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# Towards Predicting Reactive-element Tolerances in the Compositional Design of $\text{Al}_2\text{O}_3$ -scale Forming Alloys and Coatings



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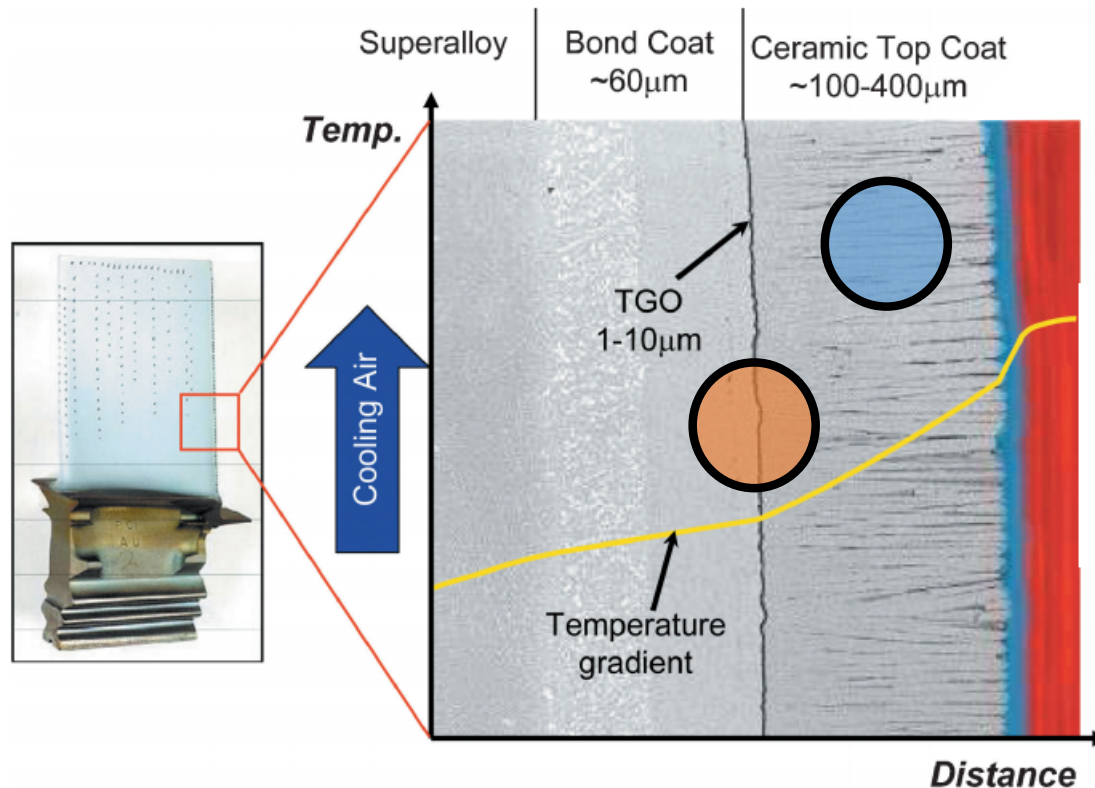


# Key Questions



- Understand the controlling factors that affect the formation of  $\text{Al}_2\text{O}_3$  scale vs internal oxidations
- Determine the effects of alloying elements on retardation of  $\text{Al}_2\text{O}_3$  scale growth
- Explore new compositional design of  $\text{Al}_2\text{O}_3$ -scale forming alloys and coatings

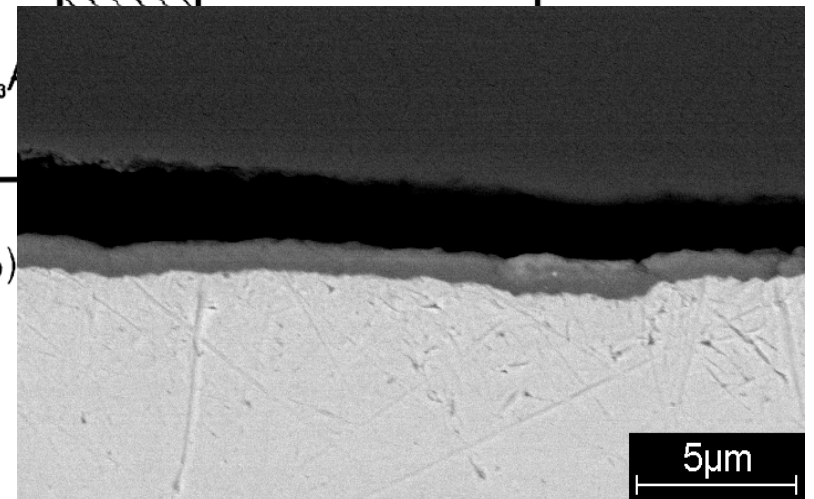
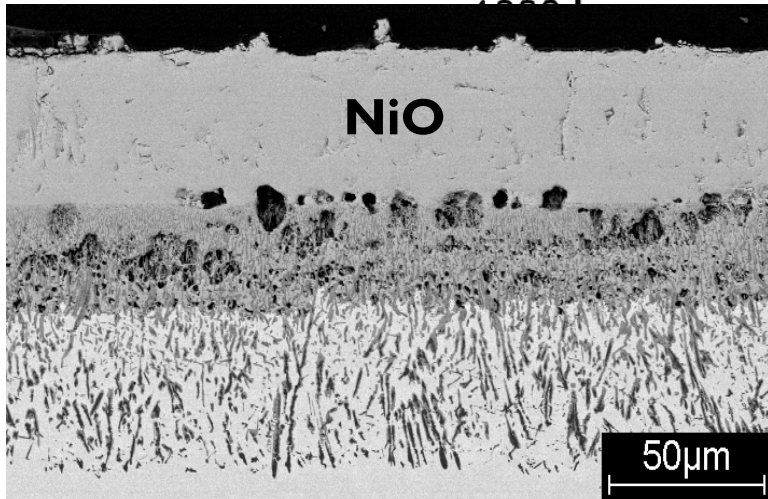
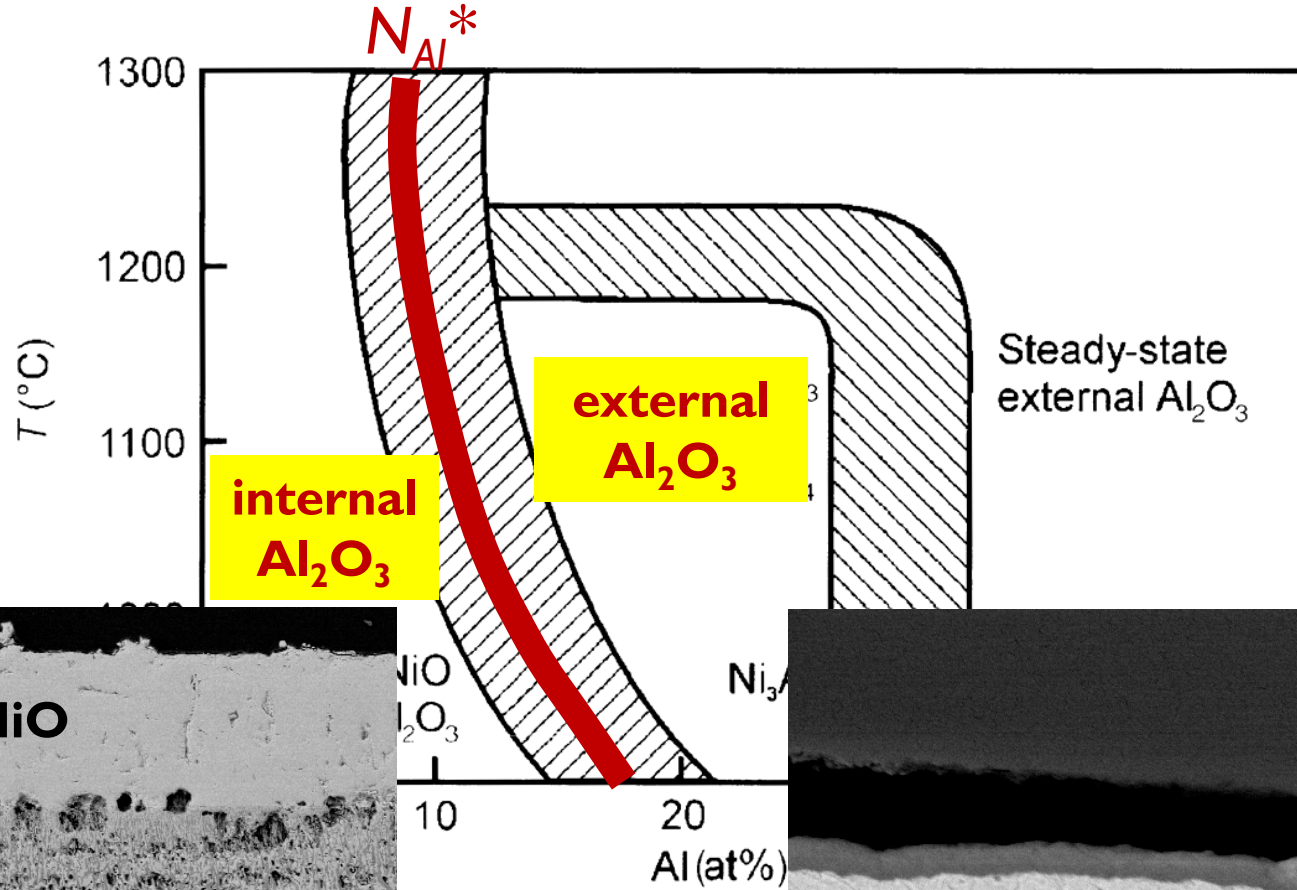
# Bond Coats in Turbines



- **Thermally grown oxide (TGO)**
  - Typically  $\alpha\text{-Al}_2\text{O}_3$  for very high temperature applications ( $T > 1000\text{ }^\circ\text{C}$ ).
  - Established using **bulk alloys** and **metallic coatings**.

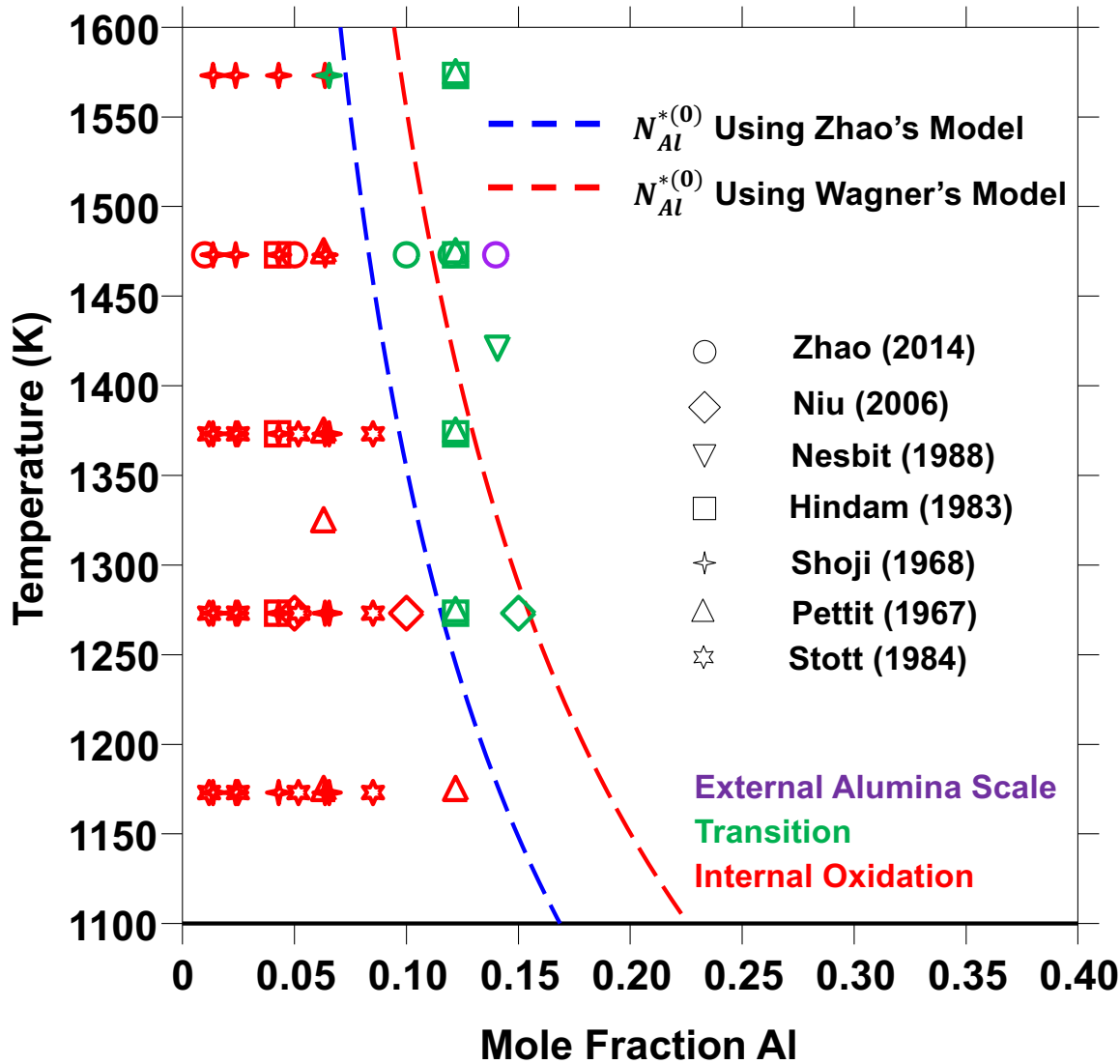
# Alumina Scale Formation on Ni-Al Alloys

Oxidation carried out in 0.1 atm pure  $O_2$



F.S. Pettit, "Oxidation mechanisms for Ni-Al Alloys at temperatures between 900 and 1300°C," *AIME Met. Soc. Trans.*, **239** (1967) 1296.

