

# **Additive Manufacturing of Smart Parts with Embedded Sensors for In-Situ Monitoring in Advanced Energy Systems**

**DE-FE0012272**

## **Investigators:**

**Hai-Lung Tsai (PI), Ming Leu, Missouri S&T  
Hai Xiao, Clemson University  
Junhang Dong, University of Cincinnati**

## **Program Manager:**

**Richard Dunst and Otis Mills, NETL**

# Outline

- **Introduction**
- **Technical Progresses and Accomplishments**
- **Summary**
- **Future Work**

- **Sensors and instrumentation are needed in advanced energy systems for**
  - Advanced process control/optimization
  - Health status monitoring of key components
  - System maintenance and lifecycle management
- **Sensors need to survive and operate in the high-T, high-P and corrosive/erosive harsh environments for a long time**

# Traditional Approach

- Traditionally, sensors are attached to or installed onto the component after the structure is fabricated
- **Costly and complicated sensor packaging** are required before installation
- **Poor survivability and reliability** of the sensors
- **Discrepancy** between the sensor reading and the actual status
- Potential **performance compromise** of the host materials/structures



# Opportunities

- **Smart parts – widely used and proven successful in civil engineering for structural health monitoring (SHM)**
- **Provide the real-time information of the component and system**
- **Reduce the complexity in sensor packaging and installation**
- **Increase the robustness and reliability of the system**

# Objectives

- **Main Objective:** Demonstrate the new concept of **sensor-integrated “smart part”** achieved by **additive manufacturing** and embedding **microwave and photonic sensors** into critical components used in advanced energy systems
- **Specific objectives**
  - Robust, distributed and embeddable **microwave photonic sensors**
  - **Additive manufacturing techniques** for rapid fabrication of “smart parts” and sensors embedment
  - Multifunctional **transition layer** between the embedded sensor and host material for **sensor protection** and performance enhancement
  - **Models** to correlate the sensor readings with the parameters of interest
  - Sensor **instrumentation** for *in situ* and distributed measurement
  - Feasibility **tests** and performance **evaluation**

- **Performers: Missouri S&T, Clemson, University of Cincinnati**
- **Interdisciplinary team**
  - Hai-Lung Tsai (PI), Professor of Mechanical Engineering, Missouri S&T, Modeling and AM of metal parts
  - Ming Leu, Professor of Mechanical Engineering, Missouri S&T, AM of ceramic parts
  - Hai Xiao, Professor of Electrical Engineering, Clemson University, Sensors and Instrumentation, test and evaluation
  - Junhang Dong, Professor of Chemical Engineering, University of Cincinnati, Sensor protections
- **Success criteria:**
  - Demonstrate concept and capability in simulated laboratory environments

# **Development of robust, distributed and embeddable sensors and instrumentation**

**Approach: Fully distributed microwave photonic fused silica  
and sapphire fiber sensors**

**Hai Xiao  
Clemson University**

- **Three types of fully distributed sensors for embedded applications**
  - 1. Microwave sensors** – uniquely harvest the robustness of high temperature coaxial cables
  - 2. Incoherent Optical carrier based microwave interferometry (OCMI) sensors** – can be used to interrogate previously difficult highly multimode fibers (e.g., quartz rod and sapphire fiber)
  - 3. Coherent OCMI sensors** – can reach extremely high resolution

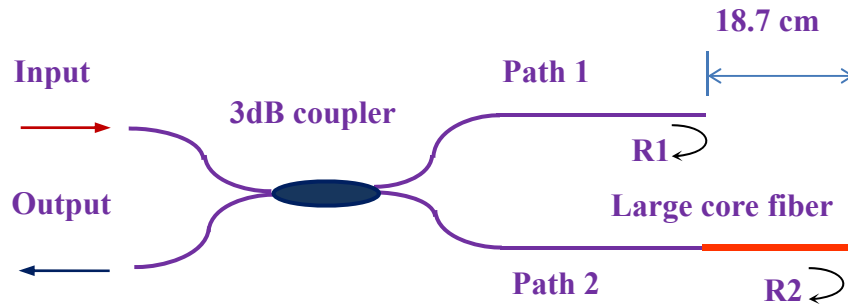
- **Optical carrier based microwave interferometry (OCMI)**
  - Read optical interferometers using microwave
  - Optics as the carrier to perform measurement
  - Microwave as the signal to locate the sensors
  - Can be implemented in either **incoherent (make the optical term become zero)** or **coherence (keep the optical term)**

Microwave term

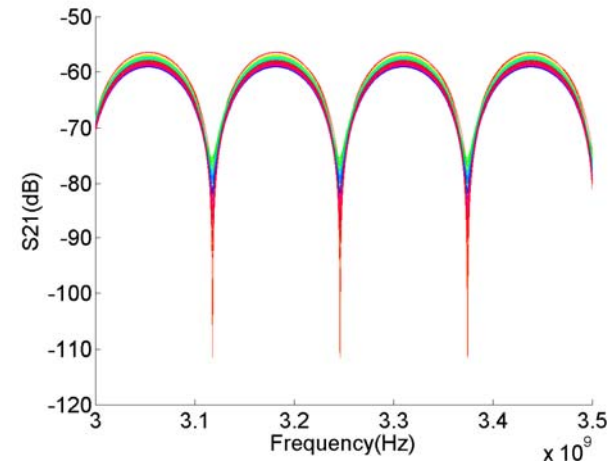
$$|E|^2 = |E_1 + E_2|^2 = 2A^2 + 2A^2 M \cos \left[ \Omega \frac{L_{O1} - L_{O2}}{2c} \right] \cos \left[ \Omega \left( t + \frac{2W + L_{O1} + L_{O2}}{2c} \right) \right]$$

$$+ 2A^2 \sqrt{\left\{ 1 + M \cos \left[ \Omega \left( t + \frac{W + L_{O1}}{c} \right) \right] \right\} \left\{ 1 + M \cos \left[ \Omega \left( t + \frac{W + L_{O2}}{c} \right) \right] \right\}} \cdot \int_{\omega_{\min}}^{\omega_{\max}} \cos \left( \omega \frac{L_{O1} - L_{O2}}{c} \right) d\omega$$

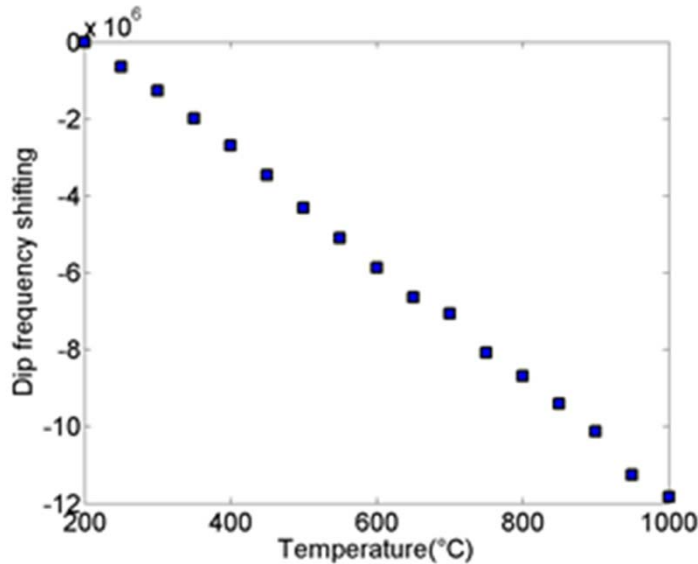
Optical term



**Fused silica rod 800 $\mu$ m dia.**

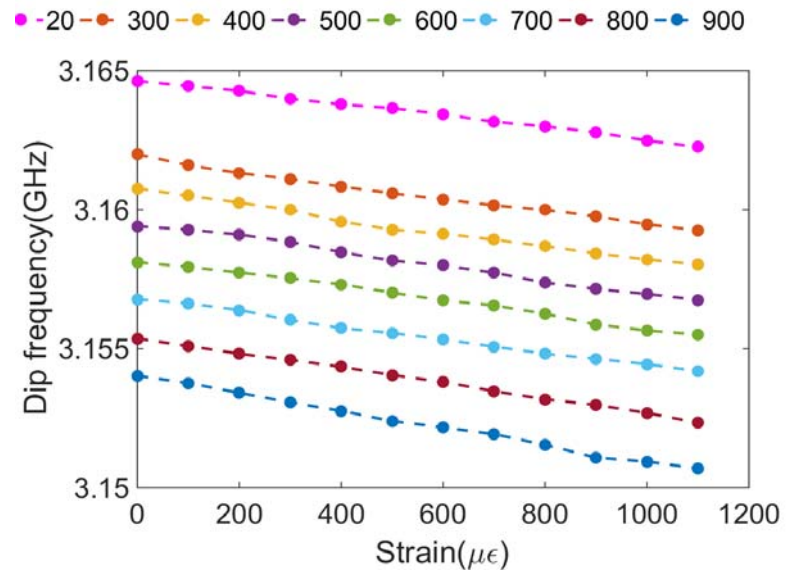


**Interference fringes**

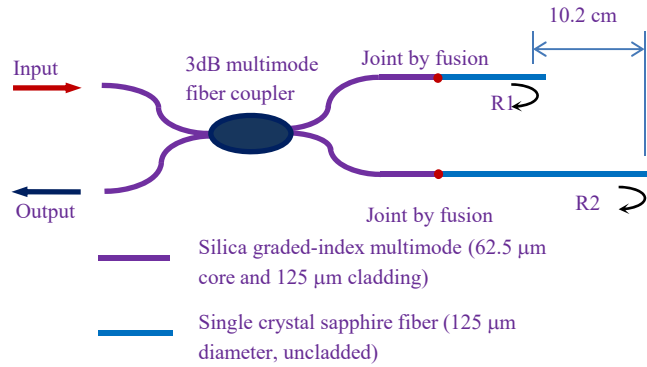


**High temperature response**

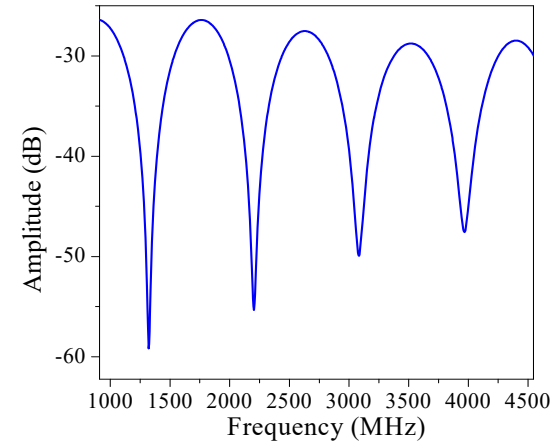
*L. Hua., Applied Optics, 2015*



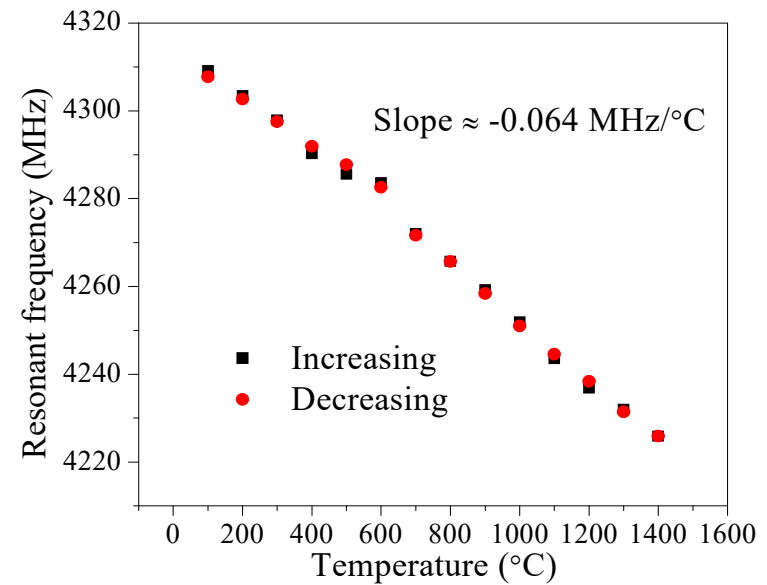
**Quartz rod can be used to measure strains at high temperatures**



**Sapphire fiber Michelson OCMI**



**Excellent fringe visibility > 30dB**

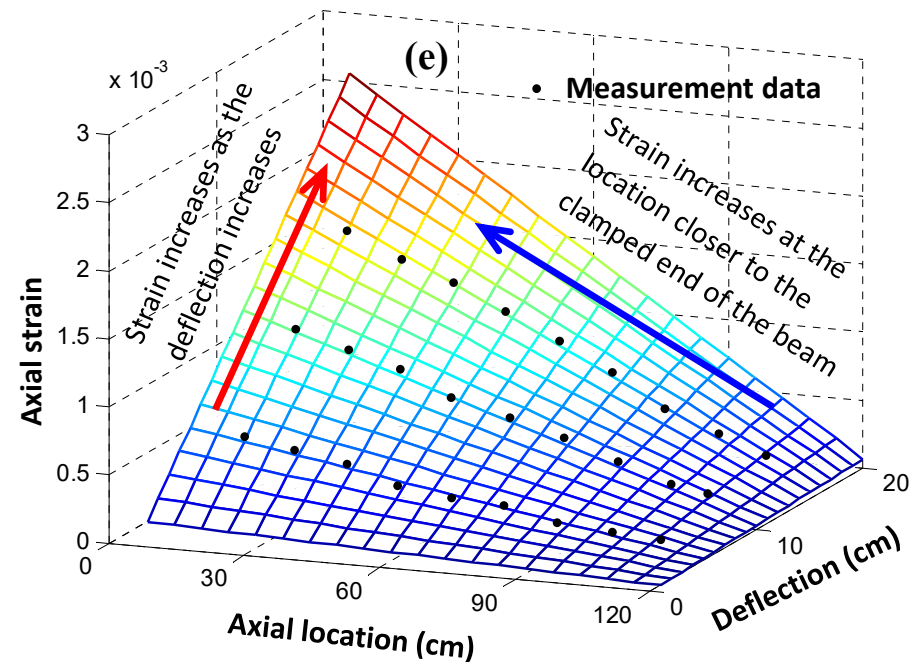
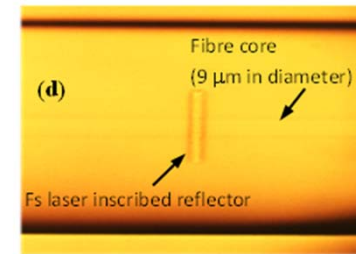
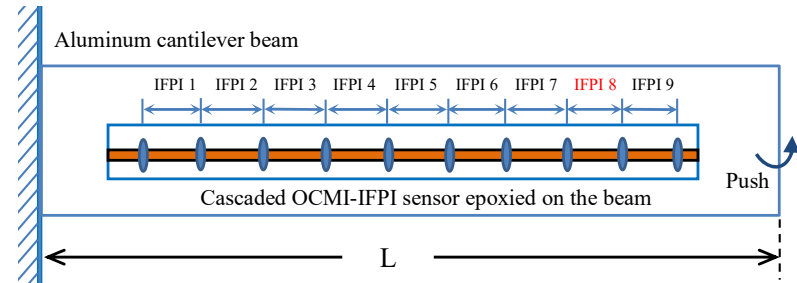


**J. Huang, et al., *IEEE Photonics Technology Letters*, 2015.**

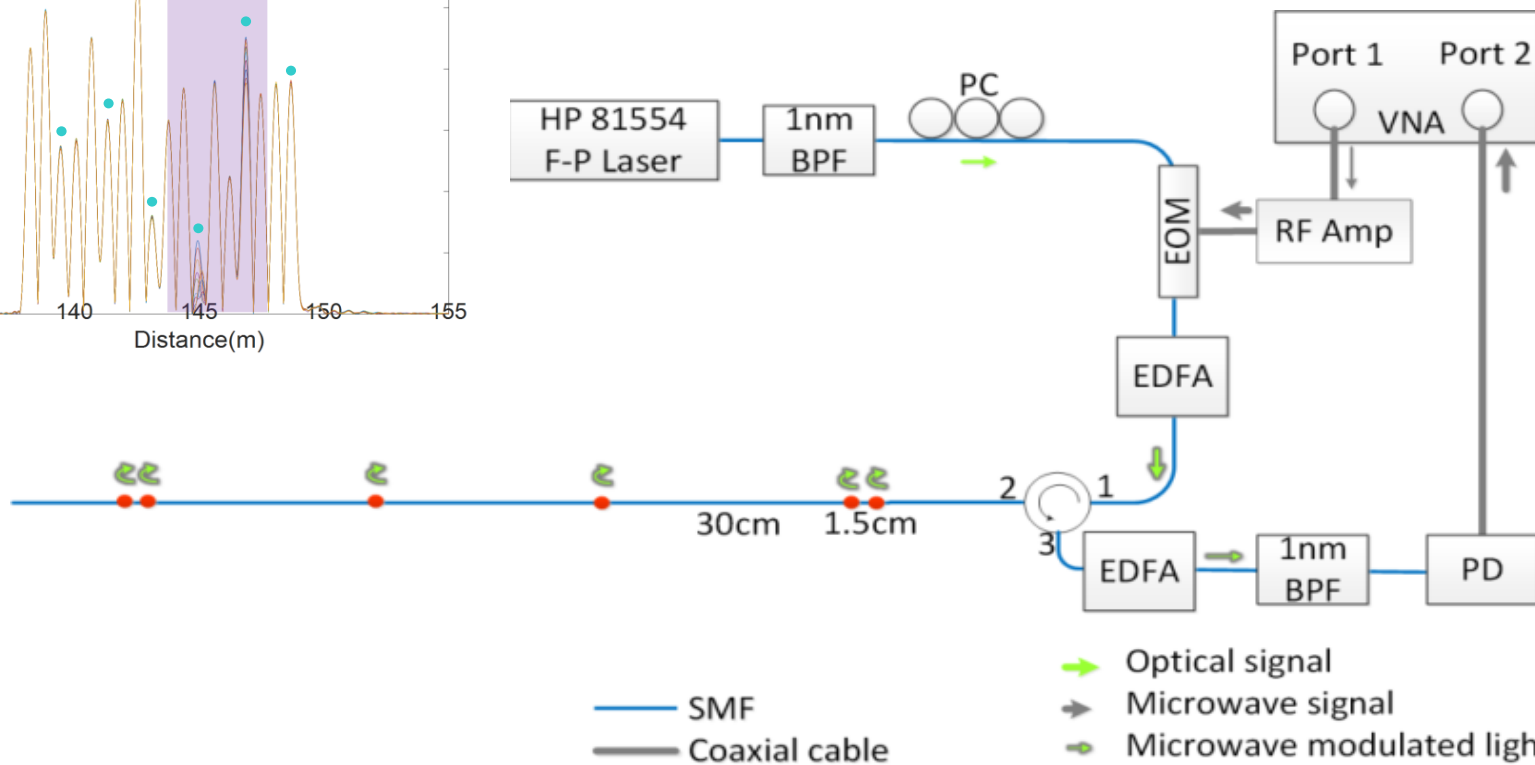
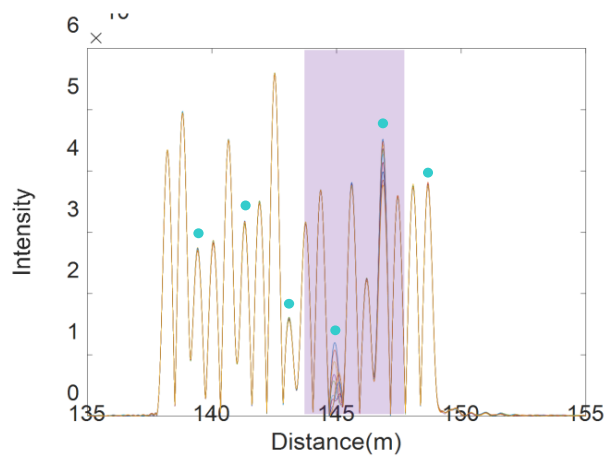


- Spatially continuous (no dark zone), fully distributed sensing.
- High spatial resolution (<1cm)
- High sensitivity ( $\sim\mu\epsilon$ )
- Flexible gauge length (1cm – 100m)
- Long reaching distance ( $\sim$ km)
- Can be implemented using various fibers including sapphire and quartz rods

