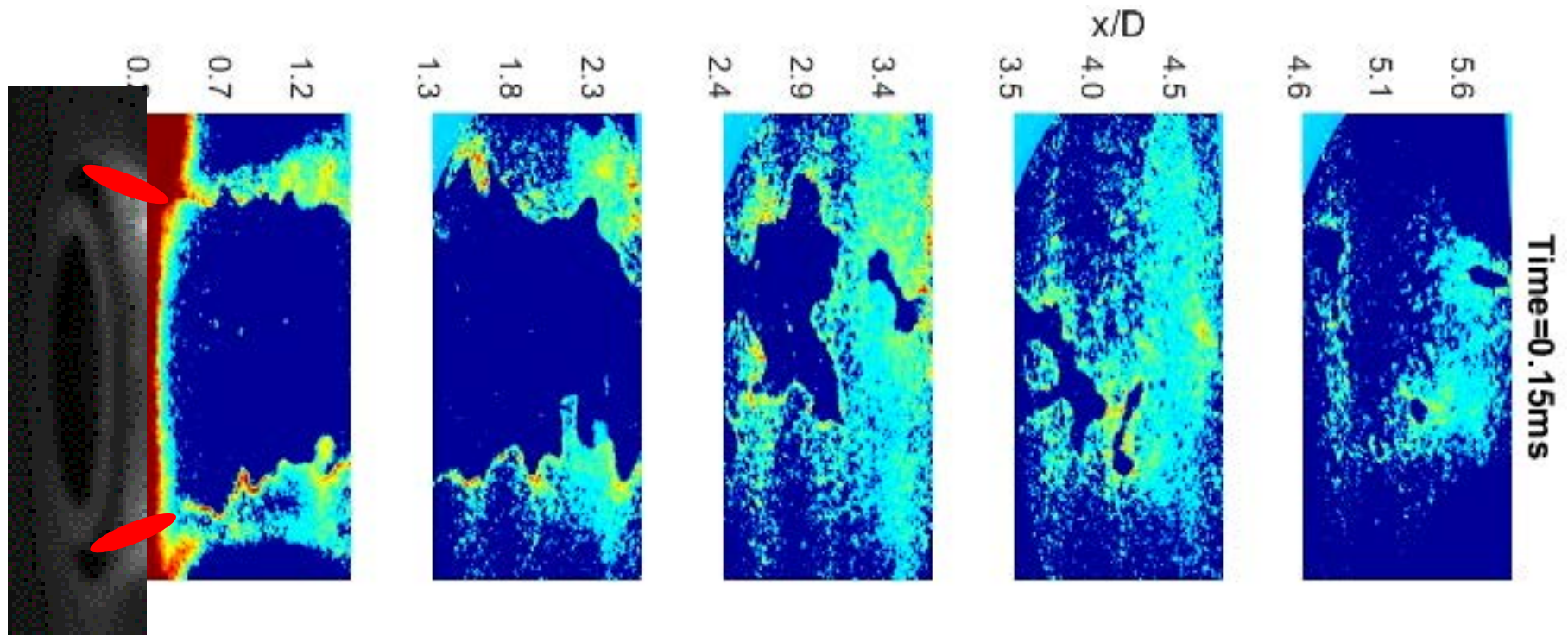
$\Phi=1, Re=10000$



Hydrogen pilot flame

# CH-OH PLIF video for flame with 5% CO<sub>2</sub> addition

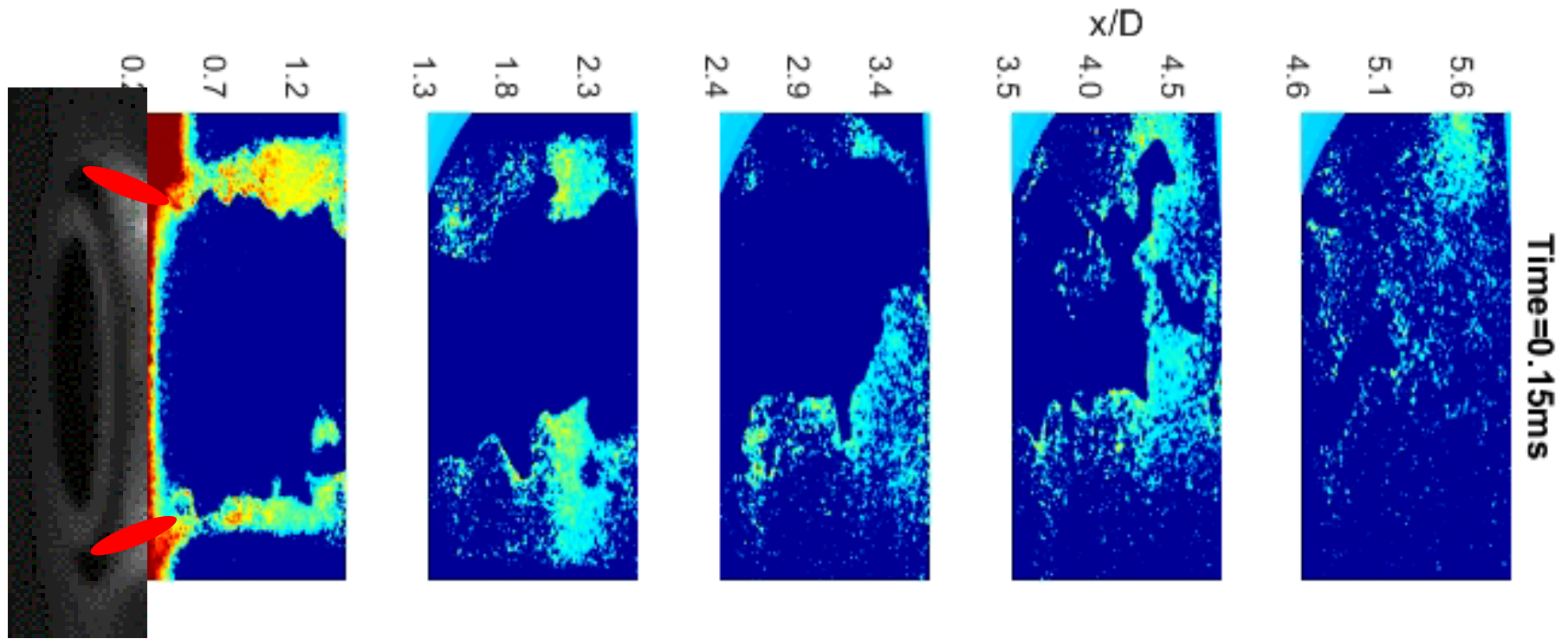
$\Phi=1, Re=10000$



