

# Final Report: An Experimental and Modeling Study of $\text{NO}_x$ -CO Formation in High Hydrogen Content (HHC) Fuels Combustion in Gas Turbine Applications (DE-FE0012005)

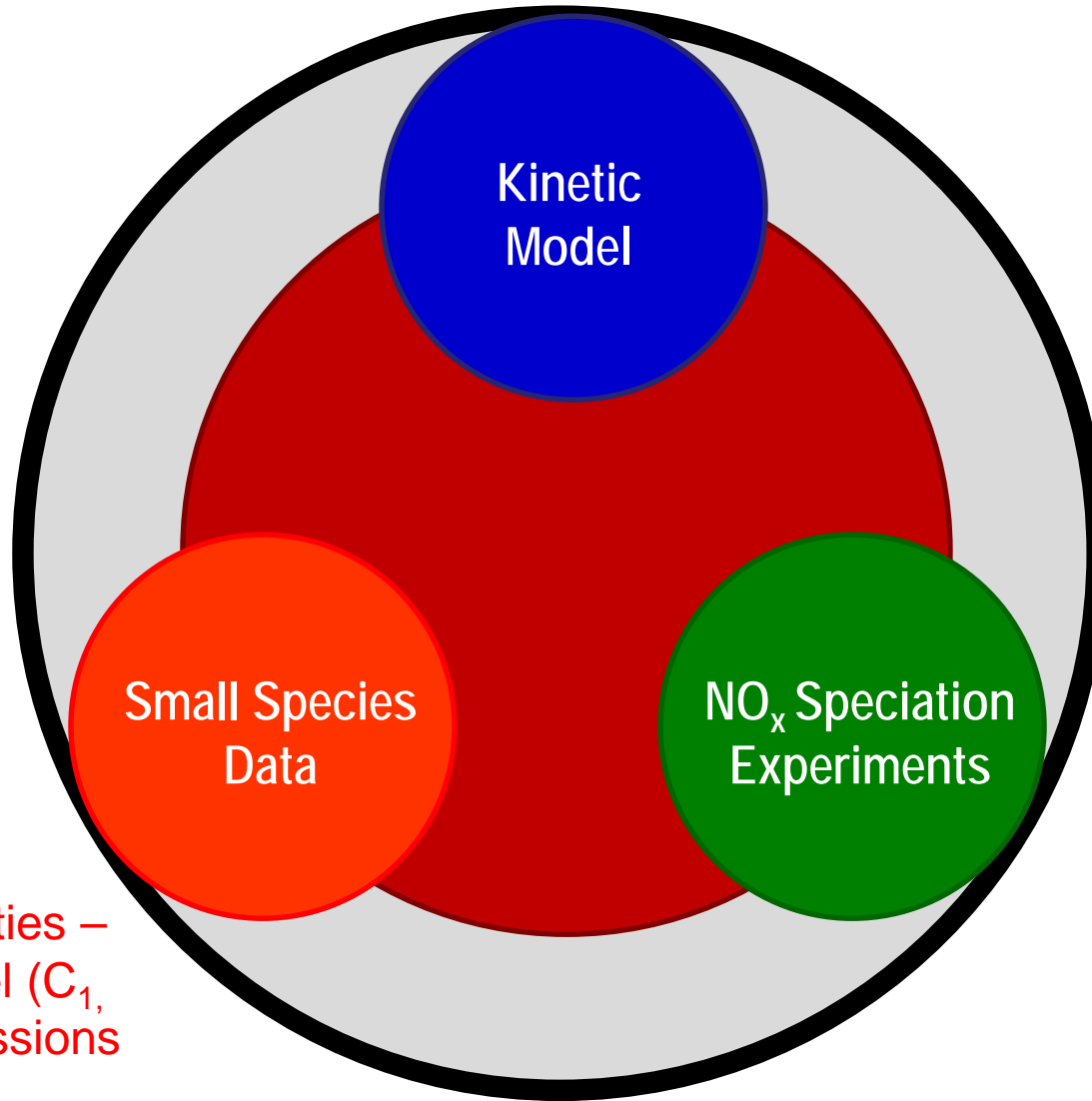
**Tanvir Farouk**

University of South Carolina, Columbia, SC 29208, USA

**2017 University Turbine System Research Workshop**

**Pittsburgh, PA**

**November 1<sup>st</sup> – 2<sup>nd</sup>, 2017**



- Predictions of  $\text{NO}_x$  to address strict emission standards

- Trace emittents –  $\text{NO}_x$  influences the global and intricate combustion dynamics

- Fuel impurities – source of fuel ( $\text{C}_1$ ,  $\text{C}_2$  ...) – emissions

Unless one considers the ***interactions of small species and emittents***, particularly on natural gas combustion the resulting model will likely have poor fidelity to be considered for engineering applications

- Detailed and validated coupled HHC + NO<sub>x</sub> kinetic model
- New experimental speciation data for the oxidation kinetics of HHC fuel compositions in presence of impurities.
- Understanding of CO, NO and NO<sub>2</sub> formation and interactions in hot and cold flow interactions.
- Detailed and reduced kinetic models for HHC fuels including detailed fuel compositions and NO<sub>x</sub>.



***Improved, higher fidelity tools for engineering design!***



- **Project management and planning**
- **Study of reactivity and speciation data for NO<sub>x</sub> under various conditions in a high pressure McKenna burner – flow tube arrangement**
- **Studies of high pressure HHC fuel kinetics using a High Pressure Laminar Flow Reactor (HPLFR)**
- **Kinetic assessment, validation and development of a comprehensive HHC fuel + NO<sub>x</sub> kinetic mechanism**

# Project Participants



## University of South Carolina and Princeton University

**PI: Dr. Tanvir Farouk, Assistant Professor**

University of South Carolina– Mechanical Engineering

- **Sheikh Farhan Ahmed** – Graduate Student
- **Fahd Ebna Alam** – Graduate Student

**Co-PI: Dr. Bihter Padak, Assistant Professor**

University of South Carolina– Chemical Engineering

- **Nazli Asgari** – Graduate Student



UNIVERSITY OF  
**SOUTH CAROLINA**

**Co-PI: Dr. Frederick Dryer, Professor**

Princeton University – Mechanical and Aerospace Engineering

- **Mac Haas** – Technical Staff



**PRINCETON**  
UNIVERSITY

# Presentation Outline

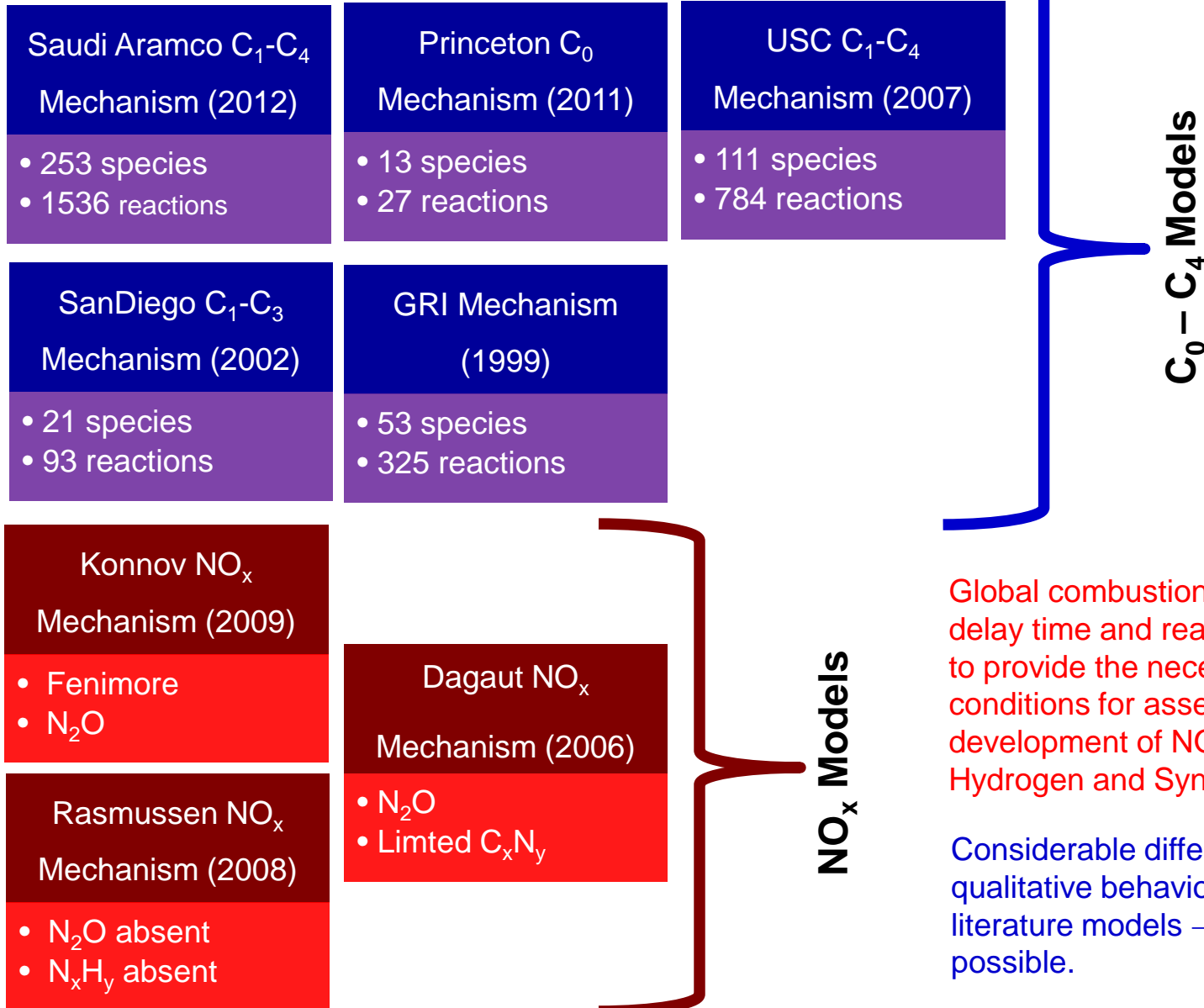


- **Project Objectives**
- **Research Tasks**
- **Research Team Members**
- **Final Report**
  - Kinetic model for NO<sub>x</sub> formation in HHC fuels**
  - Measurement of NO<sub>x</sub> perturbed oxidation experiments**
  - Experiments for speciation measurements**
  - Multi-dimensional CFD + Kinetics modeling and simulations**
- **Summary**



# Kinetic model for $\text{NO}_x$ formation in HHC fuels

# Mechanisms



Global combustion targets (e.g. ignition delay time and reactivity) are insufficient to provide the necessary constraining conditions for assessment and model development of NO<sub>x</sub> interactions with Hydrogen and Syngas Oxidation.

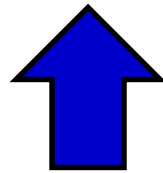
Considerable differences in even qualitative behavior among popular literature models → improvements are possible.



# H<sub>2</sub>/CO/NO<sub>x</sub> Model



Proposed H<sub>2</sub>/CO/NO<sub>x</sub> Model



Sub-mechanisms

C<sub>0</sub>-C<sub>1</sub>  
sub-mechanism

H/N/O  
sub-mechanism

NO<sub>x</sub>  
sub-mechanism

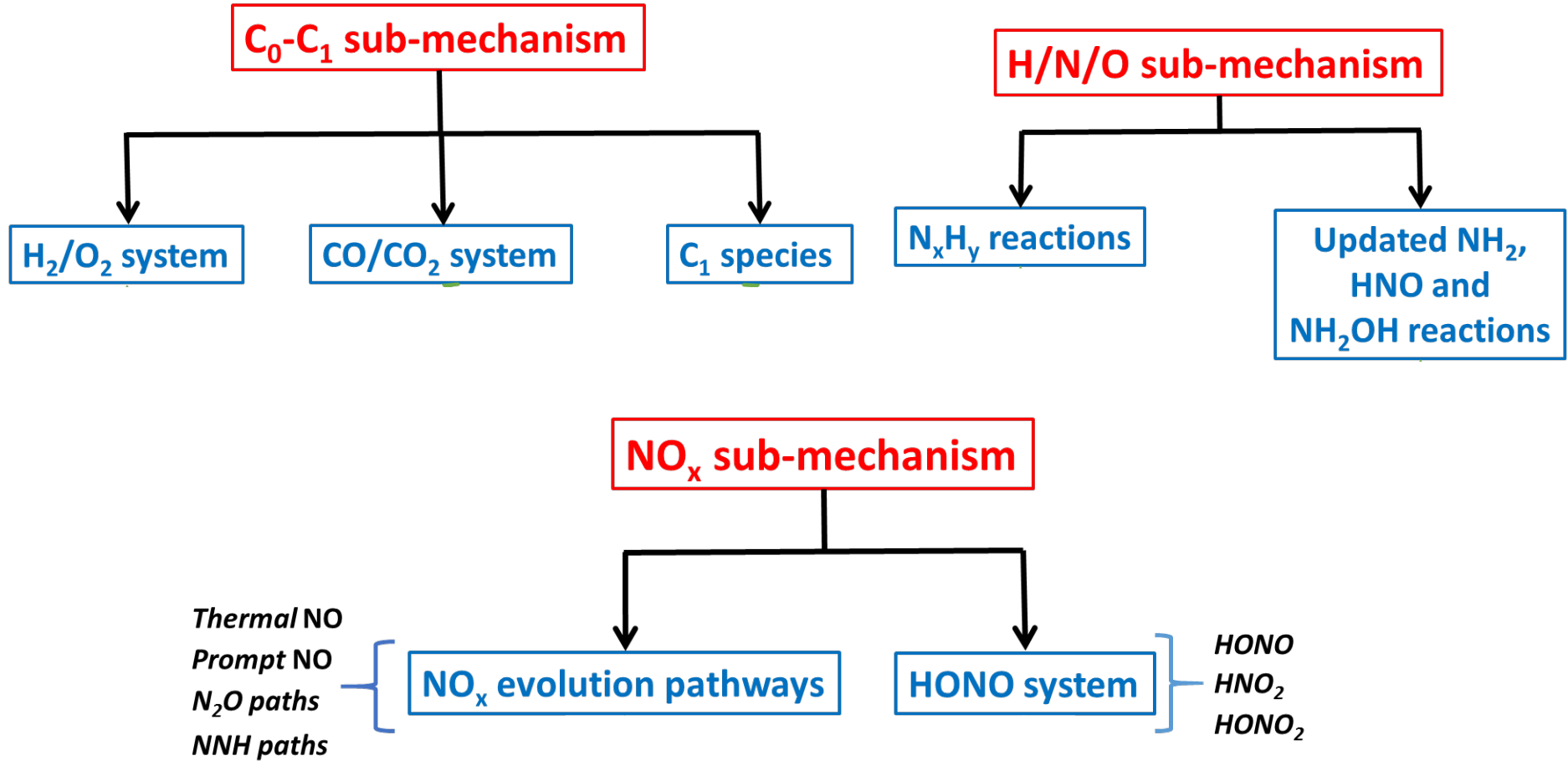
- H<sub>2</sub>/CO/NO<sub>x</sub> Model

77 species, 442 reactions

- H<sub>2</sub>/C<sub>1</sub>-C<sub>4</sub>/NO<sub>x</sub> Model

302 species, 1952 reactions

# Model Elements



<sup>1</sup>Burke et al., *Int. J. Chem. Kinet.* 44 (2012)  
<sup>2</sup>Metcalfe et al., *Int. J. Chem. Kinet.* 45 (2013)  
<sup>3</sup>Skreiberg et al., *Combust. Flame* 136 (2004)  
<sup>4</sup>Klippenstein et al., *Combust. Flame* 158 (2011)

# Prompt-NO Route Updates



Table I Reactions and forward rate parameters for the modified Fenimore reaction pathways

