



# An Experimental and Modeling Study of NO<sub>x</sub>- CO Formation in High Hydrogen Content (HHC) Fuels Combustion in Gas Turbine Applications (DE-FE0012005)

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**2015 University Turbine System Research Workshop**  
**Atlanta, GA**

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# Project Participants



## University of South Carolina and Princeton University

**PI: Dr. Tanvir Farouk, Assistant Professor**

University of South Carolina– Mechanical Engineering

- **Sheikh Farhan Ahmed** – Graduate Student
- **Fahd Ebna Alam** – Graduate Student

**Co-PI: Dr. Bihter Padak, Assistant Professor**

University of South Carolina– Chemical Engineering

- **Nazli Asgari** – Graduate Student



UNIVERSITY OF  
**SOUTH CAROLINA**

**Co-PI: Dr. Frederick Dryer, Professor**

Princeton University – Mechanical and Aerospace Engineering

- **Mac Haas** – Technical Staff
- **Fahd Ebna Alam** – Visiting Researcher (8 mos)



**PRINCETON**  
UNIVERSITY

- Detailed and validated coupled HHC + NO<sub>x</sub> kinetic model
- New experimental speciation data for the oxidation kinetics of HHC fuel compositions in presence of impurities.
- Understanding of CO, NO and NO<sub>2</sub> formation and interactions in shear layer flow regimes (hot and cold flow interactions). NO - NO<sub>2</sub> conversion in hot-cold shear layer interaction and EGR.
- Detailed and reduced kinetic models for HHC fuels including detailed fuel compositions and NO<sub>x</sub>.