Hydrogen pilot flame

# CH-OH PLIF video for flame with 10% CO<sub>2</sub> addition

$\Phi=1$ ,  $Re=10000$



Hydrogen pilot flame

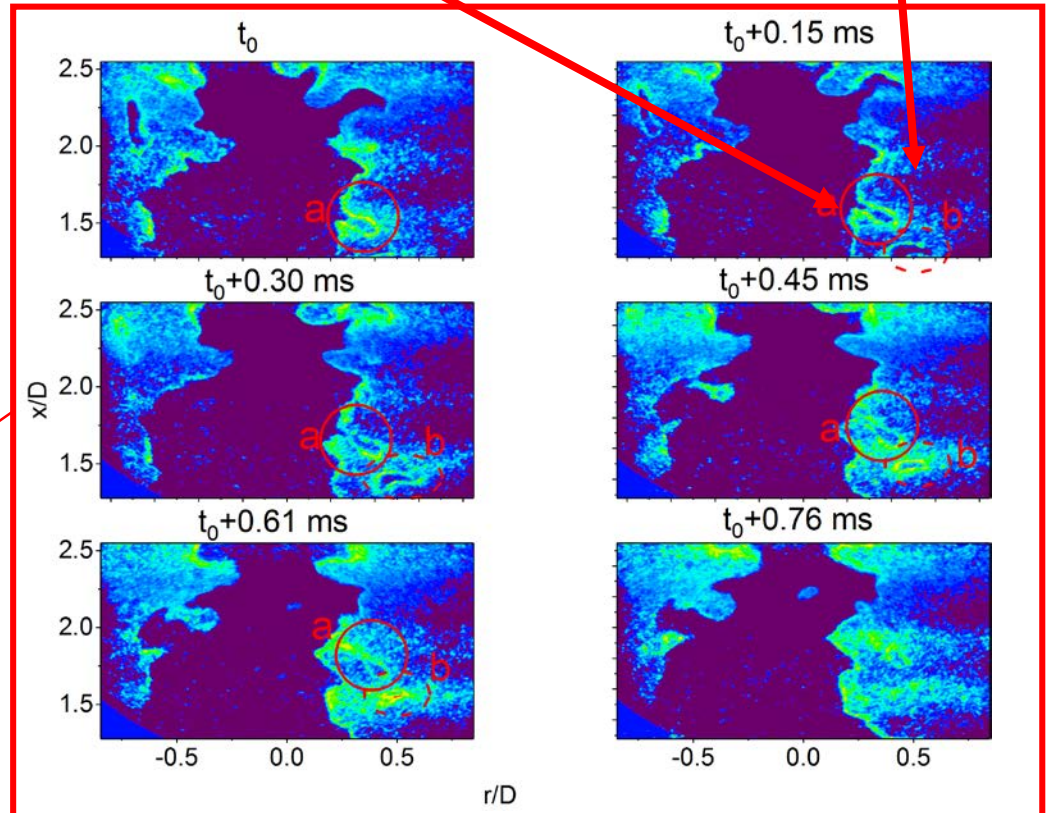
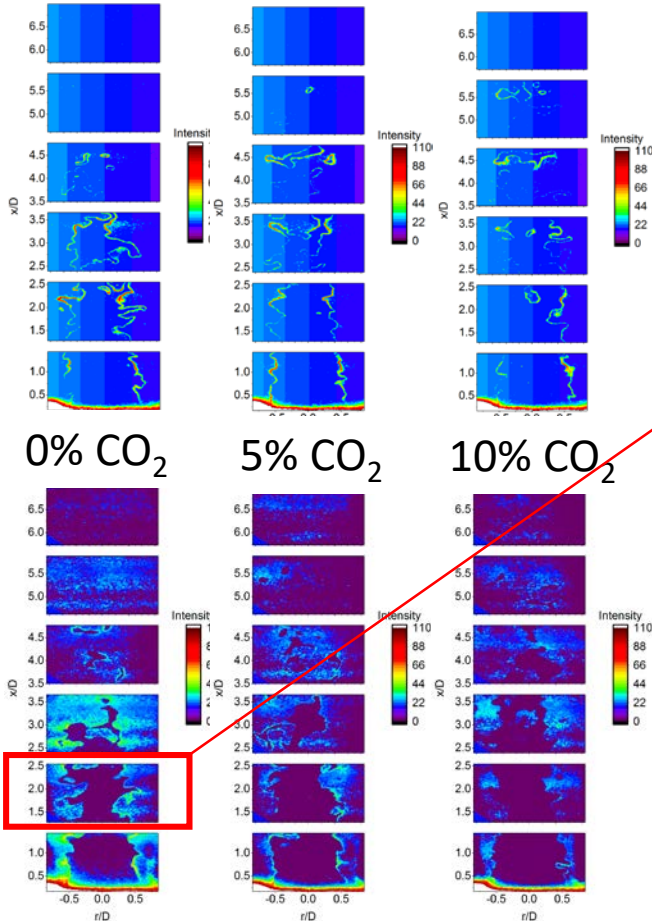


