

# **Flame Flashback in Hydrogen-rich Gas Turbines**

**Venkat Raman**  
**Department of Aerospace Engineering**  
**University of Michigan**

**Noel Clemens**  
**Dept. of Aerospace Engineering and Engineering**  
**Mechanics**  
**The University of Texas at Austin**

**DOE DE-FE0012053 with Dr. Mark Freeman as Program**  
**Monitor**

# Background

- **Overarching goal: Understand flame flashback in hydrogen-rich gas turbines**

- ➔ High pressure higher Reynolds number flow

- ➔ Fuel stratification effects

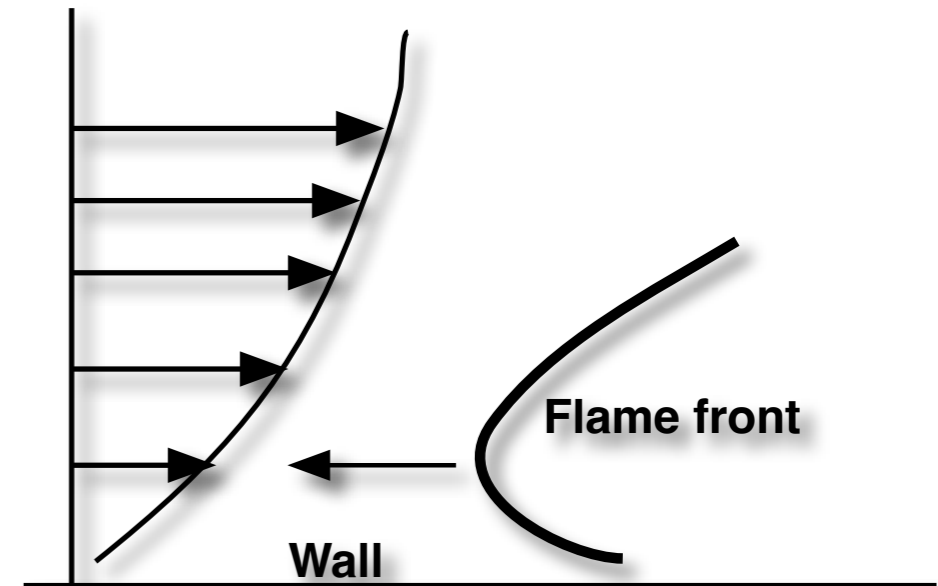
- **Experimental program**

- ➔ Conduct high pressure experiments in UT swirler configuration

- ➔ Simultaneous PIV/PLIF measurements to characterize flame/boundary layer interaction

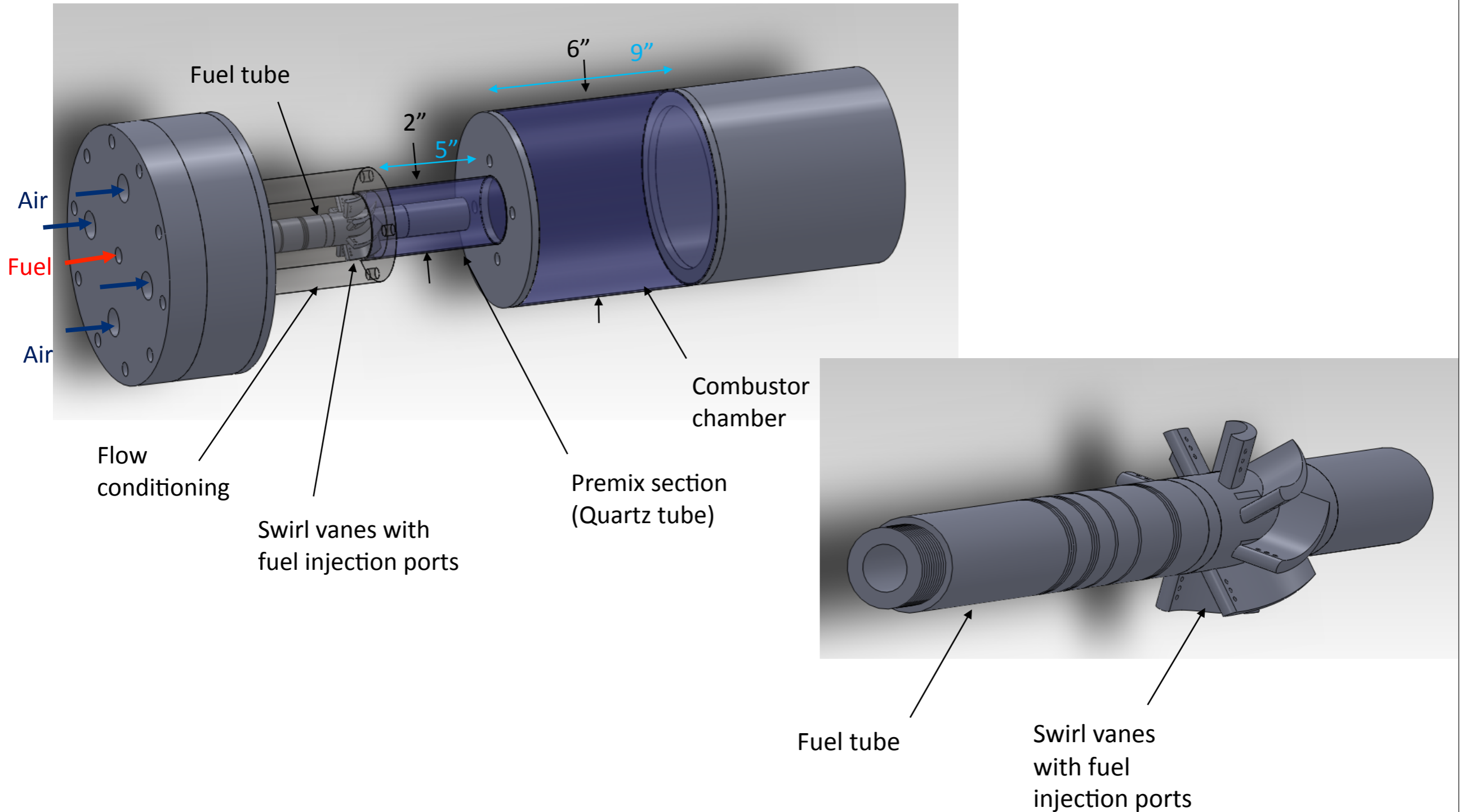
- **Computational program**

- ➔ Develop models for predicting flashback in stratified flame configurations

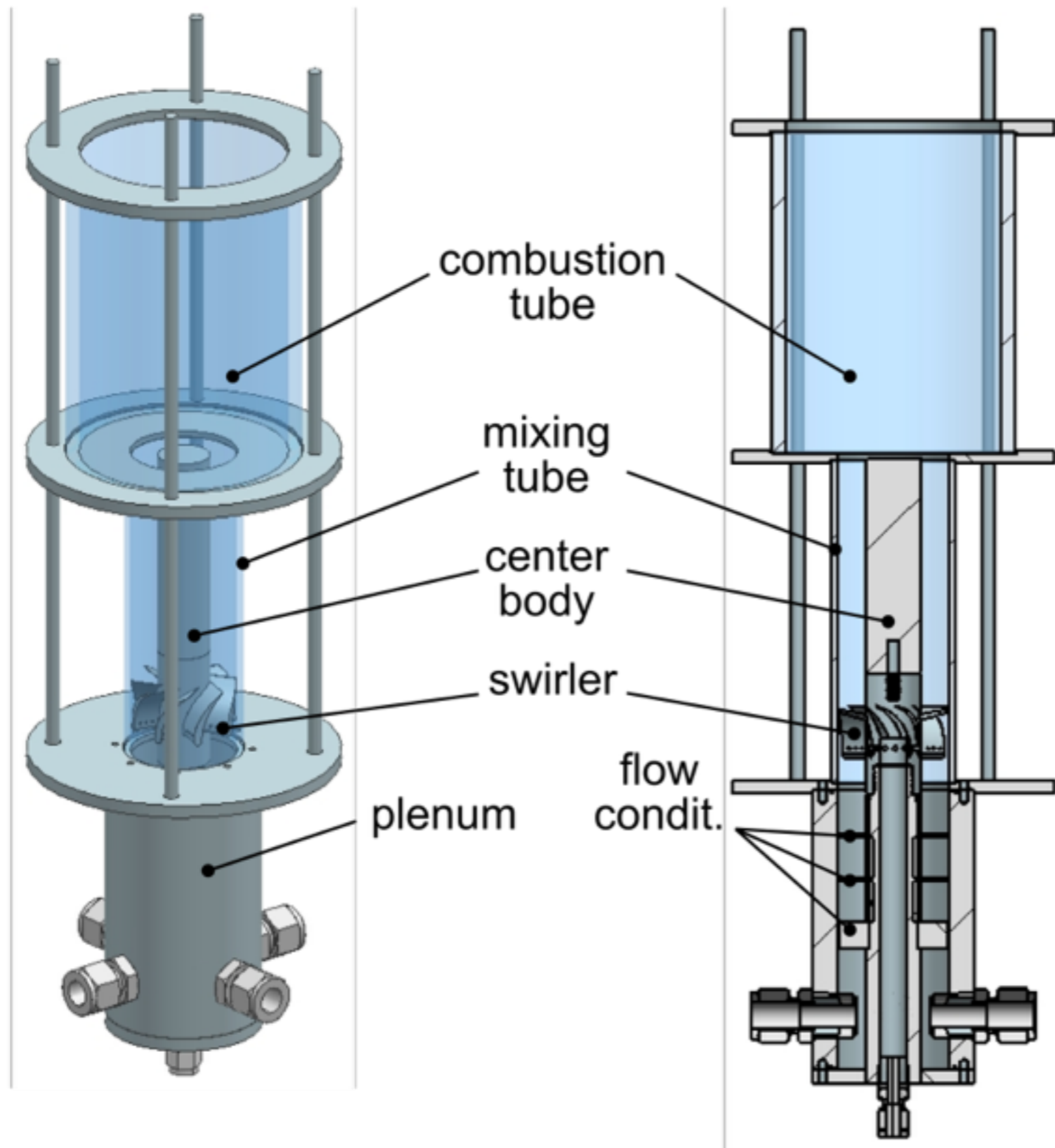


# Target-based Flashback Modeling

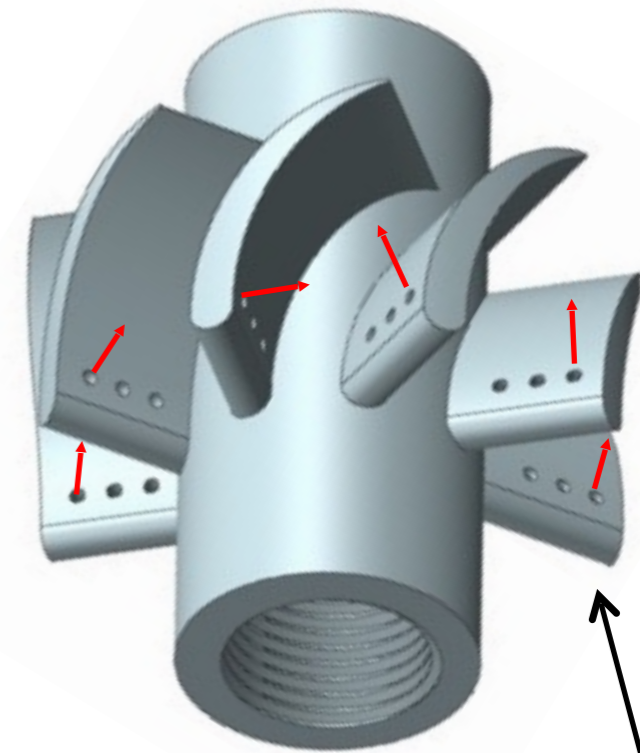
- UT high-pressure swirl combustor



# Model swirl combustor



- Produce stratified flow by selective injection through swirl vanes



Inject fuel or rich mixture through outer holes

# Summary of Results

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- **High pressure experimental data**

- ➔ 1-4 bar methane and methane/hydrogen experiments conducted
- ➔ Focus on fuel stratification

- **Understanding model sensitivities**

- ➔ Low-Ma vs compressible flow modeling
- ➔ Effect of stratification on flame structure
- ➔ Numerical modeling of flame structure propagation
- ➔ Open source LES tool for gas turbines

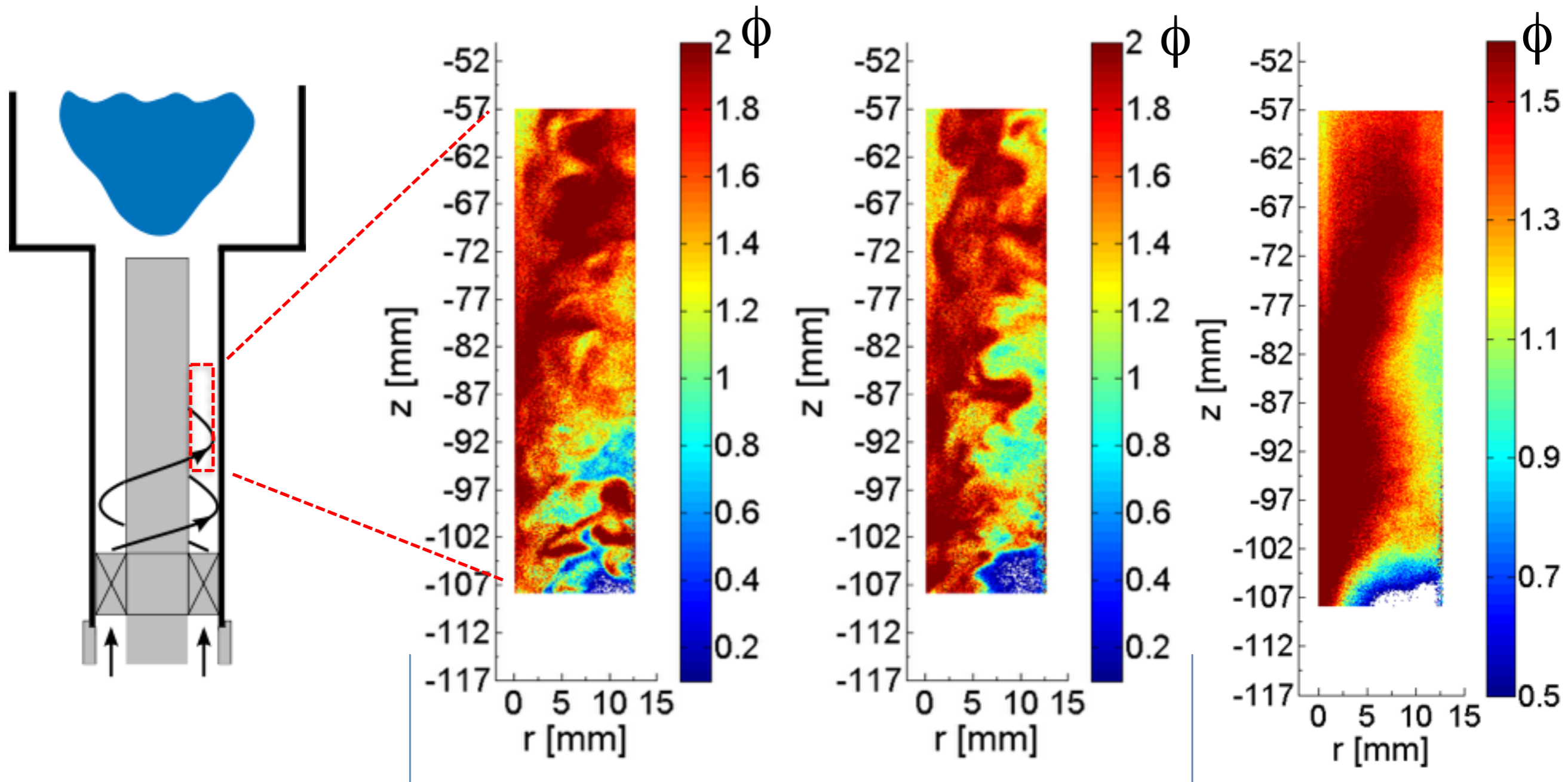
# High-Pressure Combustion Facility

- Test stratification effects at elevated pressure
  - Up to 10 bar
- Swirl burner
- Concentric stratified flame burner



