



**THE OHIO STATE UNIVERSITY**

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**ADVANCED CONTROL ARCHITECTURE AND  
SENSOR INFORMATION DEVELOPMENT**

FOR PROCESS AUTOMATION, OPTIMIZATION, AND IMAGING  
OF CHEMICAL LOOPING SYSTEMS

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Department of Chemical and Biomolecular Engineering

Crosscutting Research Review Meeting | April 20<sup>th</sup>, 2016

# Project Team

## Government Agencies

- DOE/NETL: Jessica Mullen
- Ohio Development Service Agency: Gregory Payne

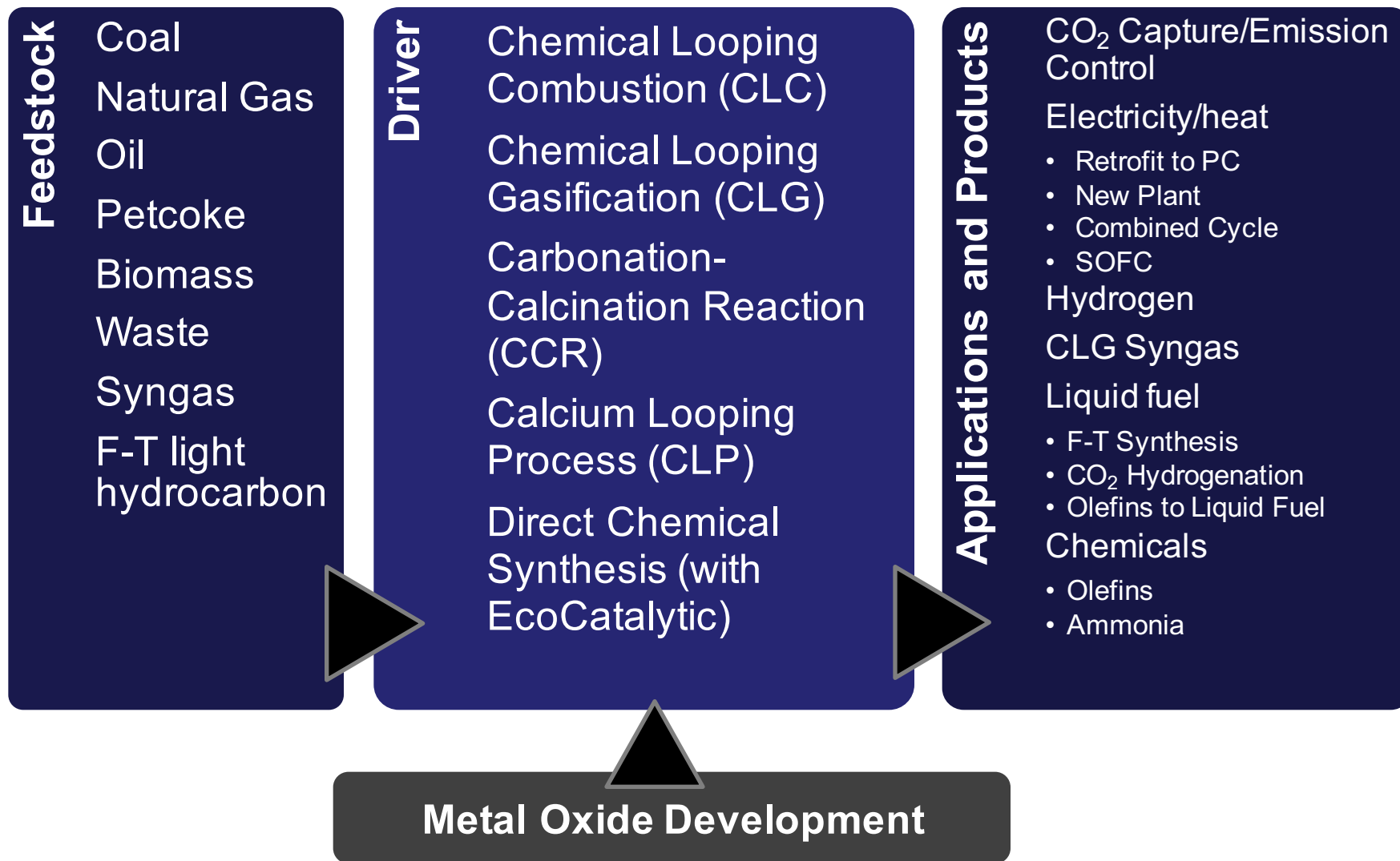
## Project Partners

- **Ohio State University:**  
Dr. Andrew Tong (PI, Dept. of Chemical & Biomolecular Engineering),  
Dr. Ümit Özgüner (co-PI, Dept. of Electrical and Computer Engineering)  
Dr. Arda Kurt (Dept. of Electrical and Computer Engineering)
- **Tech4Imaging:**  
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- **Babcock & Wilcox**  
Thomas Flynn, P.E.  
Timothy Fuller, P.E.  
Bijan Hosseininejad, P.E.

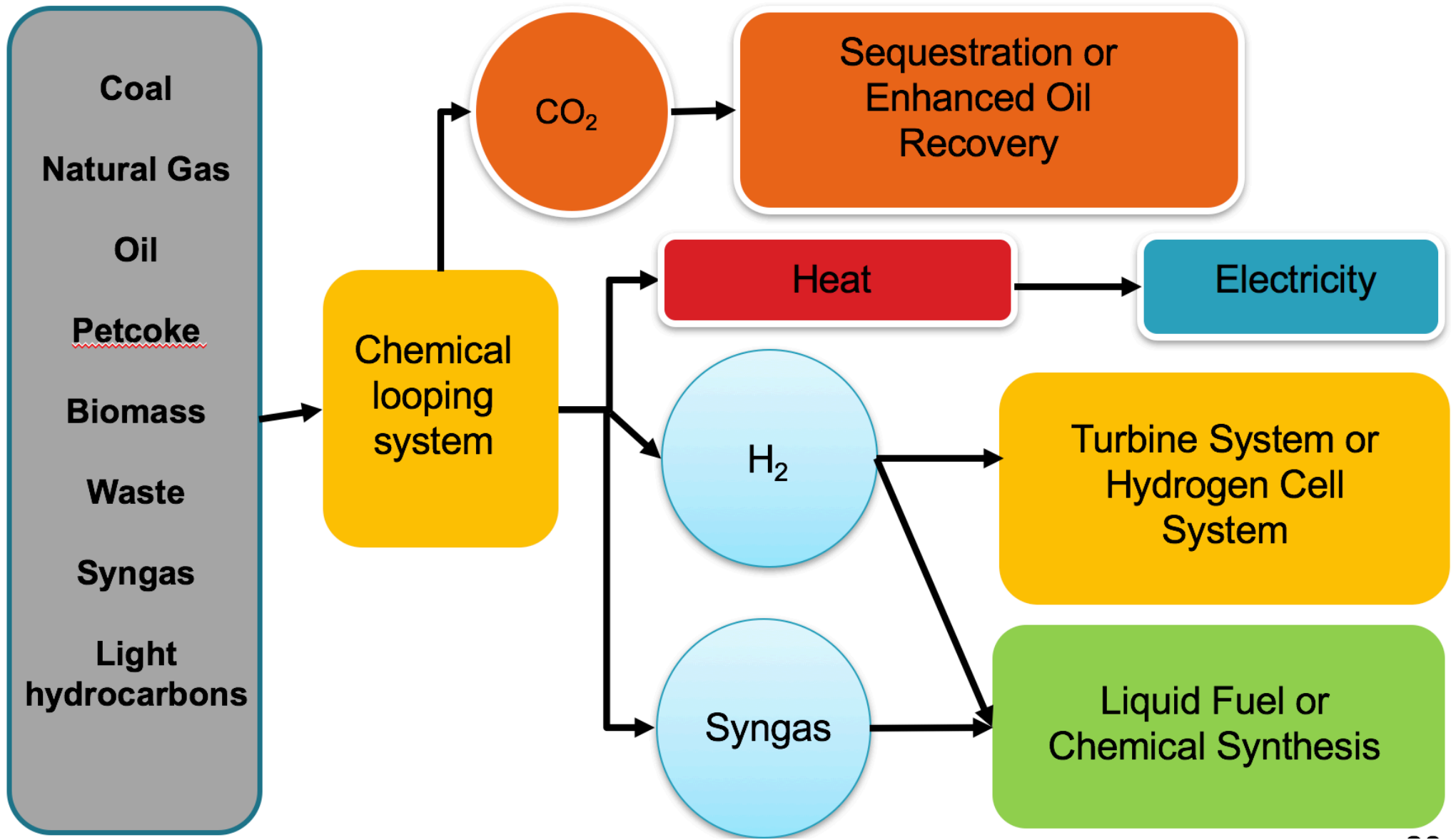




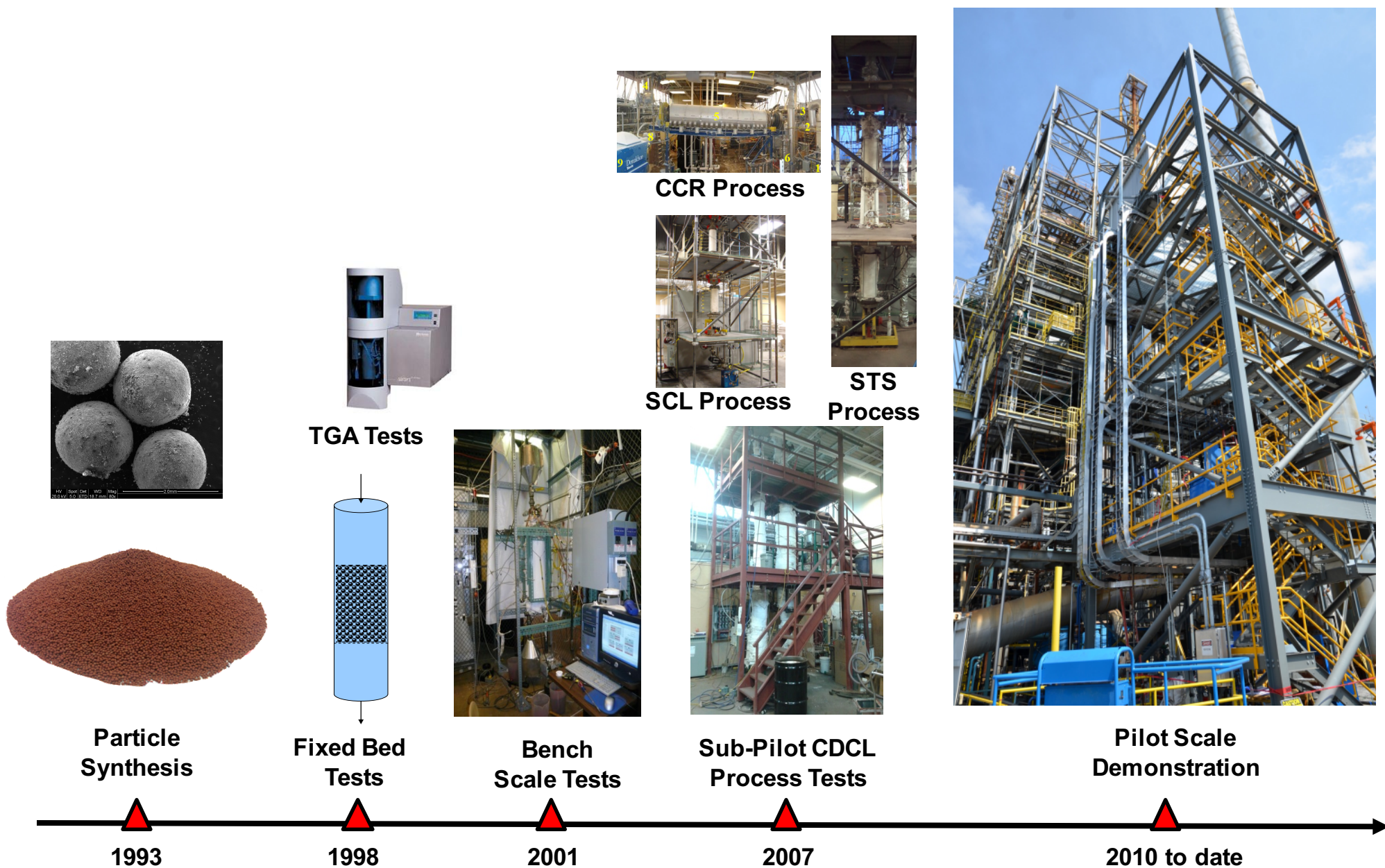
# OSU Chemical Looping Platform Technology



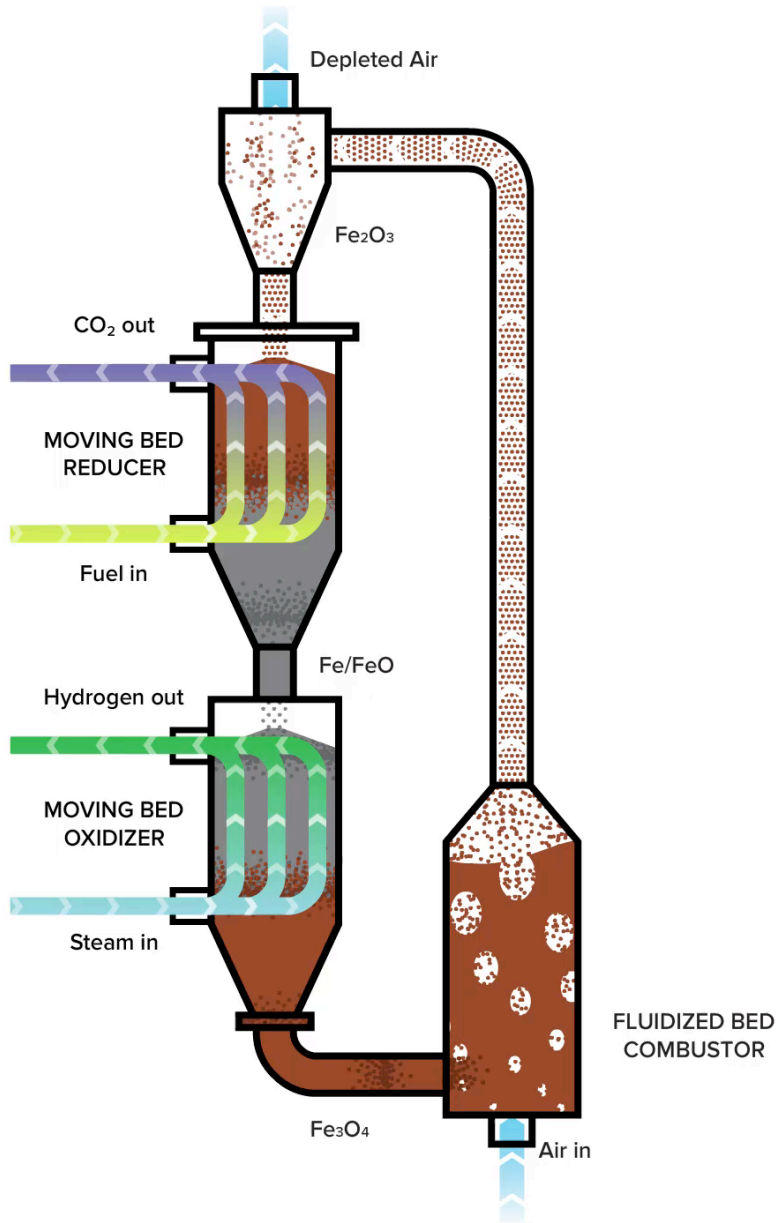
# OSU Chemical Looping Platform Technology