# Critical Al Concentration in $\gamma - \text{Ni}_{1-x}\text{Al}_x$



$$N_B^{*(0)} = \sqrt{g_{BO_v}^* \frac{V_{alloy} D_O N_O^{(s)} \pi}{V_{BO_v} D_B 2v}}$$

Oxides Block Diffusion

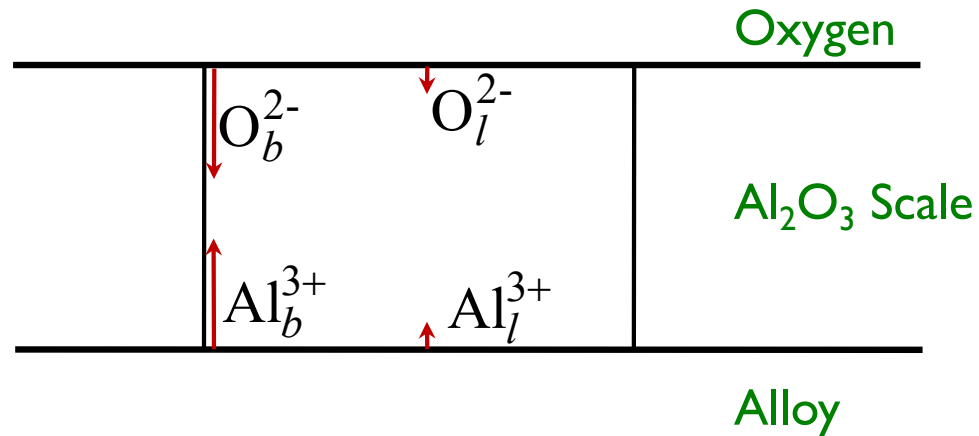
$$N_B^{*(0)} = \sqrt{\frac{\pi N_O^{(s)} D_O}{v D_B} \beta}$$

$$\beta = \left( \frac{1}{\left( \frac{V_{BO_v}}{g_{BO_v} V_{alloy}} - \frac{V_{BO_v}}{V_{alloy}} + 1 \right) \frac{2 + g_{BO_v}}{1 - g_{BO_v}}} \right)$$

**Model for oxide blocking comes close to transition data**

# Benefits of Reactive Elements (RE) on Alumina Scale Formation on Alloys

$\text{Al}_2\text{O}_3$  scale growth is dominated by grain-boundary diffusion at the temperatures of interest



$k_p$

Outward transport

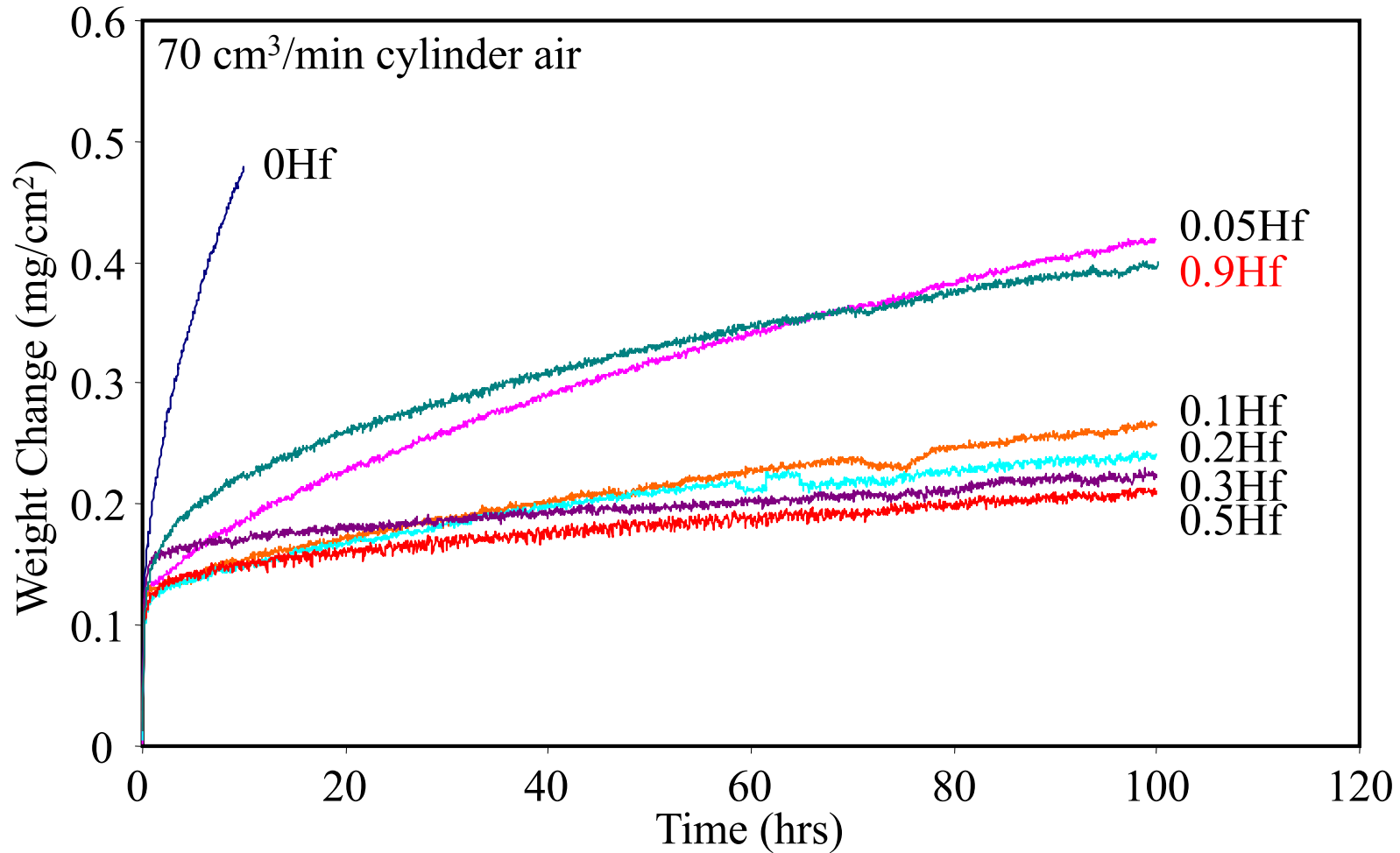
Fe, Ni-based  
with RE vs. Without

Down 2×

RE reduces  $D_b^{\text{Al}}$  by 4×

RE = Hf, Y, Zr, La, ...

# Oxidation of Ni-20Al-20Pt-xHf at 1150°C

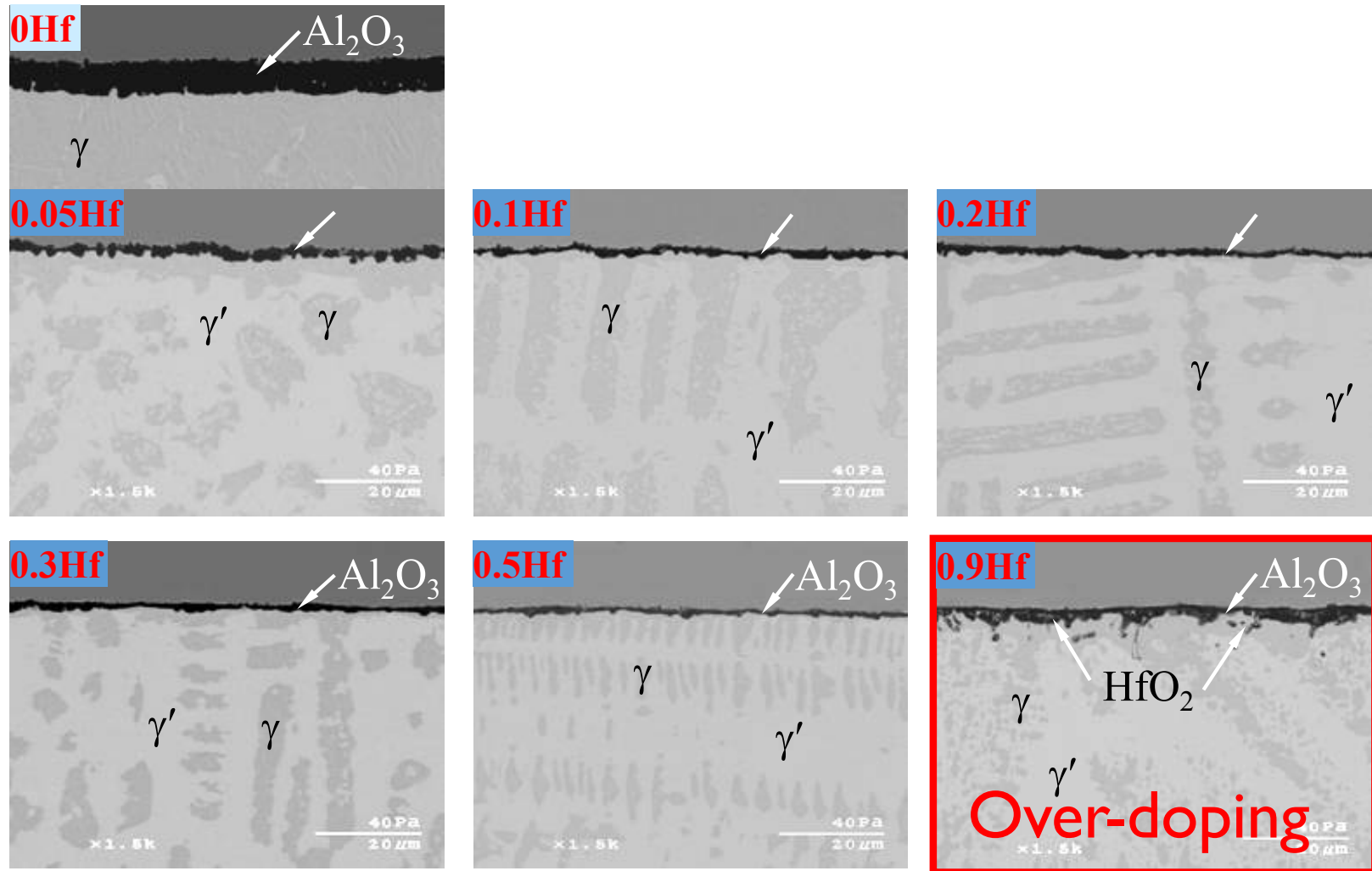


- Reactive elements offer added oxidation resistance.
- High concentrations results in **over-doping**.





# Cross-sectional Images After 100 h Oxidation at 1150°C



- This **over-doping concentration** is usually found by trial and error and depends on alloys
- Can it be determined by the thermodynamic criteria for this event?





$$dU = TdS - PdV + \sum \mu_i dN_i = \sum Y^a dX^a$$

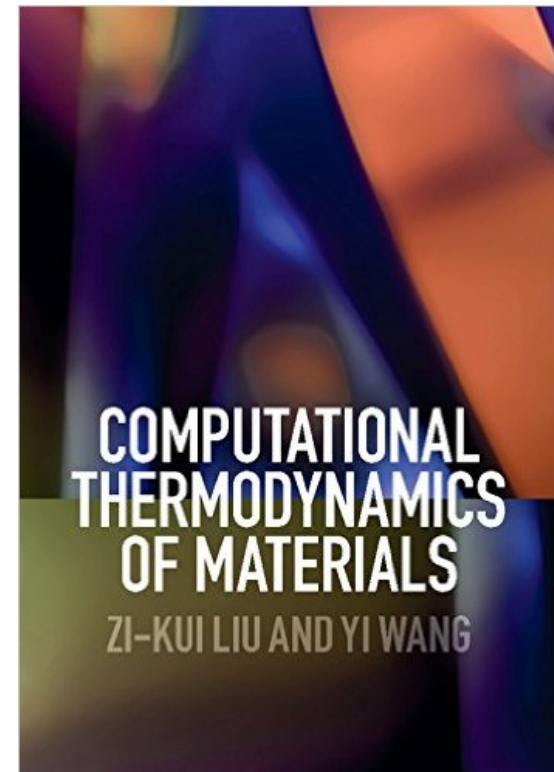
- Equilibrium thermodynamics

$$dU = \sum Y^a dX^a - D_{ip} d\xi + 0.5D_2 (d\xi)^2$$

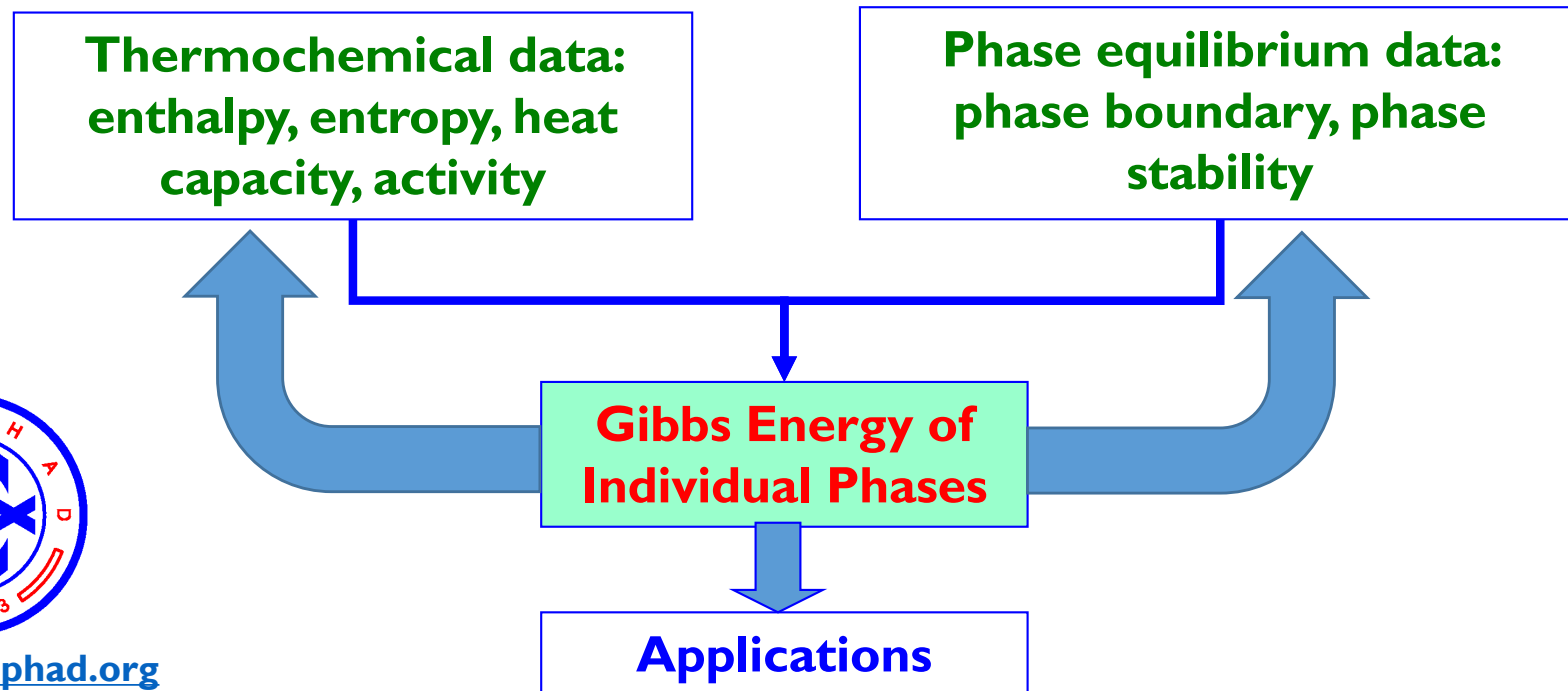
- Irreversible/non-equilibrium thermodynamics

$$S = -k_B \sum p_i \ln p_i$$

- **Statistical: Entropy for probability of configurations/states by Boltzmann/Plank/Gibbs.**