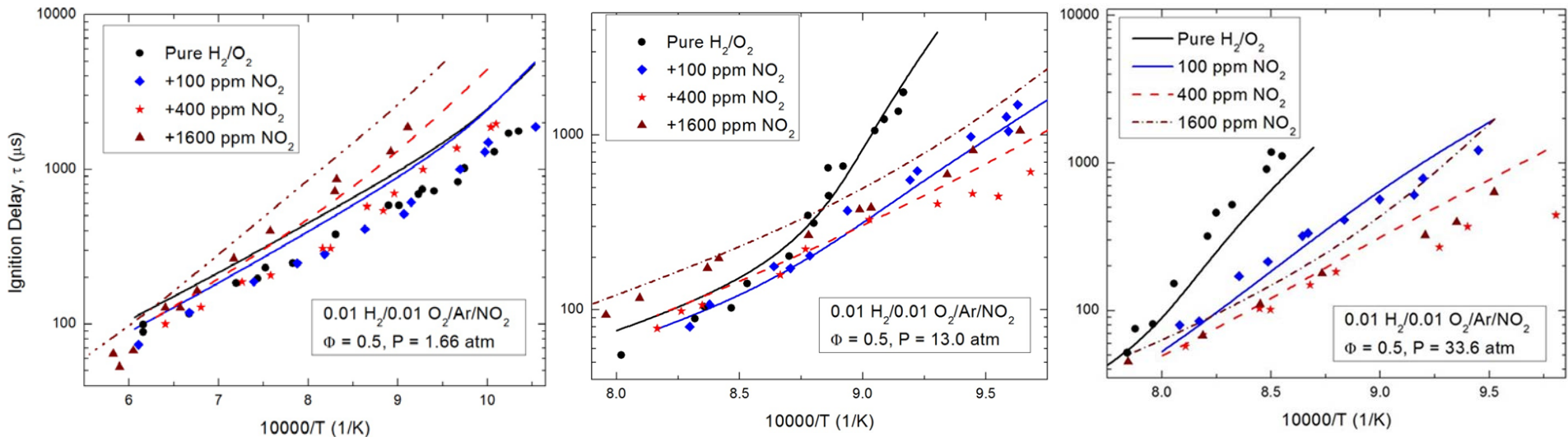
|     | Reactions  | A        | b     | E<br>(cal/mole) |
|-----|--|----------|-------|-----------------|
| 1.  | CN + HNO = HCN + NO  | 1.80E+13 | 0.0   | 0               |
| 2.  | CN + CH <sub>2</sub> O = HCN + HCO   | 4.20E+13 | 0.0   | 0               |
| 3.  | HCN + N <sub>2</sub> = H + CN + N <sub>2</sub>   | 3.60E+26 | -2.60 | 124890          |
| 4.  | HCN + M = HNC + M<br>AR/0.7/ H <sub>2</sub> O/7.0/ CO <sub>2</sub> /2.0                              | 1.60E+26 | -3.23 | 54600           |
| 5.  | HCN + OH = HNCO + H  | 2.80E+13 | 0     | 3700            |
| 6.  | HNCO + O <sub>2</sub> = HNO + CO <sub>2</sub>  | 1.0E+12  | 0.0   | 35000           |
| 7.  | NCO + NO = N <sub>2</sub> O + CO   | 4.00E+19 | -2.16 | 1743            |
| 8.  | NCO + NO = N <sub>2</sub> + CO <sub>2</sub>  | 1.50E+21 | -2.74 | 1824            |
| 9.  | HCNO + OH = NCO + H + OH   | 4.5E+12  | 0.0   | 0               |
| 10. | HCNO + OH = NCO + H <sub>2</sub> O   | 3.50E+12 | 0.0   | 0               |
| 11. | HCNO + OH = HCO + HNO  | 4.50E+12 | 0.0   | 0               |
| 12. | HCNO + OH = NO + CO + H <sub>2</sub>   | 1.42E-07 | 5.64  | 9220            |
| 13. | NO <sub>2</sub> + HCO = HONO + CO<br>N <sub>2</sub> /0.0/ O <sub>2</sub> /1.5/ H <sub>2</sub> O/10.0 | 6.50E+12 | 0.0   | 0               |
| 14. | HOCN + O = NCO + OH  | 1.70E+08 | 1.50  | 4133            |
| 15. | HOCN + OH = HCO + H <sub>2</sub> O   | 1.20E+06 | 2.0   | -248            |
| 16. | H <sub>2</sub> CN + OH = HCN + H <sub>2</sub> O  | 1.50E+19 | -2.18 | 2166            |
| 17. | HCNO + H = HCH + OH  | 7.20E+10 | 0.841 | 8612.0          |
| 18. | CN + H <sub>2</sub> O = HCN + OH   | 3.90E+06 | 1.83  | 10300           |
| 19. | OH + HCN = HOCN + H  | 5.90E+04 | 2.40  | 12500           |
| 20. | OH + HCN = HNCO + H  | 2.00E-03 | 4.0   | 1000            |
| 21. | HOCN + H = HNCO + H  | 3.10E+08 | 0.84  | 1917            |

HCN → one of the major intermediates in prompt-NO kinetics

12 additional reactions and 9 rate updates are proposed based on the path flux comparisons of the NO<sub>x</sub> model of Dagaut et al. (2008) and the proposed model

# Model Performance: Ignition Delay

## Dependence of $\tau_{ig}$ on initial $\text{NO}_2$ doping for $\text{H}_2/\text{O}_2$ system



**Pressure**



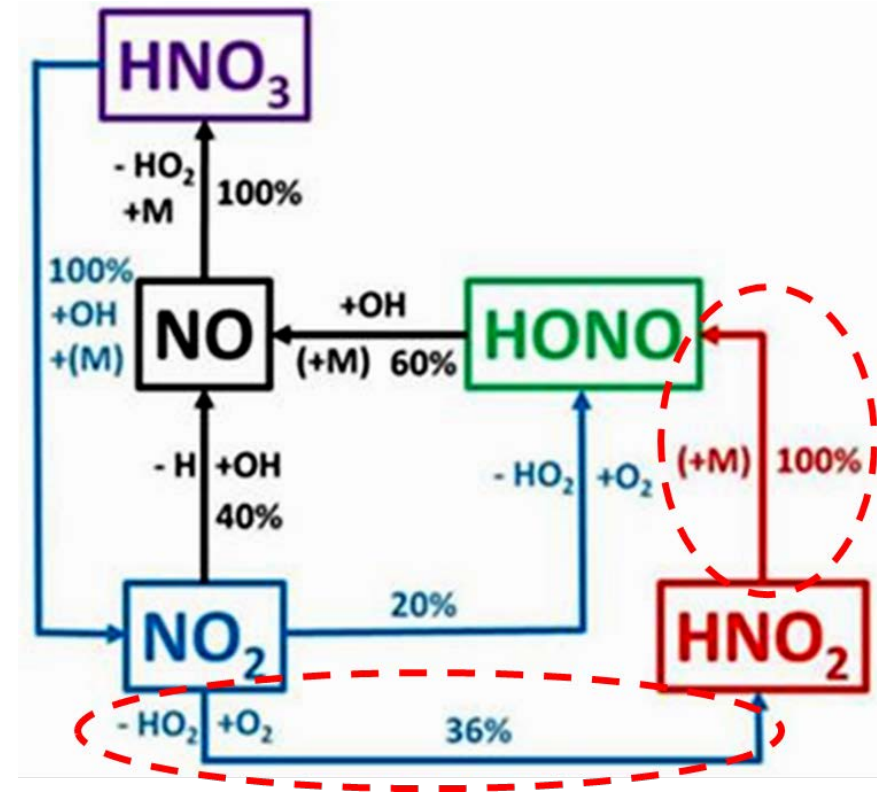
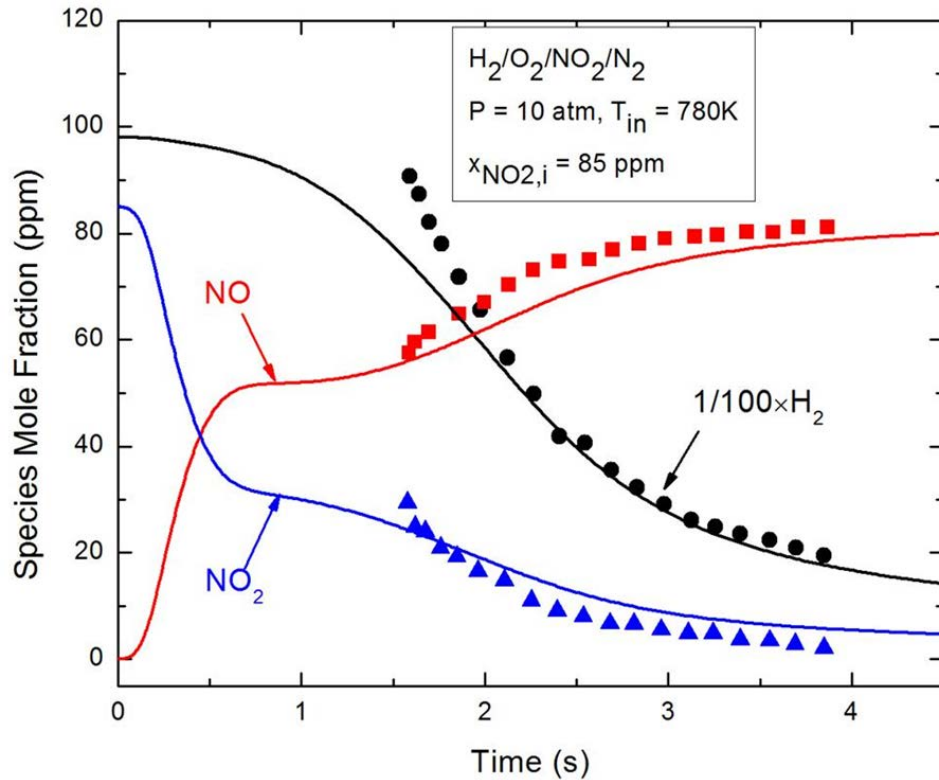
100 ppm → insignificant  
 400 ppm or higher → reactivity decreases

100 - 400 ppm → reactivity increases  
 1600 ppm → reactivity decreases

100 - 400 ppm → reactivity increases  
 1600 ppm → reactivity decreases

**High pressure non-monotonic behavior captured by the model**

# Model Performance: PFR Speciation for H<sub>2</sub>/O<sub>2</sub>/NO<sub>2</sub>/N<sub>2</sub> System



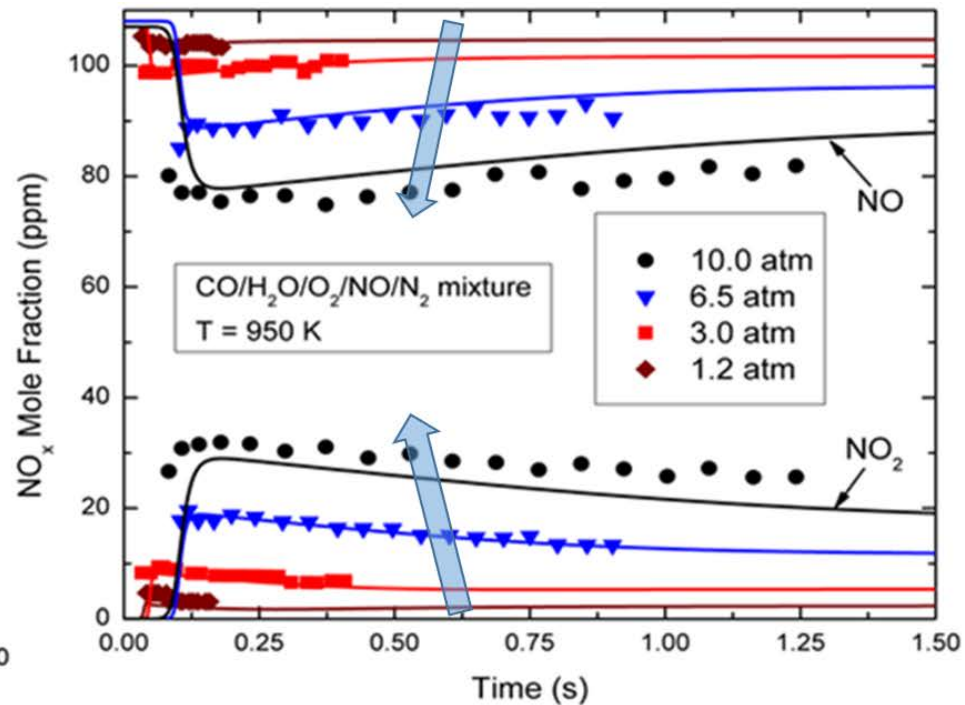
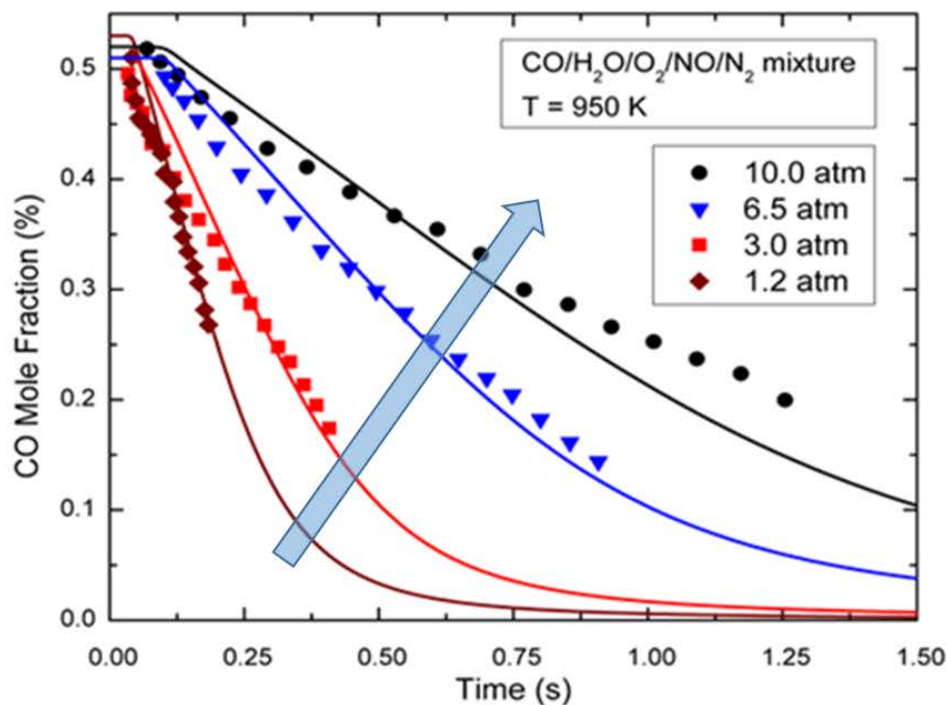
**Reasonable model prediction of fuel consumption and NO-NO<sub>2</sub> conversion**

NO → NO<sub>2</sub> conversion: through intermediate HNO<sub>3</sub>

NO<sub>2</sub> → NO conversion: (i) direct  
 (ii) through intermediate HONO  
 (iii) through intermediate HNO<sub>2</sub>

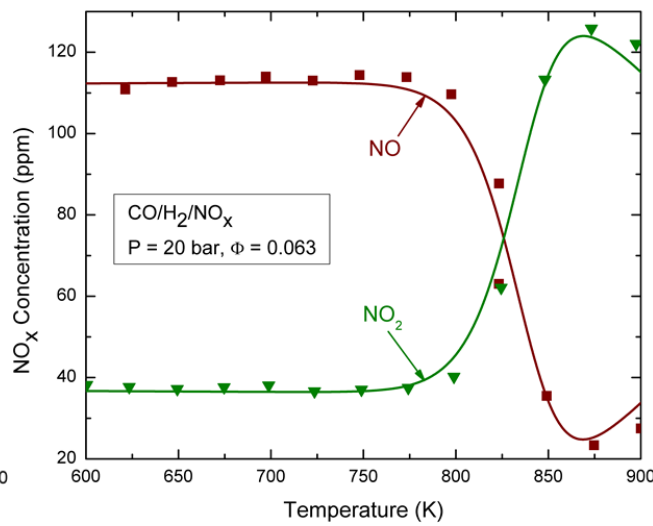
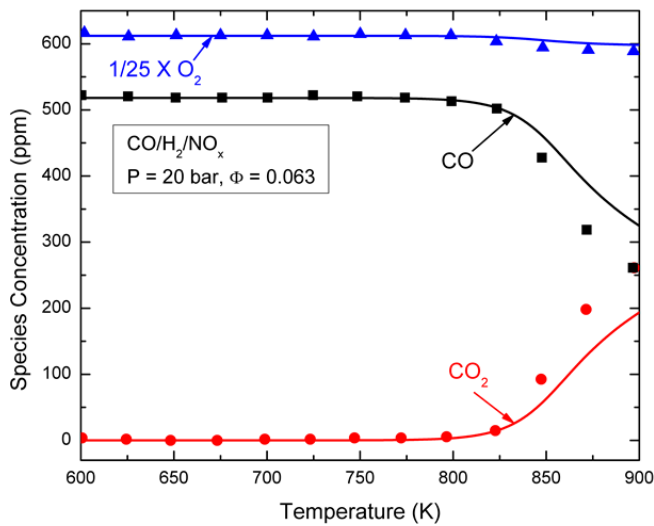
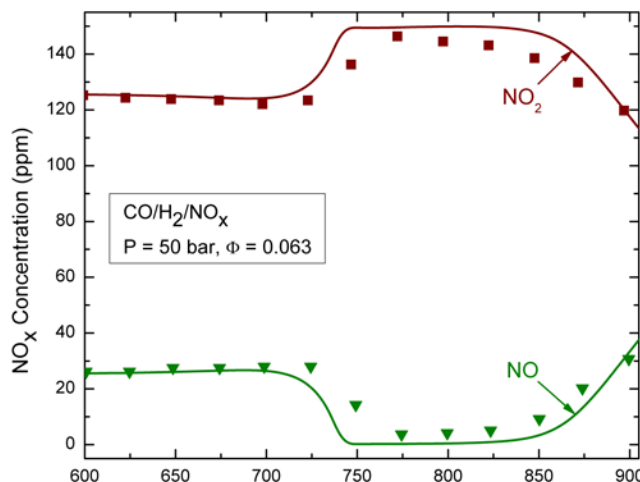
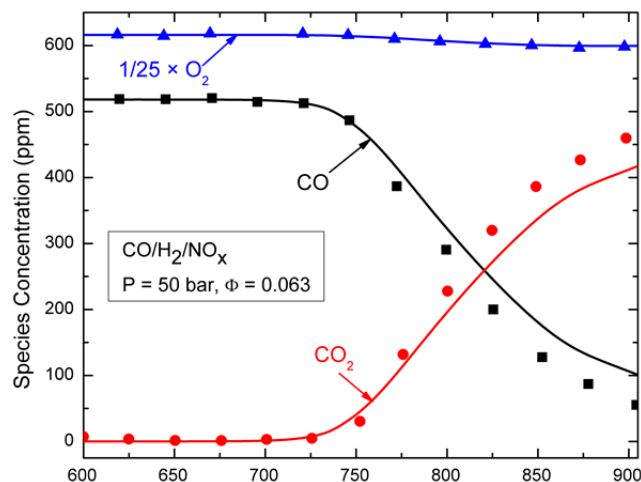
# Model Performance: Variable Initial Conditions for CO/H<sub>2</sub>O/O<sub>2</sub>/NO System