***Improved, higher fidelity tools for engineering design!***

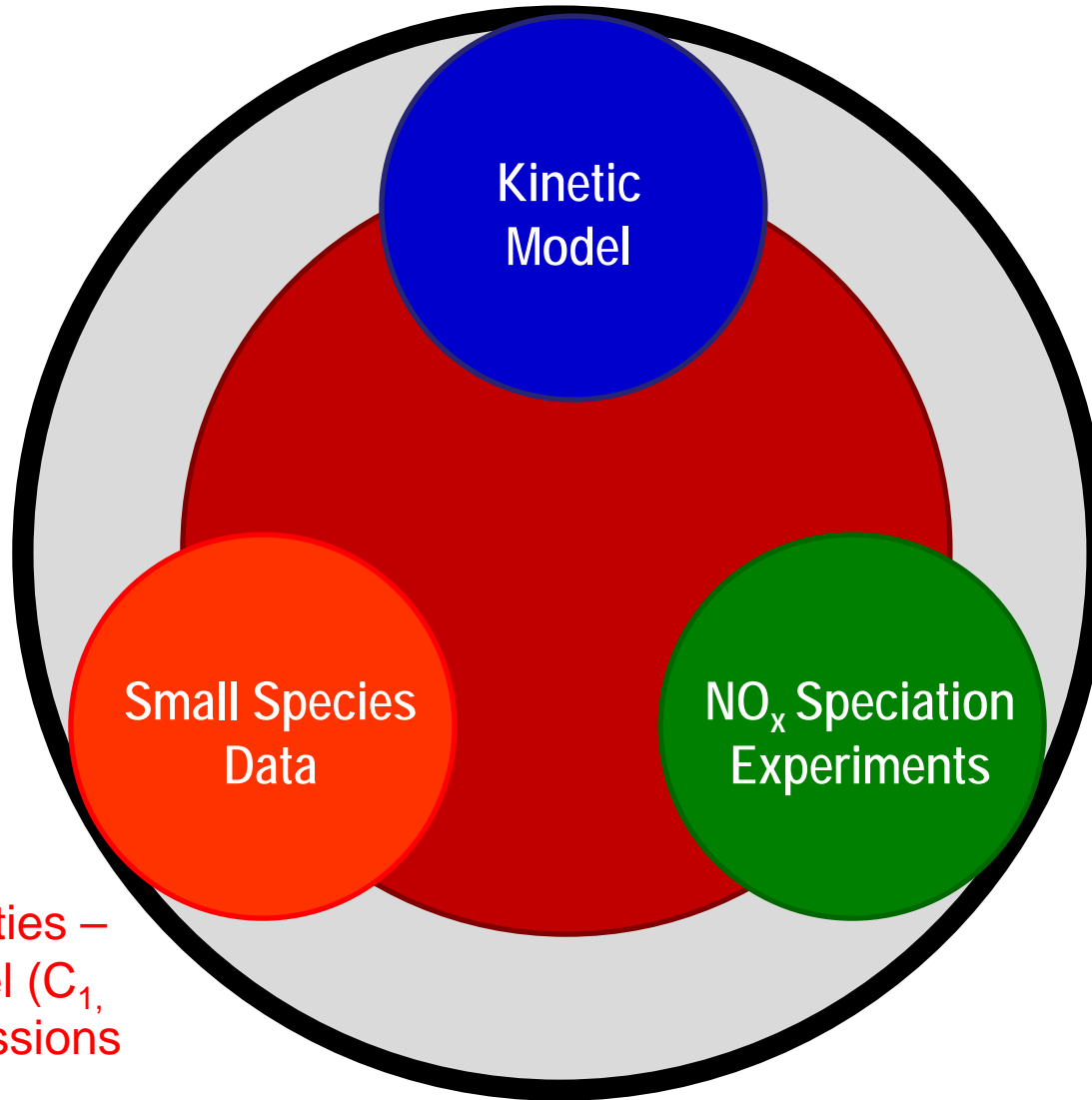


- **Study of reactivity and speciation data for  $\text{NO}_x$  under various conditions**
- **Studies of  $\text{CO}$ ,  $\text{NO}$ ,  $\text{NO}_2$  formation and conversion for  $\text{NO} \rightarrow \text{NO}_2$  in shear/mixing layers**
- **Studies of high pressure HHC fuel kinetics using a High Pressure Laminar Flow Reactor (HPLFR)**
- **Kinetic assessment, validation and development of a comprehensive HHC fuel +  $\text{NO}_x$  kinetic mechanism**

# Presentation Outline



- **Research Team Members**
- **Project Objectives**
- **Research Tasks**
- **Year 2 progress**
  - **Kinetic Modeling of NO<sub>x</sub> formation in HHC Fuels**  
– **Tanvir Farouk**
  - **Experiments for Speciation Measurements**  
– **Bihter Padak**
  - **Measurement of Small Species Data and Modeling Implications**  
– **Frederick Dryer (presented by Tanvir Farouk)**
- **Summary**

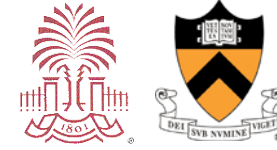


- Predictions of  $\text{NO}_x$  to address strict emission standards

- Trace emittents –  $\text{NO}_x$  influences the global and intricate combustion dynamics

- Fuel impurities – source of fuel ( $\text{C}_1$ ,  $\text{C}_2$  ...) – emissions

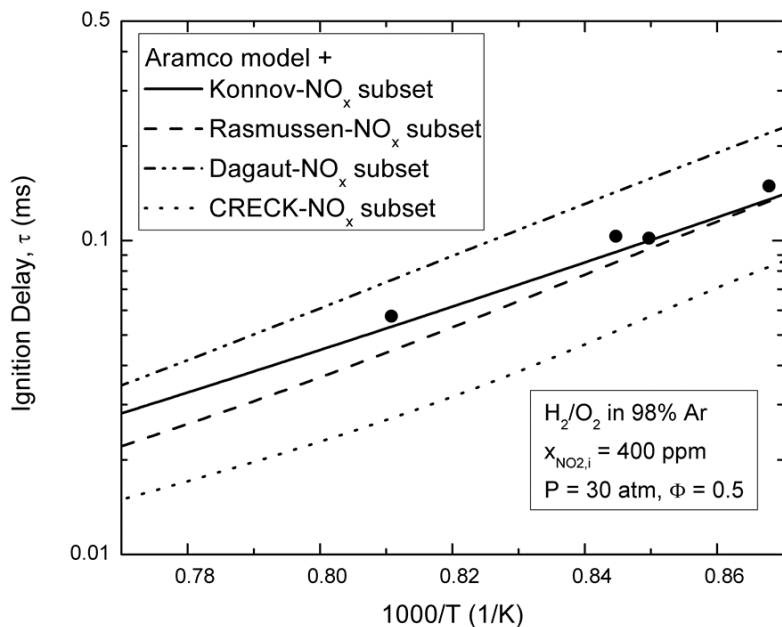
Unless one considers the ***interactions of small species and emittents***, particularly on natural gas combustion the resulting model will likely have poor fidelity to be considered for engineering applications



