

Understanding Transient Combustion Phenomena in Low-NO_x Gas Turbines

Project DE-FE0025495, Oct. 2015 – Sept. 2018

Program Monitor: Mark Freeman

PI: Jacqueline O'Connor, Ph.D.

Co-PI: Dom Santavicca, Ph.D.

RE: Bryan Quay, Ph.D.

Graduate students: Janith Samarasinghe, Ph.D.,
Wyatt Culler, Xiaoling Chen

Undergraduates: Jackson Lee

Industry Partner: GE Global Research
Keith McManus, Tony Dean, Fei Han

Mechanical and Nuclear Engineering
Pennsylvania State University
sites.psu.edu/ccpp/



Overview of presentation

- Project motivation and approach
- Year 1 Results:
 - Steady-state fuel staging – mechanisms for instability suppression
 - Transient fuel staging – natural system timescales
- Conclusions and next steps

Overview of presentation

- Project motivation and approach

- Year 1 Results:

 - Steady-state fuel staging – mechanisms for instability suppression

 - Transient fuel staging – natural system timescales

- Conclusions and next steps

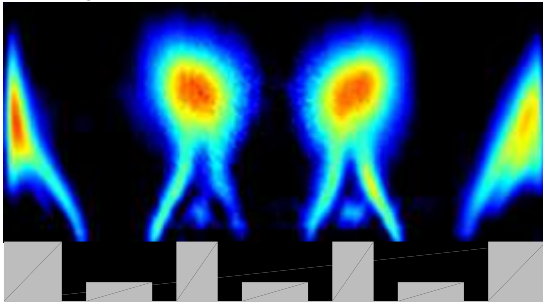
Objective of the program is to *understand, quantify, and predict* combustion instability during transient operation

- Two major deliverables for the program:
 1. Fundamental understanding of flow and flame behavior during combustion transients and mechanisms for transition to instability
 2. Development of a stability prediction or quantification framework

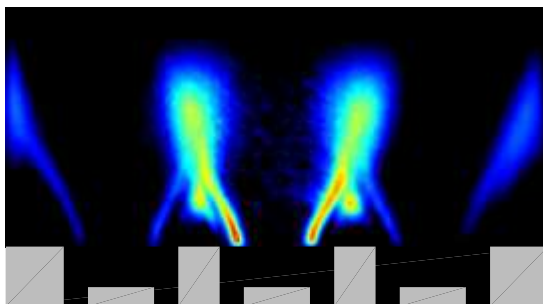
Three types of transients will be considered in the program that mimic the types of transients used in operational turbines

Fuel Splitting

$\phi = 0.65$ in all nozzles



$\phi = 0.67$ in outer nozzles,
 $\phi = 0.82$ in middle nozzle



Equivalence Ratio

$\phi = 0.48$

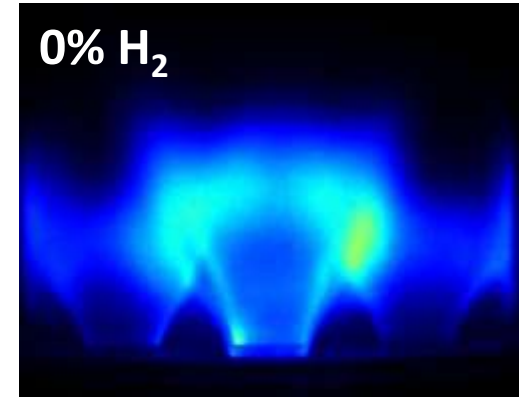


$\phi = 0.60$

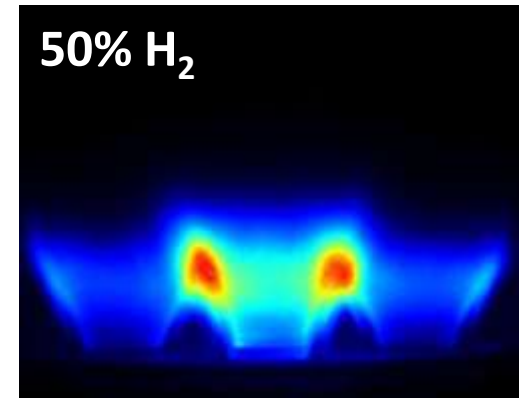


Fuel Composition

0% H₂



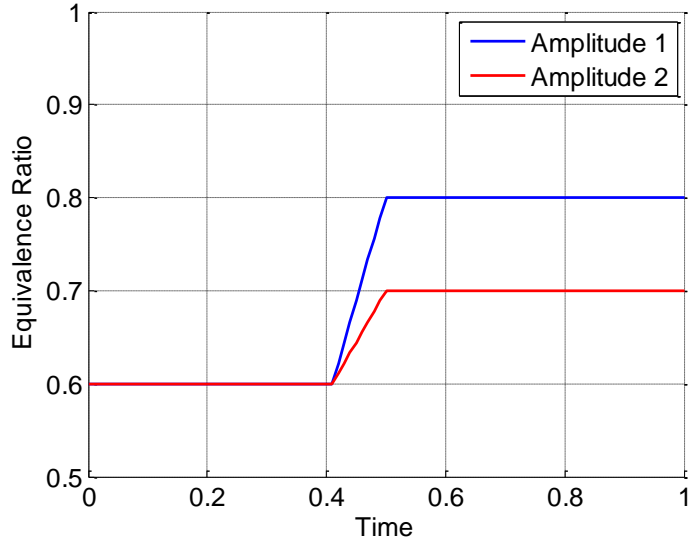
50% H₂



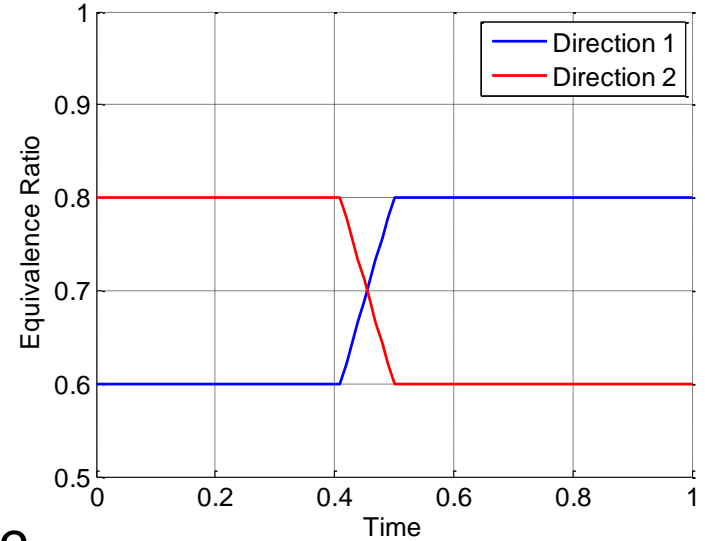
Images obtained from work done by Alex De Rosa (2011)

The transients will be quantified using three different metrics: *amplitude*, *timescale*, and *direction*

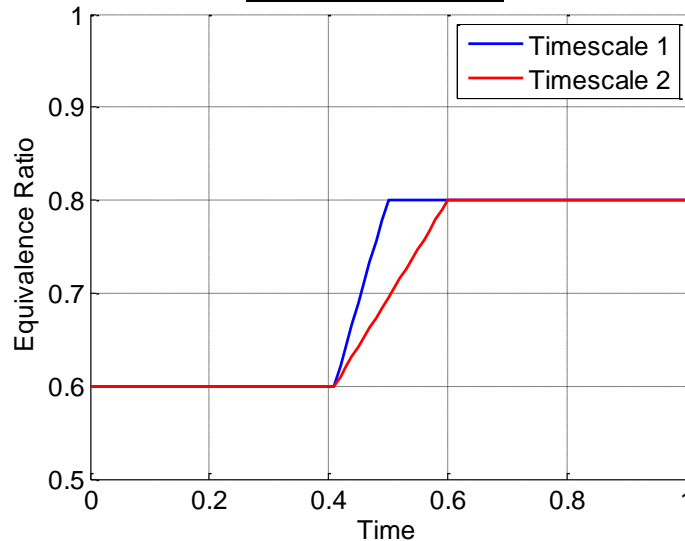
Amplitude



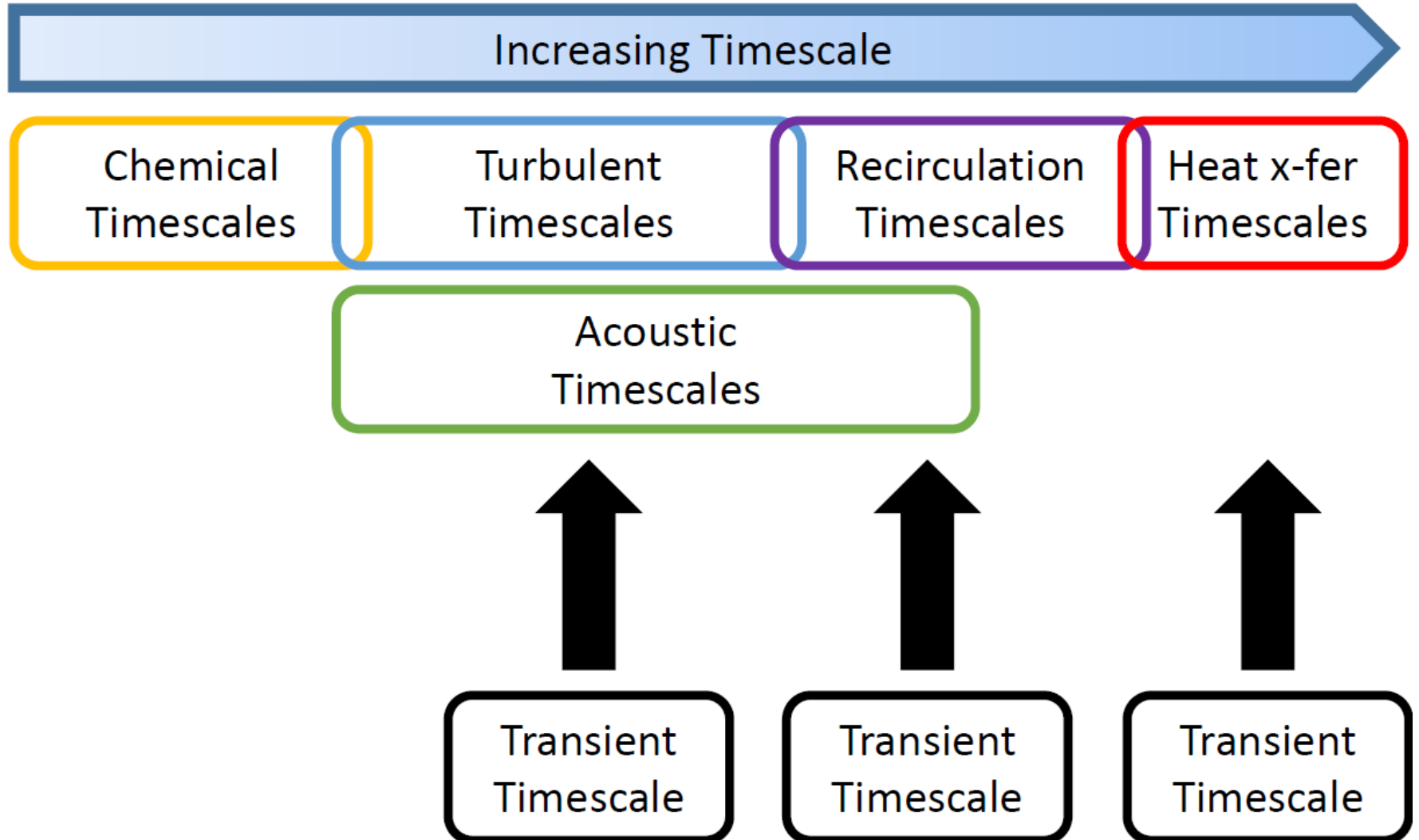
Direction



Timescale



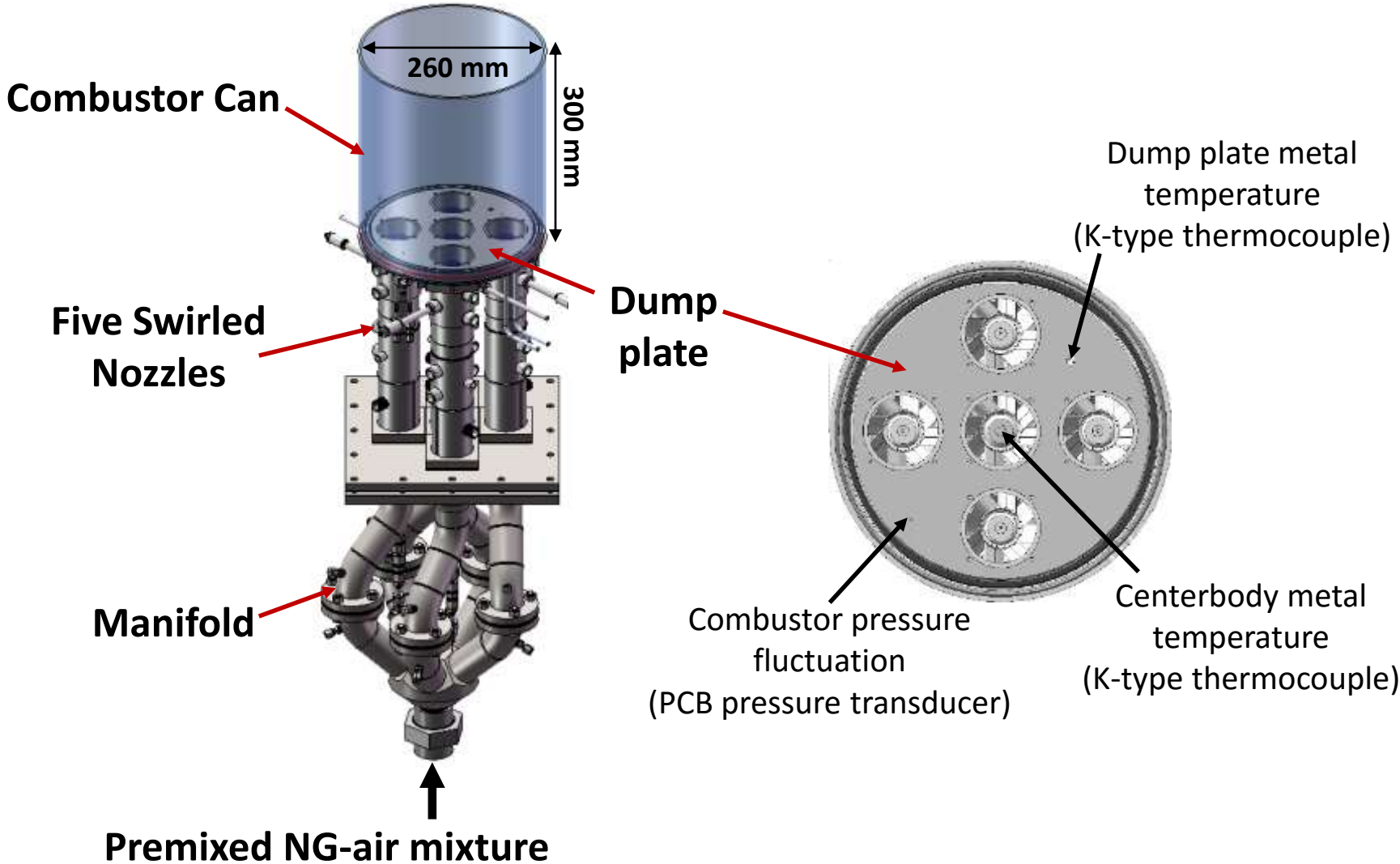
Varying the transient timescales allows for different processes to equilibrate during the transient, changing the path