# CALPHAD modeling: Individual phases



[www.calphad.org](http://www.calphad.org)

[www.journals.elsevier.com/calphad](http://www.journals.elsevier.com/calphad)

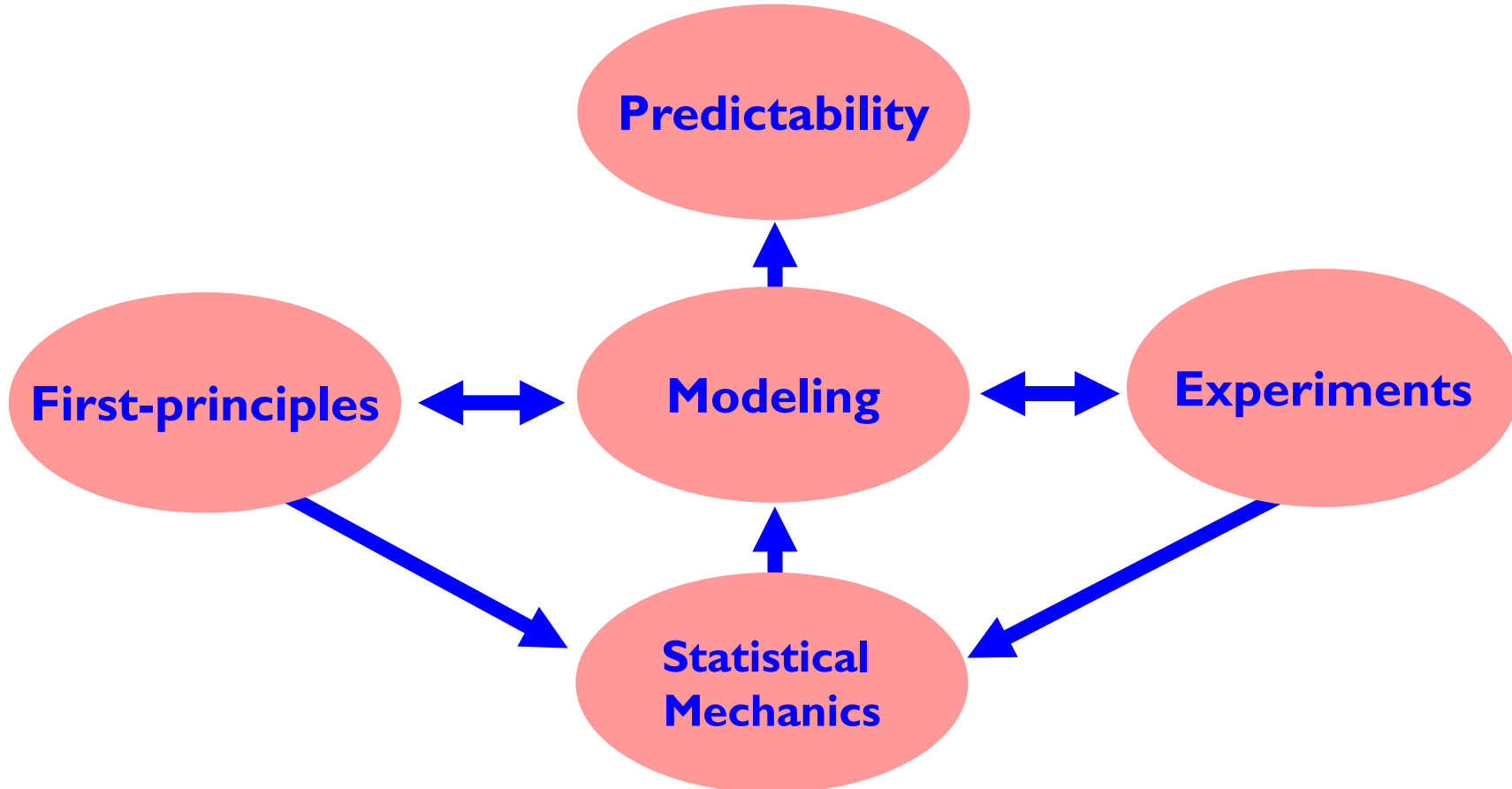
**Pure elements → Binary → Ternary → Multicomponent**

***Thermochemical and phase equilibrium data are not independent!***

**Kaufman & Bernstein: Computer Calculation of Phase Diagram. 1970**

## First-Principles Calculations and CALPHAD Modeling of Thermodynamics

Zi-Kui Liu



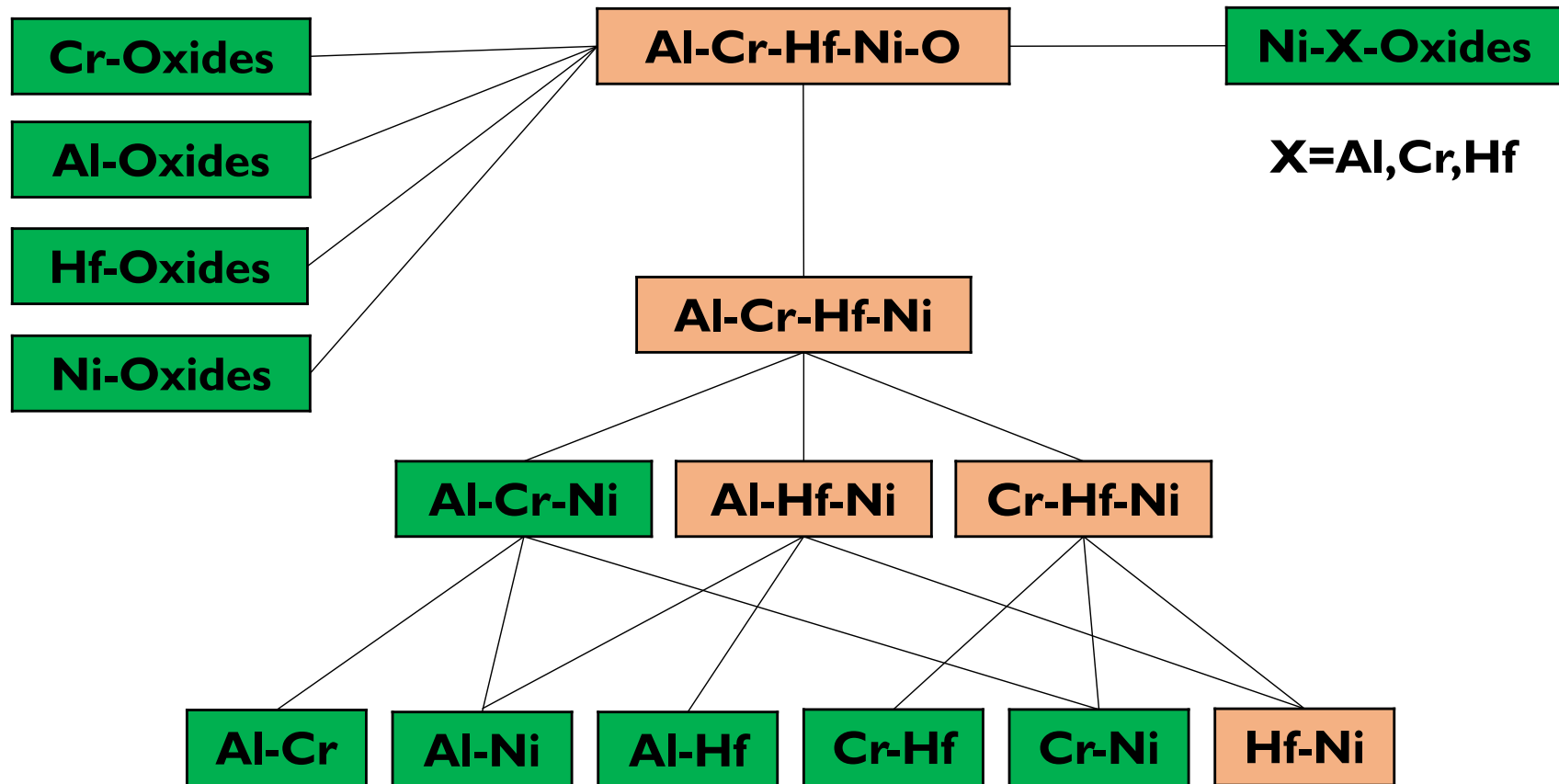


# Properties of Individual Phases and Interfaces: Dependence on $T, P, \xi$



- Electronic structures
- Thermal Properties
  - Heat capacity
  - Enthalpy, entropy, free energy
  - Thermal expansion/contraction
- Transport Properties
  - Diffusion coefficient
  - Seebeck coefficients
  - Heat of transport
- Interfacial properties
  - Stacking fault energy
  - Anti-phase boundary energy
  - Grain boundary and interfacial energy
- Mechanical properties
  - Elastic moduli/Compressibility
  - Dislocations mobility
  - Relative creep rate
- Kinetic Properties
  - Interface mobility
- Physical properties
  - Melting and Glass transition
  - Electrical properties
  - *Magnetic properties*
  - Optical properties
- Mechanical properties
  - Fracture toughness
  - Plasticity of single crystal
  - Ductility and formability
  - Hardness
  - Yield strength
  - Fatigue strength

