

# A New Superalloy Enabling Heavy Duty Gas Turbine Wheels for Improved Combined Cycle Efficiency

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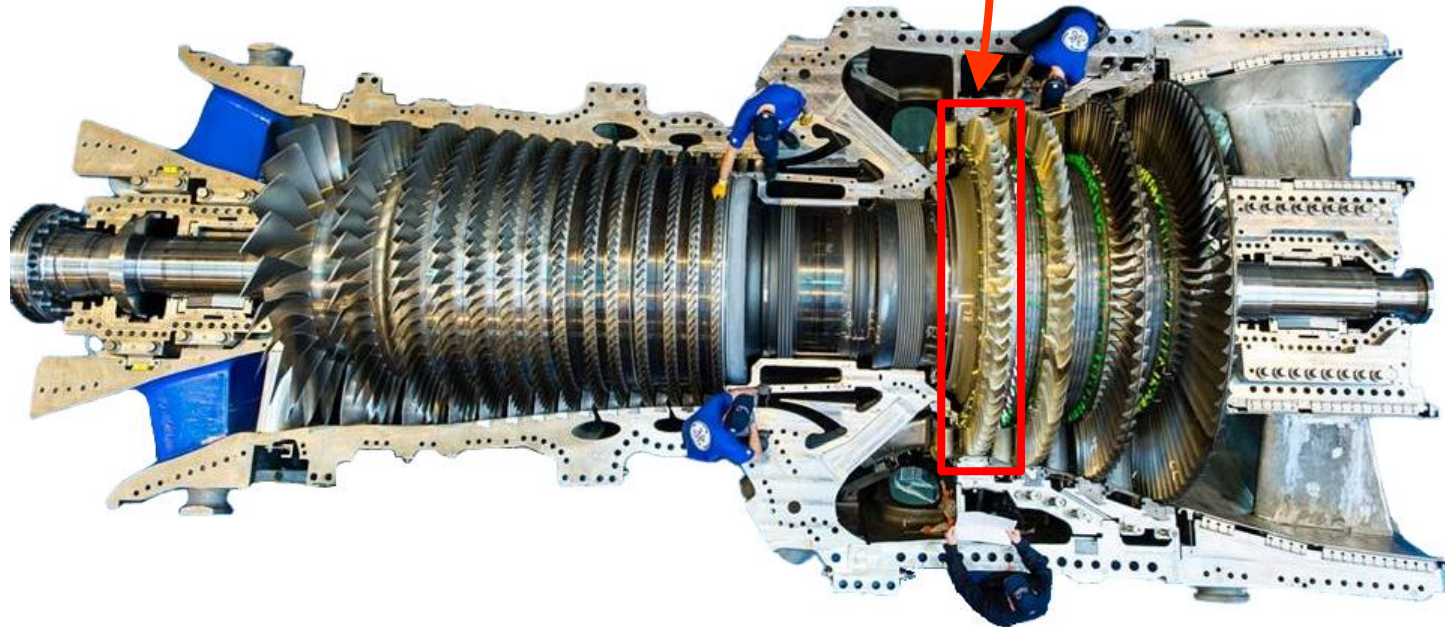
# Path to Higher Efficiency Gas Turbine

Today's  
combined cycle  
efficiency is  
~62%

Pressure Ratio: Higher  
Firing Temperature: Higher  
Sealing Flows: Lower  
Cooling Flows: Lower

**INCREASING  
WHEEL  
TEMPERATURE**

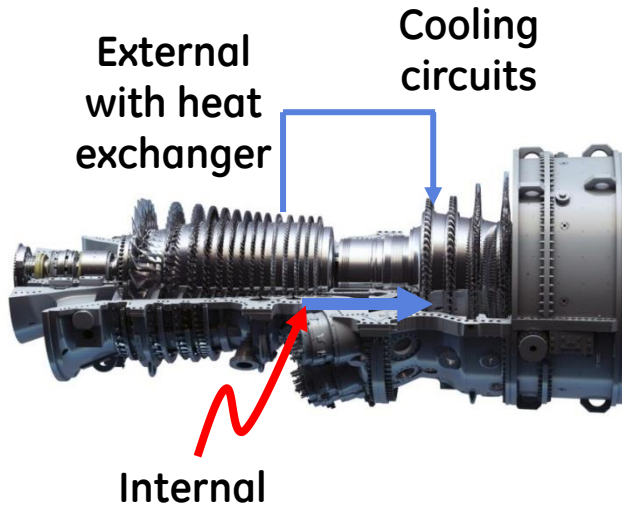
Future turbine  
combined cycle  
efficiency is  
~65%



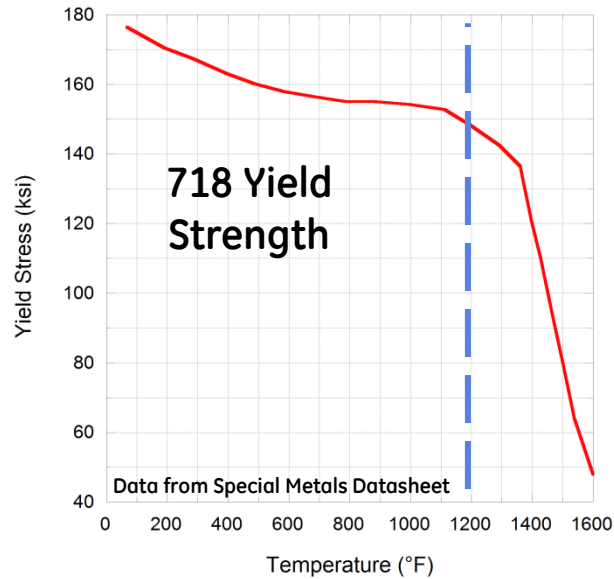
Next generation heavy duty gas turbine wheels must operate at higher temperatures to enable combined cycle efficiency improvements.

# Designing a Higher Temperature Capable Wheel

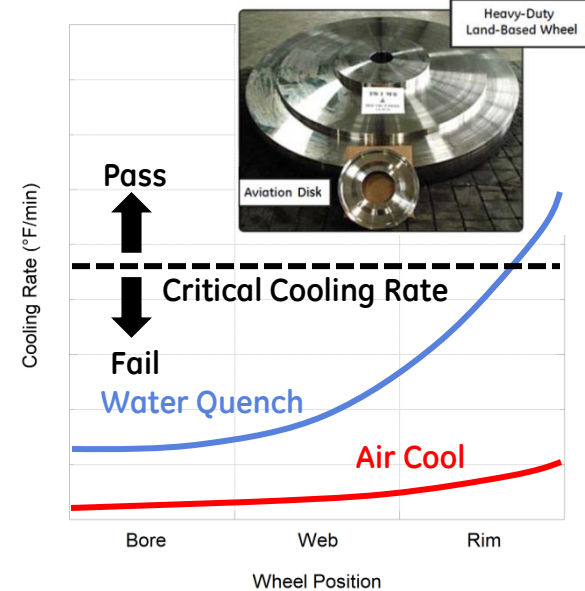
Use steel and cool to lower the effective temperature



Invent a better  $\gamma''$  ( $\text{Ni}_3\text{Nb}$ ) strengthened alloy



Use an Aviation disk alloy strengthened with  $\gamma'$  ( $\text{Ni}_3\text{Al}$ )



Cooling leads to reduced efficiency, increased complexity, & reliability risks.