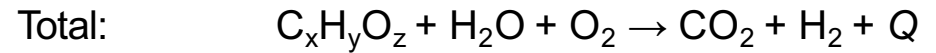
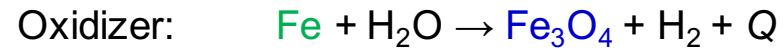
# Evolution of OSU Chemical Looping Technology



# OSU Syngas Chemical Looping Process



## Main reactions:



## Unique Reactor Design:

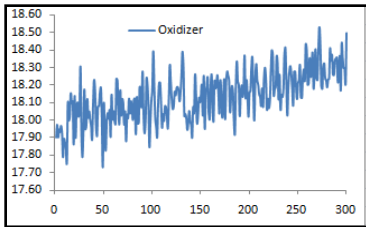
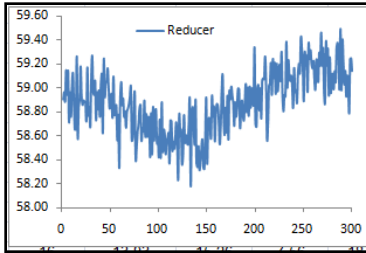
- High fuel conversion
- Near 100% in-situ CO<sub>2</sub> capture
- High purity H<sub>2</sub> generation
- High oxygen carrier conversion
- Low solid circulation rate





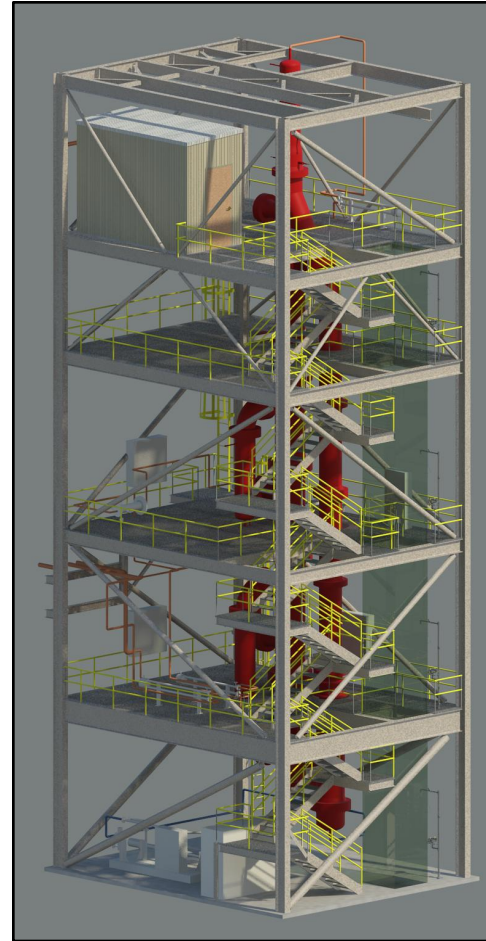
# SCL Pilot Plant Development

## 1:1 Cold Flow Model Testing



- Over 20 solids/gas flow operating conditions successfully tested
- System operation is robust
- >200 hrs continuous operation
- Non-mechanical system design successfully demonstrated
- Operational experience gained was used in developing the P&ID and operating procedures of SCL pilot scale unit at high temperature and pressure

## Pilot Plant Design



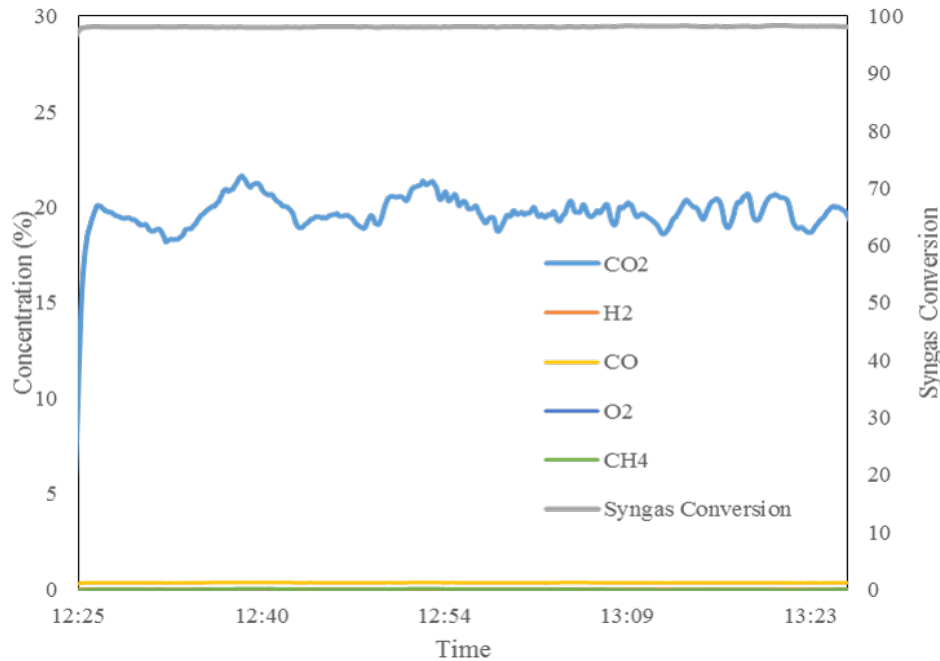
- 9 P&ID, mechanical and control specification documents
- Lab support studies
- Equipment and vessel fabrication drawings
- HAZOP Review

## Construction

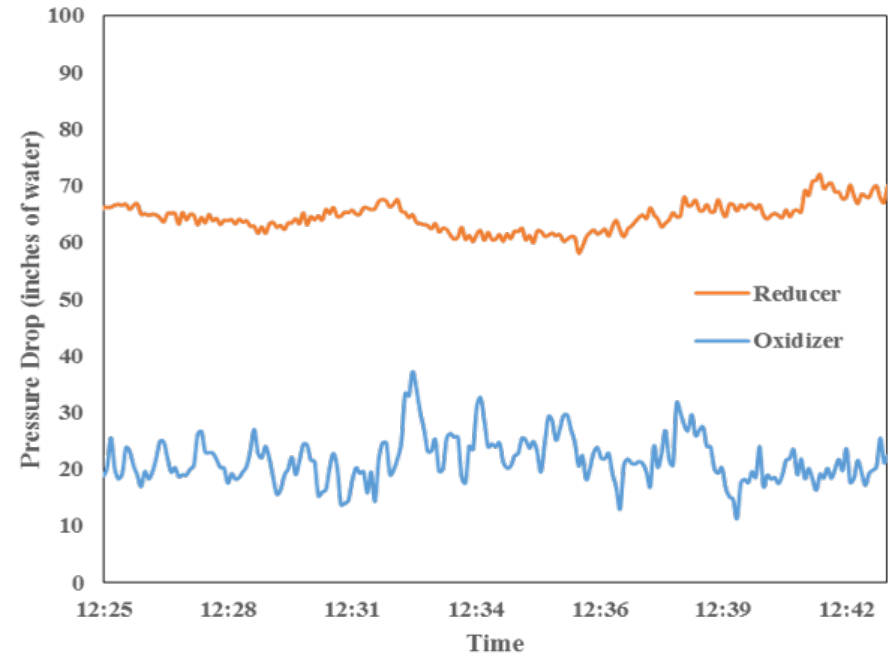


# April Operations: Syngas Injection

## Sample Reducer Composition and Conversion



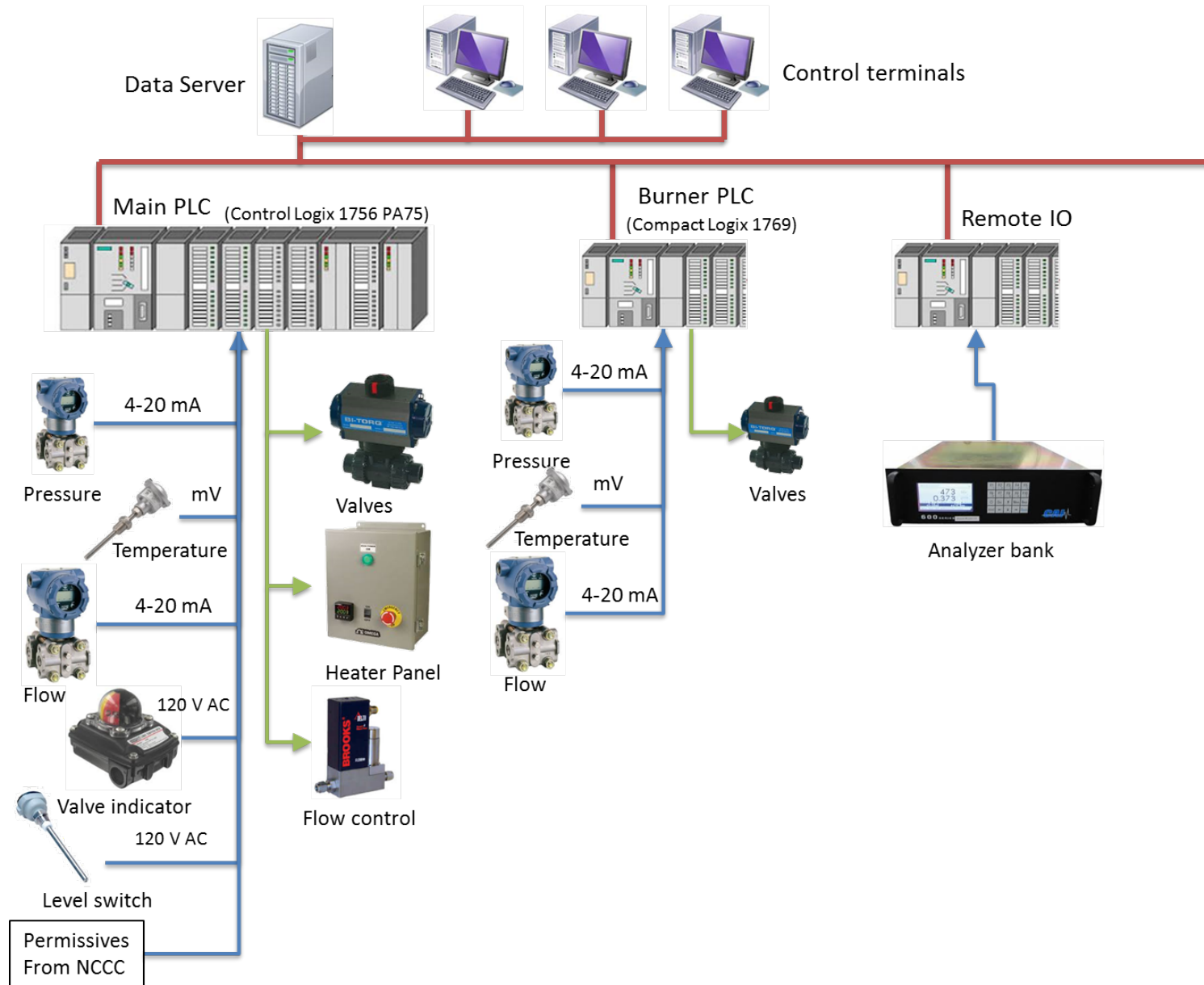
## Moving Bed Reactor Pressure Balance



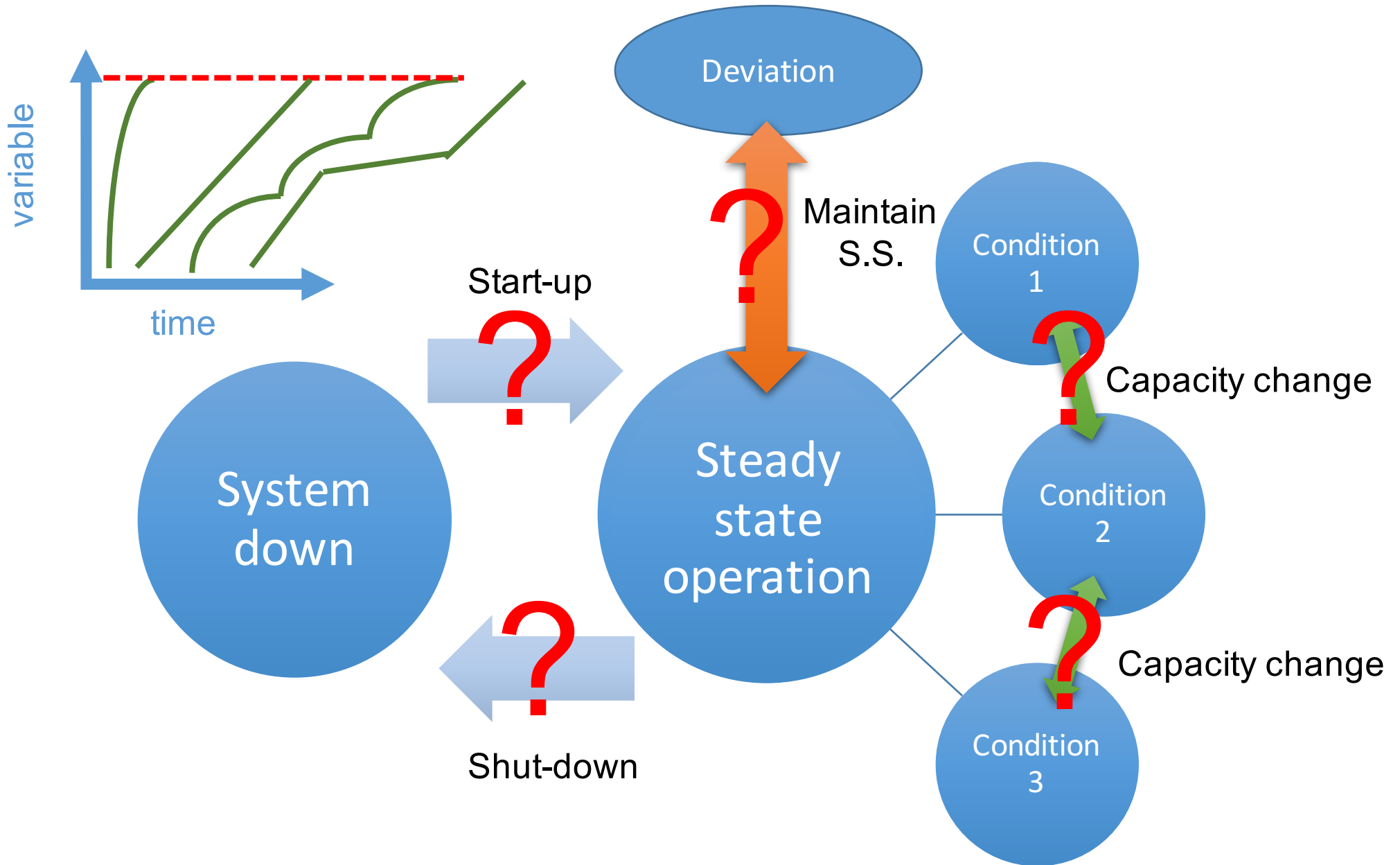
- Syngas operation initiated
  - 350 lb/hr syngas processed
- Achieved >98% syngas conversion
- Pressure balance and gas sealing maintained
- Elevated combustor temperatures confirm redox reactions
- Achieved first large-scale demonstration of high pressure, high temperature chemical looping process