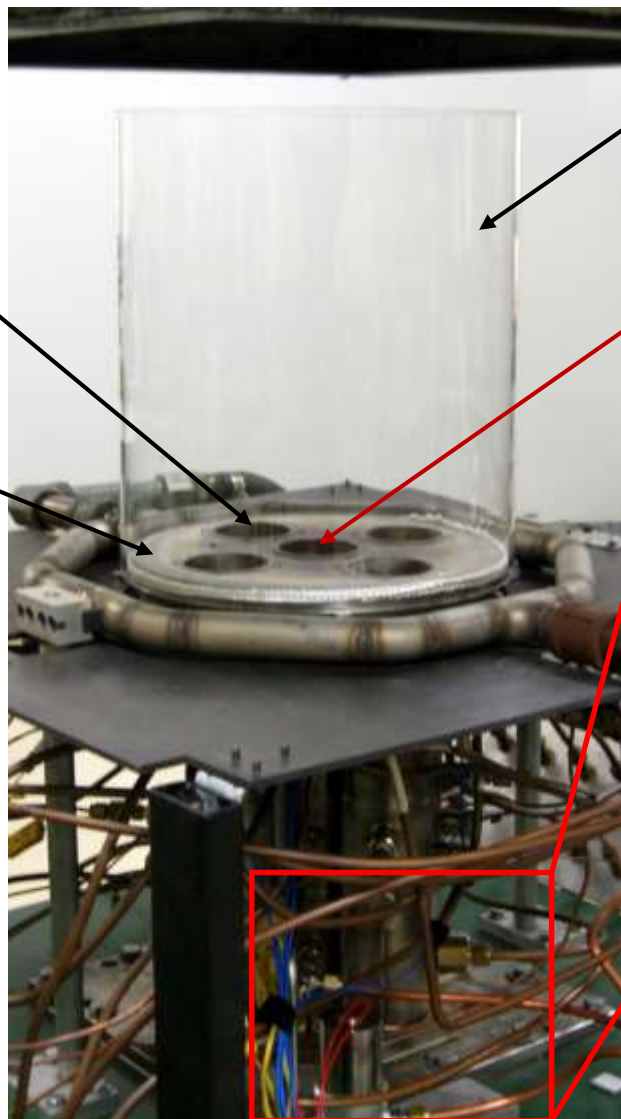
Project Management Plan – progress to date

- **Task 1** – Project management and planning
- **Task 2** – Modification of current experimental facility with monitoring diagnostics and new hardware for transient control
- **Task 3** – Map combustor timescales at target operating points
- **Task 4** – Design of transient experiments
- **Task 5** – Fuel split transients (multi-nozzle combustor)
- **Task 6** – Equivalence ratio transients (single- and multi-nozzle)
- **Task 7** – Fuel composition transients (single- and multi-nozzle)
- **Task 8** – Data analysis and determination of prediction/quantification framework

Experimental facilities include both a single-nozzle and multi-nozzle combustor, fuel splitting on multi-nozzle only



TASK 2: Hardware modification focused on a valve with linear actuation to control fuel flow transients for fuel-splitting studies



Five nozzles

Dump plate

Quartz combustor

Staging fuel enters combustor here

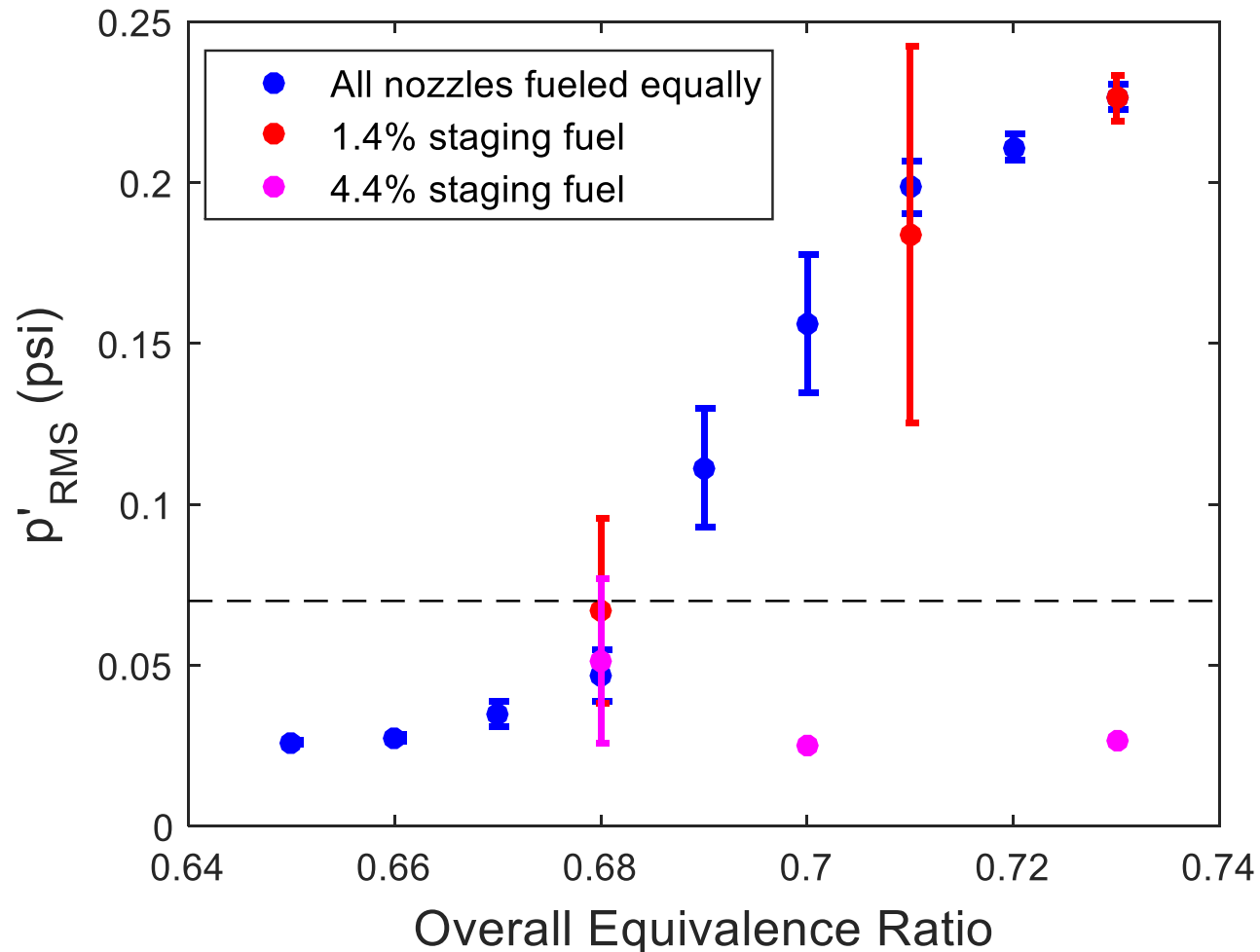


Control valve

Overview of presentation

- Project motivation and approach
- Year 1 Results:
 - Steady-state fuel staging – mechanisms for instability suppression
 - Transient fuel staging – natural system timescales
- Conclusions and next steps

In line with industry experience, we have shown that fuel staging suppresses instability in a multi-nozzle combustor

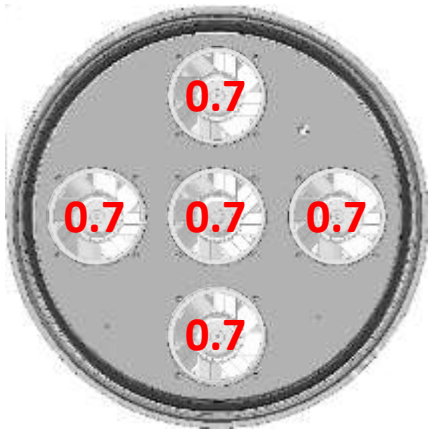


TASK 3: Test matrix was developed to measure the effect of fuel splitting and quantify repeatability, a key technical challenge

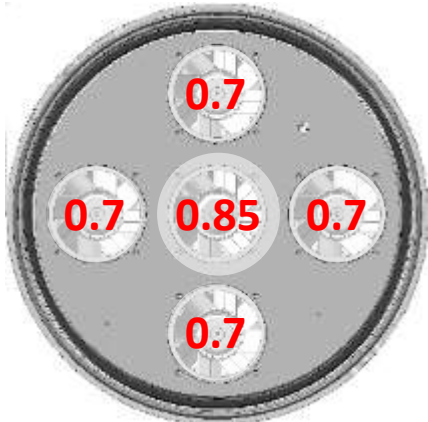
Test Case 1 – Varying Global ϕ

- ϕ_{center} increases to suppress instability
- ϕ_{outer} remains constant
- ϕ_{global} varies

Unstable:



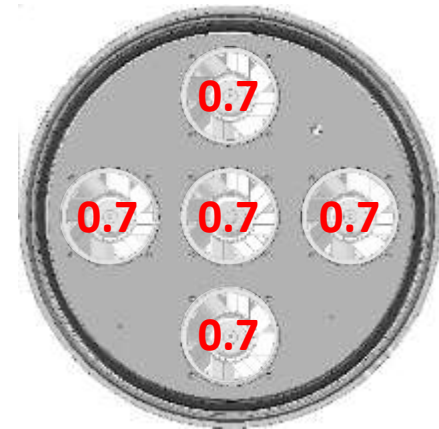
Stable:



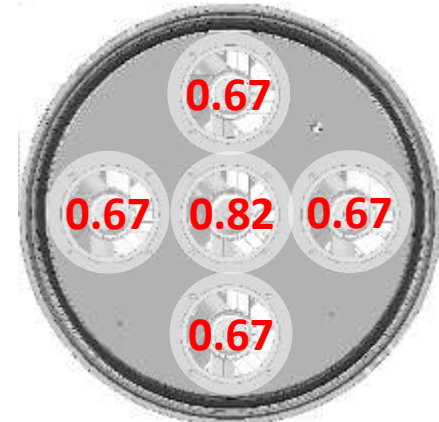
Test Case 2 – Constant Global ϕ

- ϕ_{center} increases to suppress instability
- ϕ_{outer} decreases
- ϕ_{global} is constant

Unstable:



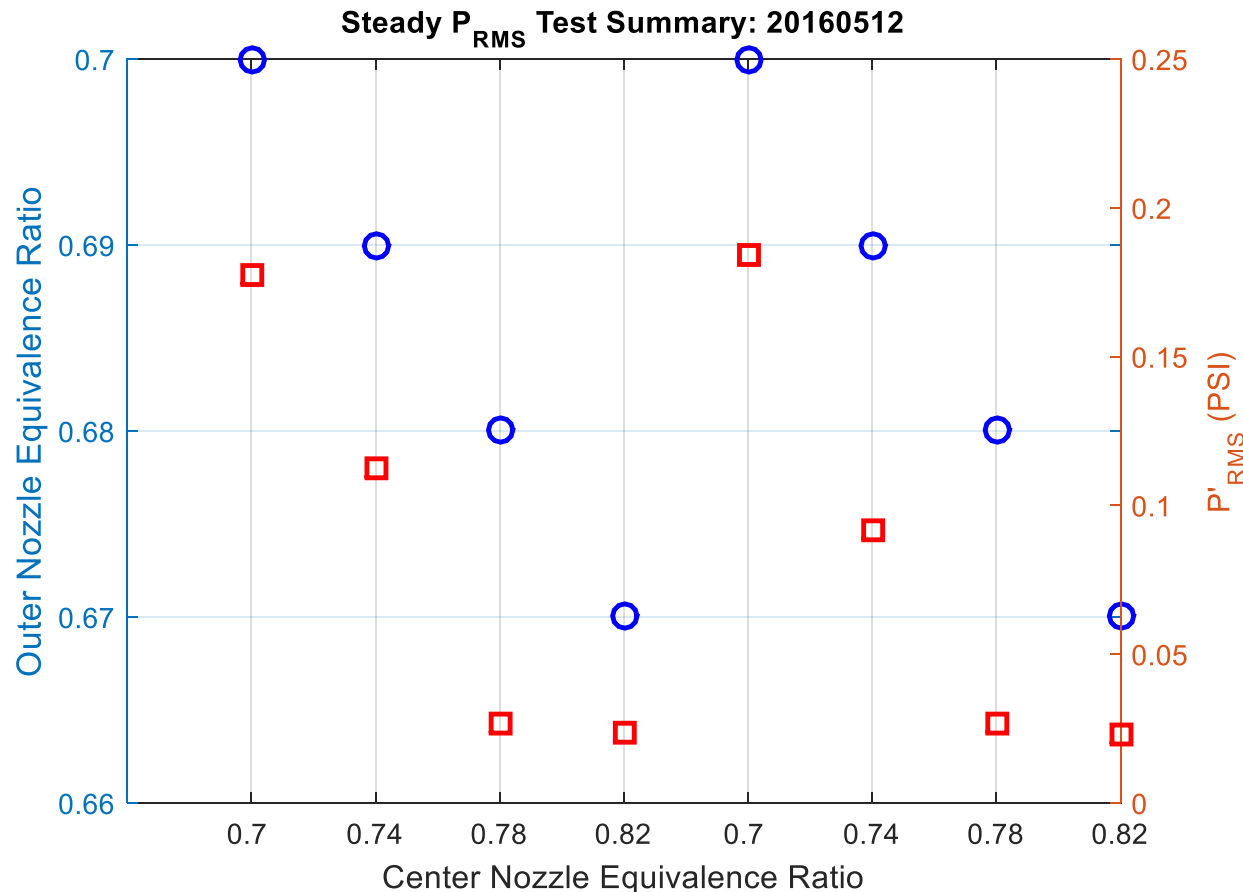
Stable:



Fuel staging was found to be able to suppress combustion instability when fuel flow is increased to middle nozzle

Test Case 2 – Constant Global ϕ

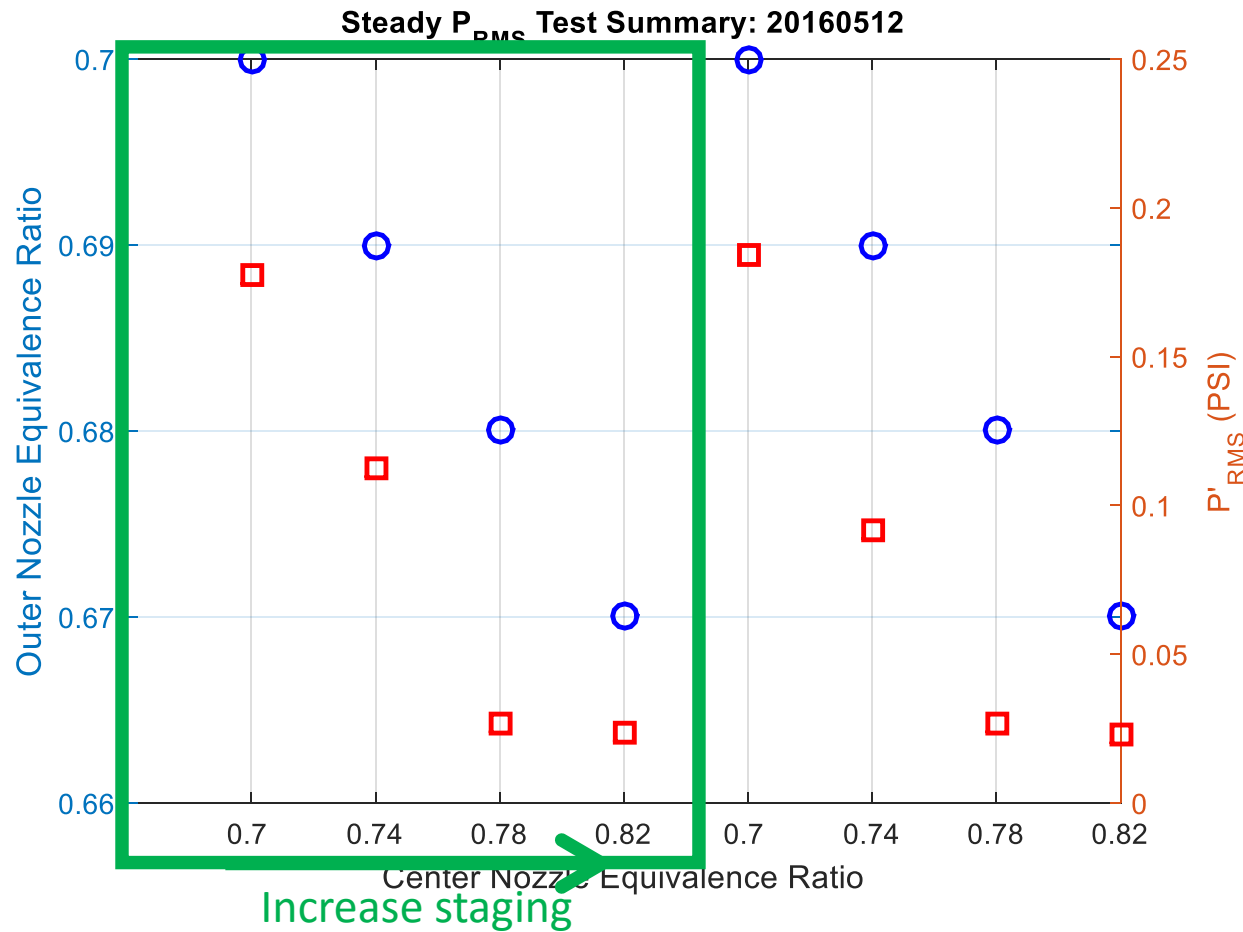
- ϕ_{center} increases to suppress instability
- ϕ_{outer} decreases
- ϕ_{global} is constant