# CH PLIF & Simultaneous CH and OH PLIF

$\Phi=1$ ,  $Re=10000$

Green: CH Layer

Blue: OH Zone

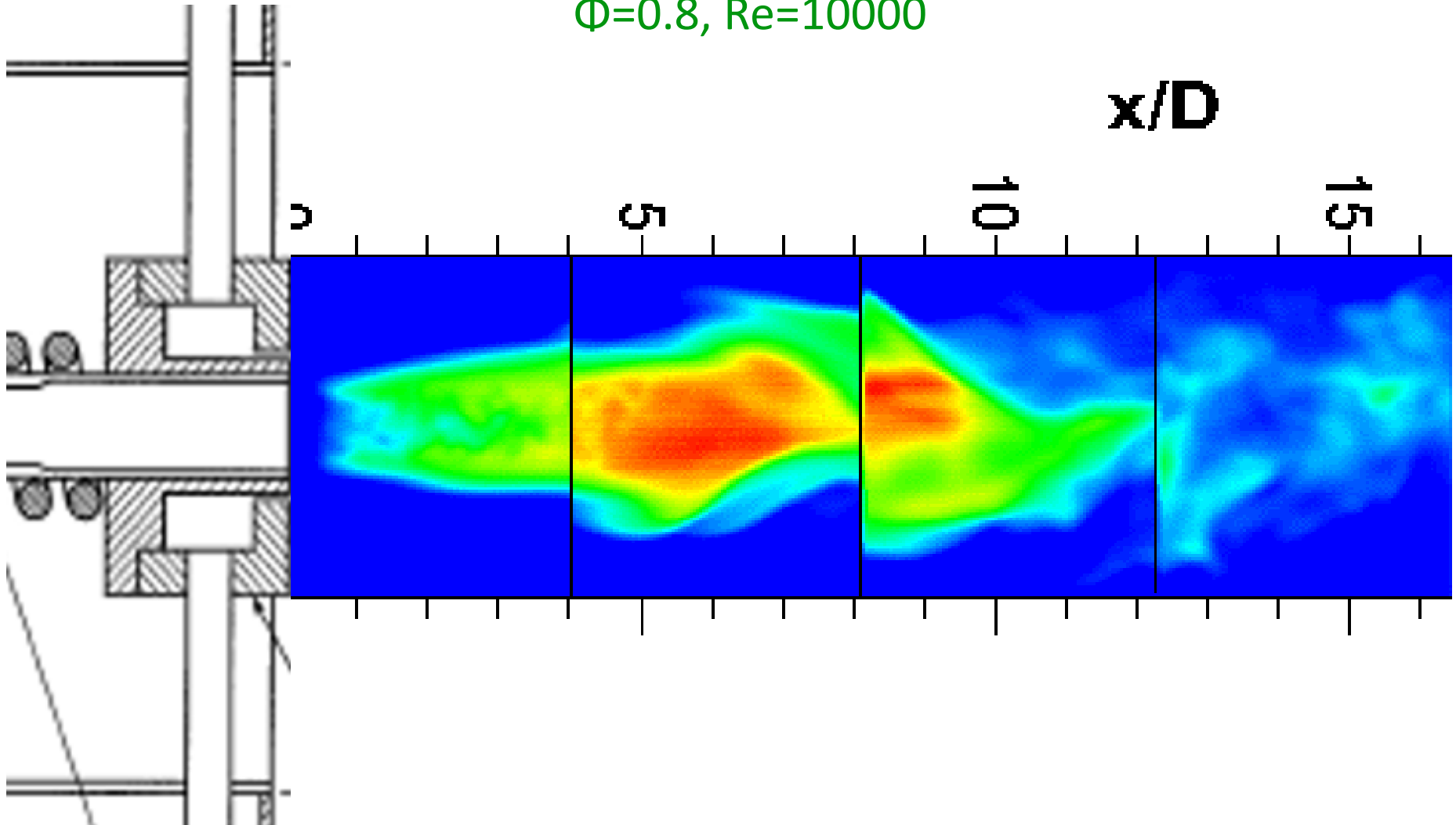


(a) wrinkled flame front, (b) unburned reactant pocket.