# SCL Controls and Integration with DCS



# Transition between stages





# Start-up: What to watch?

## Pressurization

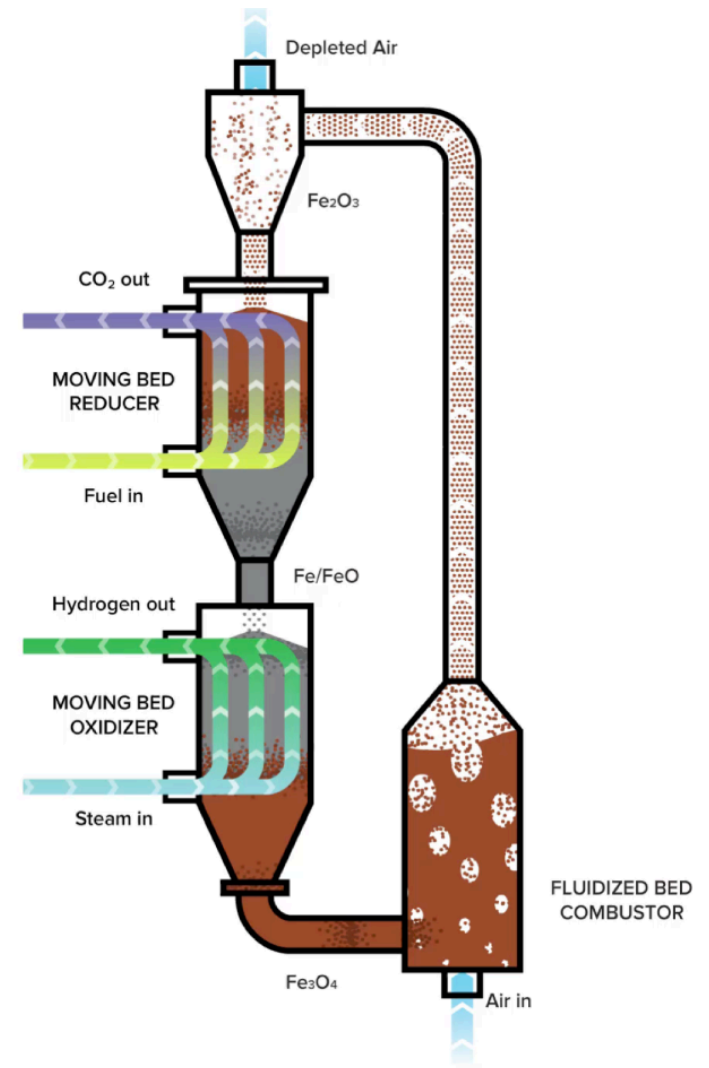
- Open combustor gas inlet/outlet to gradually pressurize, avoid local high pressure difference
- Achieve fluidization velocity in the combustor

## Initiate solid flow into the combustor

- Turn on aeration gas
- Observe pressure drop across the bed, watch for value increase and fluctuation
- Further open combustor gas inlet/outlet to achieve entrainment velocity while maintaining system pressure steady

## Confirm solid circulation established

- Watch for pressure drop spikes across riser
- Maintain fluctuation & positive value of pressure drop across the non-mechanical valve



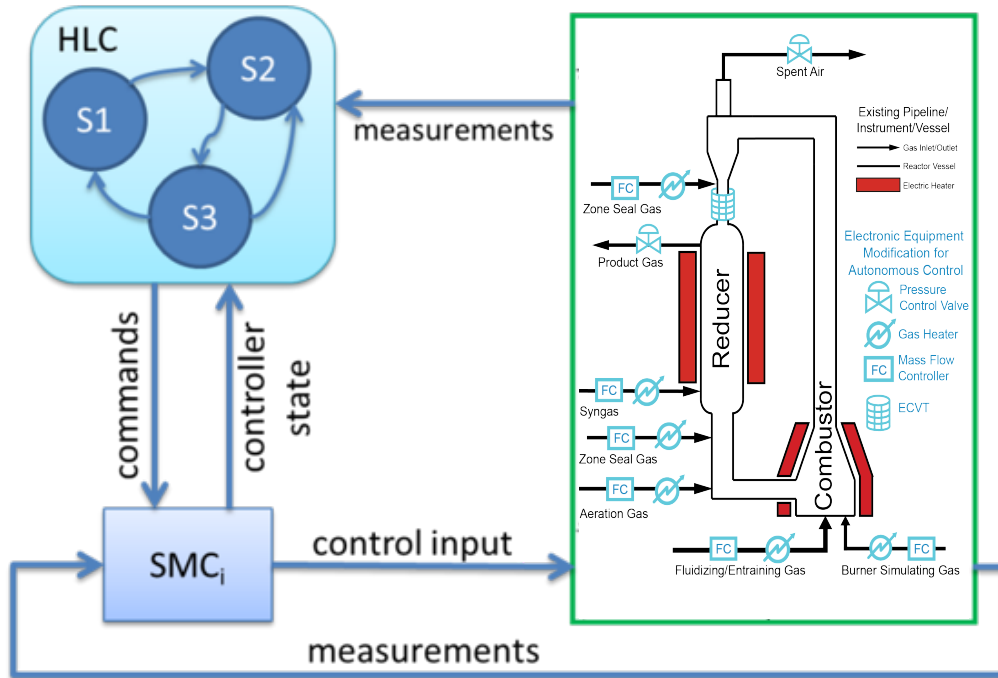
# Motivation

- Currently an open-loop system
- Highly sequential operation
- Experience- and knowledge-intensive
- Require operators' constant attention to watch for deviations
- Traditional controllers are not very effective
  - Tuned to specific operating condition
  - Not appropriate for multiple-in-multiple-out (MIMO) system
  - Lack robustness



# Summary of DE-FE0026334

## Autonomous Process Control Concept



## Sub-Pilot Unit



## Pilot Unit



- Objective: develop an advanced process automation control architecture and imaging and optimization sensor information for the OSU chemical looping process
  - Develop HLC-SMC control scheme for process automation (**OSU ECE**)
  - Establish sensor algorithm for high temperature ECVT (**Tech4Imaging/OSU CBE**)
  - Integrate process performance parameters with FocalPoint Optimization System (**B&W/OSU CBE**)
  - Prepare and test process control and optimization concepts in 25 kW<sub>th</sub> sub-pilot test unit (**OSU CBE**)

- OSU chemical looping technology: advanced solid and gaseous fuel conversion process for H<sub>2</sub> and electricity co-generation with in-situ CO<sub>2</sub> capture
- Phase I: test control concept in an integrated sub-pilot test unit at high temperature, reactive conditions
- Phase II: demonstrate control concept at commercially applicable pilot scale test unit at high temperature, high pressure, reactive conditions

## Project Team



**TECH**  
**4IMAGING**

**B&W**  
power generation group



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# Phase I Project Objectives

- Develop advanced controller, HLC-SMC, for autonomous control of chemical looping system
  - Also applicable to conventional CFB systems
- Develop high-temperature ECVT sensor and software for real-time solid flow rate measurement
- Apply FocalPoint for system performance optimization
  - Software developed by Babcock and Wilcox
  - Focus on optimizing (a) fuel/solid ratio and (b) sealing gas usage
- Demonstrate continuous operation on existing SCL sub-pilot and pilot units



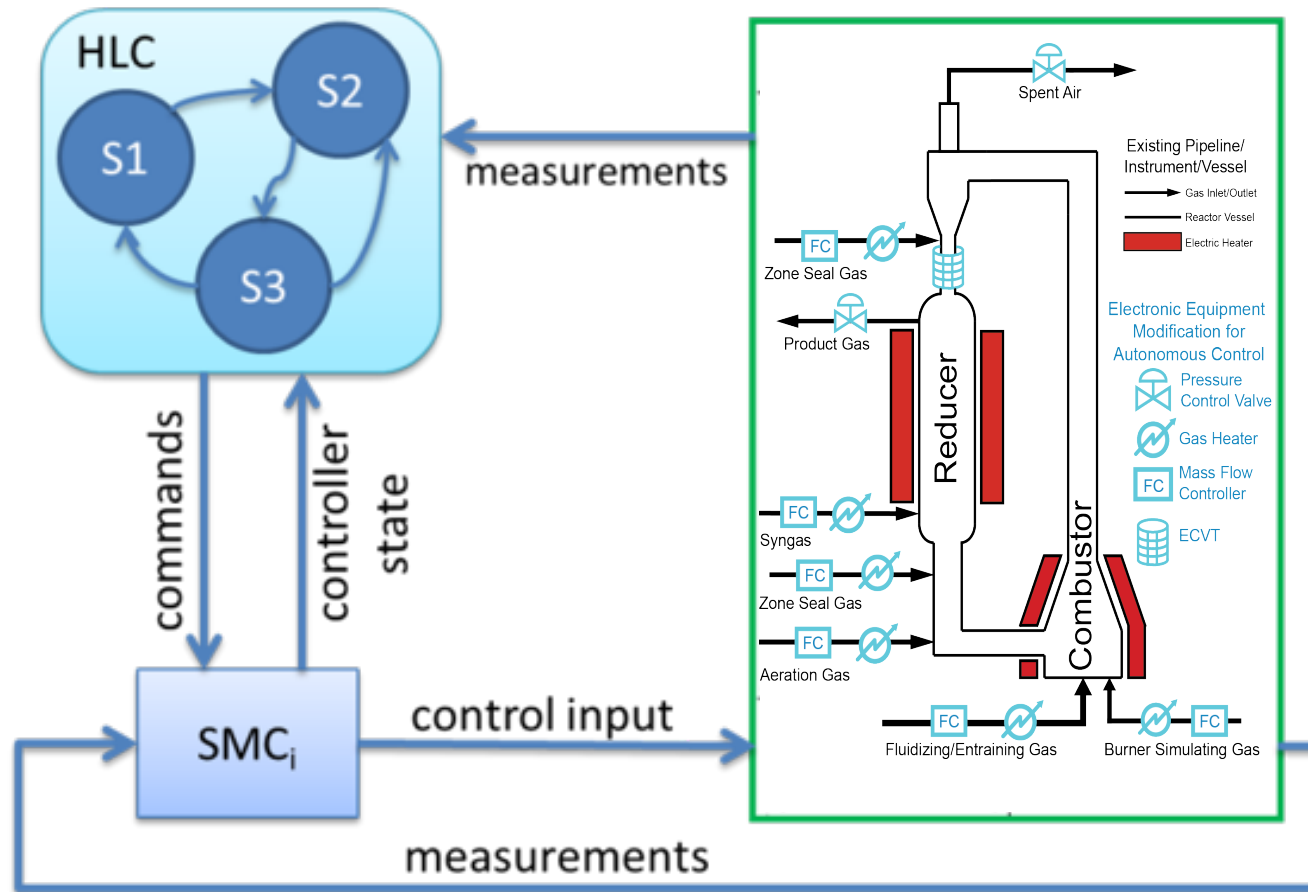
# Technical Approach – Tasks and Schedule

	Task	Start Date	End Date	Budget Period 1									Budget Period 2							
				10	11	12	1	2	3	4	5	6	7	8	9	10	11	12	1	2
<b>1.0</b>	<b>Project Management and Planning</b>	<b>10/1/15</b>	<b>3/31/17</b>																	
<b>2.0</b>	<b>Control Scheme Development for Process Automation</b>	<b>10/1/15</b>	<b>9/30/16</b>																	
2.1	Dynamic Process Model Development	10/1/15	3/31/16																	
2.2	HLC-SMC Control Algorithm Design and Realization	1/1/16	9/30/16																	
	<i>Milestone 1 - Complete HLC-SMC Algorithm Development</i>		<i>9/30/16</i>																	
<b>3.0</b>	<b>Visualization Software Development for High Temperature ECVT</b>	<b>10/1/15</b>	<b>12/31/16</b>																	
3.1	Software Development	10/1/15	9/30/16																	
3.2	Incorporate ECVT Sensor into Sub-Pilot Test Unit	4/1/16	12/31/16																	
	<i>Milestone 2 - Confirm Accurate Measurement of Solid Flow Rate at High Temperatures</i>		<i>12/31/16</i>																	
<b>4.0</b>	<b>Implementation of Process Optimization Software</b>	<b>10/1/15</b>	<b>9/30/16</b>																	
4.1	Performance Parameter Assessment and Programming	10/1/15	6/30/16																	
4.2	Software Interface Programming	7/1/16	9/30/16																	
	<i>Milestone 3 - FocalPoint Programming Completed</i>		<i>6/30/16</i>																	
<b>5.0</b>	<b>Chemical Looping Testing Unit Preparation and Testing</b>	<b>10/1/15</b>	<b>3/31/17</b>																	
5.1	Design, Procure, and Install Controller-Compatible Mechanical Components	10/1/15	6/30/16																	
5.2	Design, Construction, Programming of the Distributed Control System	1/1/16	9/30/16																	
5.3	Integration of HLC-SMC to the DCS	7/1/16	12/31/16																	
5.4	Commissioning and Testing of the Sub-Pilot Test Unit	10/1/16	3/31/17																	
	<i>Milestone 4 - Mechanical Components Selected and Procurement Initiated</i>		<i>12/31/15</i>																	
	<i>Milestone 5 - DCS Design Complete and Construction Commenced</i>		<i>3/31/16</i>																	
	<i>Milestone 6 - Demonstrate Complete Automated Chemical Looping Operation</i>		<i>3/31/17</i>																	



# Technical Approach – Task 2

Develop advanced hybrid controller, HLC-SMC, for autonomous control of chemical looping system





## TWO SIDES OF THE CONTROL AND AUTOMATION WORK

### State regulation

- Continuous states are to be controlled:
  - Temperature
  - Pressure
- Not only around setpoints
- Transitions are to be regulated
- Model uncertainties are expected
- Sliding Mode Control is chosen