Fuel staging was found to be able to suppress combustion instability when fuel flow is increased to middle nozzle

Test Case 2 – Constant Global ϕ

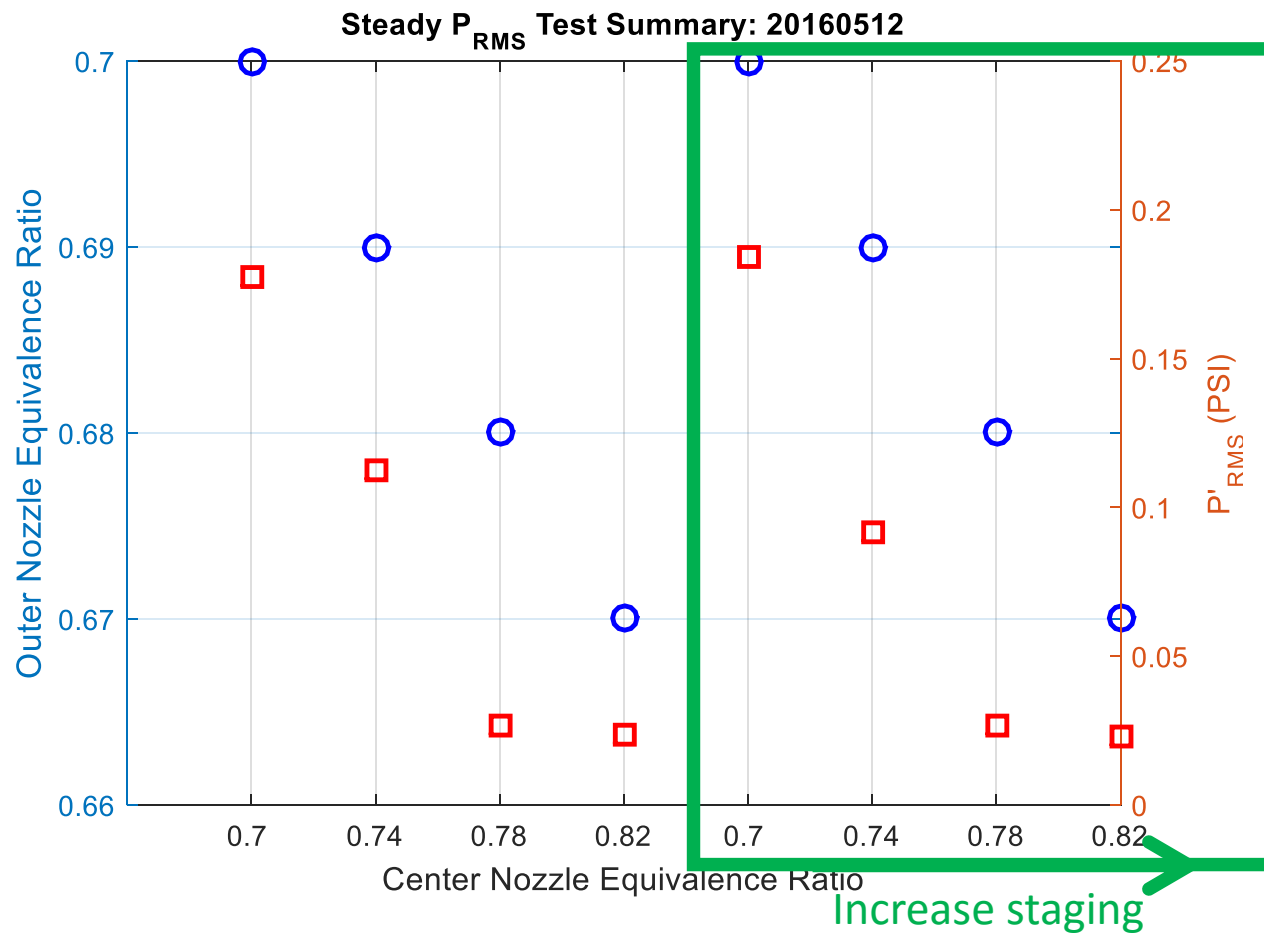
- ϕ_{center} increases to suppress instability
- ϕ_{outer} decreases
- ϕ_{global} is constant



Fuel staging was found to be able to suppress combustion instability when fuel flow is increased to middle nozzle

Test Case 2 – Constant Global ϕ

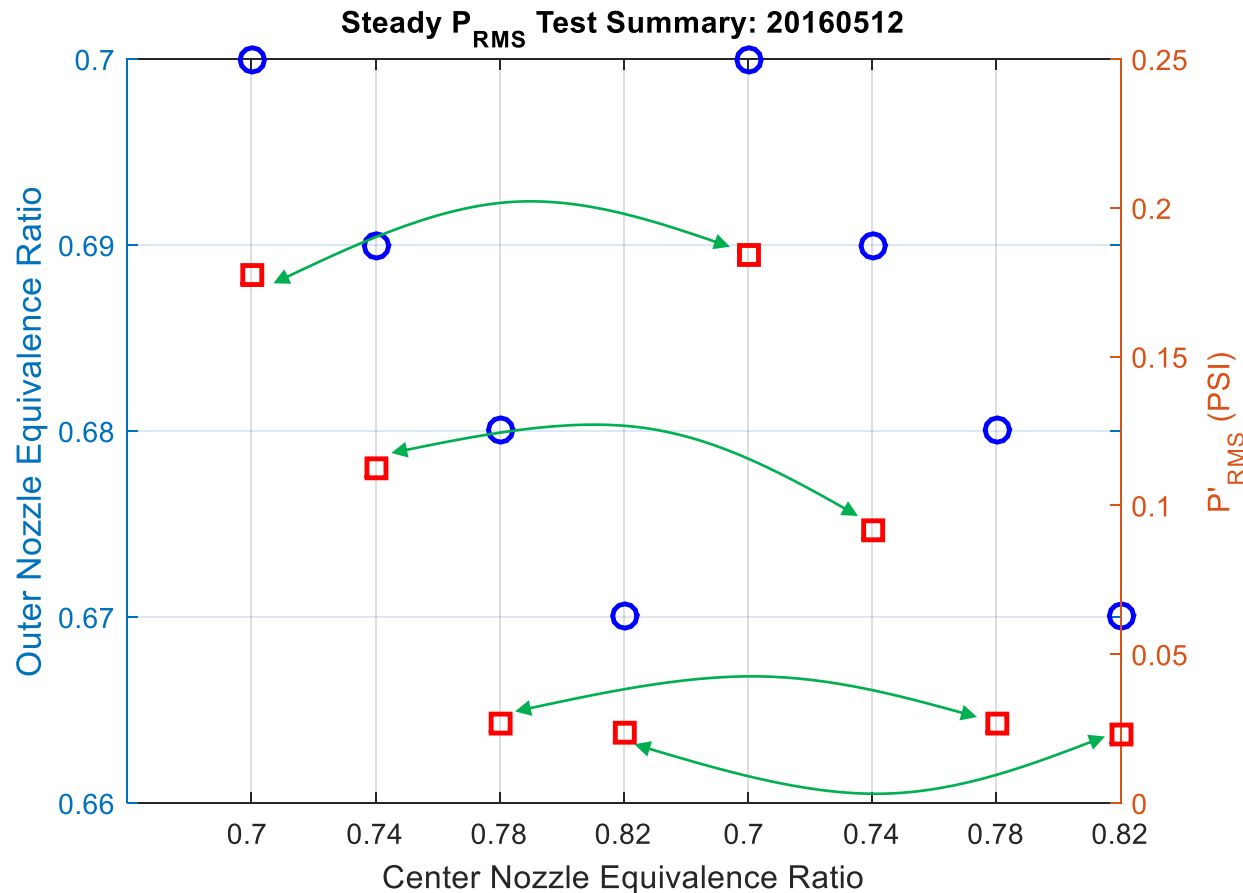
- ϕ_{center} increases to suppress instability
- ϕ_{outer} decreases
- ϕ_{global} is constant



Fuel staging was found to be able to suppress combustion instability when fuel flow is increased to middle nozzle

Test Case 2 – Constant Global ϕ

- ϕ_{center} increases to suppress instability
- ϕ_{outer} decreases
- ϕ_{global} is constant

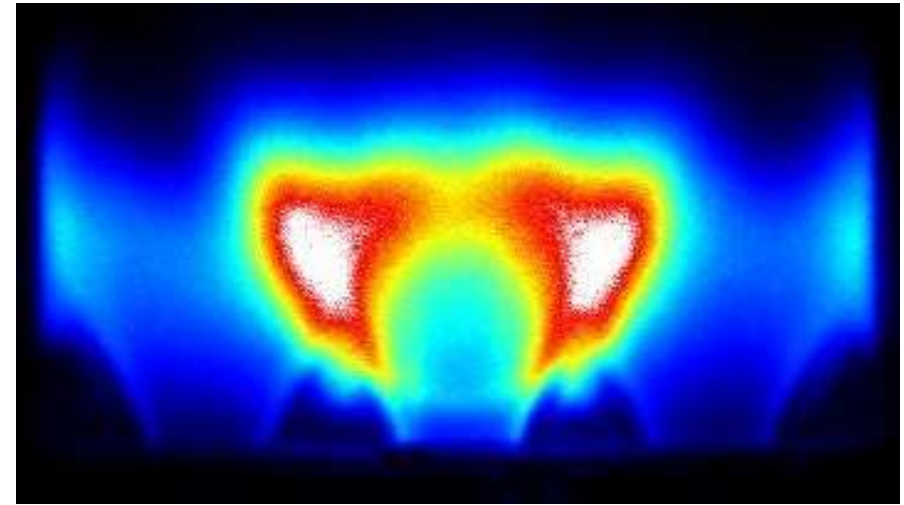


CH* chemiluminescence images are used to characterize flame structure, fluctuation, and phase

Images are obtained using a high-speed camera fitted with an intensifier



Line-of-sight photograph of multi-nozzle flame



Line-of-sight CH* chemiluminescence image of multi-nozzle flame

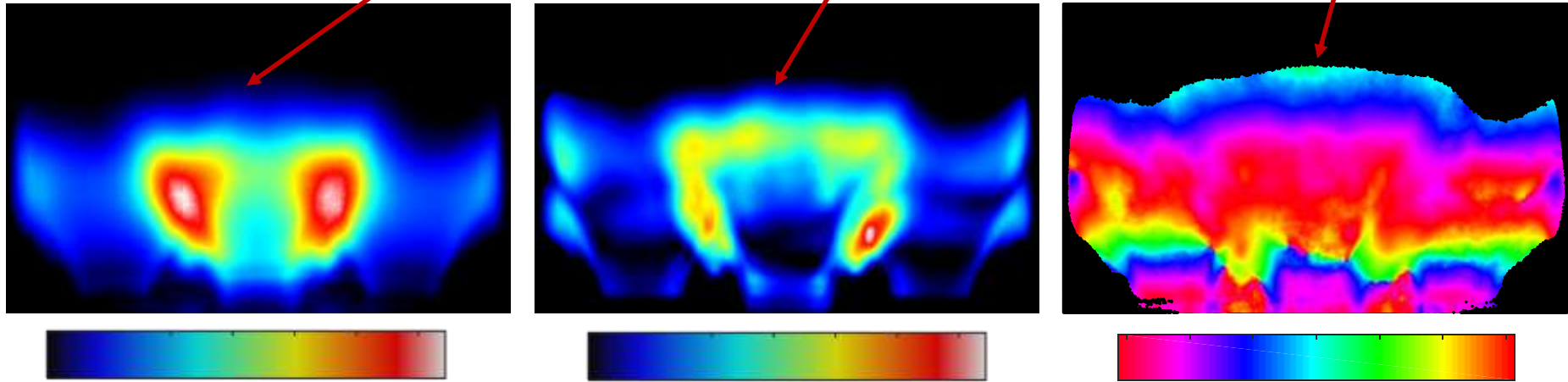
Pseudo color map is applied to chemiluminescence images



One second of high speed data is obtained at 4000 frames per second

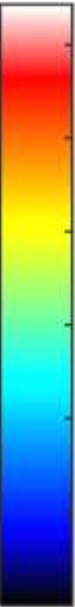
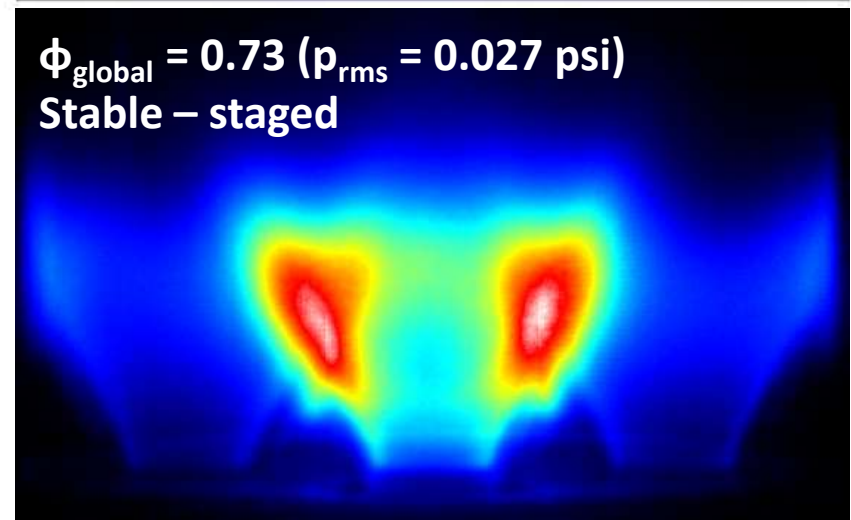
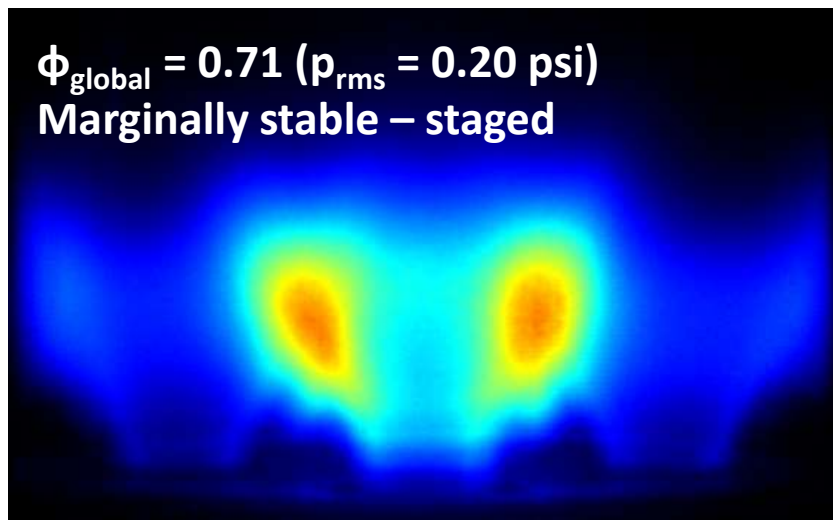
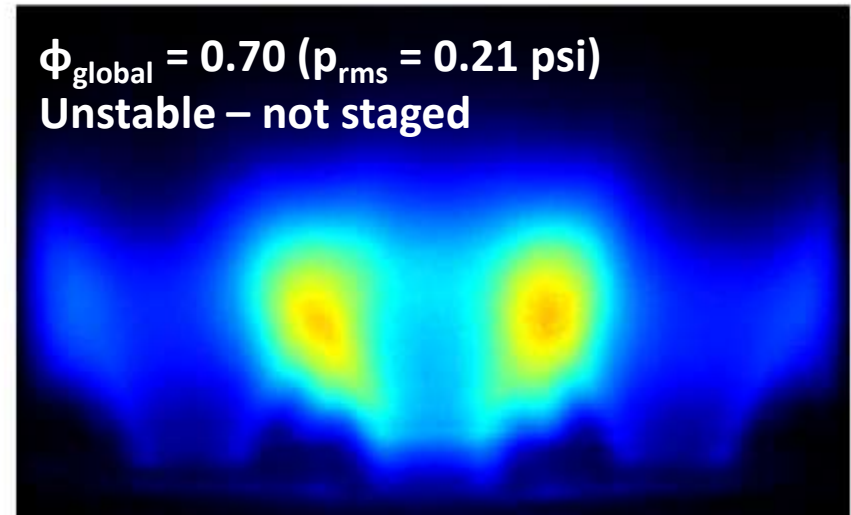
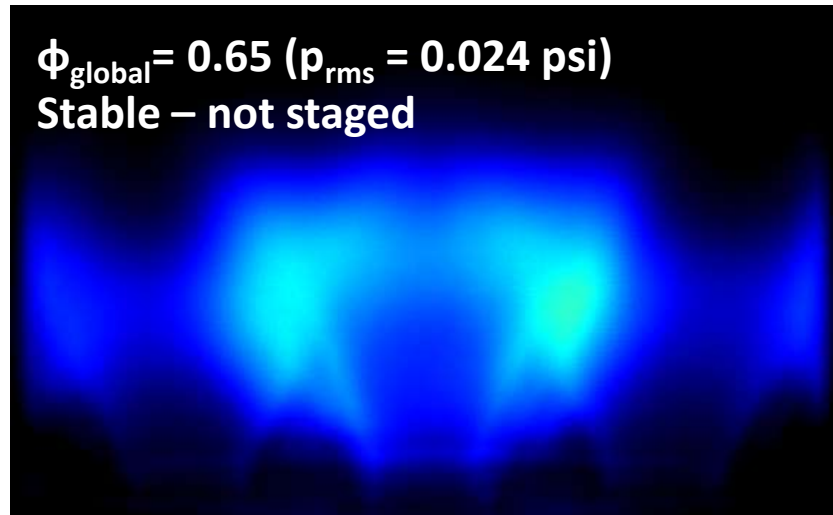
Images of forced flames can be decomposed into mean, RMS and phase components to understand instability mechanisms