$\gamma''$  strengthening phase is unstable at temperatures  $>1200^\circ\text{F}$ .

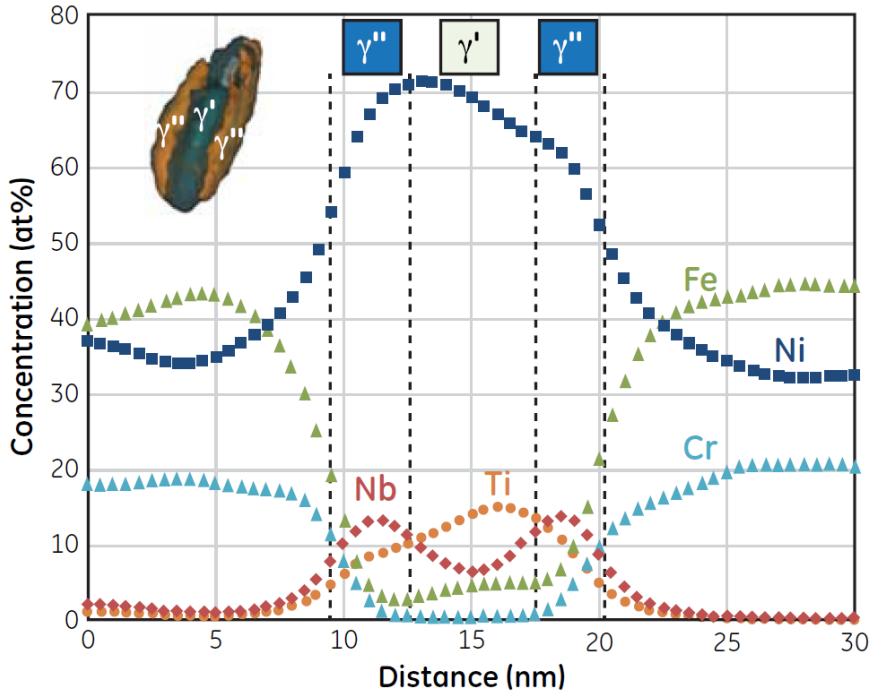
Precipitation kinetics result in severe over aging of  $\gamma'$ , yielding poor properties.

A new approach to alloy design is required to enable high temperature wheels.



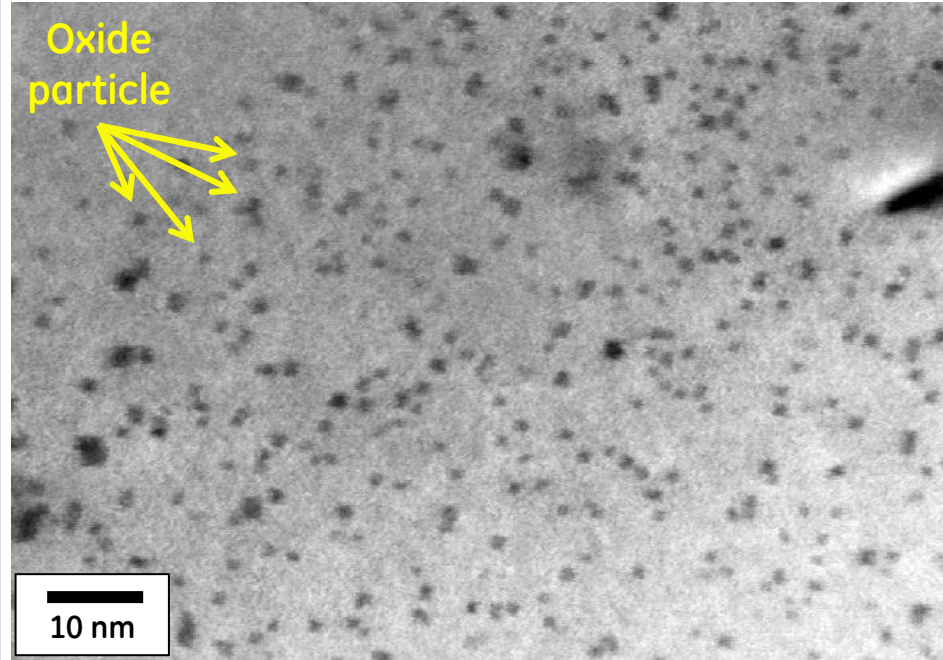
# Advanced Wheel Concepts

## Coprecipitation



Leverage the coprecipitation of  $\gamma'$  and  $\gamma''$  to restrict  $\gamma'$  coarsening during slow cooling of thick section components.

## Oxide Dispersion Strengthening



Extend the oxide strengthening concept of nanostructured ferritic alloys to Ni-based alloys.

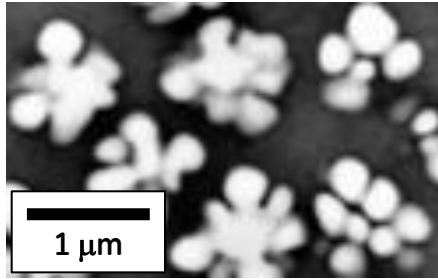
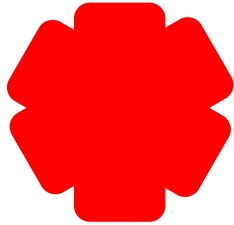
Two fundamentally different approaches being pursued during Phase 1.



# Coprecipitation Overview

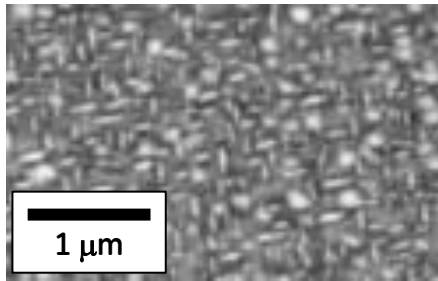
## Current Strengthening Phase Precipitation

Slow Cooled  $\gamma'$  ( $\text{Ni}_3\text{Al}$ )

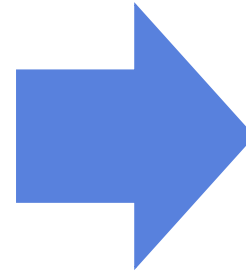


Overaged/Ineffective

Slow Cooled  $\gamma''$  ( $\text{Ni}_3\text{Nb}$ )



Temperature Limited



## Desired Coprecipitation

Slow Cooled  $\gamma'/\gamma''$



Precipitation of  $\gamma''$  limits the coarsening/overaging of  $\gamma'$  enabling  $\gamma'$  to act as an effective strengthening phase in slow cooled parts

- $\gamma'$  believed to nucleate first, enrichment in Nb at  $\gamma'/\gamma$  interface promotes  $\gamma''$  nucleation
- Subsequent coarsening limited by diffusion of Al, Ti through Nb-rich  $\gamma''$

Cozar, Pineau, Met Trans, 4, 47-59 (1973)

$\gamma''$  phase intended only to prevent  $\gamma'$  over-aging upon slow cooling.