### Operational Automation

- Current plant operation is manually controlled
- Operator skill is a major factor
- Discrete events will be defined:
  - Transition from one step to the next in the operational sequence
  - React to continuous-state changes based on thresholds
- The combined continuous/discrete setup will form a Hybrid State System



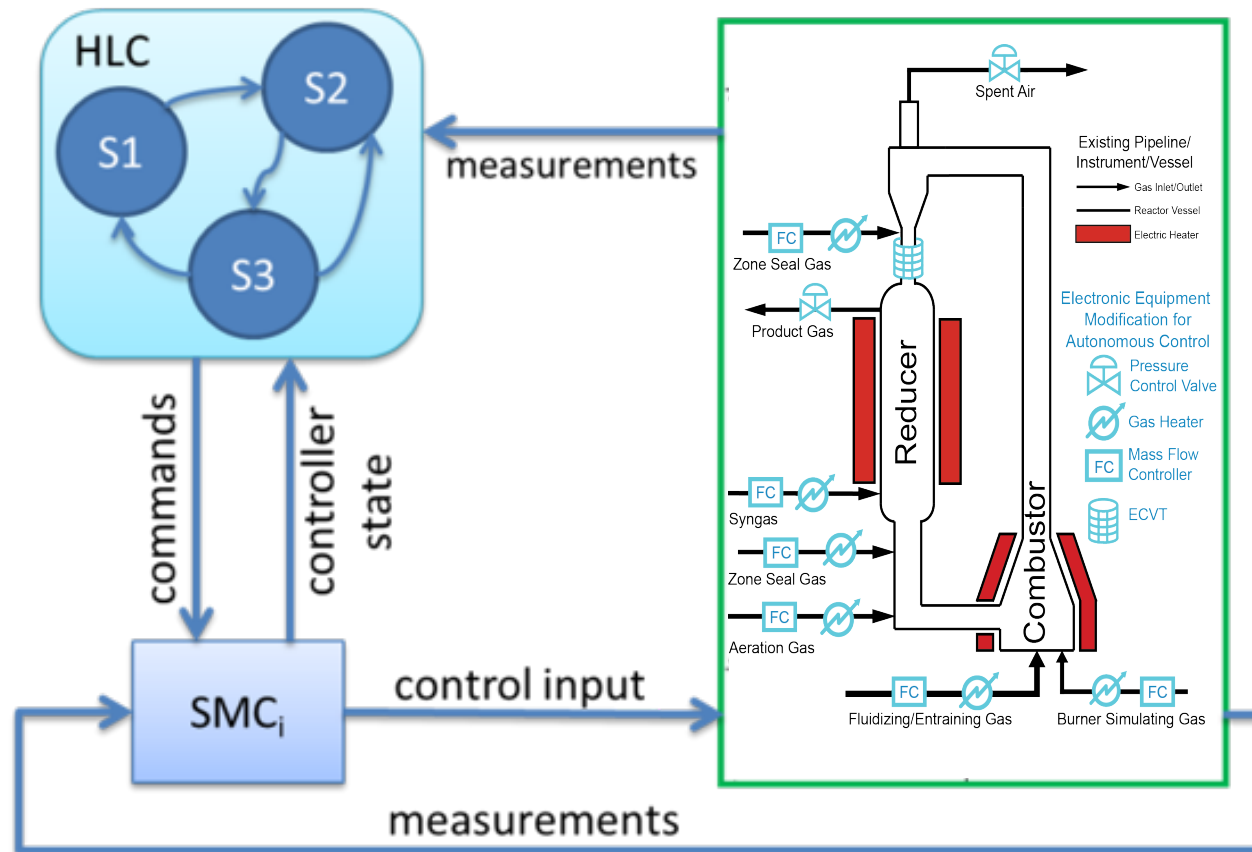


- Conventional Controllers:
  - PID
  - Smith Predictors
  - Lead-Lag Controllers
- Not robust/versatile enough
- Highly affected by modeling uncertainties
- Designed to control the system around a sequence of waypoints
  - No explicitly designed transient behavior
- Alternative:
  - Sliding Mode Control

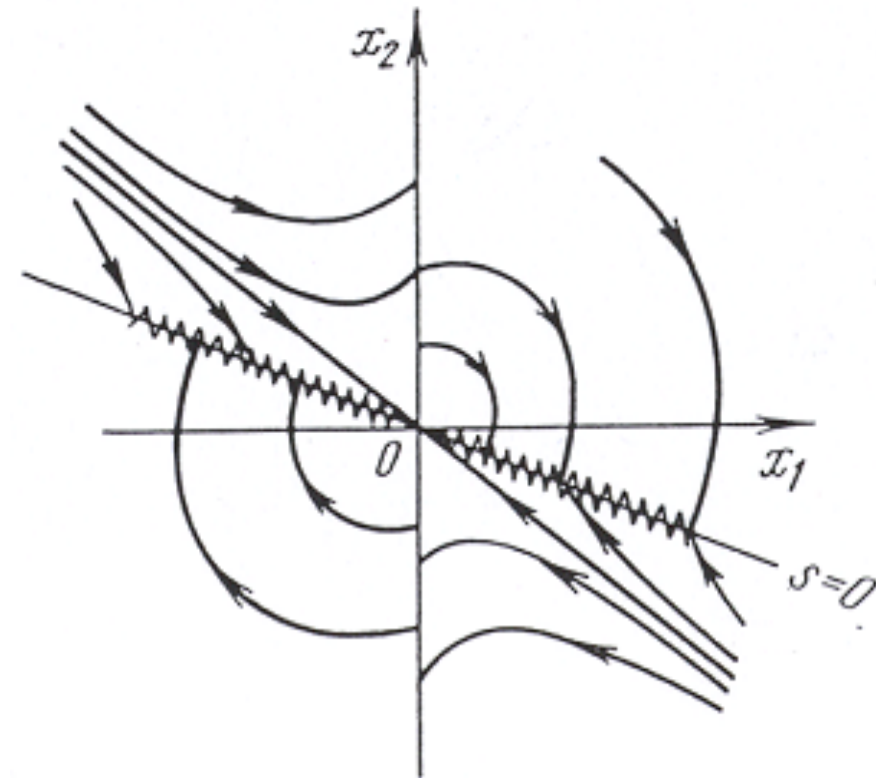




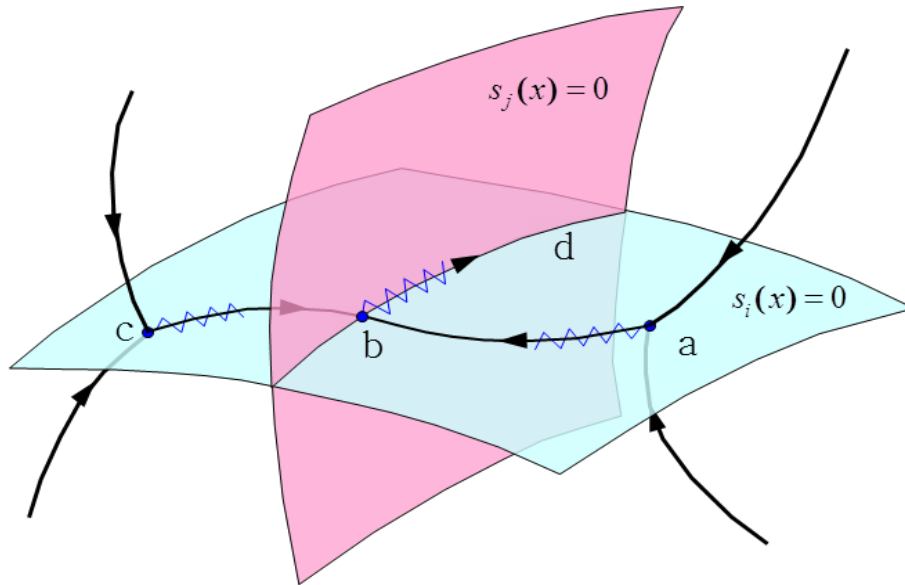
- High-level controller (HLC) observes the system and switches SMCs (controllers/surfaces) as desired setpoints are reached.



- Control where the system states will converge, and restrict the trajectory to get there
- Find/define a surface that the states can slide to its desired value
- Derived from Variable Structure Control [Utkin1977]
- Controller changes behavior as the state trajectory crosses the surface
- Two stages:
  - Reaching mode: to get to the sliding surface
  - Sliding mode: reduced order motion on the surface
  - The discontinuity of the controller is responsible for reaching



Utkin, V., "Variable structure systems with sliding modes," *Automatic Control, IEEE Transactions on* , vol.22, no.2, pp.212,222, Apr 1977



- Use multiple surfaces in multiple dimensions
- Along a series of setpoints
- Surfaces/controllers switch once certain points are reached
- Transient between setpoints governed by the sliding surfaces

- Two possible SMC extensions are being considered right now:
  - Second order SMC
  - Extremum-seeking SMC
- Depending on the simulation results with the models that are being built, we might consider other specific SMC implementations or go back to the traditional first order SMC if that gives adequate control performance

- The system is given  $\dot{x}_2 = f(t, x_1, x_2) + g(t, x_1, x_2)u$
- The control is defined  $u = u(x_1, x_2)$  with a bounded disturbance  $f(x_1, x_2, t)$

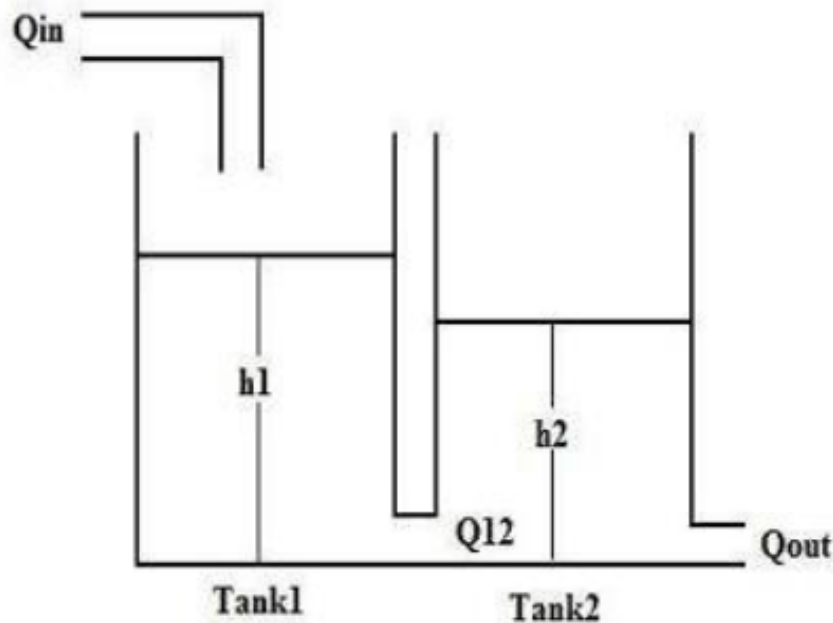
- Proposed SOSMC is

$$u = -\rho_1 |\sqrt{\sigma}| \text{sign}(\sigma) - \rho_2 |\sqrt{-2\lambda x_1 + \sigma}| \text{sign}(-2\lambda x_1 + \sigma)$$

- In SMC, the aim is to force the state or error to move on the switching surface  $\sigma(t)$ , so  $\sigma = \lambda e(t) + \dot{e}(t)$ , where

$$e = x_1 - x_{desired}, \lambda > 0$$

# Level Control of Two-Tank System

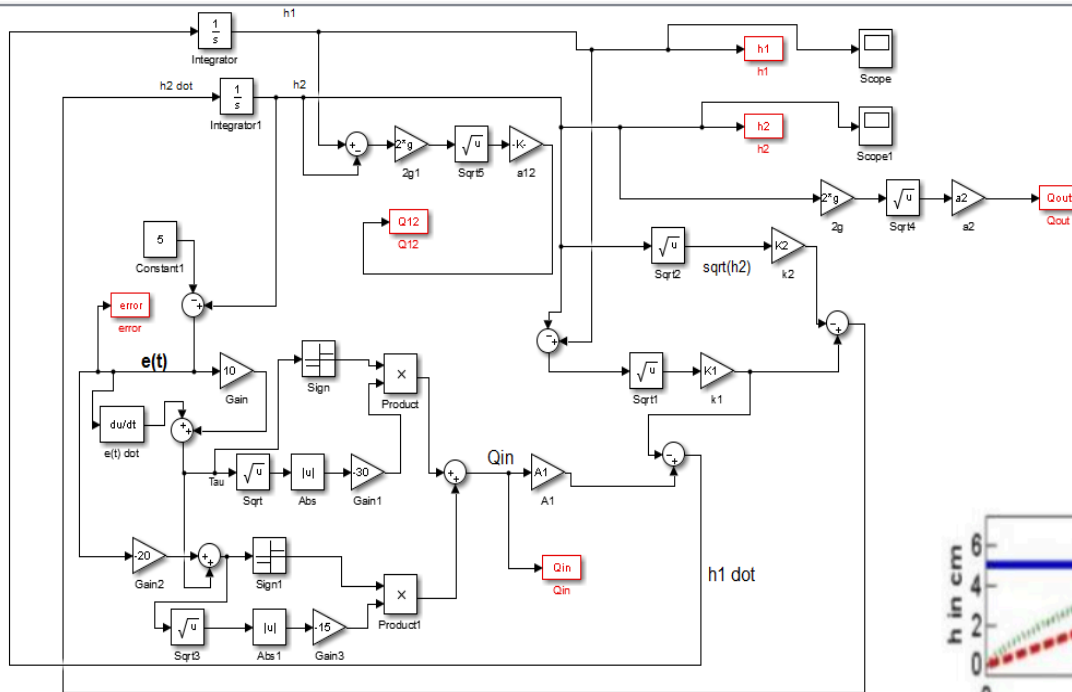


$$\frac{dh_1}{dt} = \frac{Q_{in}}{A} - k_1 \sqrt{h_1 - h_2}$$

$$\frac{dh_2}{dt} = k_1 \sqrt{h_1 - h_2} - k_2 \sqrt{h_2}$$

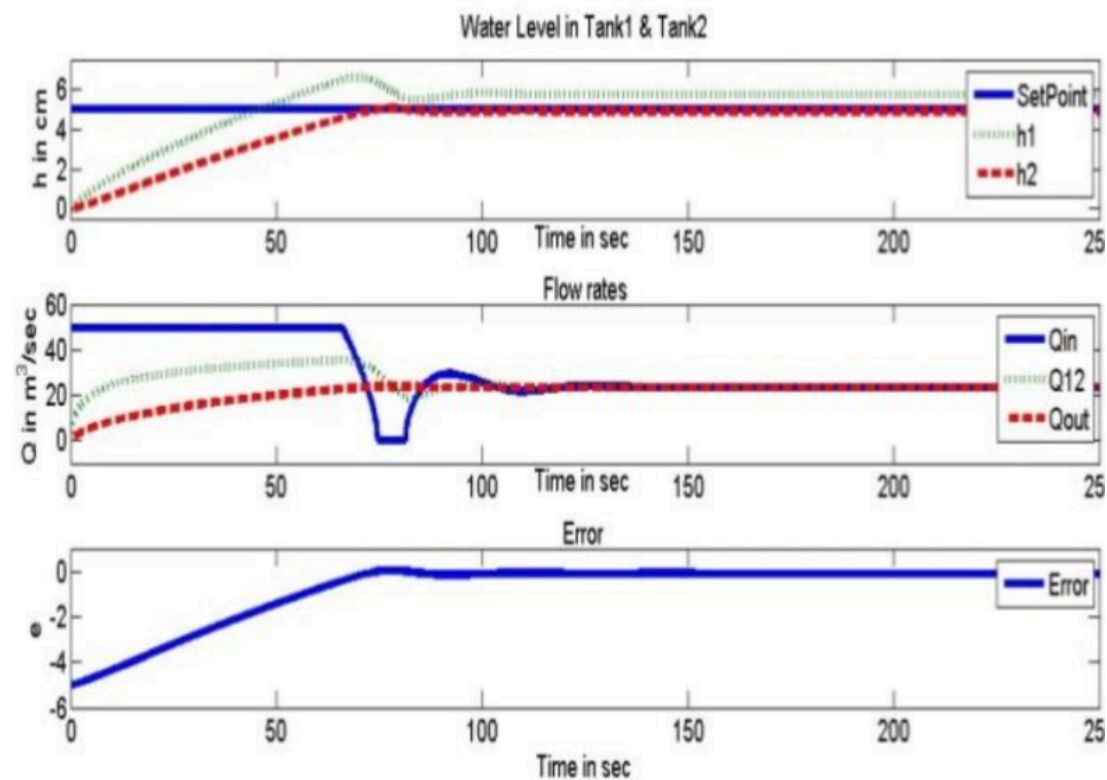
$$u = -30 \sqrt{|\sigma|} \text{sign}(\sigma) - 15 |-2\lambda e + \sigma| \text{sign}(-2\lambda e + \sigma) \quad \sigma = \lambda e(t) + \dot{e}(t) \quad \lambda = 10$$