$$\text{Filtered Image} = \text{Mean Image} + \sqrt{2} * \text{RMS Image} * \cos(2\pi ft + \text{Phase Image})$$

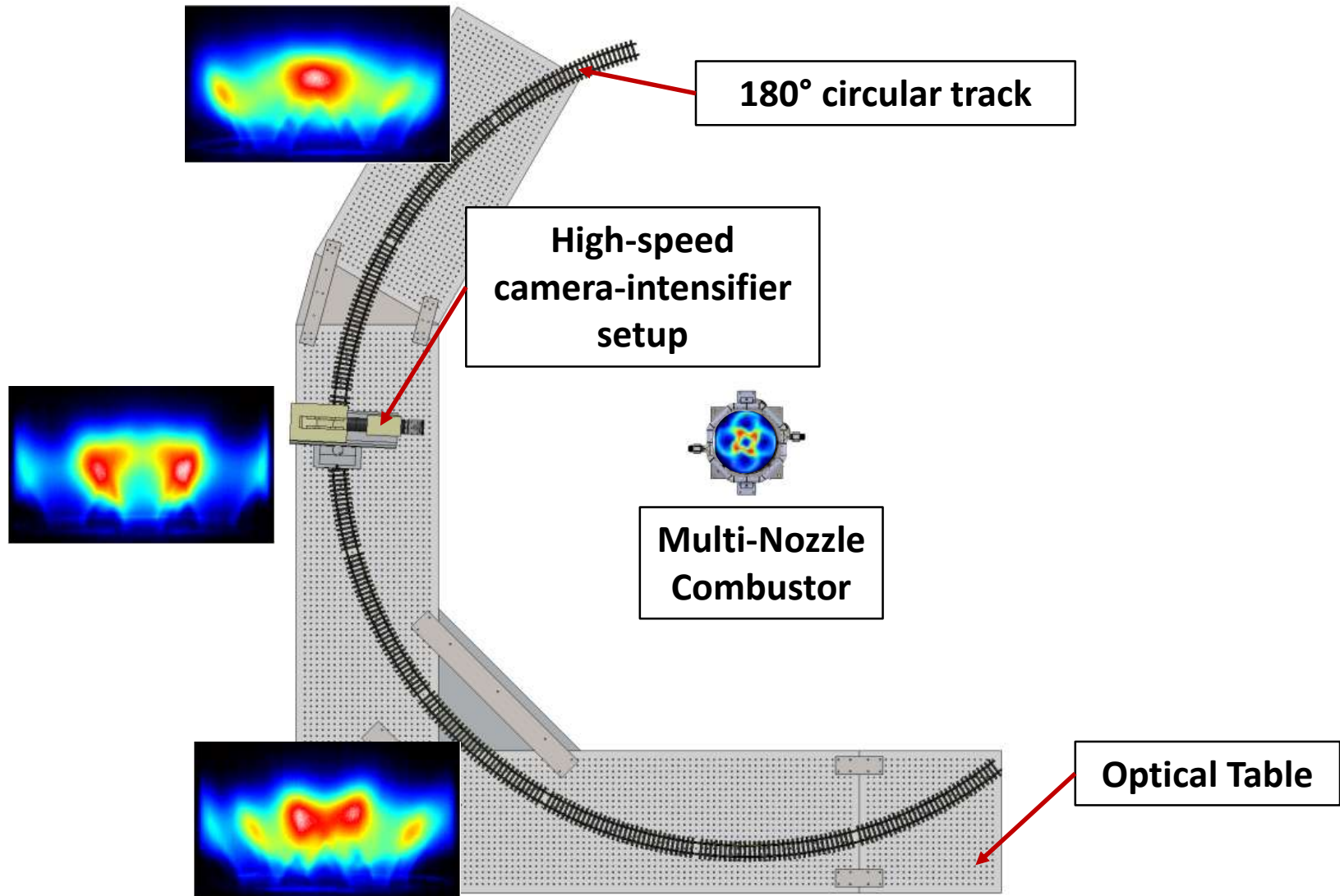


Mean, RMS, and phase images are analyzed at different test conditions to determine the effects of fuel staging on time-averaged and phase-averaged flame structure

Flame structure does not change significantly with additional staging, though center flame has higher heat release



Line-of-sight chemiluminescence images are acquired at 5° increments around the combustor to create tomographic image



Different flame structures are observed between stable unstaged and stable staged cases through tomographic imaging



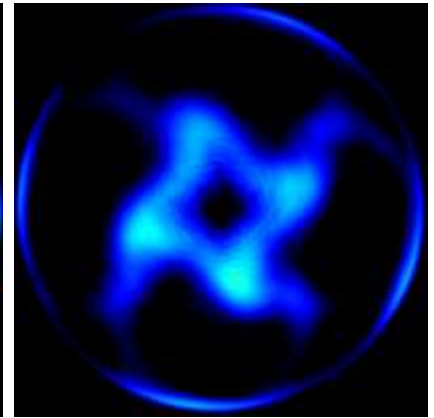
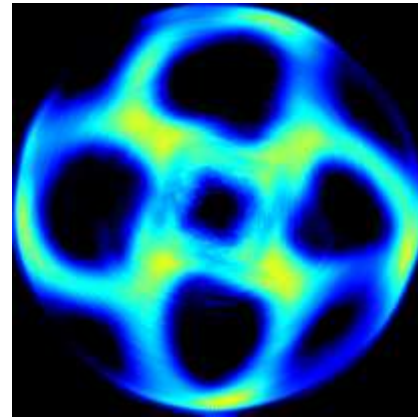
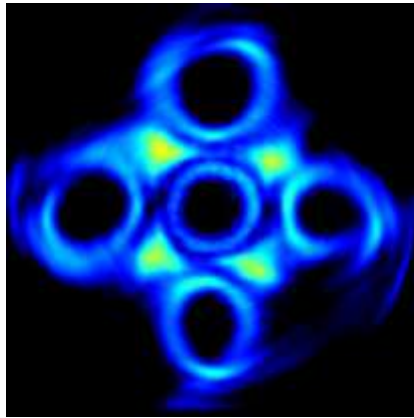
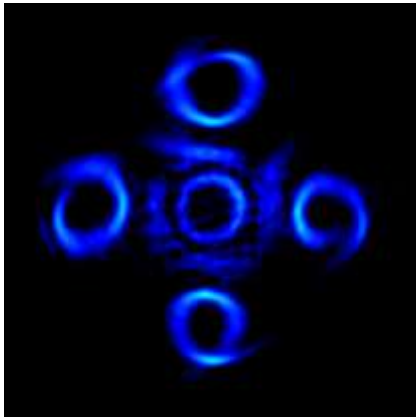
10 mm

25 mm

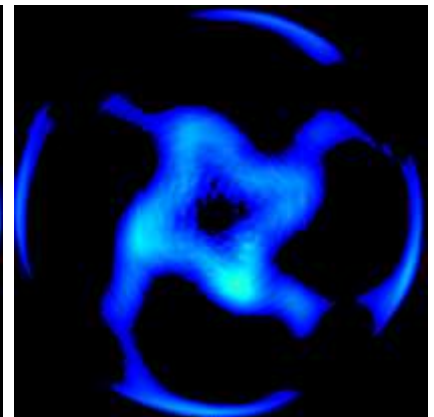
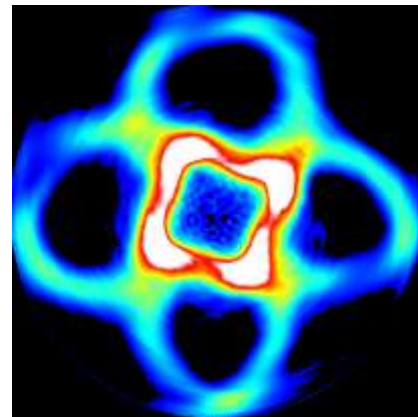
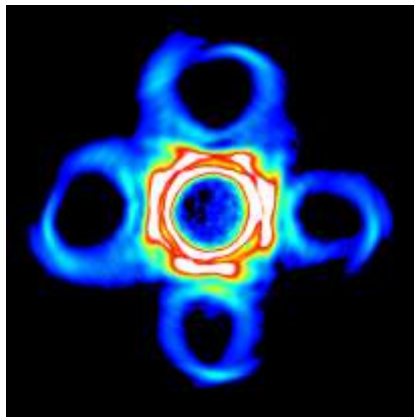
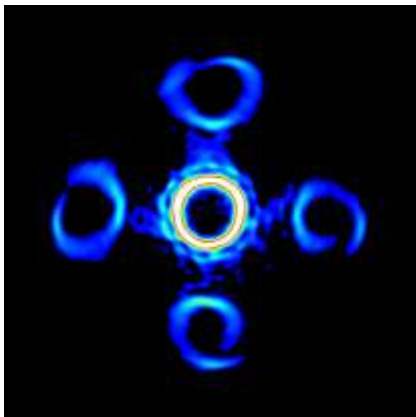
50 mm

90 mm

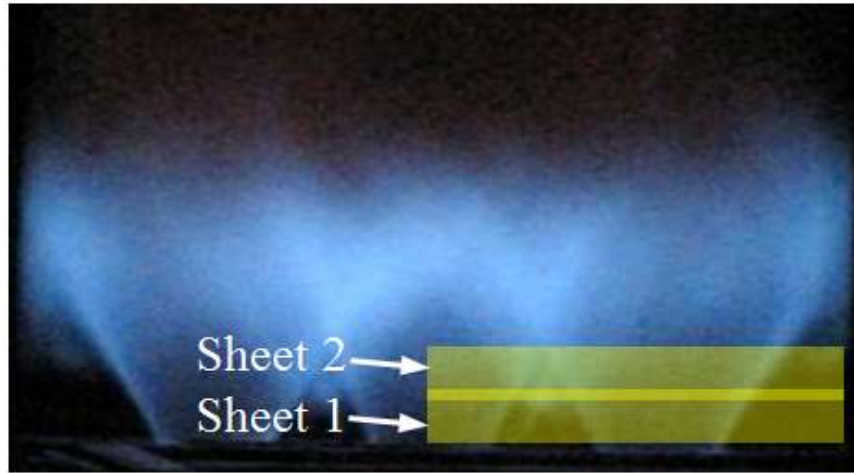
No fuel staging-
Global
 $\phi=0.65$



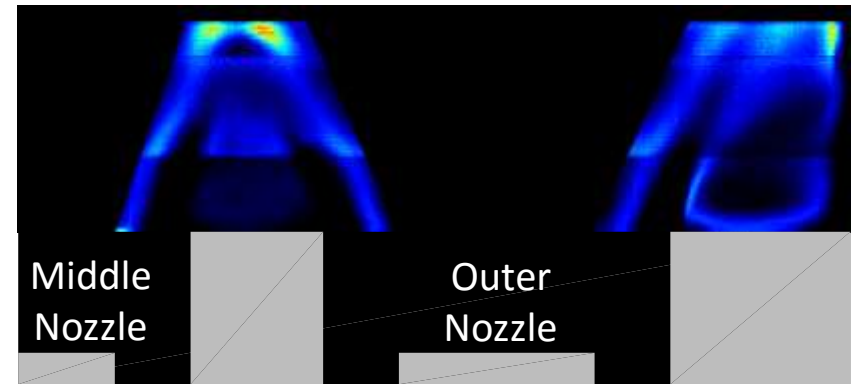
Fuel staging-
Global
 $\phi=0.7$



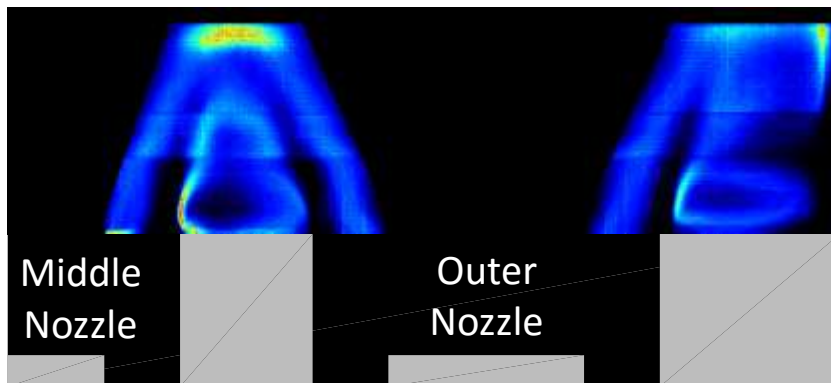
OH-PLIF imaging of the interaction region during staged cases shows instantaneous oscillations of the flame with staging