## Variable Initial Pressure



- ✓ Model reasonably predicts the experimental trends with variable initial pressure
- ✓ Complete NO-NO<sub>2</sub> interconversion without any formation of molecular nitrogen

# Model Performance: PFR Species Evolution for CO/H<sub>2</sub>/NO<sub>x</sub> Oxidation System



✓ Flow reactor experiments at constant mass flow rate with temperature dependent residence time<sup>1</sup>

Pressure ↑

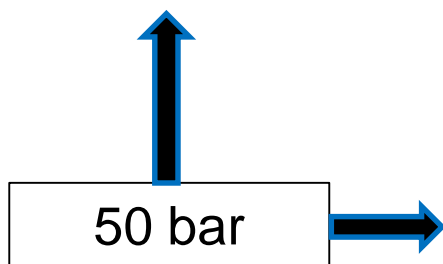
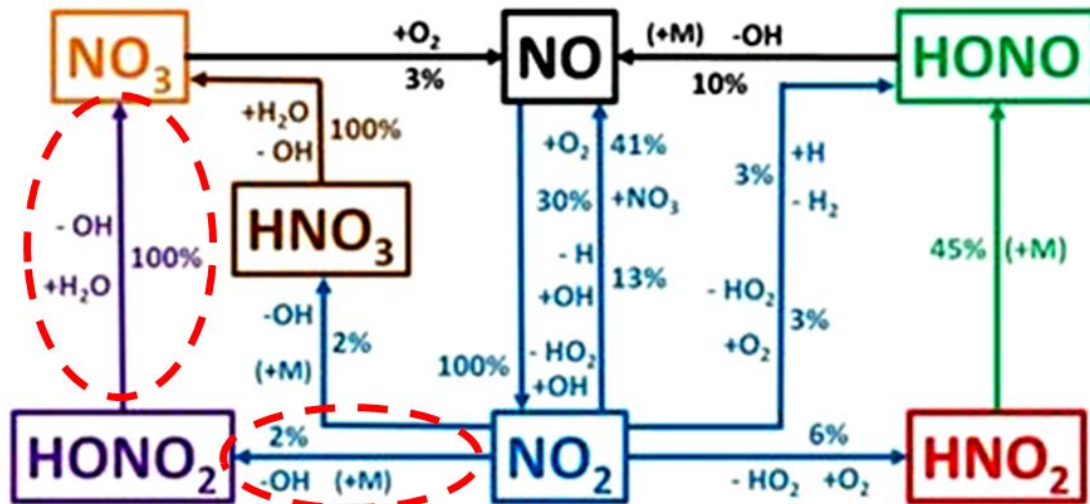
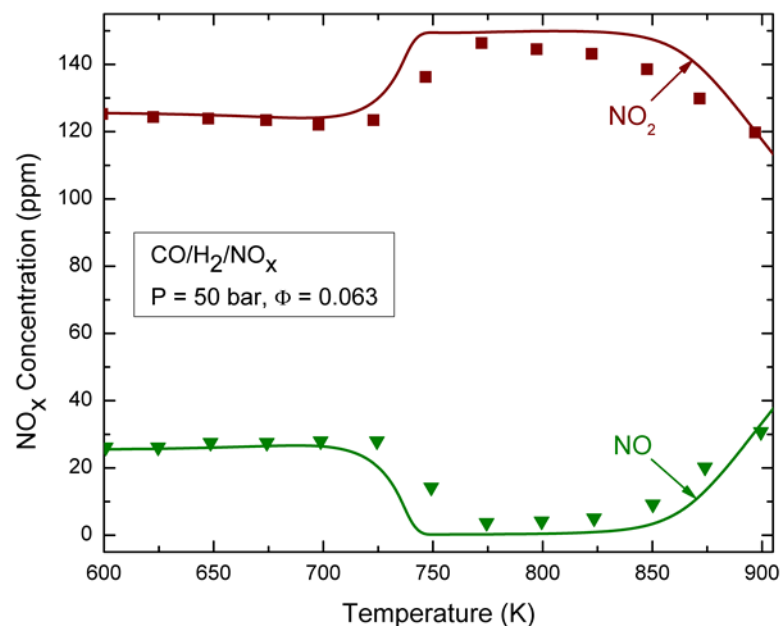
$$\tau_{20 \text{ bar}} = 2350/T$$

$$\tau_{50 \text{ bar}} = 6030/T$$

✓ Reasonable predictions for CO-CO<sub>2</sub> and NO-NO<sub>2</sub> conversion



# Proposed Model Performance: PFR Species Evolution for CO/H<sub>2</sub>/NO<sub>x</sub> Oxidation System



**Dominance of pressure-dependent reactions: two additional NO ↔ NO<sub>2</sub>**



# Summary



- $C_0 - C_4/NO_x$  model has been developed
- $H_2/CO/NO_x$  model has been validated
- Influence of trace impurities on combustion characteristics
- Trace  $NO_x$  – emittents can alter the combustion behavior, global/optimized models can not capture intricate features



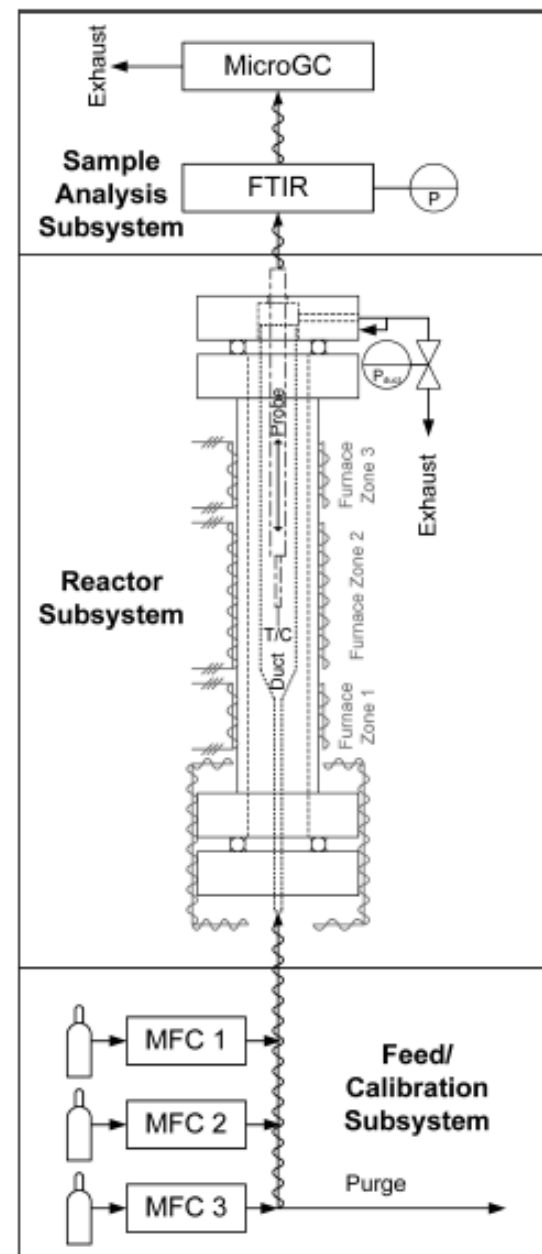
# Measurements of $\text{NO}_x$ perturbed oxidation experiments

# Influence of Trace Nitrogen Oxides on Natural Gas Oxidation

## Nominal Feed Condition

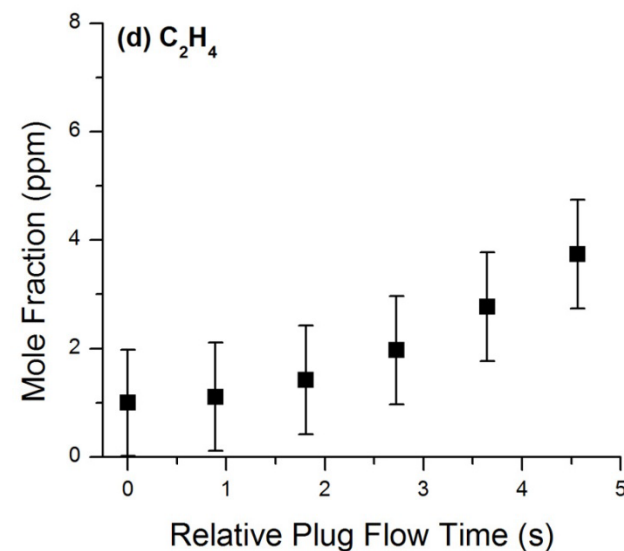
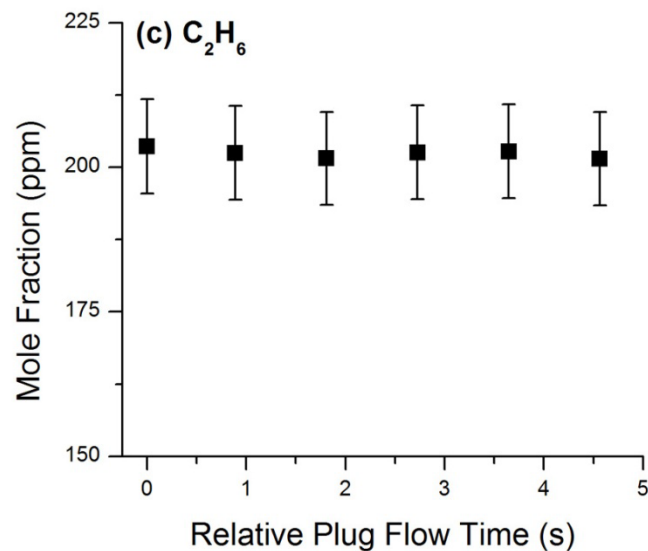
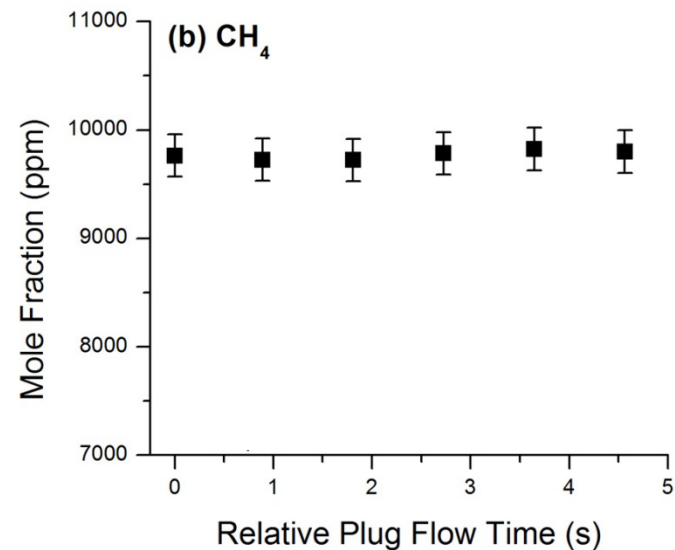
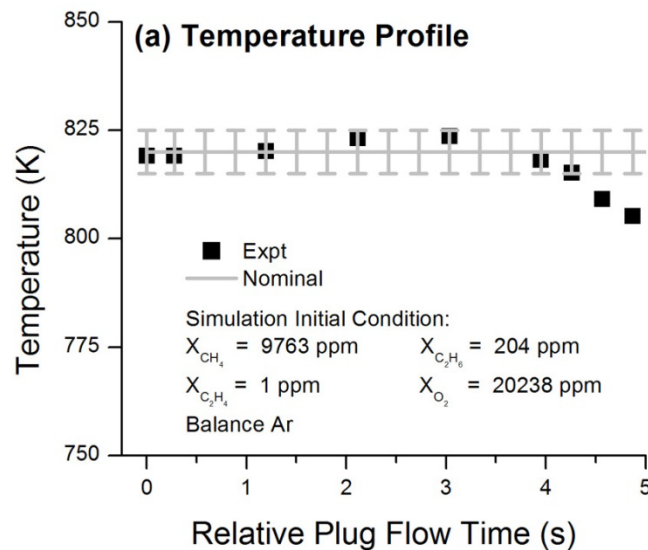
|                        |   |
|------------------------|---|
| $\text{CH}_4$          | = 9800 ppm ( $\pm \sim 2\%$ )                     |
| $\text{C}_2\text{H}_6$ | = 200 ppm ( $\pm \sim 4\%$ )                      |
| $\text{O}_2$           | = 10150 / 20300 /<br>40600 ppm ( $\pm \sim 2\%$ ) |
| $\phi$                 | = 2.0 / 1.0 / 0.5                                 |
| Ar                     | = Balance   |
| $Q_{\text{total}}$     | = 1300 sccm                                       |
| NO                     | = 25 ppm ( $\pm 1$ ppm)                           |
| T                      | = $819 \pm 5$ K                                   |