Proposed SOSMC is applied to,  $Q_{in}=u$ ,  $e(t)=h_2(t)-h_{2\_desired}=h_2-5$



Simulink model

Simulation results





- Extremum Seeking Control (ESC) deals with the problem of tracking an optimum operating point for a system with unknown performance function.
- Extremum Seeking control via sliding mode (ESC-SM) approach introduced in the context of static optimization by Korovin and Utkin and generalized, analyzed and applied by Ozguner and his co-authors.
- Applications: ABS (Automotive), PID tuning, Photovoltaic systems,...etc.
- In chemical systems, it was introduced, in the context of **Bioreactor** optimization in [Wang99]. Further development was introduced later with the application to general **batch reactor** [Titica2003] ,**continues stirred tank reactors** [Guay2004], and **tubular reactors** [Cougnon2006] and with consideration of **multivalued cost function** [Bastin2009].

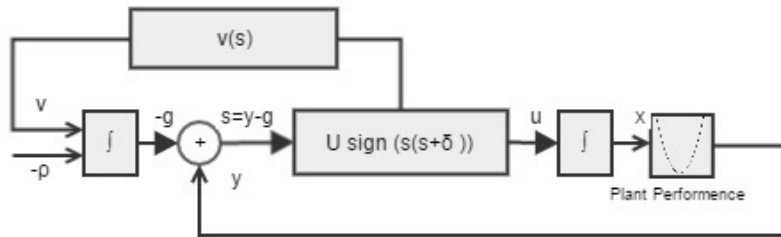


Figure.1 Block Diagram [1]

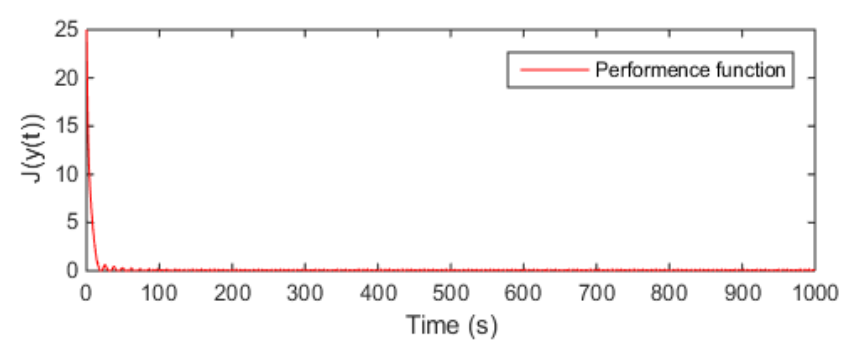
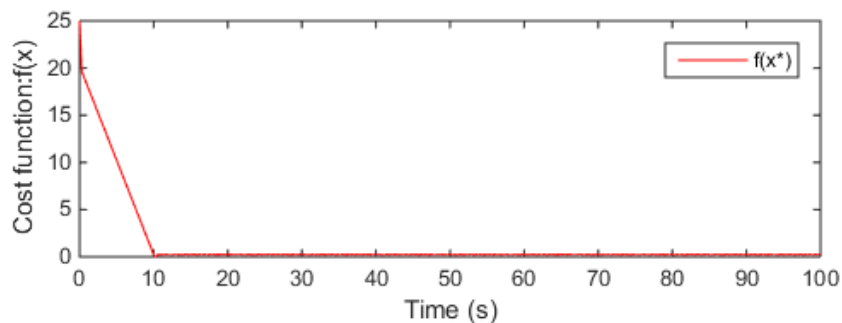
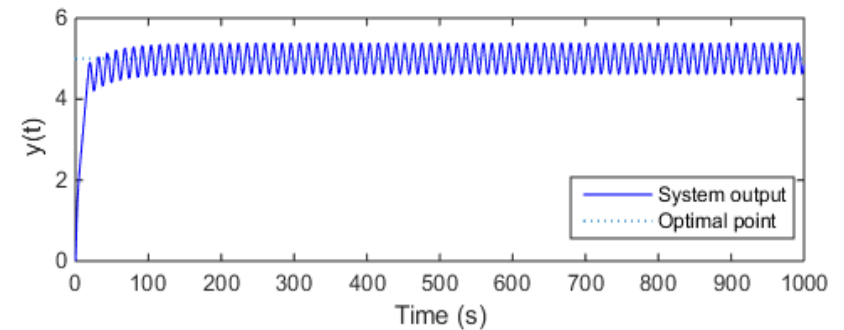
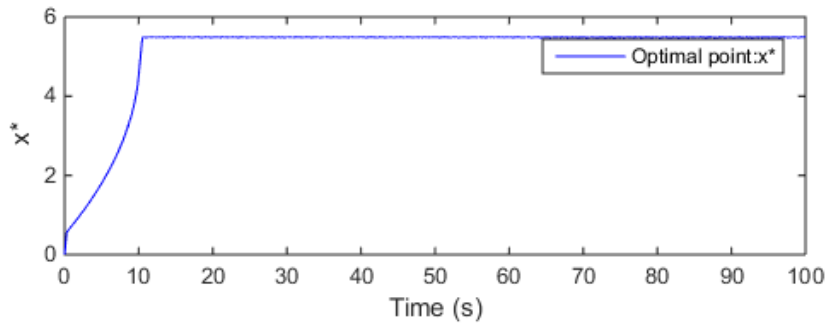
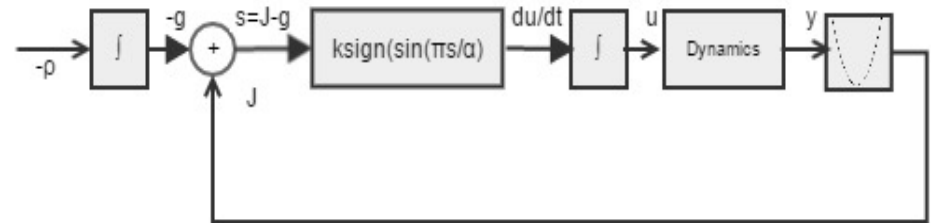


Figure.2 Simulation Results

Figure.2 Simulation Results





- Utkin, V., "Variable structure systems with sliding modes," *Automatic Control, IEEE Transactions on* , vol.22, no.2, pp.212,222, Apr 1977.
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- Drakunov, S.V., Özgüner, Ü, Dix, P., Ashrafi, B.: ABS control using optimum search via sliding modes. *IEEE Transactions on Control Systems Technology* (3), 79–85 (1995)
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- Guay, M., Dochain, D., Perrier, M.: Adaptive extremum seeking control of continuous stirred tank bioreactors with unknown growth kinetics. *Automatica* 40(5), 881–888 (2004)
- Cougnon, P., Dochain, D., Guay, M., Perrier, M.: Real-time optimization of a tubular reactor with distributed feed. *AIChE J.* 52(6), 2120–2128 (2006)
- Bastin, G., Nešić, D., Tan, Y., Mareels, I.: On extremum seeking in bioprocesses with multivalued cost functions. *Biotechnol. Prog.* 25(3), 683–689 (2009)



- In order to build a simulation model of the plant to apply SMC
  - Using the basic dynamics of each main component in the sub-pilot and pilot units
  - System equations are being modeled in Matlab/Simulink
  - Data collected from the real units are used where available
- The hybrid controllers that are being designed and tested using these models/simulations will form the basis of the sub-pilot and pilot controllers



# Technical Approach – Model Equations

- Ergun Equation

$$DP_{360} = \frac{150\mu_{N_2}L_{361}(1-\epsilon)^2}{d_p^2 \epsilon^3} u_{361} + \frac{1.75\rho_{360}L_{361}(1-\epsilon)}{d_p \epsilon^3} u_{361}|u_{361}|$$

- Valve Equation

$$\left\{ \begin{array}{l} F_{590} = 3.455 \times 10^{-5} \left( \text{mol} \cdot \text{s}^{-1} \cdot Tg_{490}^{\frac{1}{2}} \cdot Pa^{-1} \right) \times C_v \cdot x_{490} \cdot \sqrt{\frac{P_{490}^2 - P_0^2}{Tg_{491}S_g}} \text{ when } \frac{P_{490}}{P_0} < 1.89 \\ F_{590} = 2.934 \times 10^{-5} \left( \text{mol} \cdot \text{s}^{-1} \cdot Tg_{490}^{\frac{1}{2}} \cdot Pa^{-1} \right) \times C_v \cdot x_{490} \cdot P_{490} \sqrt{\frac{1}{Tg_{491}S_g}} \text{ when } \frac{P_{490}}{P_0} > 1.89 \end{array} \right.$$

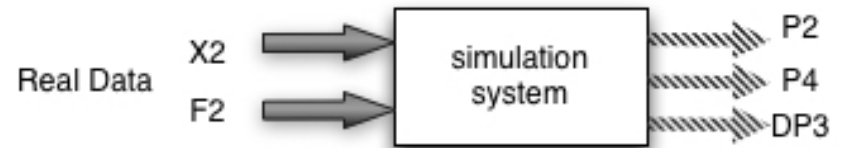
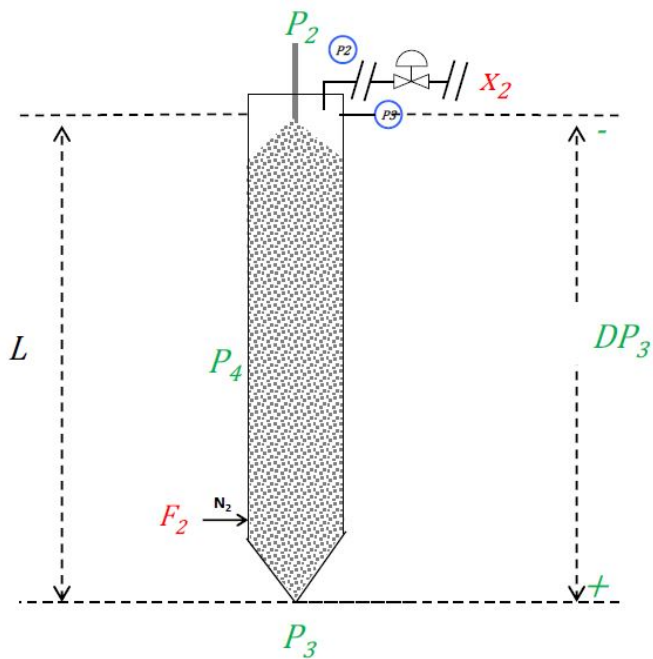
- Gas Mass Balance

$$\frac{dP_O}{dt} = \frac{R \cdot Tg_{490} \cdot (F_{420} + F_{371} + F_{362} - F_{490})}{V} + \frac{P_O}{Tg_{490}} \cdot \frac{dTg_{490}}{dt}$$