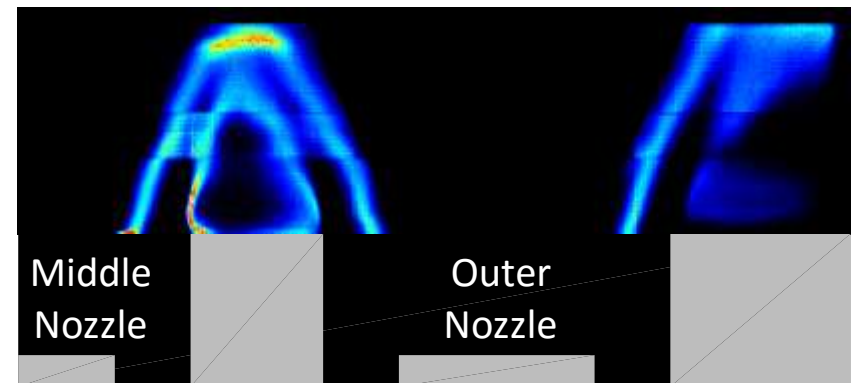
$\phi = 0.65$, stable – unstaged



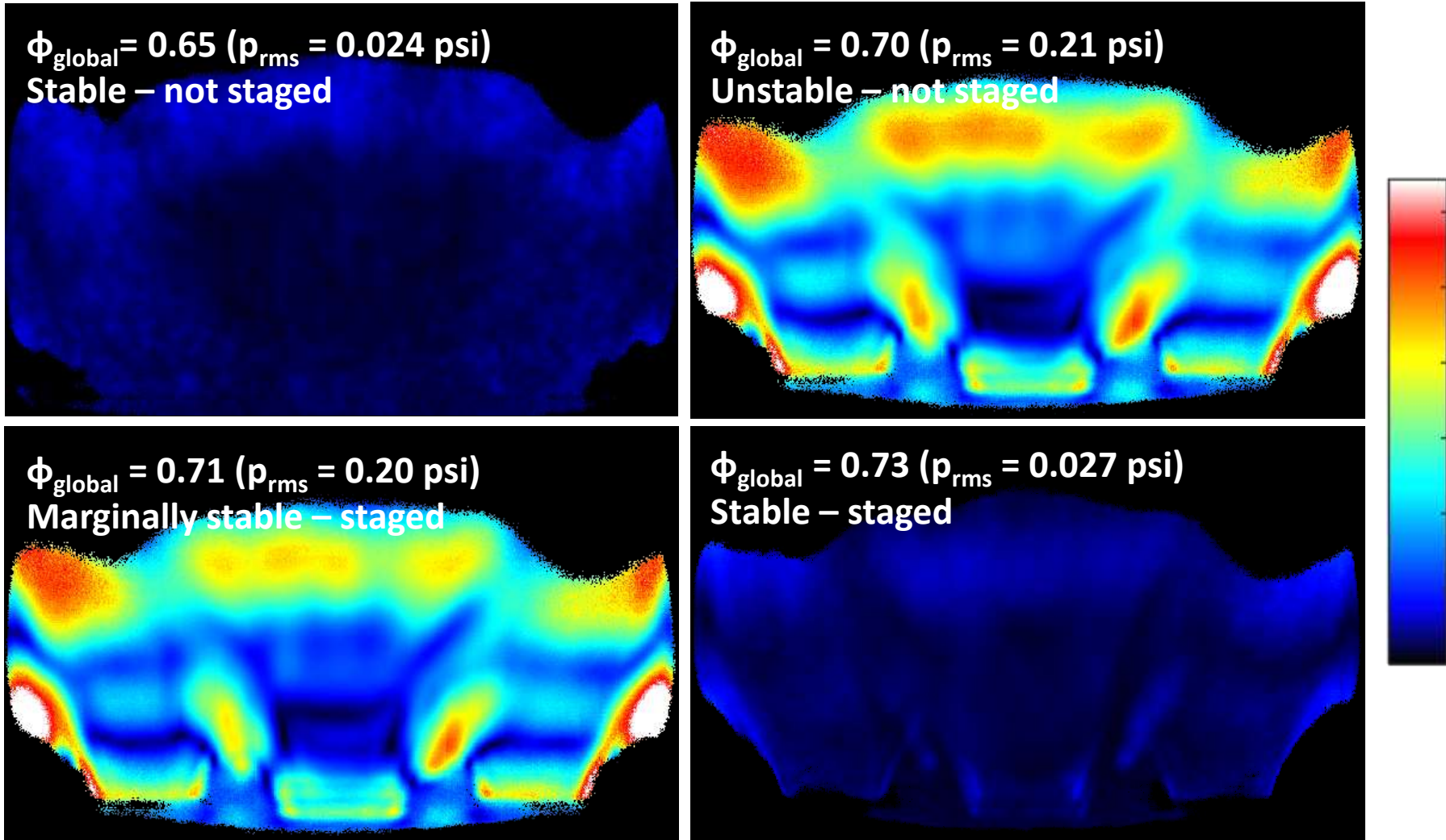
$\phi = 0.70$, unstable – unstaged



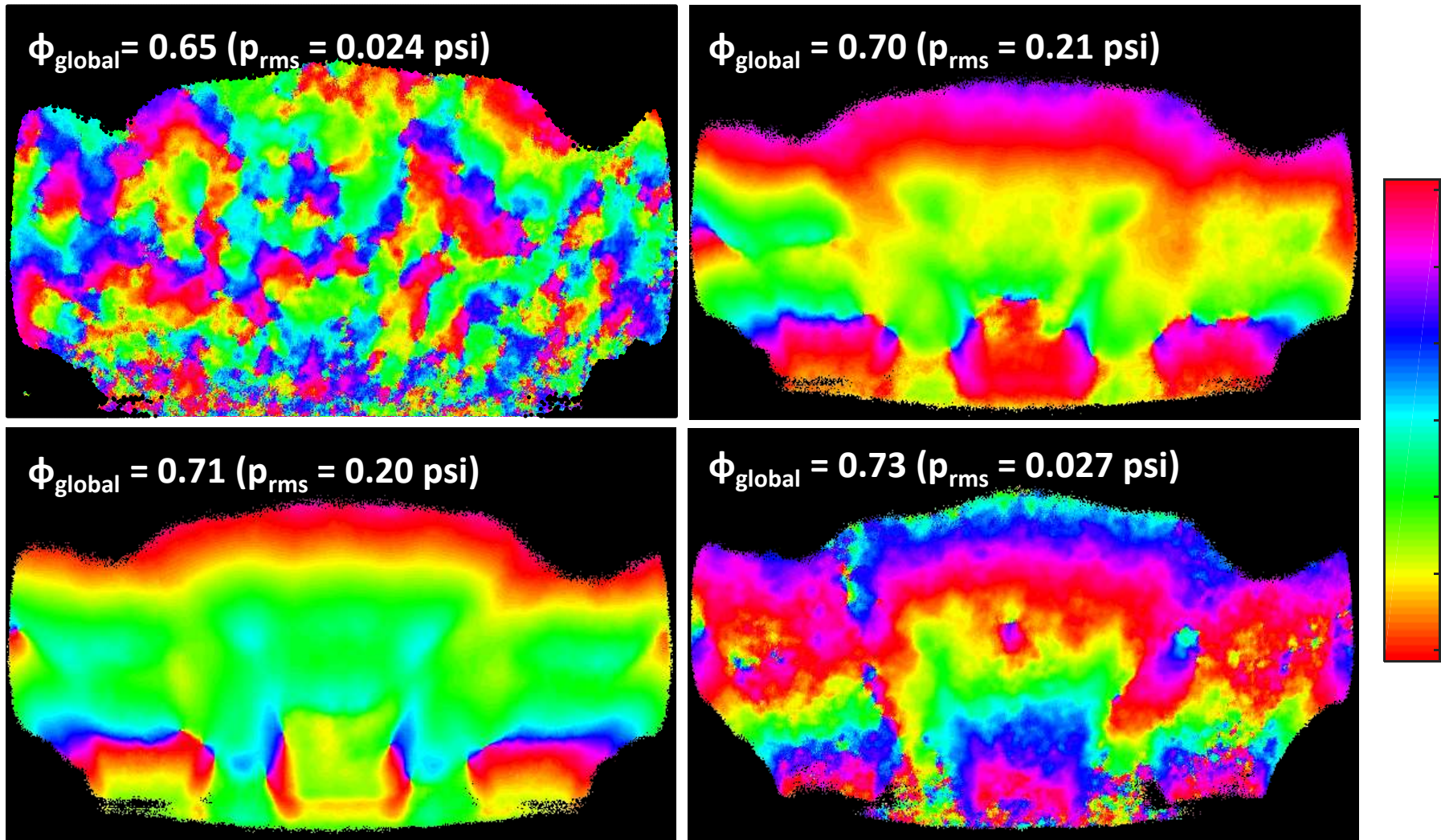
Staged - $\phi_{\text{outer}} = 0.70$, $\phi_{\text{middle}} = 0.85$



Heat release rate RMS levels are suppressed with staging, though signature is visible even at highest staging amount

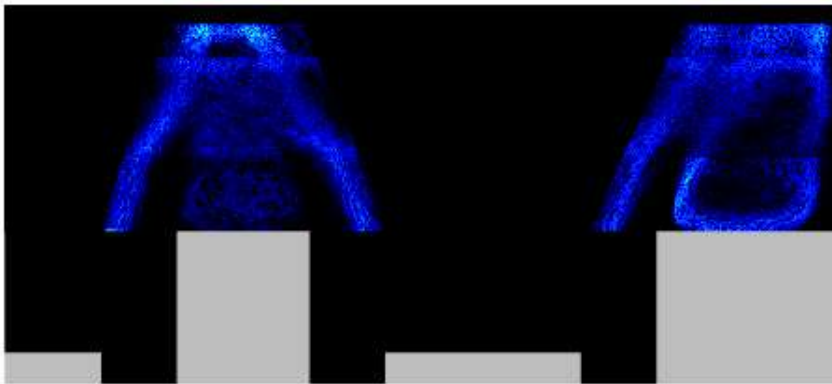


Phase of oscillations seems to indicate phase shift in oscillations during staging, possible suppression mechanism

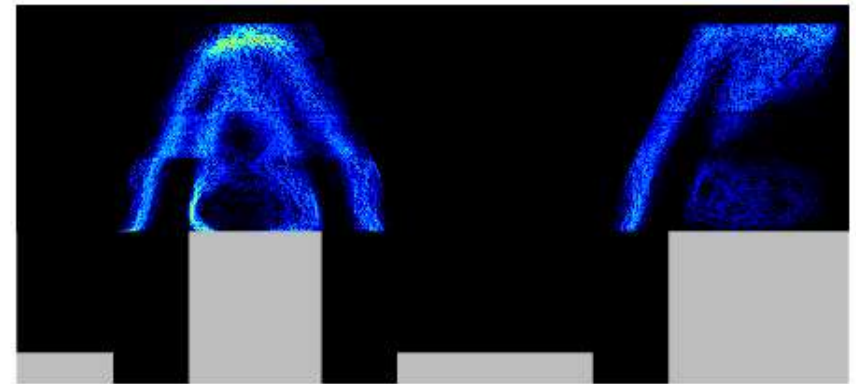


Differences in flame structure and the disturbances along the flame likely drive the phase-cancellation phenomenon

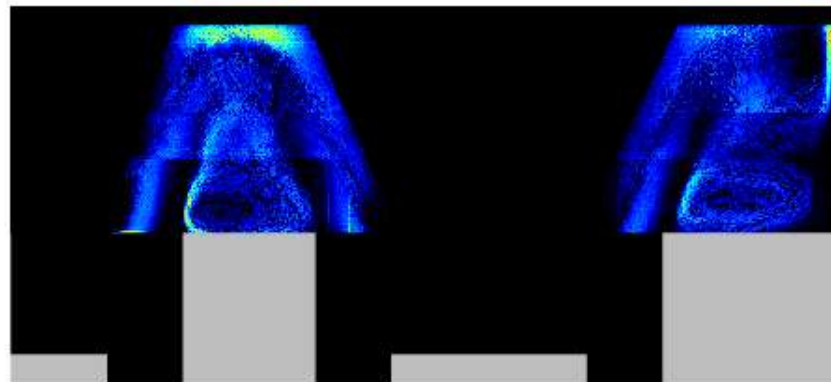
Stable – Unstaged
($\phi=0.65$)



Stable – Staged
($\phi_{\text{outer}} = 0.70, \phi_{\text{middle}} = 0.85$)



Unstable – Unstaged
($\phi=0.70$)



Overview of presentation

- Project motivation and approach

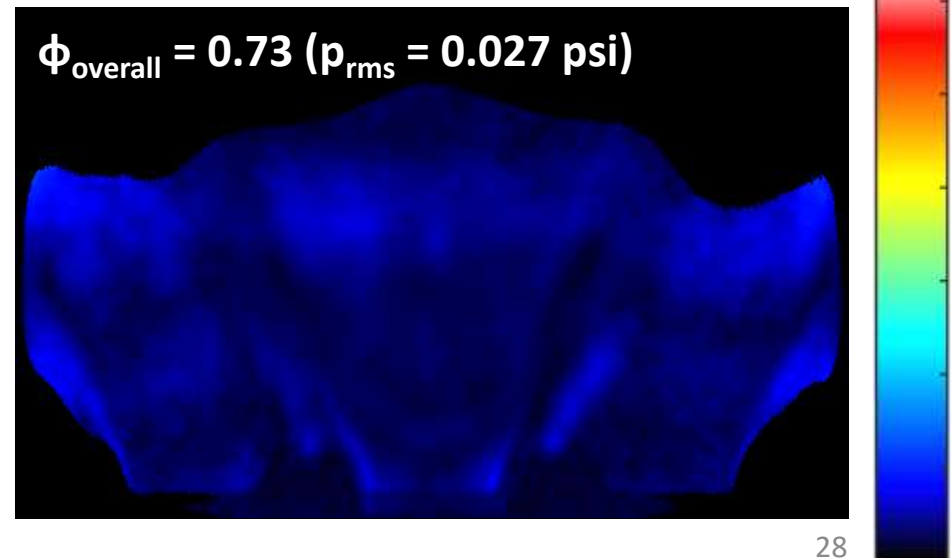
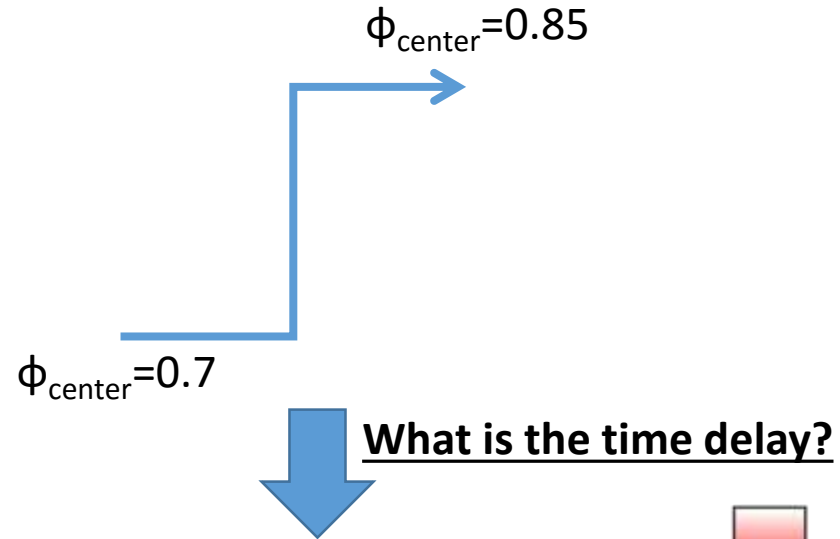
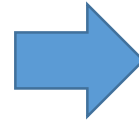
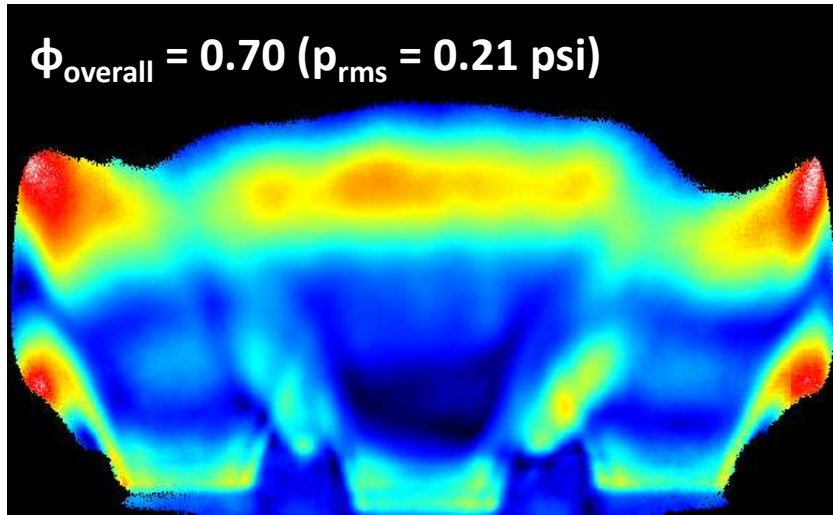
- Year 1 Results:

 - Steady-state fuel staging – mechanisms for instability suppression

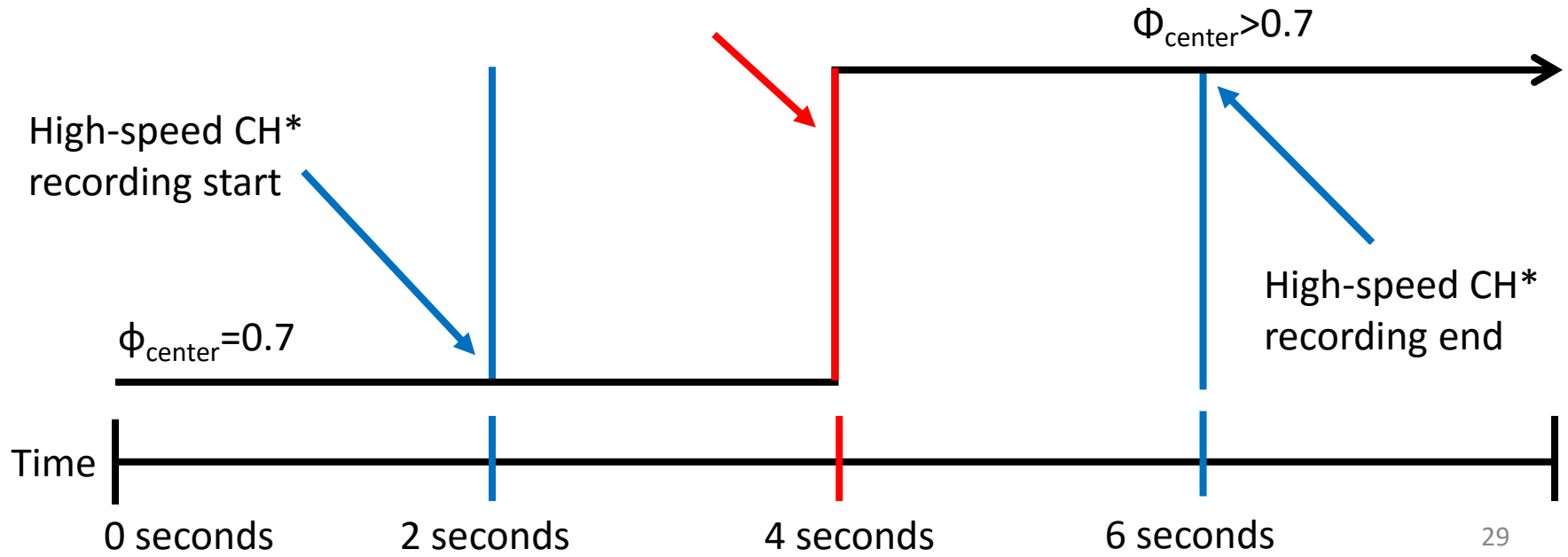
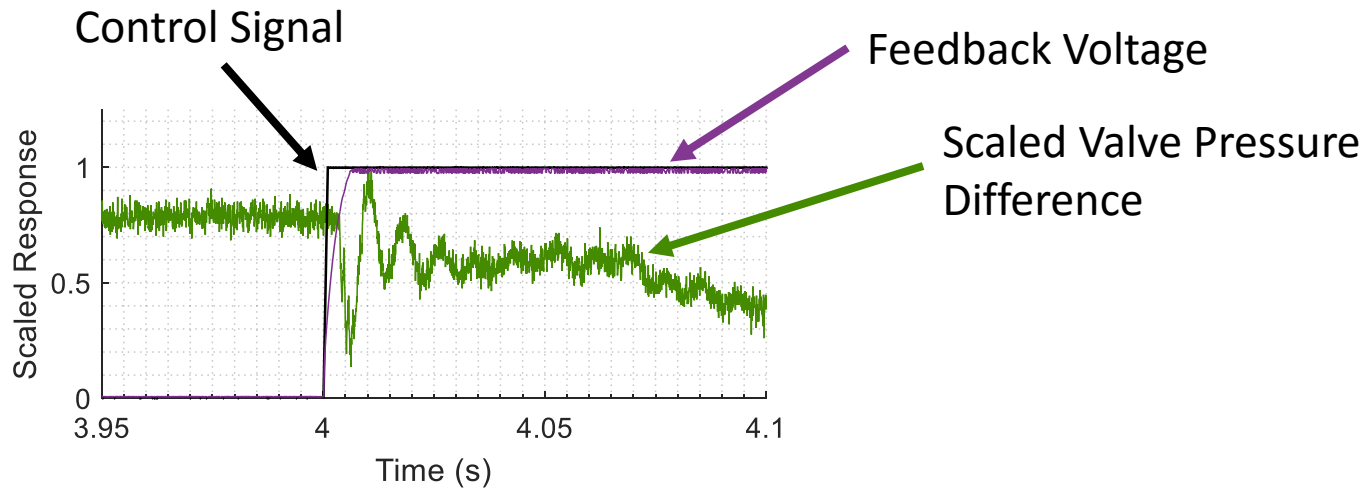
 - Transient fuel staging – natural system timescales

- Conclusions and next steps

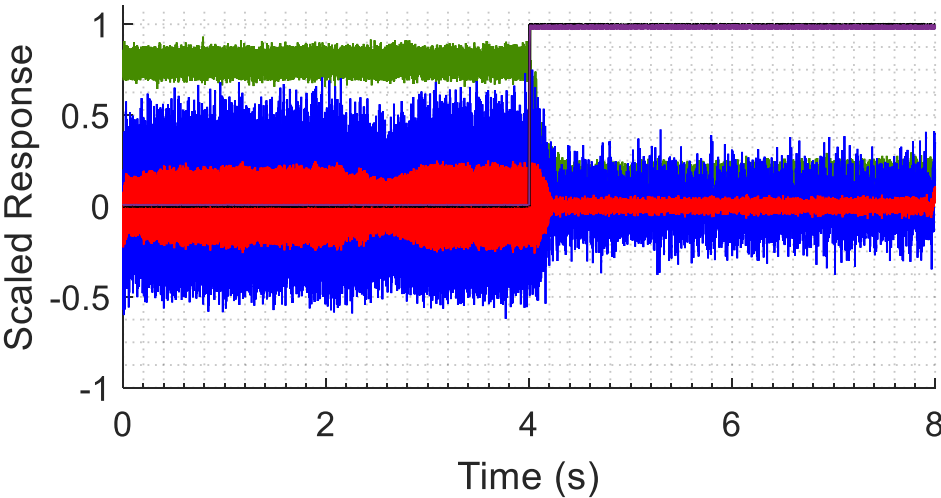
Task 4: Test matrix for initial transient testing considers step-change transients to determine natural time-scales of system



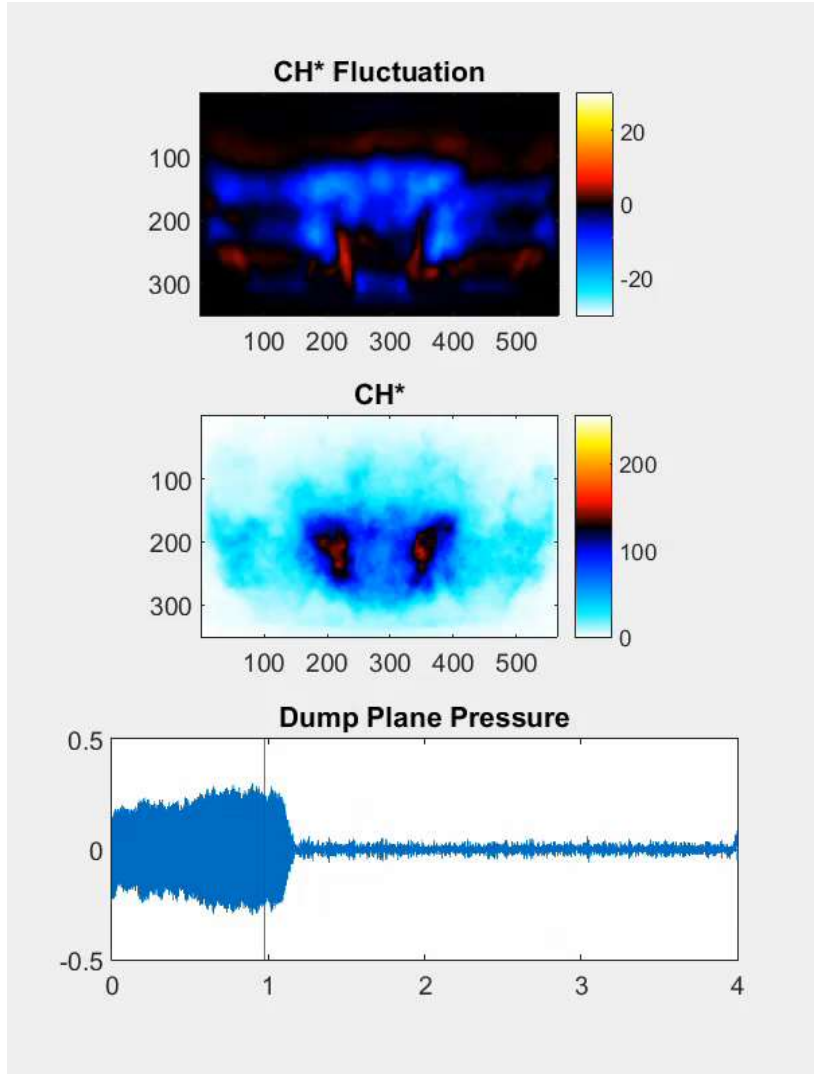
Impulse transients are executed using a fast-acting proportional control valve



Both the fluctuation in CH* (blue) and pressure (red) track each other through the transient event.



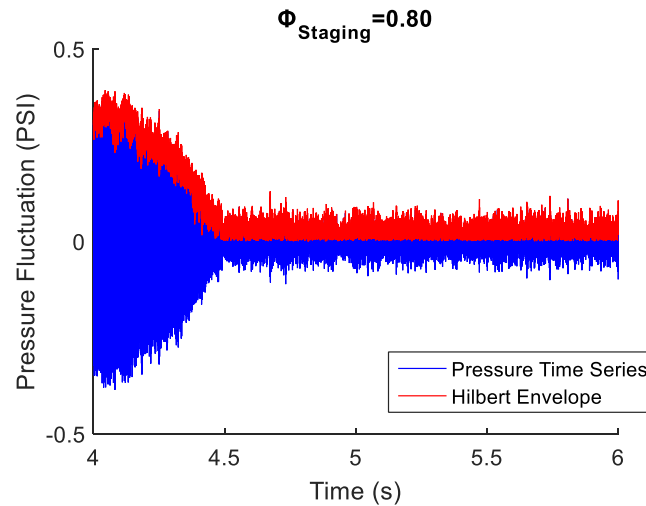
- Valve Pressure (1 scale)
- CH* (0.75 scale)
- Dump Plane Pressure (0.25 scale)
- Control Voltage (1 scale)
- Feedback Voltage (1 scale)



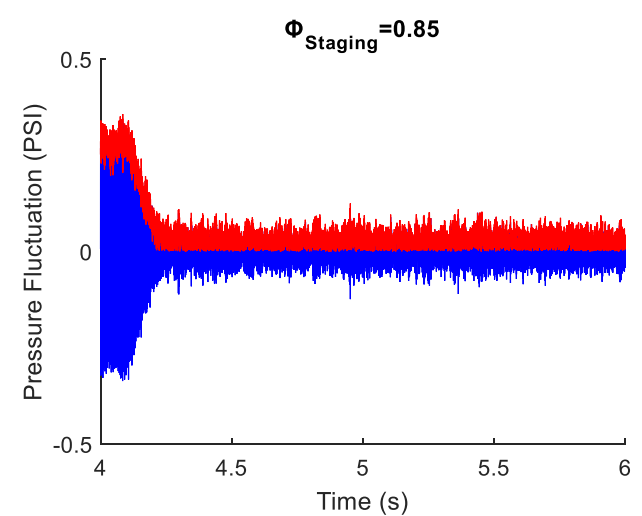
The growth/decay time of the instability reflects a natural time-scale of the system, and is dependent on staging level

Unstable →
Stable

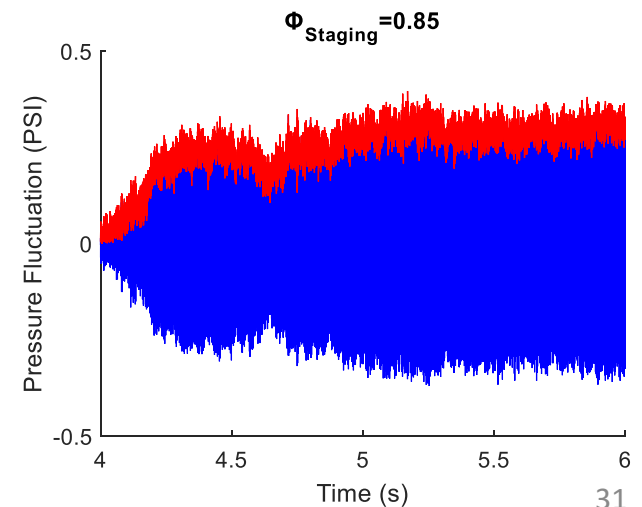
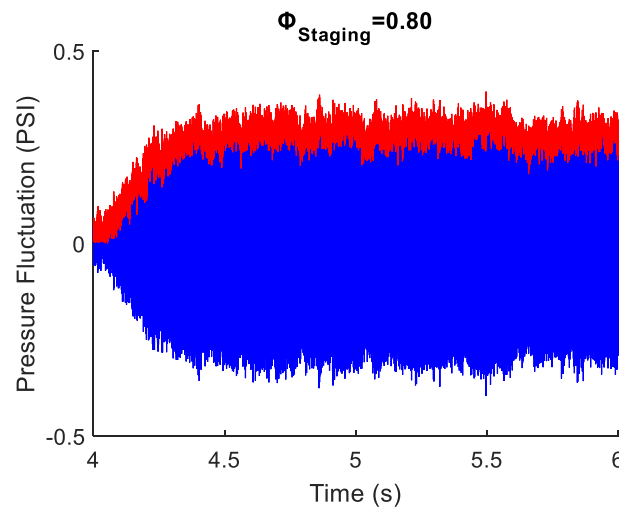
Center-nozzle: $\phi=0.8$



Center-nozzle: $\phi=0.85$



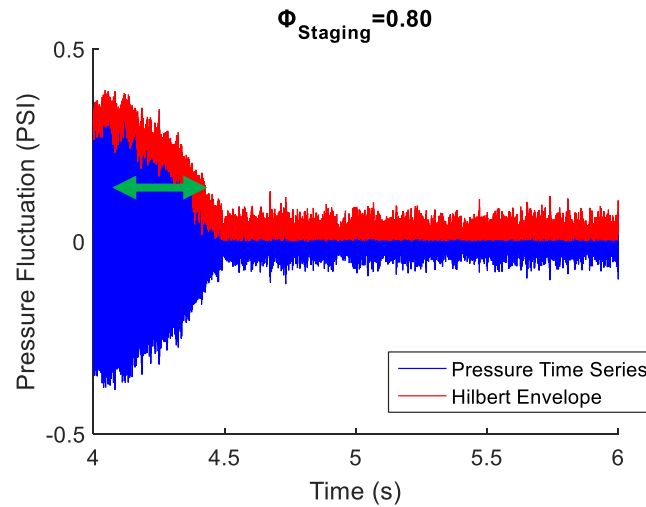
Stable →
Unstable



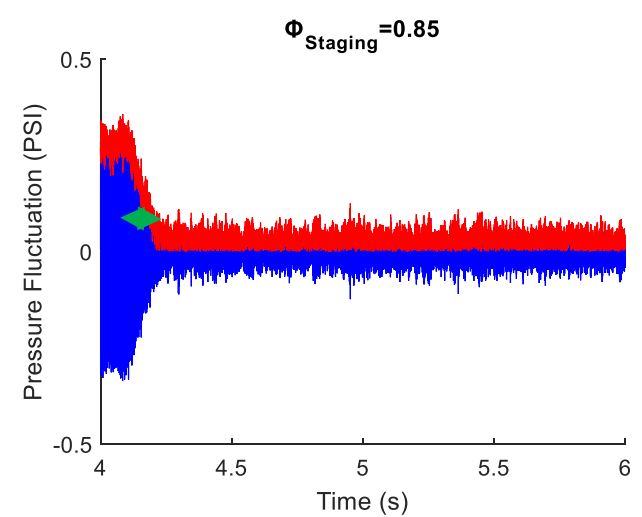
The growth/decay time of the instability reflects a natural time-scale of the system, and is dependent on staging level