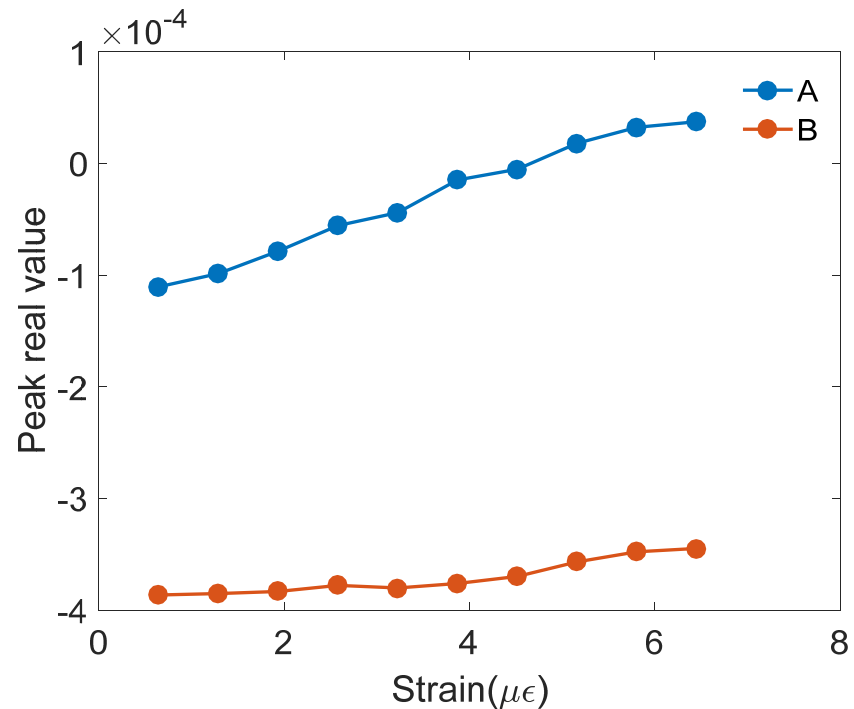
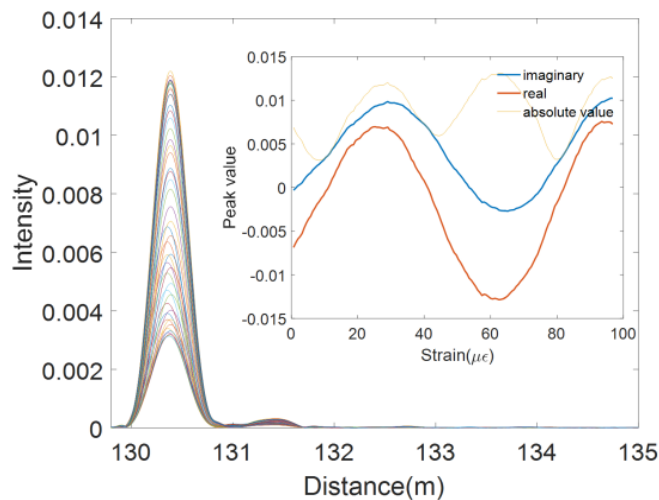
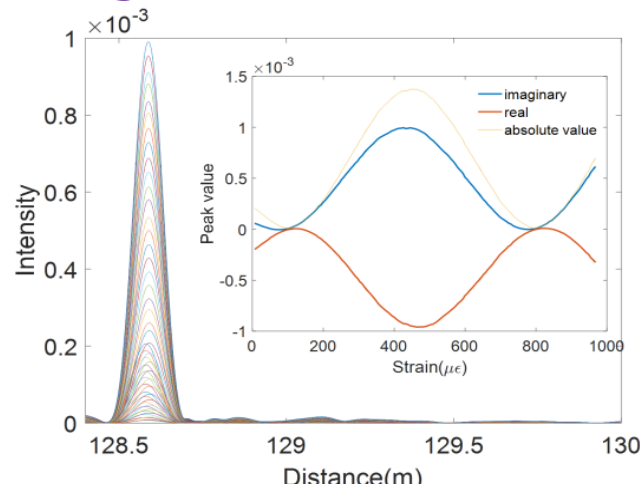
J. Huang, et al., *Optics Express*, 2014.



- Use a coherent light source
- Arrange the interferometers within the coherent length of the source



- Use both real and imaginary part of the signal (quadrature)
- Resolution reaches  $10\text{n}\epsilon$  using an interferometer with a length of 10cm.

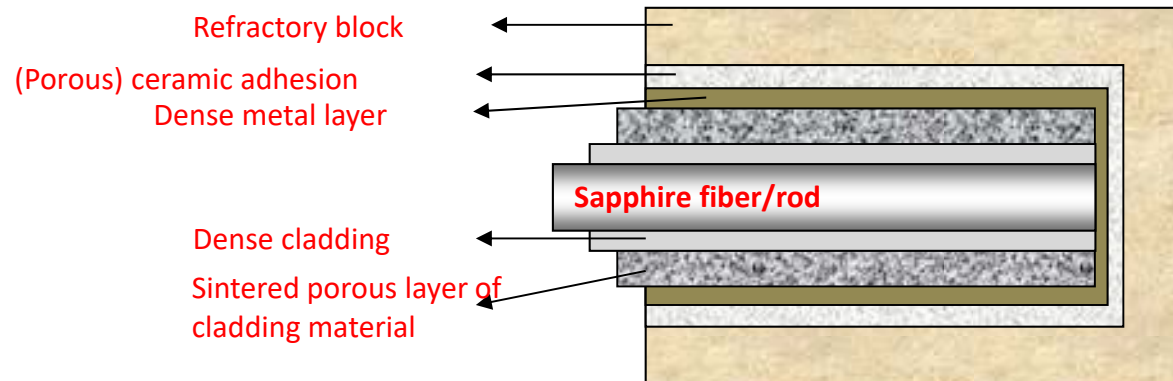


- **Incoherent OCM** – use incoherent (i.e., broadband) optical source
  - Large dynamic range
  - Resolution is limited, about  $10^{-5}$  -  $10^{-6}$
- **Coherent OCM** – use coherent (i.e., narrow bandwidth) optical source
  - Limited dynamic range
  - Resolution can be extremely high, about  $10^{-8}$  -  $10^{-9}$
- **The two can be combined into a single system with two optical sources to achieve a high resolution in a large dynamic range.**
  - Sensing Range (Spatial resolution): 100 km(1m), 2km(2cm)

# Develop a multifunctional transition layer between the embedded sensor and the host material for sensor protection

Approach: Design and select ceramic and metal materials based on structural and chemical potteries

Junhang Dong,  
University of Cincinnati

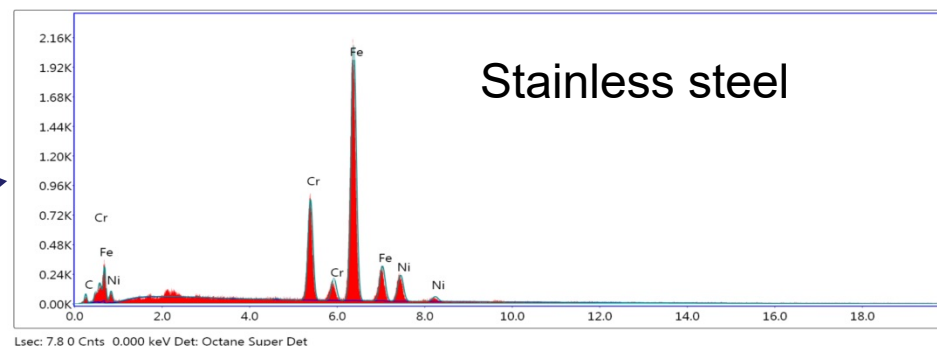
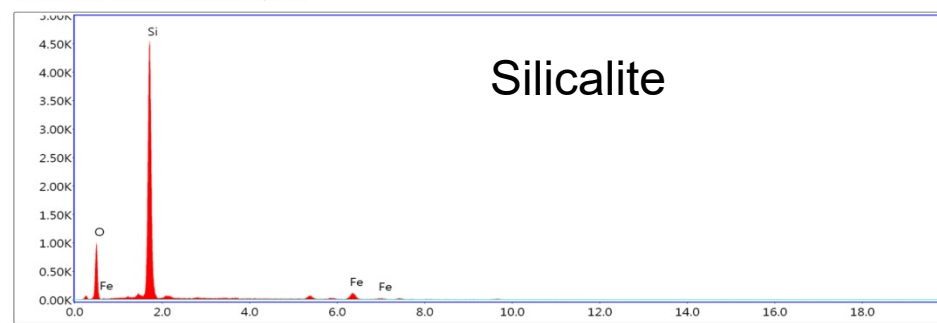
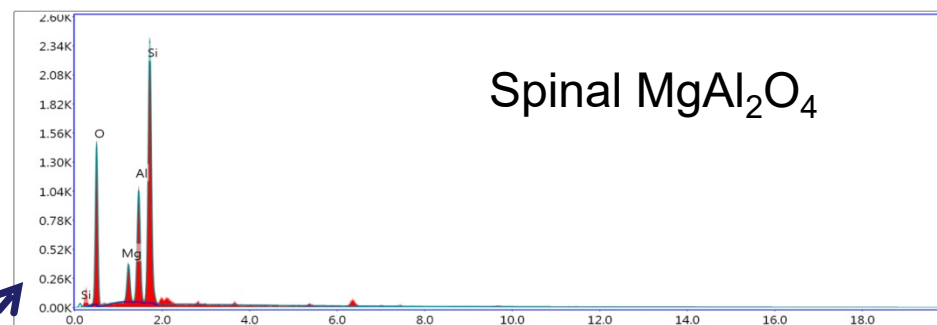
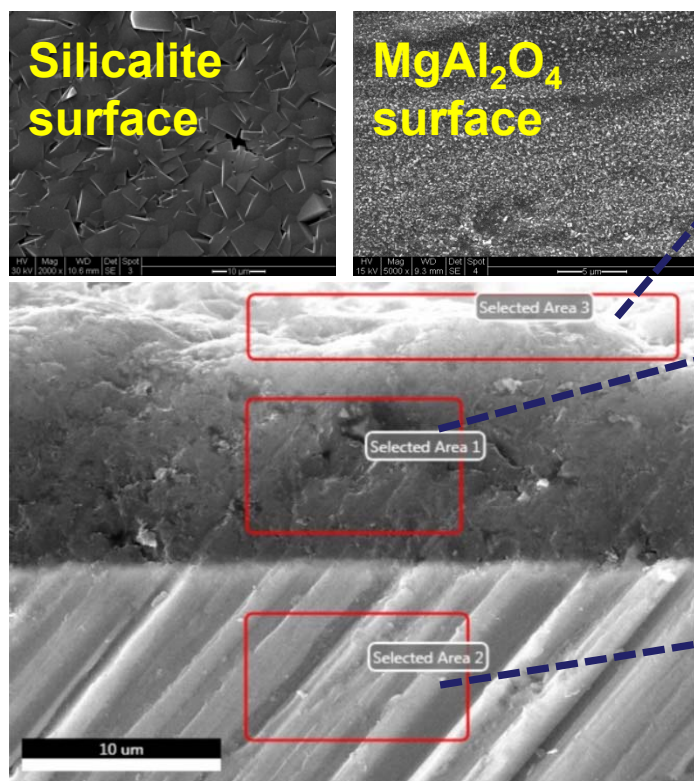


# Summary of Accomplishments

- **Silica fiber optic sensors packaged in the ceramic host capillary tubes are fully functional at high temperature (tested up to 1000°C) with good stability**
- **Silicalite layers directly grown on the sapphire fibers may be used both as fiber cladding and sensor protection (up to ~900°C)**
- **MgAl<sub>2</sub>O<sub>4</sub> layers can be used as sapphire cladding for operation up to 1250°C.**

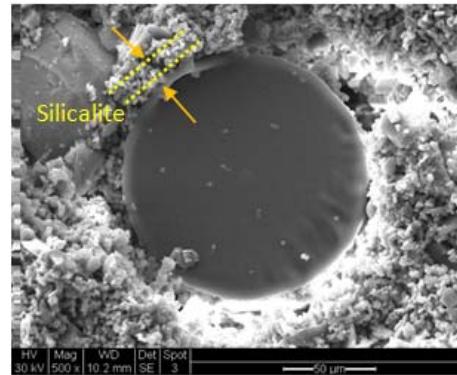
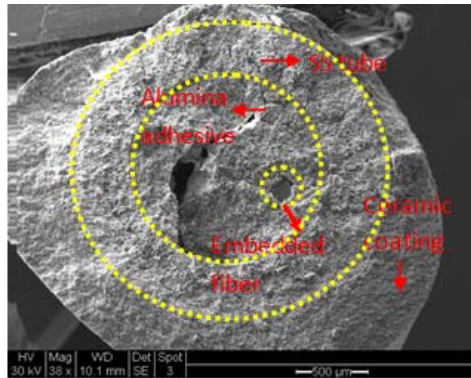
# Interface Stability in Layered Structure for Sensor Protection

**Results:** Stainless steel has been identified as the most stable metal among the candidates (Ti/Pd, Al, Cu, etc.) and demonstrated to be stable when coated with ceramics at  $1000^{\circ}\text{C}$  for  $>100\text{h}$



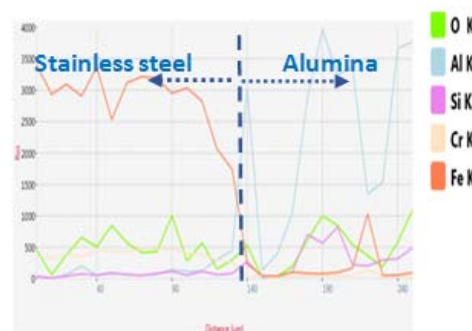
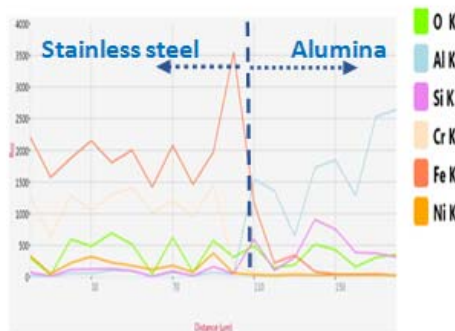
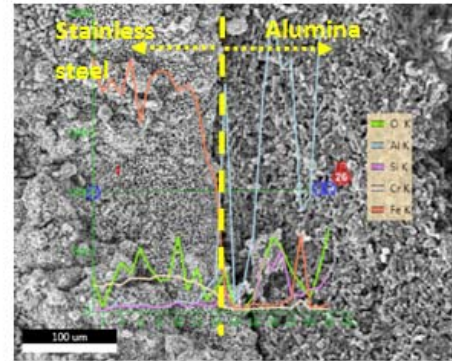
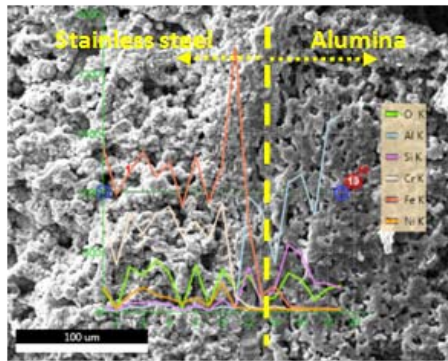


# Sensor Protection by ceramic adhesive in sintered SS capillary tube



## Stainless steel hosted fiber unit:

Fused silica optical fibers as a packaged sensor unit for direct installation in “smart bricks”. Porous ceramic adhesion layers (e.g. alumina and zirconia based materials) used to fix the fiber with the host capillary tube.

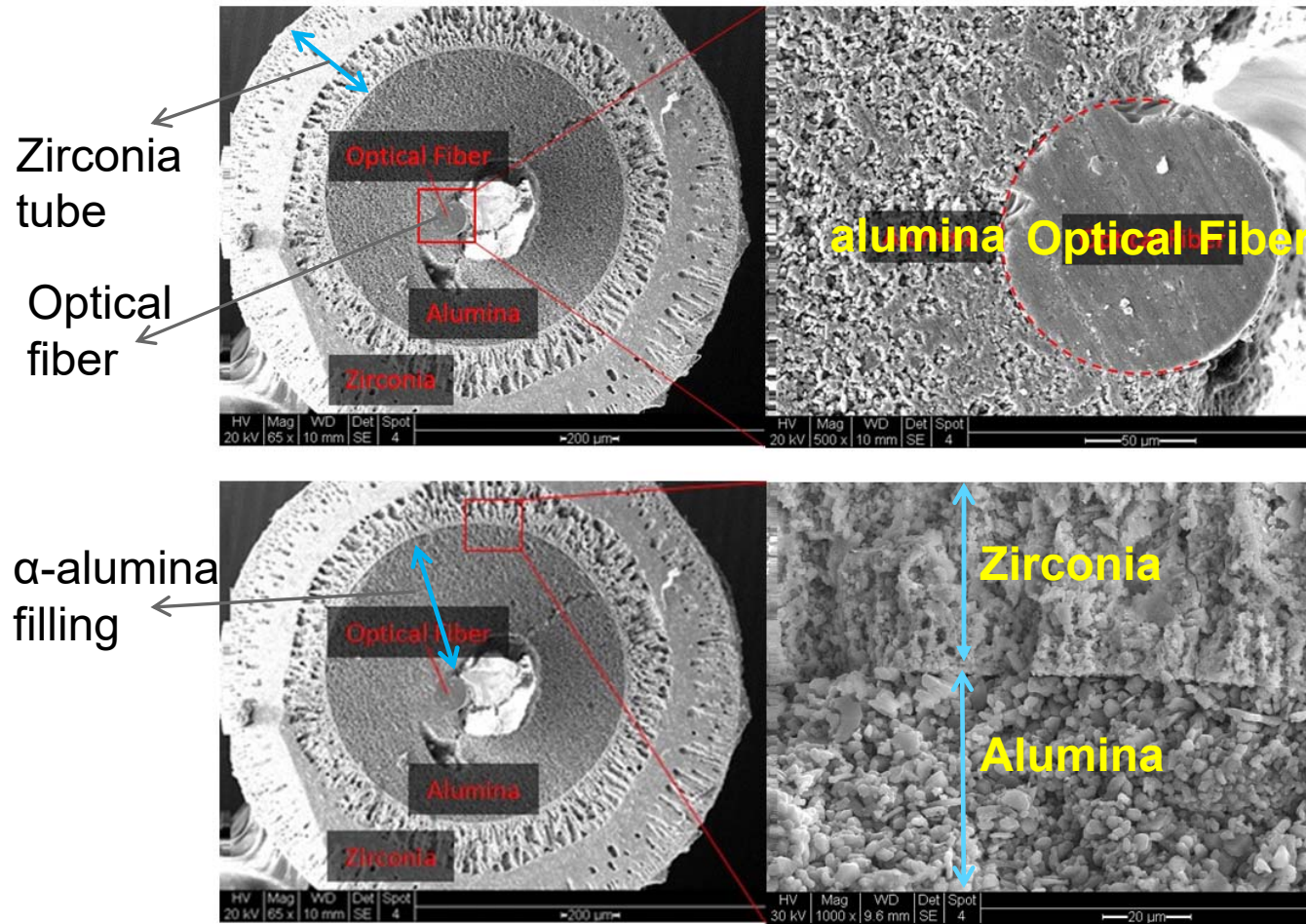


EDS line scan across the SS/alumina interface/fiber interfaces indicated no significant solid state reaction or diffusion at 1000<sub>o</sub>C over extended period.