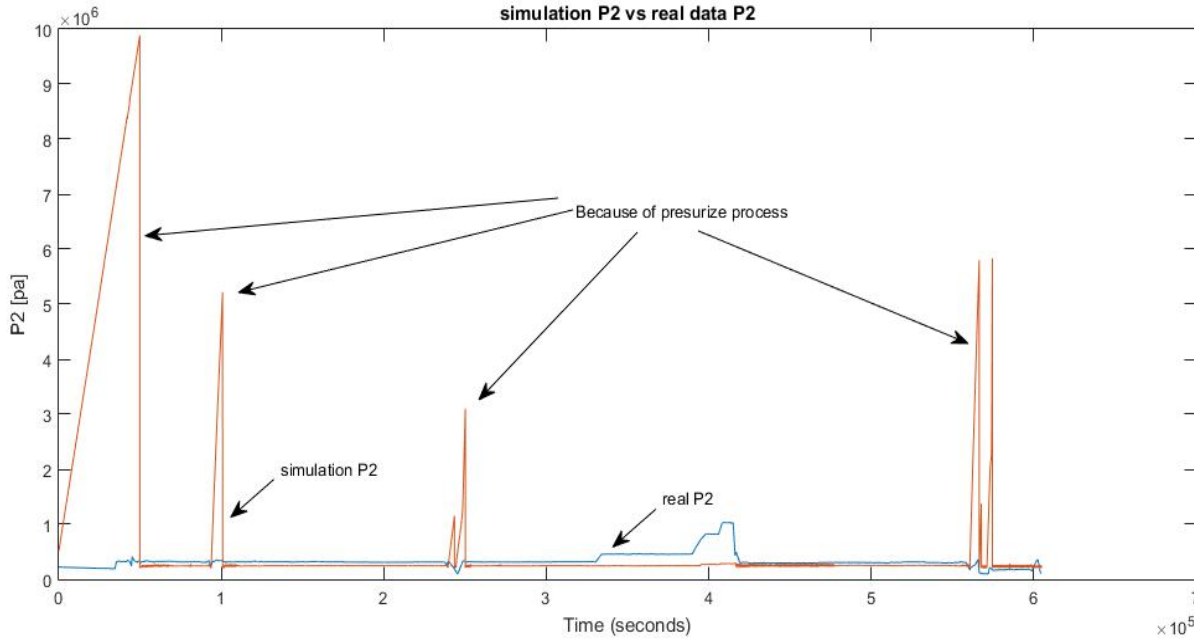
- Fludized Bed/Riser Correlation



# One tank system modeling & validation

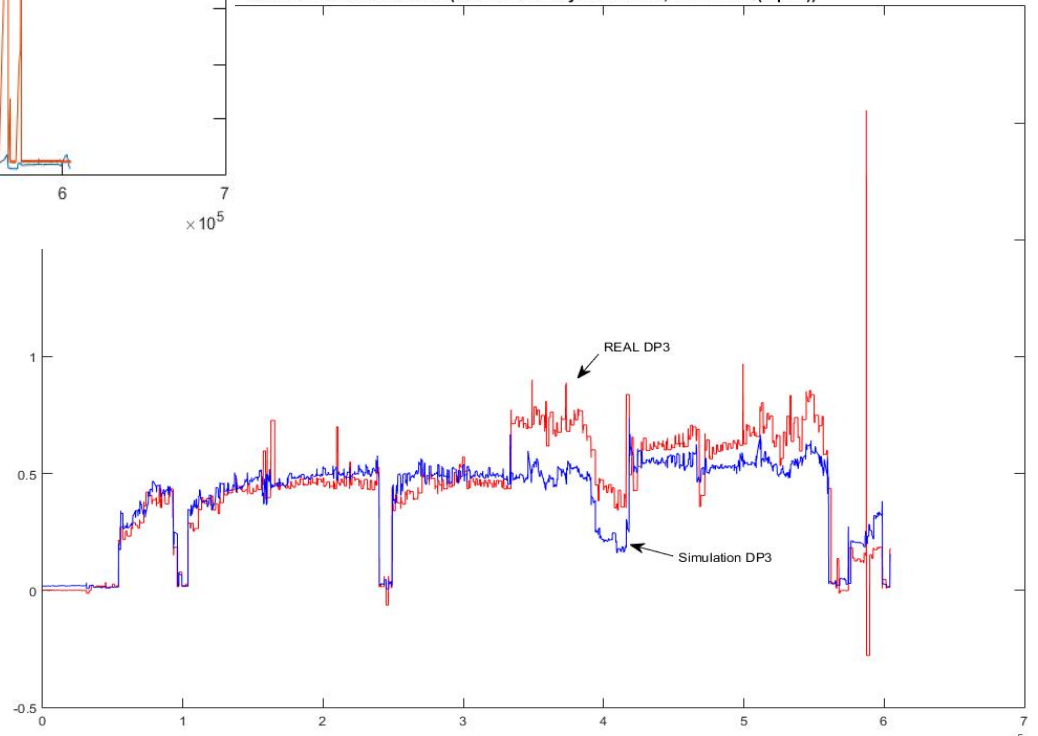


- **Test input (experimental data):**
- X2(valve 2), F2(air flow 2)
- **Test output(simulation outcome):**
- P2, P4, DP3



## Simulation P2 vs real P2

take F0 into consideration (due to F0 is way more small,  $V_s = F_0^2 \cdot R \cdot T / (2 \cdot p \cdot P_4)$ )



## Simulation DP3 vs real DP3

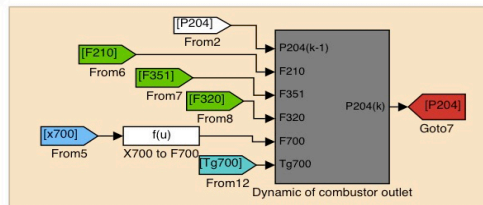


# SIMULATION METHOD 1 - SIMULINK

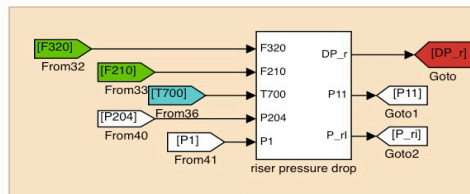
## THREE TANK SYSTEM MODEL



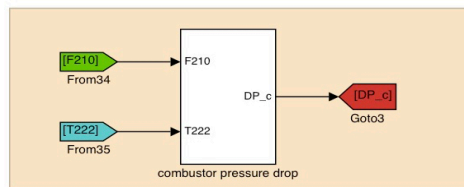
Green : airflow input  
Light blue: valve open percentage  
Cyan: temperature  
Red: main states



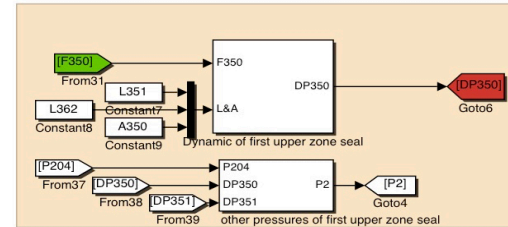
combustor outlet



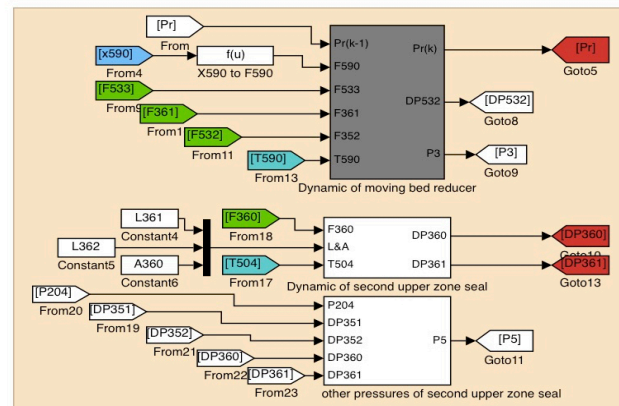
riser



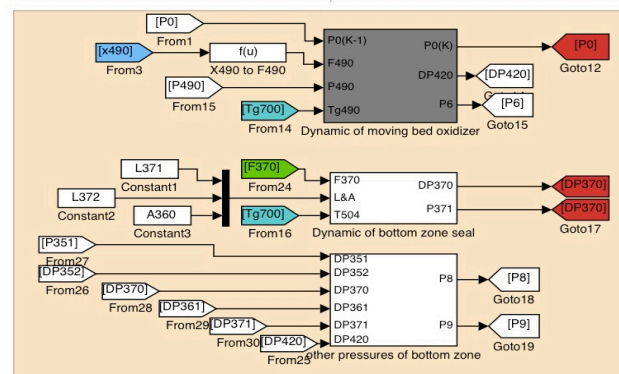
combustor



first tank



second tank



third tank

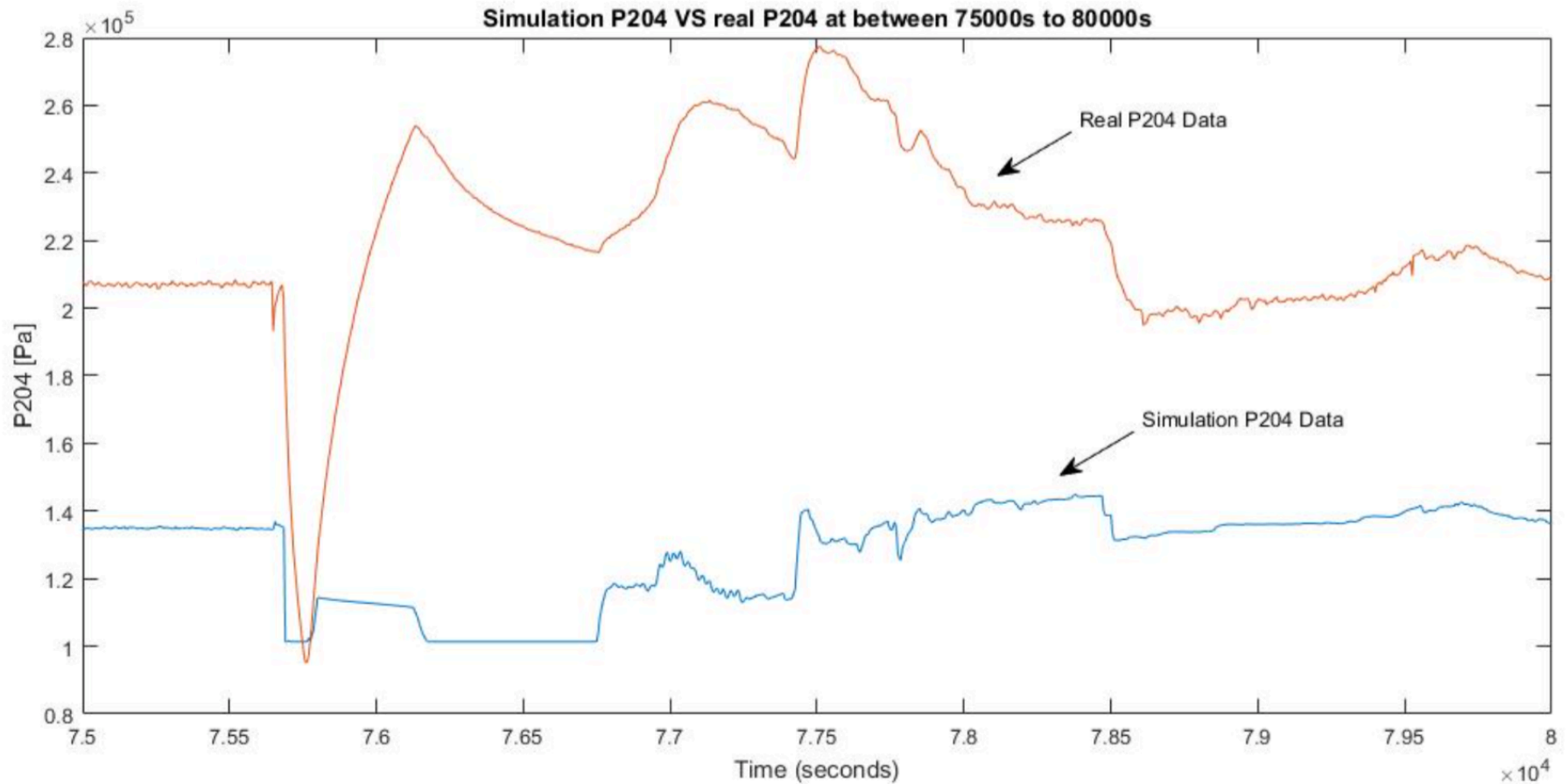


# SIMULATION METHOD 1 – SIMULINK

## SAMPLE RESULT



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CENTER FOR AUTOMOTIVE RESEARCH





# Simulation Method 2 - Matlab

SCL

Start / Continue

Stop and save

Reset

PCV700 opening 22.8 %

FE700 1700.8

DP350 0.85

TE350 70

DP351 -6.76

PE350 30.04

FE350 0

PE204 30.01

RED500

PE590 30.25

PCV590 opening 24 %

TE593 0

FE590 505.92

DP532 32.56

PE550 30.84

TE531 70

PE530 31.43

FE533 500

DP360 1.74

PE360 31.49

TE360 70

DP203 100.28

DP361 -12.89

OXI400

PE490 31.89

PCV490 opening 19 %

TE493 0

FE490 415.14

Ug\_Riser 6.50

Ut\_Riser 5.39

DP420 13.71

PE450 32.14

TE420 70

PE420 32.39

FE420 400

Ug\_Combustor 1.04

Umf 0.45

DP370 22.55

PE370 33.20

TE370 70

DP371 -42.39

PE320 33.92

FE361 0

FE320 70

COM200

PE203 33.63

TE222 0

Solid Holdup 207.99

TE210 70

FE210 1650

DP372 8.03

Time 6351 s

Acceler 1

Mass Flow 1760.8



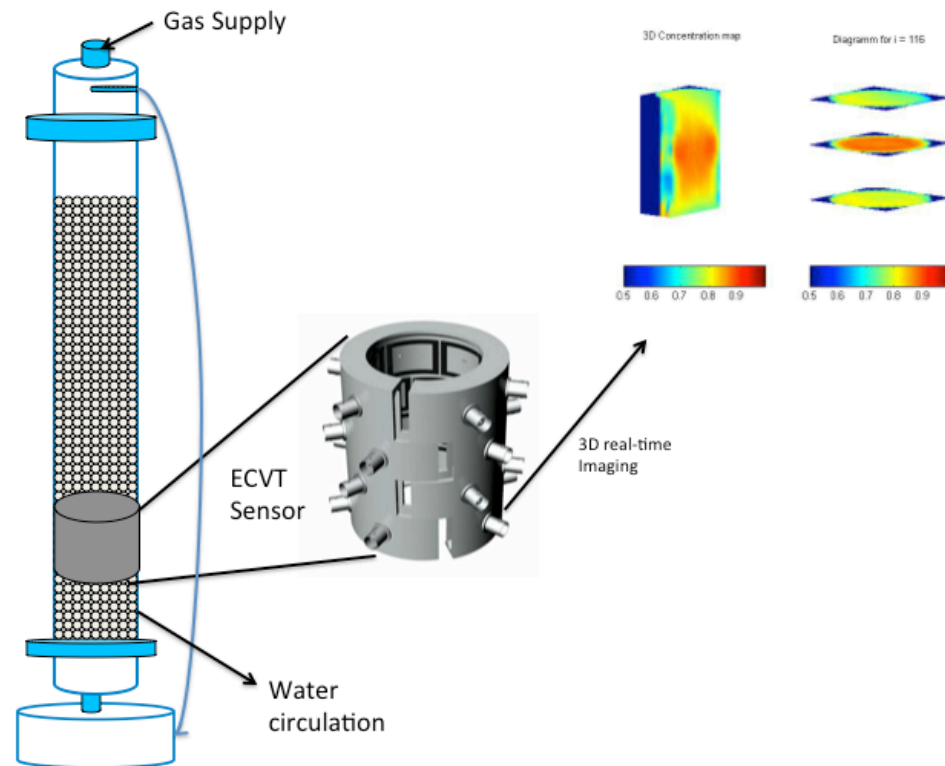
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	<i>Milestone 6 - Demonstrate Complete Automated Chemical Looping Operation</i>		<i>3/31/17</i>																	♦