Unstable →
Stable

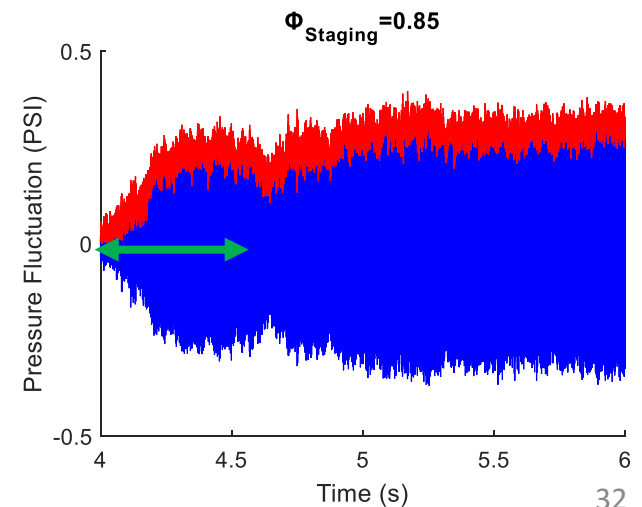
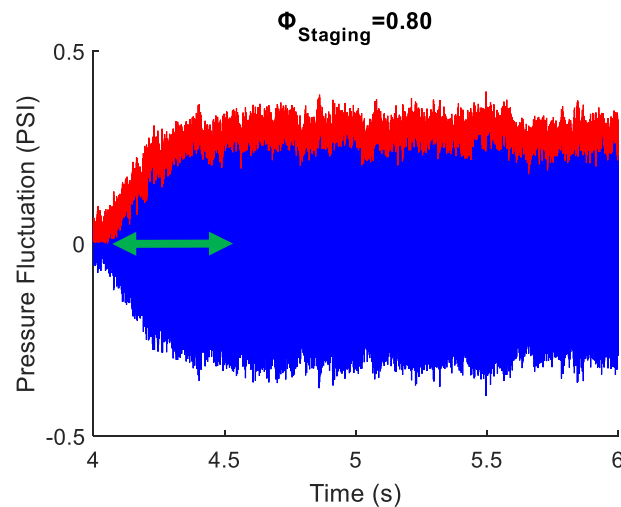
Center-nozzle: $\phi=0.8$



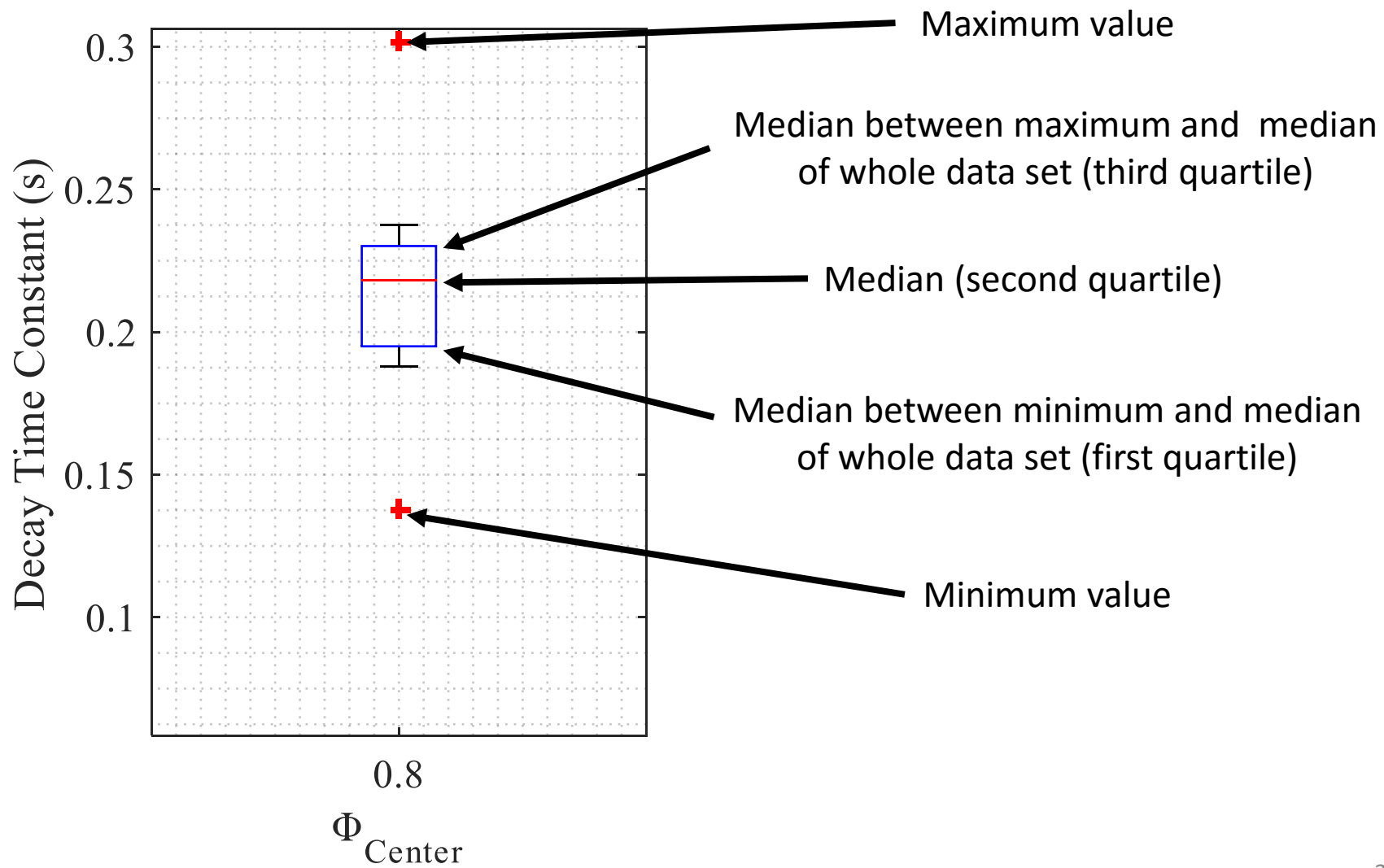
Center-nozzle: $\phi=0.85$



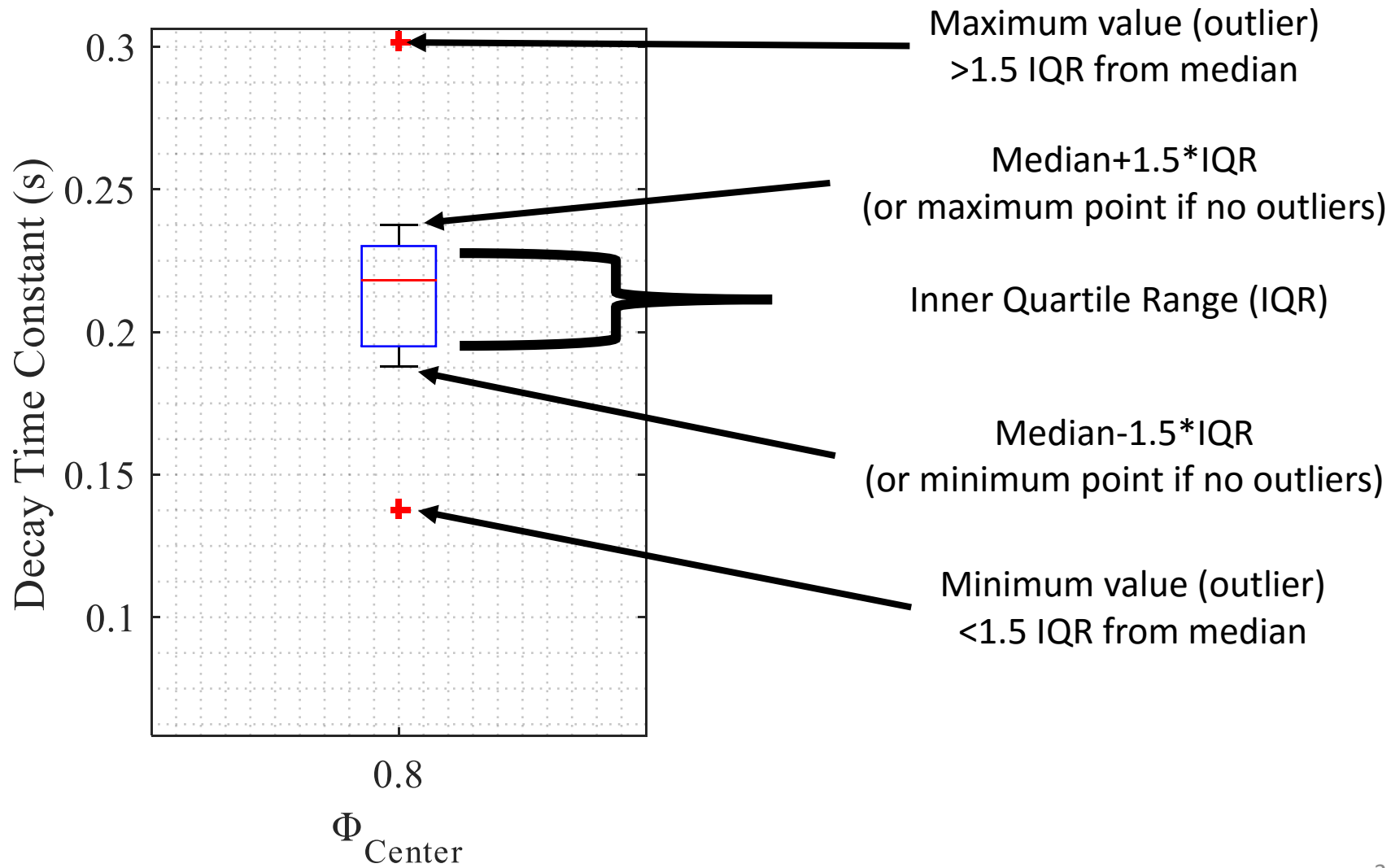
Stable →
Unstable



Box-and-whisker plots provide a useful way to visualize ensemble data.

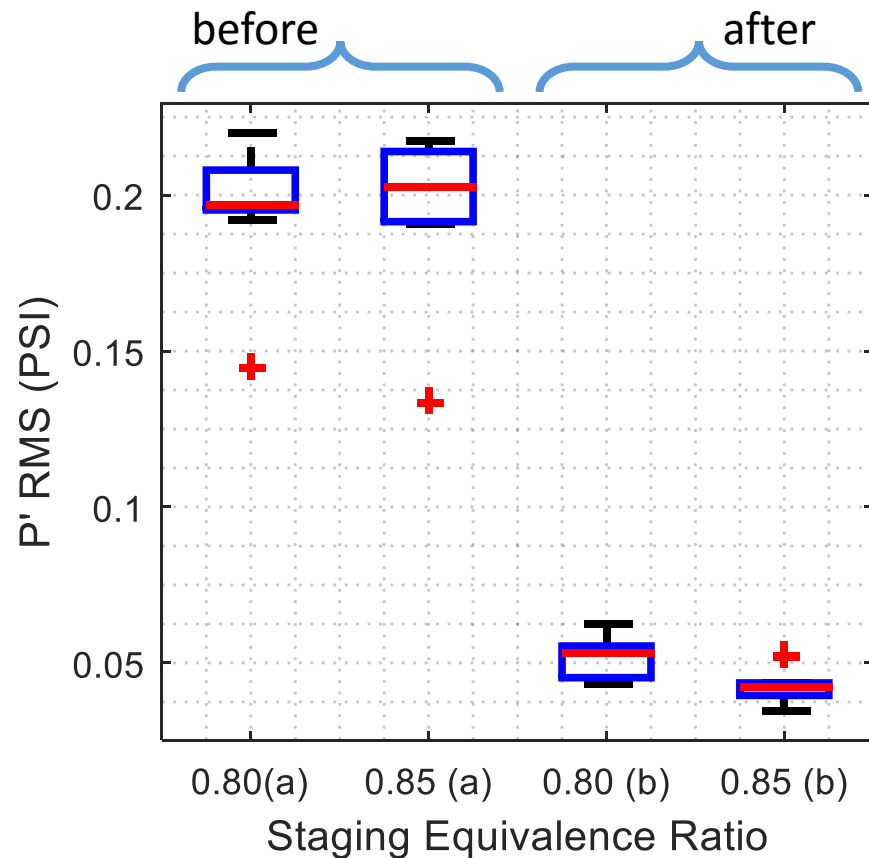


Box-and-whisker plots provide a useful way to visualize ensemble data.

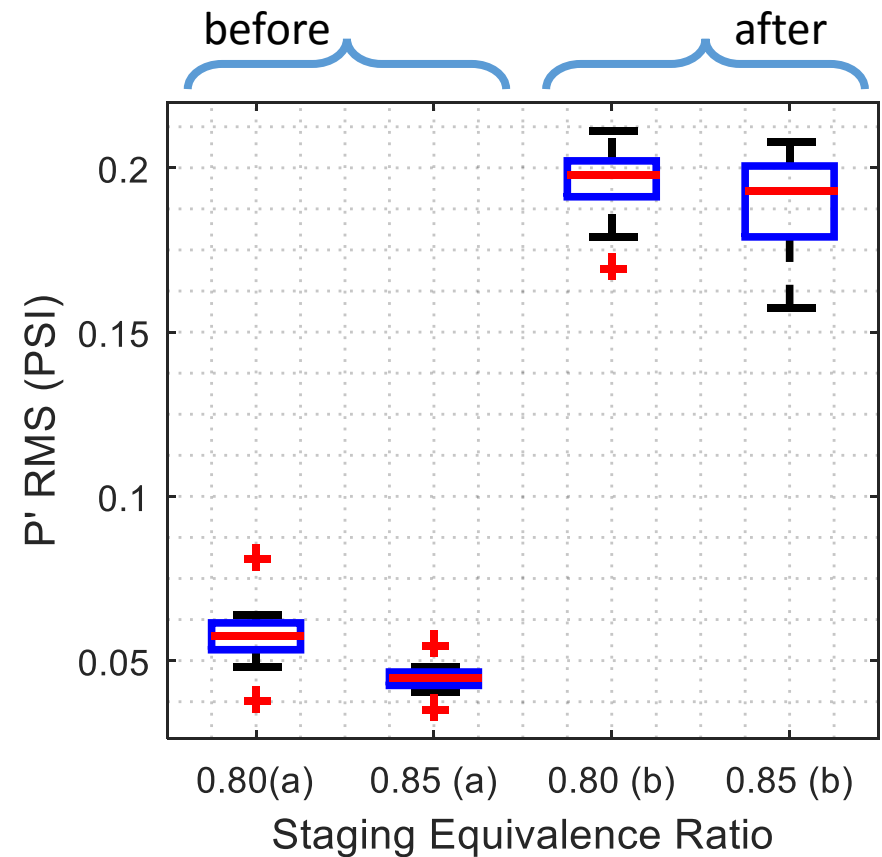


The pressures before and after the transient mirror the steady-state test results, showing high repeatability