# Acetone PLIF to assess stratification

- Acetone-CH<sub>4</sub> mixture injected through outer holes only
- Signals mapped to equivalence ratio



Instantaneous equivalence ratio

Mean

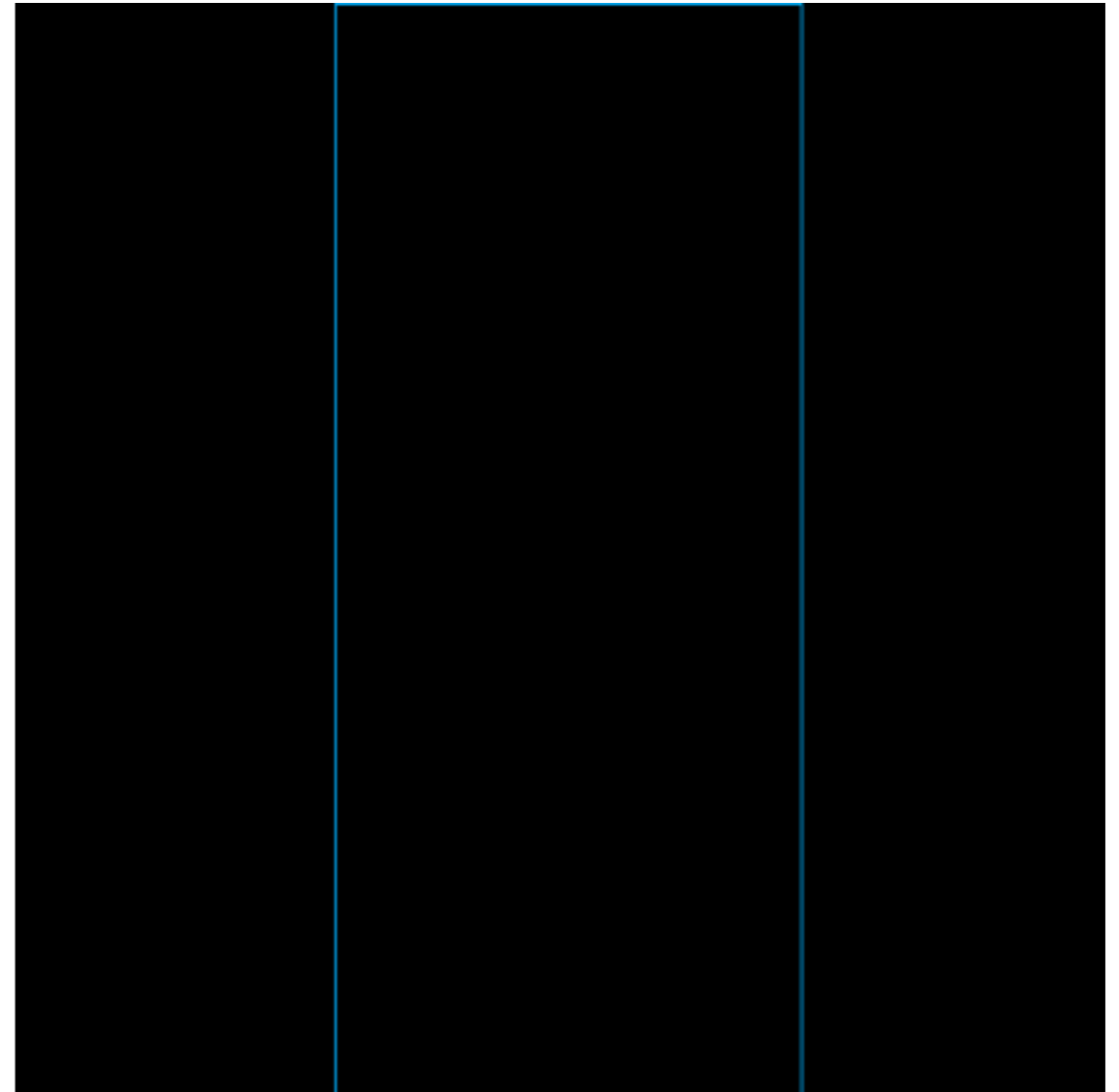
# Effect of stratification on flashback

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- Comparison of flashback with fully premixed and stratified reactants



Fully premixed



Stratified



# Summary of Results

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- **High pressure experimental data**

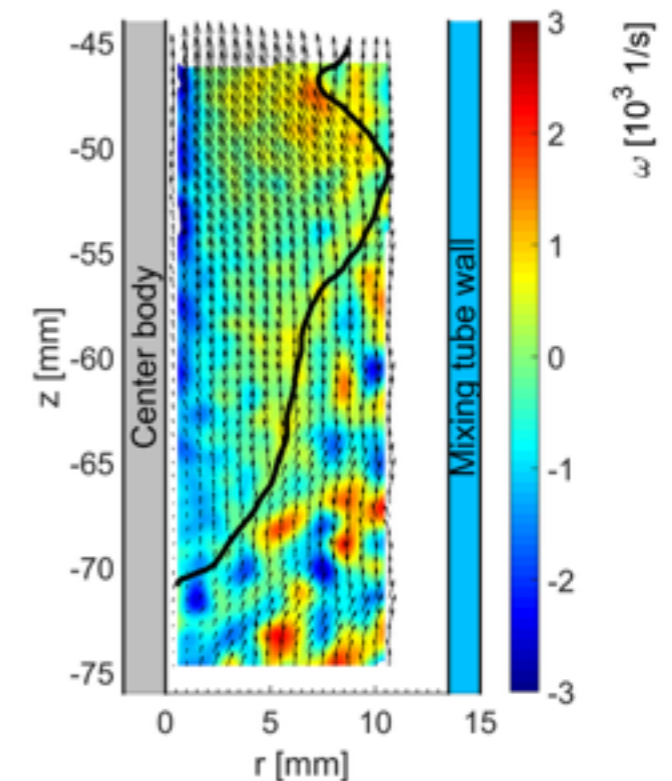
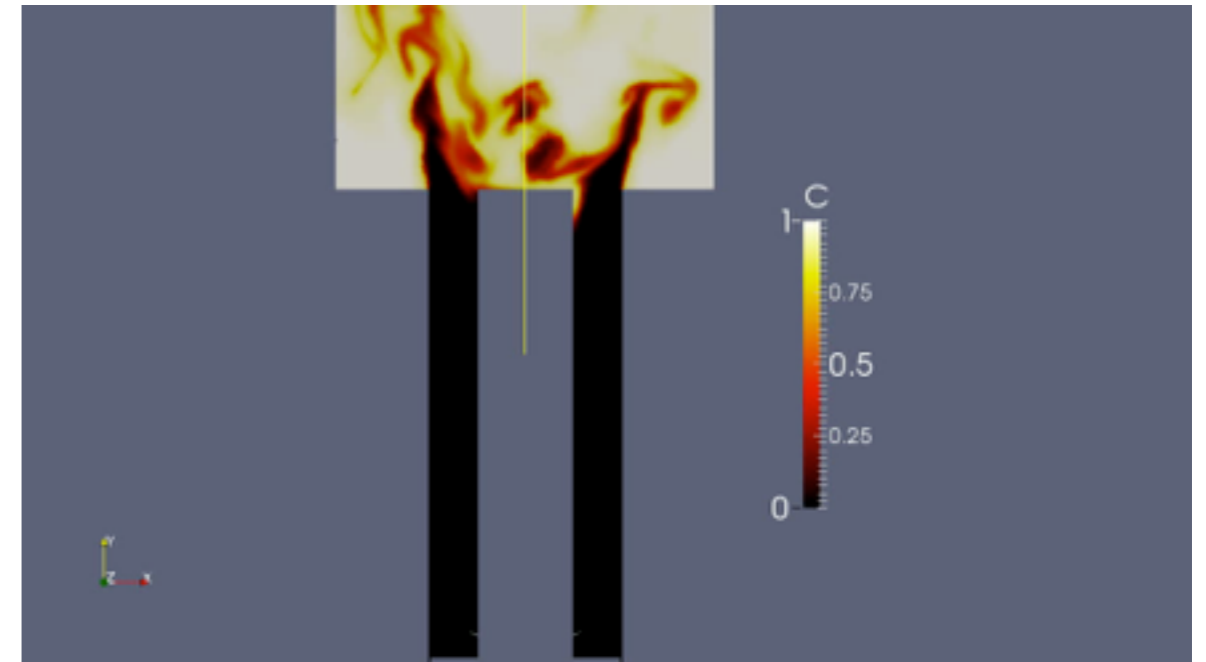
- ➔ 5 bar methane and methane/hydrogen experiments conducted
- ➔ Focus on fuel stratification

- **Understanding model sensitivities**

- ➔ Low-Ma vs compressible flow modeling
- ➔ Effect of stratification on flame structure
- ➔ Numerical modeling of flame structure propagation
- ➔ Open source LES tool for gas turbines

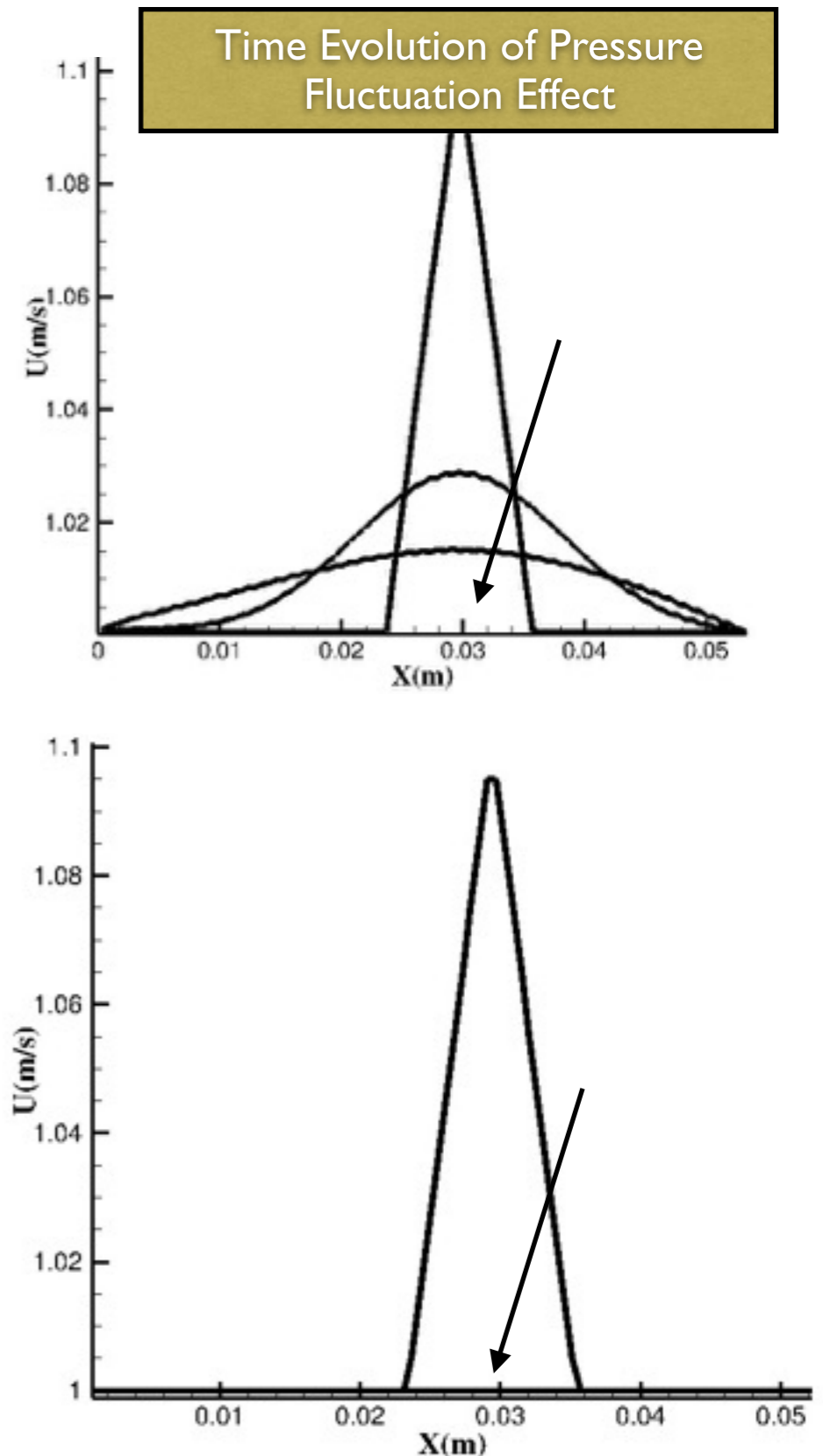
# Flow Laminarization

- **LES solvers based on low Mach number approximation**
  - ➔ Necessary for accelerated calculations in low speed flows
- **Flame propagation affects upstream turbulence more significantly than experiments**
  - ➔ Is there a finite propagation speed of pressure fluctuations?
  - ➔ Leads to laminarization of flow ahead of the flame
- **Are basic flow assumptions not valid in unsteady confined flame motions?**