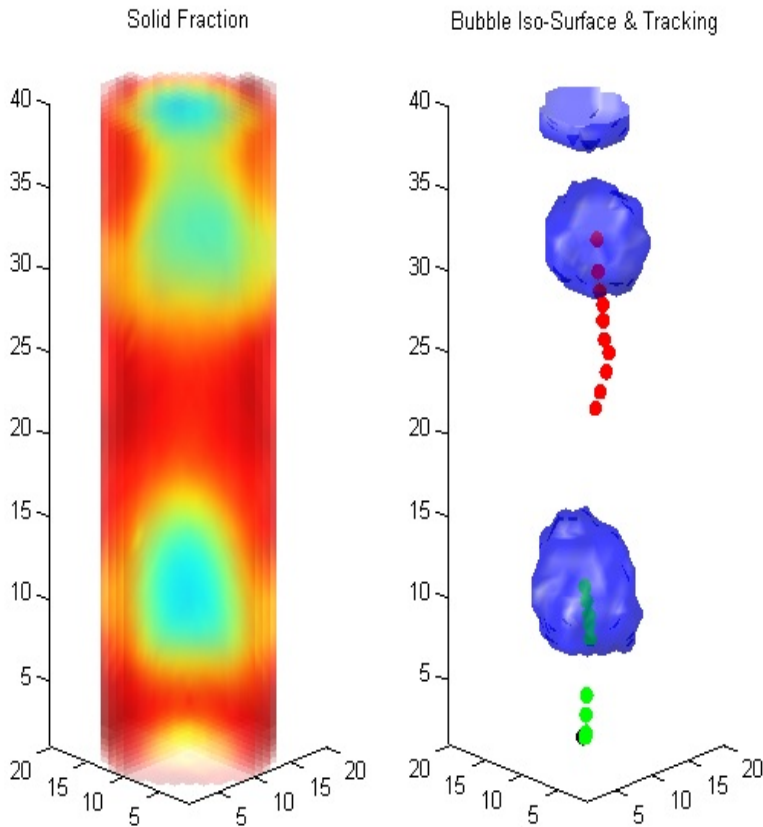
# Technical Approach – Task 3

Develop high-temperature Electrical Capacitance Volume Tomography (ECVT) sensor and software for real-time solid flow rate measurement



# ECVT System

- non-invasive sensors are used to measure changes in electrical capacitance in response to flow dynamics
- measured changes are mapped into phase concentrations using image reconstruction techniques



3D images of  
Multi-Phase Flow

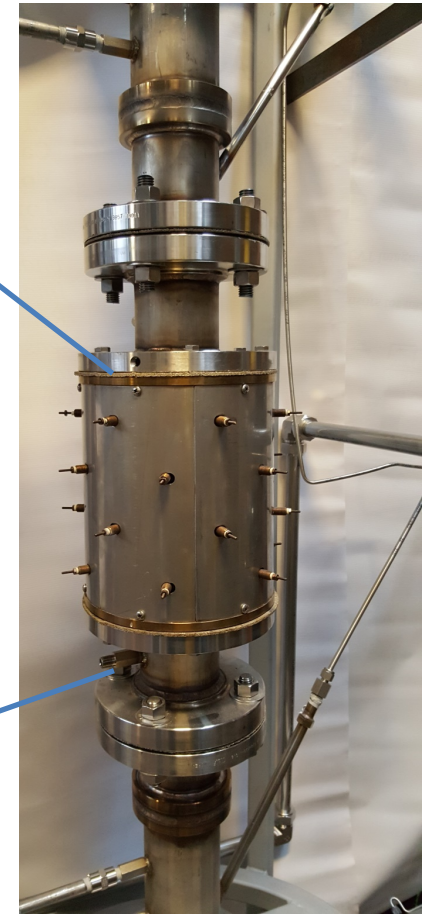
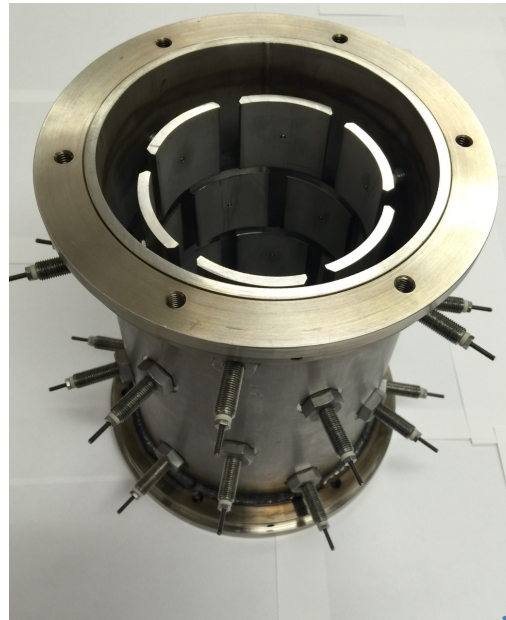
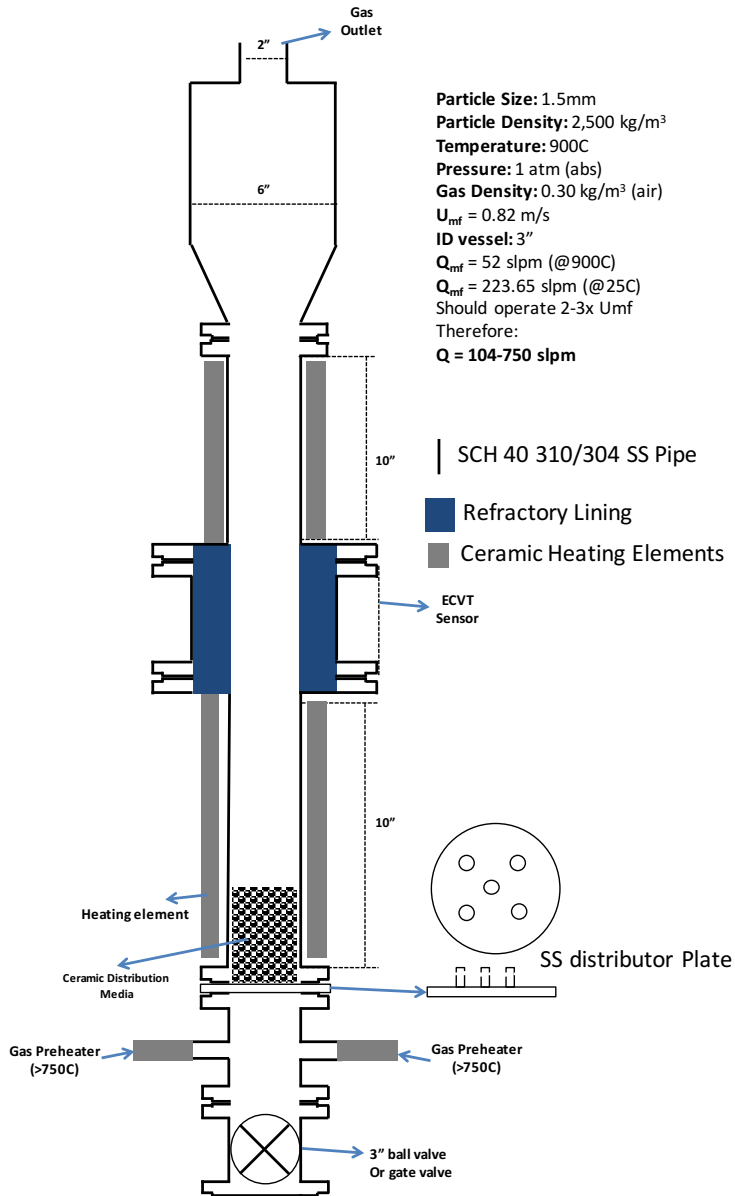


Data Acquisition and  
ECVT Sensor

TECH  
4IMAGING



# ECVT Hot Unit Design and Assembly





# ECVT Hot Unit Design and Assembly

- Temperature controller integrated
- Fluidization gas with flow control
- Manual valve for solid discharge to simulate moving bed mode



**TECH**  
**4IMAGING**



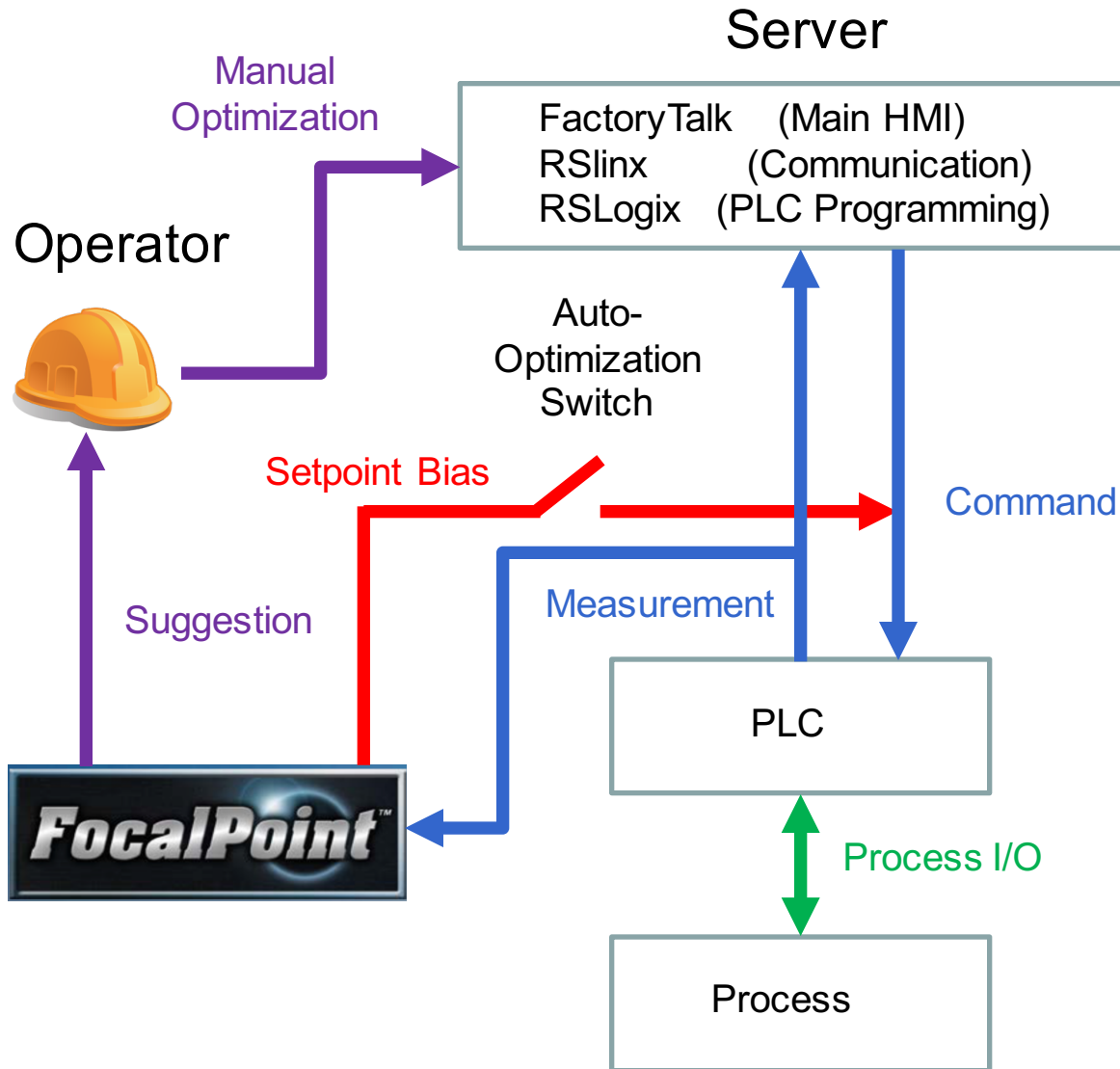
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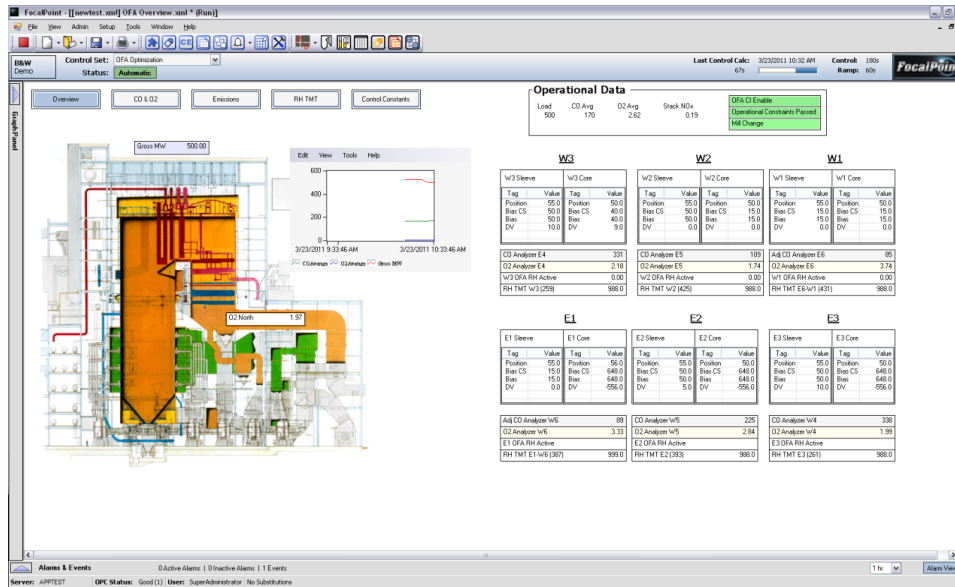
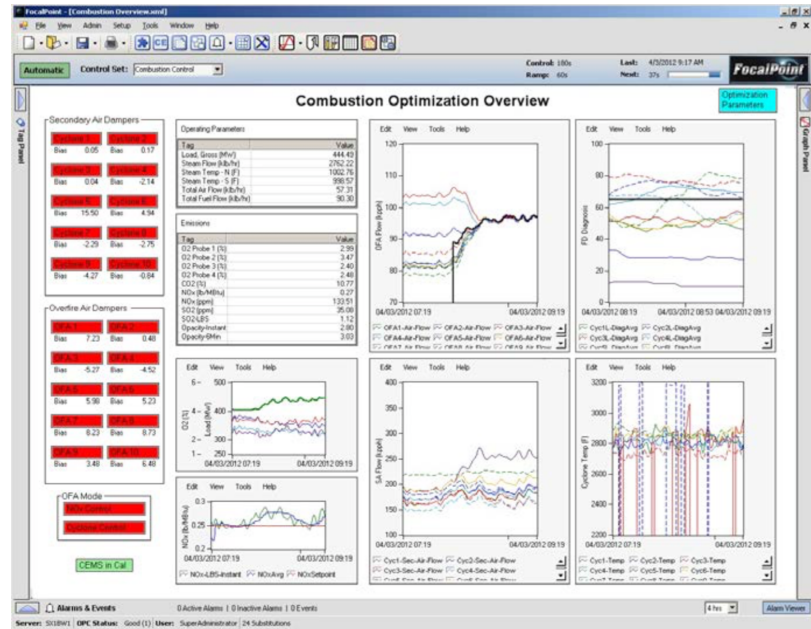
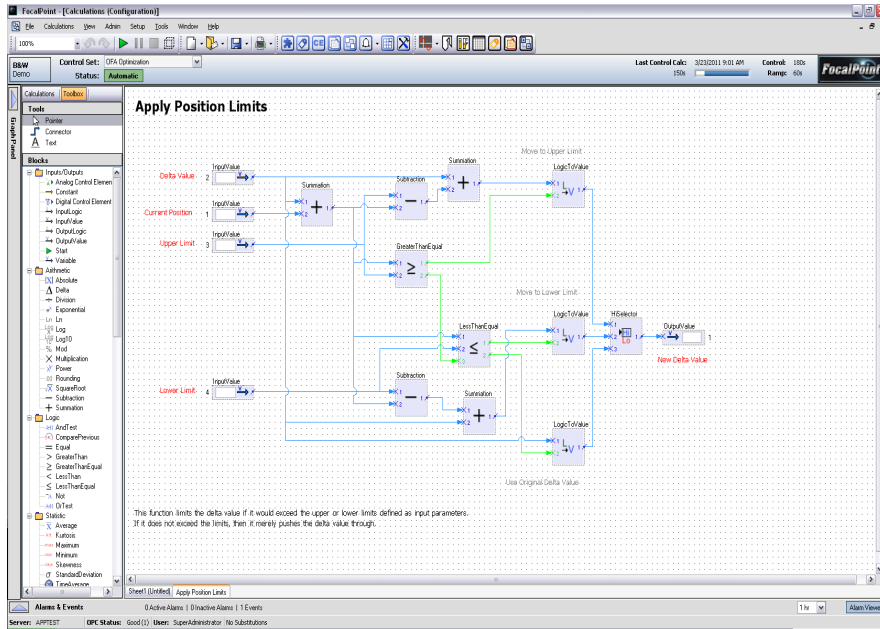