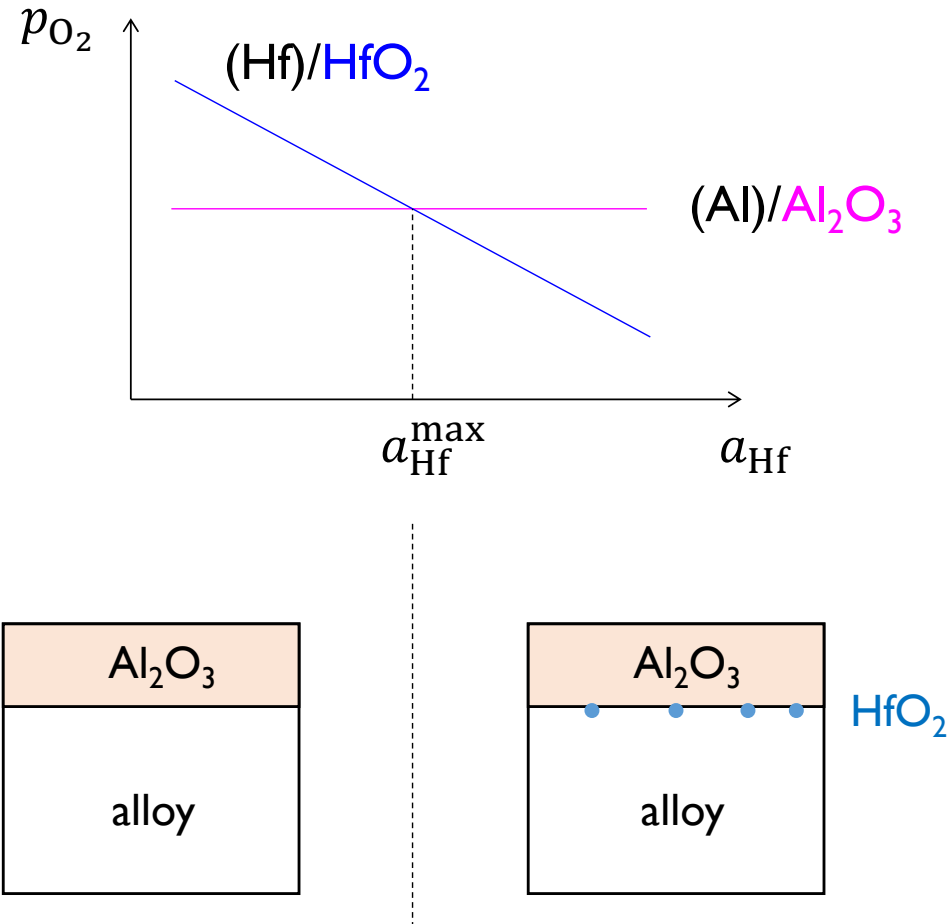
# Ni-Al-Cr-Hf-O



Modeled in the Literature

Modeled by PSU

# HfO<sub>2</sub> Stability in an Al<sub>2</sub>O<sub>3</sub> Forming Alloy

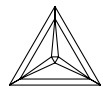
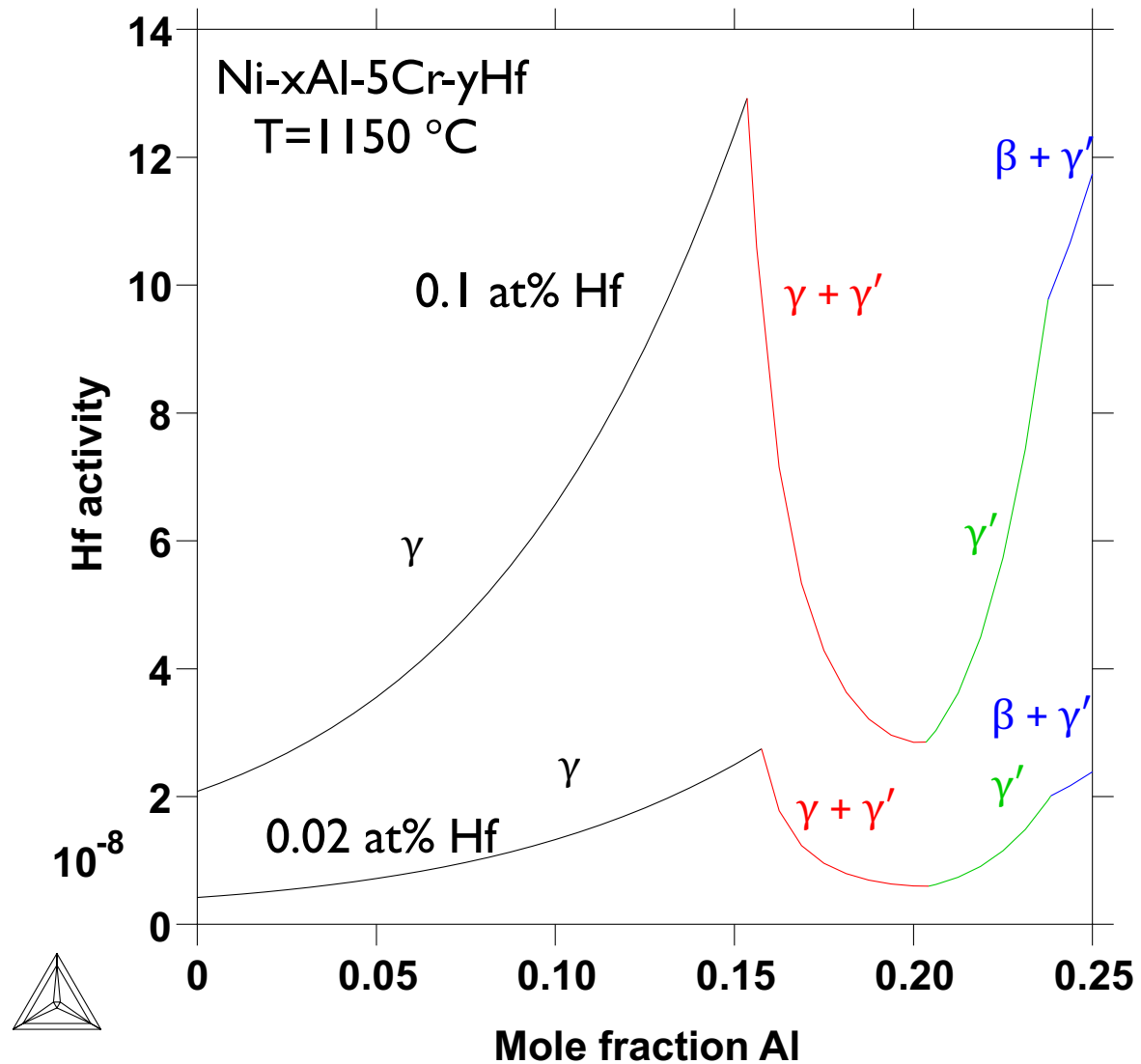


# Hf Activity Changes with Hf Concentration, Al Concentration and Phases Present

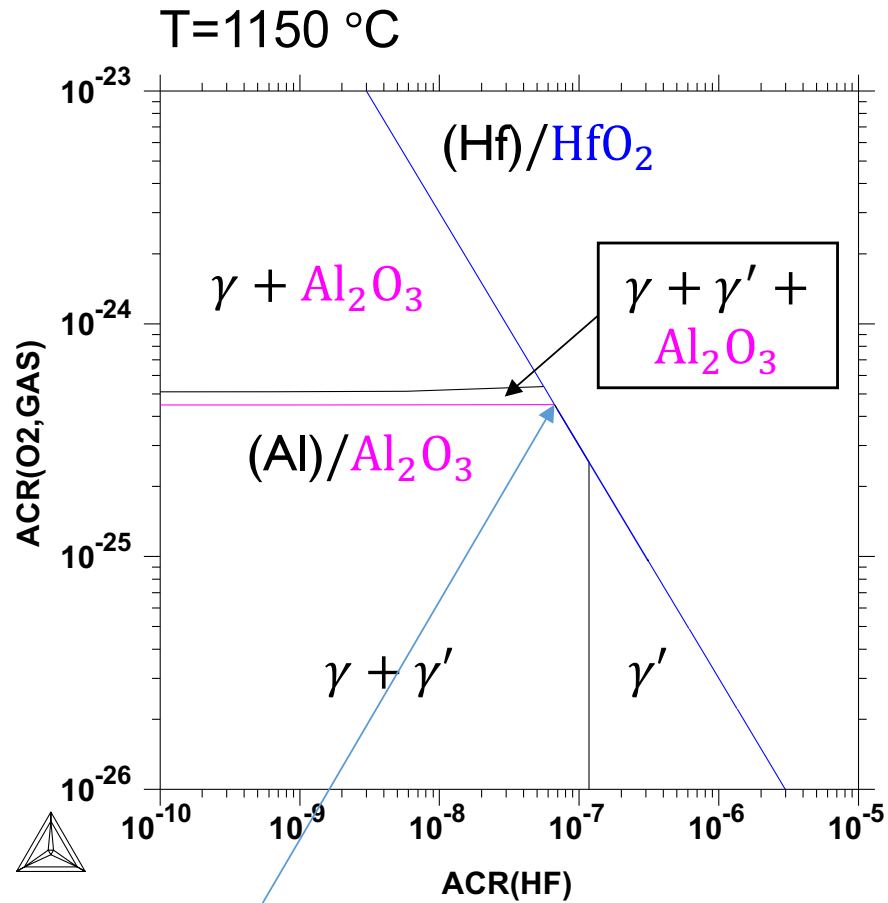
In single phase

$$\frac{\partial \mu_{Hf}}{\partial N_{Al}} > 0$$

In two-phase region:  
average of two phases



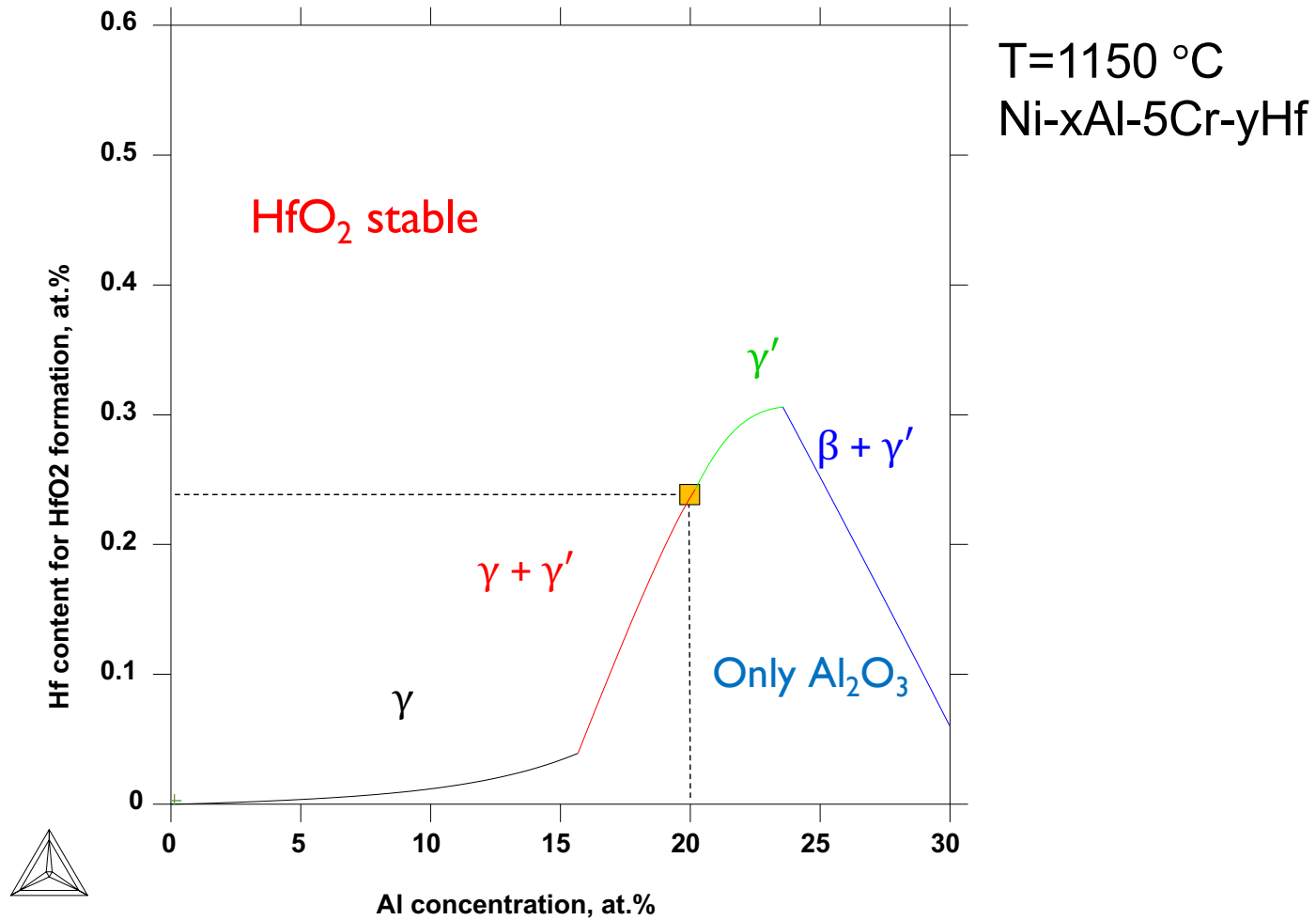




$$a_{\text{Hf}}^{\text{max}} = 6.7 \cdot 10^{-8}$$

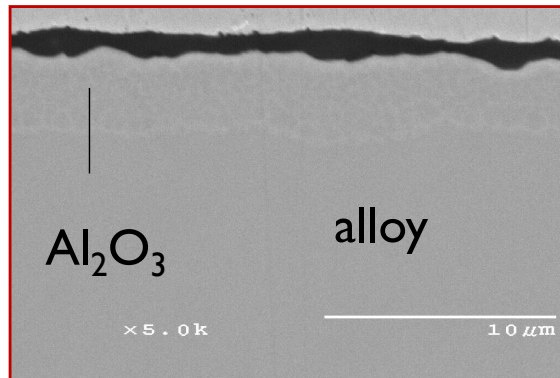
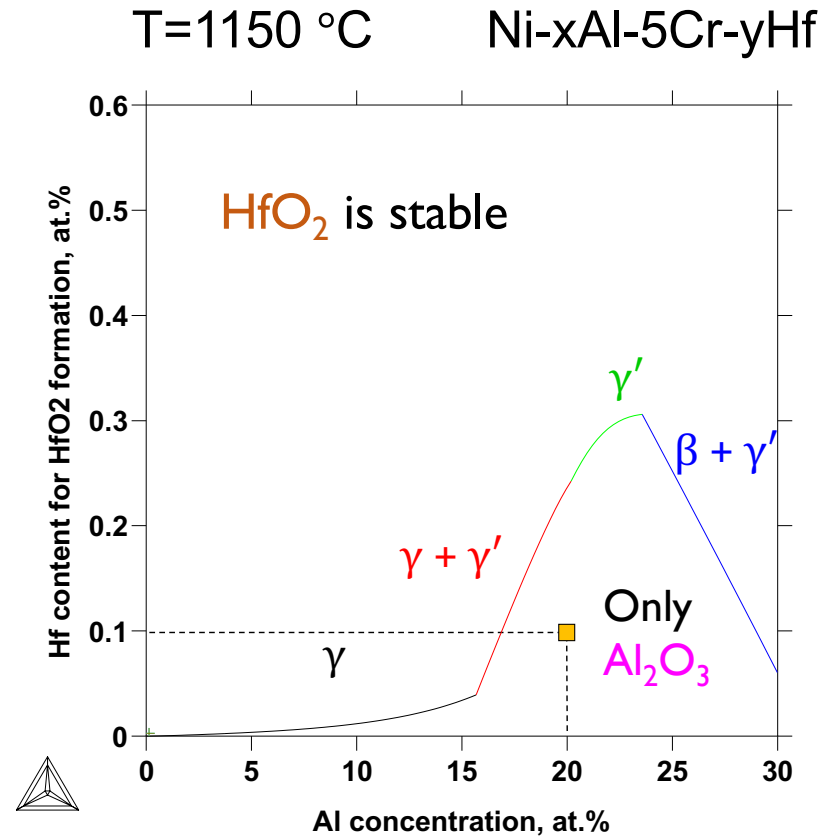
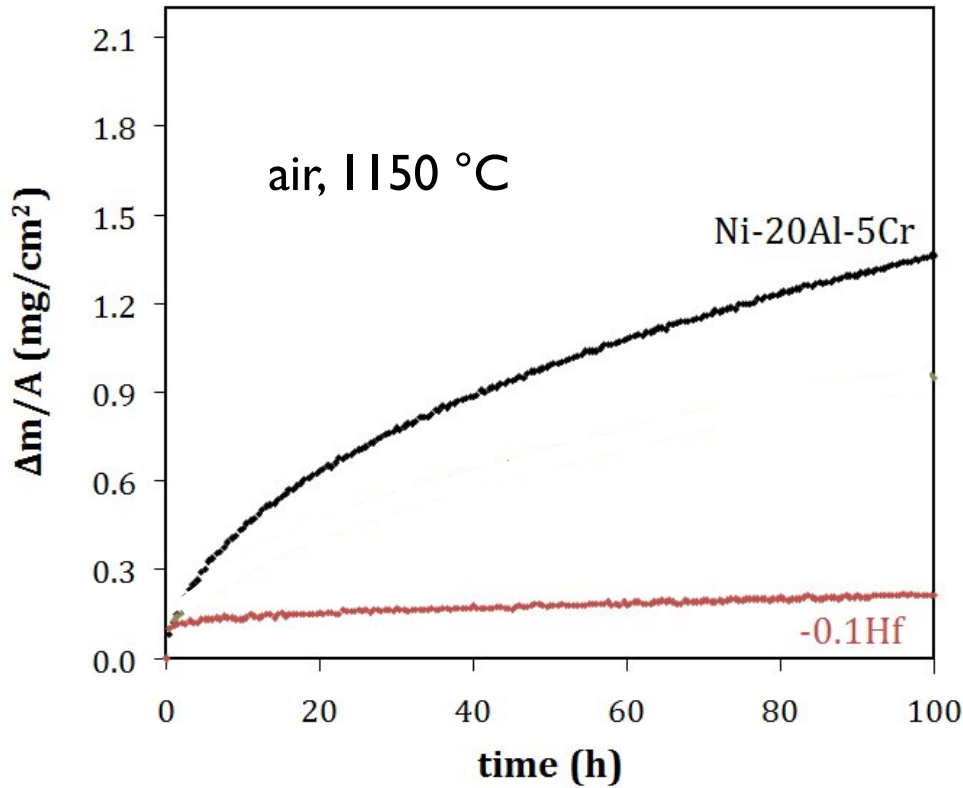
$$x_{\text{Hf}}^{\text{max}} = 0.24 \text{ at}\%$$