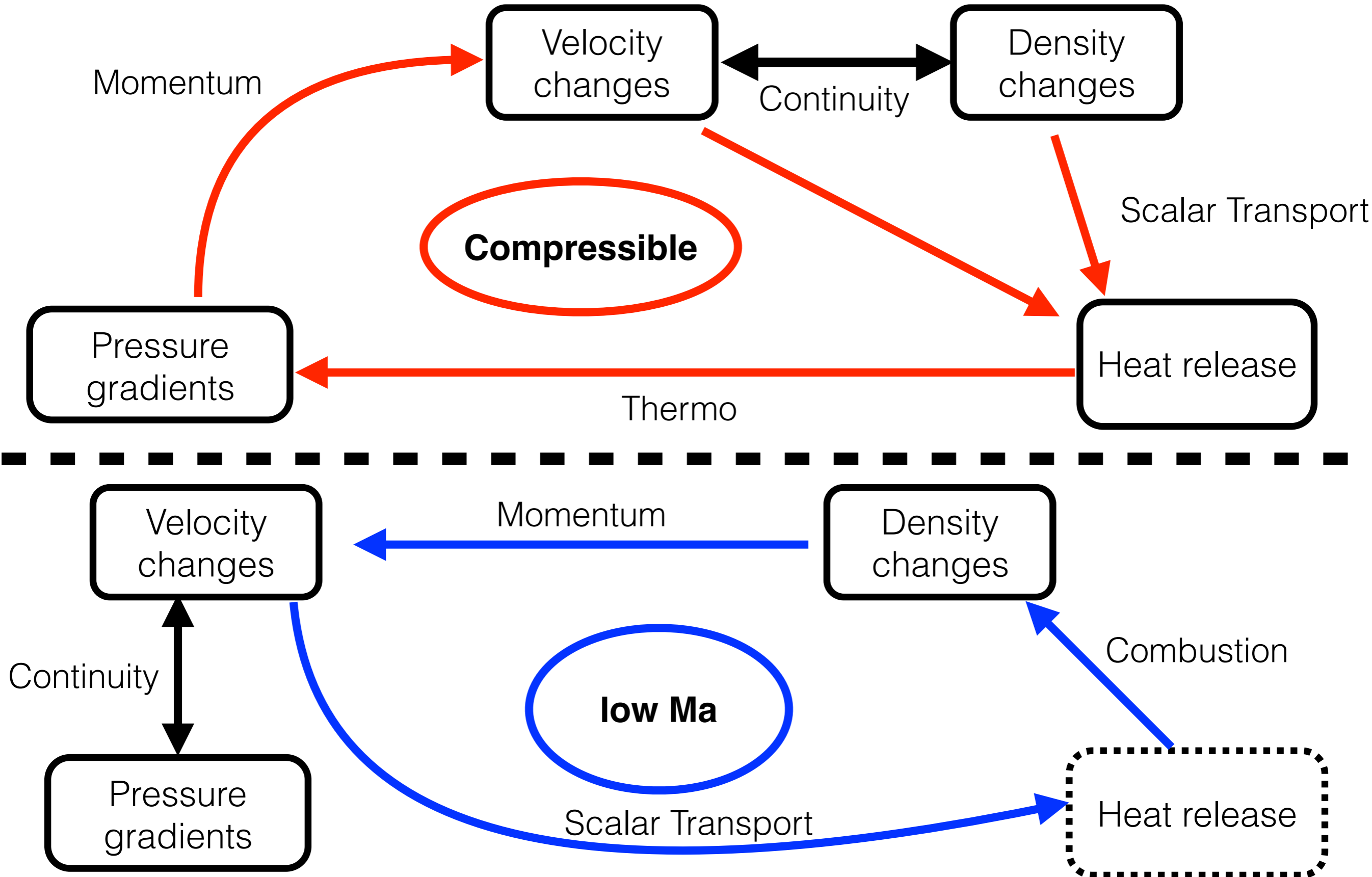


# Effect of Compressibility on Transient Flows

- **Flow governing equations solved in two different ways**
  - ➔ Fully compressible formulation
    - No assumptions regarding compressibility
    - Time step limited by speed of sound
  - ➔ Low Mach number formulation
    - Assume pressure waves propagate at infinite speed
    - Time step limited by local fluid velocity
      - ▶ Ideal for slow but variable density flows
- **Is low Ma assumption valid for transient flashback events?**
  - ➔ Pressure gradients propagate at finite speed changing local flow structure



# Compressible vs Low Mach Number Solver



# Numerical procedure

## Compressible

- 5th order WENO scheme for convection
- 6th order central scheme for diffusion
- BQUICK for scalar

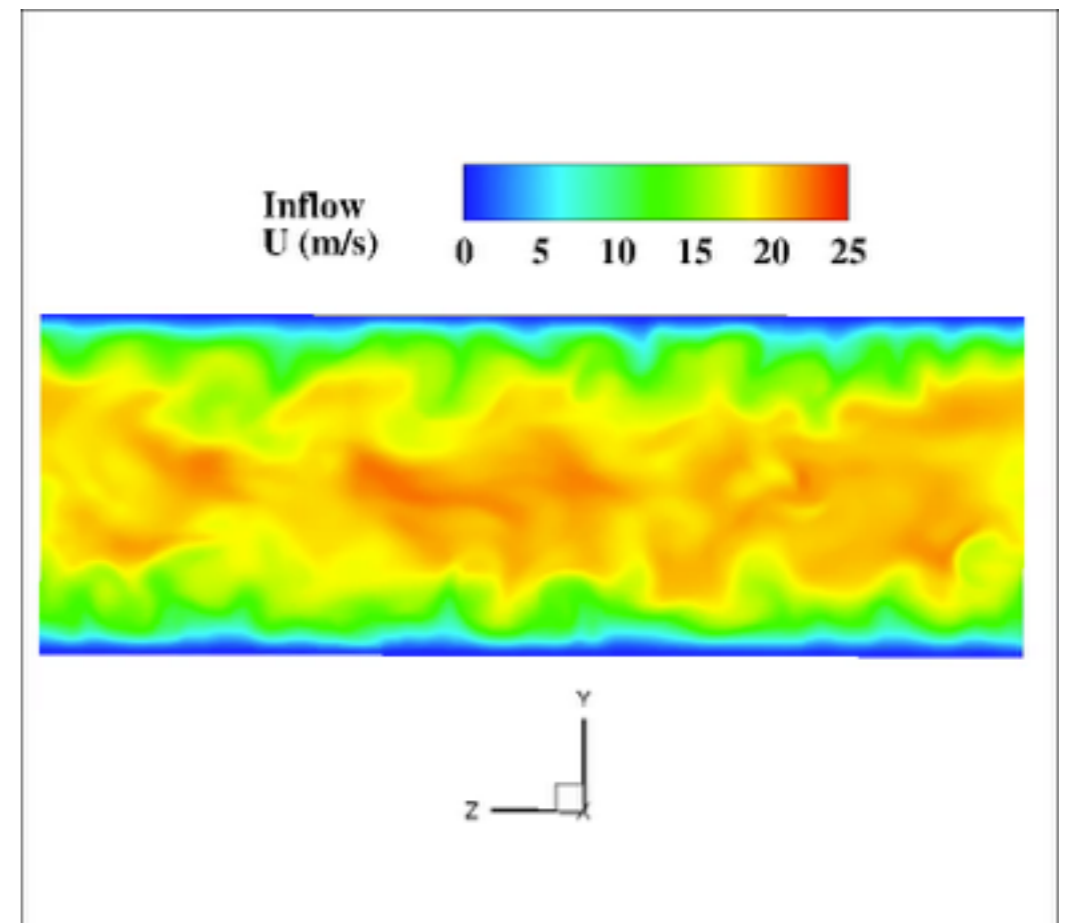
## Low Ma

- 6th order central scheme for convection
- 6th order central scheme for diffusion
- BQUICK for scalar

- **LES with dynamic Smagorinsky model**

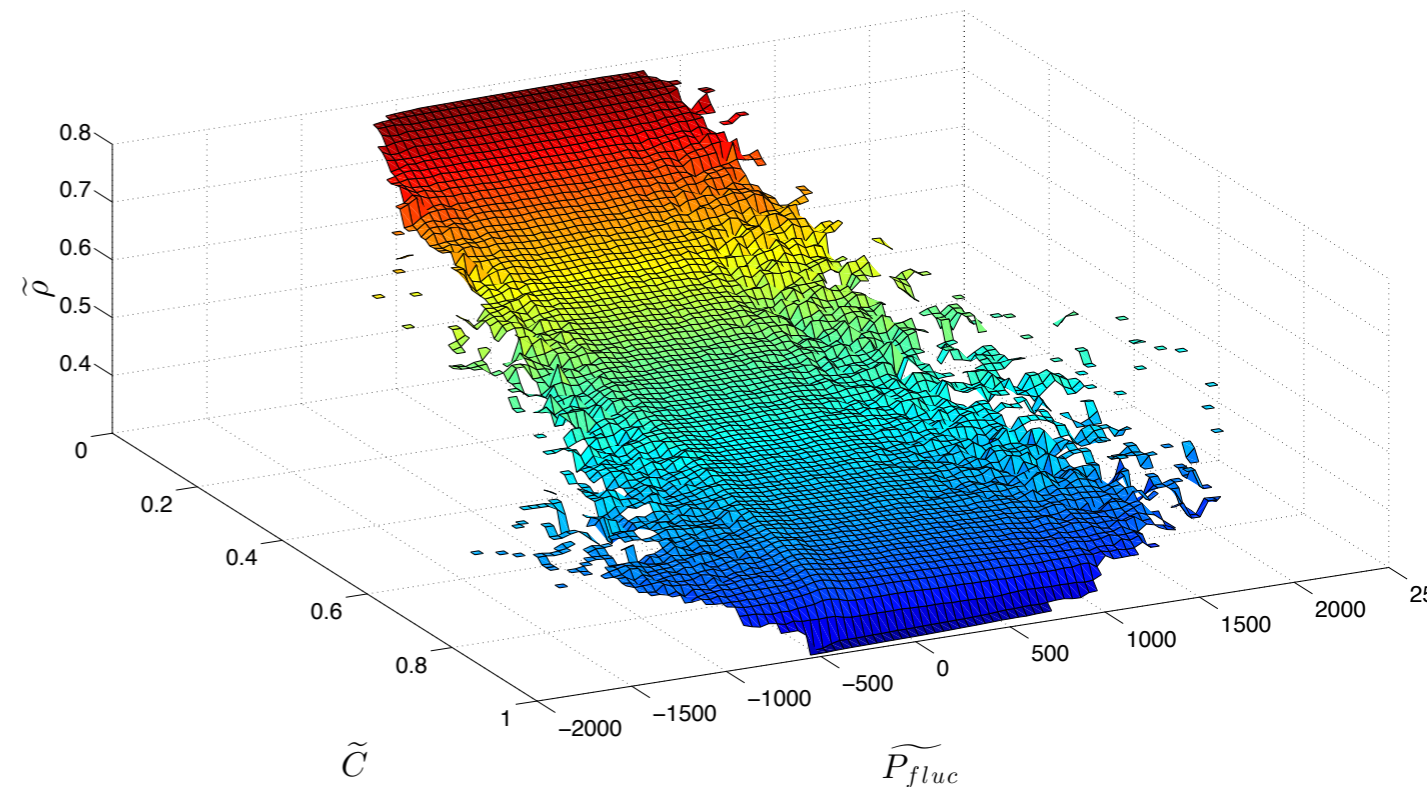
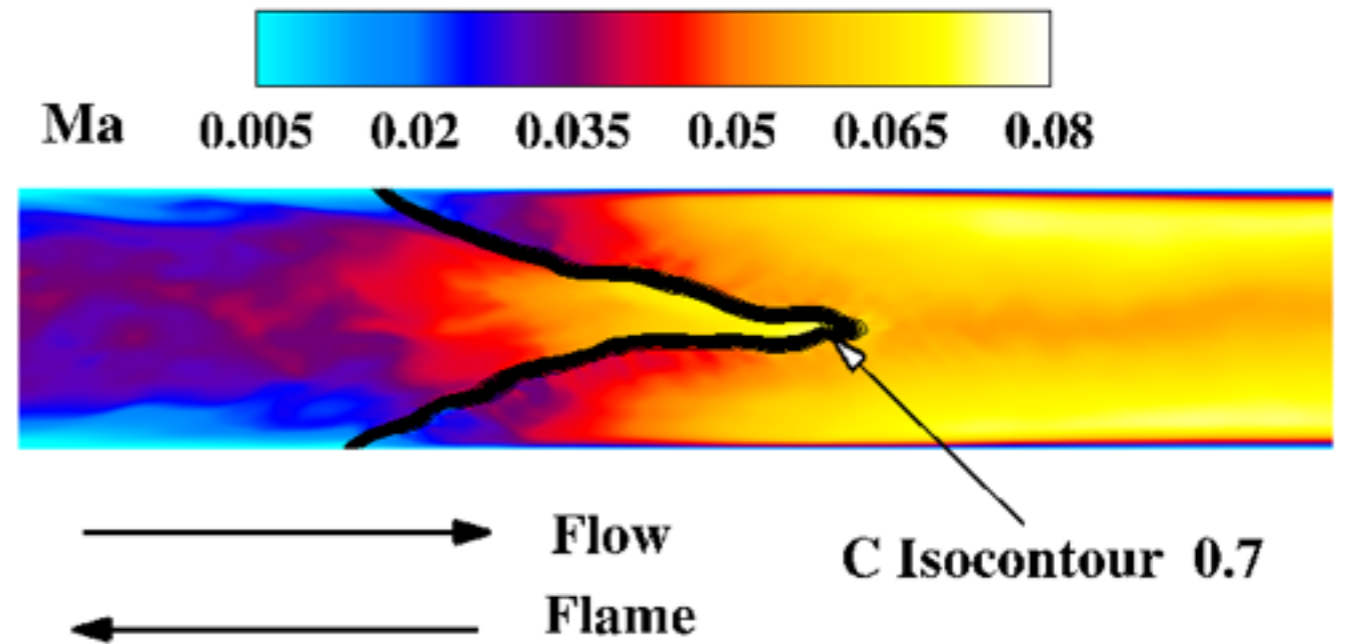
$$\Delta_{LES} = 0.1 \text{ mm}$$

- Kolmogorov length scale  $\sim 0.25 \text{ mm}$
- Laminar flame thickness  $\sim 0.175 \text{ mm}$