**P = 10 atm**  
**T = 820 K**



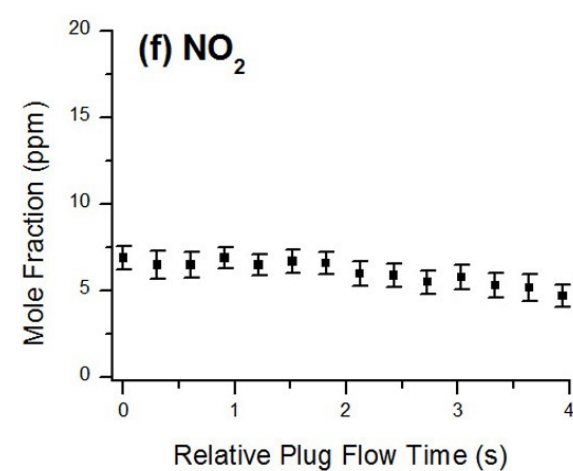
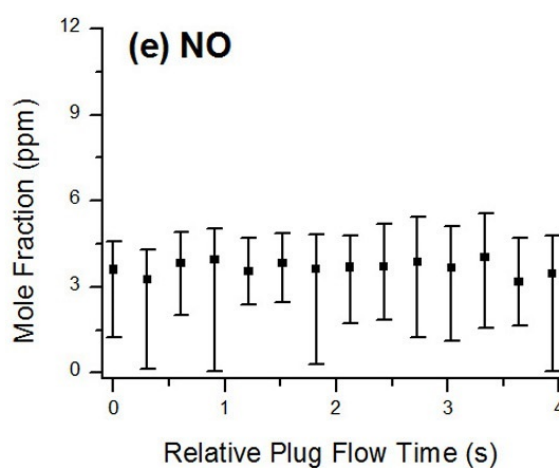
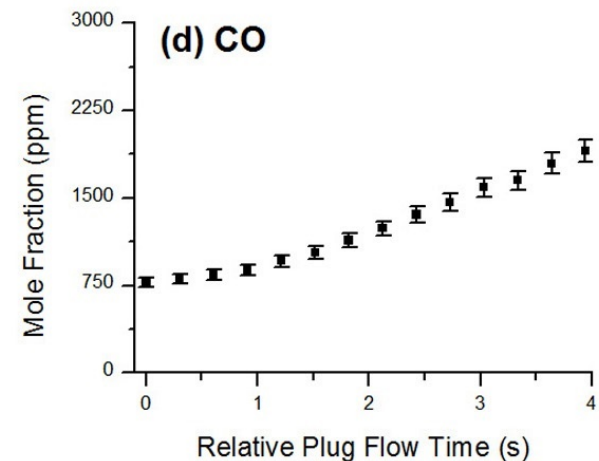
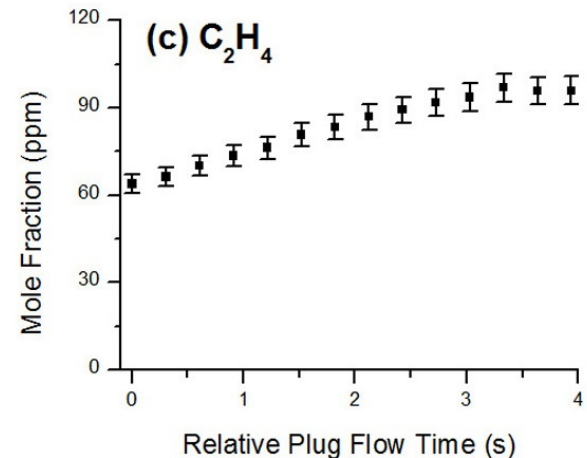
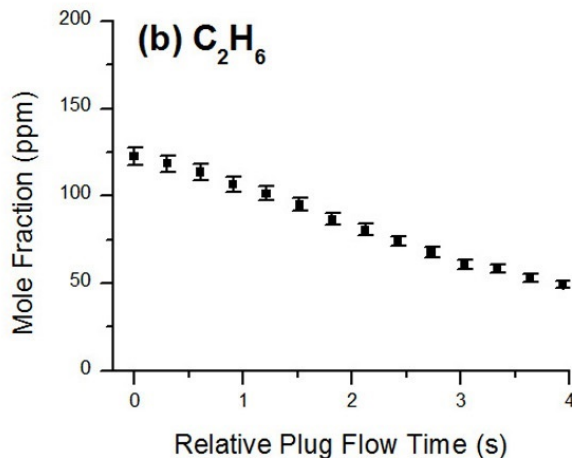
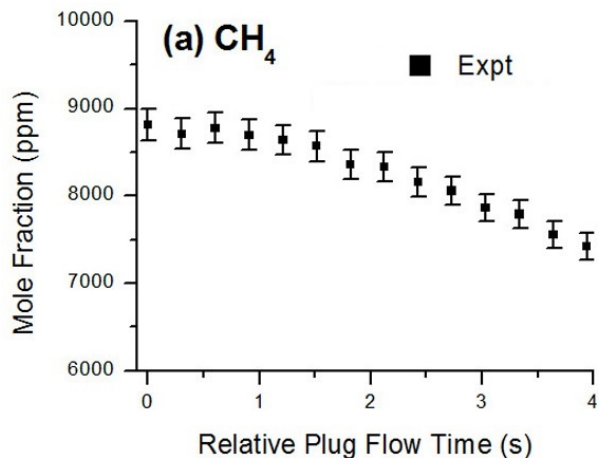
# Non-NO<sub>x</sub> Perturbed case ( $\phi = 1.0$ )

- No evidence of reaction for measured profiles of CH<sub>4</sub>, and C<sub>2</sub>H<sub>6</sub>.
- Few ppm of C<sub>2</sub>H<sub>4</sub> quantified @ distinct 950 cm<sup>-1</sup> FTIR wave number.
- Conditions of incipient of reactions. C<sub>2</sub>H<sub>6</sub> oxidation via flux through C<sub>2</sub>H<sub>5</sub> ⇌ C<sub>2</sub>H<sub>4</sub>.



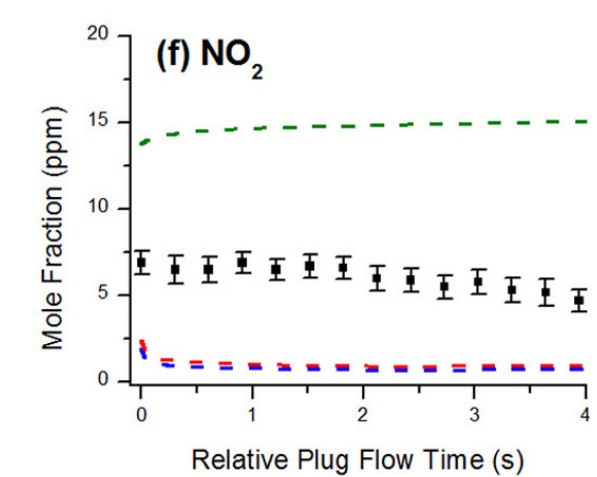
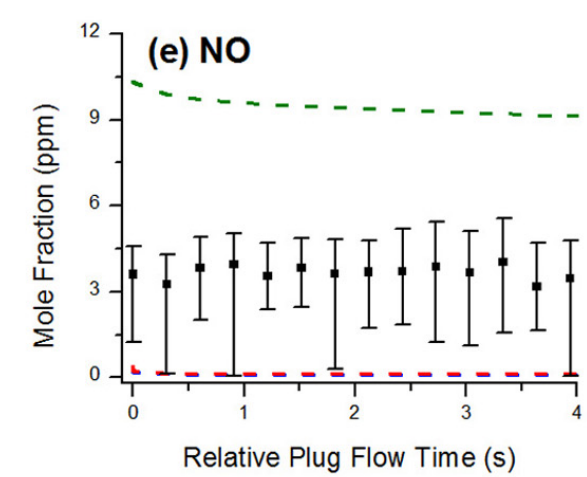
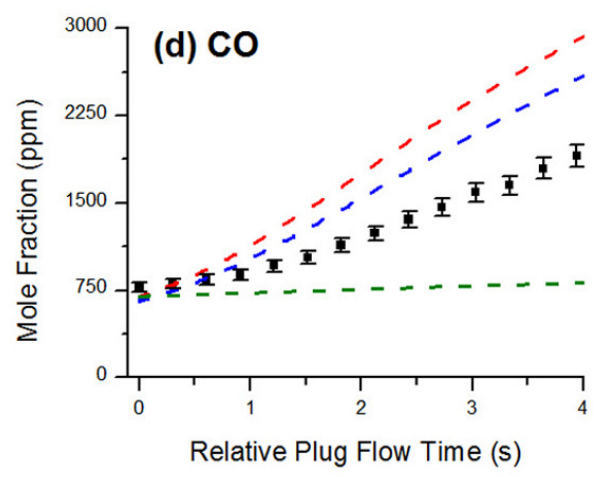
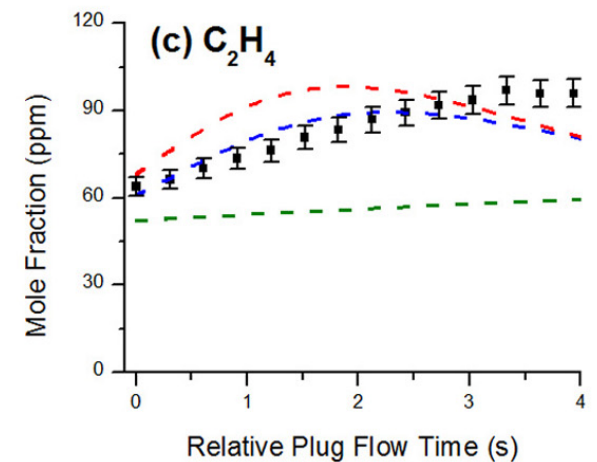
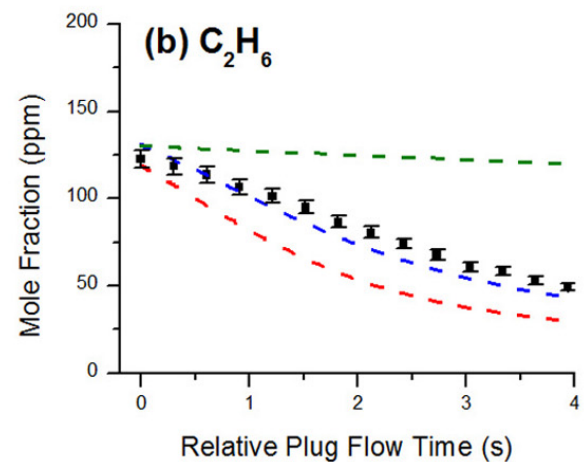
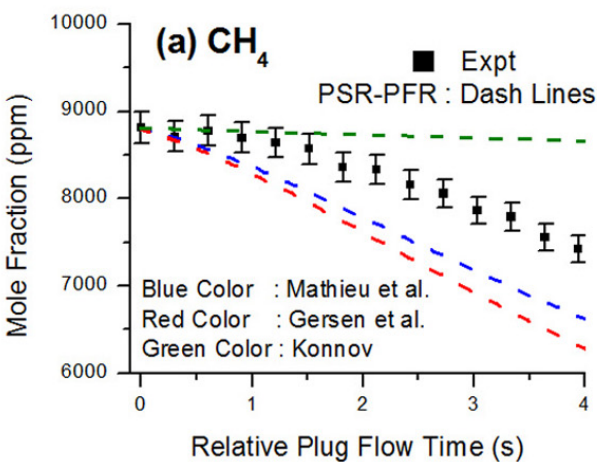
# Trace $\text{NO}_x$ Perturbed Case ( $\varphi = 1.0$ )

Reactivity induced due to trace  $\text{NO}_x$  (~ 25 ppm)

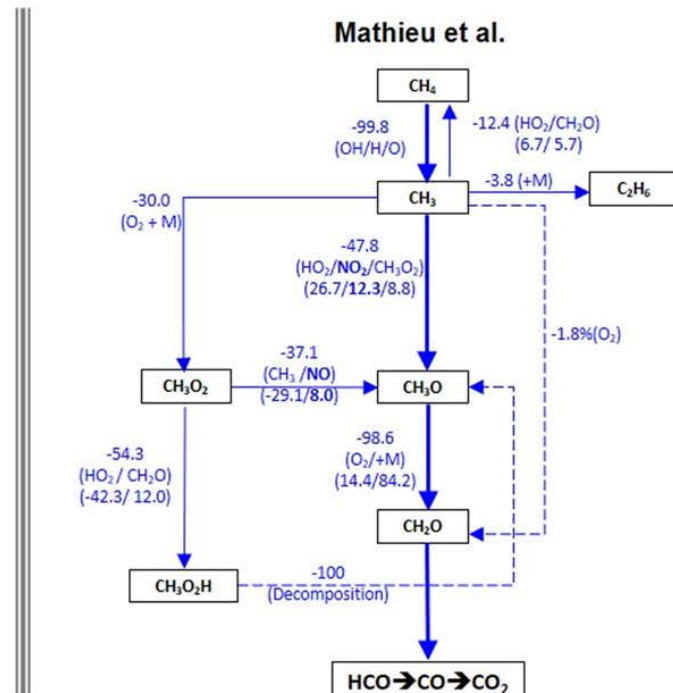
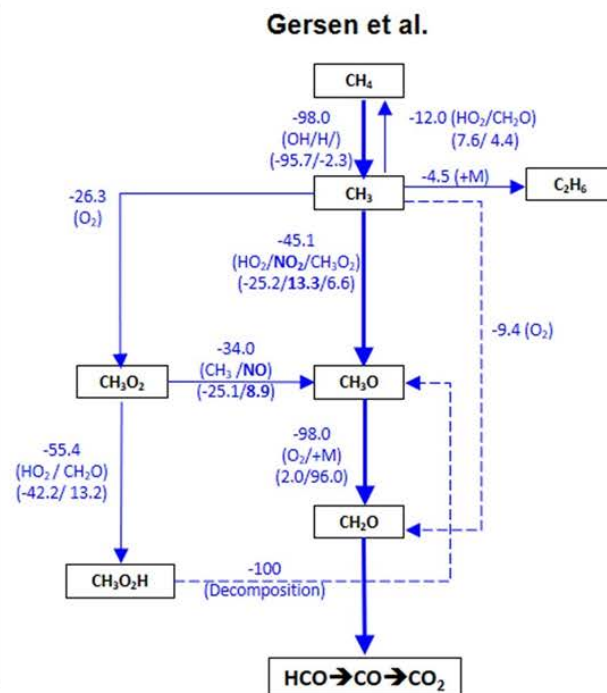
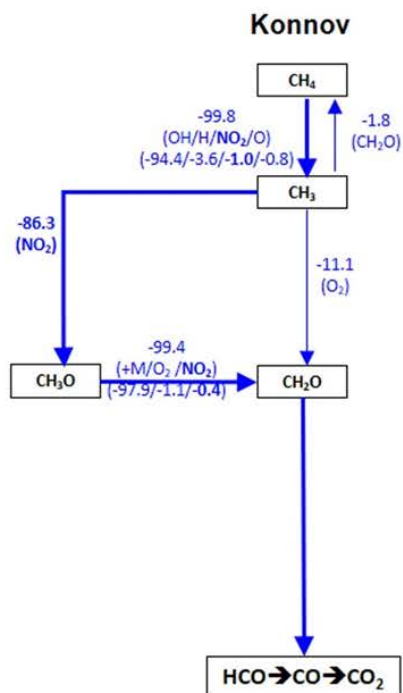


# Trace NO<sub>x</sub> Perturbed Case ( $\varphi = 1.0$ )

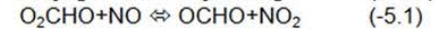
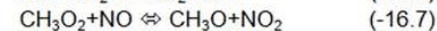
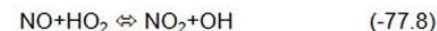
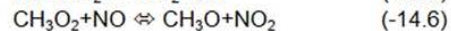
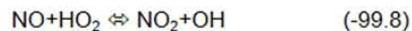
NO<sub>x</sub> mole fraction predictions indicated near-complete destruction of NO<sub>x</sub> (NO+NO<sub>2</sub>) → CH<sub>3</sub>NO<sub>2</sub>



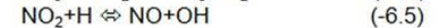
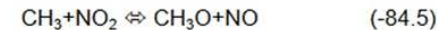
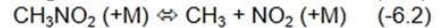
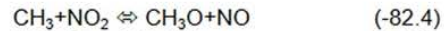
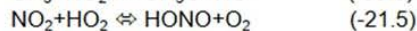
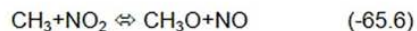
# Kinetic Analysis – Path Flux ( $\varphi = 1.0$ )