# Hf Tolerance: Engineering in Composition Space

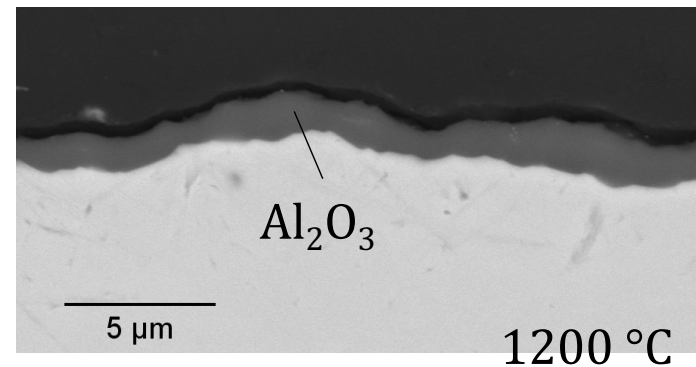
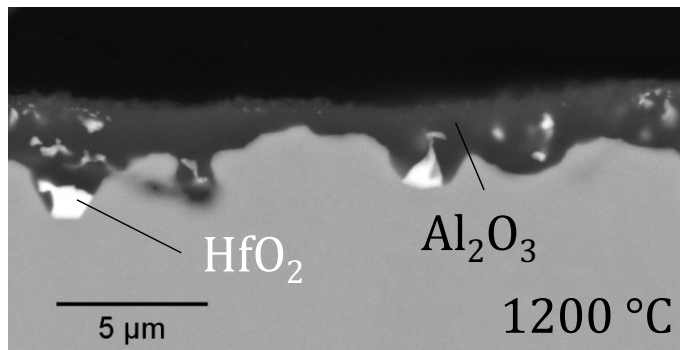
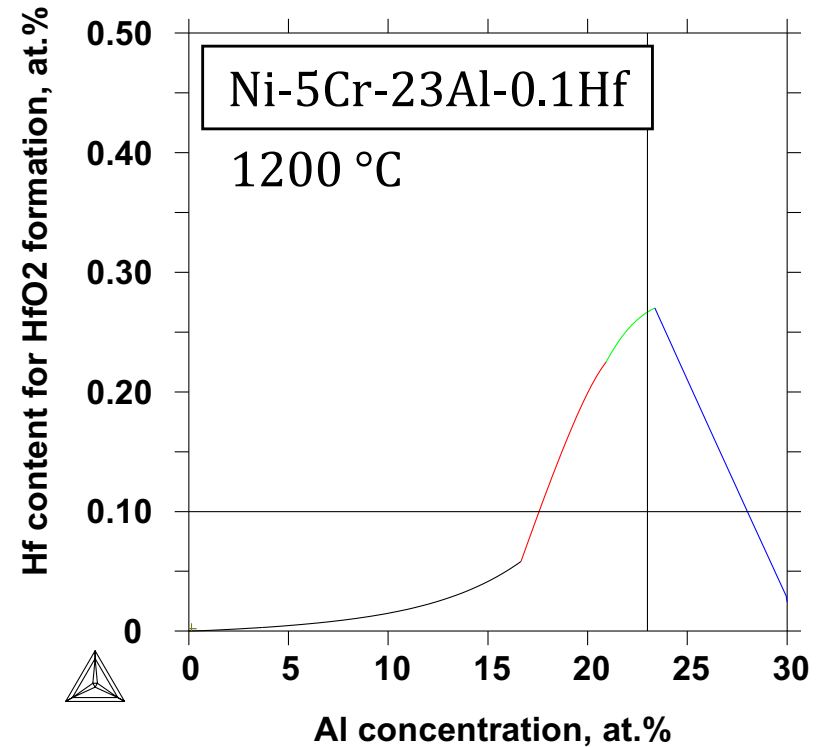
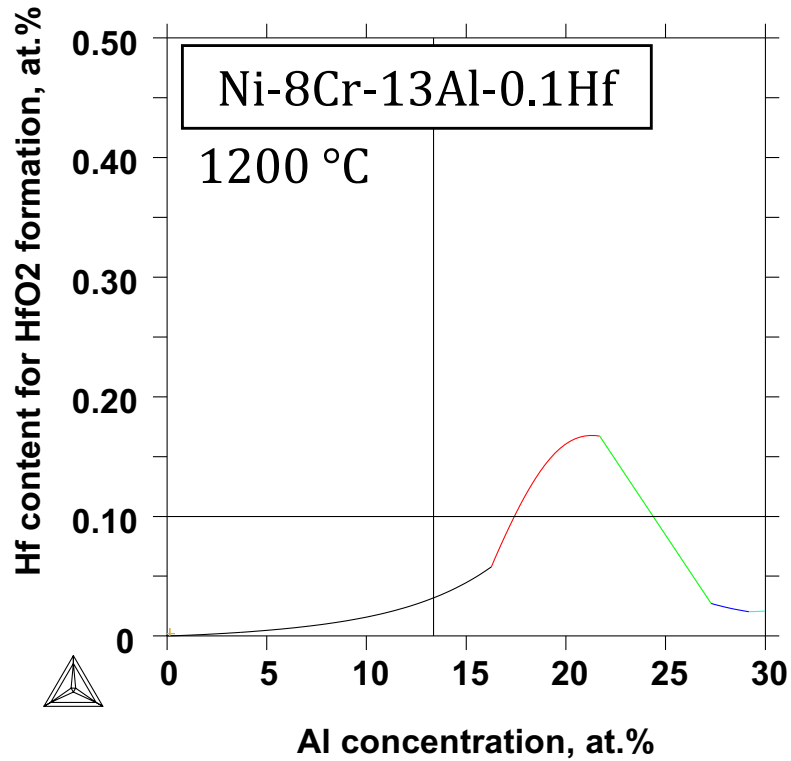




# Reactive Element Doping: Ni-20Al-5Cr-0.1Hf (at%)



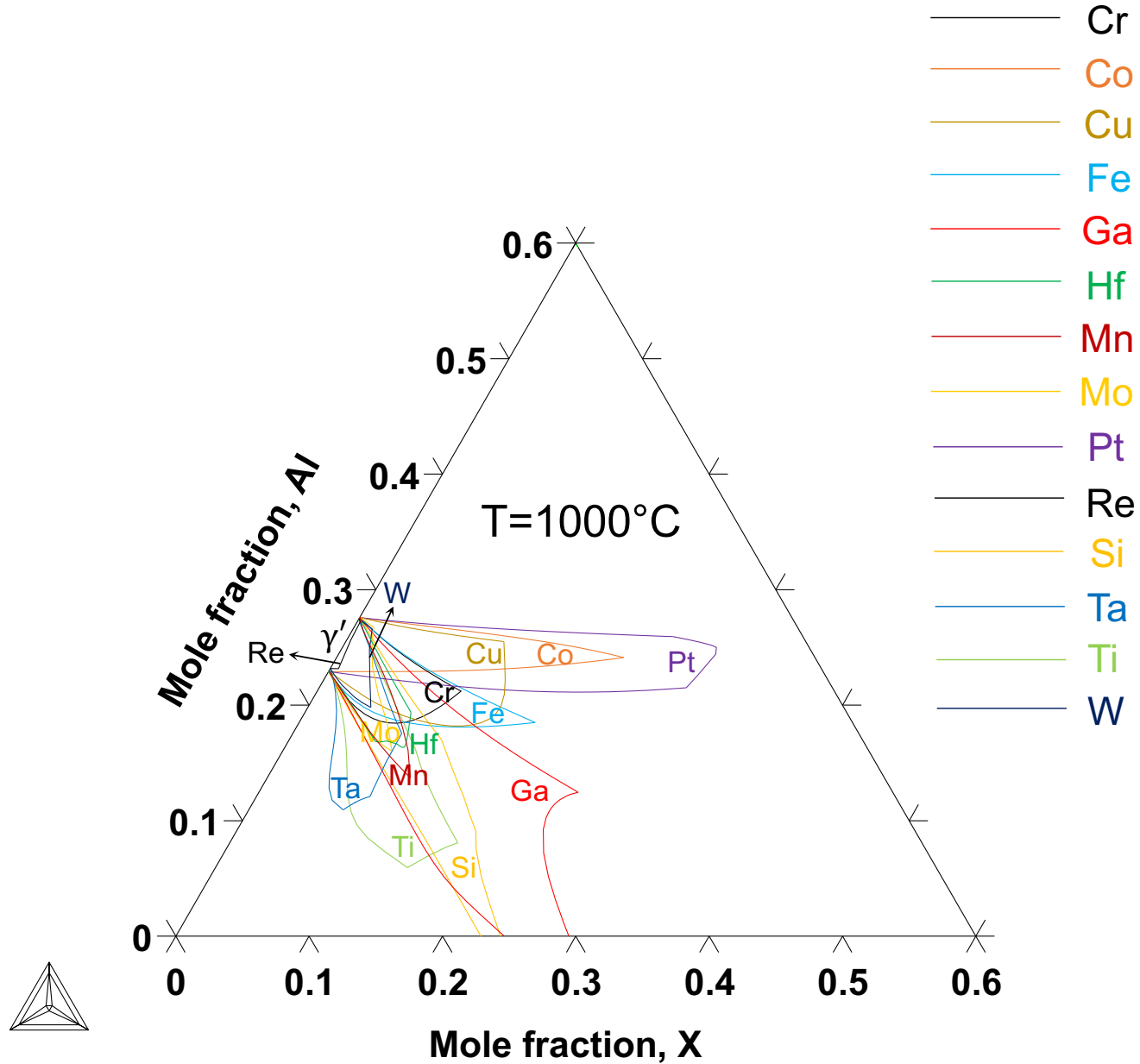
# Experimental Results



# Two Major Factors Affecting Hf Tolerance In The Design of High Temperature Alloys

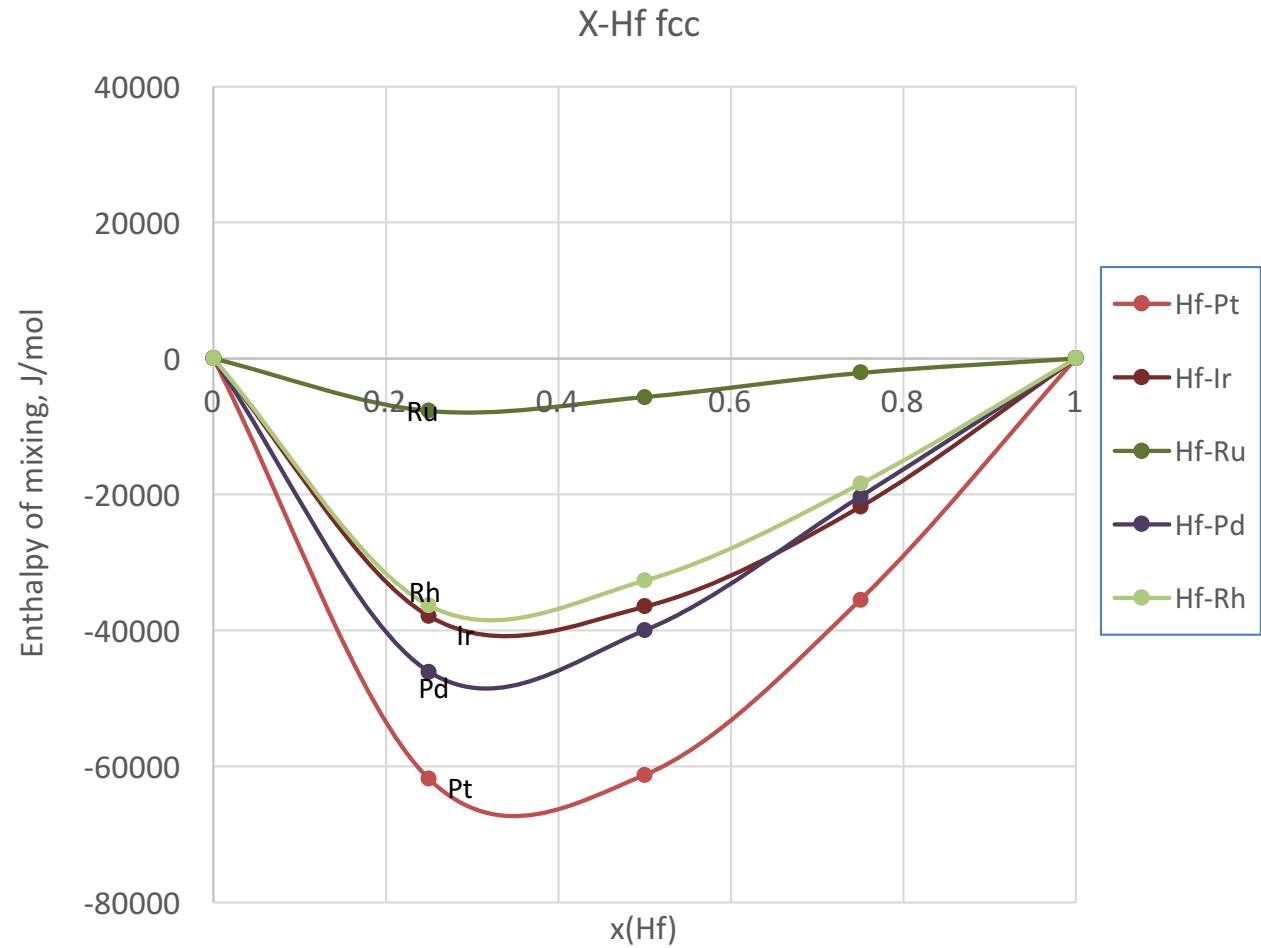
- **$\gamma'$  phase stability:** In Ni-Al-X systems, elements can be added which **increase the  $\gamma'$  phase fraction** when substituting Ni or Al.
- **Hf-X chemical interaction:** In the Al-Hf-Ni-X systems, elements can be added which **decrease the Hf activity in  $\gamma$  and  $\gamma'$** .
  - Effect of X on activity of Hf can be found by determining the enthalpy of mixing between Hf and X.