Challenging for lean premixed flames with CO<sub>2</sub> dilution due to low CH signal

# IR imaging video for CH<sub>4</sub>/air flame

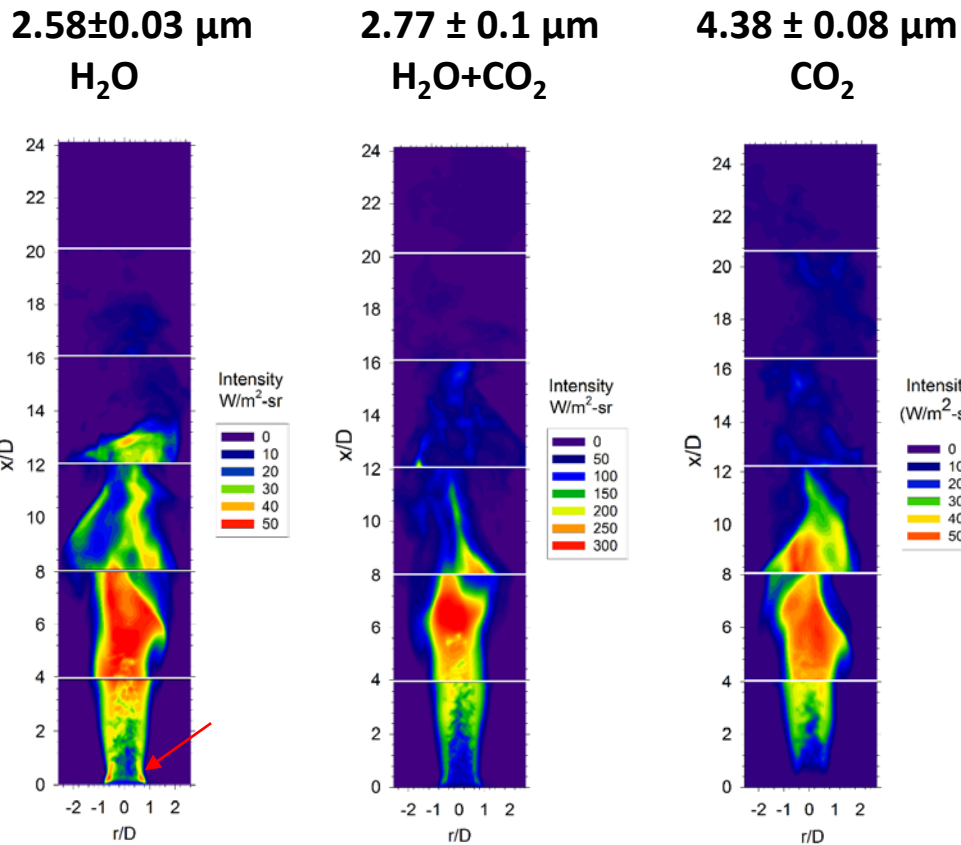
$\Phi=0.8$ ,  $Re=10000$



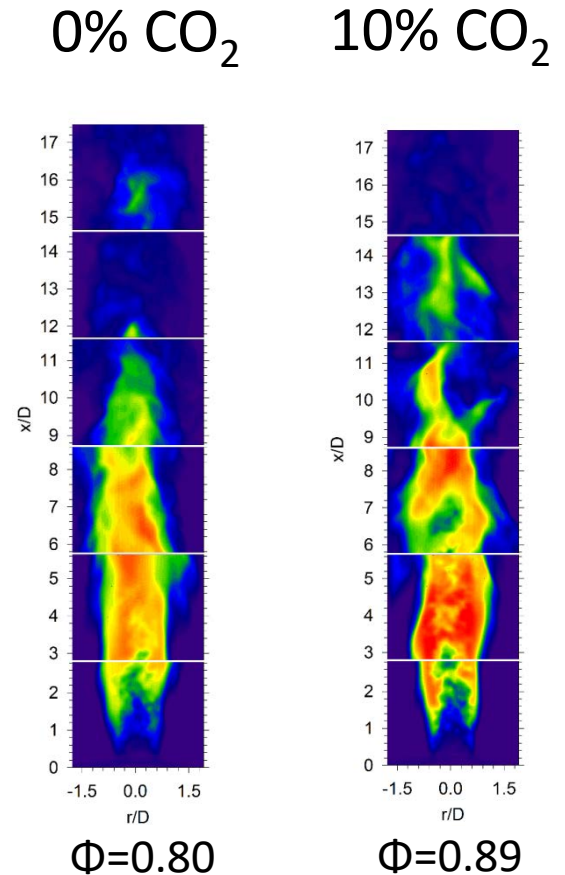
# Instantaneous IR images

Multiple bandpass filters with KC burner

Varying CO<sub>2</sub> with PARAT burner



CH<sub>4</sub>/air  $\Phi=0.80$  Re=10000



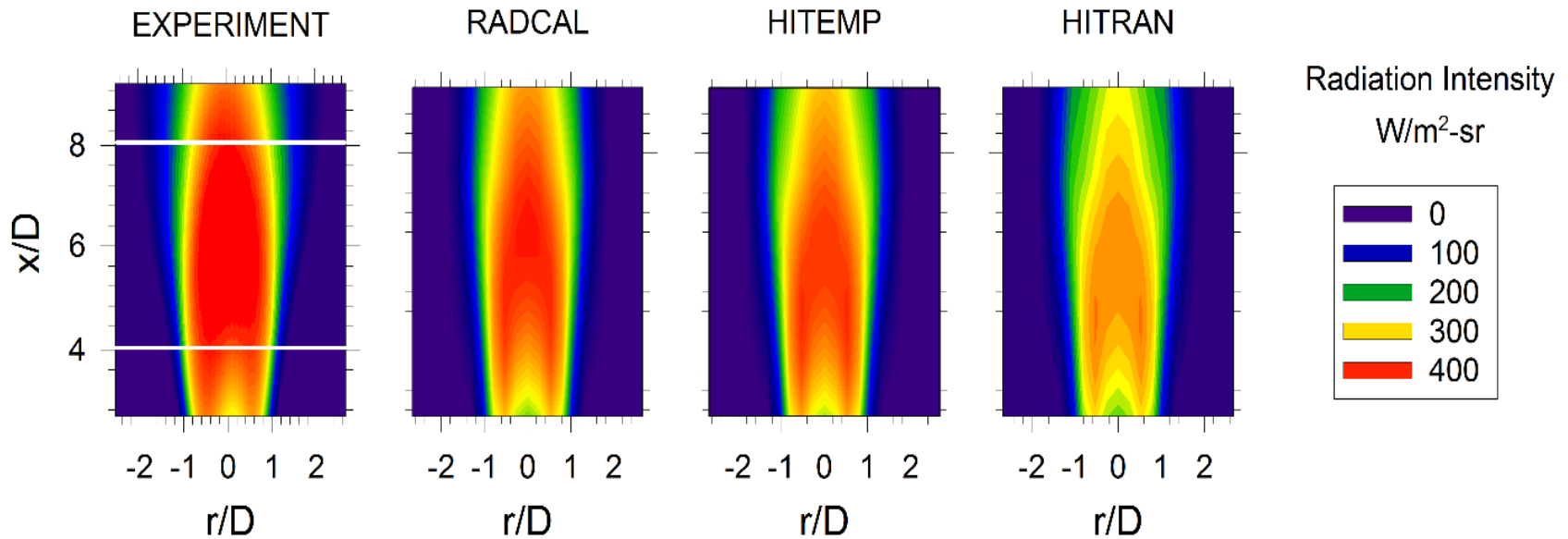
Re=10000