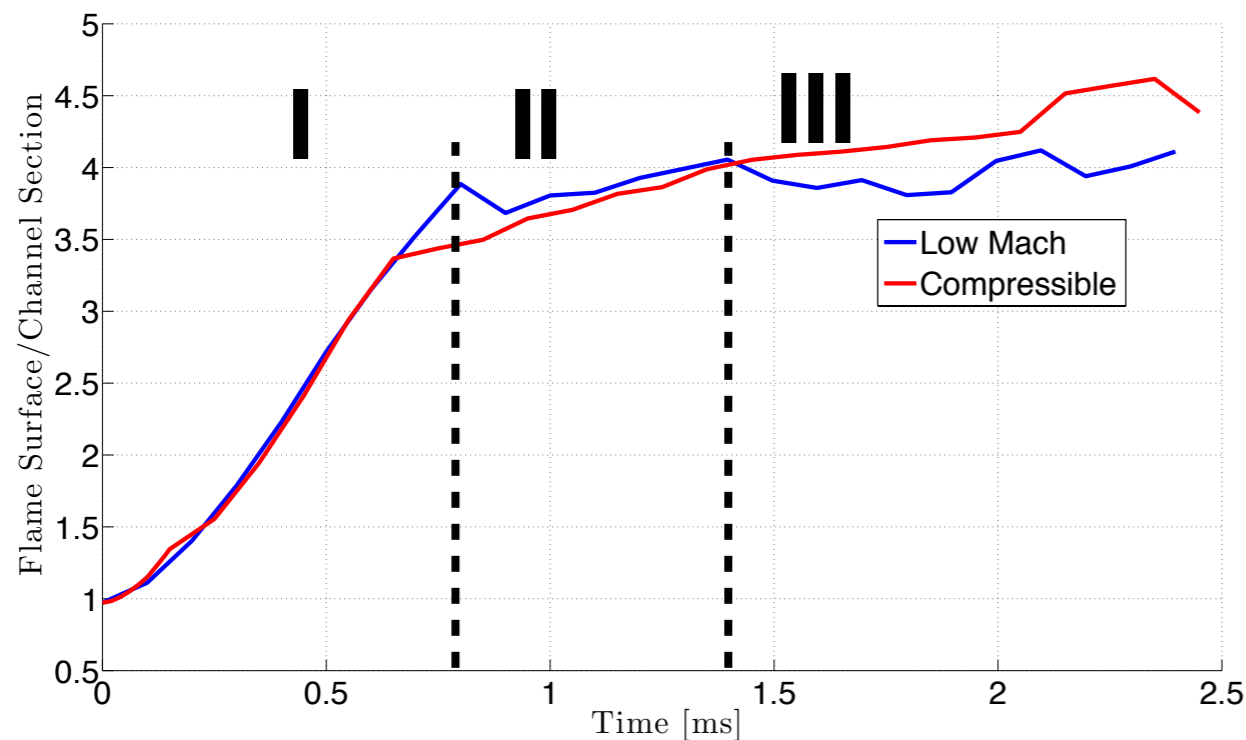
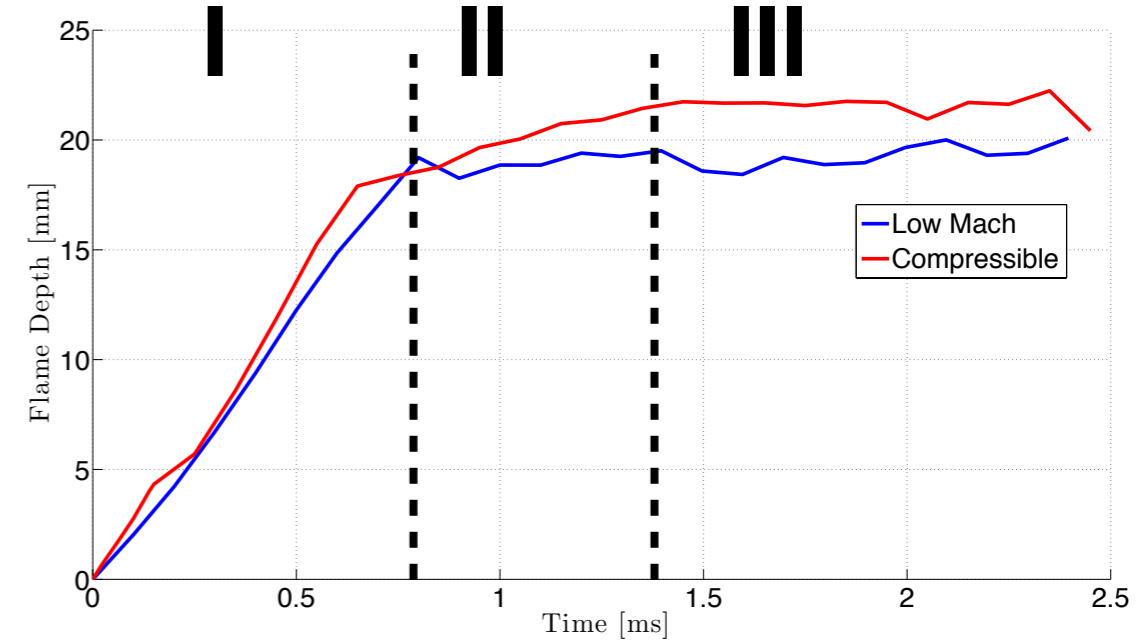
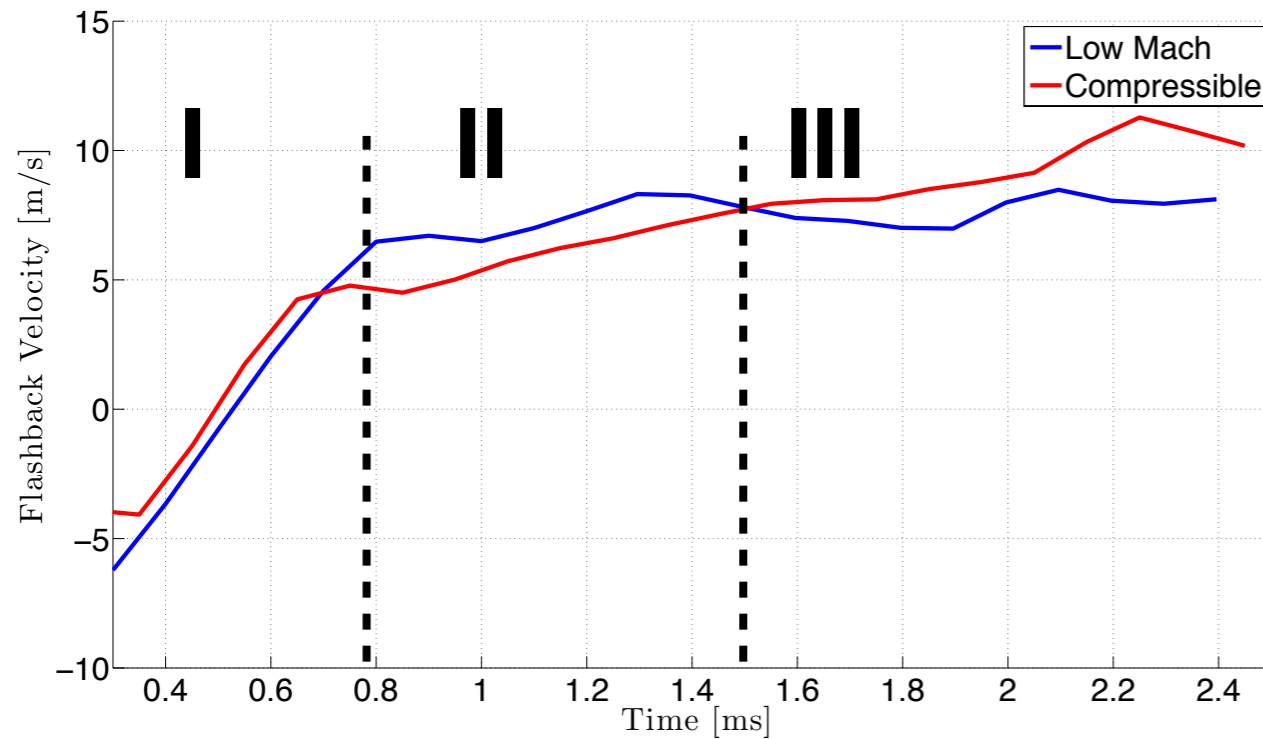


# Compressibility regime

- Ma  $\ll 1$
- Far away from compressible regime
- With the compressible solver :
  - $d\rho = \frac{\partial\rho}{\partial C}dC + \frac{\partial\rho}{\partial P}dP$
  - Two competing phenomena affect density : combustion and dynamic pressure
  - The effect of combustion on density overwhelms the effect of local compression

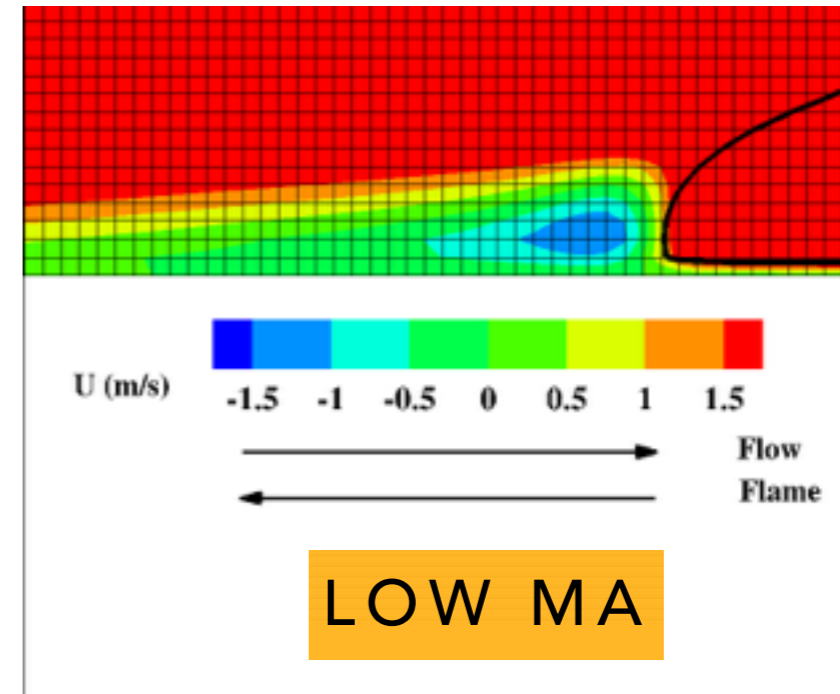
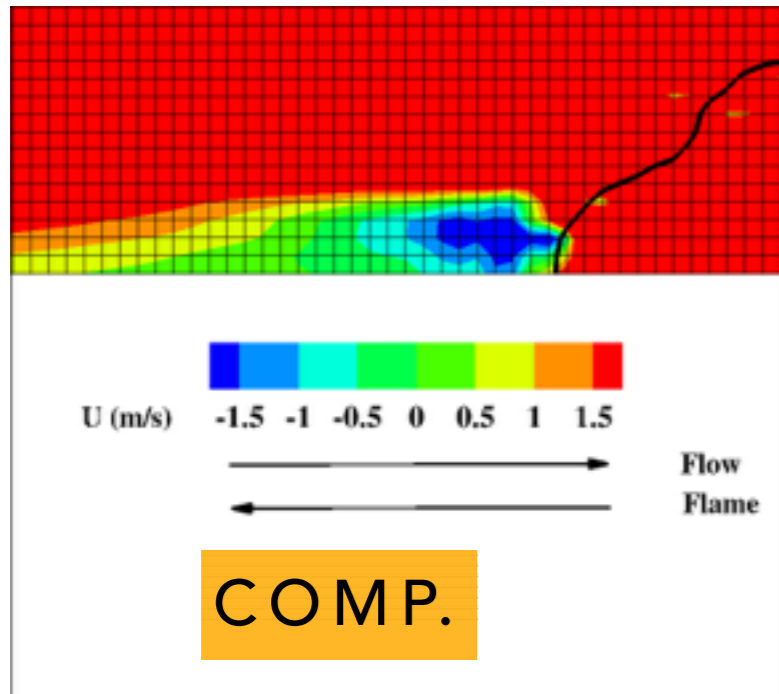


# Differences in Flame Characteristics

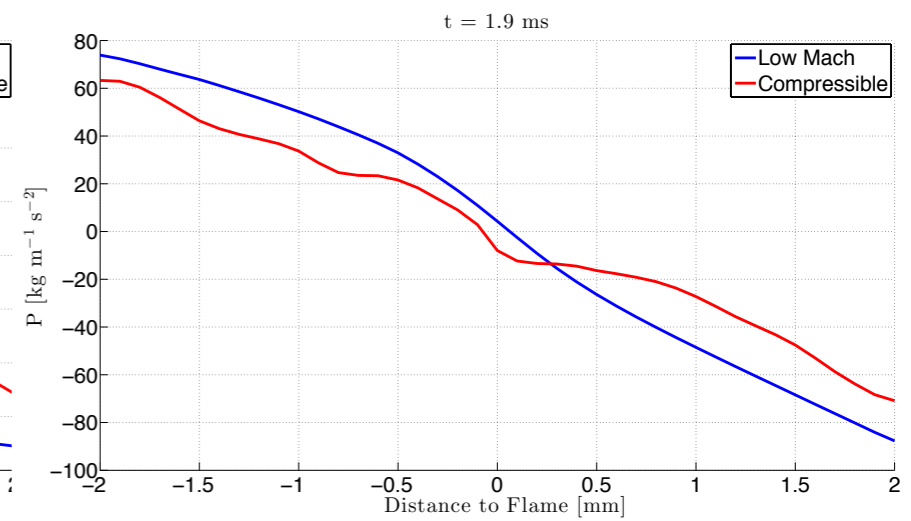
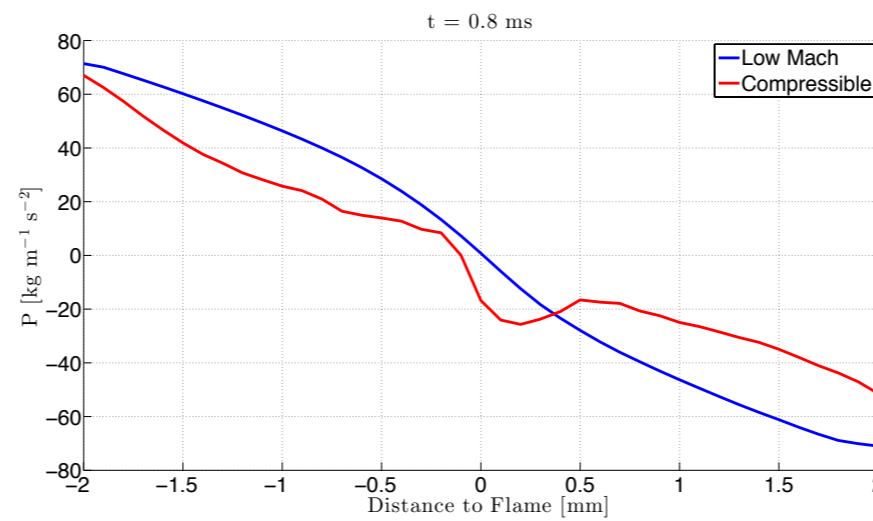
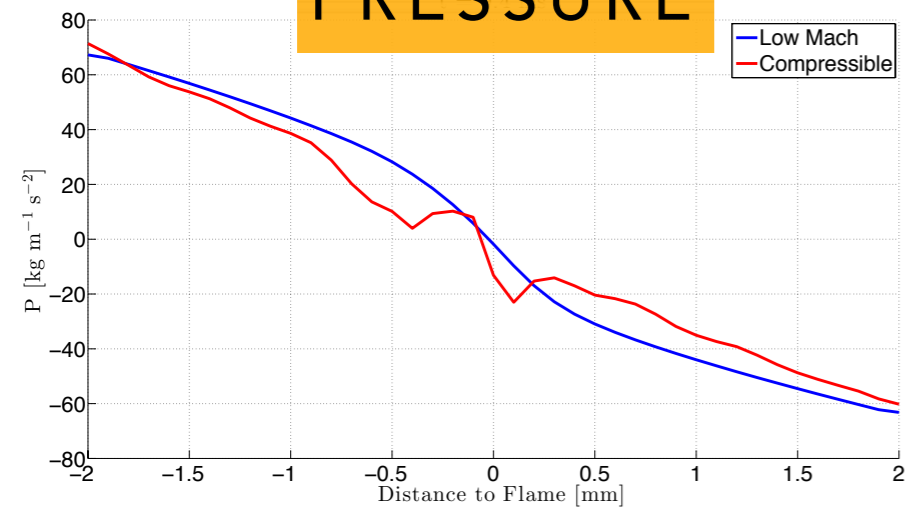


- **Phase I :** Both solvers are very close during the onset phase. The depth stops increasing earlier for the compressible solver leading to a defect in flashback speed.
- **Phase II :** The depth stabilized for the low Ma number solver but keeps on increasing for the compressible solver. Flashback speed recovers. Wrinkling is underestimated.
- **Phase III :** The compressible depth is stable but the flashback speed keeps on increasing. Flame wrinkling is increasing.