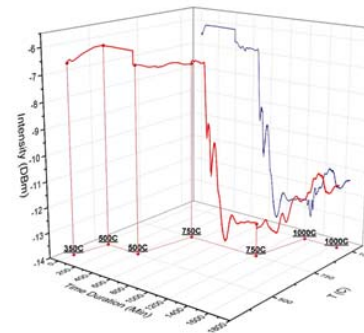
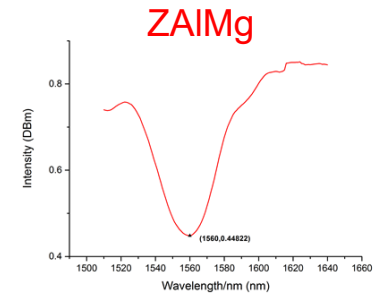
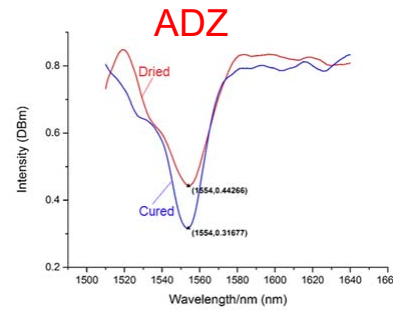
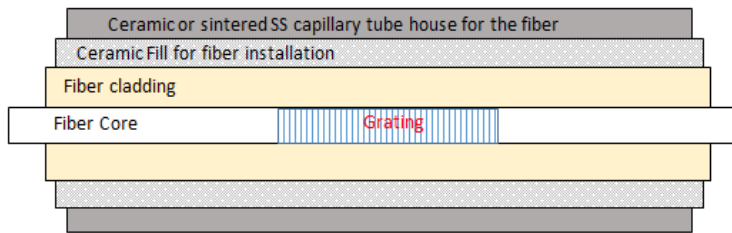
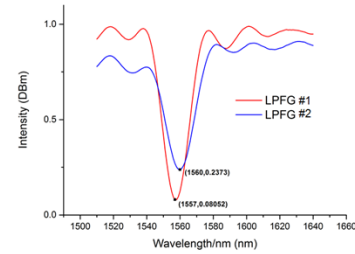
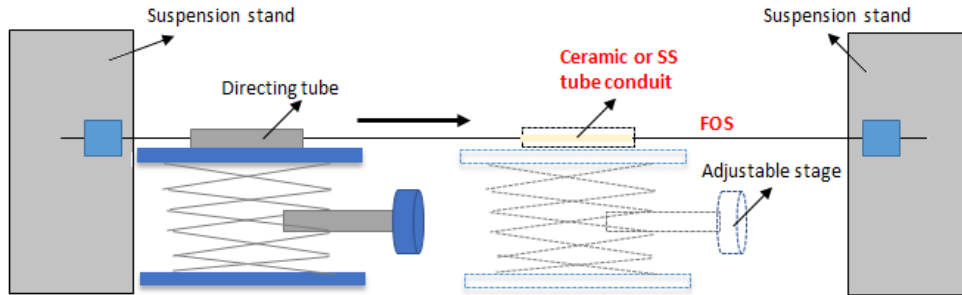


# Sensor Protection by ceramic adhesive in ceramic capillary tube

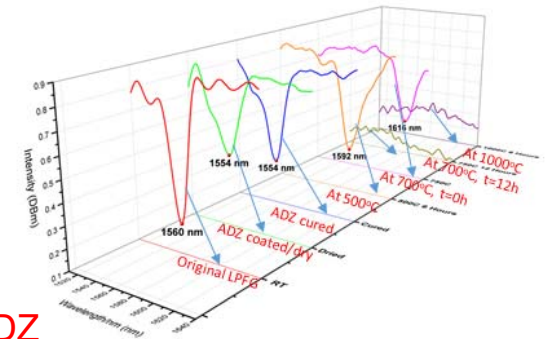
Results: pre-packaging of fibers in ceramic capillary tubes (e.g. porous zirconia and  $\alpha$ -alumina) has been demonstrated using ceramic adhesion and tested at 1000°C stable over extended periods.



# Packaging of Fiber Optic Sensor in Host Ceramic (or SS) Capillary Tubes

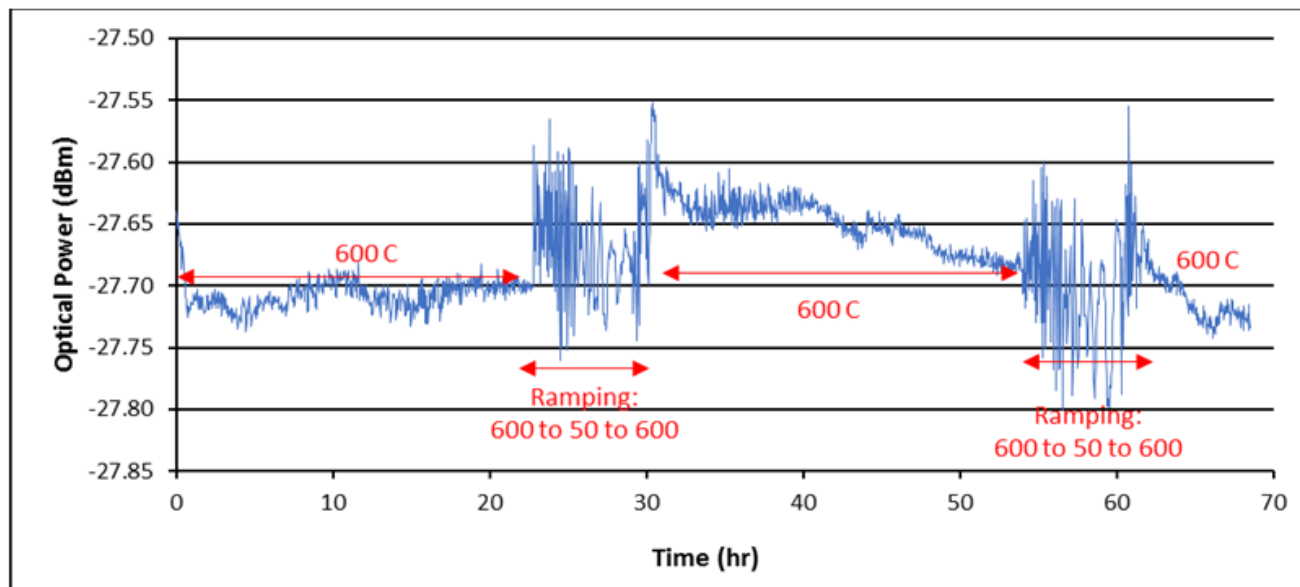
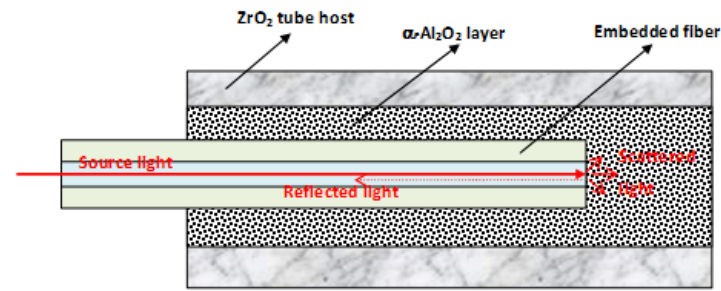


ADZ

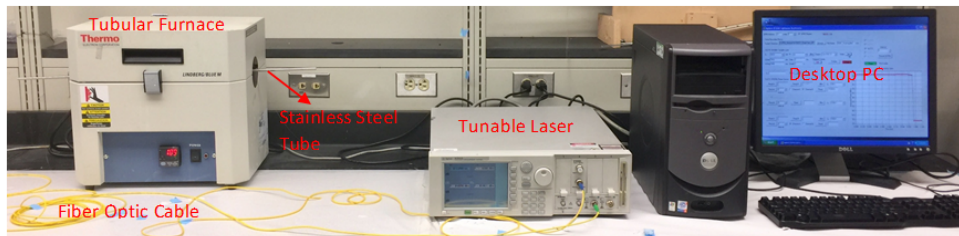
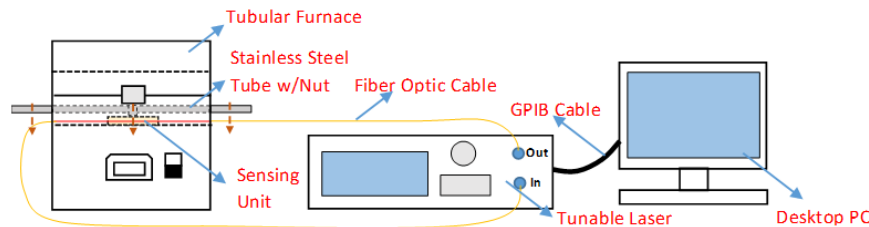
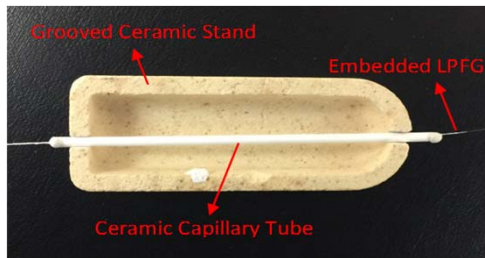
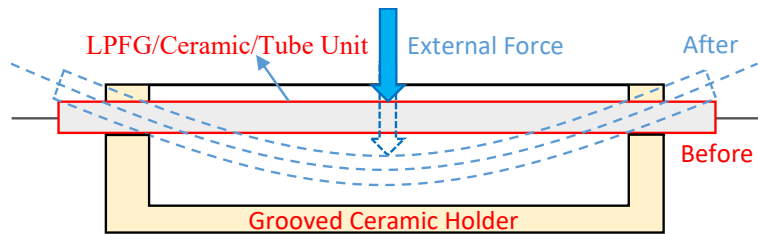


# Optical Functionality Tests for the Fiber Sensor in Capillary Tubes

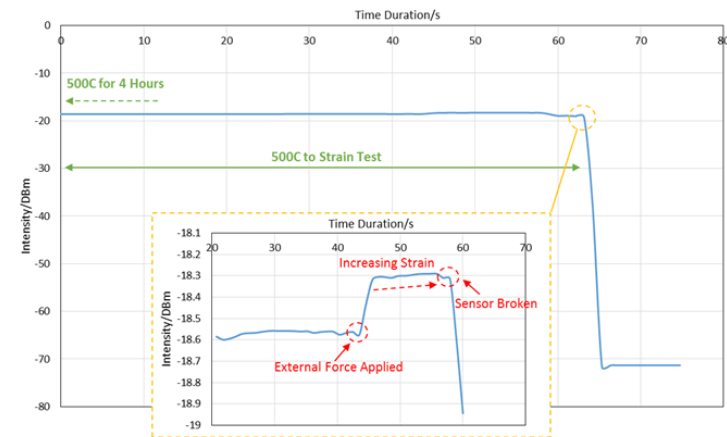
**Results:** *The fibers pre-packaged in the host tubes have been verified to be optically functional for signal generation and transmission at high temperatures*



# Test of Packaged Fiber Sensor (LPG) for Monitoring Strain and breakage



A fused silica LPG sensor was packaged in a ceramic capillary and connected to a tunable laser for monitoring strain and structure damage at high temperature. The packaged sensor was able to detect the external force induced strain and fracture of the packaged unit that indicate promise for installation in refractory liners for structural health monitoring.

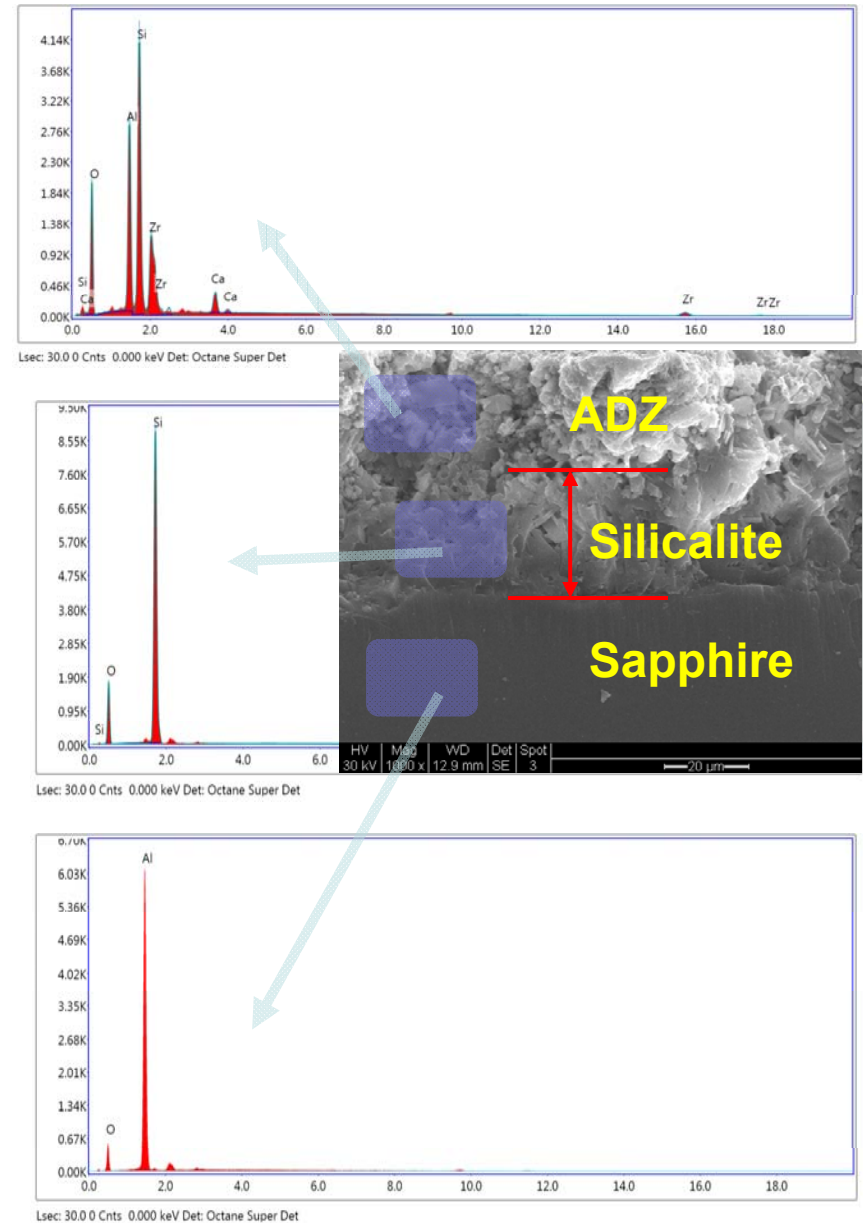
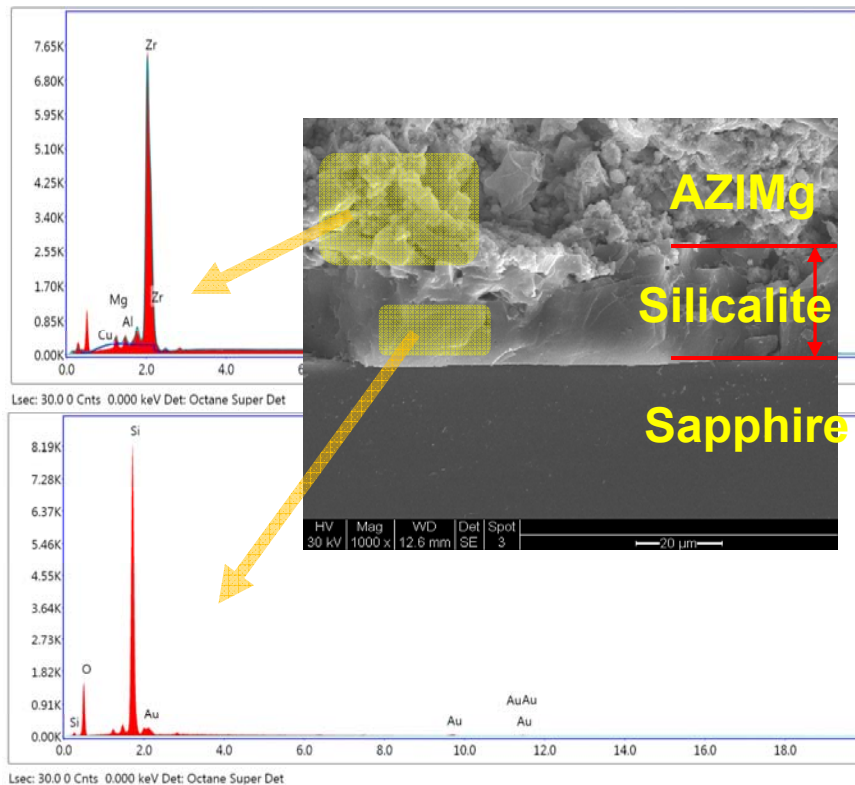


Single wavelength ( $\lambda=1612$  nm) transmission intensity as a function of time at 500°C.



# Long-Term Stability of Sapphire Multilayer Protection

The structures of silicalite-coated-sapphire with an overcoats of ZAlMg ( $ZrO_2$ - $Al_2O_3$ -MgO mixture) and ADZ ( $Zr_{1-0.75x}Al_xSiO_4$ ) are both stable after firing at **1000°C for 200 h** according to SEM and EDS examinations – No structural damage or inter-layer element diffusion was found.



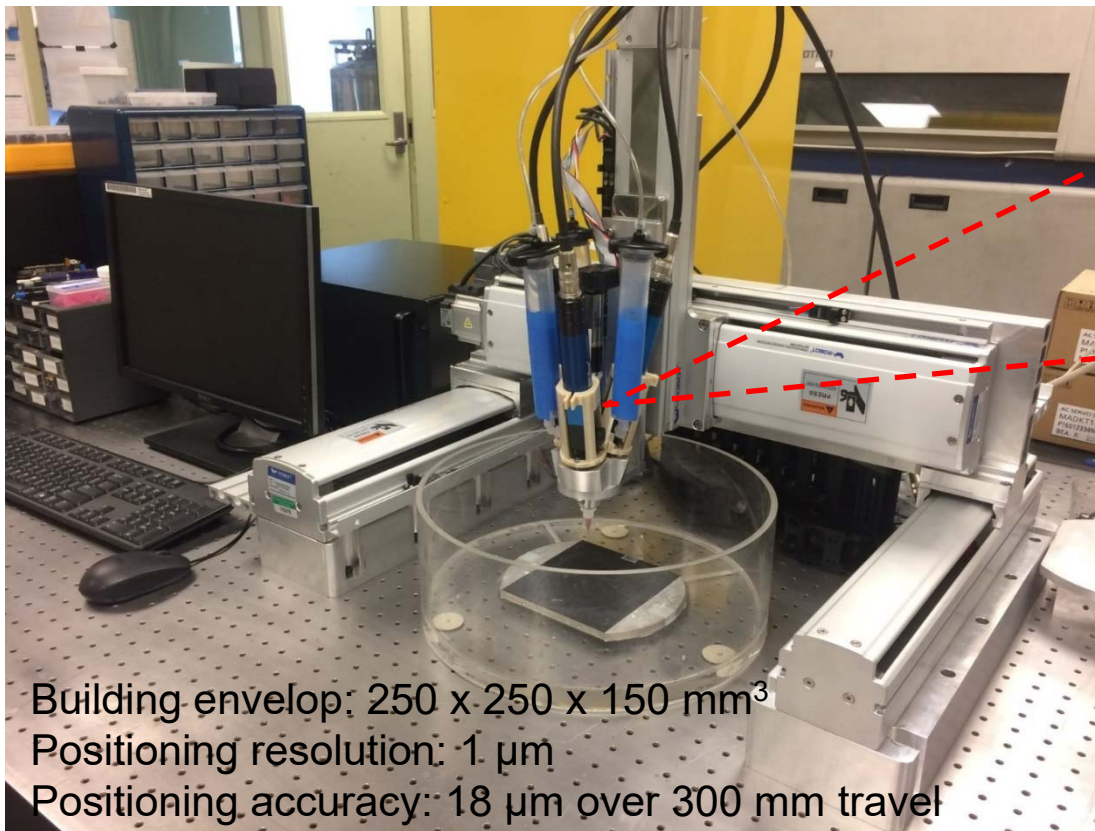
# **Additive Manufacturing of Ceramics**

**Approach: Multi-extruder freeze-form extrusion based  
additive manufacturing**

**Ming Leu**

**Missouri University of Science and Technology**

- A new ceramic on-demand extrusion (CODE) system has been developed to fabricate Functionally Graded parts (Configuration 1) and Multi-Material parts (Configuration 2).