# Time Averaged Radiation Model Validation

Turbulence radiation interaction (TRI) modeling:

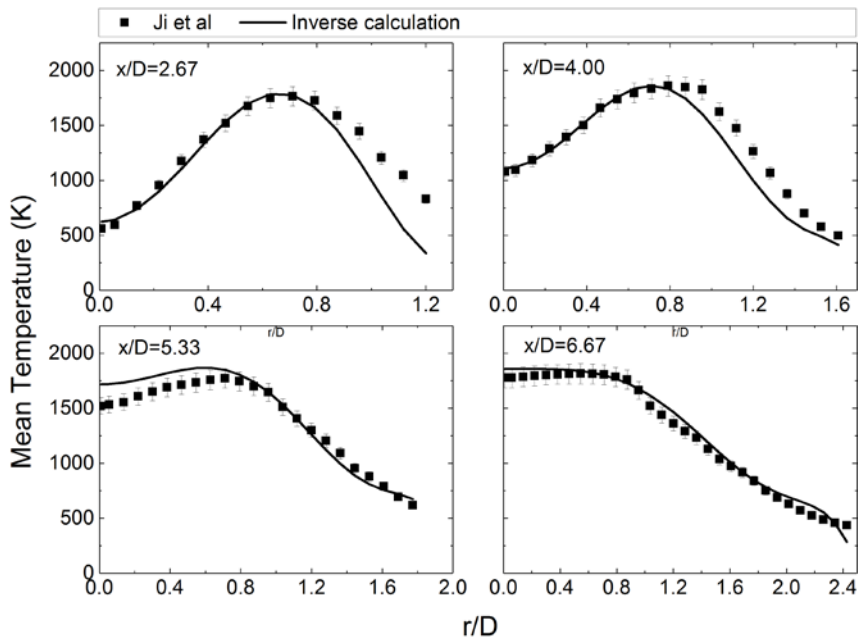
Stochastic time and space series analysis (STASS)

$$I = \int_{\lambda_1}^{\lambda_2} \alpha_{\lambda} I_{\lambda}(0) e^{-\tau_{\lambda}} d\lambda + \int_{\lambda_1}^{\lambda_2} \int_0^{\tau_{\lambda}} \alpha_{\lambda} I_{b\lambda}(\tau_{\lambda}^*) e^{-(\tau_{\lambda} - \tau_{\lambda}^*)} d\tau_{\lambda}^* d\lambda$$