# Coprecipitation Model

## Inputs

- Chemical free energy
- Elastic modulus
- Lattice parameter
- Diffusivity
- Interfacial energy



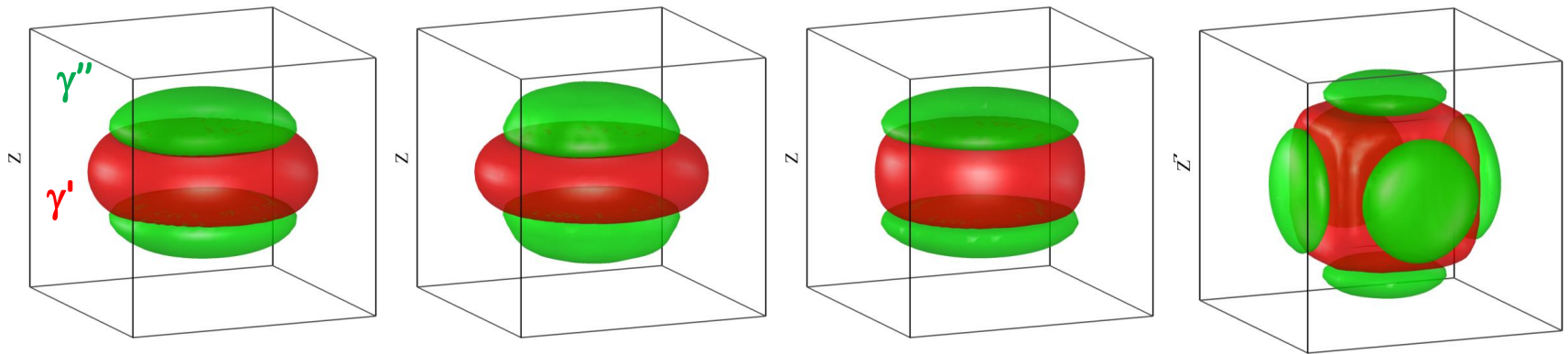
## Models

- 1) Isothermal multi-phase field model
- 2) Continuous cooling simulation



## Outputs

- 1) Prediction of compositional ranges that yield coprecipitation
- 2) Slow cooled microstructure prediction

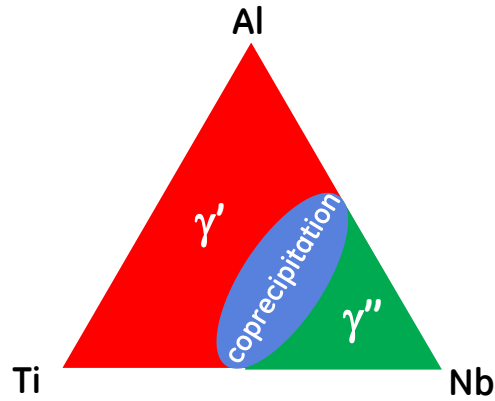


A parametric study of interfacial energies ( $\gamma/\gamma'$ ,  $\gamma/\gamma''$ ,  $\gamma'/\gamma''$ ) shows how their variation leads to different coprecipitation shapes.

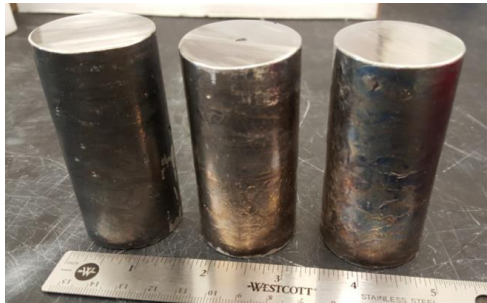
The phase field model allows coprecipitation parametric studies to be successfully completed.