# Technical Approach – Task 4



- B&W's commercial real-time, closed-loop optimization system
- Realize modeling techniques, optimization algorithms and knowledge-based strategies
- Features more advanced function blocks such as fuzzy logic for control purposes
- Will be used to optimize
  1. solid circulation rate
  2. sealing gas usage

# Technical Approach – Task 4



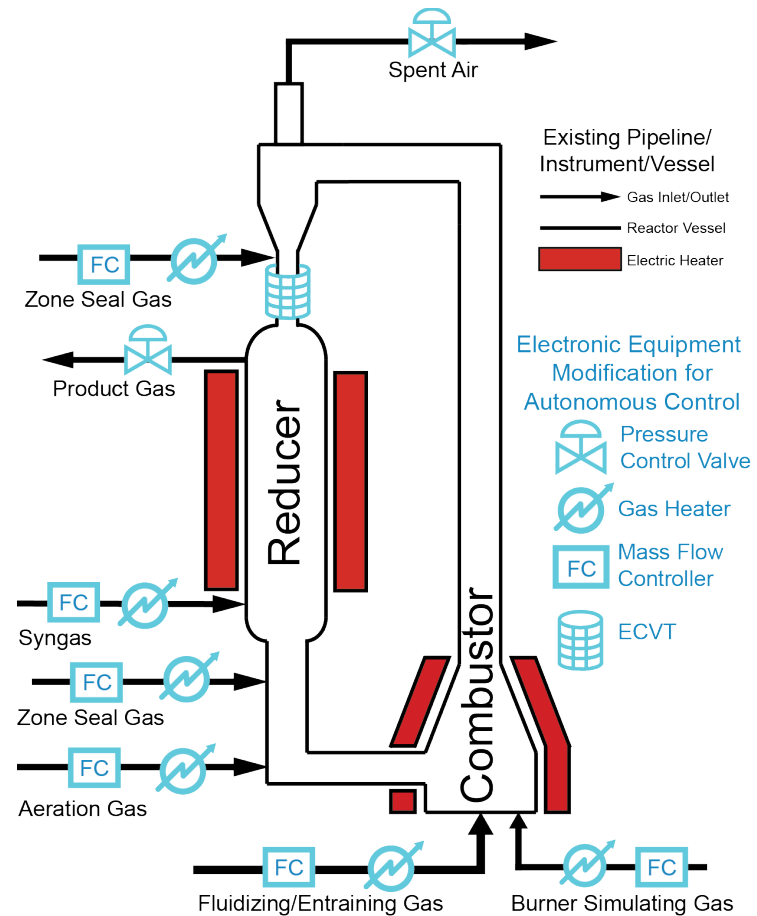
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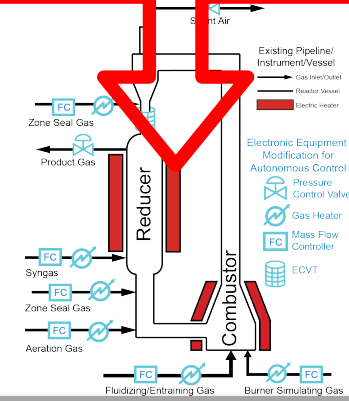
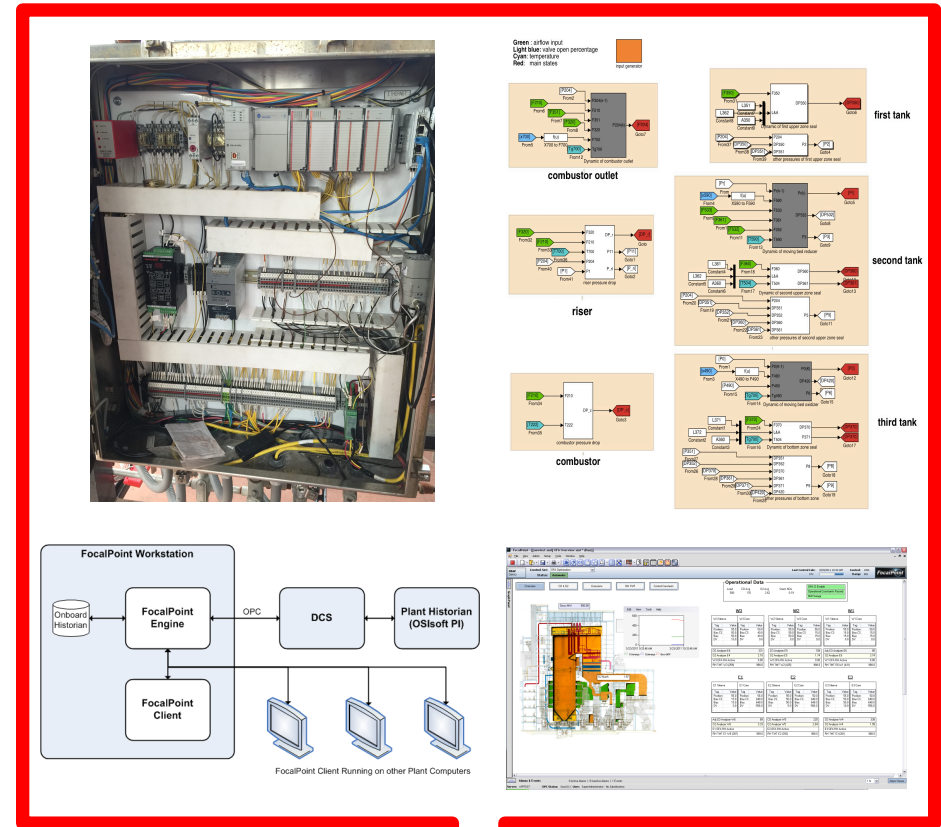
# Technical Approach – Task 5

Demonstrate continuous operation on existing SCL sub-pilot and pilot units



# Technical Approach – Task 5

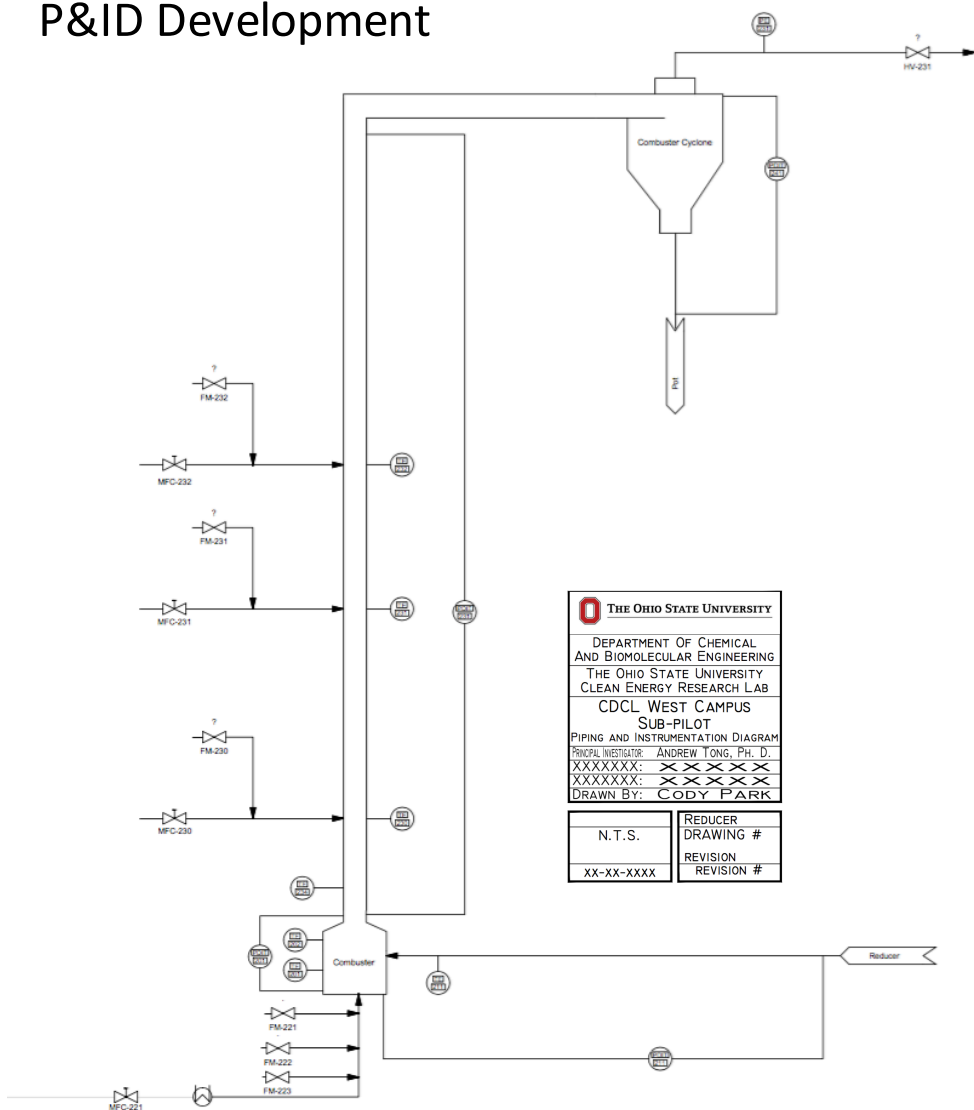
- Replace current manually-controlled components with controller-compatible components (ex: electronic mass flow controllers, control valves, gas heaters with relays) for autonomous control
- Upgrade the control system (HMI, PLC, client software) to industrial grade
- Integrate HLC-SMC control algorithm and FocalPoint with the standard system
- System assembly commissioning, instrument calibration
- Perform continuous operation and controller testing






# Task 5 status

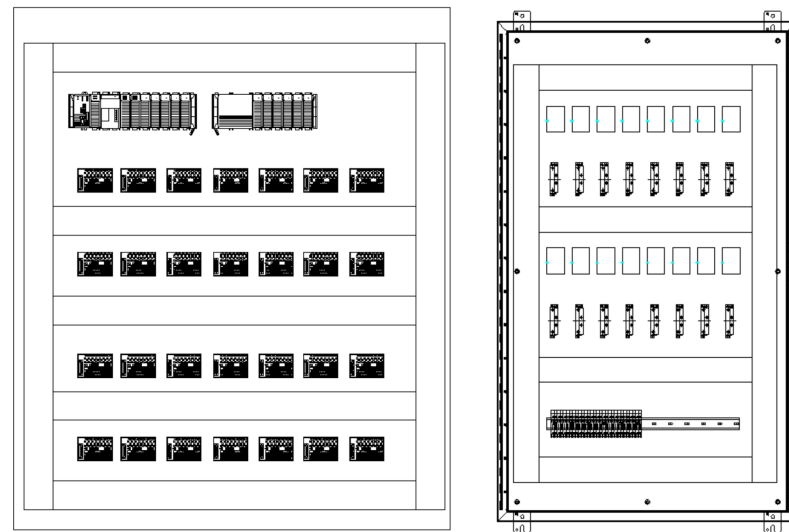
## P&ID Development



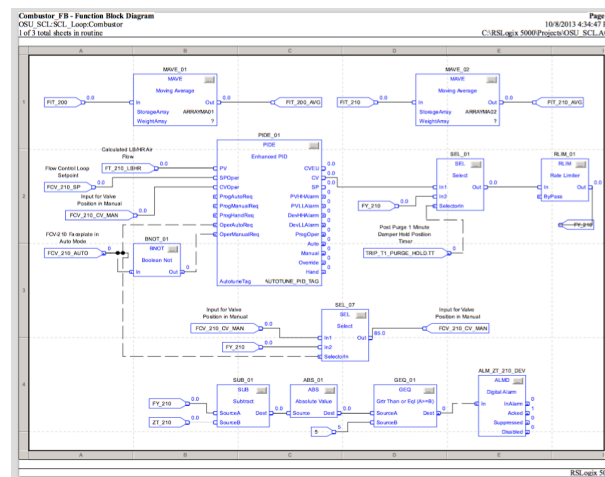
 THE OHIO STATE UNIVERSITY  
 DEPARTMENT OF CHEMICAL AND BIOMOLECULAR ENGINEERING  
 THE OHIO STATE UNIVERSITY CLEAN ENERGY RESEARCH LAB  
 CDCL WEST CAMPUS SUB-PILOT  
 PIPING AND INSTRUMENTATION DIAGRAM  
 PRINCIPAL INVESTIGATOR: ANDREW TONG, PH. D.  
 XXXXXXXX: XXXXXXXX  
 XXXXXXXX: XXXXXXXX  
 DRAWN BY: CODY PARK

N.T.S.	REDUCER DRAWING #
XX-XX-XXXX	REVISION #

## Control Panel Design



## PLC Control Programming



# Progress summary

- Developed dynamic models of the 3-reactor system based on the SCL-Pilot Unit at NCCC, qualitative characteristics validated
- Hot ECVT testing apparatus built
- FocalPoint incorporated in the server, training on-going
- Procured PLC, control software and control instruments

## Future work

- Develop HLC-SMC
- Calibrate and test the Hot ECVT unit in fluidized bed/moving bed mode
- Program interface between FocalPoint and control softwares
- Assembly testing units





# Acknowledgements

## Project Sponsors:



**National Energy Technology Laboratory:** This material is based upon work supported by the **Department of Energy** under Award Number **DE-FE0026334**



**Development Services Agency**

**Ohio Coal Development Office (OCDO) of the Ohio Development Services Agency (ODSA)**

## Industrial Collaborators:

- **Babcock and Wilcox Power Generation Group, Inc**
- **Tech4Imaging**
- **American Electric Power**



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