**Config. 1**  
FGM  
printing

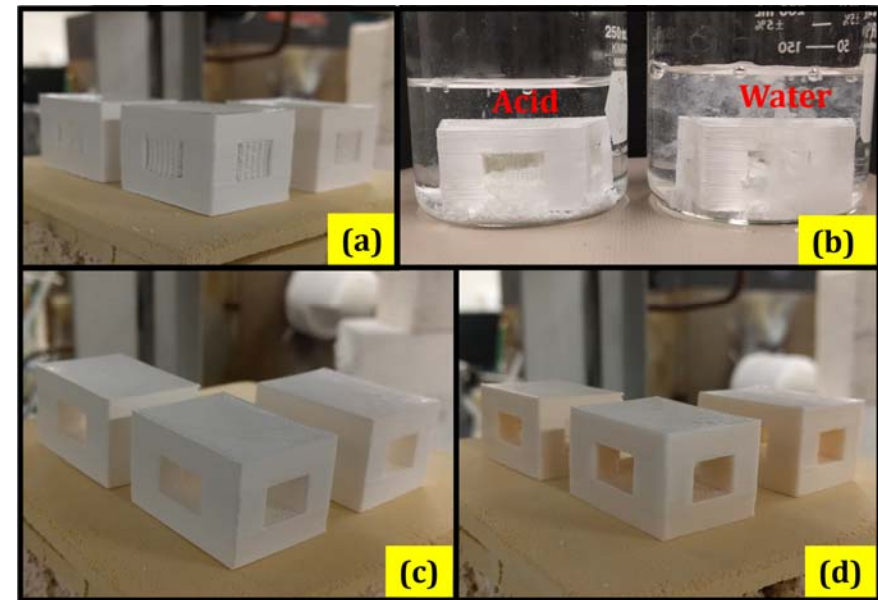
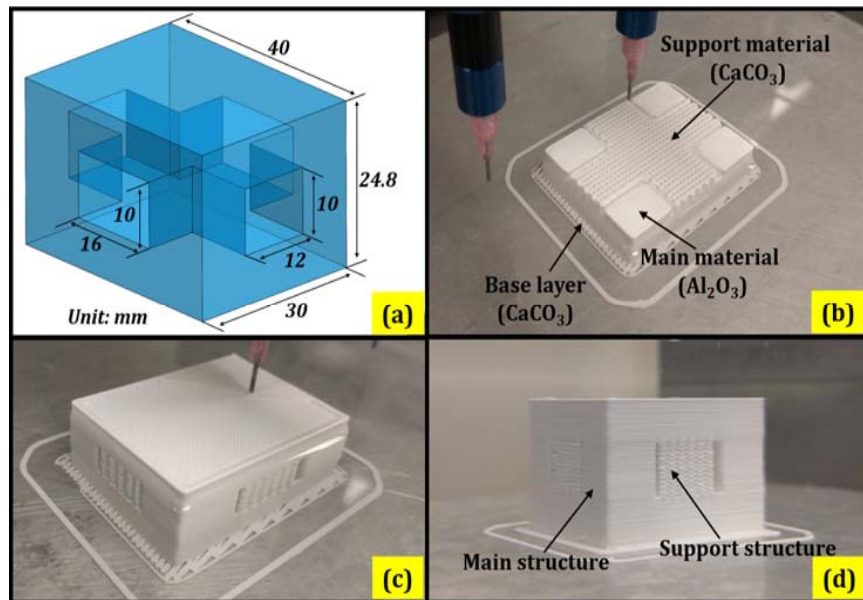


**Config. 2**  
Multi-  
material  
printing

# Fabricating Parts with Support Material

## Printing

## Post processing

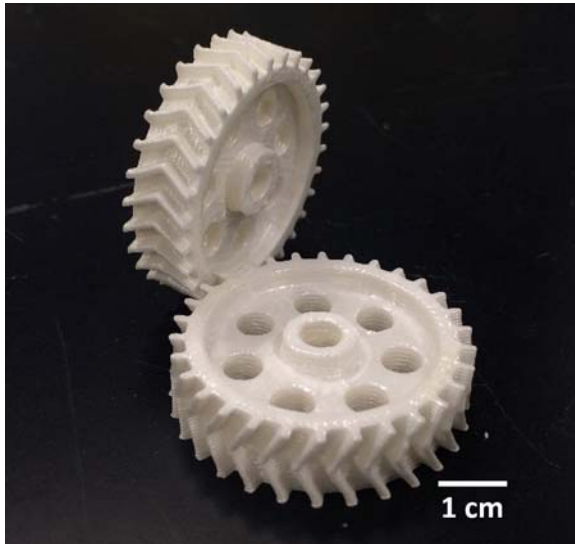


- (a) CAD model
- (b) Support structure being printed
- (c) Overhanging structure being printed
- (d) Part having been printed completely (surrounded by oil)

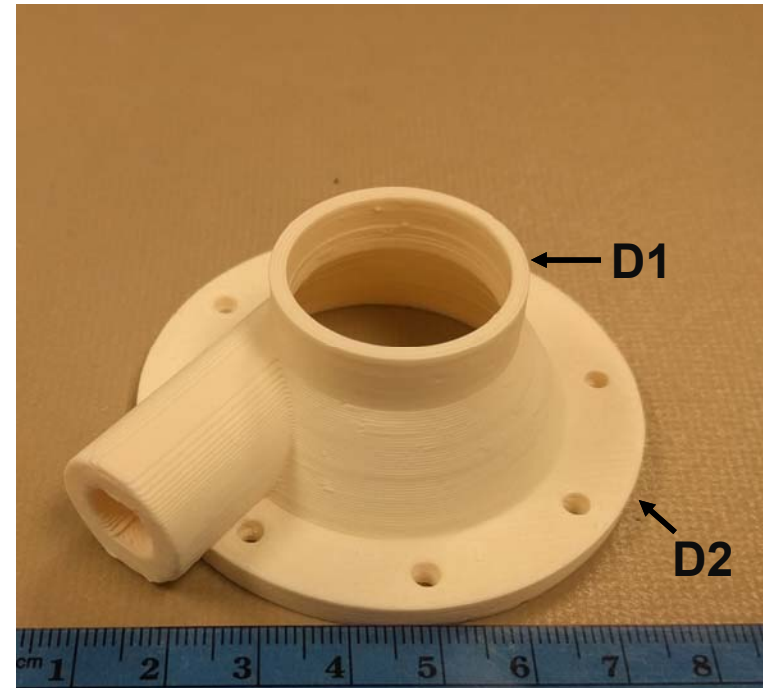
- (a) Parts after 1<sup>st</sup> step sintering (1100 °C)
- (b) Support structures being dissolved
- (c) Cleaned parts (after support removal)
- (d) Final sintered parts



# Sample Parts Fabricated with the CODE System



**Zirconia gears:**  
 400  $\mu\text{m}$  layer  
 98.5% Density

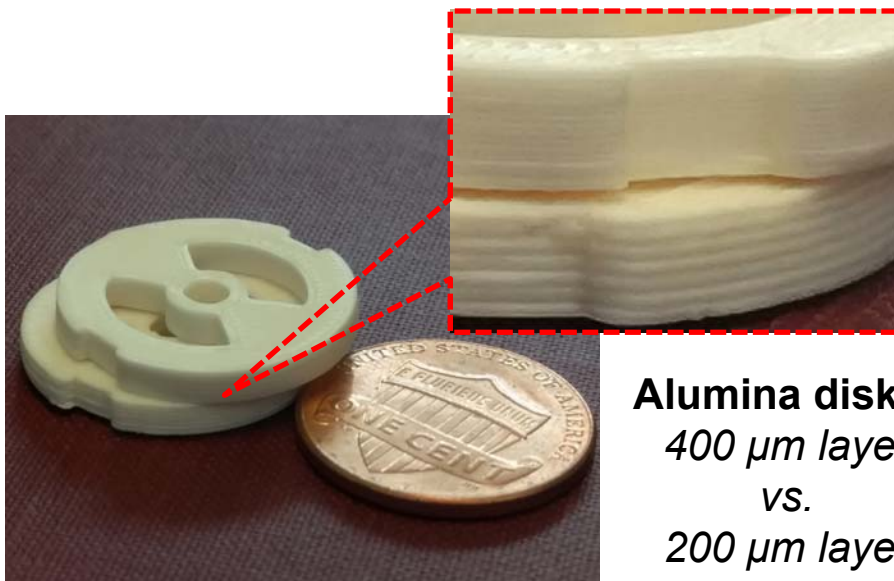


**Alumina turbine blower housing**  
 400  $\mu\text{m}$  layer, 97.5% density

*Good circularity*

D1: Mean = 29.3 mm, Std.Dev. = 0.07 mm

D2: Mean = 63.7 mm, Std.Dev. = 0.05 mm



**Alumina disks:**  
 400  $\mu\text{m}$  layer  
 vs.  
 200  $\mu\text{m}$  layer

# **Additive Manufacturing of Metals**

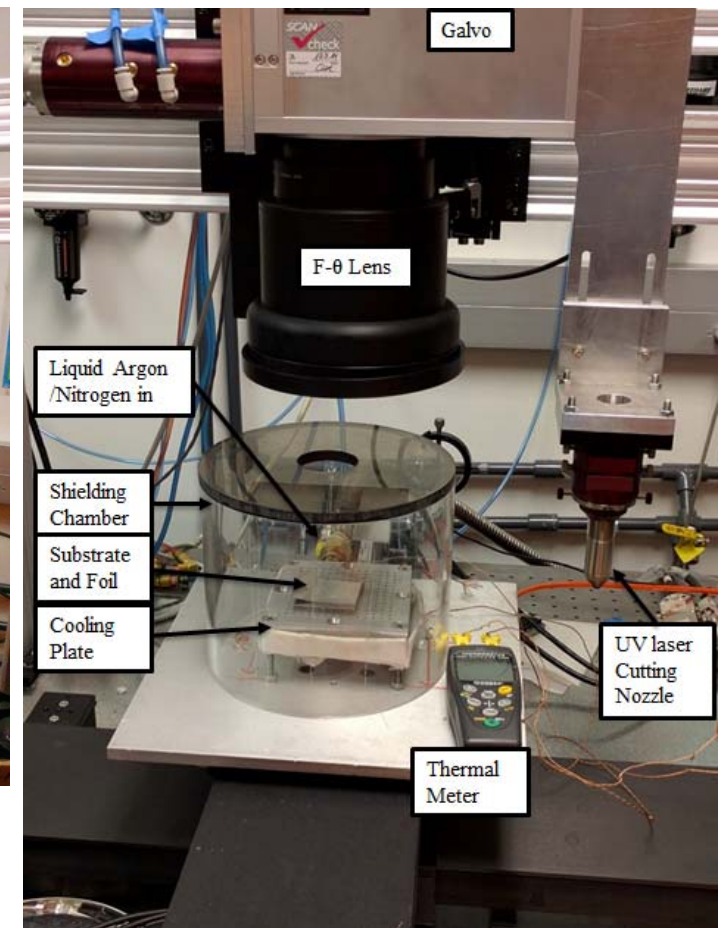
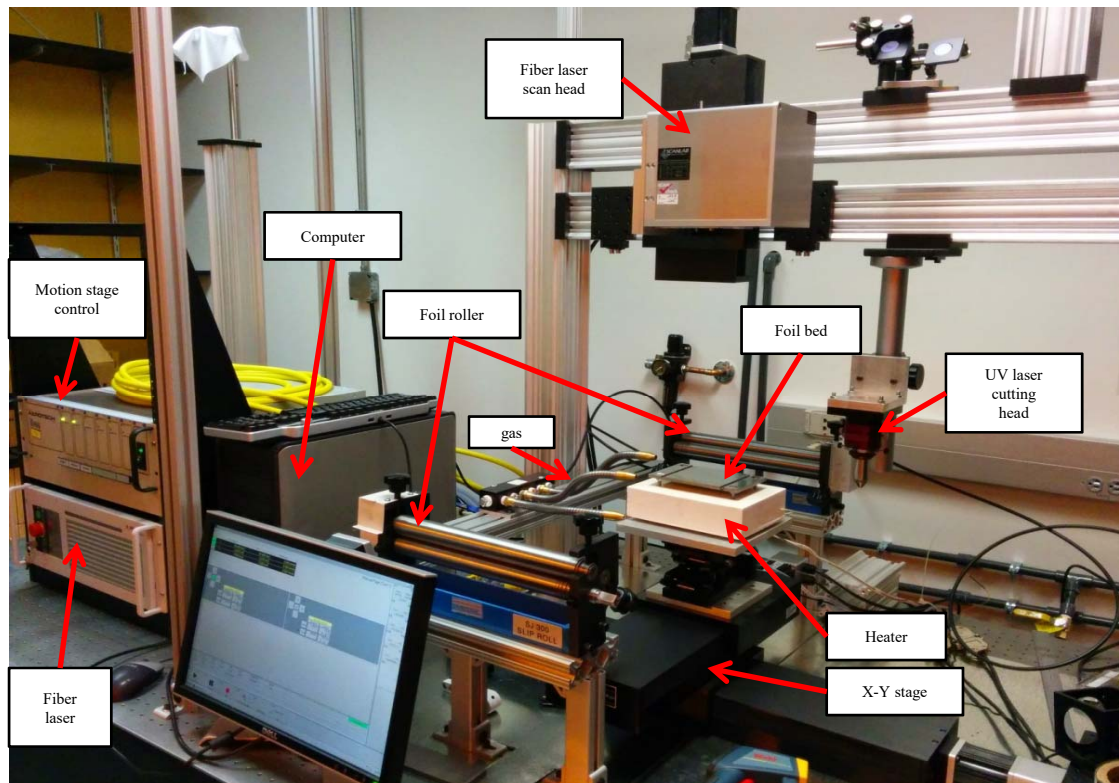
**Approach: Foil-Based Dual-Laser Additive Manufacturing  
Technology**

**Hai-Lung Tsai**

**Missouri University of Science and Technology**

# Laser-Foil-Printing AM Technology

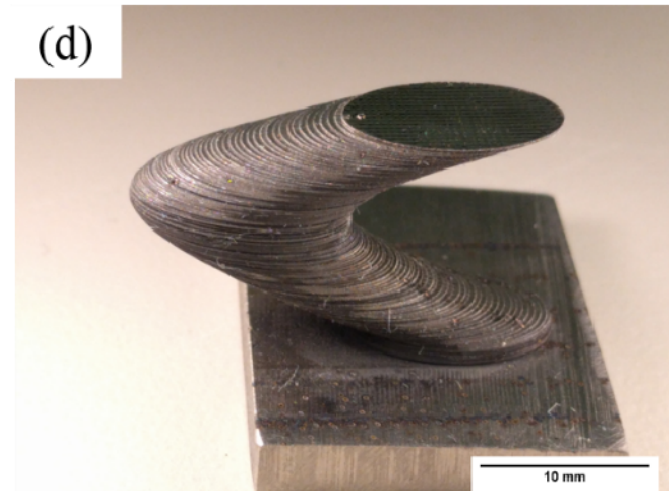
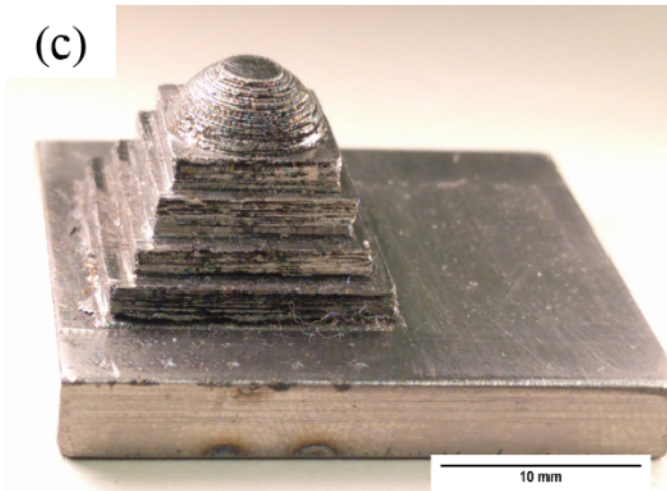
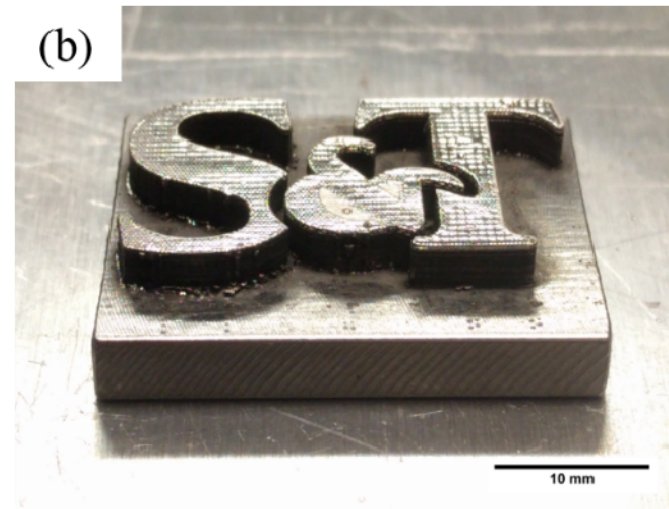
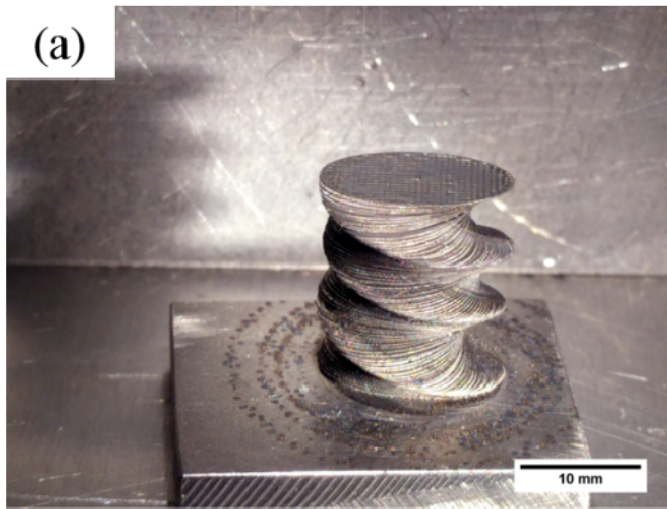
- System Design, Hardware and Software Implementations, and Integration.