# Coprecipitation Experimental Approach

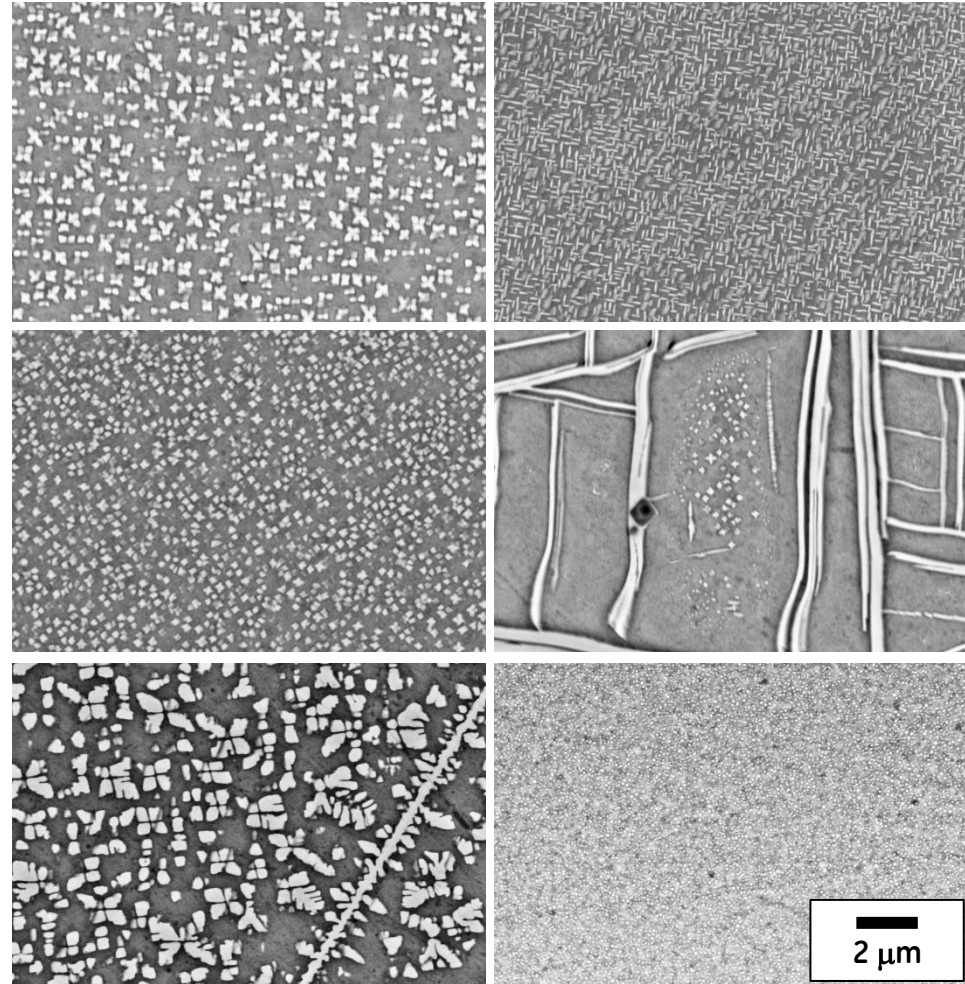
- Choose base alloys to vary chemistry



- Vacuum induction melt & homogenize



- Slow cool from homogenization & examine precipitate structure



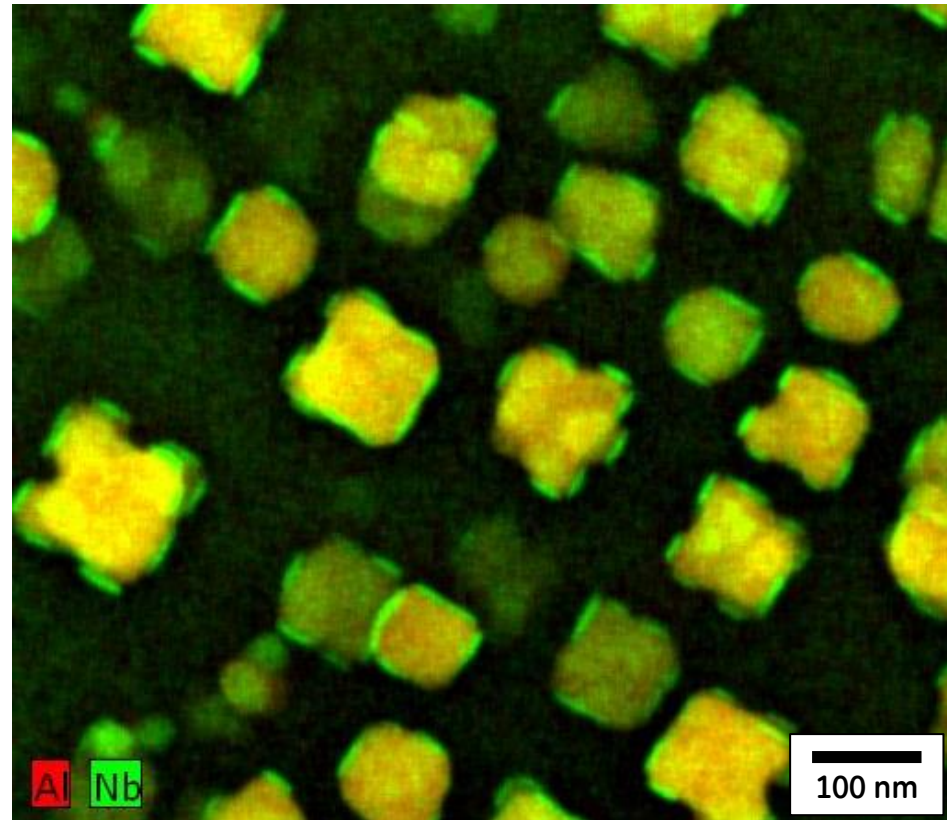
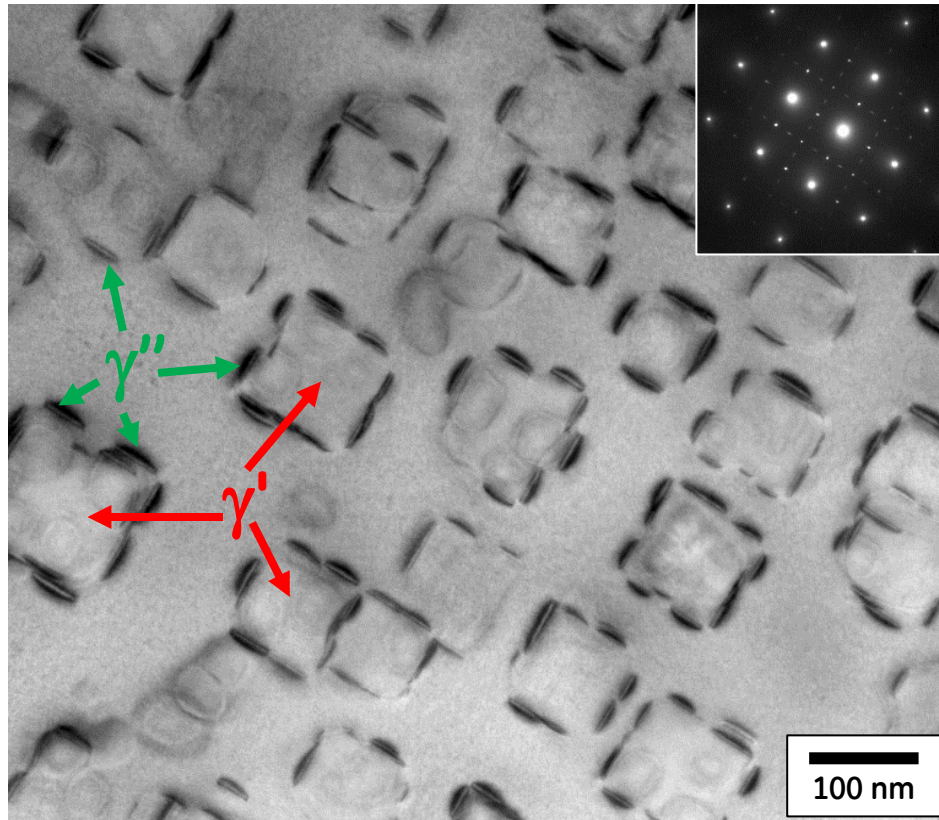
Process allows for rapid alloy chemistry screening for desired space showing fine precipitates without deleterious TCP phases.