## Dominant NO Consumption Pathways

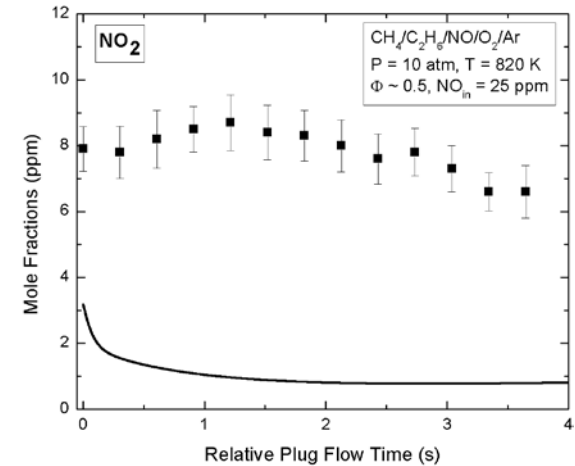
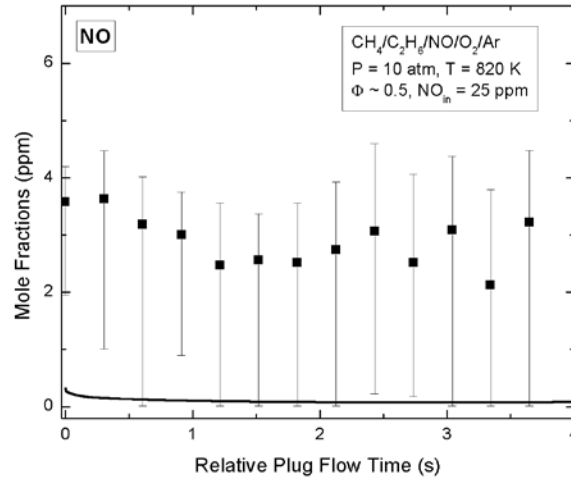
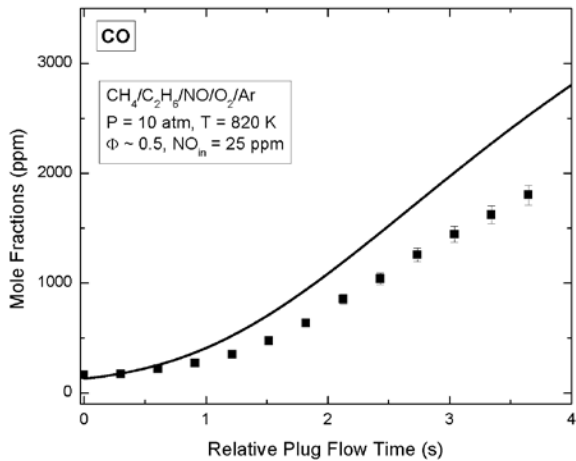
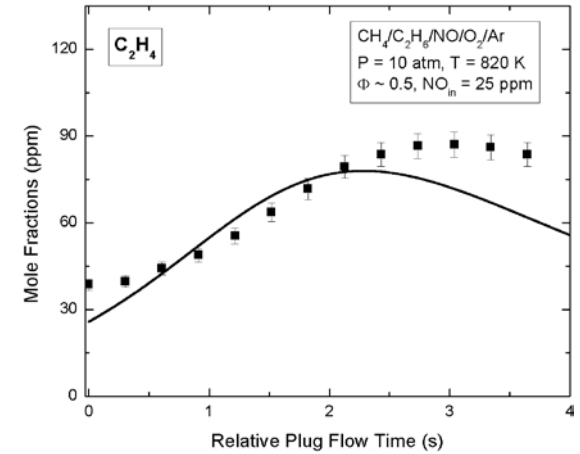
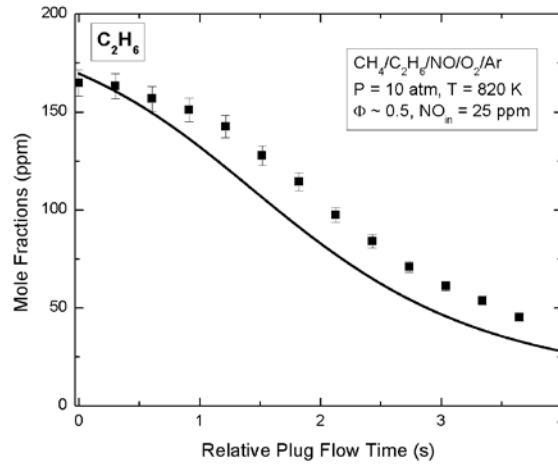
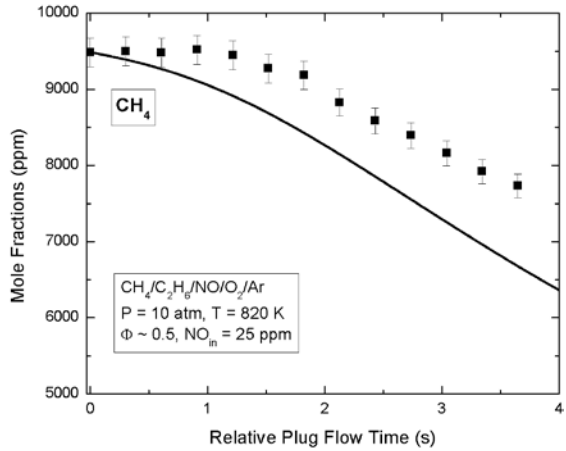


## Dominant NO<sub>2</sub> Consumption Pathways



# Current Model Predictions

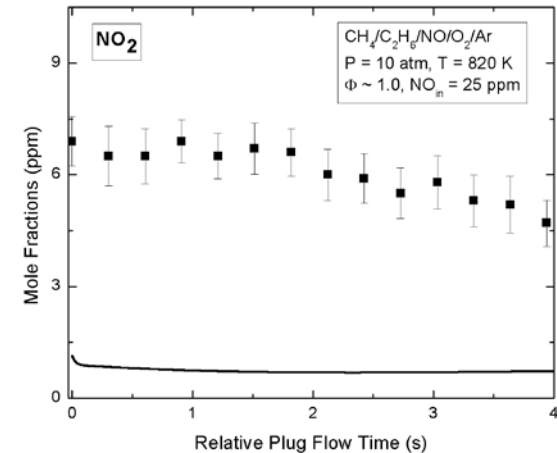
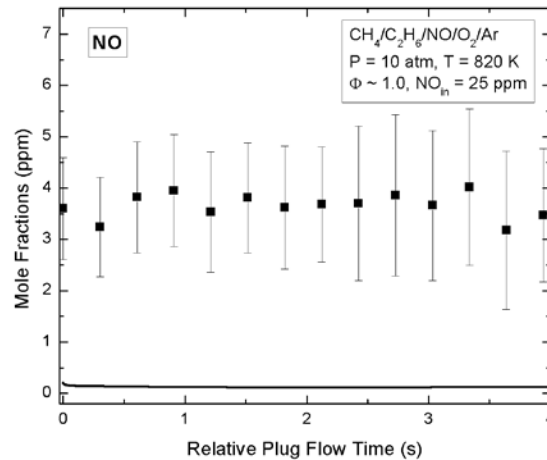
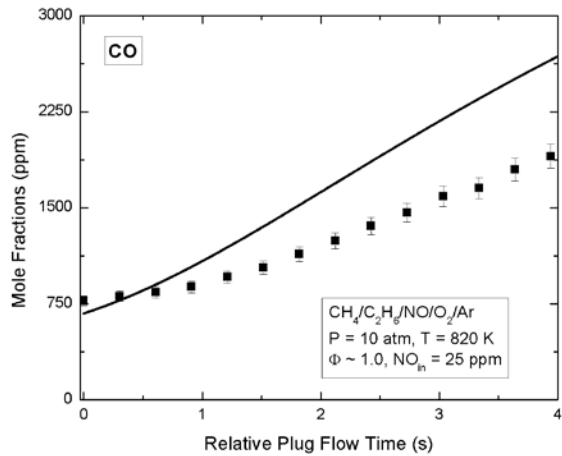
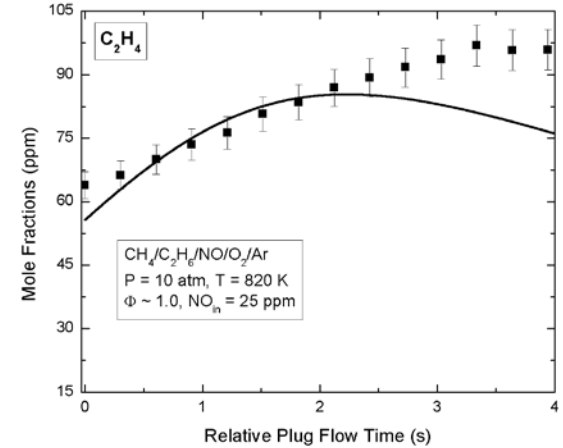
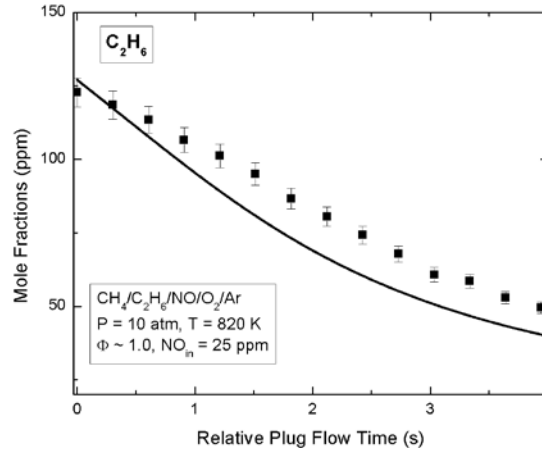
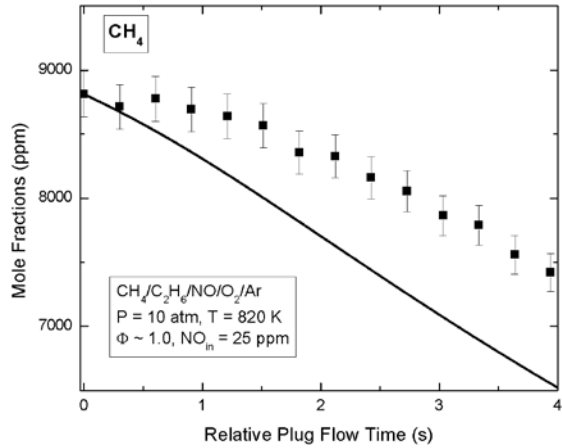
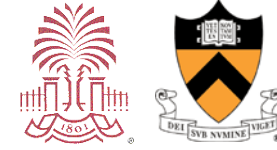
## Trace $\text{NO}_x$ Perturbed Case ( $\phi = 0.5$ )





# Current Model Predictions

## Trace $\text{NO}_x$ Perturbed Case ( $\phi = 1.0$ )



# Summary

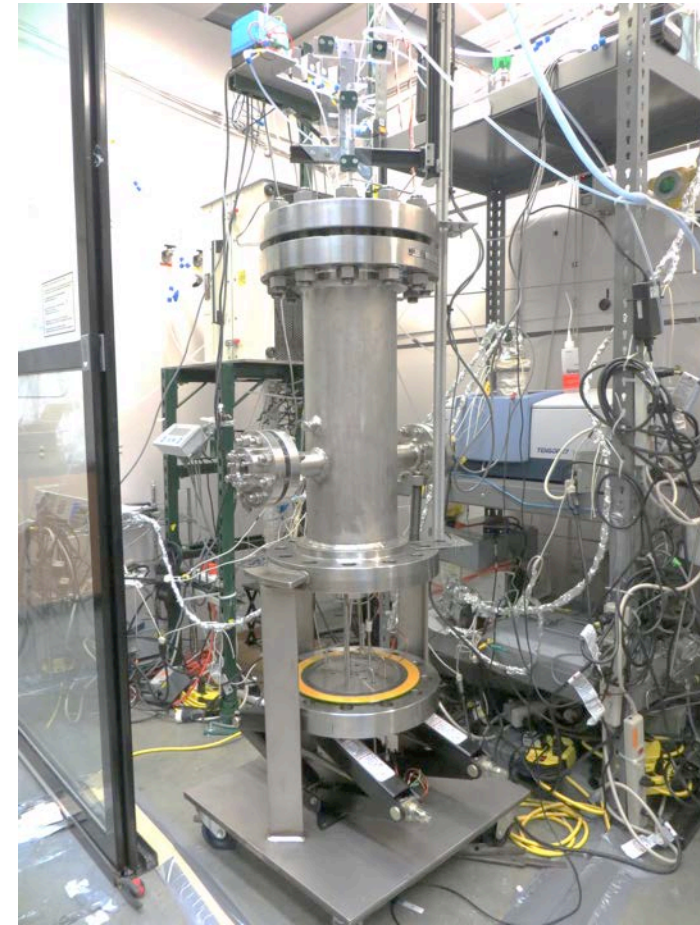
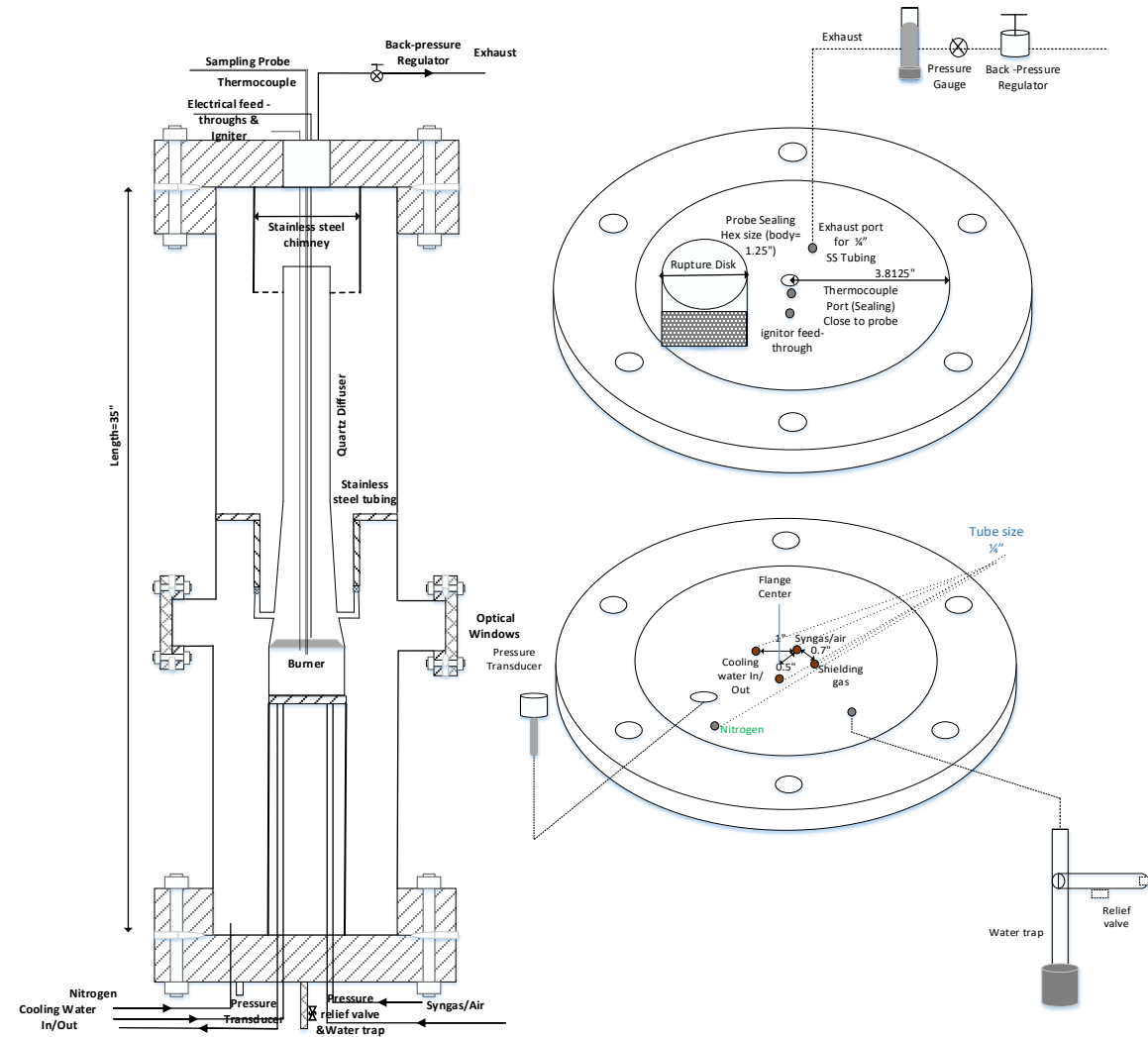


- Influence of trace impurities on combustion characteristics.
- Performance of existing model has been analyzed and inclusions were proposed and incorporated in the present model to include/predict the influence of trace emittents .