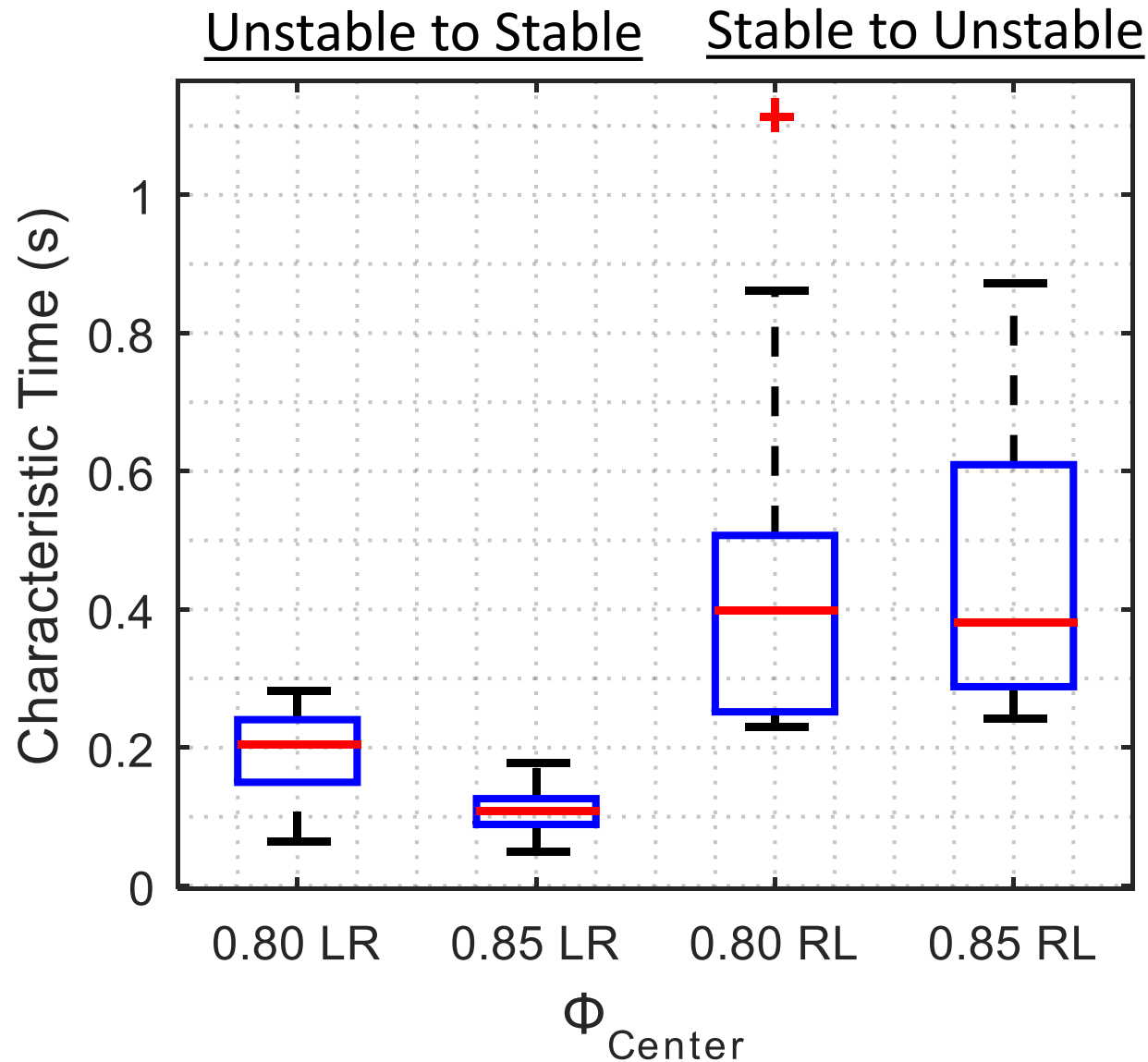
Unstable to Stable



Stable to Unstable

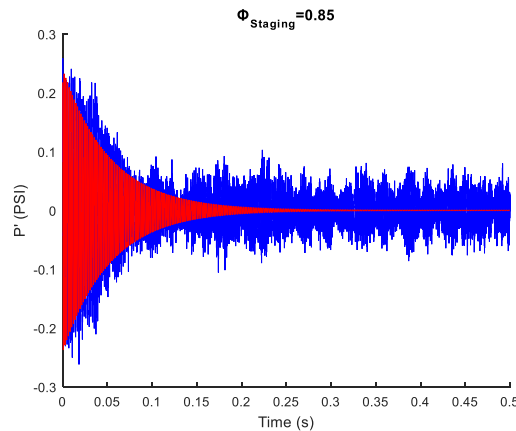


The characteristic decay time depends on staging amplitude, but the characteristic rise time does not appear to

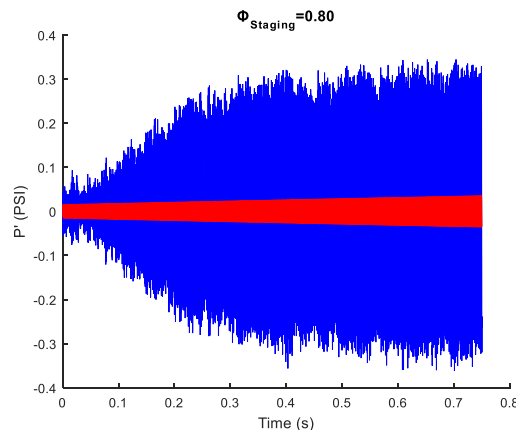


The functional form of the growth and decay profiles can help illuminate some of the physics involved in the processes

Model 1: Damped linear oscillator
decaying at a single frequency



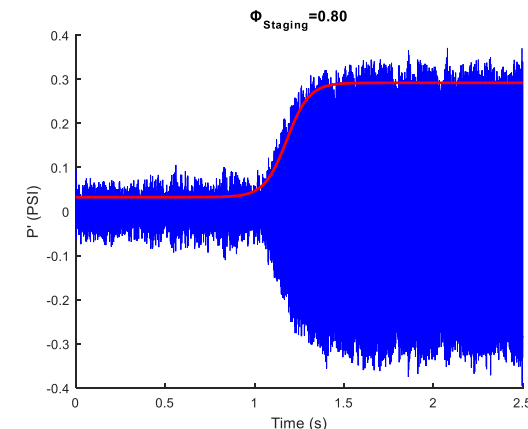
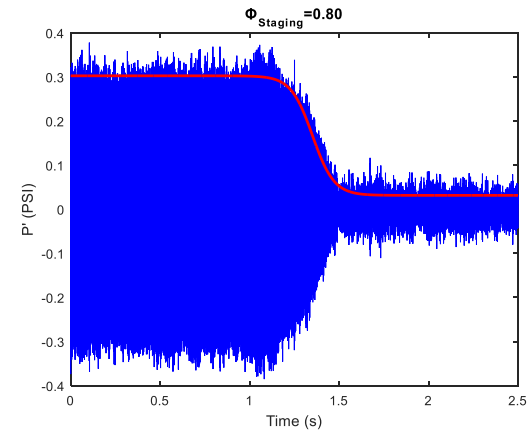
$$P'(t) = Ae^{-\lambda t} + AB * (1 - e^{-\lambda t}) * \sin(\omega t + \Phi)$$



$$P'(t) = AB e^{-\lambda t} + B * (1 - e^{-\lambda t}) * \sin(\omega t + \Phi)$$

Model 2: General Logistic
Growth/Decay

$$P'(t) = \frac{A - B}{(1 + e^{k(t-t_0)})} + B$$



Overview of presentation

- Project motivation and approach
- Year 1 Results:
 - Steady-state fuel staging – mechanisms for instability suppression
 - Transient fuel staging – natural system timescales
- Conclusions and next steps

Wrap-up and Questions

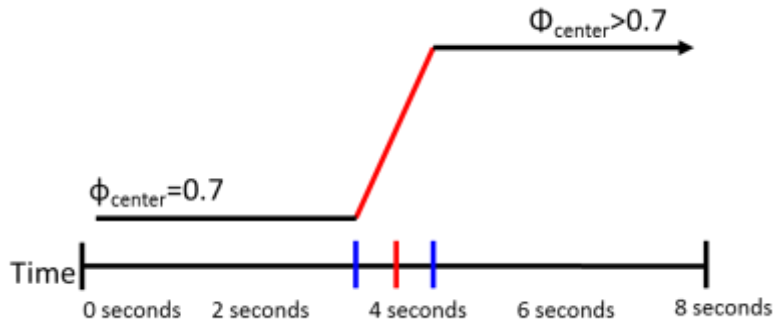
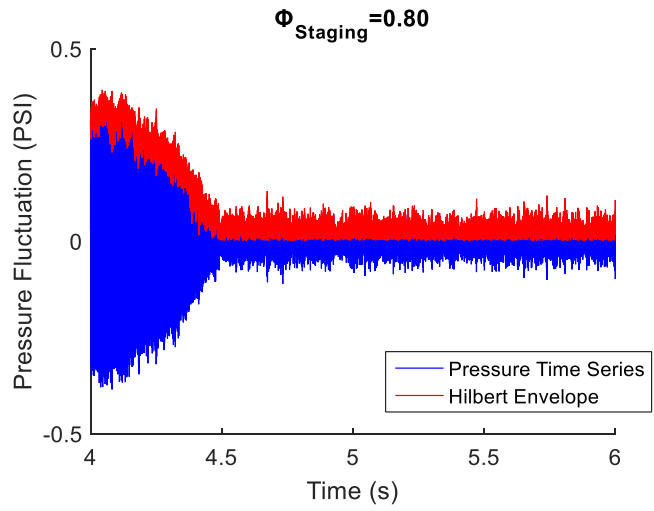
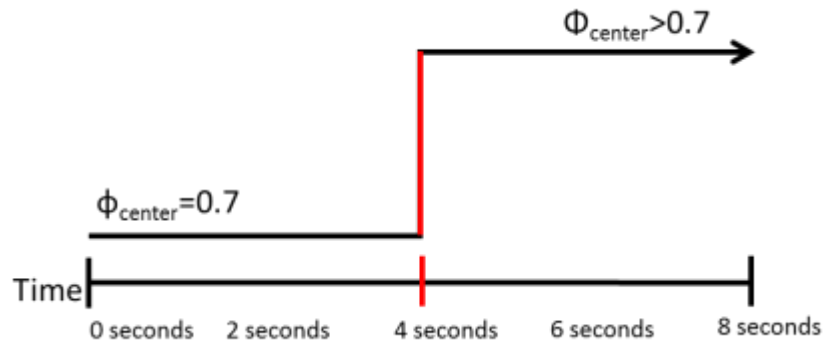
— Key findings to date

- Combustion instability can be suppressed using fuel staging in experimental facility, as it is in operational gas turbines
- Recent data may provide mechanism by which fuel staging suppresses instability; can be used as baseline for transient tests
- Transient instability growth and decay rates are different, likely driven by different processes in the combustor

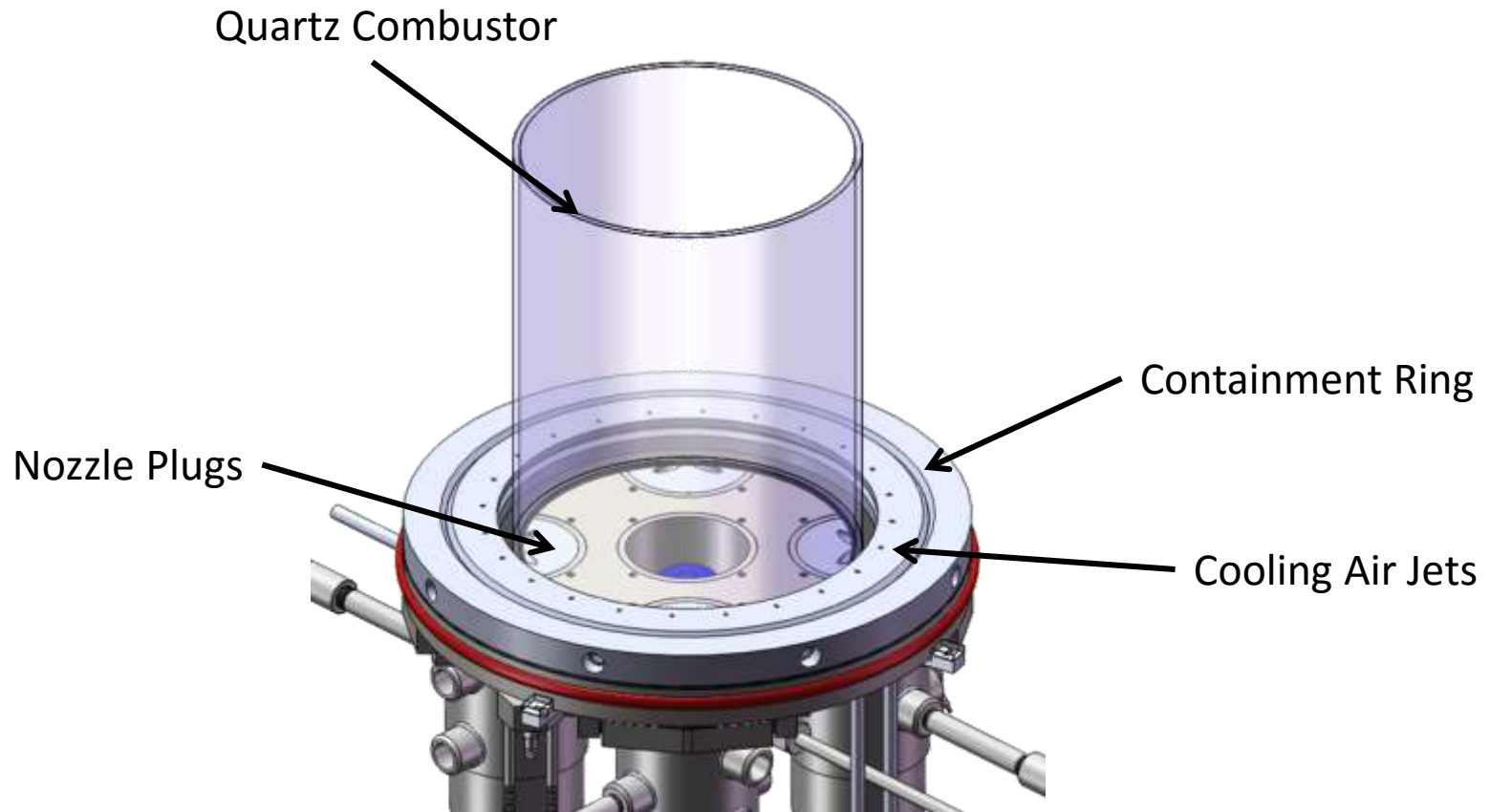
— Next steps

- Develop better models for capturing instability growth and decay processes → likely non-linear oscillators
- Transient testing at different fuel-staging time-scales
- Comparisons to single-nozzle operation

Different fuel-staging time-scales will be used to quantify the sensitivity of the combustor stability to transient timescale



Single-nozzle operation will be completed on the same rig with the same nozzles for direct comparison to current data



Acknowledgements

- **Penn State:** Dom Santavicca, Bryan Quay, Janith Samarasinghe, Wyatt Culler, Xiaoling Chen, Jackson Lee, Steve Peluso, Ankit Tyagi
- **GE Global Research:** Keith McManus, Tony Dean, Fei Han
- **DOE/NETL:** Mark Freeman
- College of Engineering Instrumentation Grant Program, Mechanical and Nuclear Engineering at Penn State

Questions?

Understanding Transient Combustion Phenomena in Low-NO_x Gas Turbines

Project DE-FE0025495, Oct. 2015 – Sept. 2018

Program Monitor: Mark Freeman

PI: Jacqueline O'Connor, Ph.D.

Co-PI: Dom Santavicca, Ph.D.

RE: Bryan Quay, Ph.D.

Graduate students: Janith Samarasinghe, Ph.D.,

Wyatt Culler, Xiaoling Chen

Undergraduates: Jackson Lee

Industry Partner: GE Global Research

Keith McManus, Tony Dean, Fei Han

Mechanical and Nuclear Engineering

Pennsylvania State University

sites.psu.edu/ccpp/