# Slow Cool Coprecipitation Results

Bright Field TEM & [001] SAD

TEM EDS Map

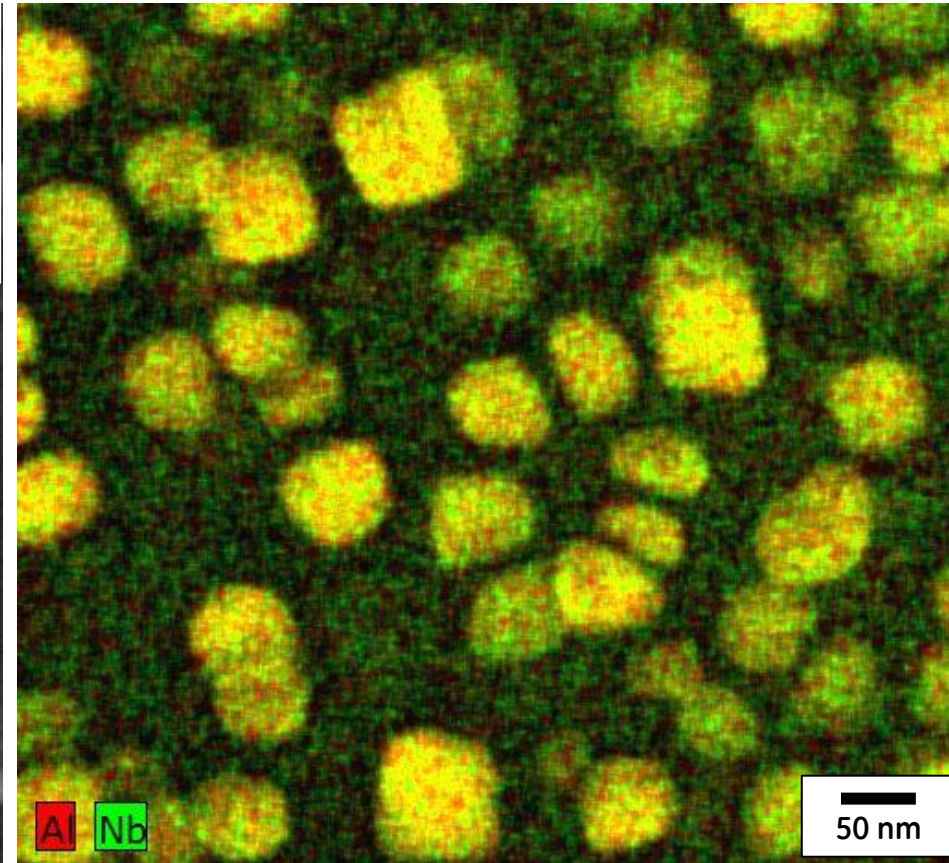
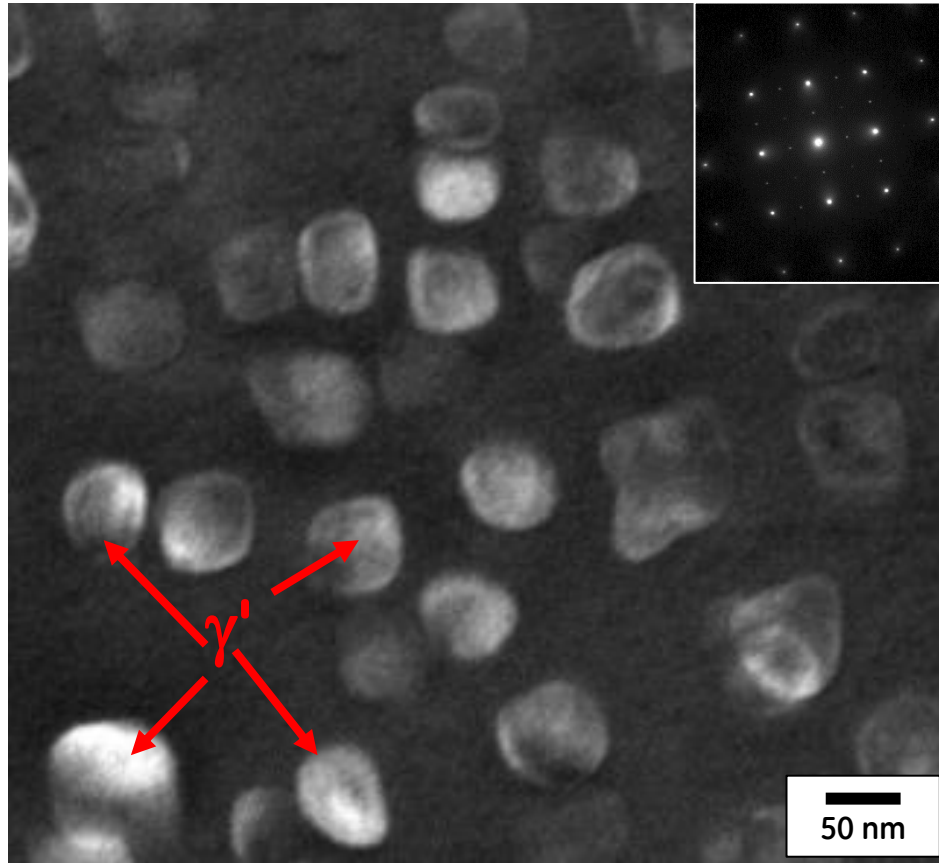


$\gamma''$  precipitation on  $\gamma'$  precipitates have successfully led to a fine  $\gamma'$  size following a slow cool from homogenization.

# Slow Cool Sluggish $\gamma'$ Precipitation Results

Dark Field TEM & [001] SAD

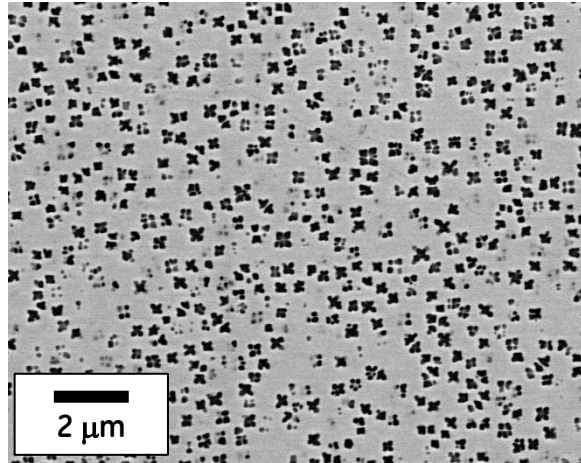
TEM EDS Map



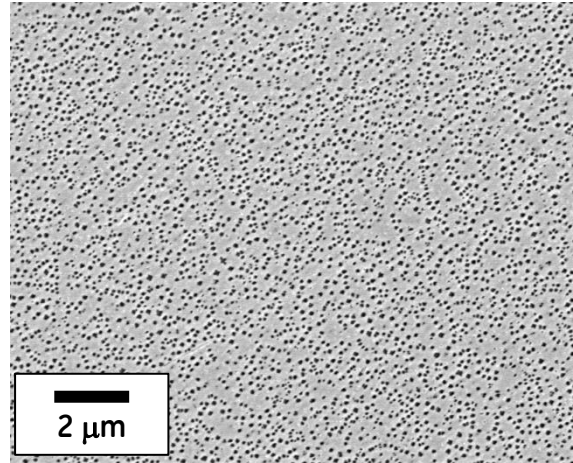
This composition surprisingly yields very fine  $\gamma'$  precipitates despite the slow cooling rate imposed (no coprecipitation seen).

# Slow Cool Precipitate Comparison

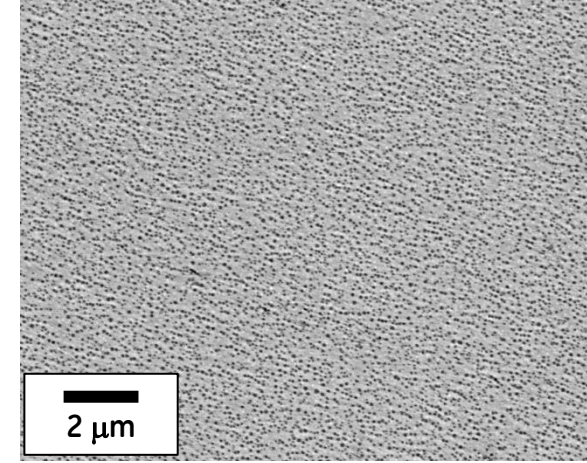
Baseline  $\gamma'$  Alloy  
19% Area Fraction