# Flame Front Flow Features

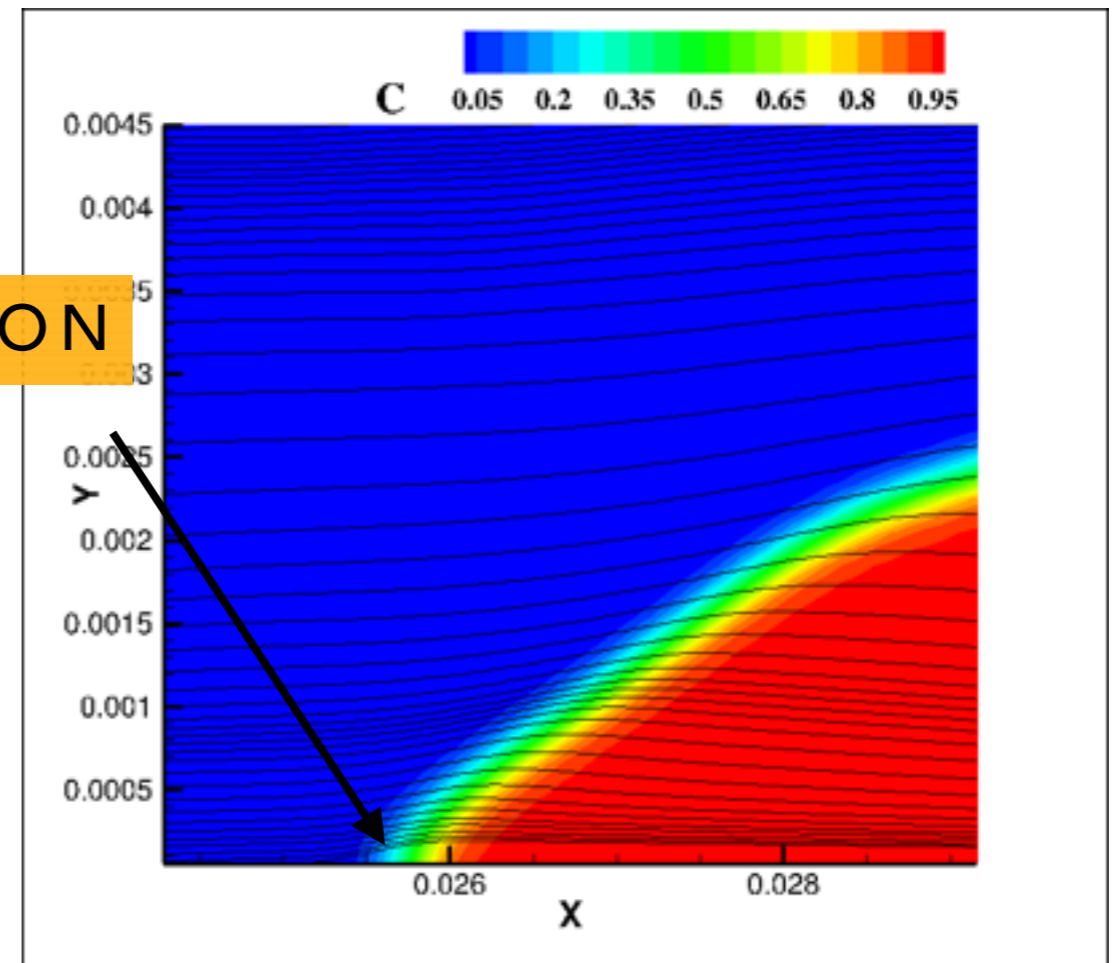
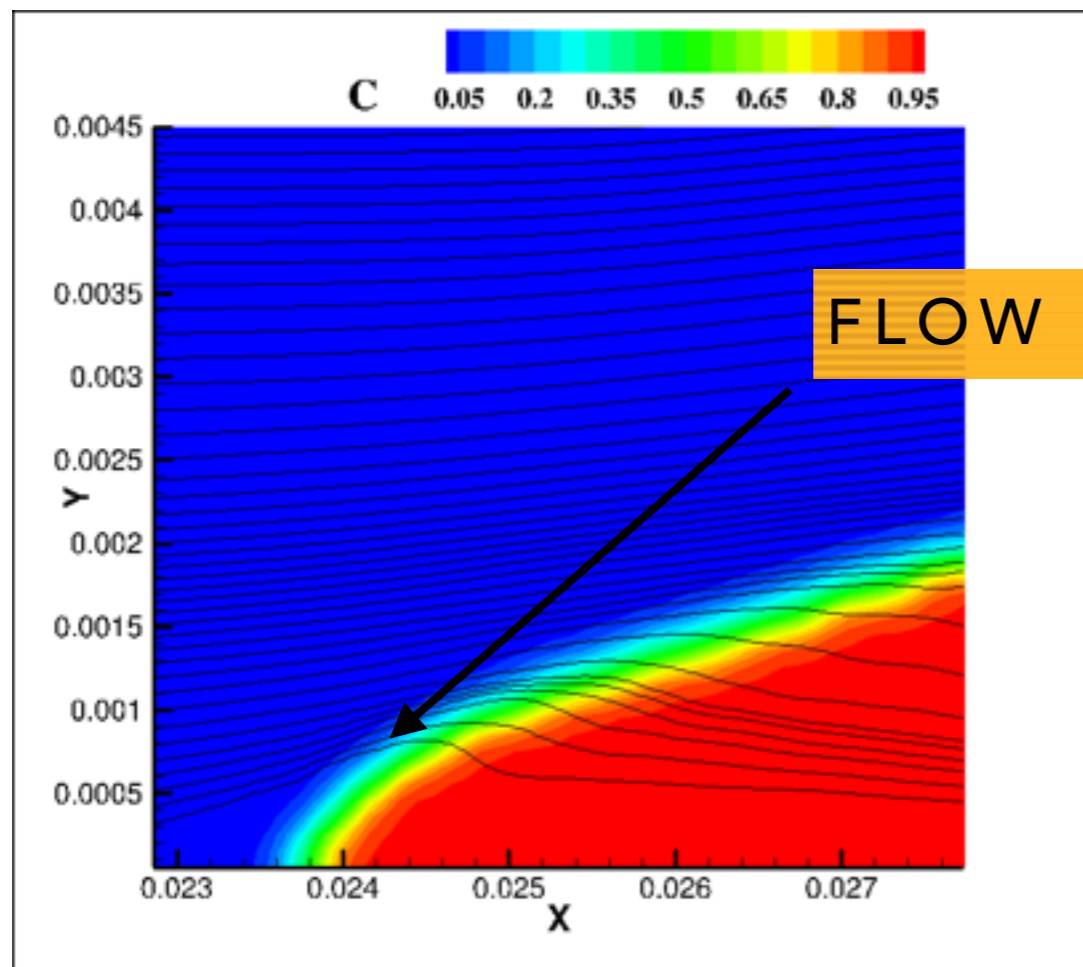
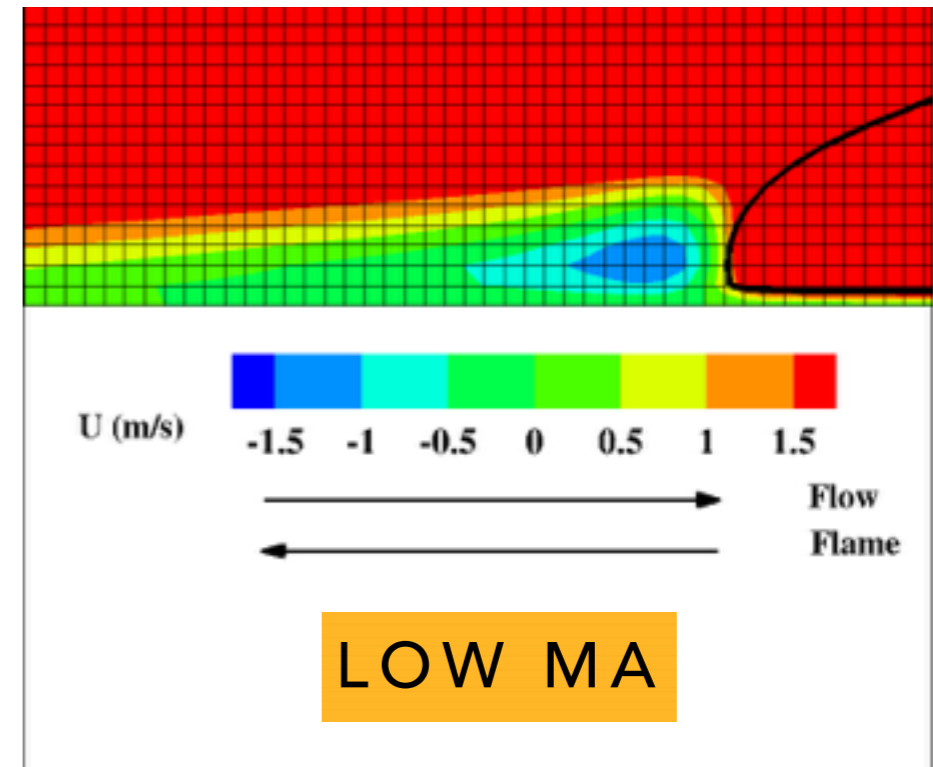
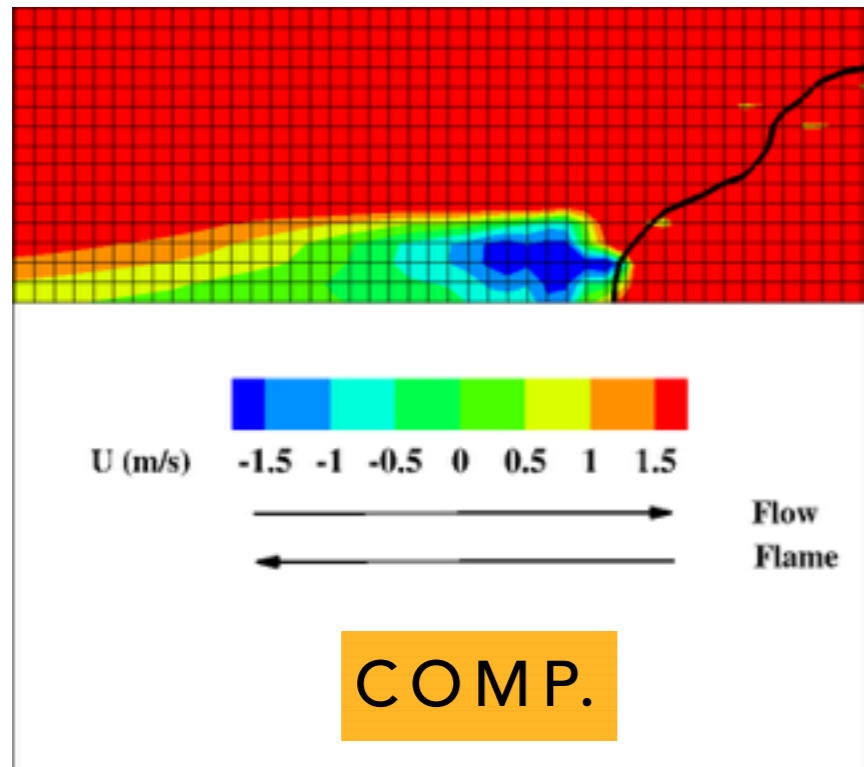


## PRESSURE





# Flame Front Statistics



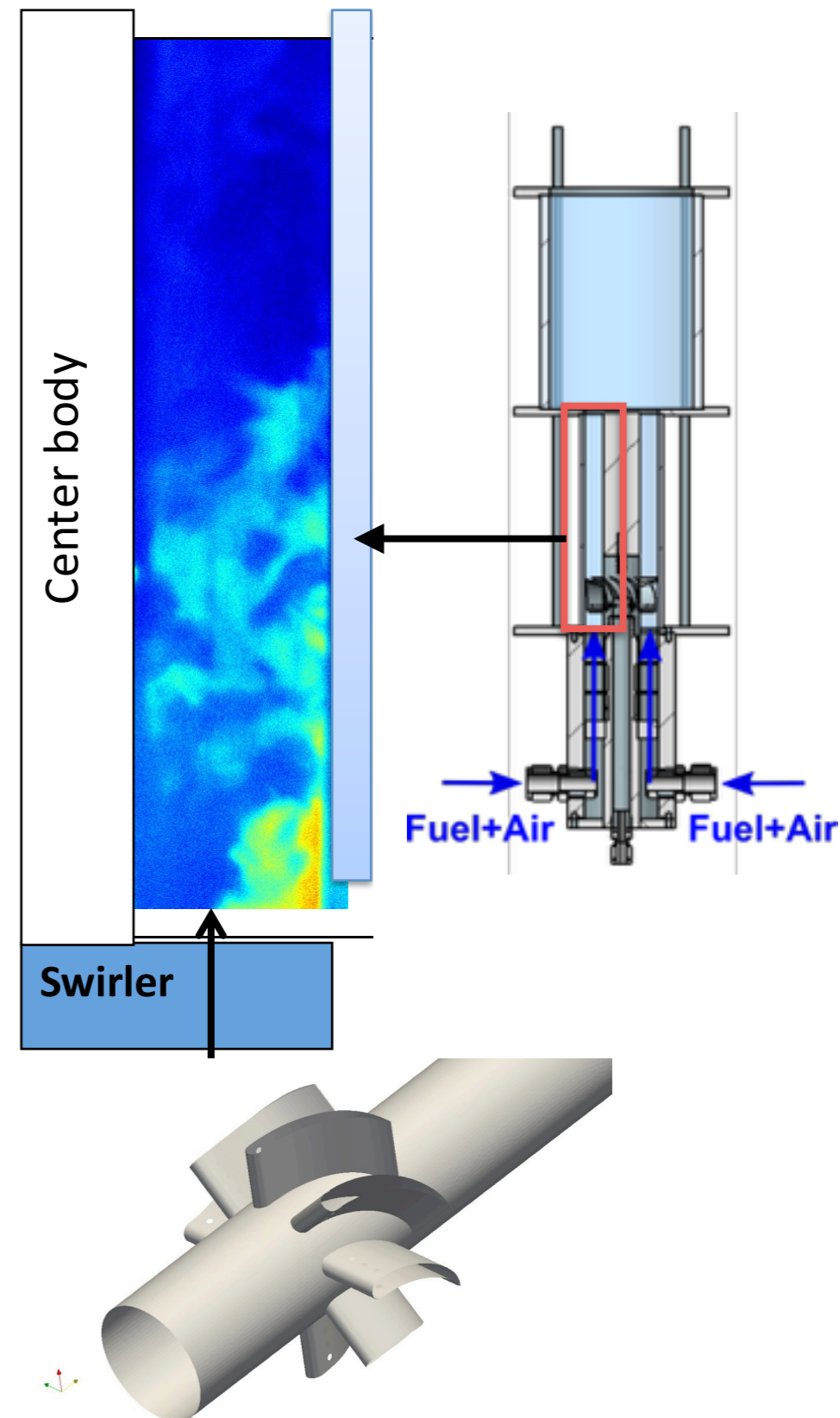
# Conclusions #1

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- **Low Ma version predicts global characteristics**
  - ➔ Differs significantly from compressible formulation
  - ➔ Introduces uncertainty in the results
- **Current plan**
  - ➔ Test low-Ma and compressible solvers for a variety of flashback conditions; estimate differences
  - ➔ Ensure that low-Ma solver is reliable for the range of conditions tested
    - Else, develop compressibility-enhanced versions
      - ▶ One approach is to introduce acoustics-based techniques