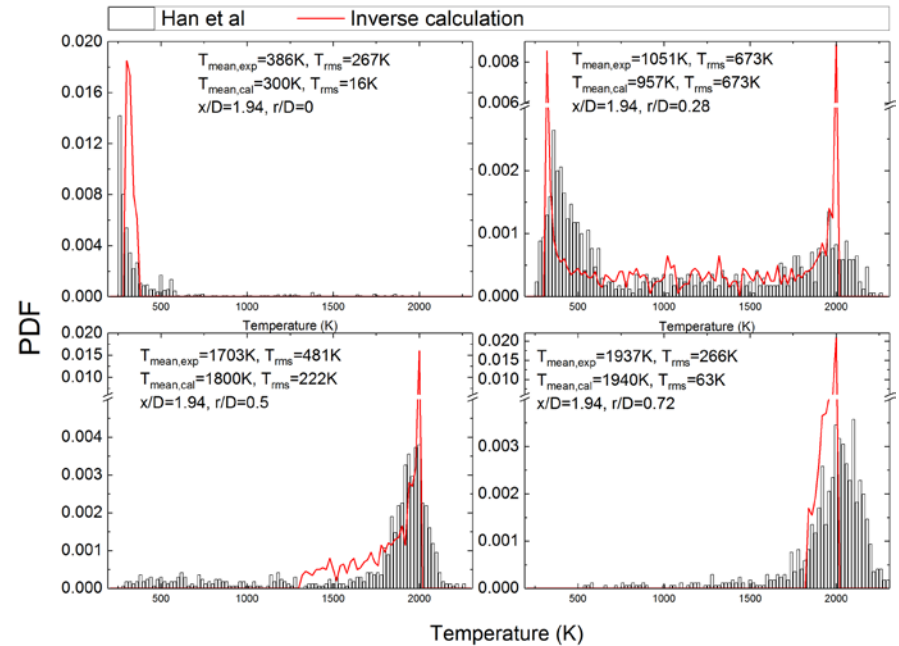


# Temperature Deconvolution

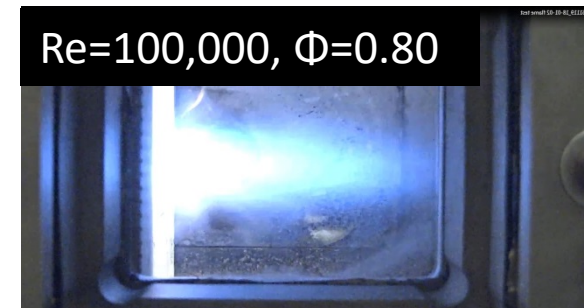
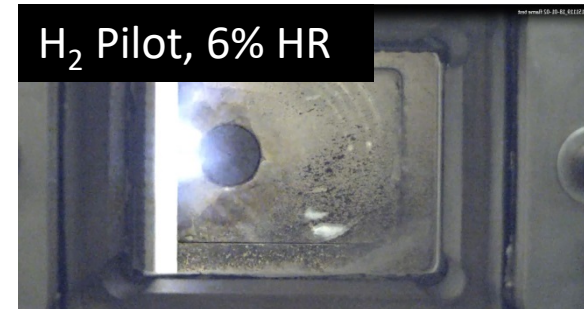
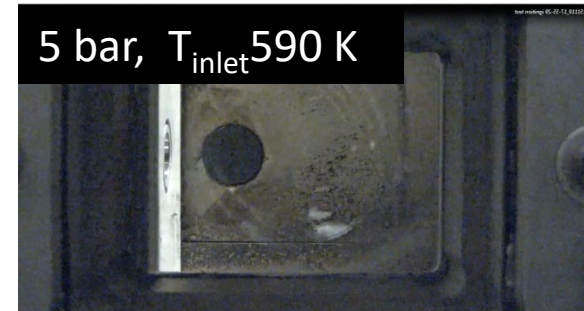
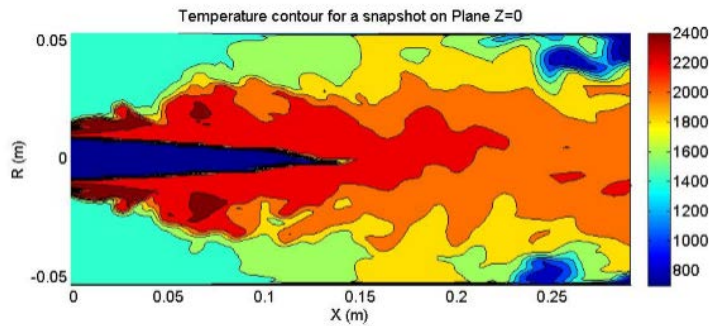
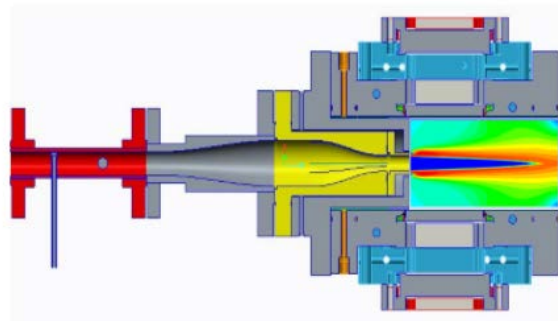
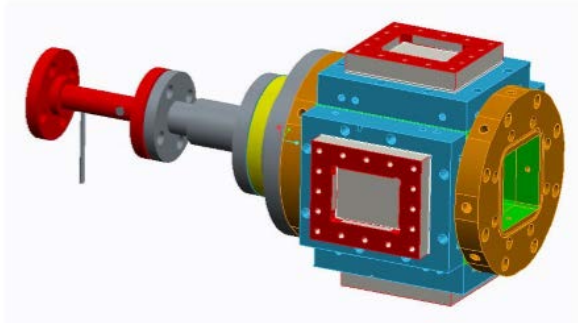
## Computed temperature vs thin filament thermometry