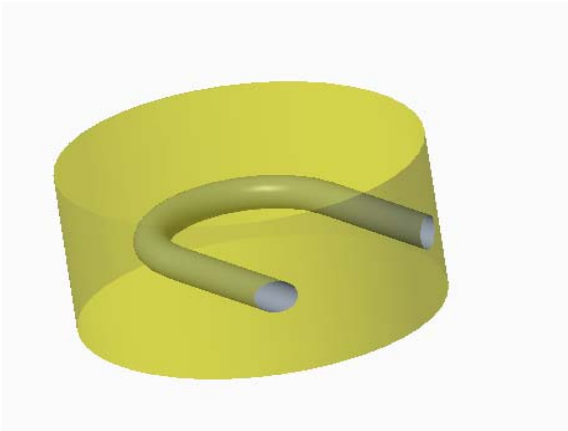
31



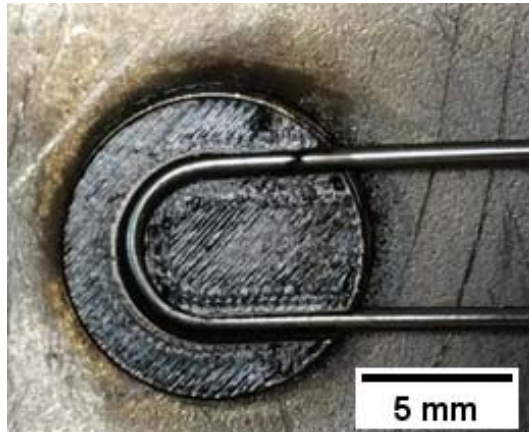
# As-Fabricated Metallic Glass Samples



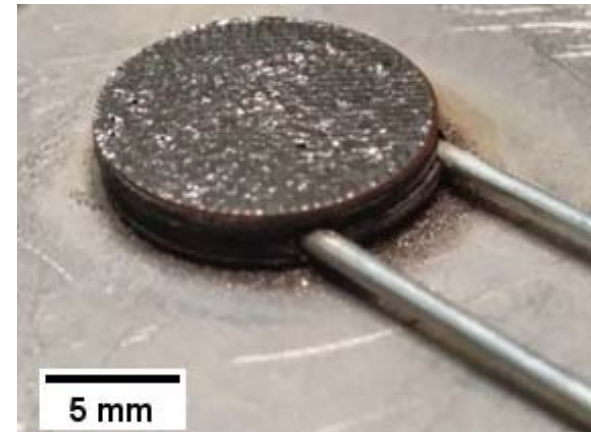
# Sensor-Embedded Parts Fabrication



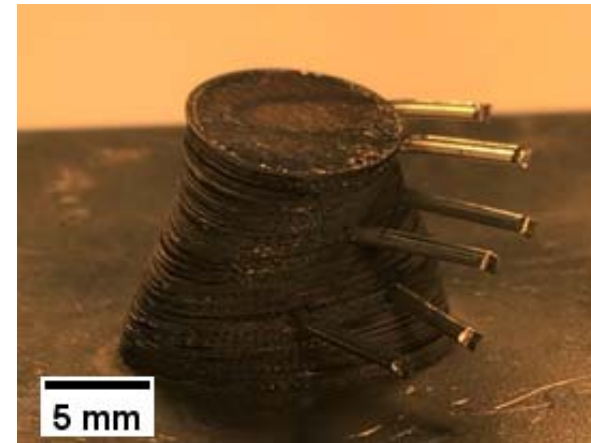
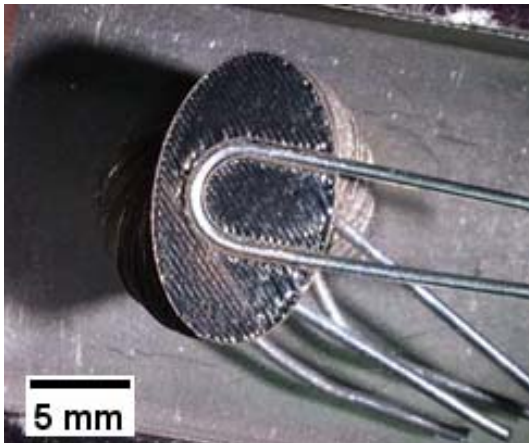
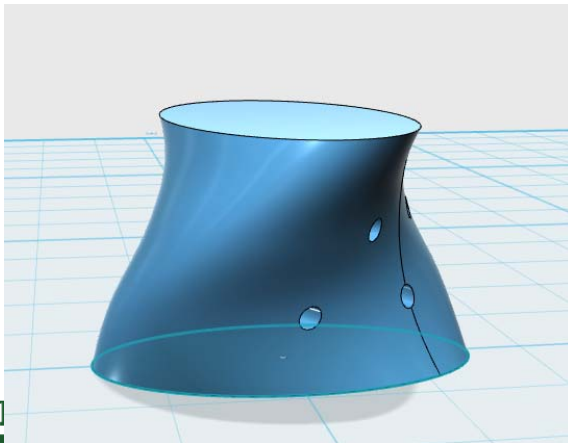
3D models for sensor embedding.



Curved sensors to be embedded in the printing process.

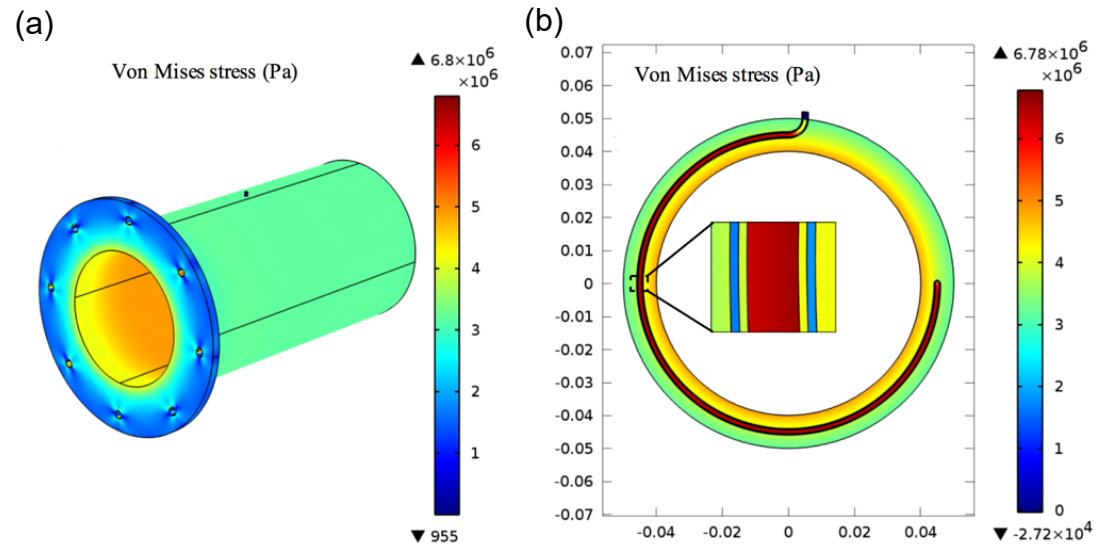


Sensors are embedded in the parts.

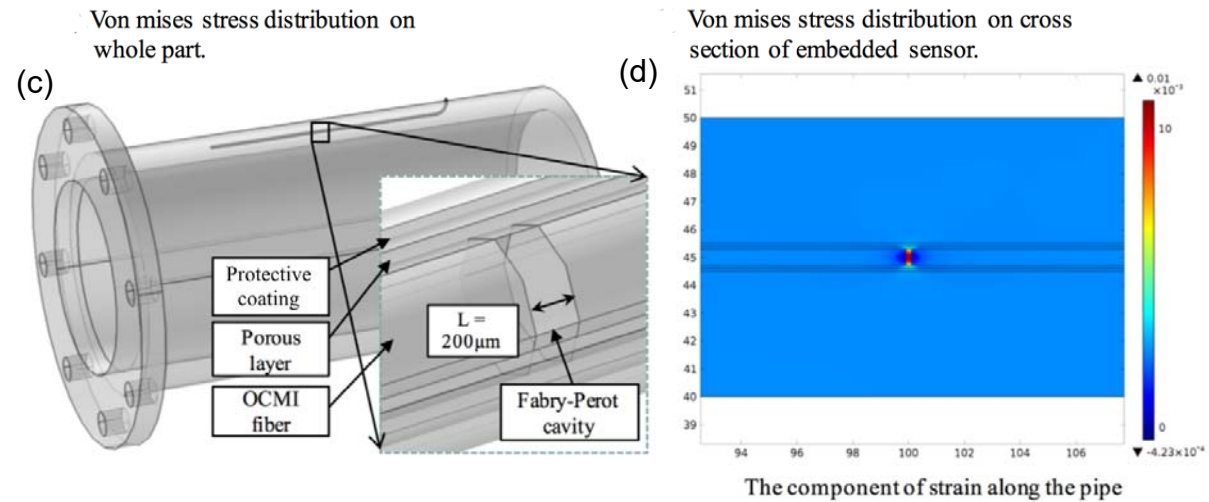


# Thermal Stress-Strain Modeling of Embedded Sensors

Pressure Caused Stress-Strain Distribution



Temperature Caused Stress-Strain Distribution



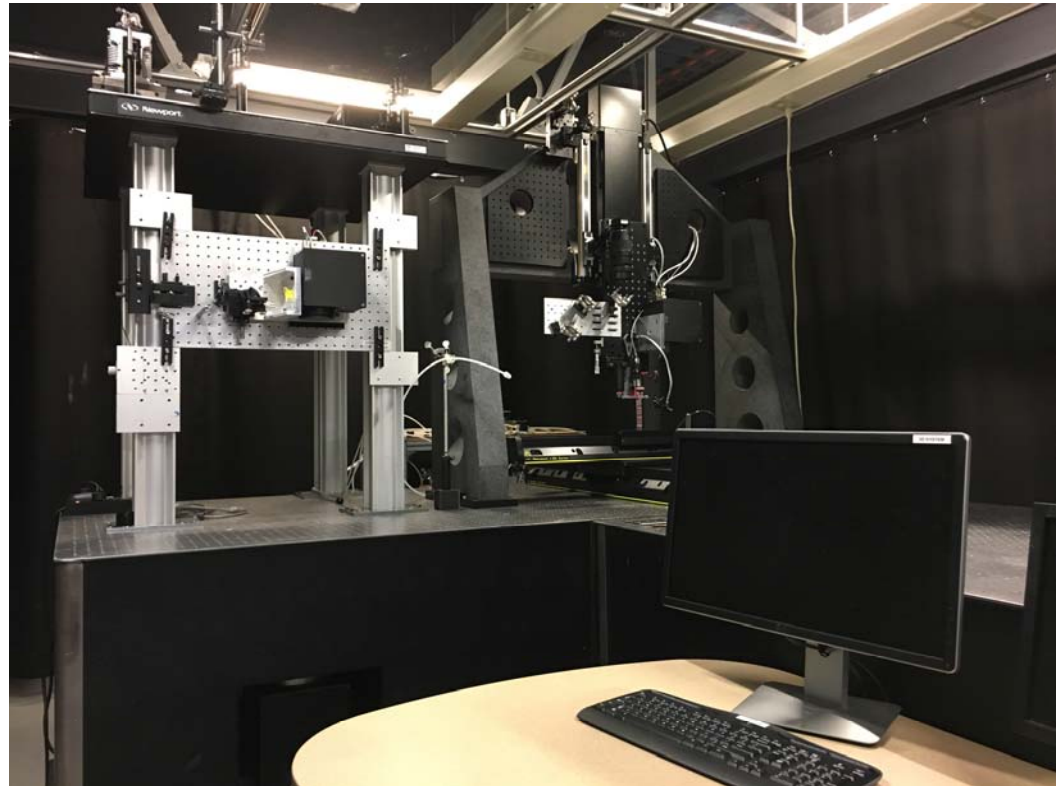
# **Additive Manufacturing and Test of Sensor Embedded Parts**

**Approach: Fully distributed microwave photonic fused silica  
and sapphire fiber sensors**

**Hai Xiao  
Clemson University**

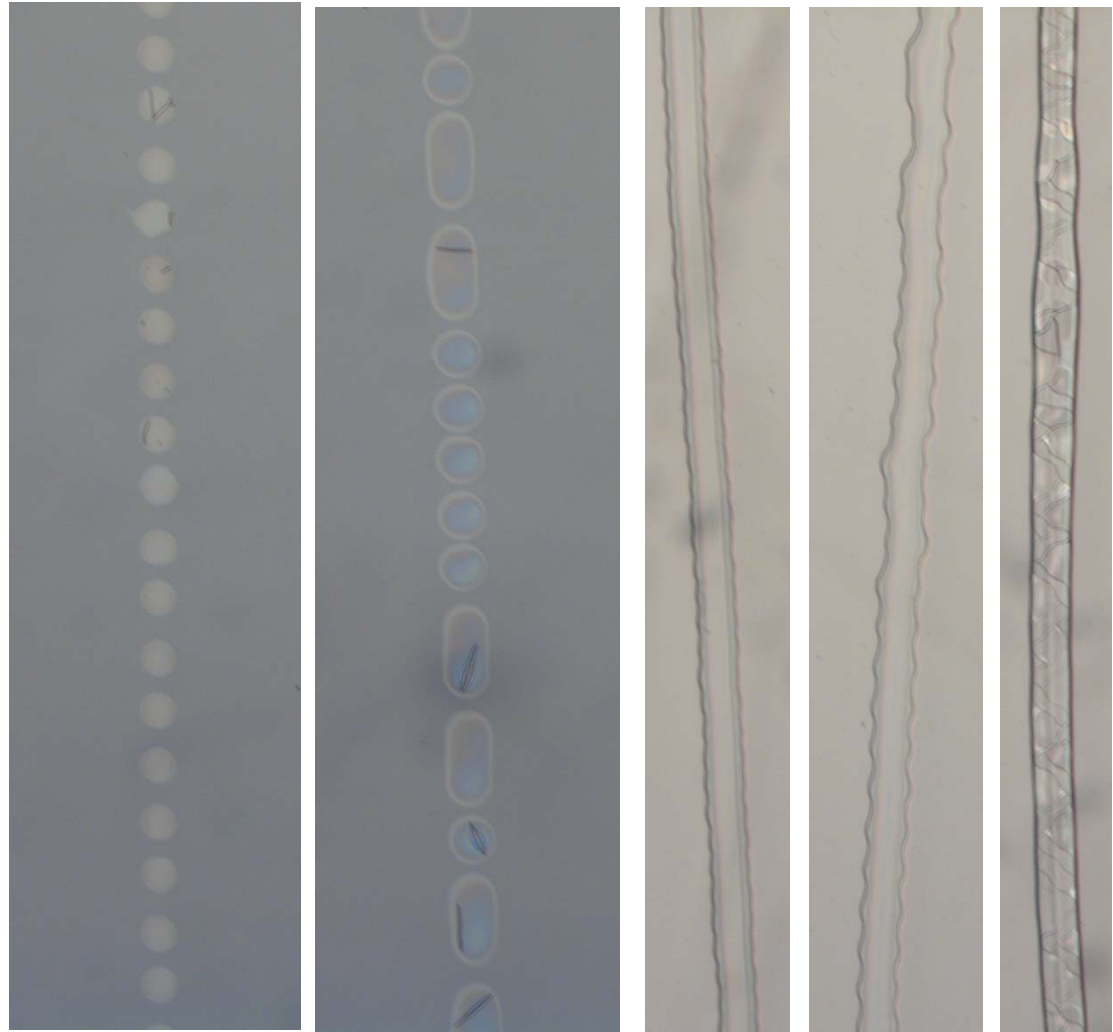


- **An advanced manufacturing system integrates both additive and subtractive manufacturing**
  - **Multiple dispensers based 3D printing**
  - **Multiple extruders based paste 3D patterning**
  - **CO<sub>2</sub> laser based 3D heating and sintering**
  - **ps and fs lasers based 3D fine cutting**
  - **Computer controlled motion stages and CAD fusion capability**
  - **Ceramic, metal and plastic and composites**

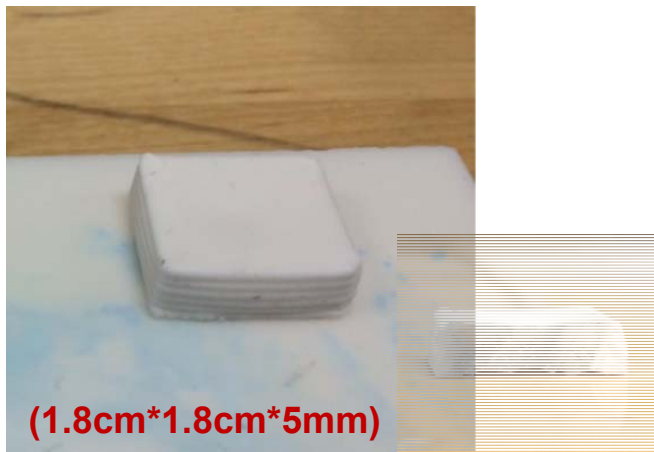
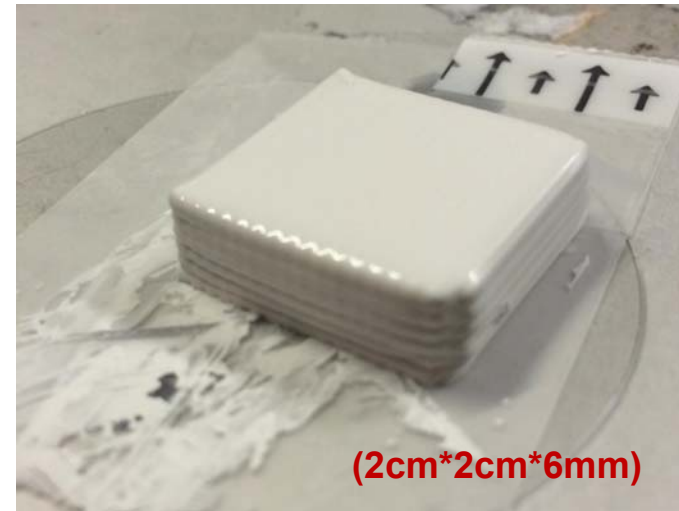
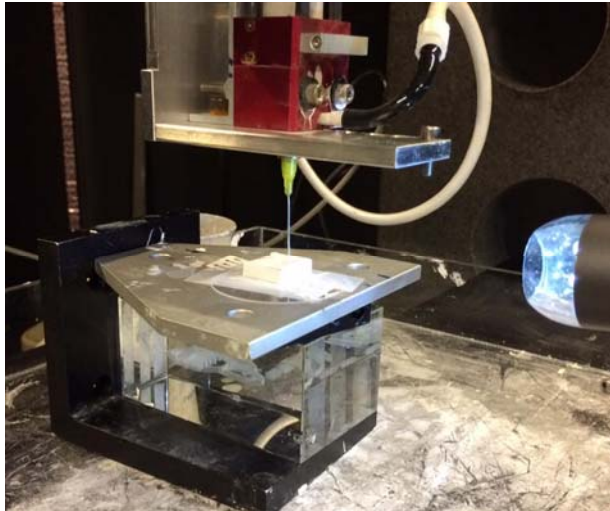




- Direct printing by dispensed sol-gel and laser in situ sintering

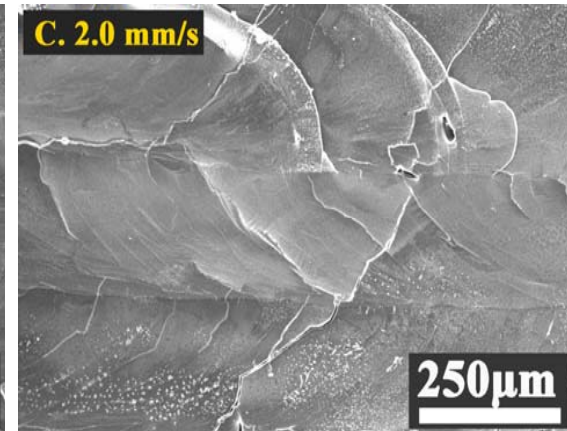
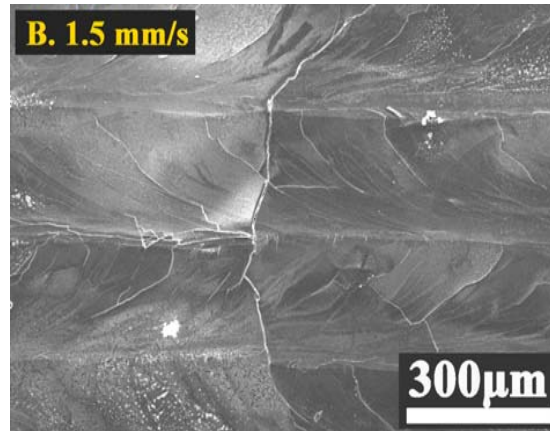
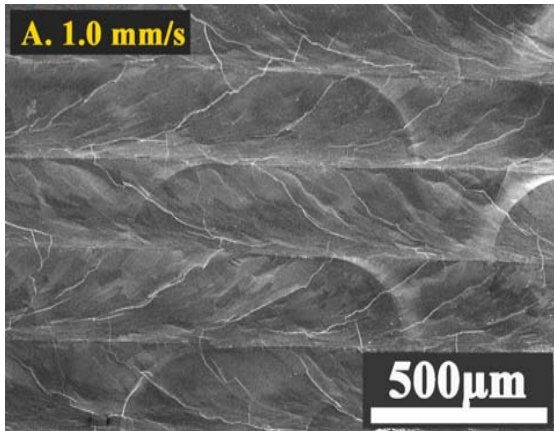