# Alloying Effects on $\gamma'$ Phase Stability in Ni-Al-X



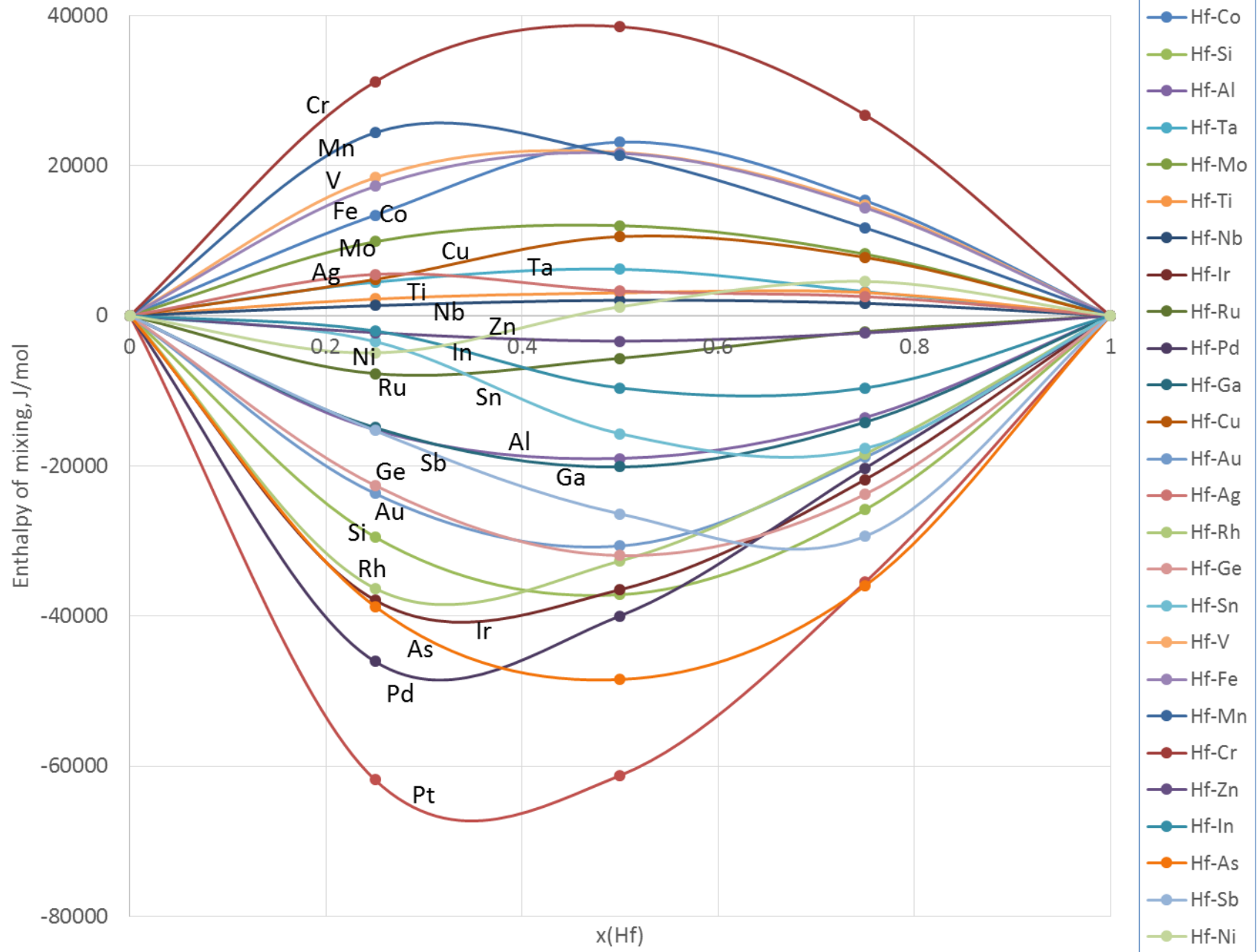
# Calculations Using Special Quasi-random Structures to Calculate Hf-X Mixing Enthalpy

												Al	Si	P
Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As		
Y	Zr	Nb	Mo	Tc	Ru	Rh	Pd	Ag	Cd	In	Sn	Sb		
RE	Hf	Ta	W	Re	Os	Ir	Pt	Au	Hg	Tl	Pb	Bi		