## Computed temperature vs CARS thermometry



# High Pressure PARAT Experiments and LES



# Summary & Conclusions

1. Developed a PARAT burner and demonstrated multiple diagnostic methods including PIV, CARS, OH/CH PLIF and IR imaging for turbulent premixed combustion applications.
2. Performed a comprehensive investigation of the non-thermal effects of CO<sub>2</sub> addition on turbulent premixed combustion for the first time.
3. CO<sub>2</sub> addition extends flame length, Modifies flame brush to be longer and thinner, alters local flame surface area, reduces burning velocities, and enhances pocket formation with negligible effects on pocket consumption speed
4. Developed LES simulation tool for CH<sub>4</sub>/air/CO<sub>2</sub> flames and validated using temperature and velocity measurements

# Appendix

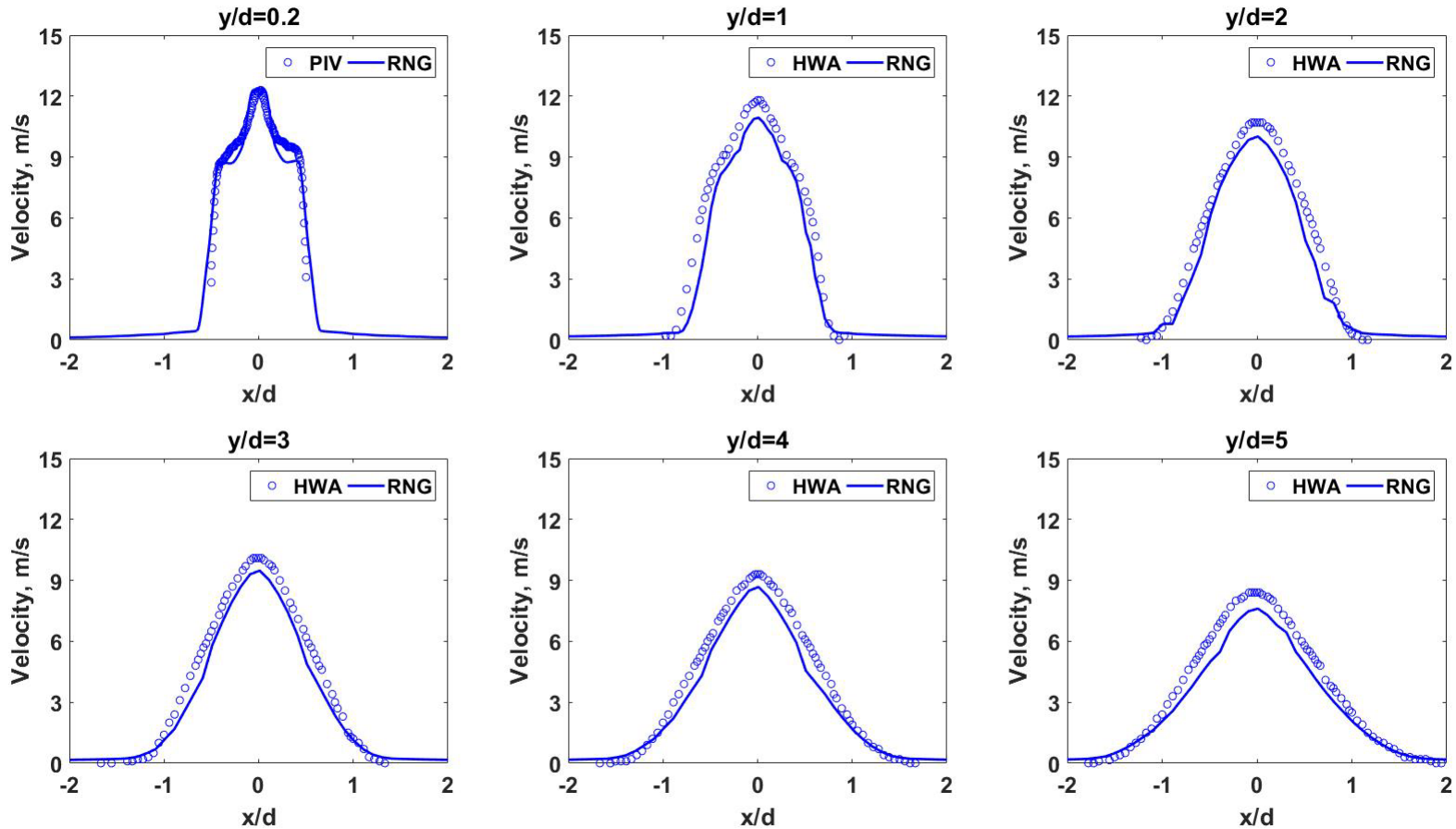
## Flame operating conditions

Flame #	1	2	3
Reynolds number ( $\pm 50$ )	10000		
Adiabatic Temperature ( $\pm 50$ K)	2030		
Equivalence ratio ( $\pm 0.02$ )	0.80	0.84	0.89
CO <sub>2</sub> % by total mass ( $\pm 0.1$ )	0.0	5.0	10.0
CH <sub>4</sub> mass flow rate ( $\pm 2$ mg/s)	111	110	109
Air mass flow rate ( $\pm 20$ mg/s)	2440	2300	2150