## Printing ceramic block

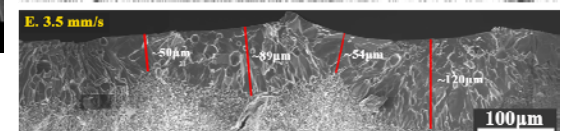
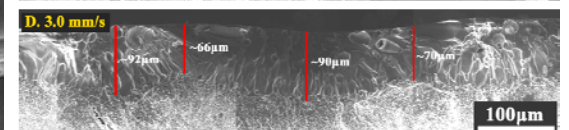
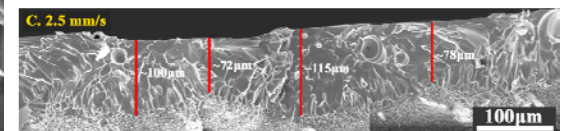
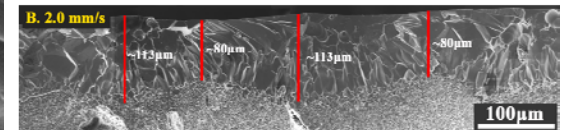
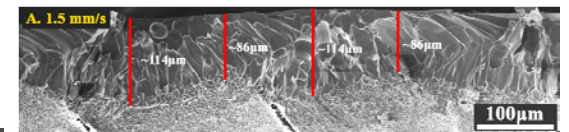
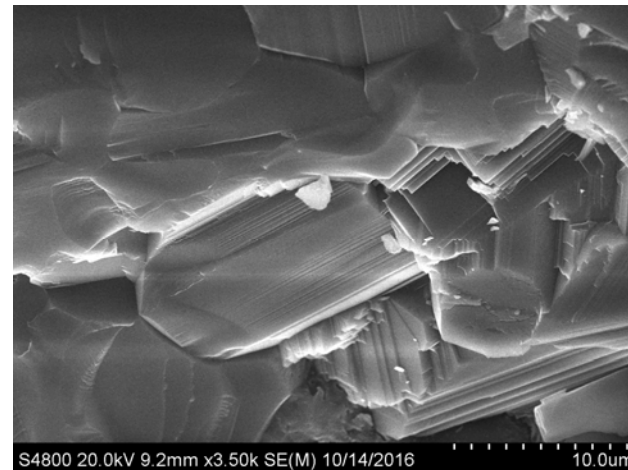
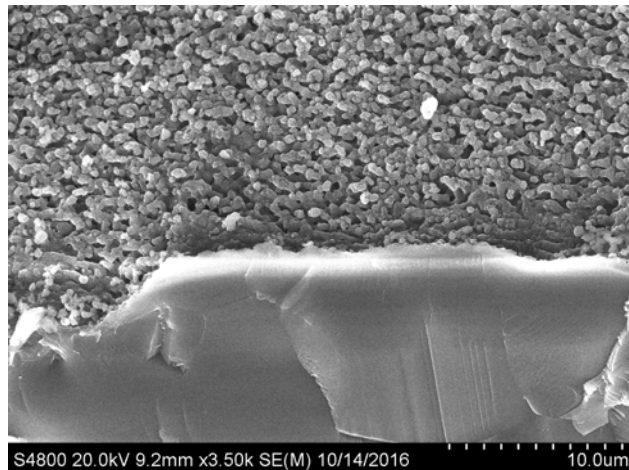


Shrinkage	Parts only
Shrinkage in length	>10%
Shrinkage in width	>10%
Shrinkage in height	>20%
Volumetric shrinkage	>32.5%
Relative density (Archimedes principle)	88%

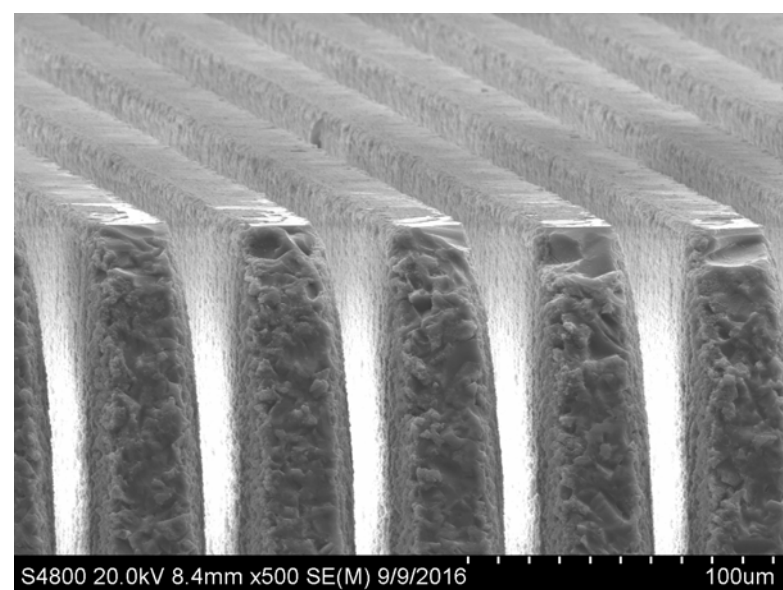
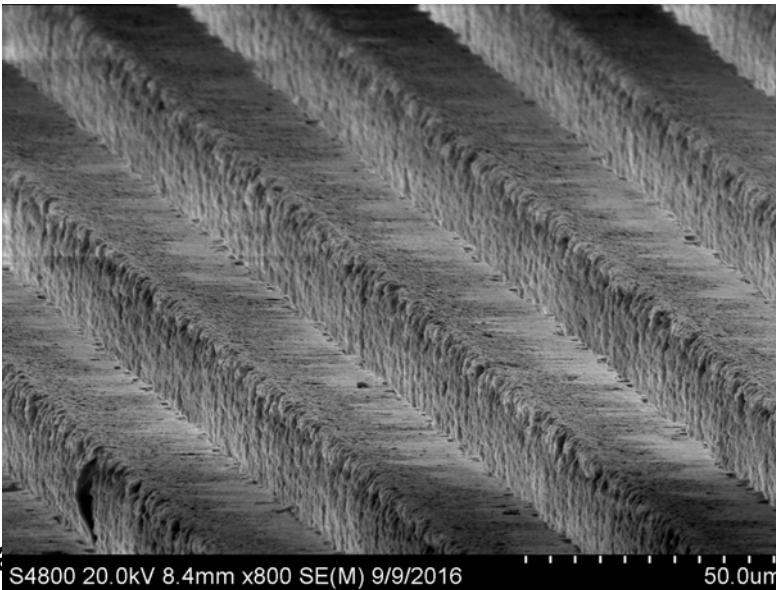
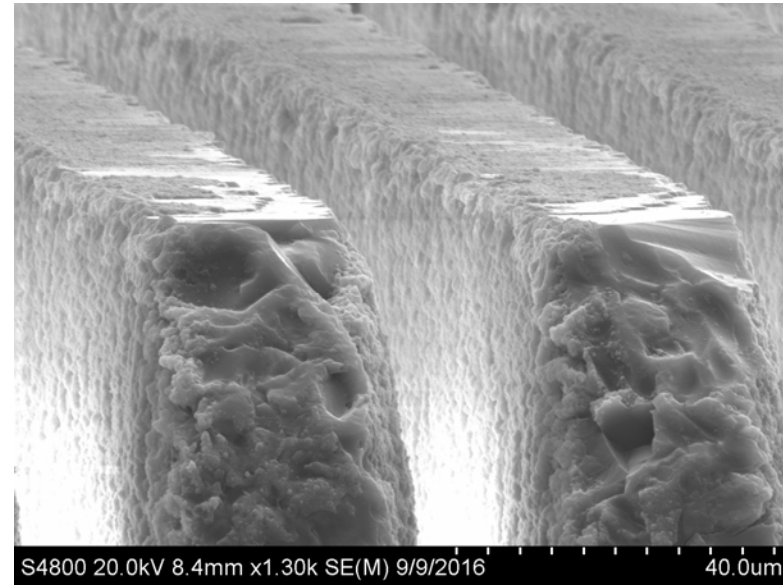
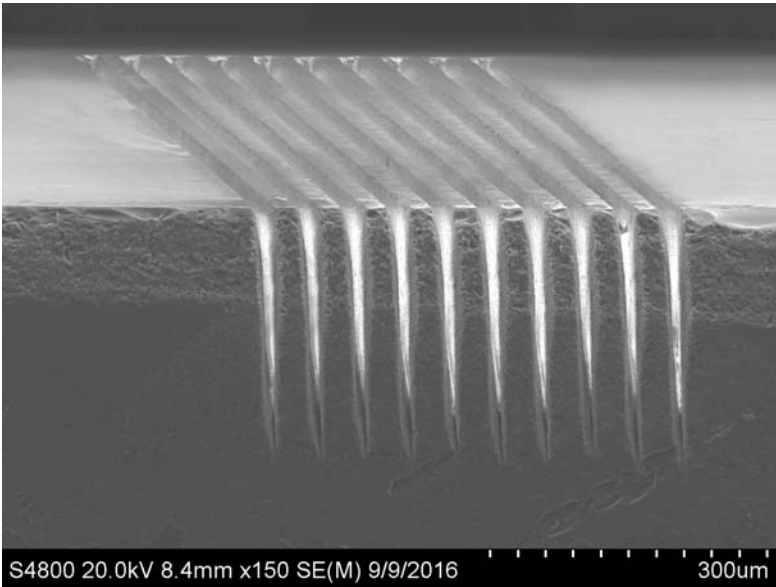
- **Surface**

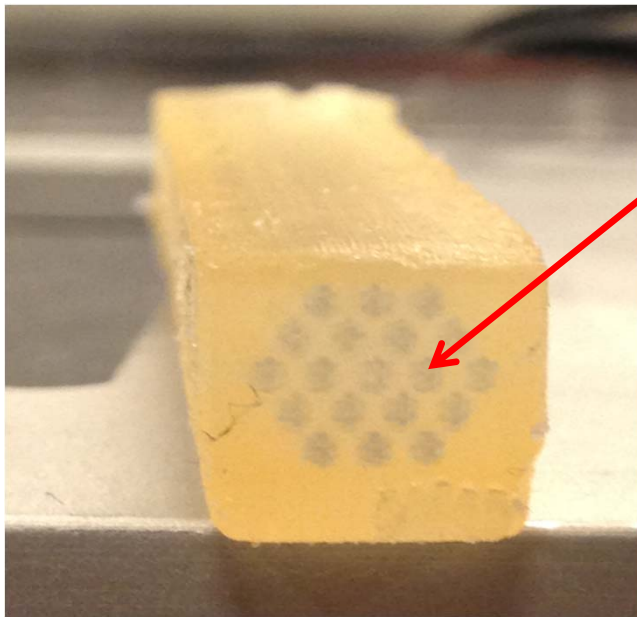
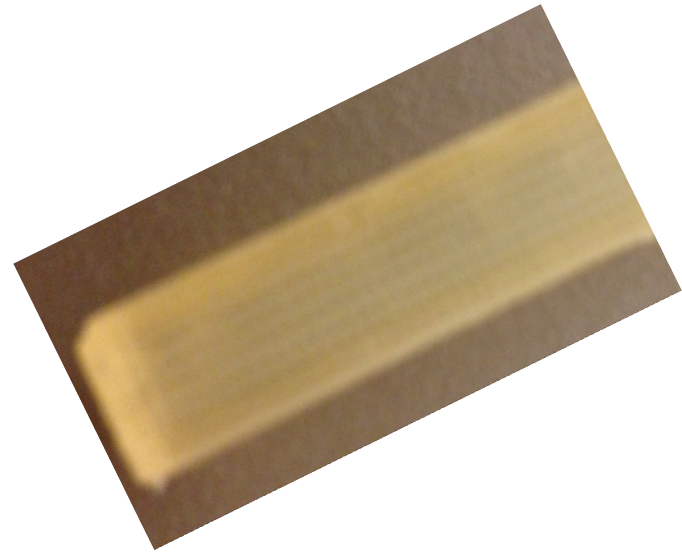
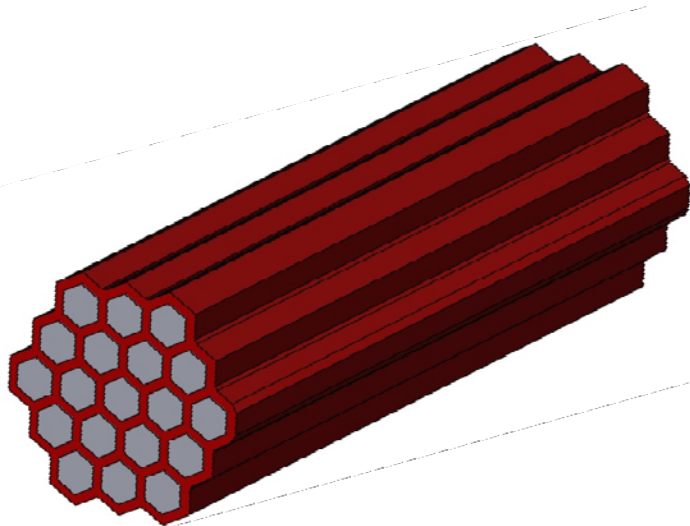


- **Cross sections**

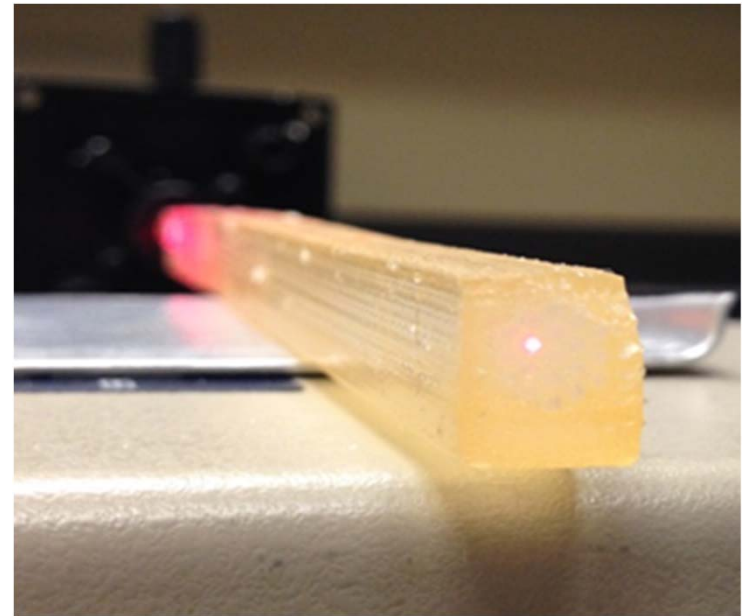
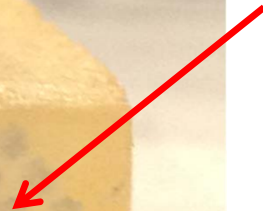






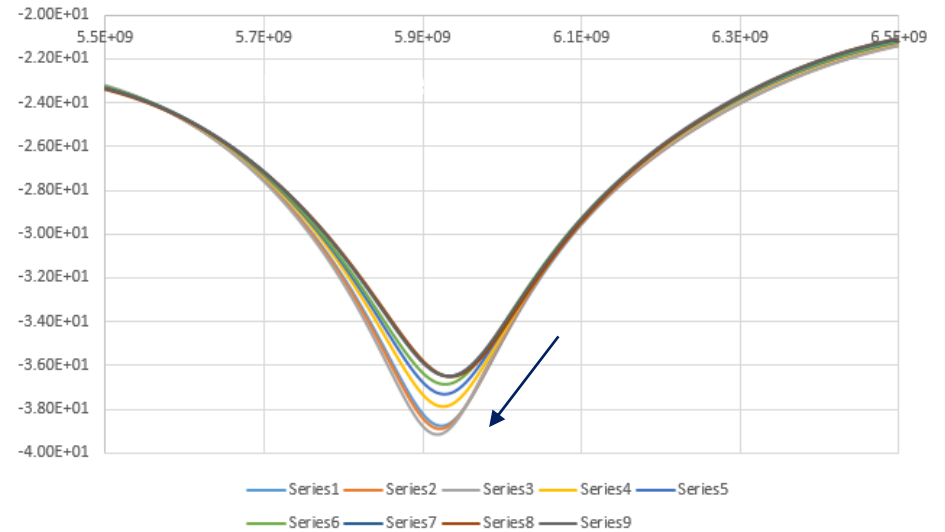
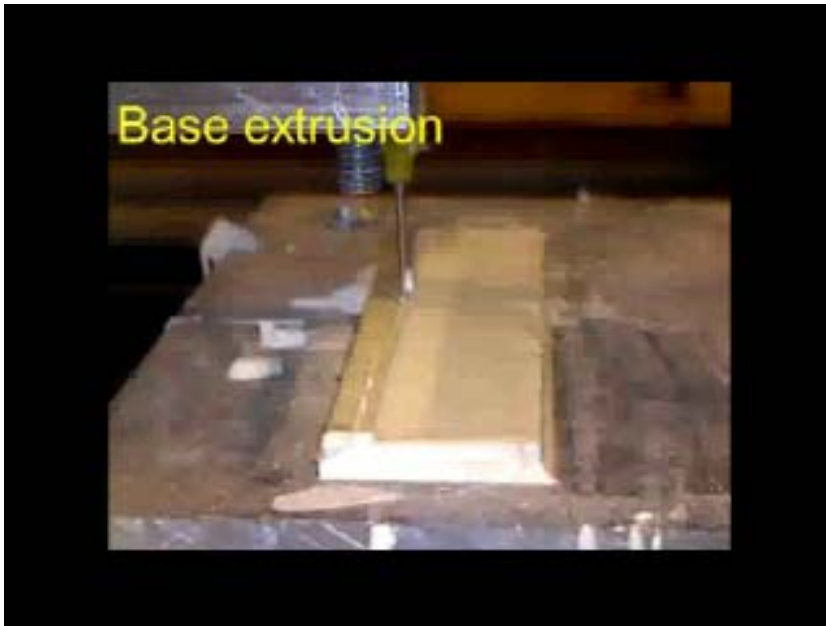
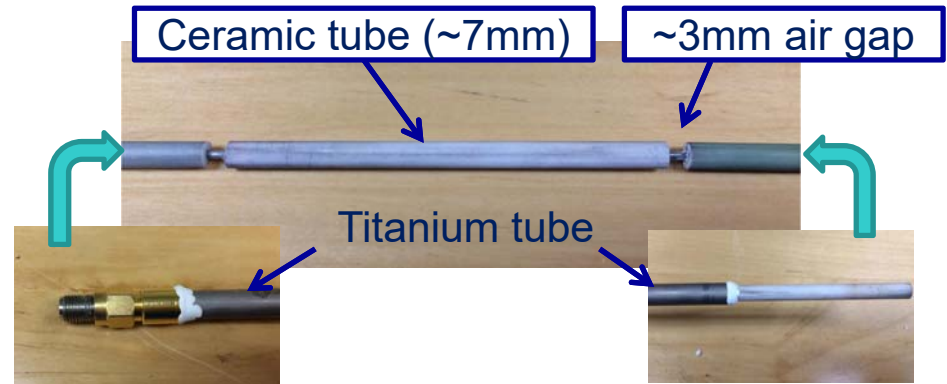
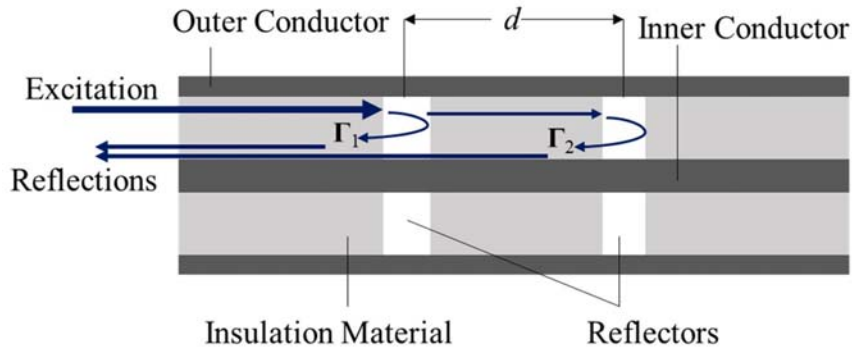