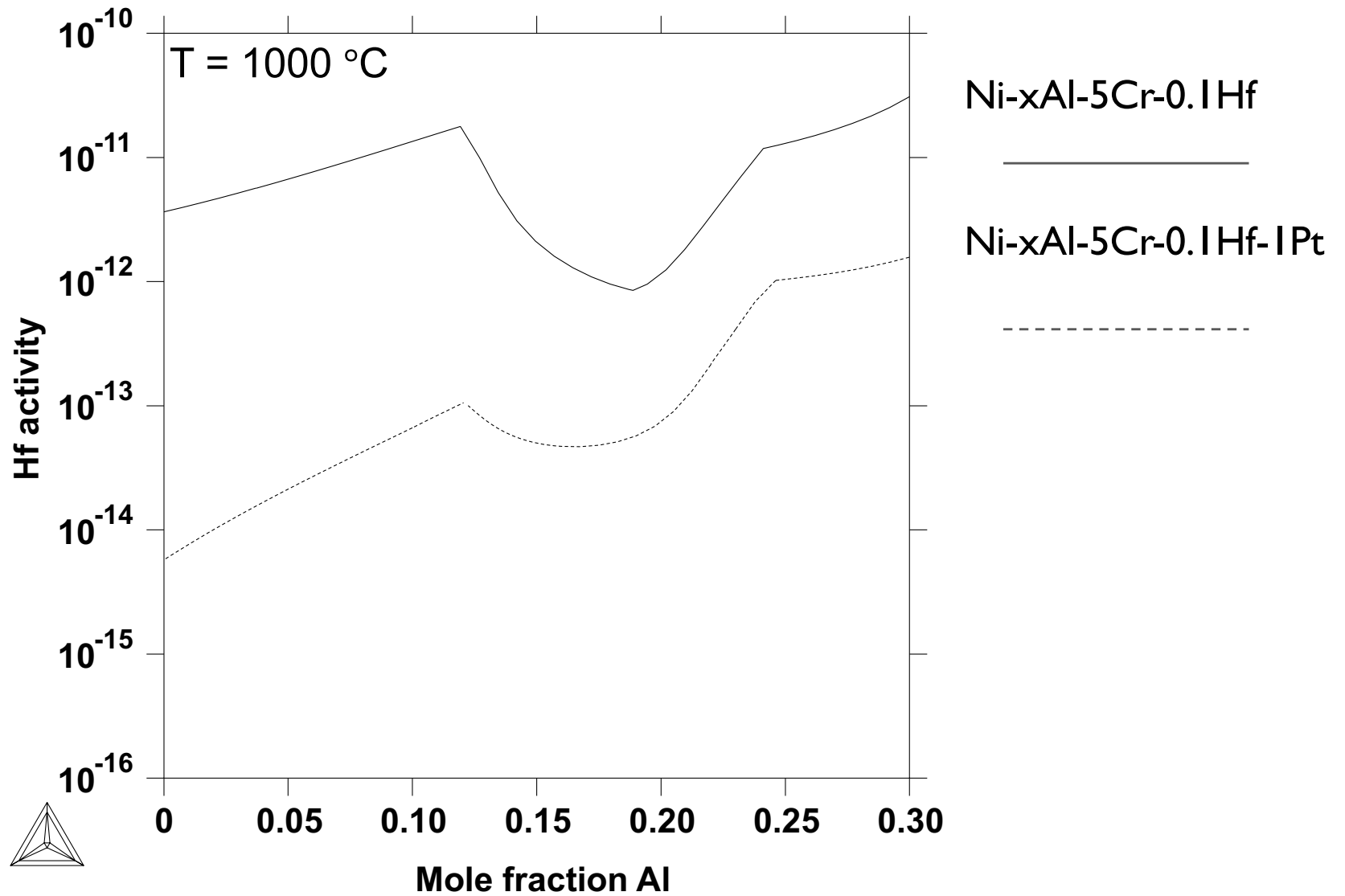




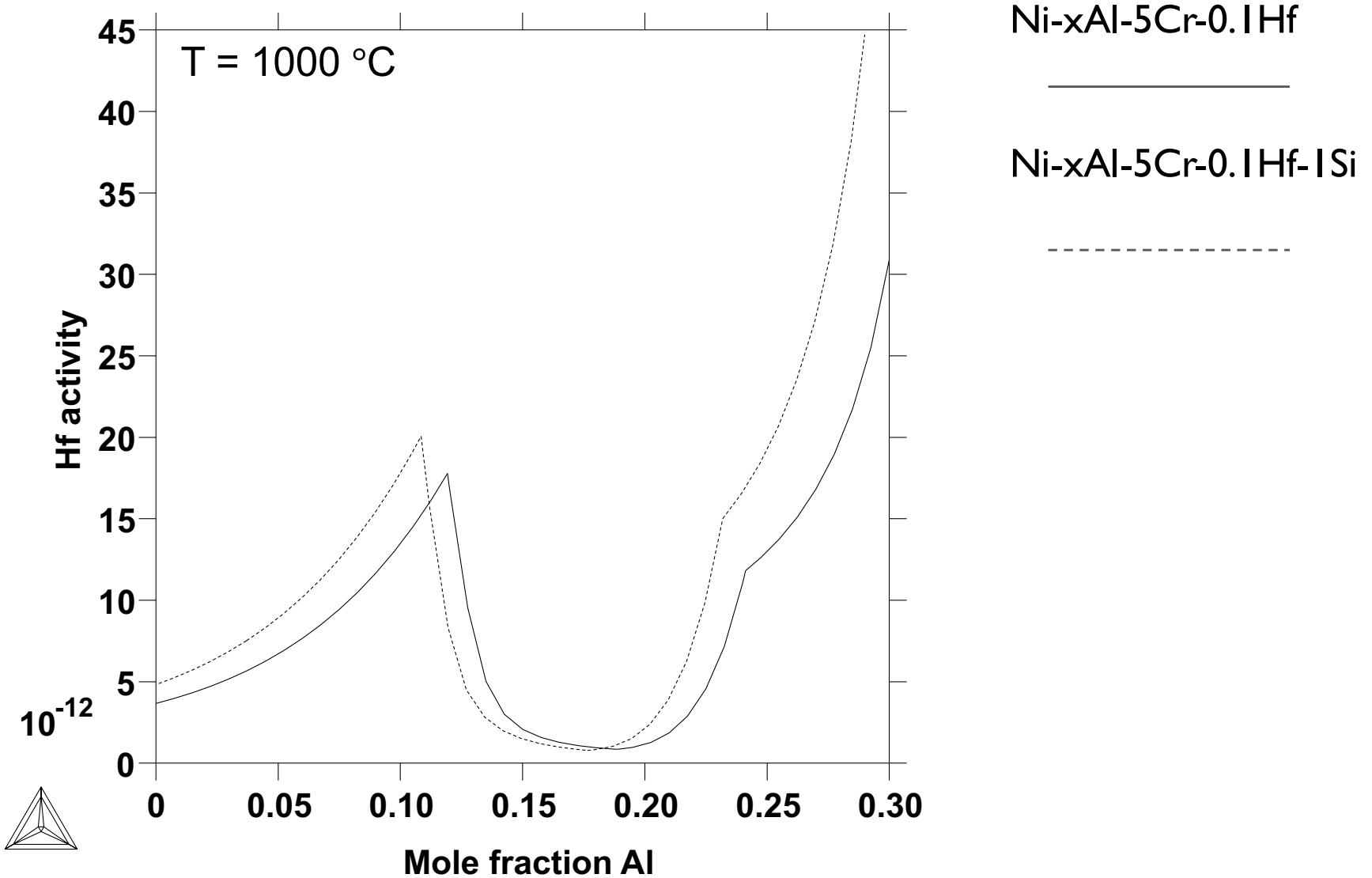
X-Hf Hmix in fcc phase



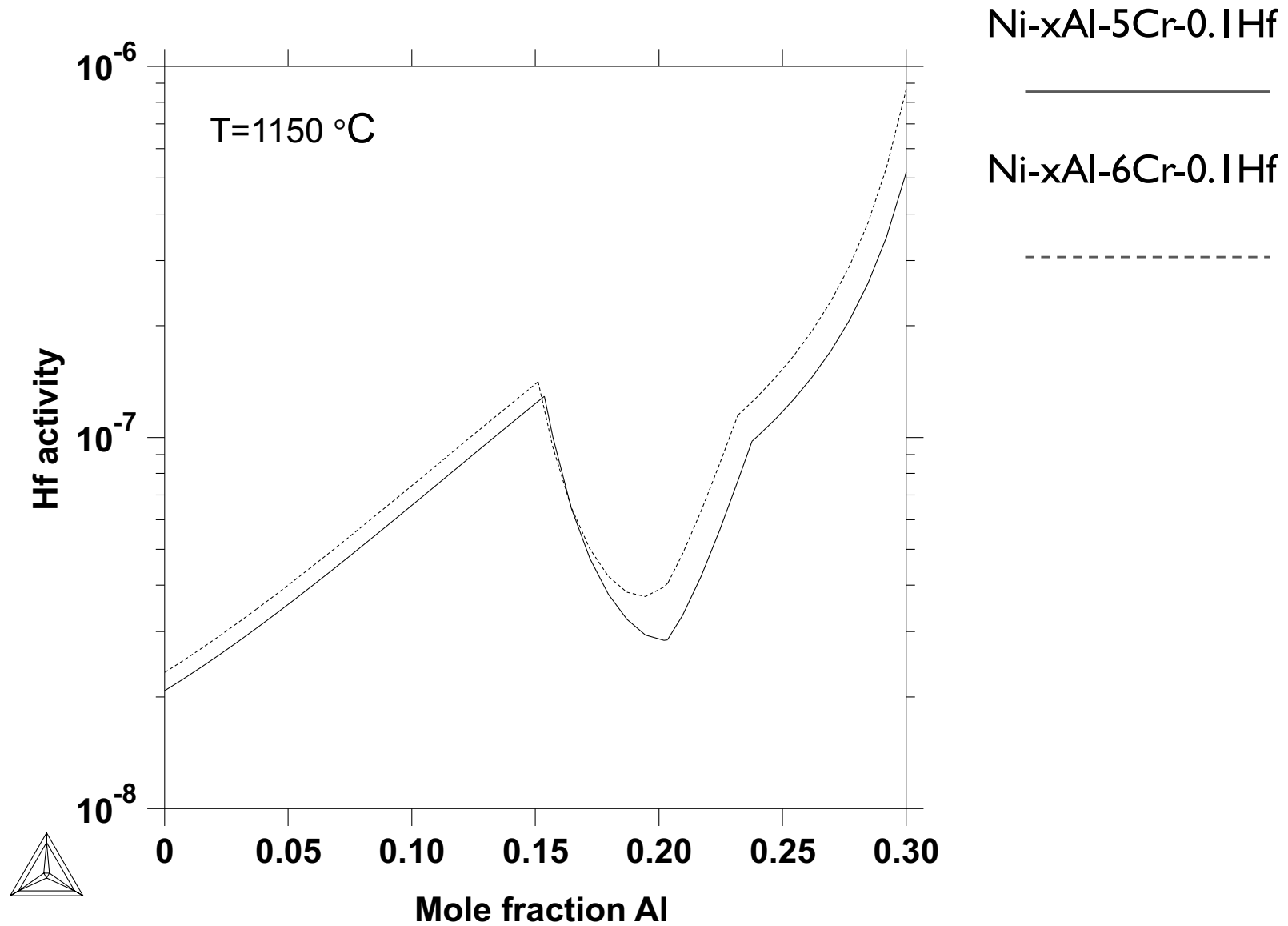
# Calculated Effect of Pt on Hf Activity



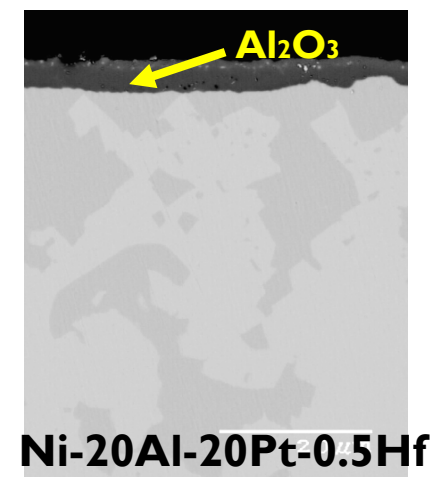
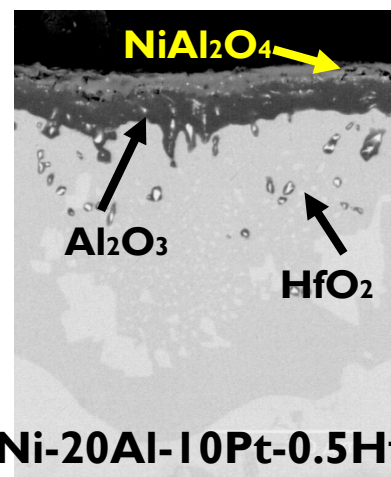
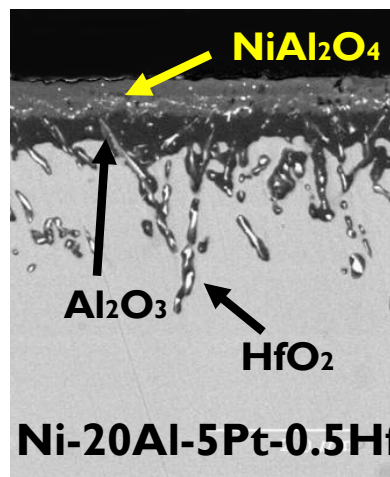
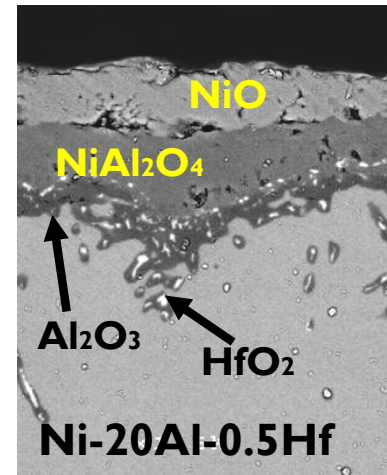
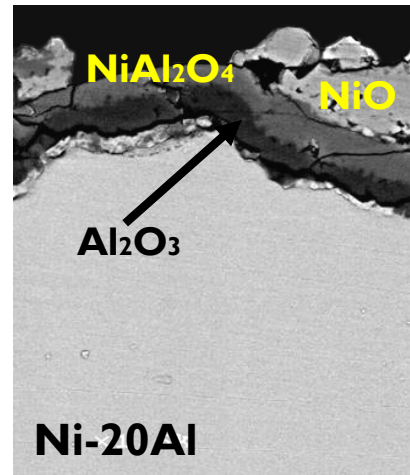
# Calculated Effect of Si on Hf Activity



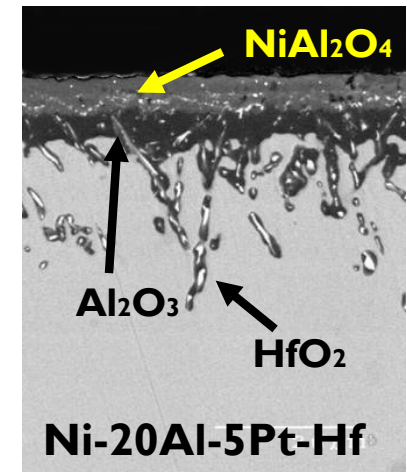
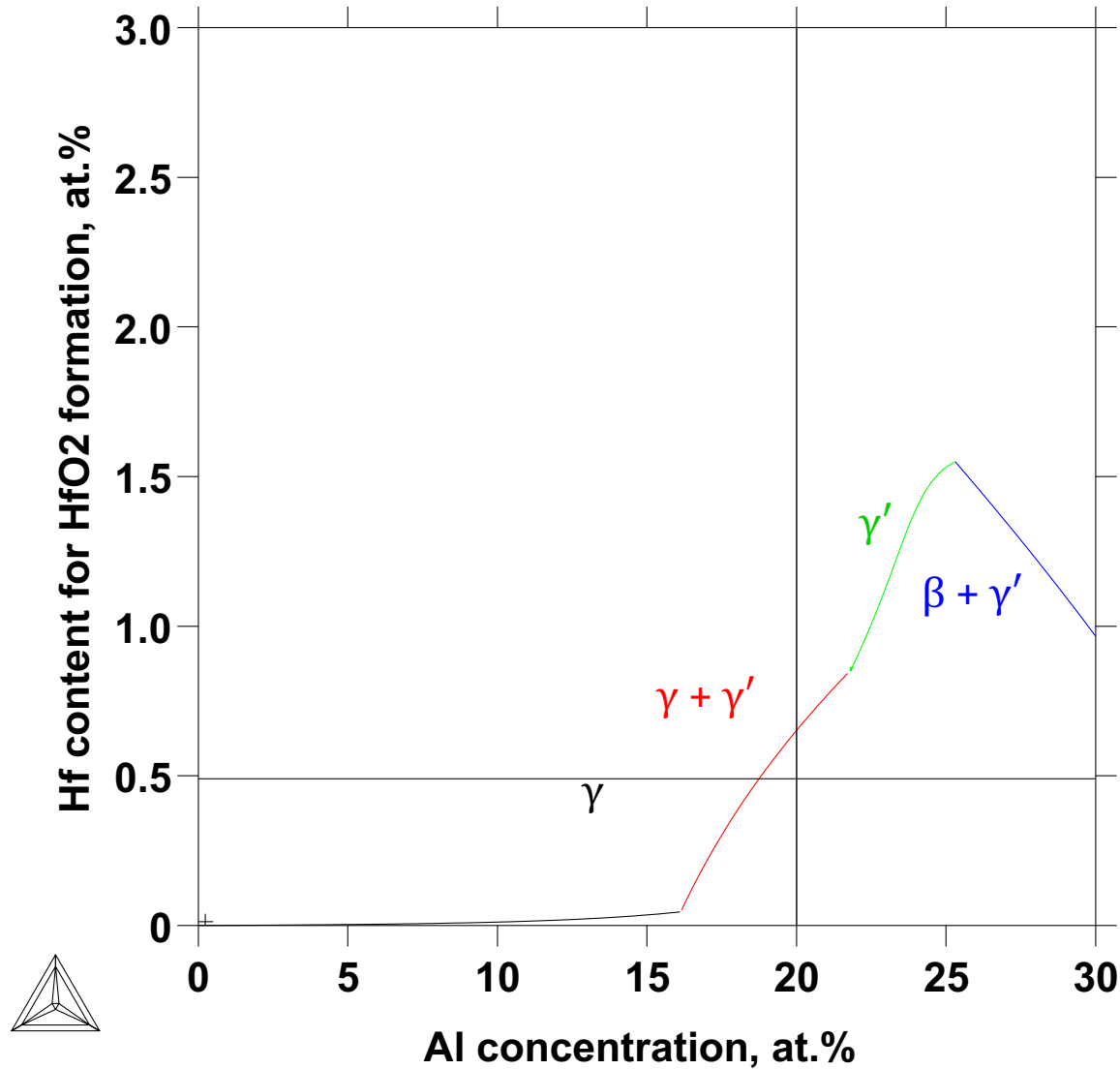
# Calculated Effect of Cr on Hf Activity



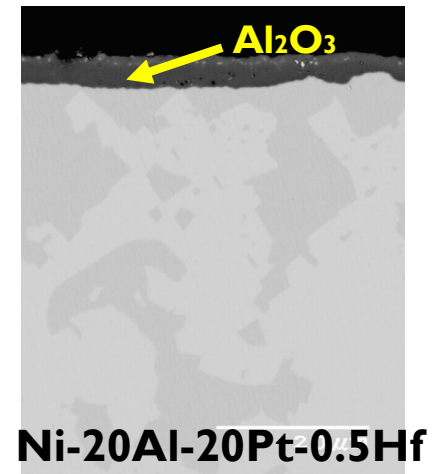
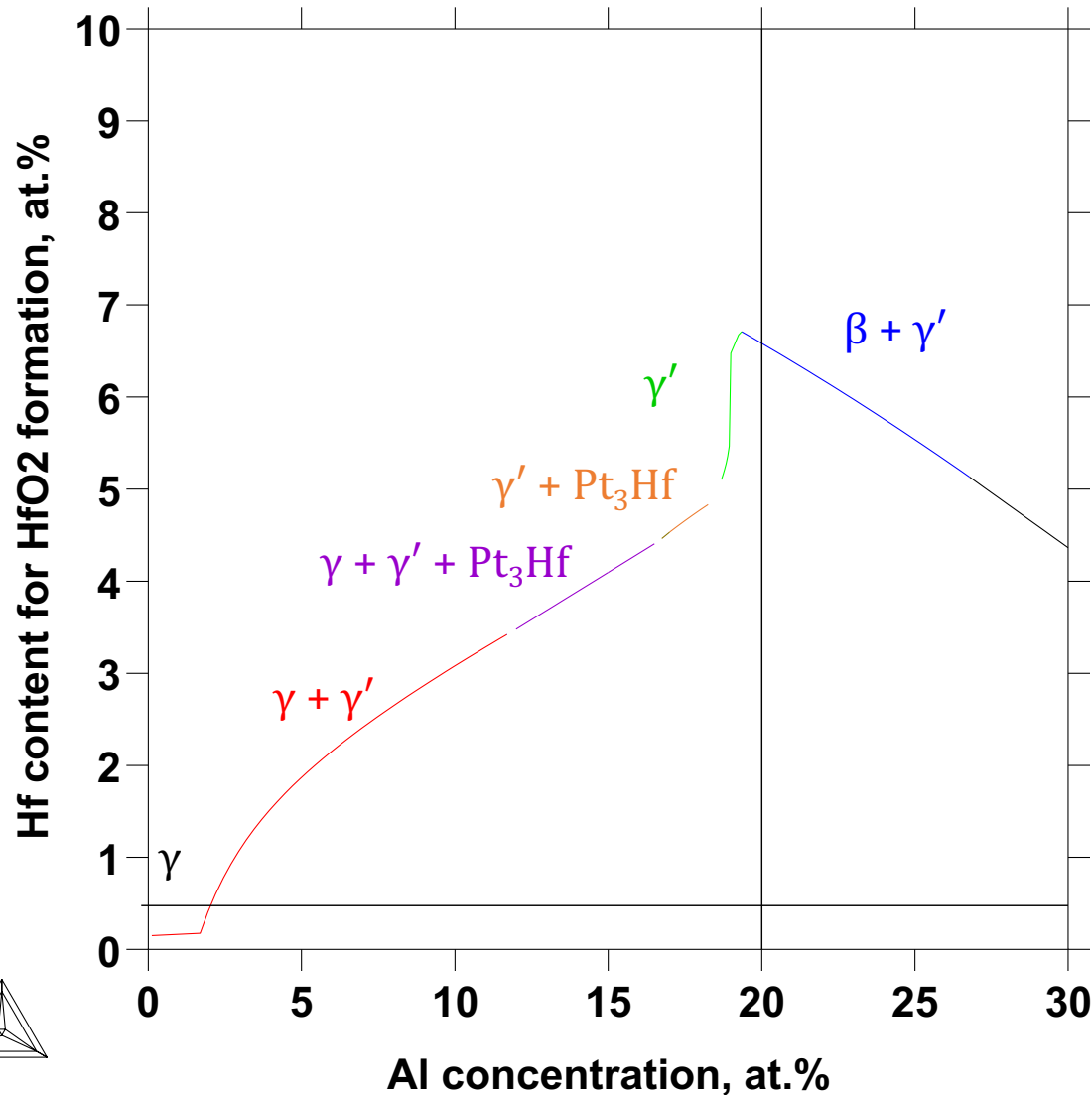
# Cross-Sectional Images of Ni-20at.%Al-Pt-Hf $\gamma/\gamma'$ Alloys After 500 Oxidation Cycles at 1150°C in Air