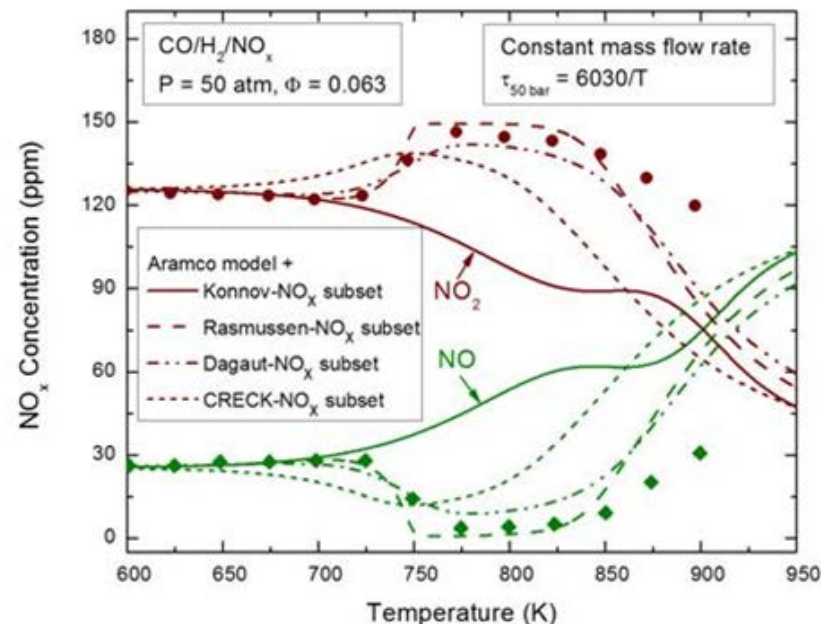
# Kinetic Modeling



# Current Predictive Models of NO<sub>x</sub> Formation



Global combustion targets are insufficient to provide the necessary constraining conditions for assessment and model development of NO<sub>x</sub> interactions with Hydrogen and Syngas Oxidation.



Detailed species evolution measurement necessary

Considerable differences in even qualitative behavior among popular literature models => improvements are possible.

Mathieu et al., Proc. Combust. Inst. 34 (2013)

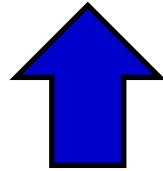
Rasmussen et al., Int. J. Chem. Kinet. 40 (2008)