Coprecipitation Alloy  
17 $\pm$ 2% Area Fraction

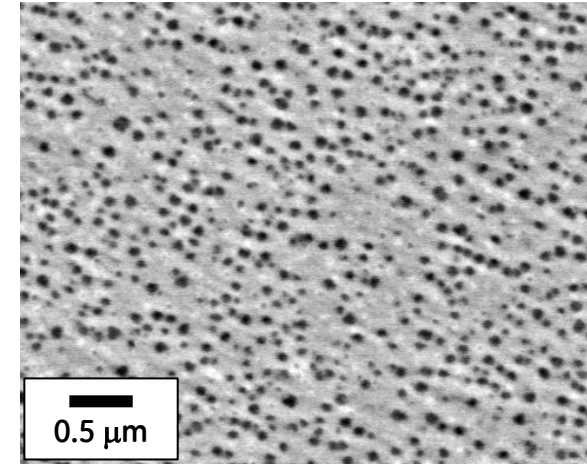
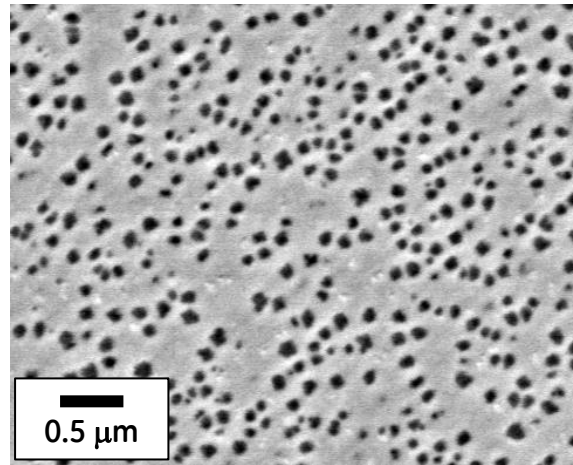
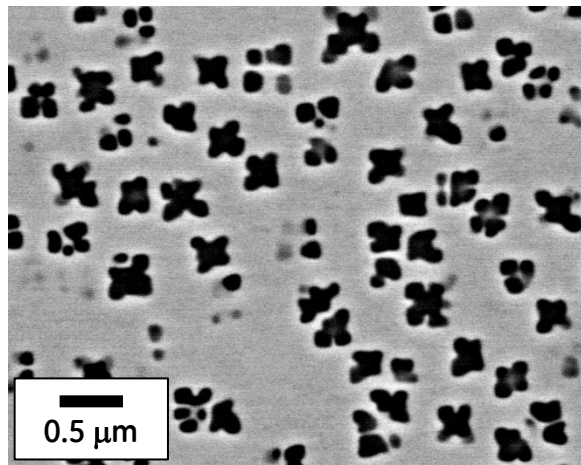


Sluggish  $\gamma'$  Alloy  
16 $\pm$ 4 % Area Fraction



Low Magnification

High Magnification

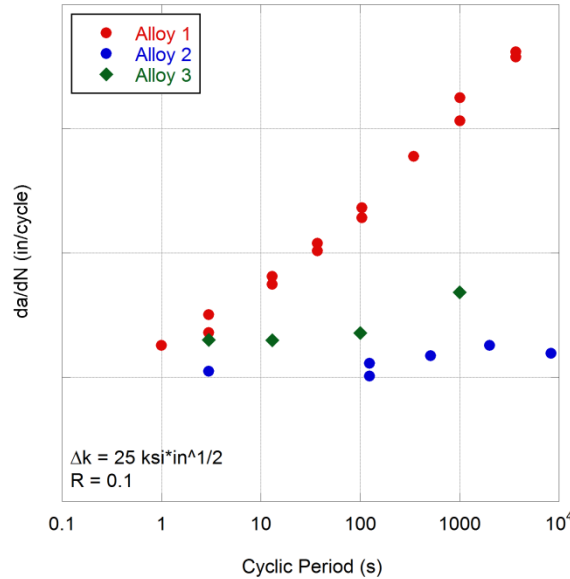


The new alloys yield substantially finer strengthening precipitates than the slow cooled baseline structure.