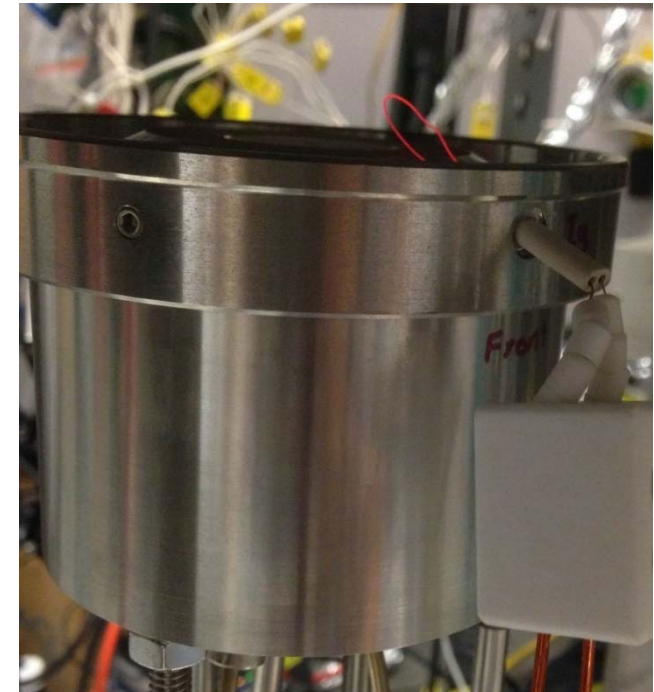
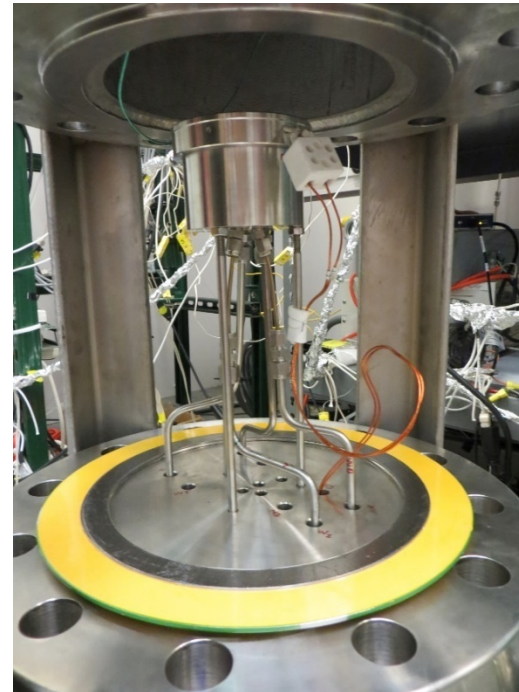
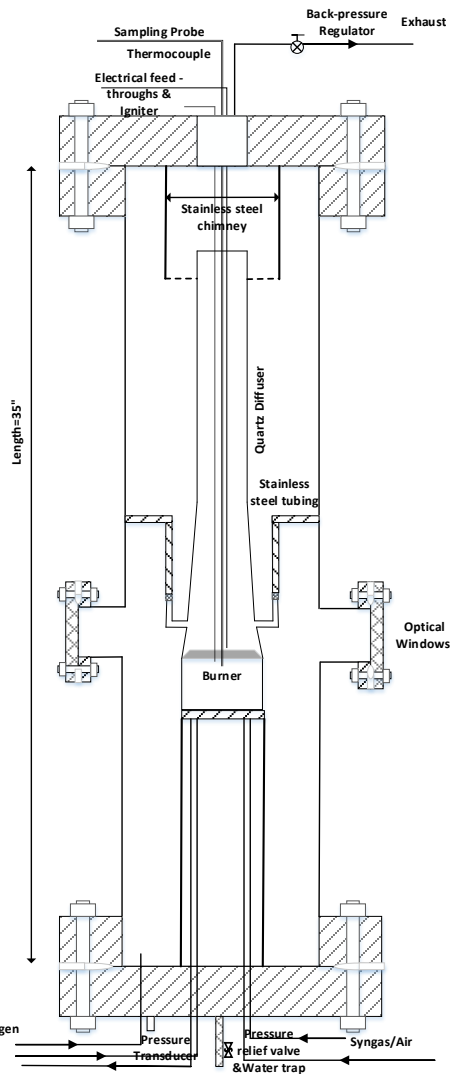


# Experiments for Speciation Measurements and Multidimensional CFD Modeling

# High Pressure Reactor System

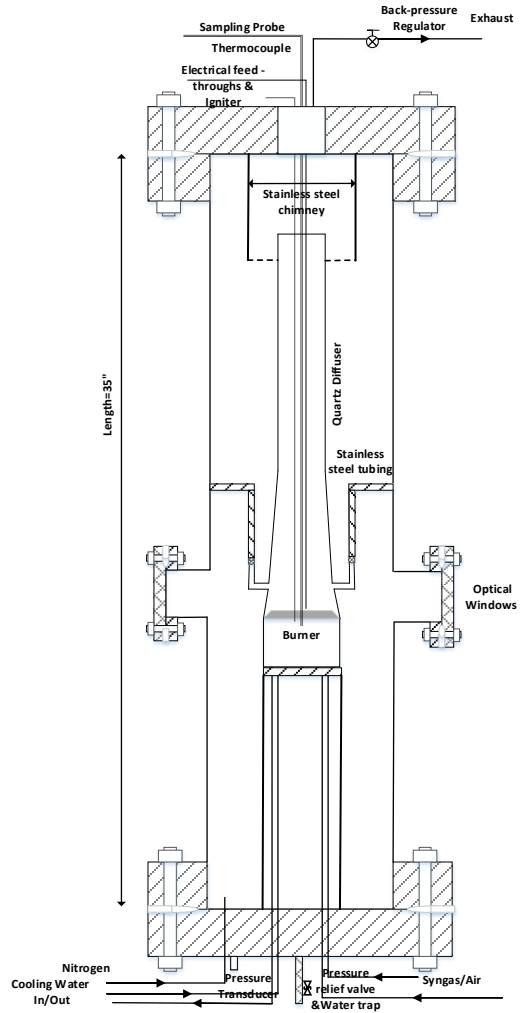


# High Pressure Reactor System

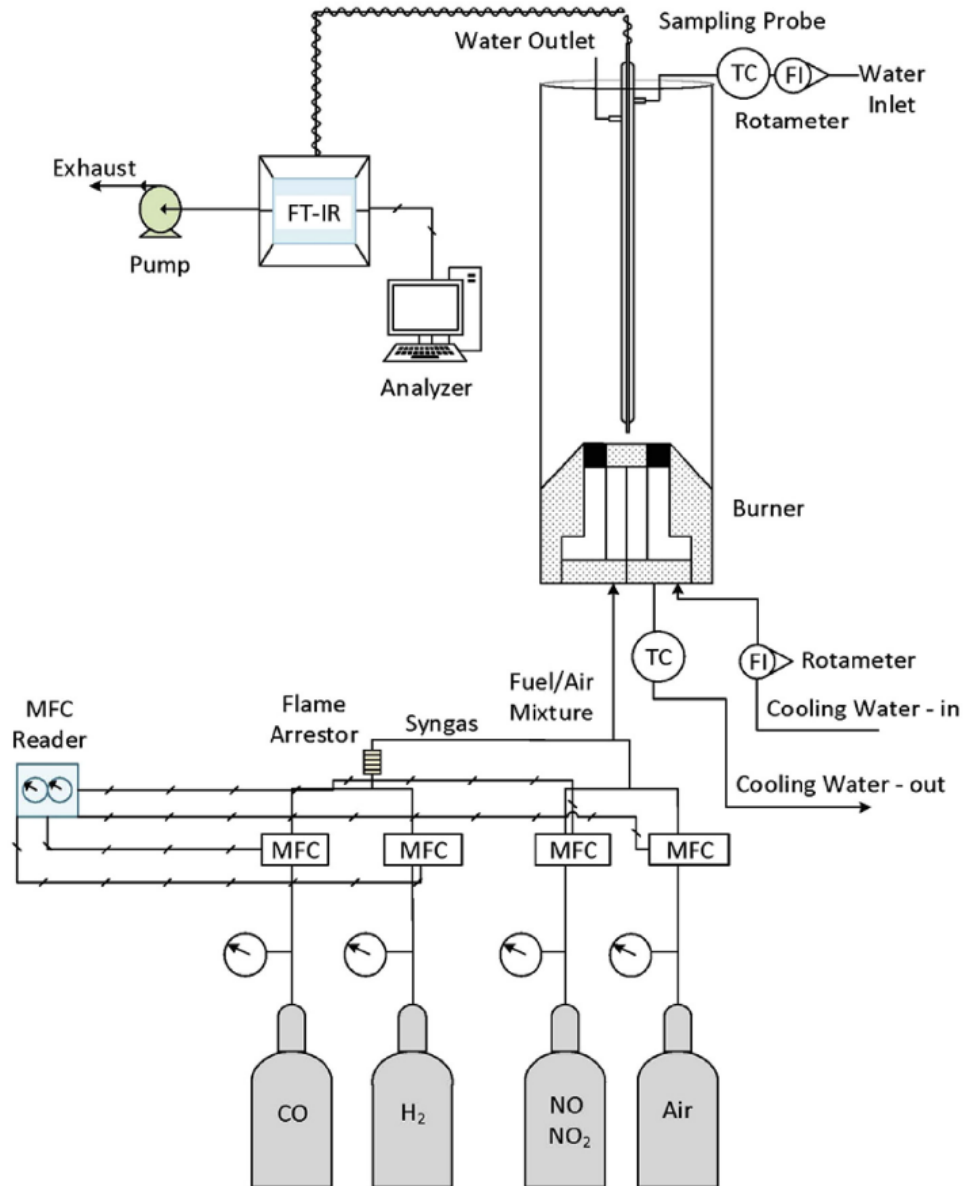




# High Pressure Reactor System



# Schematic of the Experimental Setup



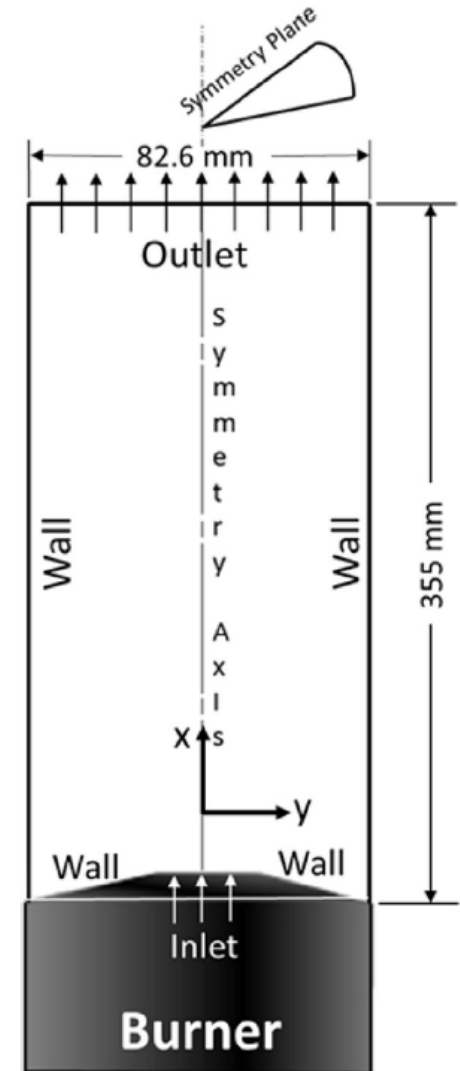
- Quartz glass probe for measuring species distribution in the reactor (axial and radial profiles)
- Thermocouple probe for measuring the temperature distribution

# Multi-dimensional Laminar Reacting Flow Modeling

- Experiments were simulated using an in-house multi-dimensional laminar reacting flow model which solves the conservation equations.
- Two-dimensional axi-symmetric analysis of syngas/ $\text{NO}_x$  oxidation in the McKenna burner and its associated tube arrangement was performed adopting the open-source OpenFOAM® framework.
- Detailed syngas/ $\text{NO}_x$  oxidation chemistry was employed in the simulation which includes 77 species and 442 elementary reactions.

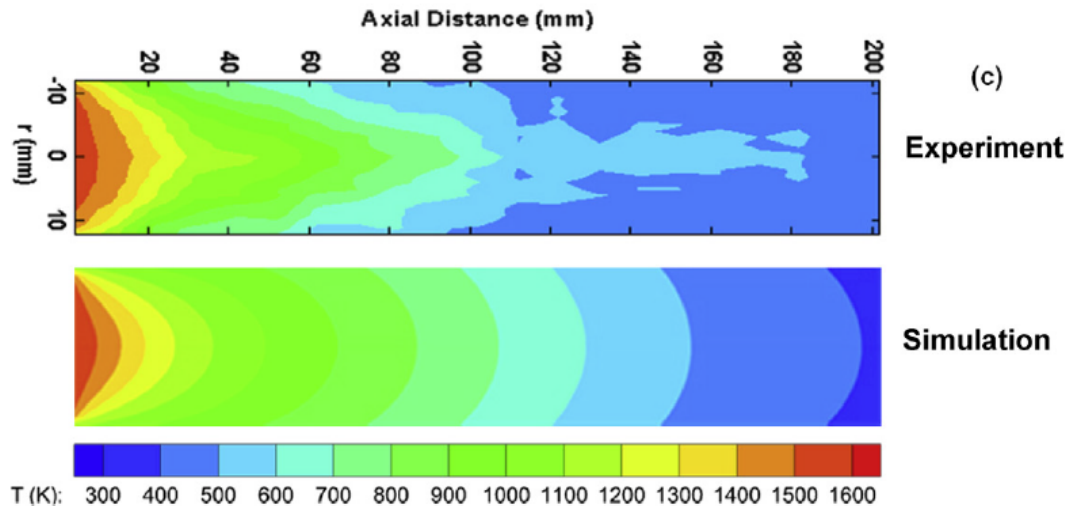
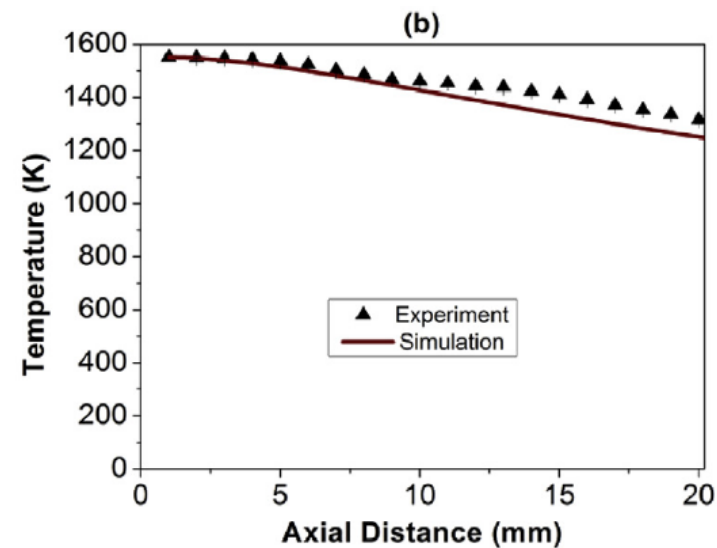
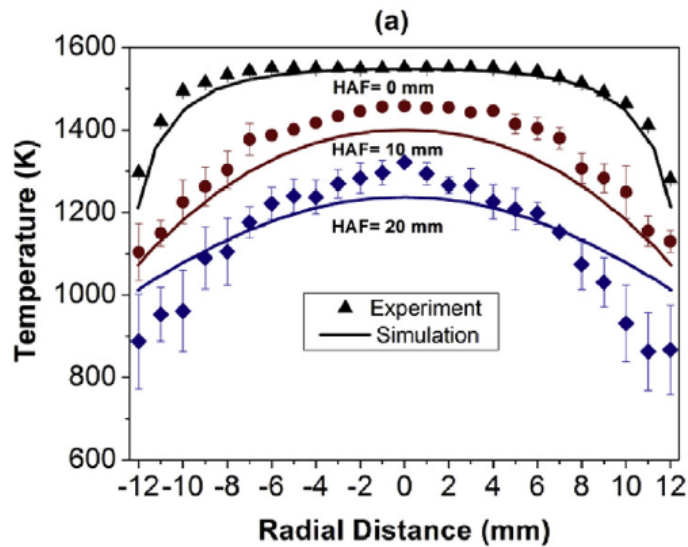
## POST FLAME MODEL - REACTIVITY

- The McKenna burner itself is not computationally resolved instead the post flame reactivity is modeled.
- The post flame combustion products obtained from the CHEMKIN PRO burner stabilized module were provided as the inlet boundary conditions for this model.
- The wall temperature was prescribed to be room temperature (300 K).
- The experimental measurements of the centerline temperature and  $\text{NO}_x$  speciation were compared with the post flame modeling results.