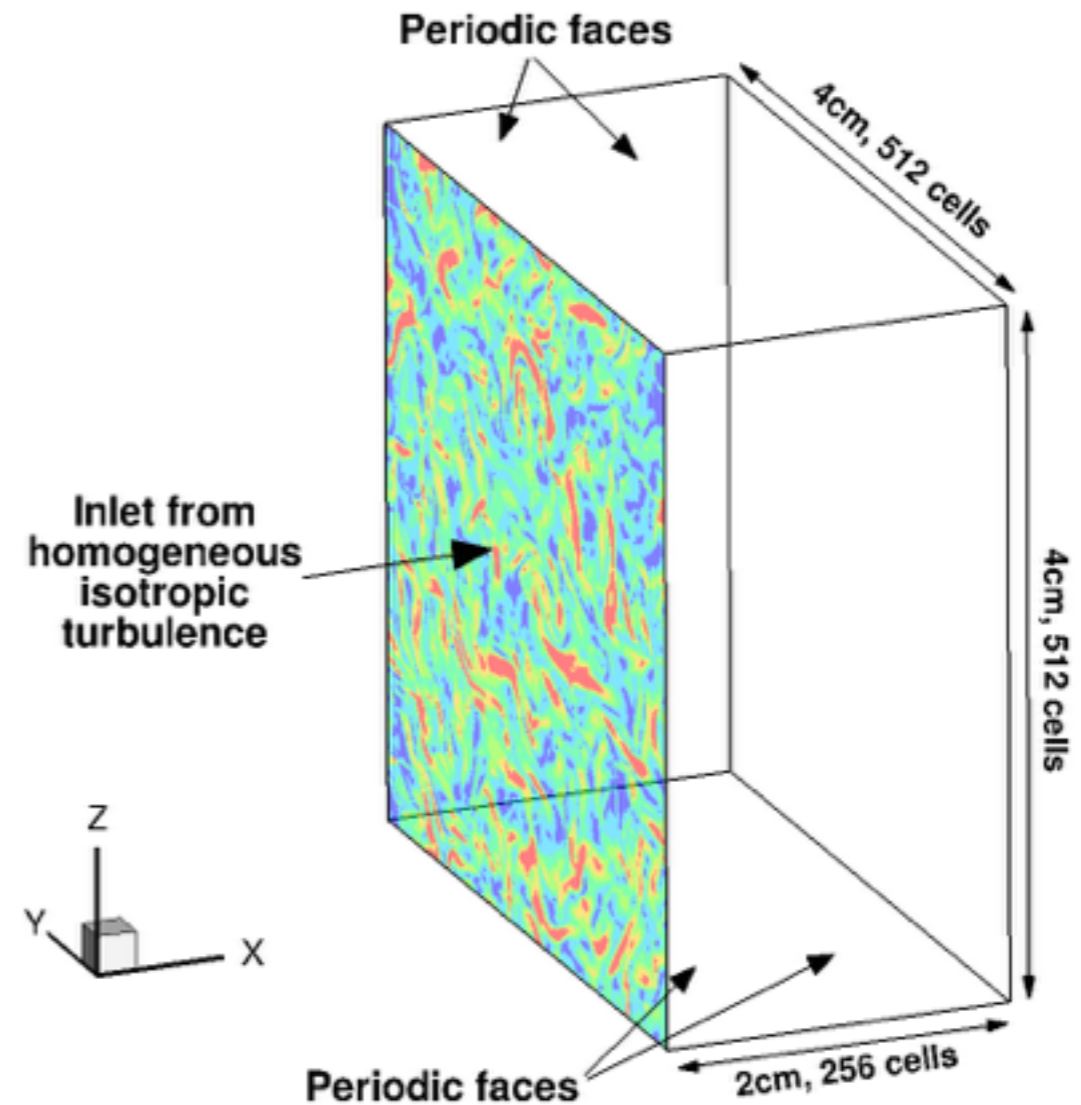
# Effect of Stratification

- **Strategy for flashback control**
  - ➔ Introduce stratification
  - ➔ Leaner mixtures injected near walls
- **How does stratification affect flashback**
  - ➔ Mixture no longer with constant equivalence ratio
  - ➔ Premixed combustion models cannot be used
- **For stratification in gas turbines**
  - ➔ Is the flame structure altered?



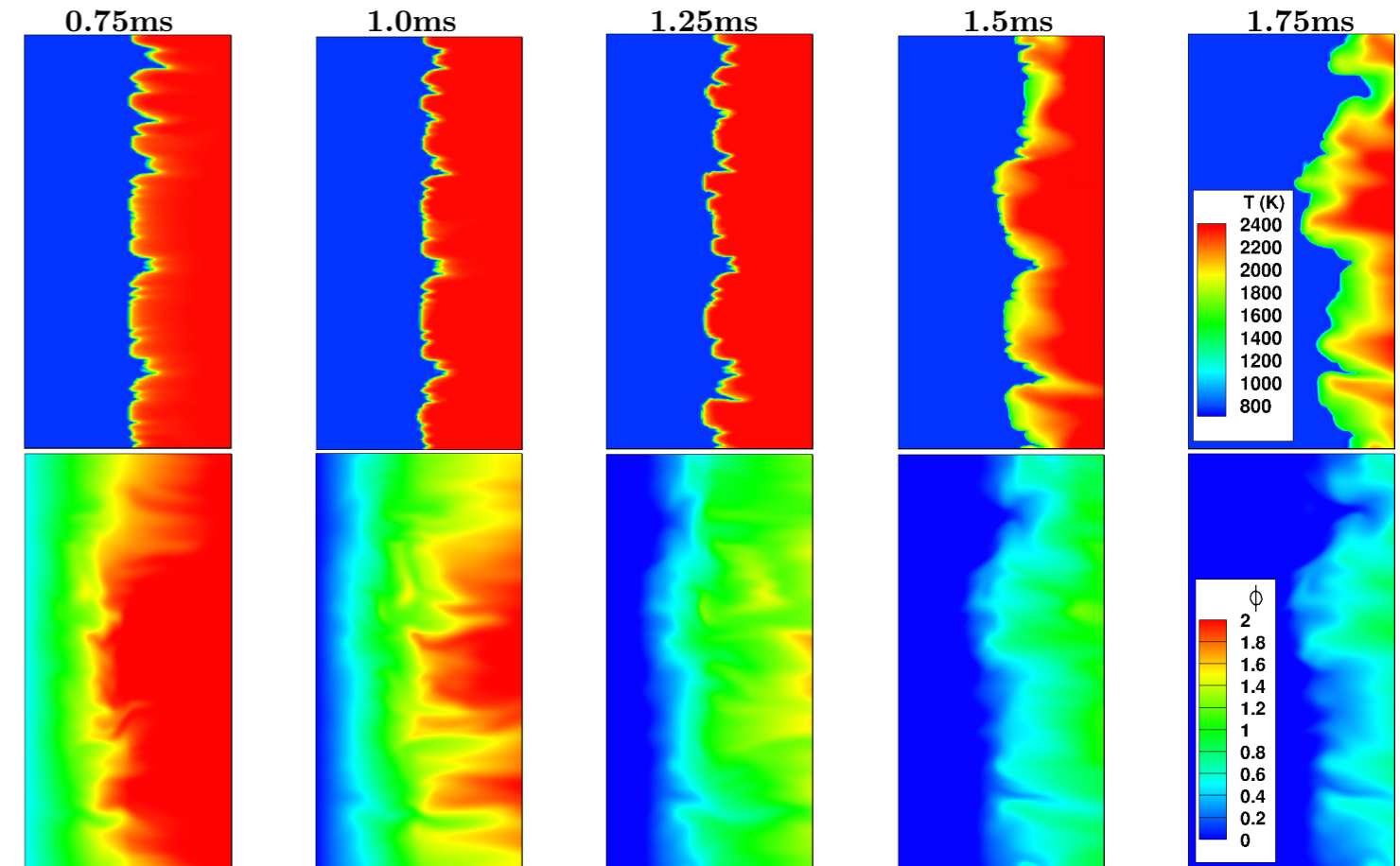
# DNS of Flame in a Box

- **DNS of homogeneous isotropic turbulence with uniform mean flow**
  - ➔ Detailed chemical kinetics
- **Two cases**
  - ➔ Large scale stratification
    - Inflow equivalence ratio varied from 2 to 0 over 3/4 residence time
  - ➔ Small scale stratification
    - Equivalence ratio variations introduced as small-scale structures

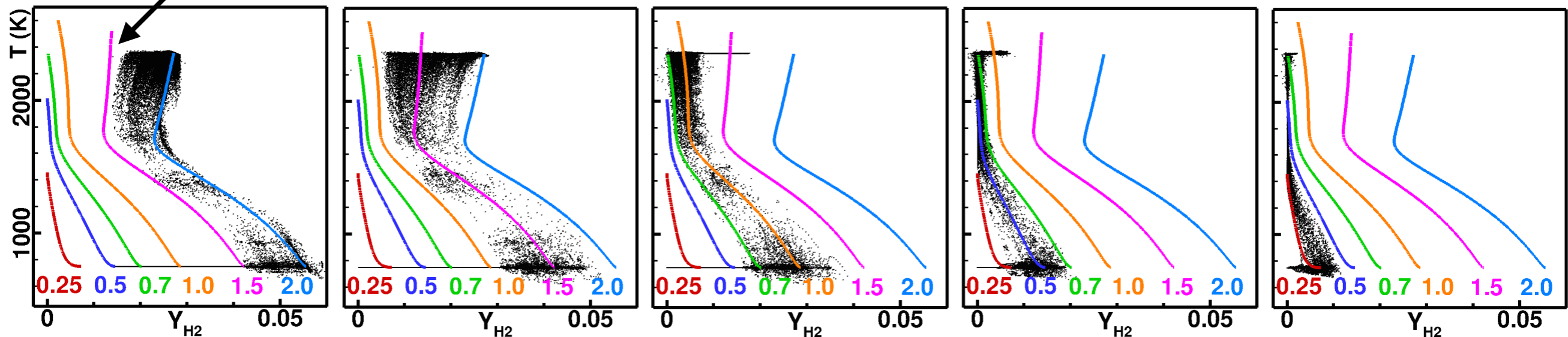


# Large-scale Stratification

- Flame structure a sequence of flamelets
- Equivalence ratio is variation not sufficient to affect flame front