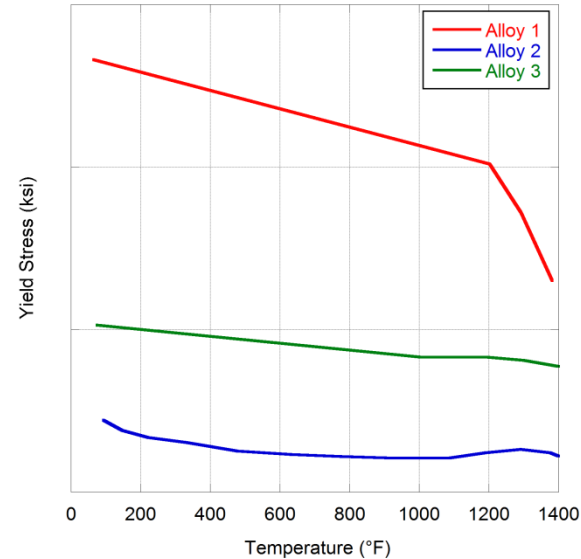


# Oxide Dispersion Strengthening Overview & Approach

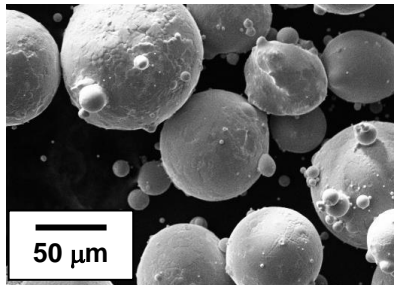
Hold time  
fatigue crack  
growth data



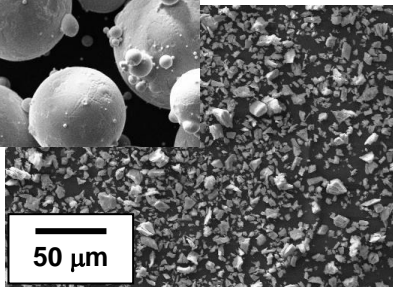
Tensile  
data



Ni Alloy Powder



$\text{Y}_2\text{O}_3$



High energy  
ball milling

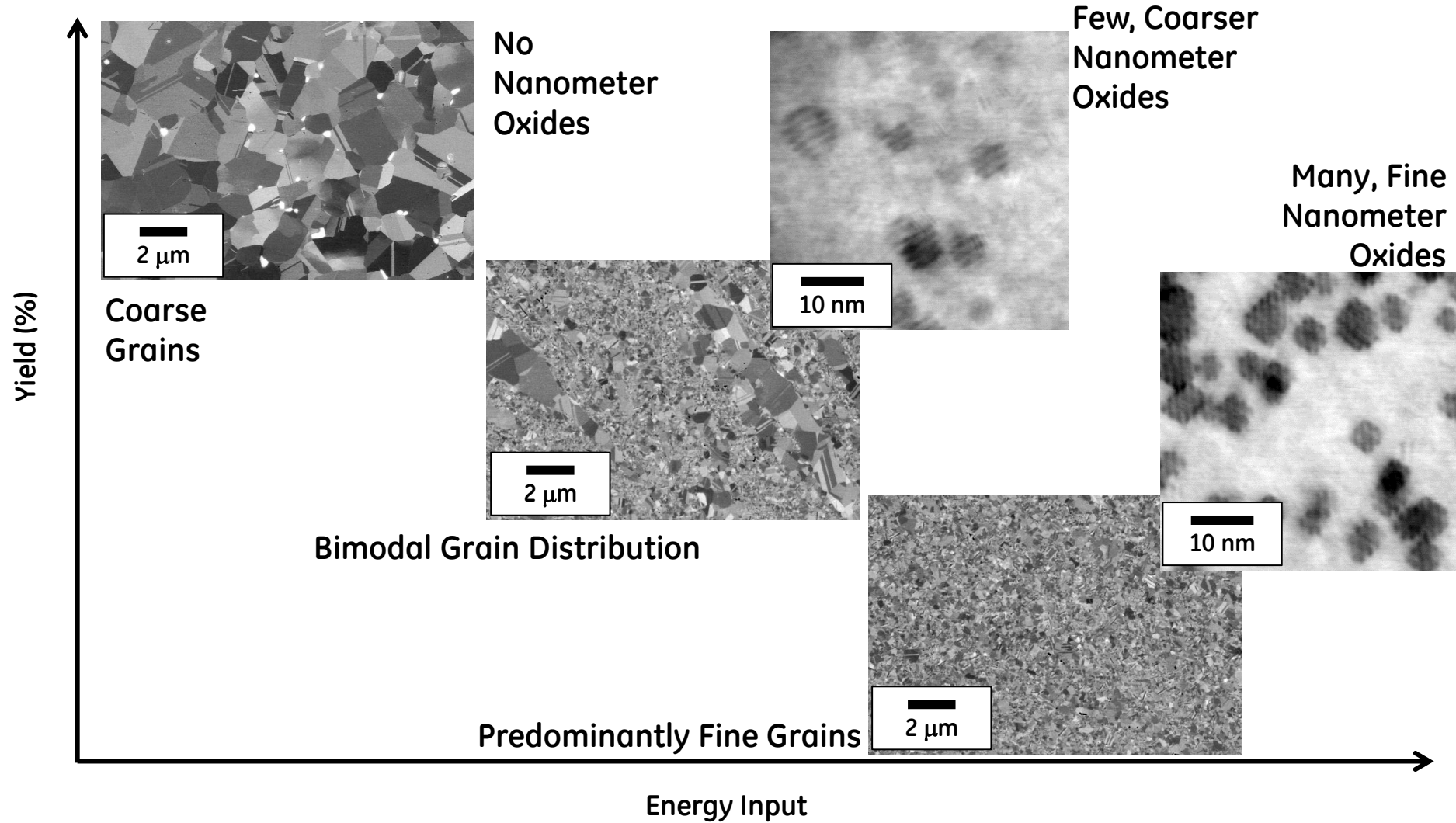


HIP + Forge



Use oxides to strengthen existing alloys without debiting the desired hold time fatigue crack growth resistance.

# ODS Process Development

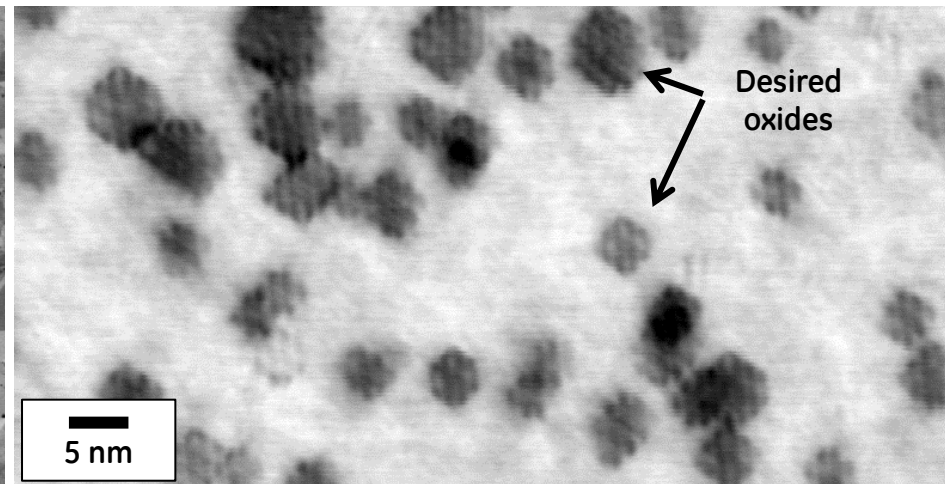
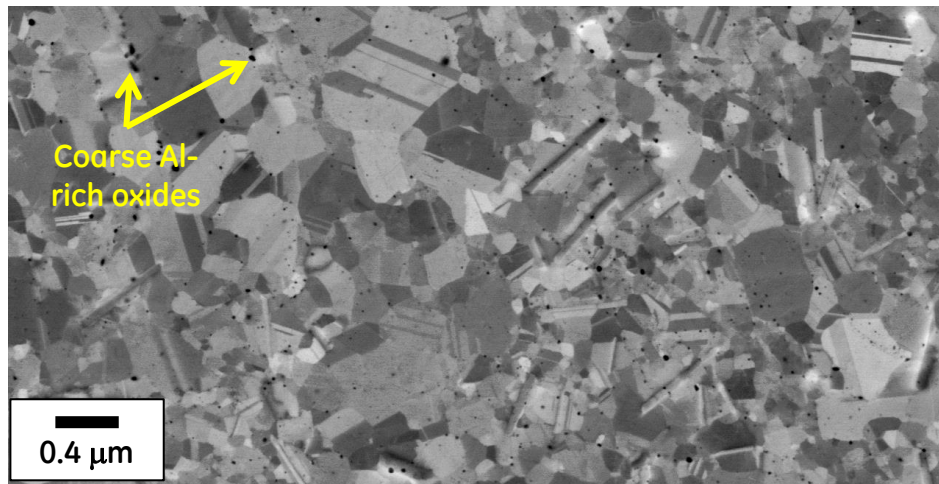
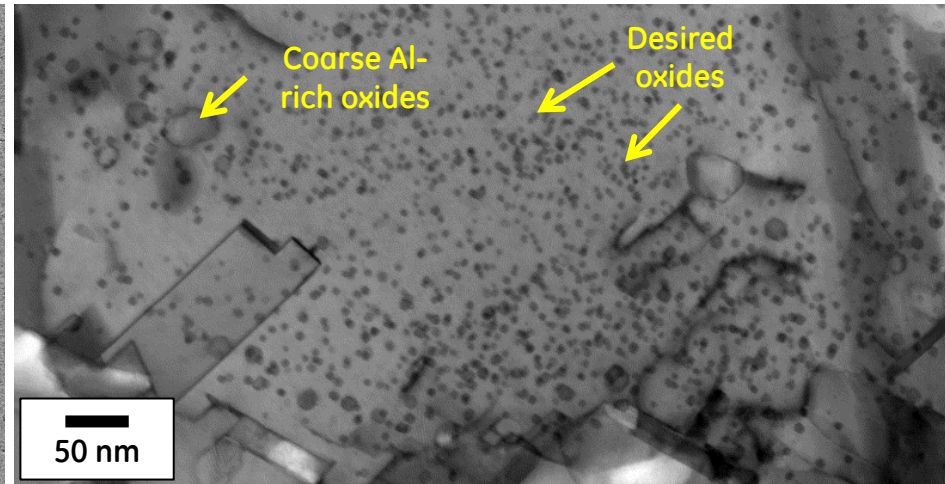
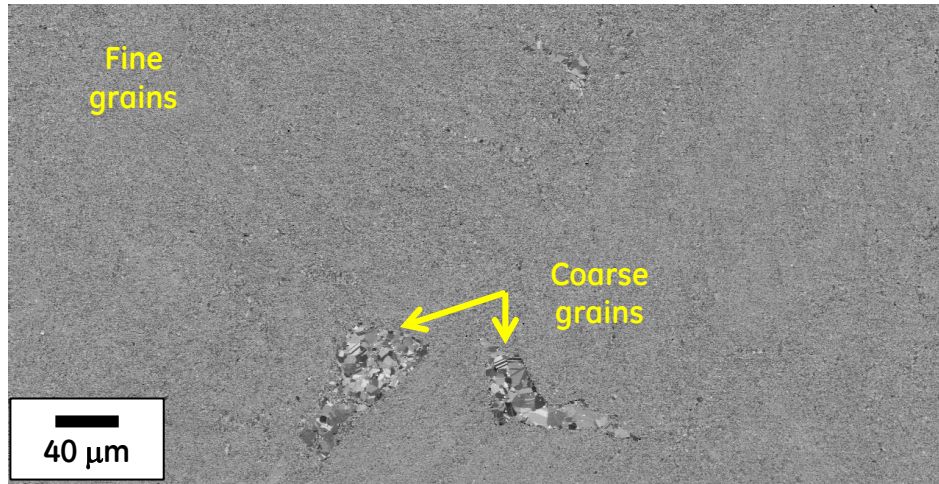


Current selected process gives up high yield to increase mill energetics to drive grain refinement and homogeneous oxide precipitation.