# Measurements and Predictions

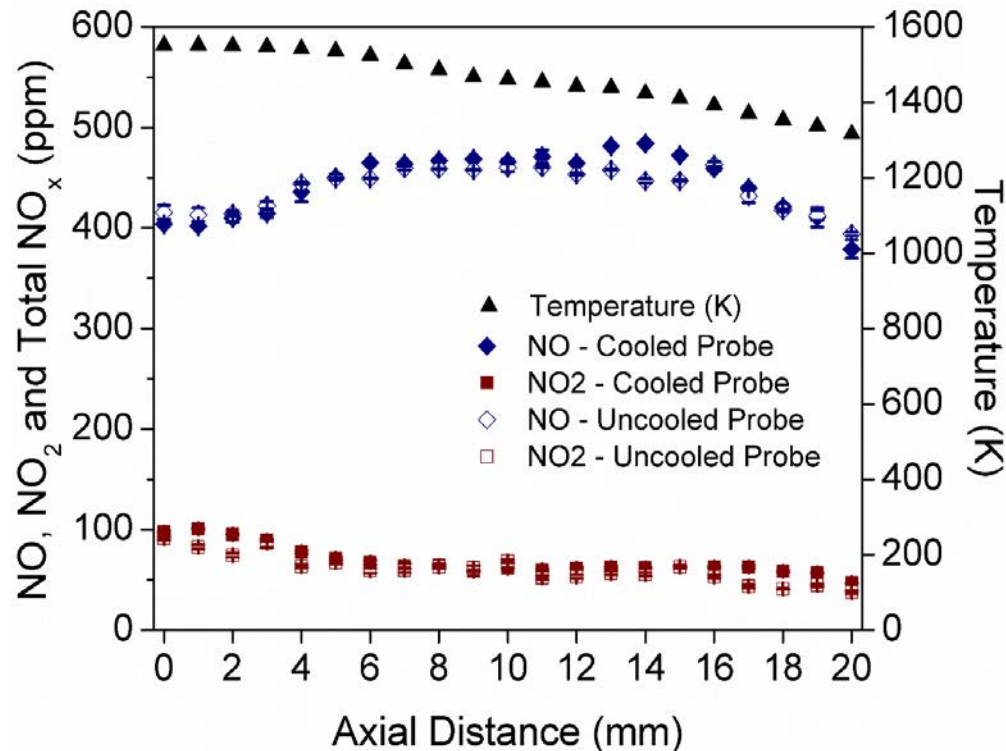


Measured and predicted a) radial temperature profiles at different height above the flame (HAF), b) centerline temperature profile and c) 2-D temperature contours for  $H_2/CO = 1$  and  $\phi = 0.5$ . The contour levels for the experiments and simulations are identical

# Experimental NO<sub>x</sub> Speciation Profile – Probe Effects

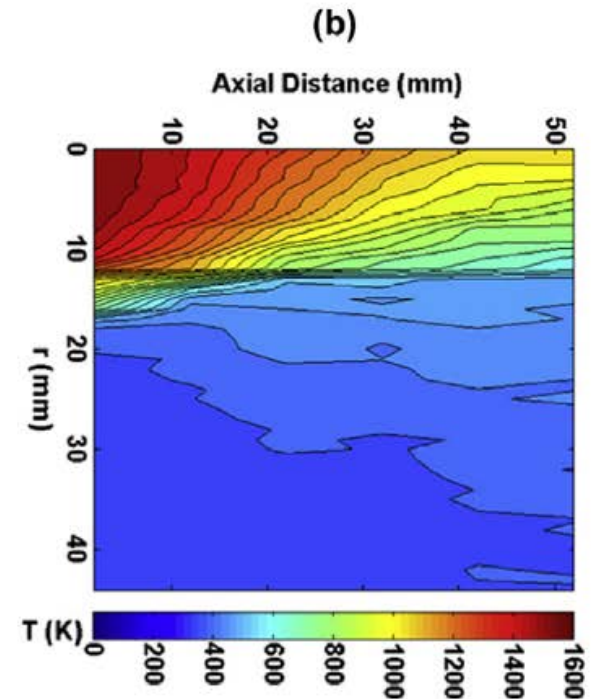
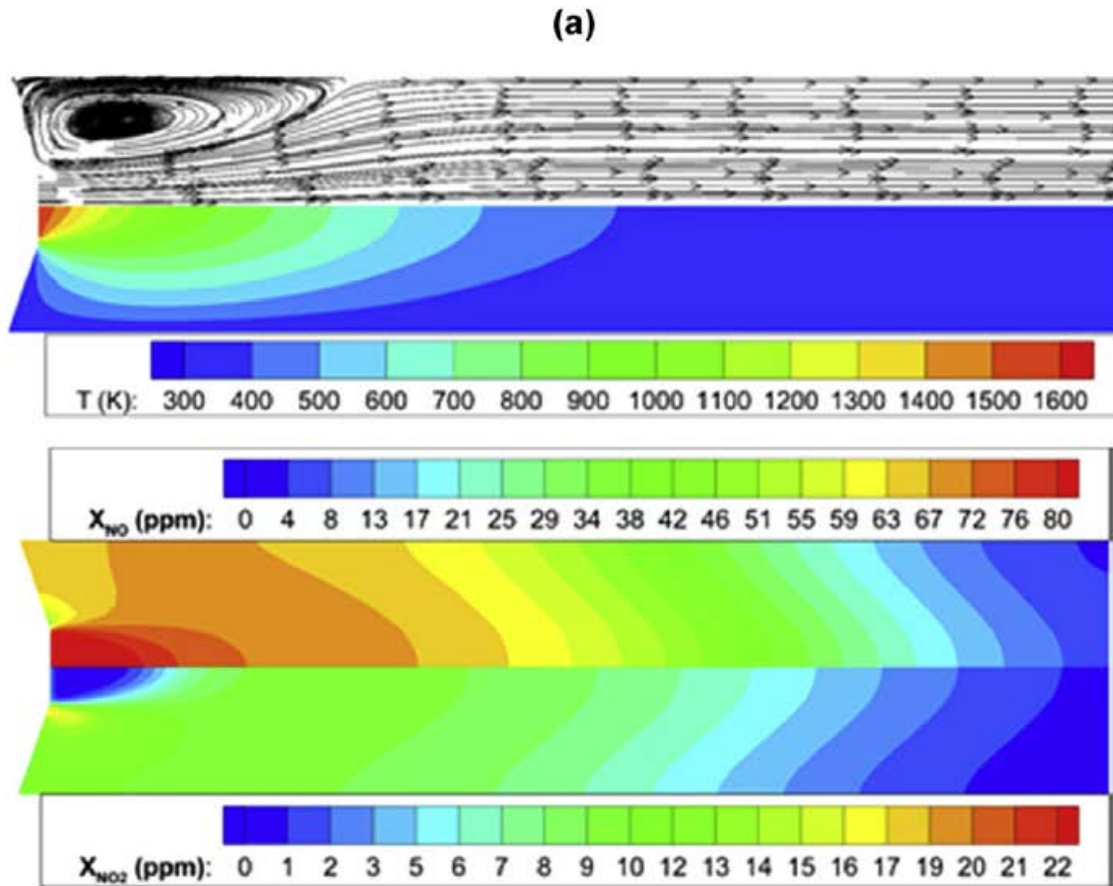
## Sampling with cooled probe vs. uncooled probe

H<sub>2</sub>/CO=1,  $\Phi$ =0.5, 500 ppm initial NO doping



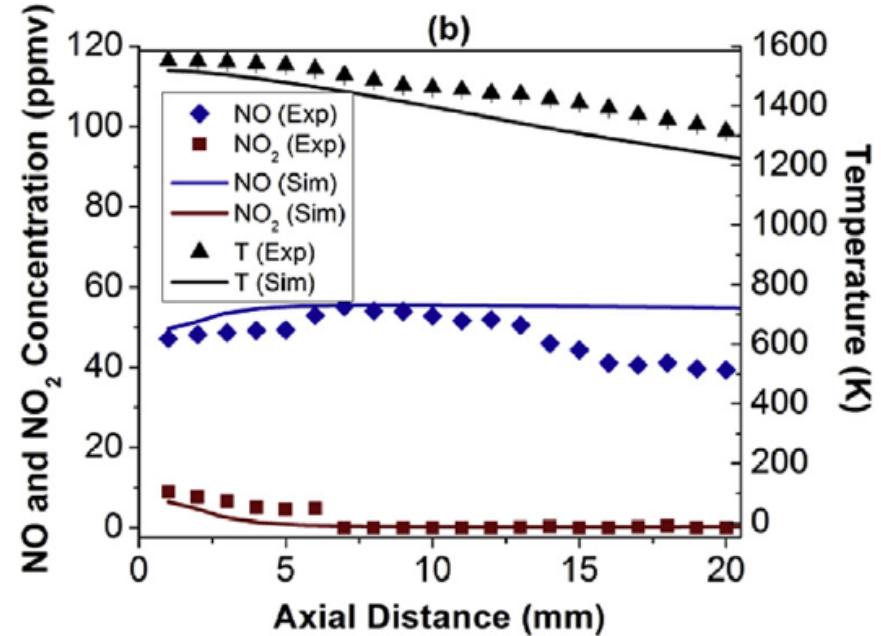
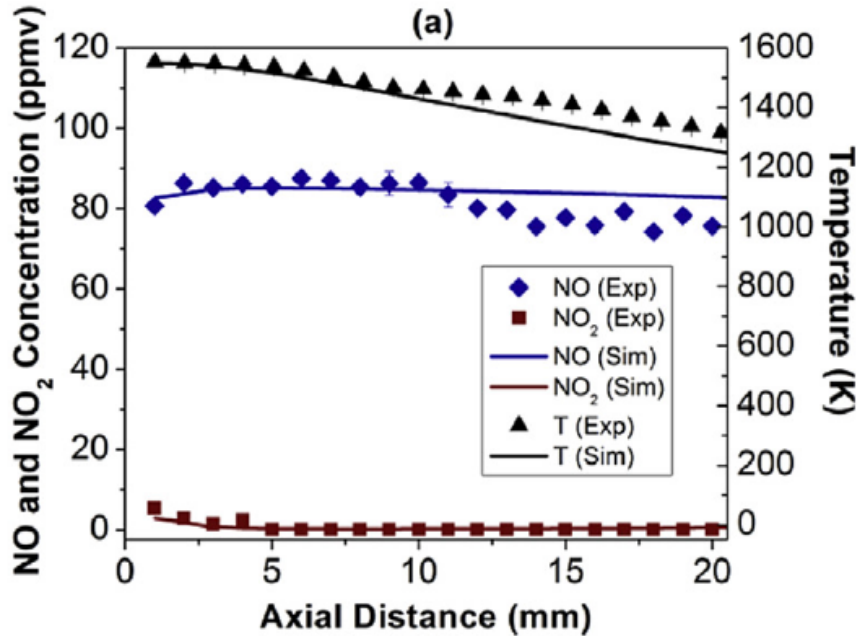
- Experiments were repeated with uncooled probe to see if there is any NO<sub>2</sub> formation in the sampling probe.
- Consistent results were obtained for both cooled and uncooled probes

# Measurements and Predictions



a) Temperature and NO/NO<sub>2</sub> concentration contours obtained from multi-dimensional simulations, and b) measured temperature contour for H<sub>2</sub>/CO = 1 and  $\phi = 0.5$ .

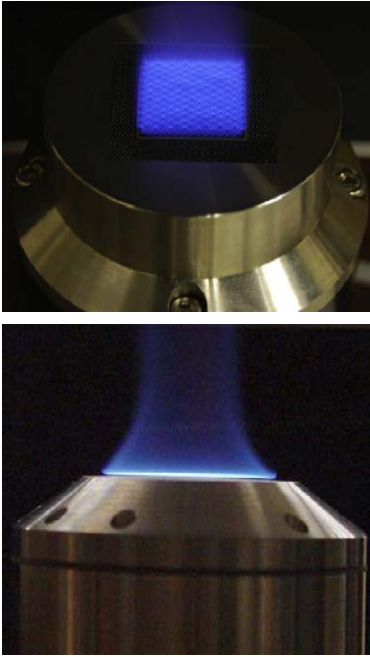
# Measurements and Predictions



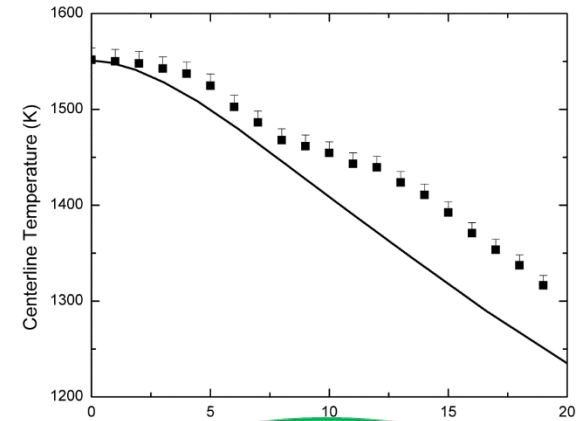
Measured NO<sub>x</sub> speciation and temperature data with multidimensional simulation predictions for H<sub>2</sub>/CO = 1 and  $\phi = 0.5$  with a) 100 ppm NO doping and b) 75 ppm NO<sub>2</sub> doping.

The model is able to predict the NO-NO<sub>2</sub> speciation in the post flame and also provide insight on the reaction processes contributing to the inter-conversion.

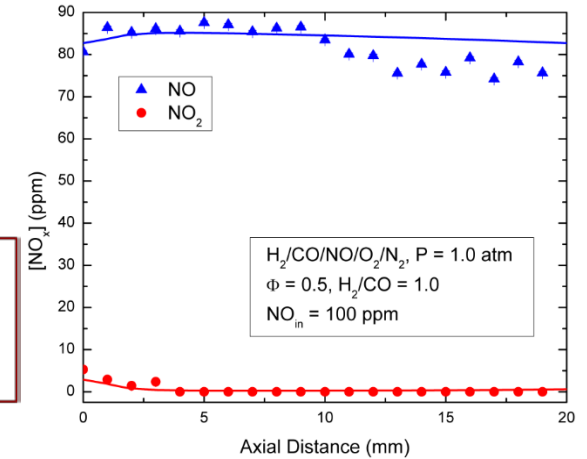
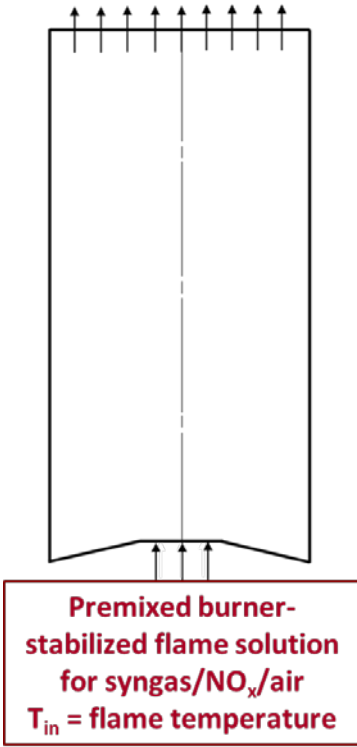
# Resolving the Flame and Post Flame Simultaneously



Post-flame simulation alone can not capture the initial  $\text{NO}_x$  recycling observed by the measurements



No initial  $\text{NO-NO}_2$  conversion



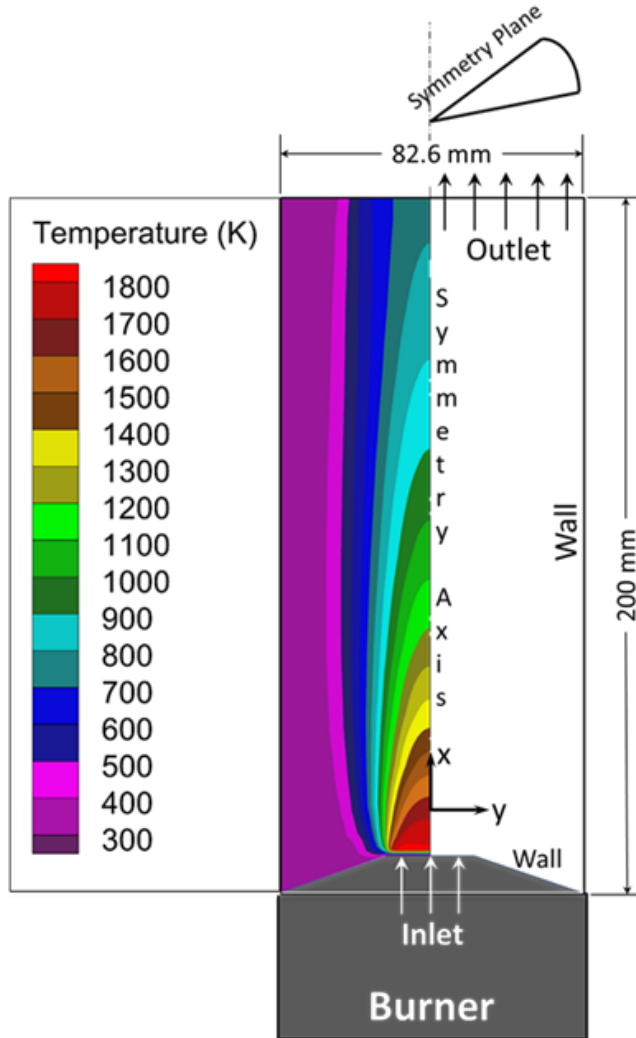
Initializing with burner-stabilized flame solution