800  $\mu\text{m}$   
hexagons

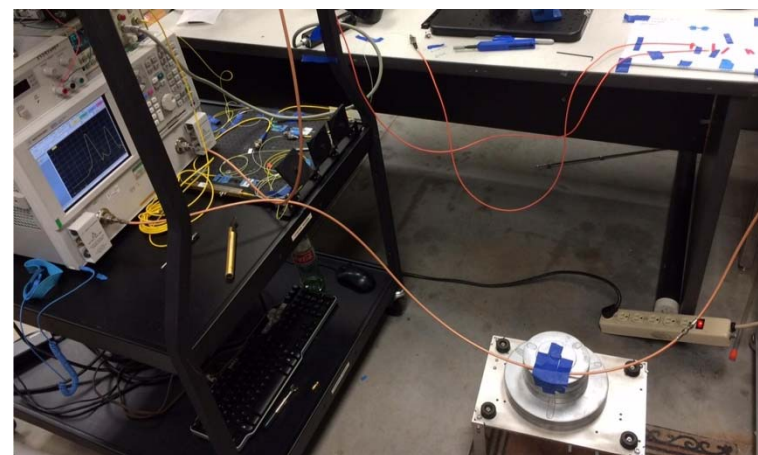
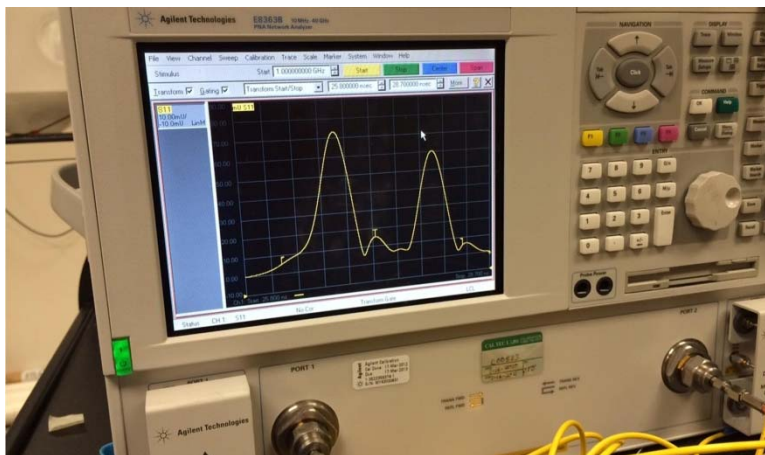
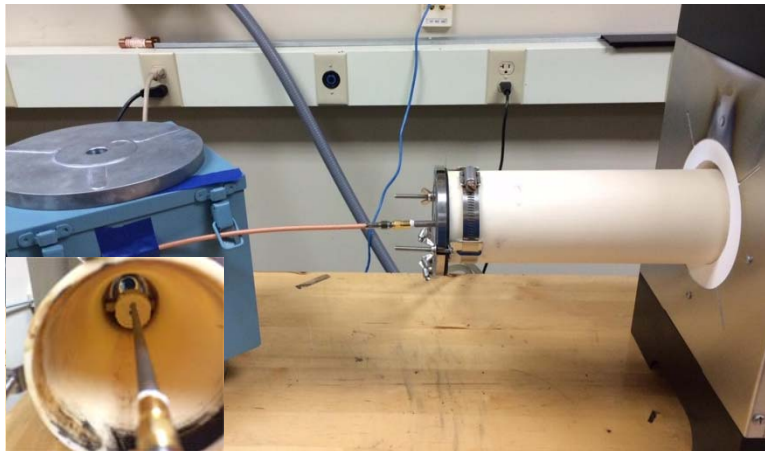




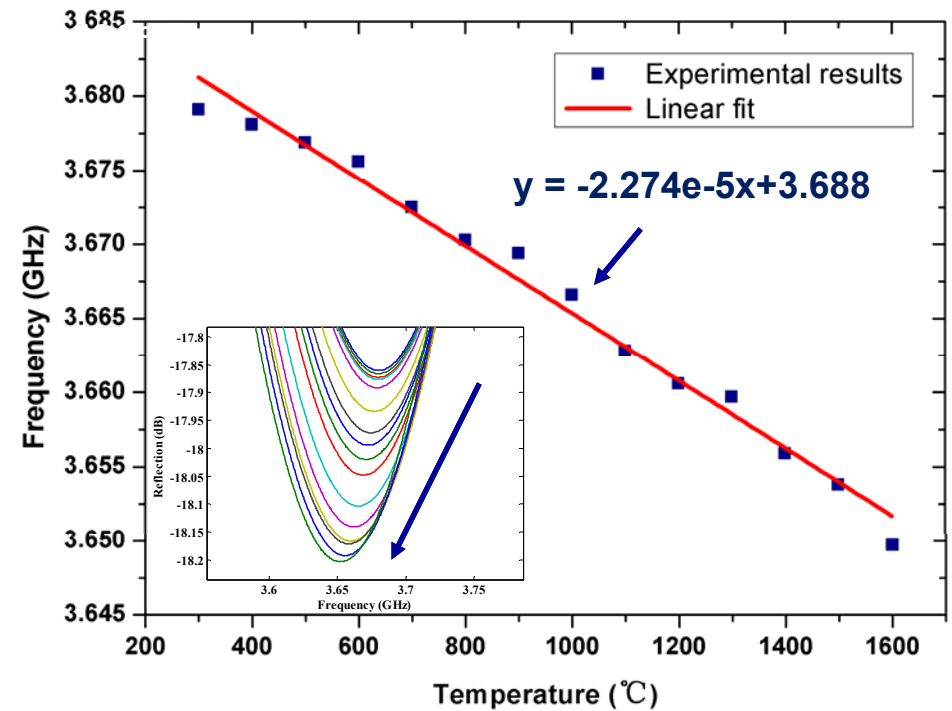
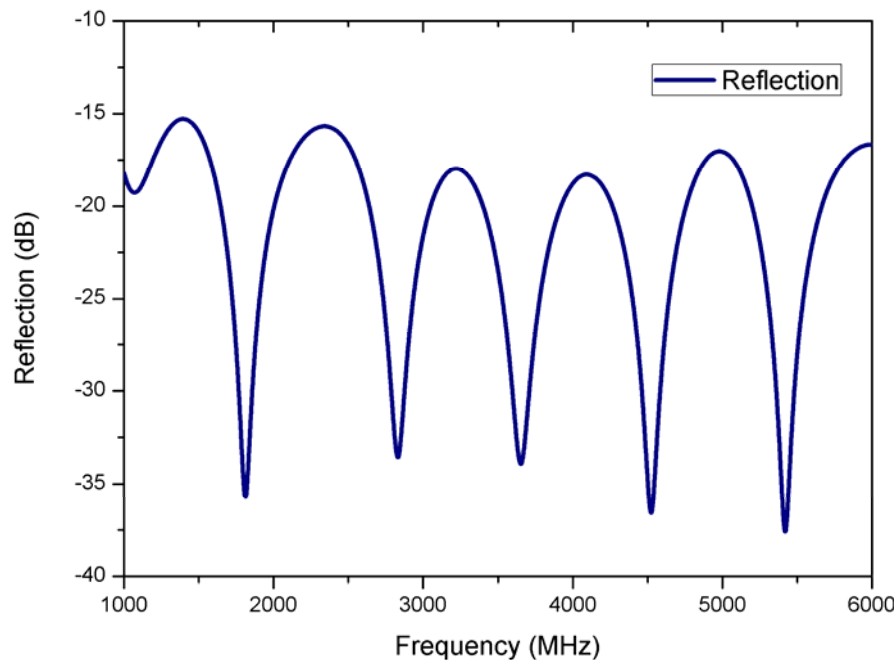
## ● Embedded cable for strain test



## High temperature test of the smart part embedded with a metal-ceramic coaxial Cable (MCCC) Sensor



- Embedded Metal-Ceramic Coaxial Cable (MCCC) Fabry-Pérot Interferometric Sensor**

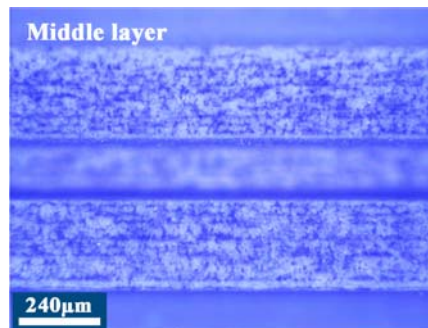
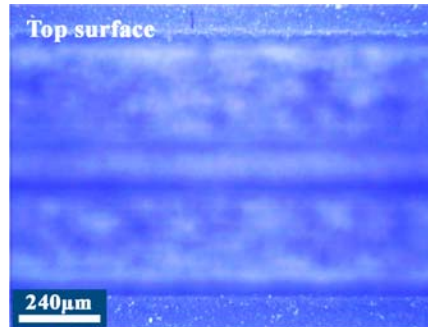
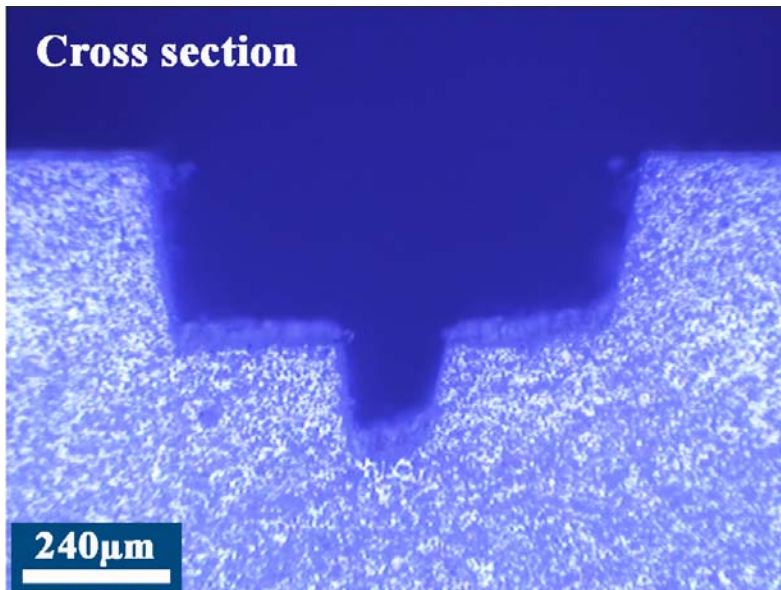
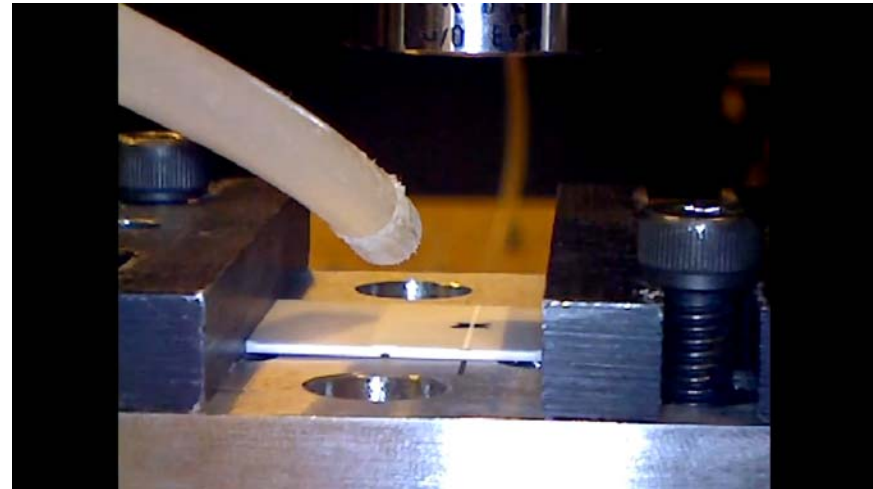
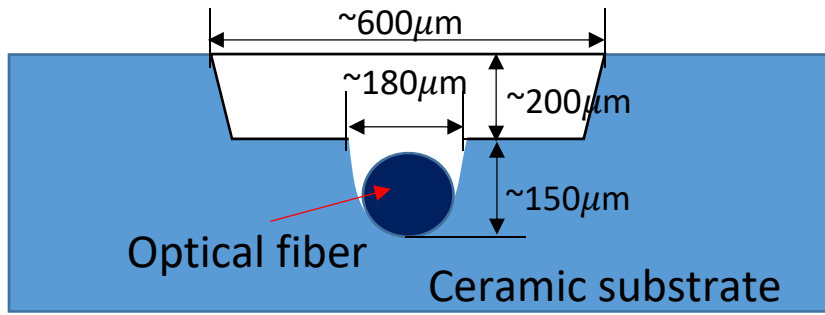


- Such cable can be operated at 1600°C

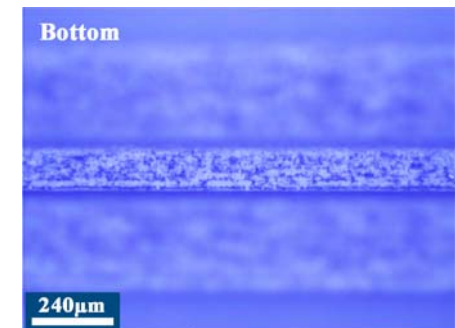
Sensitivity =  $-2.274e-5$  GHz/°C



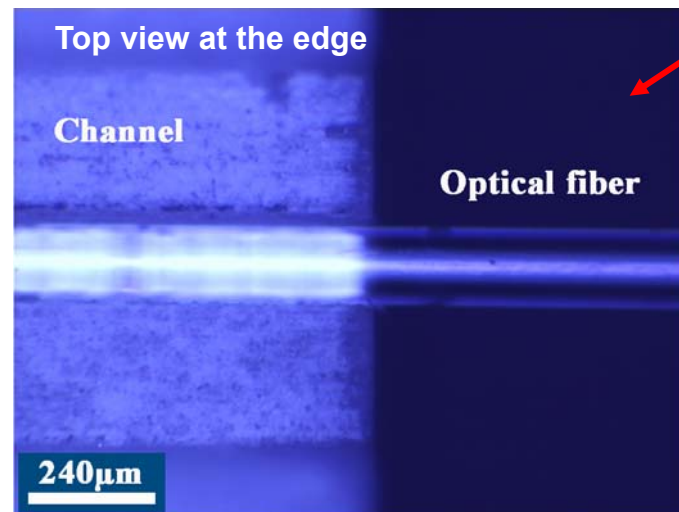
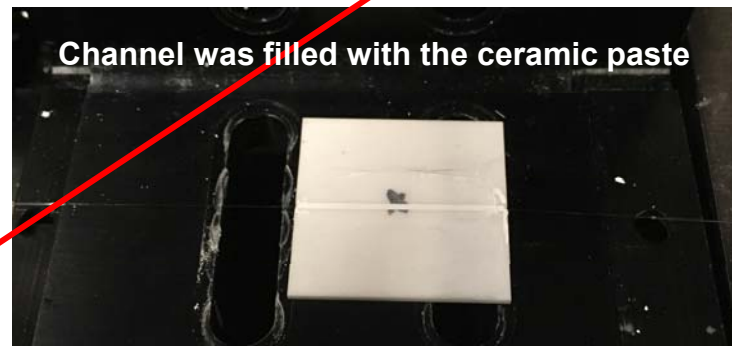
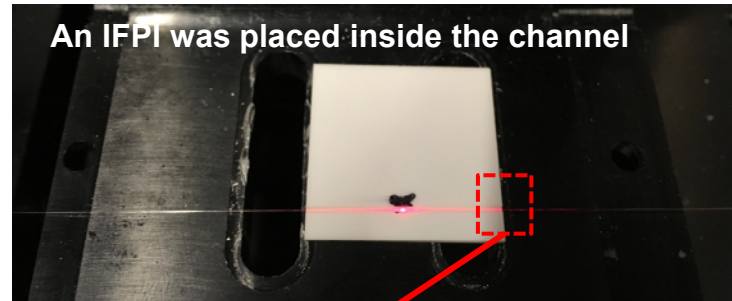
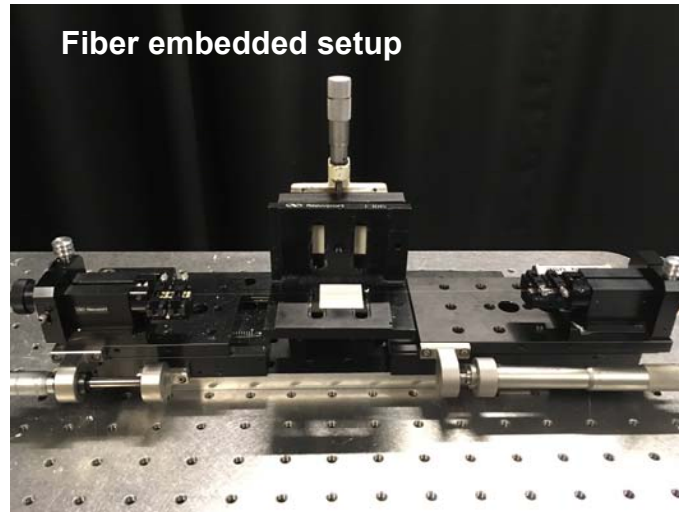
## 1. Fabricate the channel on the ceramic substrate with designed shape for fiber embedding



- ❖ Easy to fabricate by ps-laser with high resolution
- ❖ Confining the fiber into the small channel can provide more protection to the optical fiber
- ❖ Control the thickness of the ceramic filler by controlling the depth of the channel



## 2. Place the optical fiber sensor into the channel and filled the channel with the ceramic paste

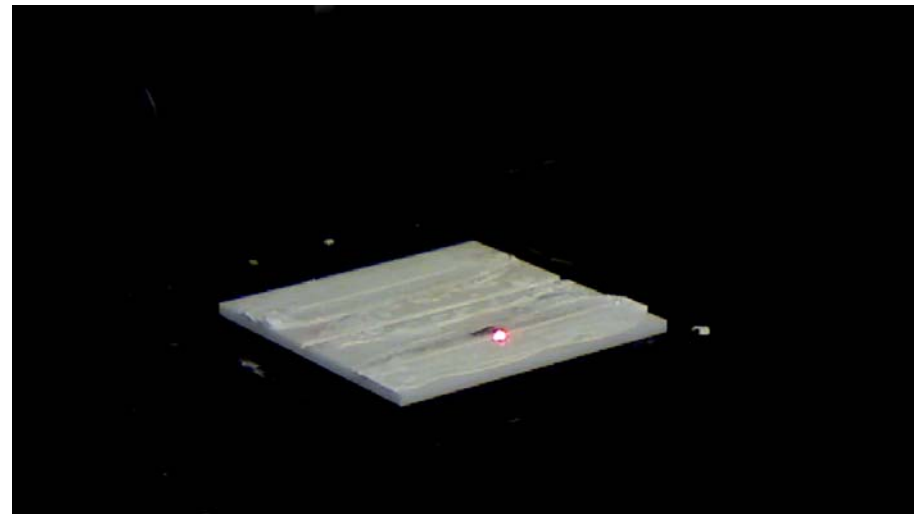


- ❖ Slightly applied tensile stress on two ends of the optical fiber to make sure it was straight and touch the bottom of the channel

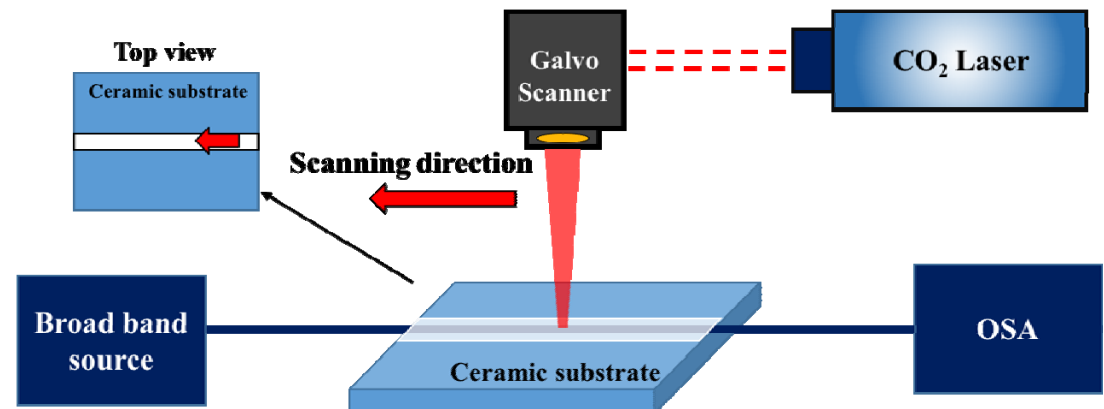


### 3. Use a CO<sub>2</sub> laser to process the filling materials and seal the fiber inside

- ❖ Laser operating parameters:
  - Laser output power: 9 W
  - Scanning speed: 0.2 mm/s
  - Spot size: 1.1 mm
- ❖ high speed scanning at low power to pre-heat the materials before high power processing
- ❖ The optical fiber was monitoring by the OSA during the whole embedding process