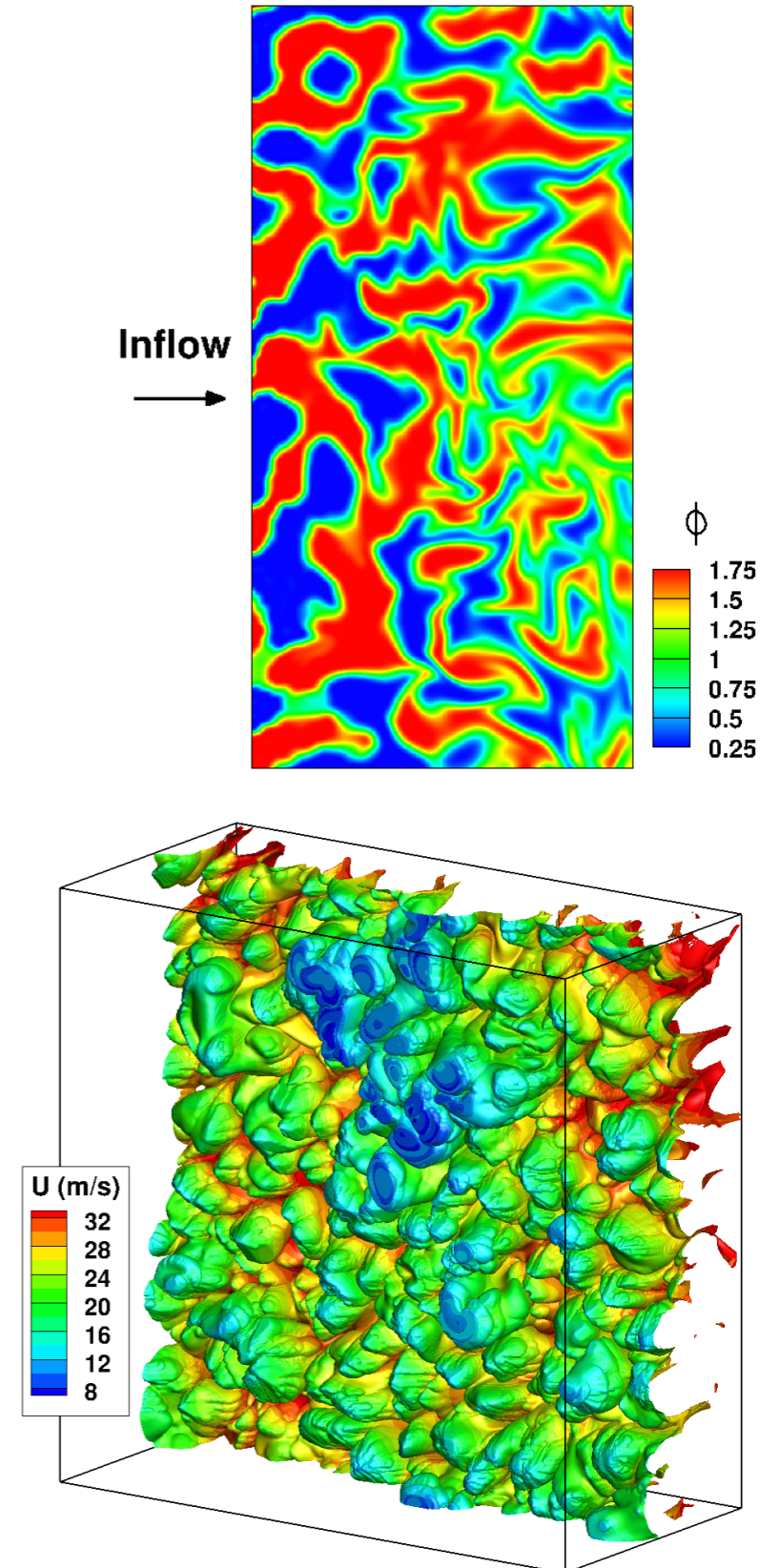
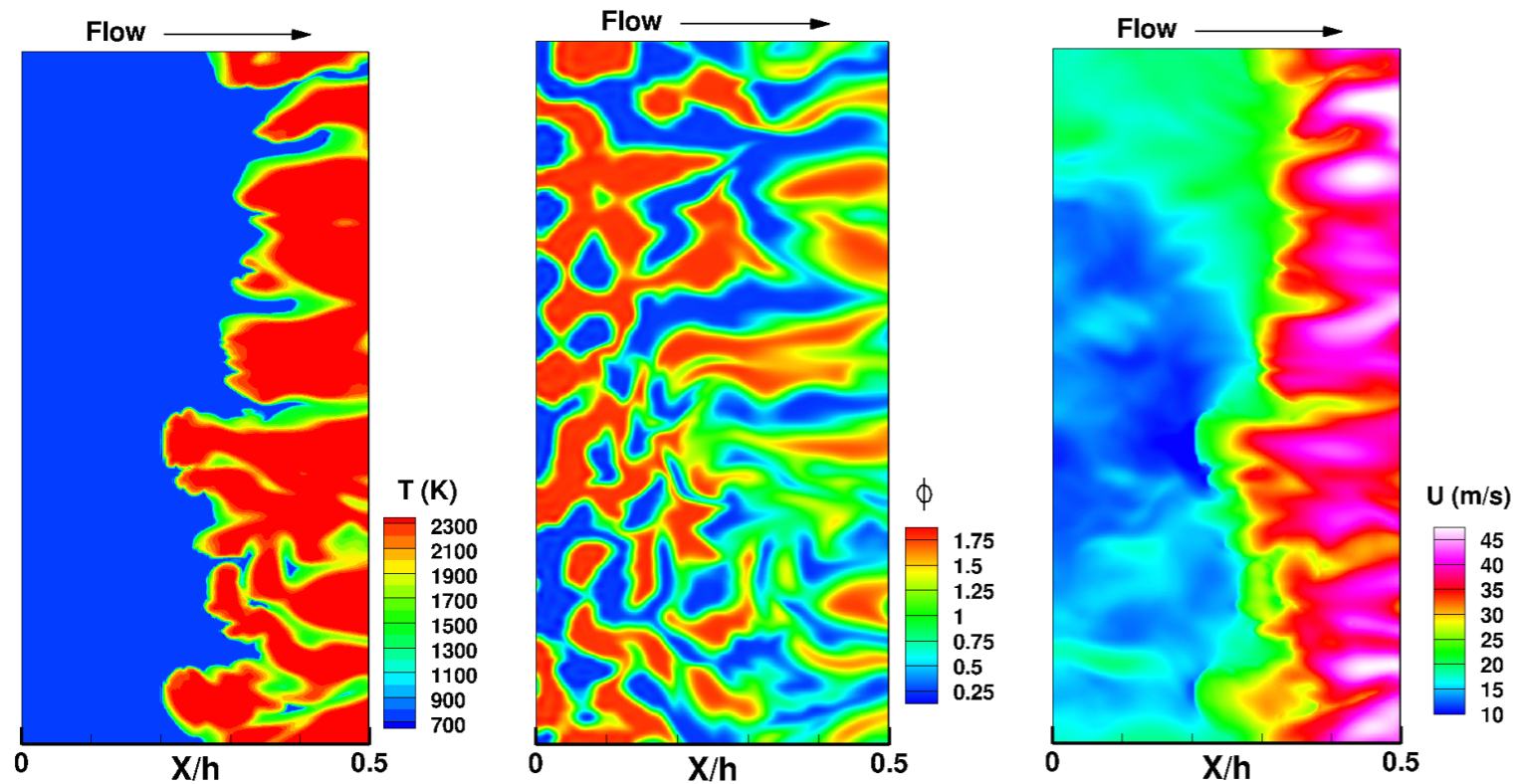


FLAMELET SOLUTIONS



# Small-scale Stratification

- Scalars generated using model spectrum
- Peak energy at 1/12 domain height
- Statistically stationary case



# Conclusions #2

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- **Small-scale stratified flame significantly different**

- Post-flame velocities are lower

- Less flame wrinkling

- Distributed heat release

- **Current plan**

- Complete DNS studies

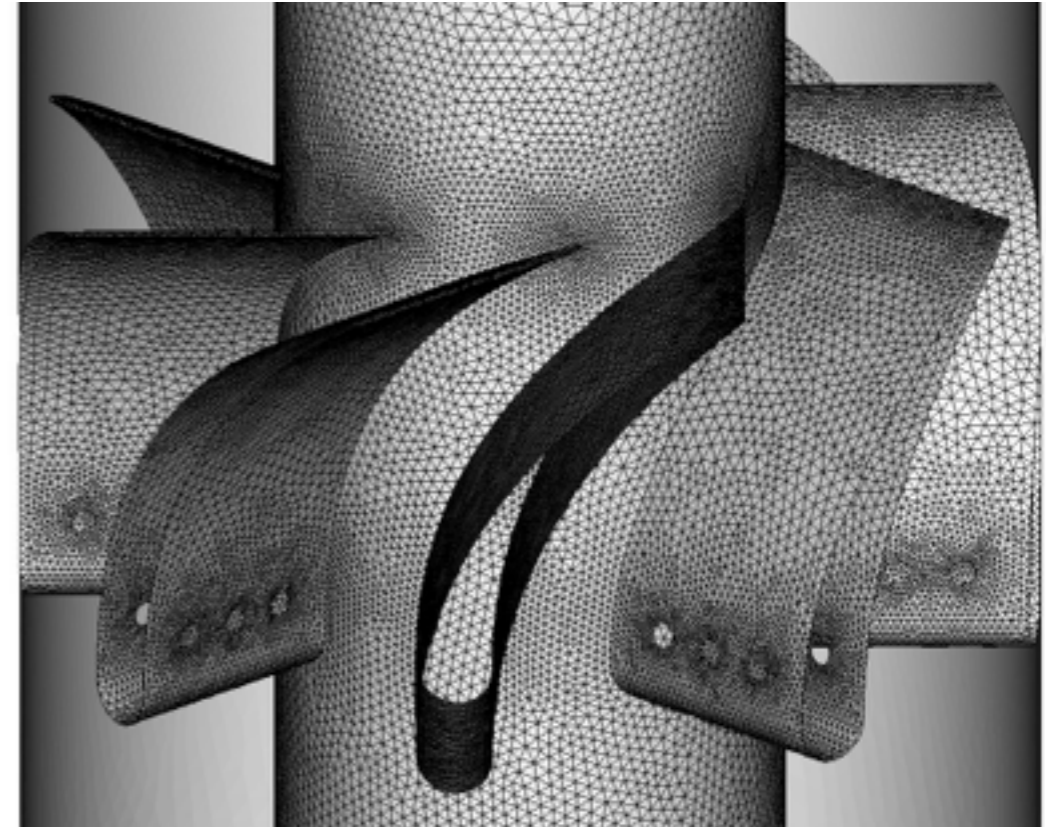
- Establish base line models for stratified mixtures

- Choice between PDF-based approaches or flame-surface based approaches

# Numerical Modeling of Flames

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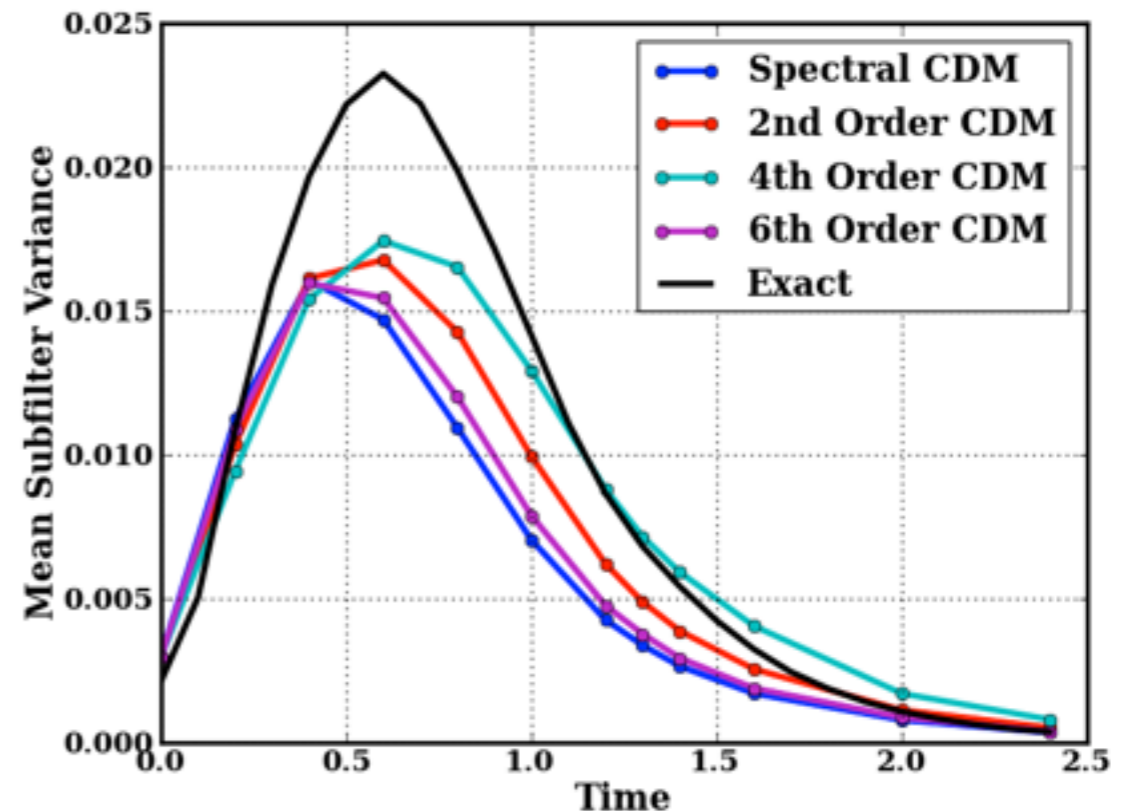
- **LES is the accepted tool for modeling turbulent flames**
- **LES has unique challenges**
  - ➔ Strong interference of numerical method on solution
  - ➔ Grid convergence is all-but-impossible
- **How to mitigate numerical errors?**
- **Current model development procedure**
  - ➔ Relies exclusively on structured grids
    - Toy problems of very little relevance to industry
- **Is there an effect of unsteadiness on model formulations?**





# Numerical Errors in LES

- **LES resolves a range of turbulent length scales**
  - ➔ A spectrum of wavenumbers
- **Numerical methods used to discretize partial differential equations**
  - ➔ Assume smooth underlying flow field
    - Not correct for turbulent flow
    - Introduces errors
  - ➔ Numerical errors scale with wavenumber
    - Highest errors at filter scale
    - Contaminates numerical solution
    - Can lead to counterintuitive behavior



# Flame Surface Models

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- **For premixed combustion at moderate Reynolds numbers**
  - ➔ Flame surface models are reasonable
  - ➔ The motion of flame surface is treated using a single field variable
    - G (level-set) variable or progress variable
- **Level set approach**
  - ➔ Numerically better suited for predicting flame surface
    - However, encounters flame volume loss
  - ➔ Difficult to transition to stratified combustion models
- **Approach used here: Progress variable description**

# Progress Variable Approach and Flashback

- **Transport equation for C**

$$\frac{\partial \rho C}{\partial t} + \nabla \cdot (\rho U C) = \nabla \cdot (D(C) \nabla C) + \dot{\omega}(C)$$