# Hf Tolerance: Ni-20Al-5Pt-0.5Hf



# Hf Tolerance: Ni-20Al-20Pt-0.5Hf



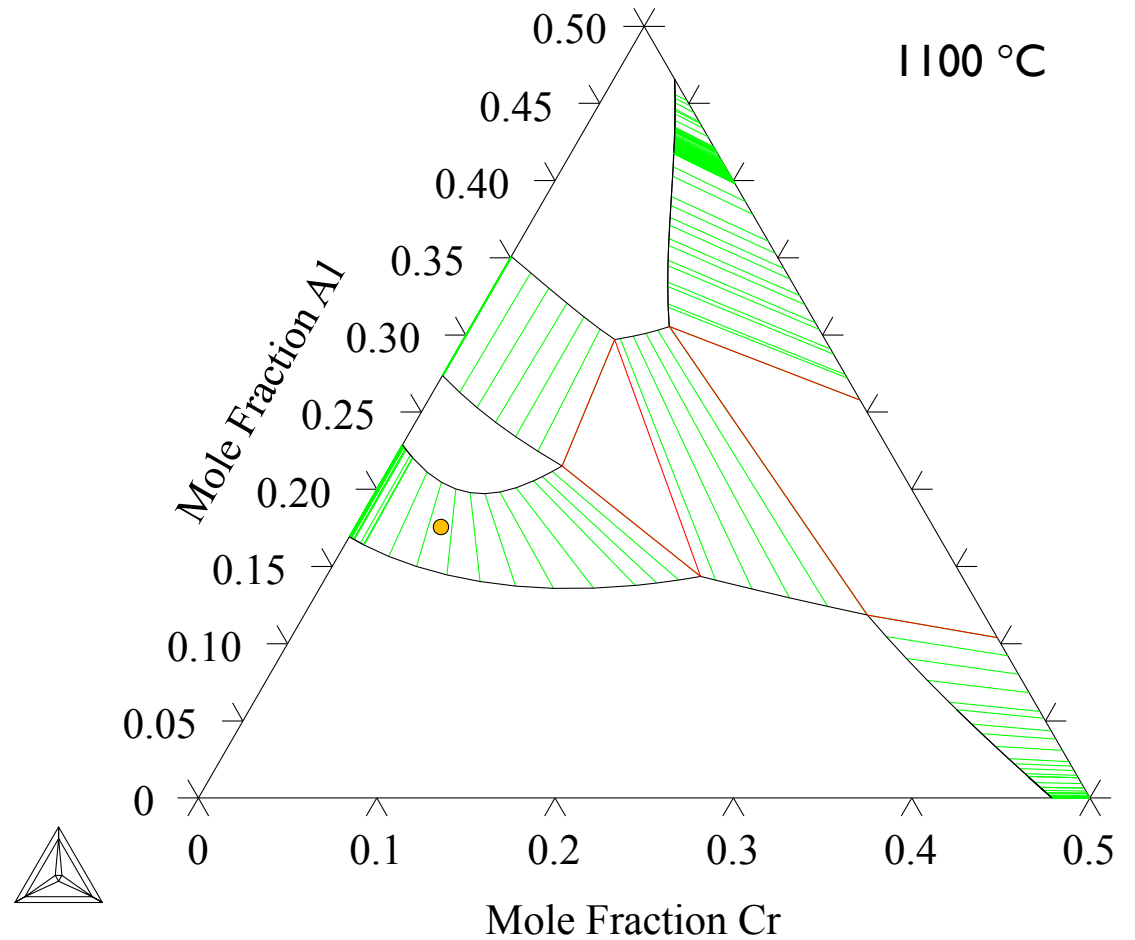




# Engineering a RE-doped Alloy/Coating : Choosing a Base Composition

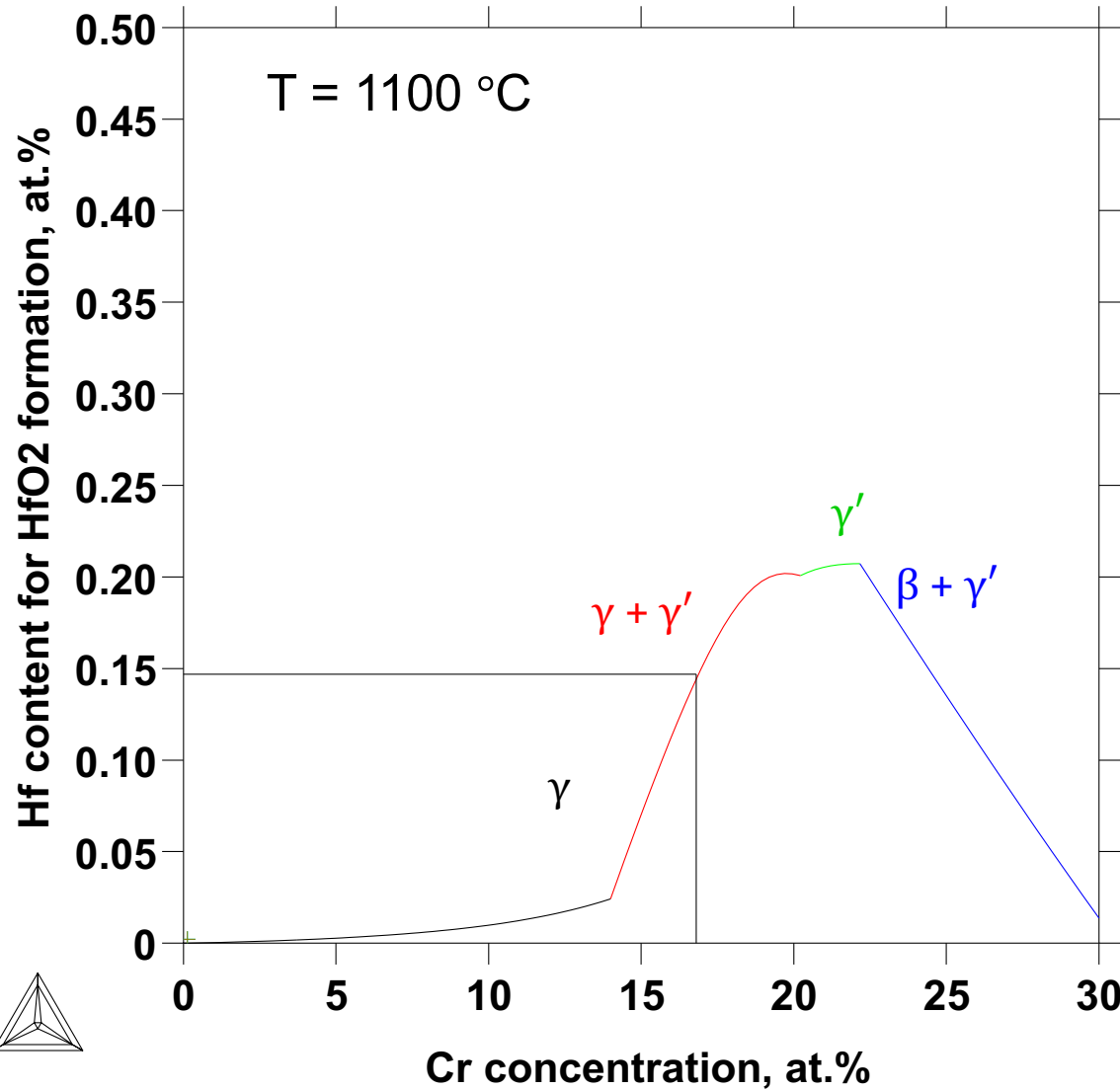
Parameters:  
 $f_{\gamma'} = 0.57$   
 $\chi_{Al} = 17 \text{ at}\%$   
 $\chi_{Cr} = 8 \text{ at}\%$

Alloy:  
Ni-17Al-8Cr





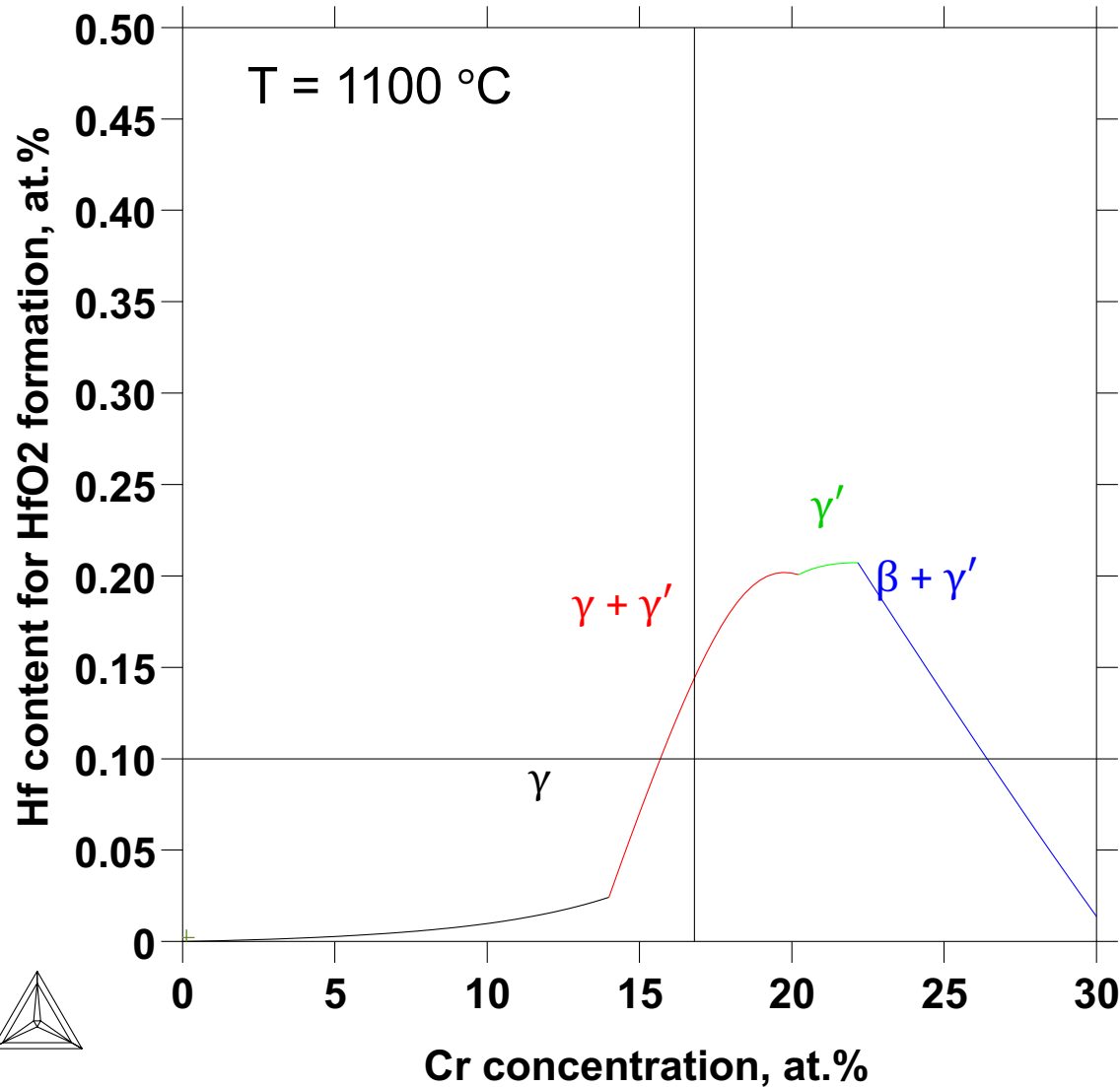
# Engineering a RE-doped Alloy/Coating: Doping with Hf



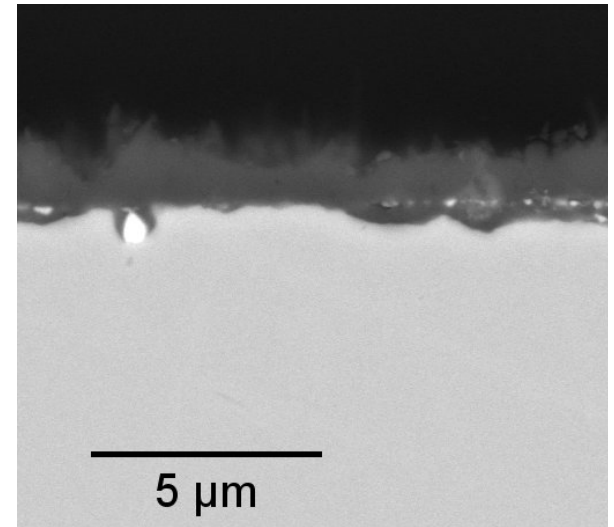
Parameters:  
 $f^{\gamma'} = 0.57$   
 $\chi_{Al} = 17 \text{ at}\%$   
 $\chi_{Cr} = 8 \text{ at}\%$

Alloy:  
Ni-17Al-8Cr-(**<0.15**)Hf

# Experimental Results for Hf Doped Alloy



Alloy:  
Ni-17Al-8Cr-(0.1)Hf



- The  $\gamma'$  phase in Ni-superalloys produces an appreciable decrease in Hf activity compared to the  $\gamma$  phase, resulting in a high solubility of Hf in  $\gamma'$ .
- The Hf tolerance, a thermodynamic criterion for Hf over-doping, was established in terms of the relative stabilities of  $\text{HfO}_2$  and  $\text{Al}_2\text{O}_3$  and , showing excellent agreement with observations in oxidation experiments.
- First-principles calculations were used to predict the effects of alloying elements on Hf tolerance, with favorable results demonstrated for an alloy.
- The developed approach has the potential for applications such as the effects of  $\text{CO}_2$ , steam, and other service conditions.
- Similar approaches may be developed for the  $\text{Cr}_2\text{O}_3$  scale growth.