CO <sub>2</sub> mass flow rate ( $\pm 4$ mg/s)	0.00	124	246
Pilot H <sub>2</sub> mass flow rate ( $\pm 0.03$ mg/s)	2.7		
Pilot H <sub>2</sub> heat release percent of total (%)	6		
Lewis number	1		
Laminar flame speed (cm/s)	34	30	25
Laminar flame thermal thickness ( $\mu\text{m}$ )	70	80	90
RMS turbulence fluctuation (m/s)	1.7		
Integral length scale (mm)	1		



# Appendix

## Cold flow Results with RANS based RNG k- $\epsilon$ model

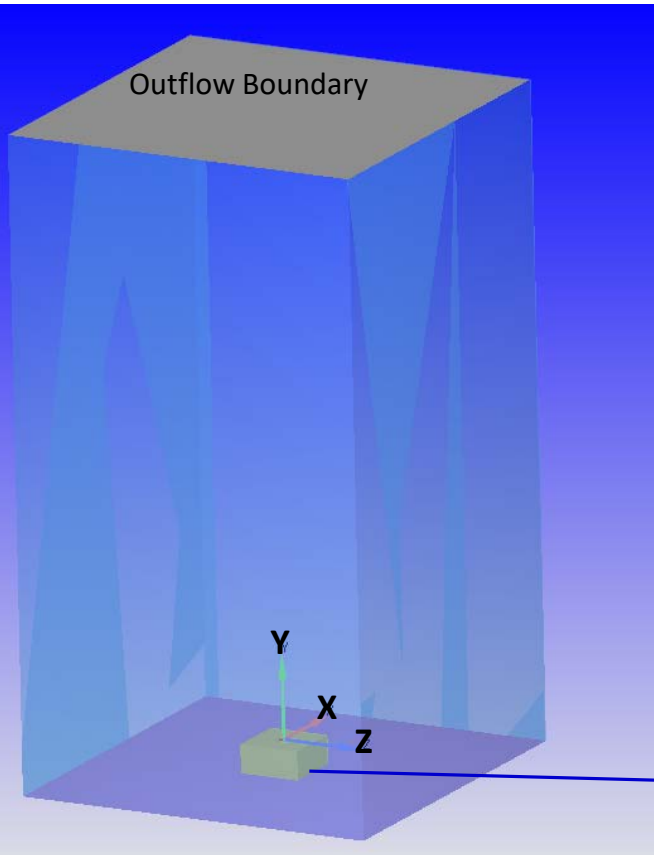


**Good Agreement with Hot wire anemometer measurements**

# Appendix

## CFD Domain and BCs - Reacting

36D x 64D x 36D, D= 18 mm



$$u_i = u_{i, set} + u'_i$$

$$u'_i(x_j) = 2 \sum_{n=1}^N \hat{u}^n \cos(\kappa_j^n x_j + \psi^n) \sigma_i^n$$

$\hat{u}^n$  Amplitude of the  $n$ th Fourier mode based on the modeled turbulent spectrum

$\psi^n$  Phase of the  $n$ th Fourier mode

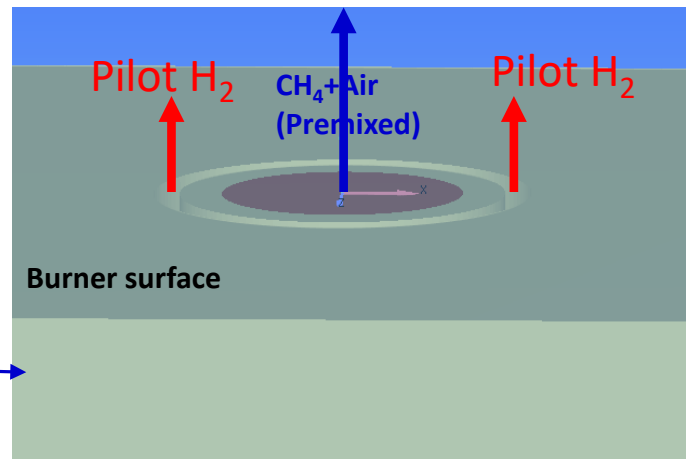
$\sigma_i^n$  Direction of the  $n$ th Fourier mode

$\kappa_j^n$  Wavenumber of the  $n$ th Fourier mode in the  $j$  direction

Nozzle Exit: Specified mean velocity profile.

Turbulent Fluctuations: Random Fourier Approach

Davidson et.al, IJHF, 27, 2006



**Premixing Tube Excluded to Reduce Computational Time**