# ODS Alloy 2 As-HIP Results Summary

SEM

TEM



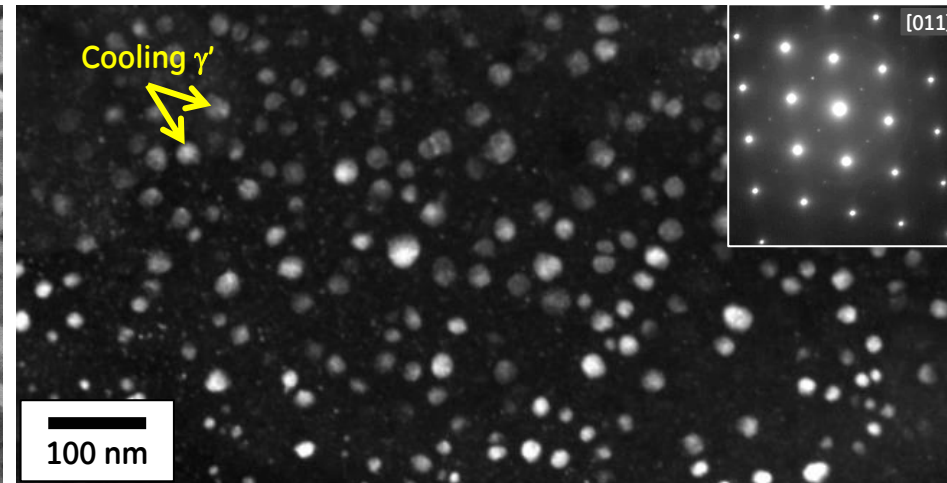
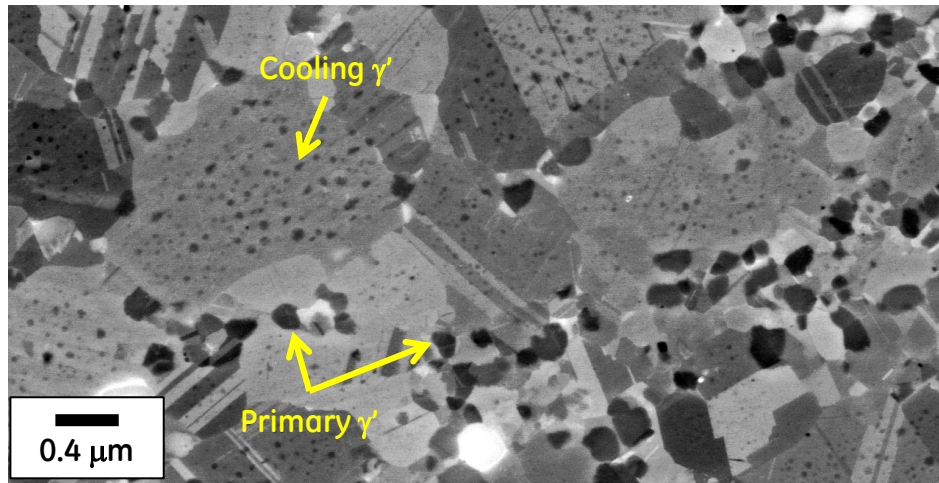
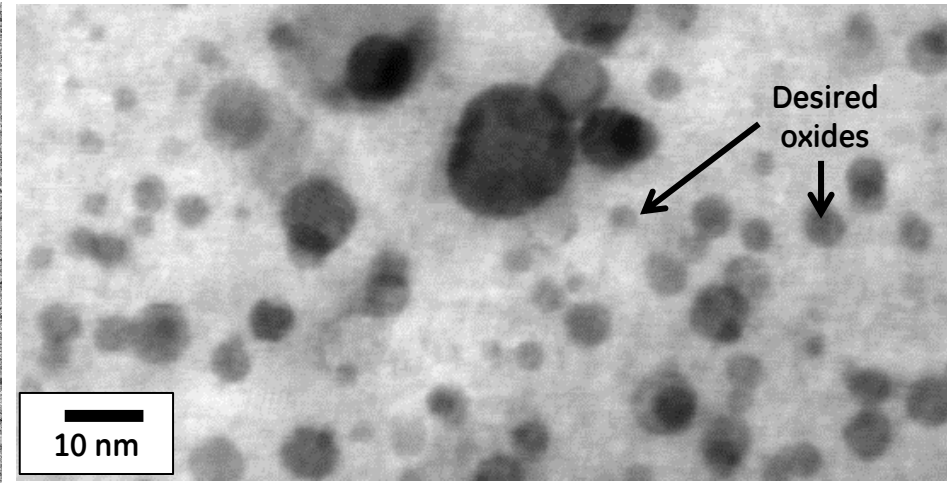
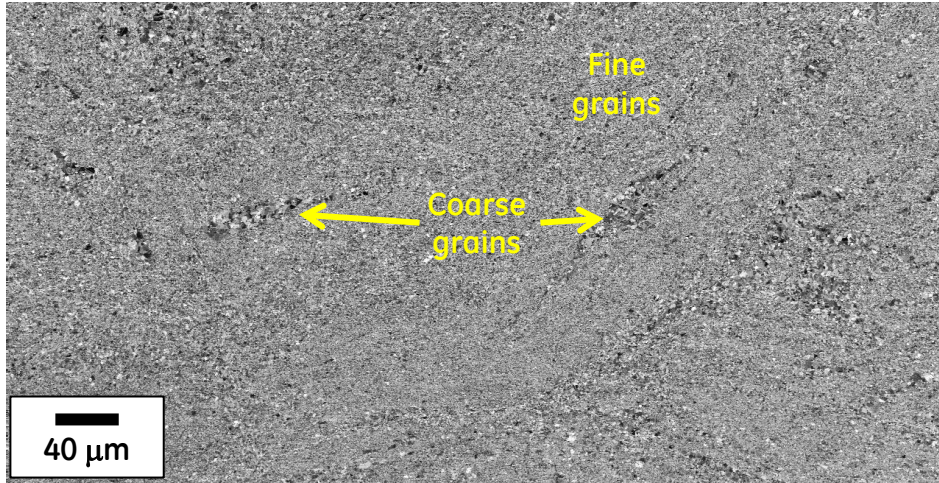
Initial results show dense oxide precipitation that can be controlled by chemistry and mill energy.



# ODS Alloy 3 As-HIP Results Summary

SEM

TEM



Initial results show dense oxide precipitation coexists with  $\gamma'$  precipitation.

# Conclusions & Next Steps

- Experimental results for coprecipitation & ODS support the technical feasibility of each concept
- Established a 3D phase-field model with  $\gamma'/\gamma''$  co-precipitation
- Thermo-mechanical processing is critical to achieving a viable broken down microstructure suitable for mechanical testing
- Hold time fatigue crack growth and tensile tests will be used to screen the effectiveness of each alloy