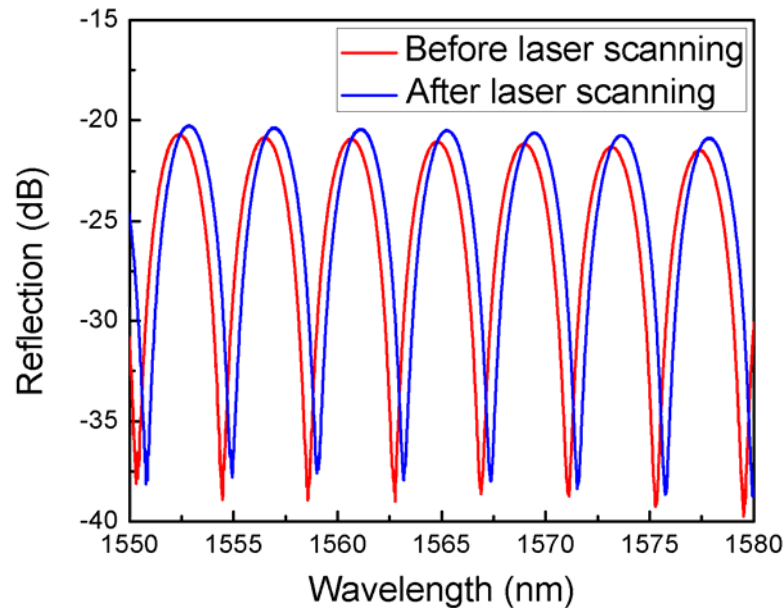


Max Output Power	20W
Operation	Continuous wave (CW)
Mode Quality	TEM <sub>00</sub> , M <sup>2</sup> < 1.1 ± 0.1
Beam Diameter before focusing	2.5mm ± 0.5mm
Beam Diameter after scanner	~1.0 mm
Wavelength	10.6 μm
Polarization	Linear (Horizontal)

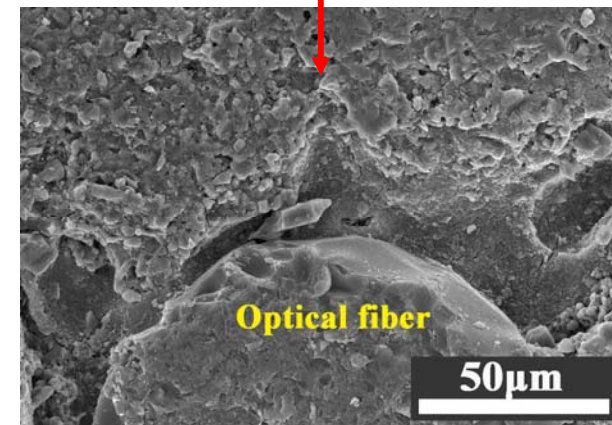
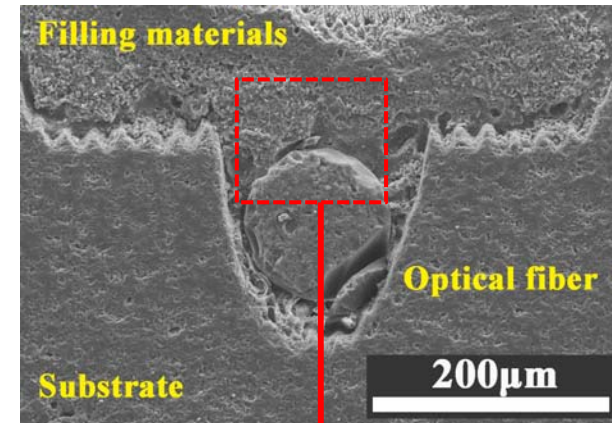


## 3. Use CO<sub>2</sub> laser to process the filling materials to seal the fiber inside

(2) Embed an IFPI optical fiber sensor into the ceramic substrate and seal it by the CO<sub>2</sub> laser



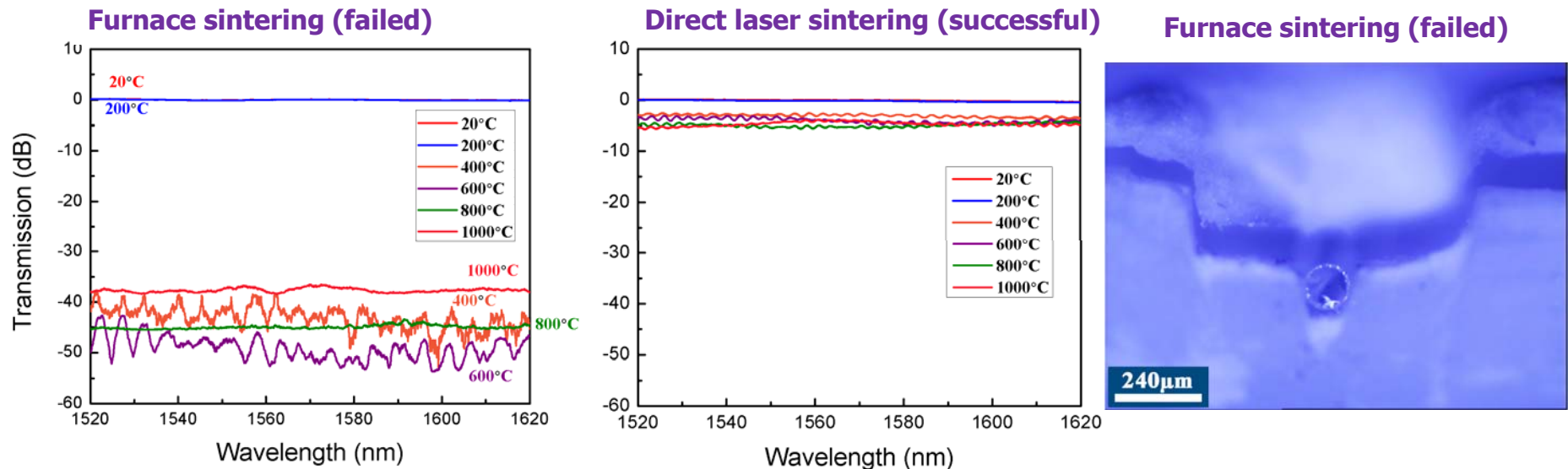
- ❖ For the IFPI sensor, after laser processing, the spectrum slightly shifted to longer wavelength for about 1 nm
- ❖ Known from the cross-sectional image, the channel was filled well but it seems that there were still pores at the part that was close to the optical fiber



the cross section after laser scanning on the surface

## 4. Test the high temperature stability of the embedded optical fiber sensor

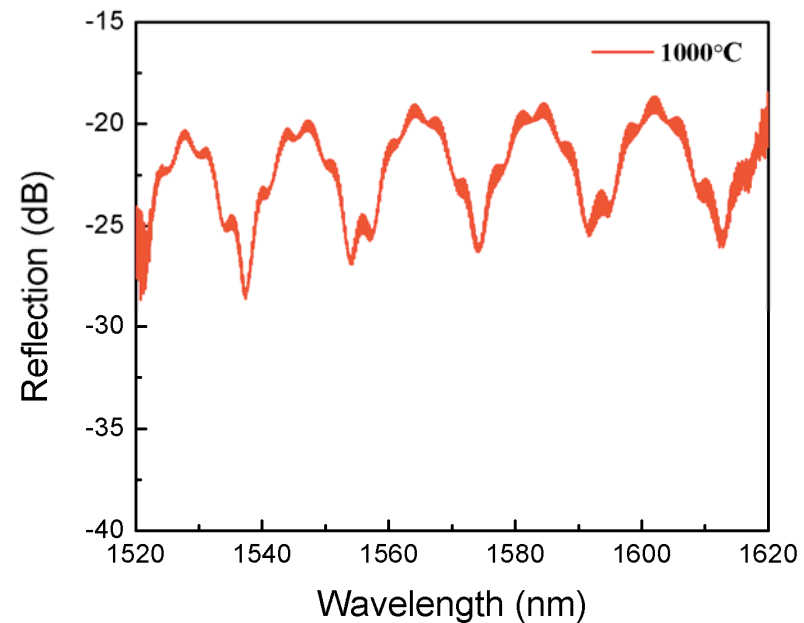
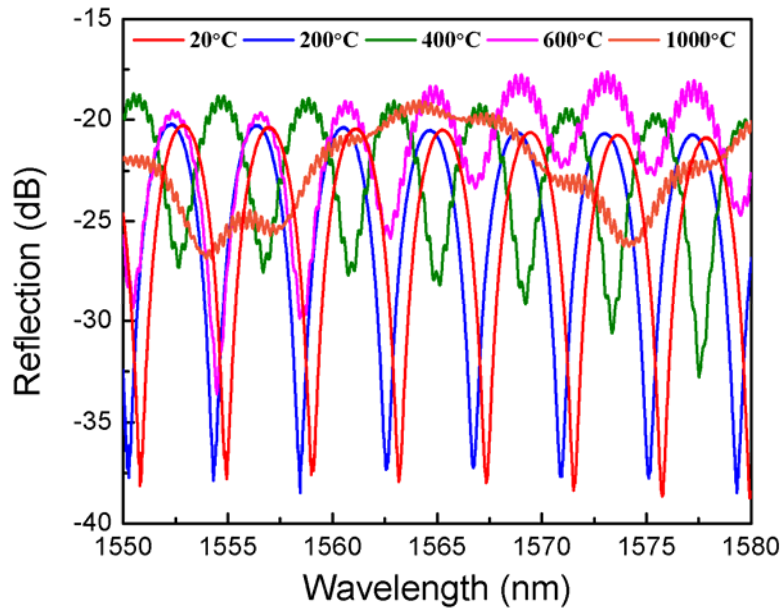
### (1) Improved high temperature stability of the embedded optical fiber by laser sintering



- ❖ Traditional furnace based sintering, the embedded optical fiber had a huge loss (~45 dB) when the temperature reached 400°C
- ❖ Direct laser sintering, though small ripples occurred after 400°C, the transmission spectrum generally maintain straight and only 5 dB loss when the temperature reached 1000°C

## 4. Test the high temperature stability of the embedded optical fiber sensor

### (2) High temperature stability of the embedded intrinsic Fabry-Perot interferometer (IFPI)



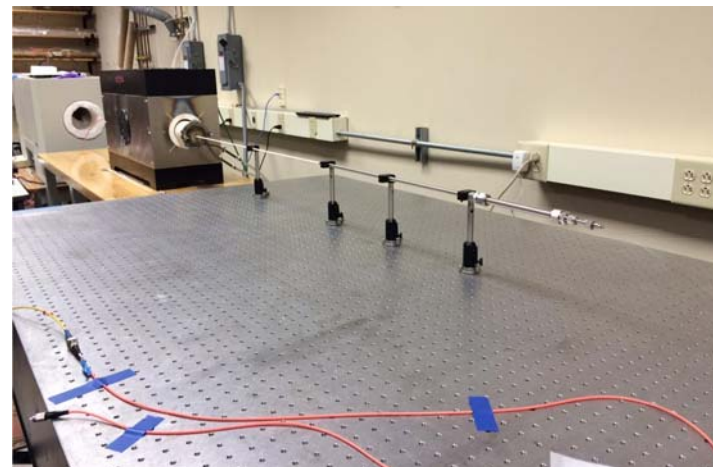
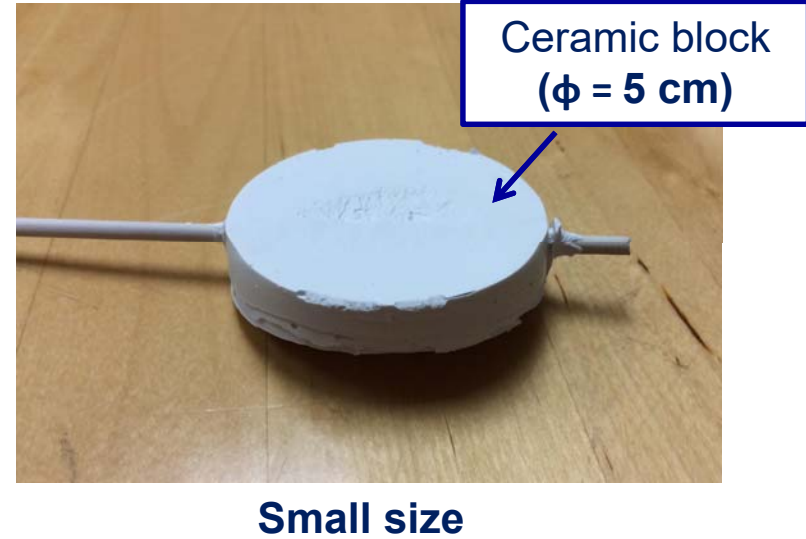
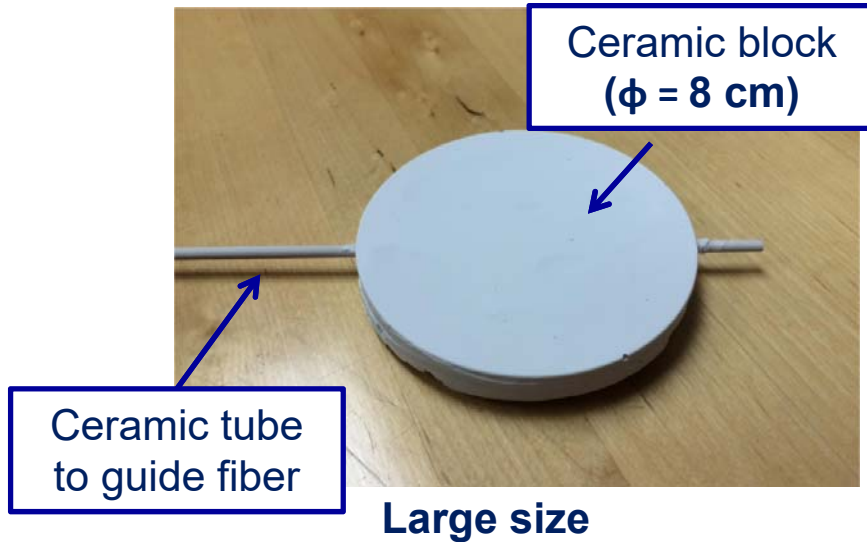
- ❖ Survived 1000°C and still produced good signals
- ❖ Slightly compression of the optical fiber that reduced the cavity length of the IFPI
- ❖ Need further improvement and optimization

- **Manufacturing of sensor embedded smart parts (a smart ceramic washer)**



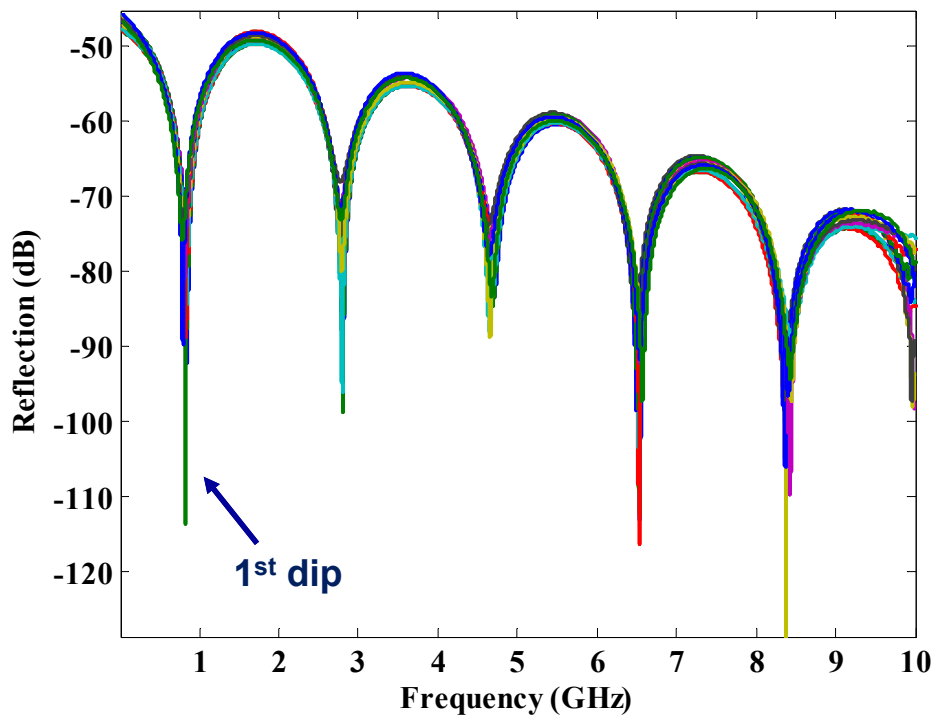


- **Embedment and experimental setup**

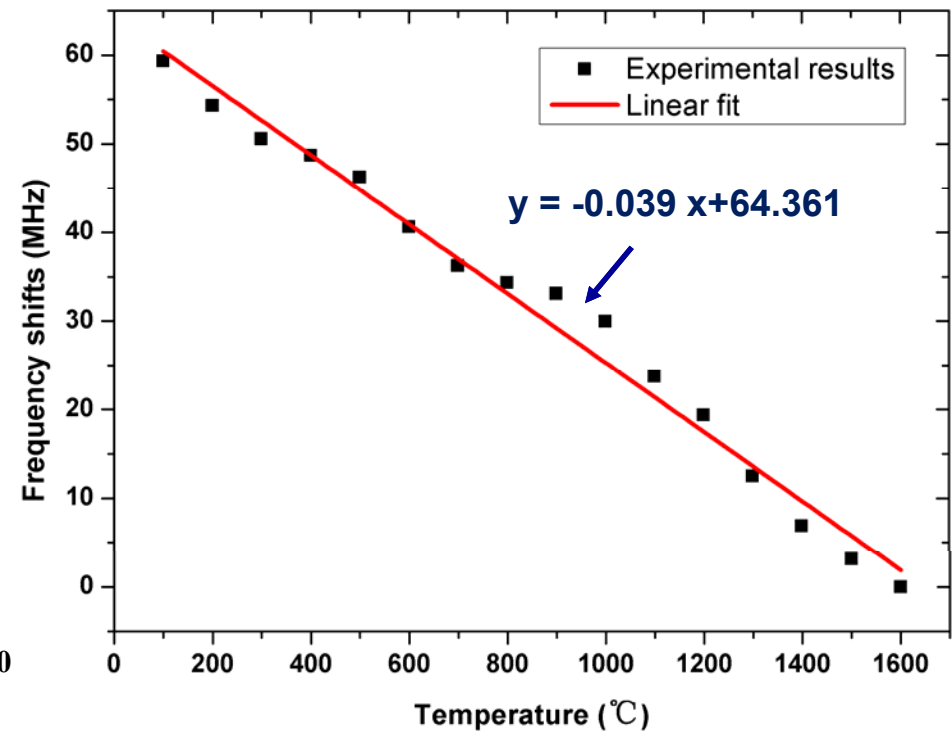


- Embedded Sapphire Fiber Michelson interferometer

## High temperature results (100-1600°C)



Frequency domain



Frequency response VS temperature

# Summary of Progresses

- Distributed microwave and photonic sensors and instrumentation have been developed and proven**
- Protective coating materials have been identified and successfully coated on silica and sapphire optical fibers**
- Additive Manufacturing techniques have been developed for fabrication of metal and ceramic parts**
- Smart parts with embedded sensors have been fabricated using advanced manufacturing and preliminarily tested**

# Future Work

- **Manufacture more smart parts**
- **Comprehensive tests of the smart parts**

# Acknowledgement

- **NETL Managers and Engineers (current and former)**
  - Robert Romanosky
  - Susan Maley
  - Robie Lewis
  - Steve Seachman
  - Barbara Carney
  - Sydni Credle
  - Paul Ohodnicki
  - Benjamin Chorpening
  - Richard Dunst
  - Jessica Mullen
  - Otis Mills