- ➔ Filtered; Leads to unclosed terms; Need modeling

- **Models for chemical source term**

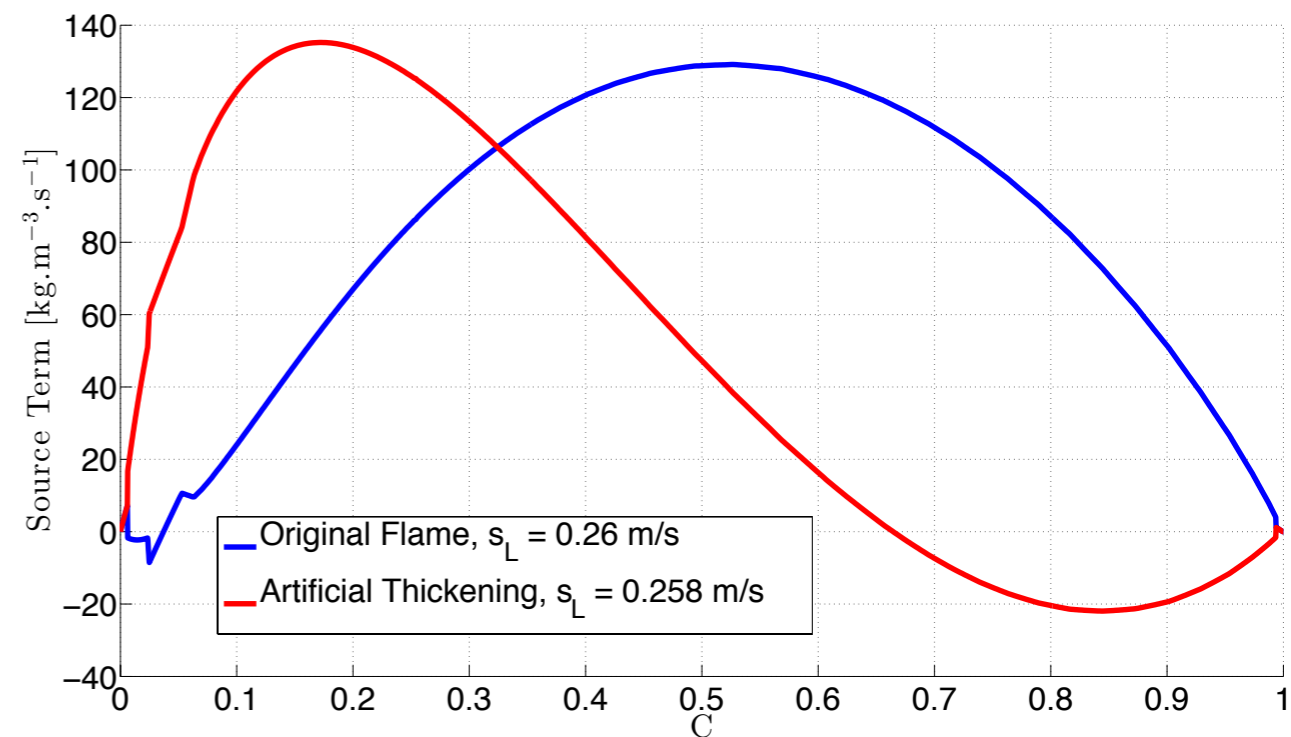
- ➔ Require underlying flame structure

- **LES problem**

- ➔ Imposed flame structure is not maintained as simulation proceeds

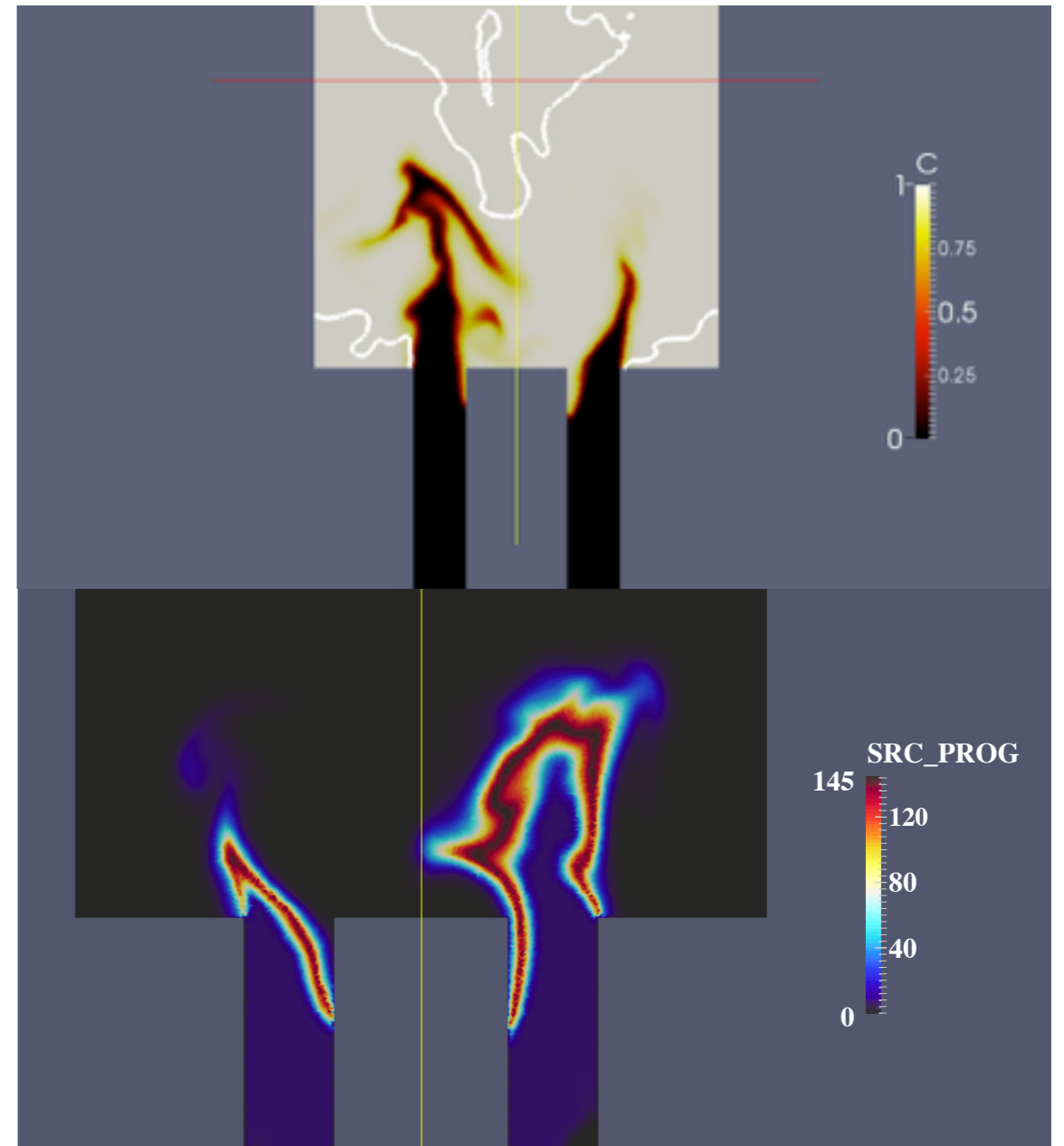
- ➔ Not a big issue for steady-state problems

- ➔ Unsteady flashback accumulates these errors over time



# Flame Thickness

- **Model closures use two different terms**
  - ➔ Imposed flame thickness ( $L$ ) and source term
  - ➔ Product is proportional to consumption speed
- **Counter-intuitive LES behavior**
  - ➔ Flame thickness is reduced with time
    - Leads to reduced burning rate
    - Arrests flashback



# Structure-Preserving Reaction Model

- **Treat progress variable discretely (in space and time)**

$$C(t + \Delta t) = C(t) + f(C, u)$$

- **Introduce time-dependent translation**

$$F : C(x, t) \rightarrow \widetilde{C}(x, t) = C\left(x - \left(\frac{\rho_0 s_L t}{\rho(C)} - \frac{1}{\rho(C)} \int_0^t \rho u(t') dt'\right), t\right)$$

- **We require the distribution of  $\widetilde{C}(x, t)$  to be independent of time**

- **Introduces numerical flame structure**

$$f(x, t) = \left(\frac{\rho_0 s_L}{\rho(x, t)} - \frac{1}{dt} \int_t^{t+dt} u(t') dt'\right) \frac{\partial \widetilde{C}}{\partial x}$$

- **Guarantees constant local flame speed; Enables consistent flame thickening**

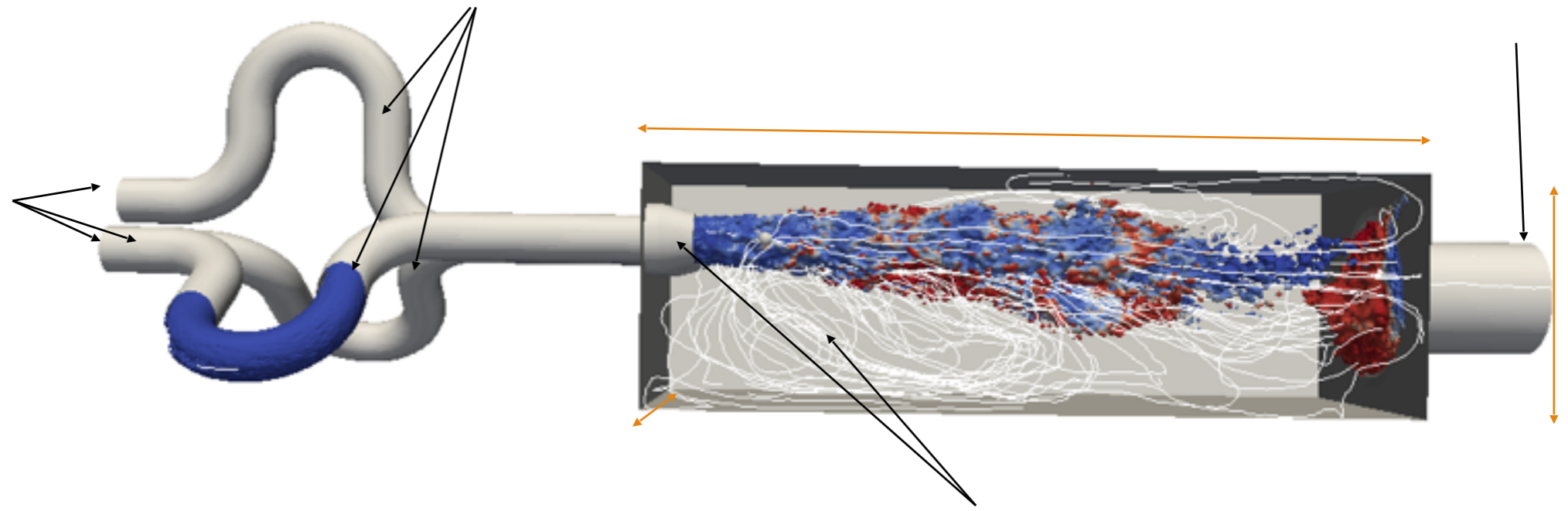
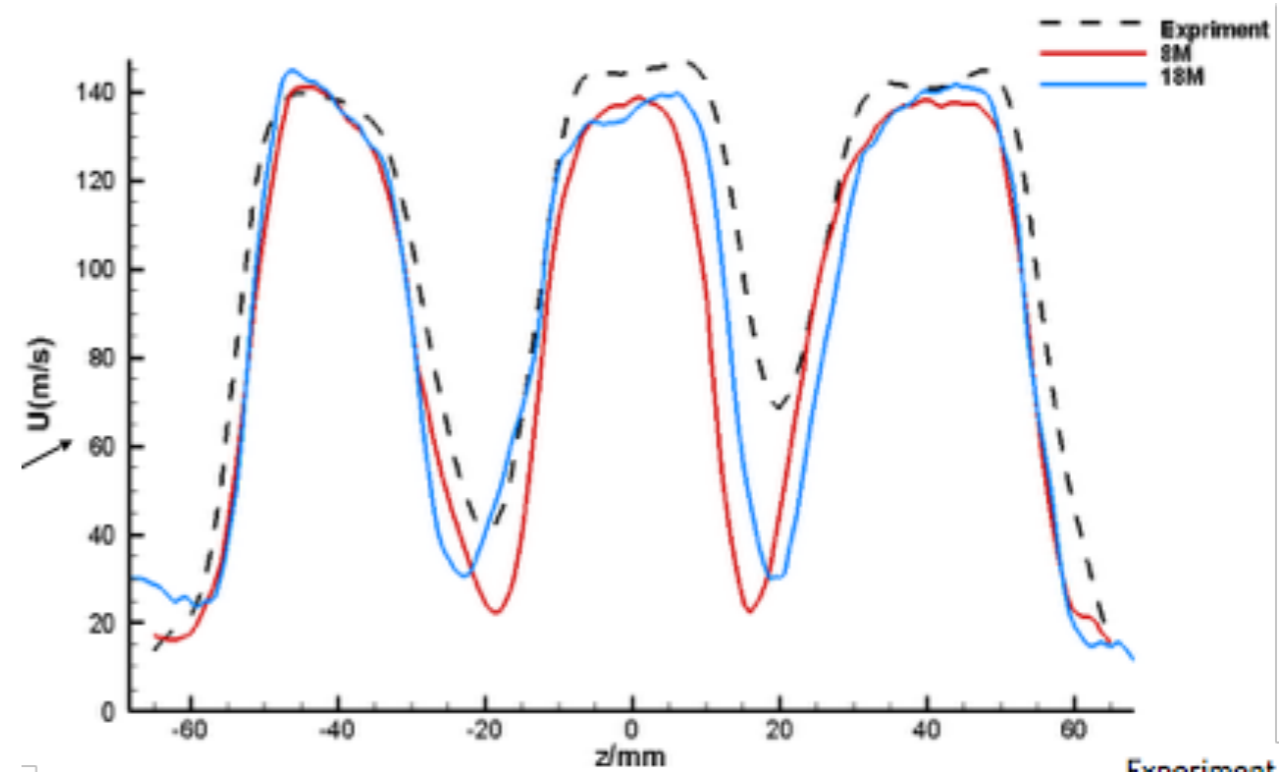
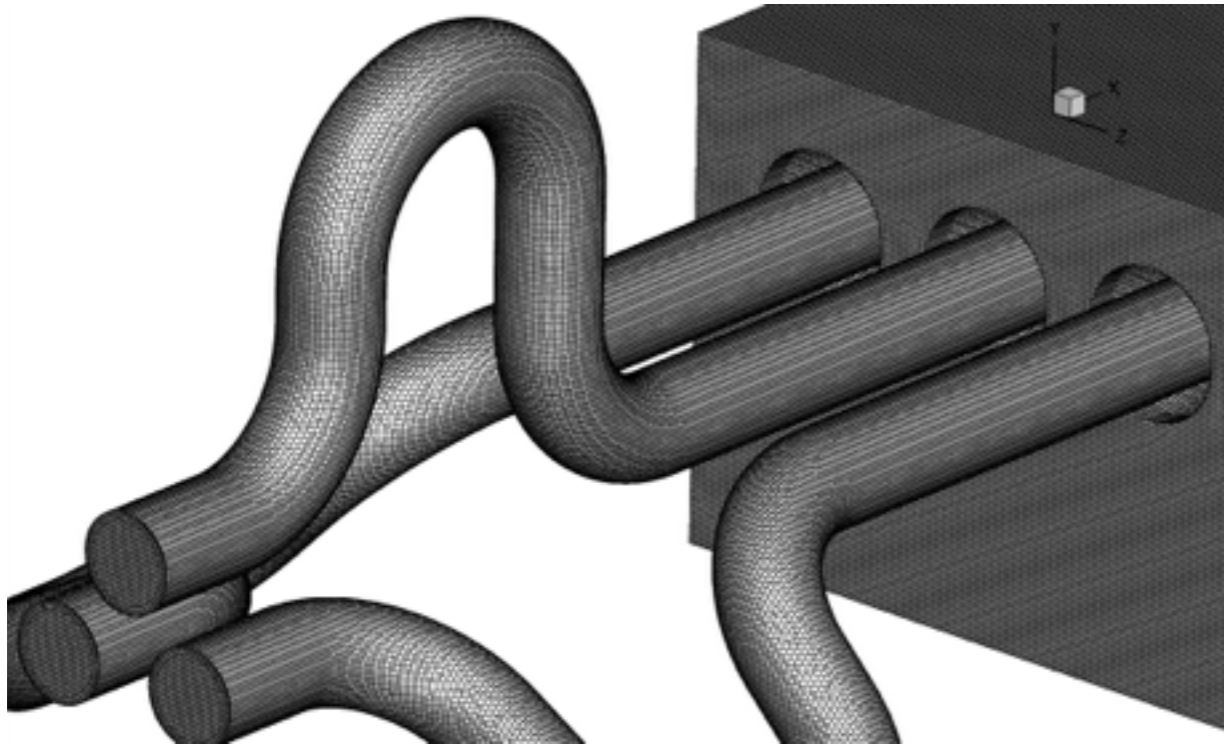
# Open Source Gas Turbine Software Platform

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- **Integral part of the flashback model project**
- **Enable rapid dissemination of results**
- **Prior collaboration with Siemens**
- **Currently working with Oregon State, Iowa State, KAUST, UT Austin, and Princeton on enhancing capabilities**
- **Progress in last year**
  - ➔ All models implemented in OpenFOAM
  - ➔ Minimal kinetic energy dissipation enforced

# Siemens DLR 3-jet Combustor

- Lean combustion with heat loss



# Next Steps

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- **Develop structure-preserving reaction model**
  - ➔ Implement and validate using UT swirler data and legacy data (Darmstadt)
- **Develop stratified combustion model with heat loss**
  - ➔ Conduct DNS to evaluate flame structure
  - ➔ Identify model formulations
- **Fuel effects at high pressure**
  - ➔ Identify the role of differential diffusion, and fuel composition on boundary-layer/flame interaction
    - Experiments and DNS data