Separate flame-post flame regimes of solution

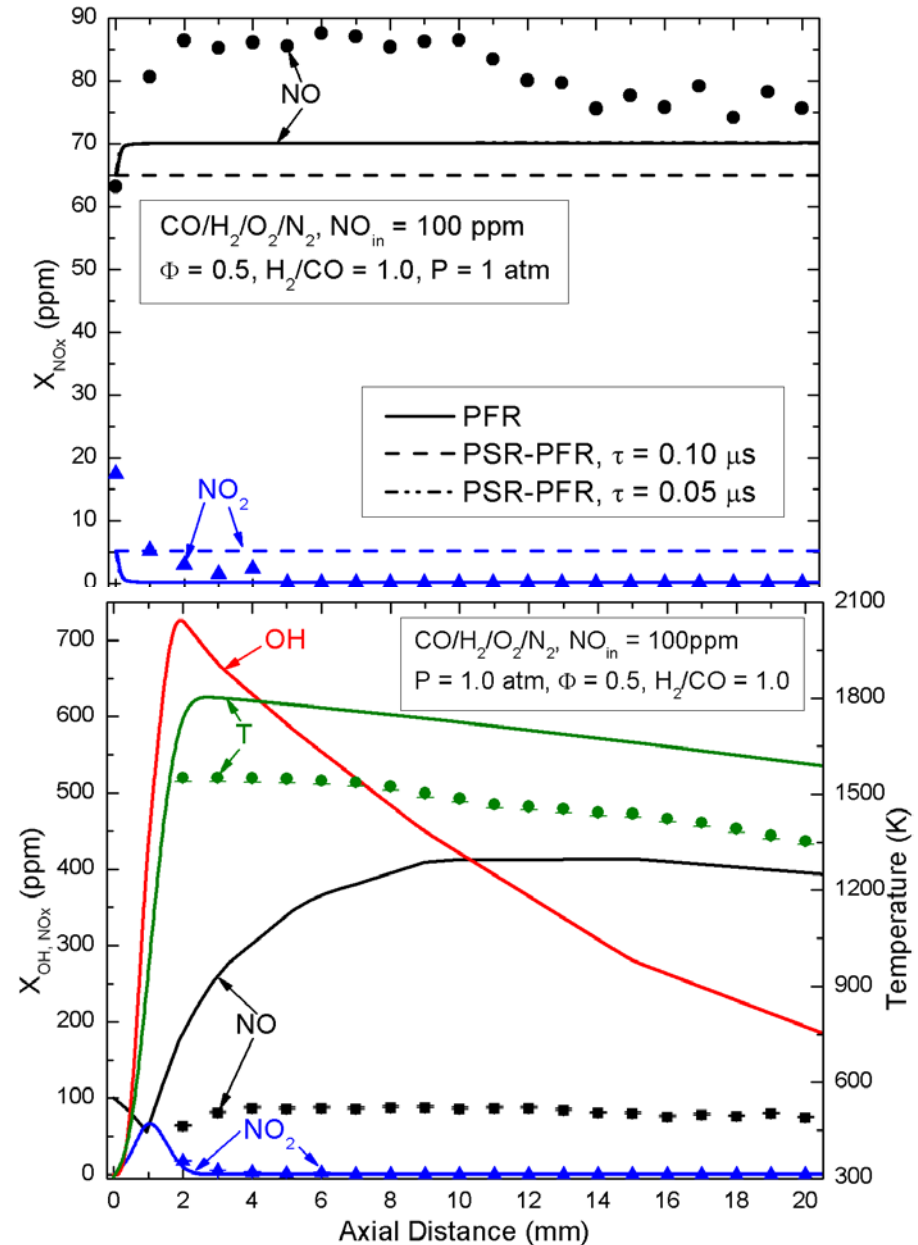
1-D flow reactor/tube modeling



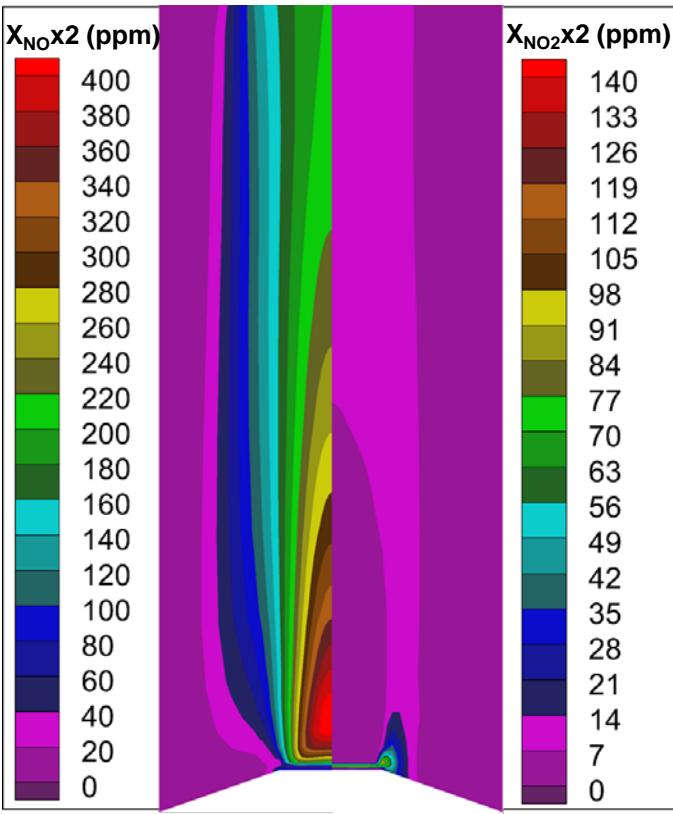
# Resolving the Flame and Post Flame Simultaneously



Schematic illustration of the computational domain of the burner-coupled model (right half) and the temperature field of the base case ( $\text{NO}_{\text{in}} = 100 \text{ ppm}$ )

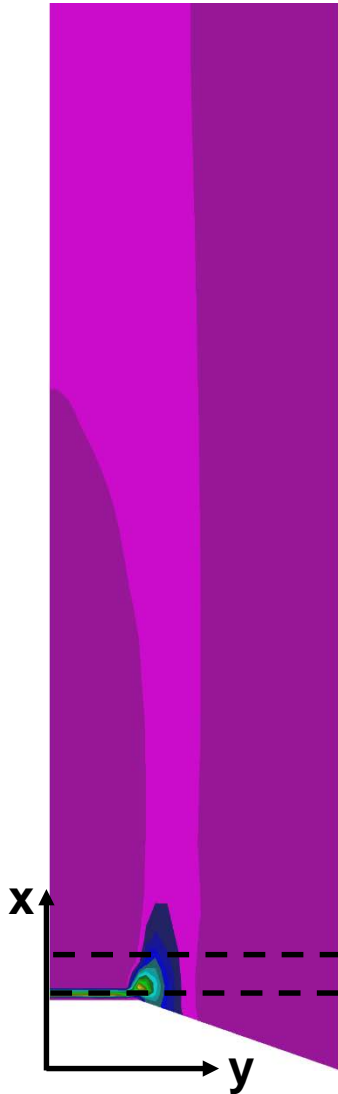
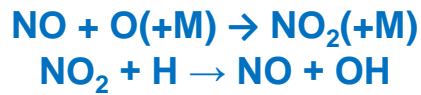


# Resolving the Flame and Post Flame Simultaneously

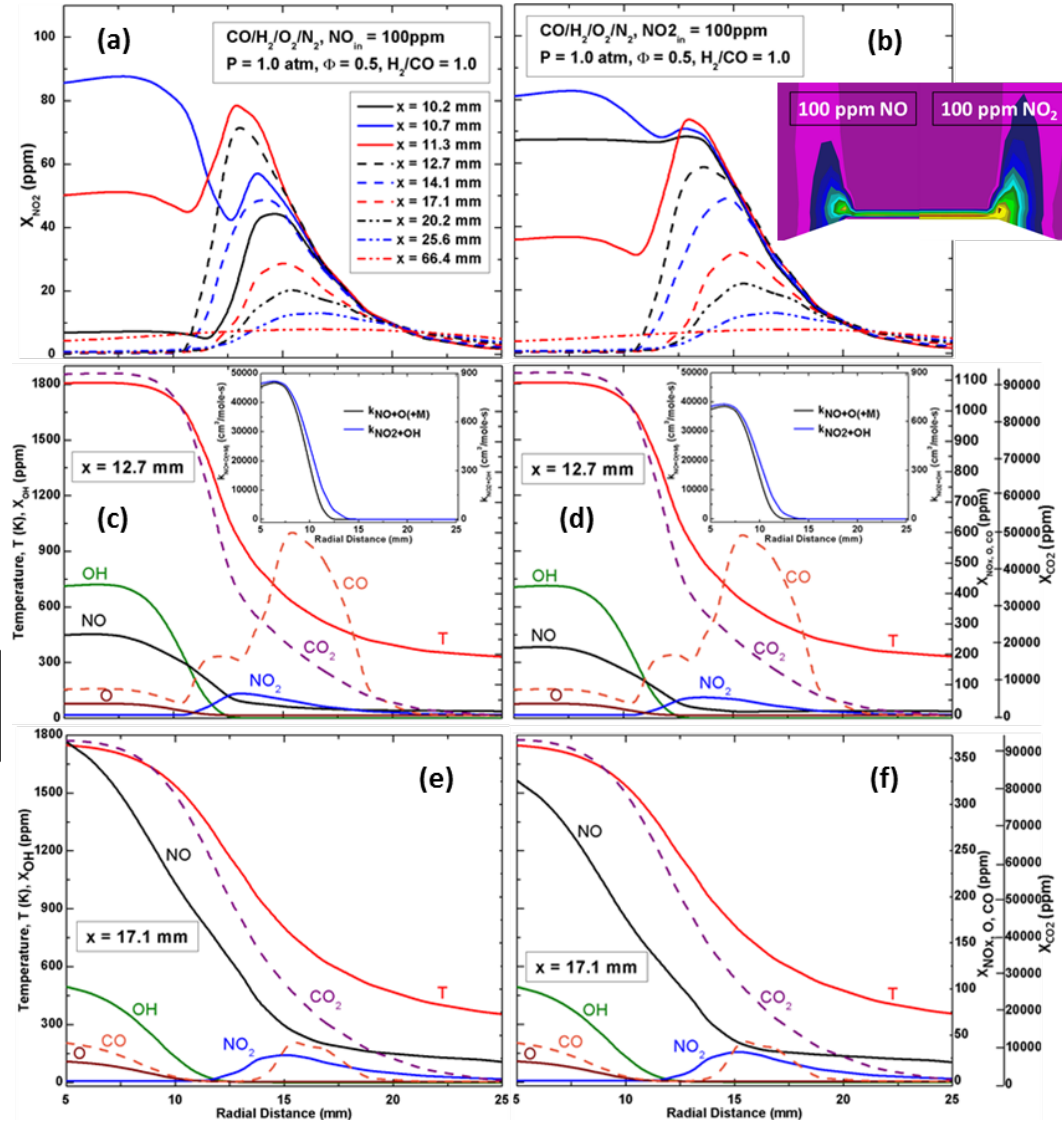


# Resolving the Flame and Post Flame Simultaneously

- NO-NO<sub>2</sub> partial equilibrium dominants at ≈850 K
- Presence of active radicals and non-participating wall



-X = 17.1 mm  
-X = 12.7 mm

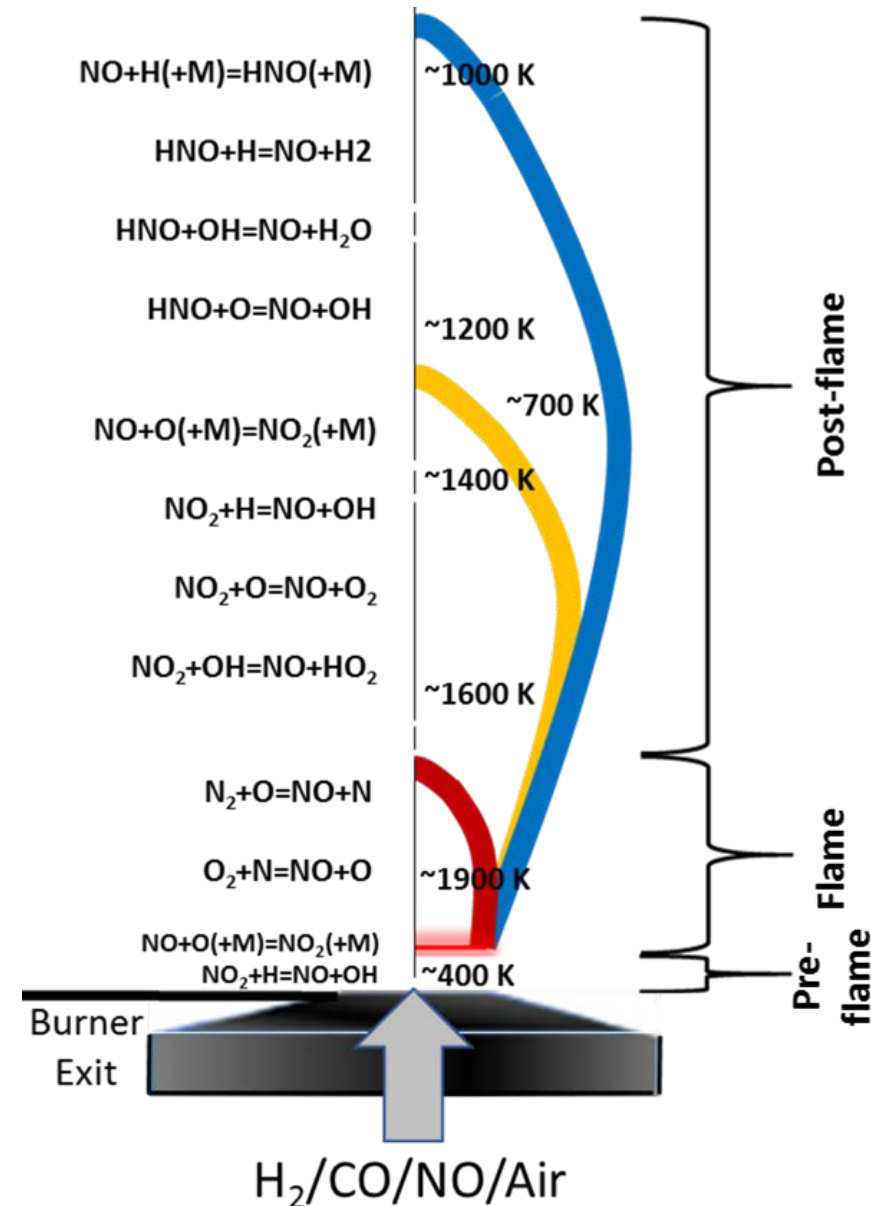




# Summary



- High pressure reactor to obtain speciation data under a wide range of conditions
- Multidimensional reactive flow model with detailed  $\text{NO}_x$  chemistry
- Resolve McKenna flame along with the post combustion region
- Capability to analyze  $\text{NO}_x$  formation in pre, post and flame locations
- $\text{NO}_x$  recycling not only a post flame phenomena
- Early  $\text{NO}_x$  recycling happens prior to the flame close to the inlet
- Reaction pathways vary for  $\text{NO}_x$  recycling at pre, post and flame locations



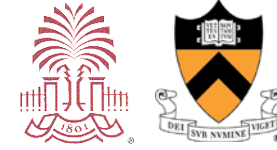
# Overall Summary



- $\text{NO}_x$  model for high hydrogen content fuel; model has been validated against a wide range of targets.
- $\text{NO}_x$  perturbed natural gas oxidation experiments conducted in a flow reactor configuration. Presence of trace  $\text{NO}_x$  significantly alters the oxidation behavior.
- Speciation data over a wide range of conditions were obtained.
- Multi-dimensional post flame CFD simulations. The model captures the post flame reactivity with the coupled transport and detailed kinetics.
- Multi-dimensional CFD+Kinetic model resolving, pre, flame and post flame region in a self consistent fashion.
- Model and simulations data are compared against experiments to assess the model performance and fidelity.



- Asgari, N., Ahmed, S., Farouk, T., Padak, B., “NO<sub>x</sub> formation in post flame gases from syngas/air combustion at atmospheric pressure” ***International Journal of Hydrogen Energy*** (2017), 24569 – 24579.
- Alam, F., Haas, M., Farouk, T., Dryer, F., “Influence of trace nitrogen oxides on natural gas oxidation: Flow reactor measurements and kinetic modeling” ***Energy and Fuel*** (2016), 31, 2360 – 2369.
- Ahmed, S., Santner, J., Padak, B., Dryer, F., Farouk, T., “Computational study of NO<sub>x</sub> formations at conditions relevant to gas turbine operation part II: NO<sub>x</sub> in high hydrogen content fuel combustion at elevated pressure” ***Energy and Fuel*** (2016), 30, 7691 - 7703.
- Santner, J., Ahmed, S., Farouk, T., Dryer, F., “Computational study of NO<sub>x</sub> formation at conditions relevant to gas turbine operation, part I” ***Energy and Fuel*** (2016), 30, 6745 – 6755.
- Ahmed, S., Dasgupta, A., Dryer, F., Farouk, T., “Multidimensional numerical investigation of NO<sub>x</sub> formation in a burner coupled flow tube configuration: NO<sub>x</sub> kinetics in post, pre and flame locations ” *10<sup>th</sup> U.S. National Combustion Meeting*, College Park, Maryland, April 23 – 26, 2017.
- Alam, F., Haas, F., Farouk, T., Dryer, F., “Flow reactor measurements and kinetic modeling of nitrogen oxides (NO<sub>x</sub>) perturbed synthetic natural gas oxidation ” *Spring Technical Meeting of the Eastern States Section of the Combustion Institute*, Princeton, New Jersey, March 13 – 16, 2016, Pages 1 – 6.
- Ahmed, S., Santner, J., Dryer, F., Farouk, T., “Comprehensive kinetic model for predicting NO<sub>x</sub> during hydrogen content fuel combustion at elevated pressure” *9<sup>th</sup> U.S. National Combustion Meeting*, Cincinnati, Ohio, May 17 – 20, 2015.
- Santner, J., Ahmed, S., Farouk, T., Dryer, F., “Computational study of NO<sub>x</sub> formation at conditions relevant to gas turbine operating conditions” *9<sup>th</sup> U.S. National Combustion Meeting*, Cincinnati, Ohio, May 17 – 20, 2015.



**Thank You**