# Proposed H<sub>2</sub>/CO/NO<sub>x</sub> Model



Proposed H<sub>2</sub>/CO/NO<sub>x</sub> Model



Sub-mechanisms

C<sub>0</sub>-C<sub>1</sub>  
sub-mechanism

H/N/O  
sub-mechanism

NO<sub>x</sub>  
sub-mechanism

- H<sub>2</sub>/CO/NO<sub>x</sub> Model

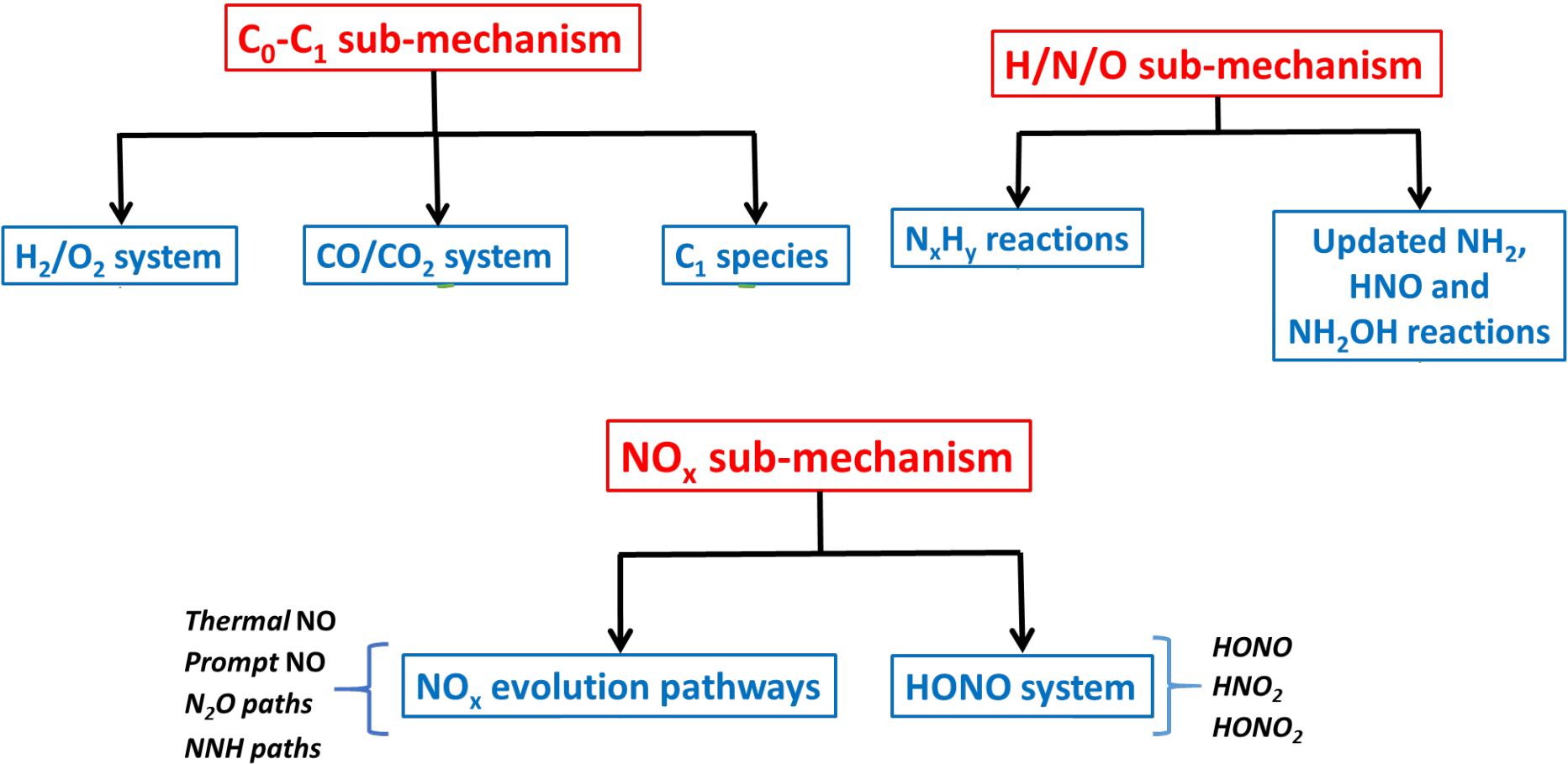
77 species, 442 reactions

- H<sub>2</sub>/C<sub>1</sub>-C<sub>4</sub>/NO<sub>x</sub> Model

302 species, 1952 reactions



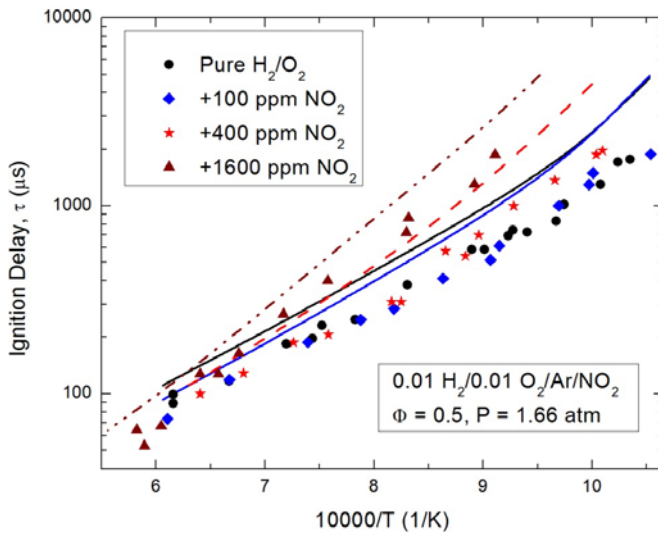
# Model Elements



<sup>1</sup>Burke et al., *Int. J. Chem. Kinet.* 44 (2012)  
<sup>2</sup>Metcalfe et al., *Int. J. Chem. Kinet.* 45 (2013)  
<sup>3</sup>Skreiberg et al., *Combust. Flame* 136 (2004)  
<sup>4</sup>Klippenstein et al., *Combust. Flame* 158 (2011)

# Proposed Model Performance: Ignition Delay

## Dependence of $\tau_{ig}$ on initial $\text{NO}_2$ doping for $\text{H}_2/\text{O}_2$ system

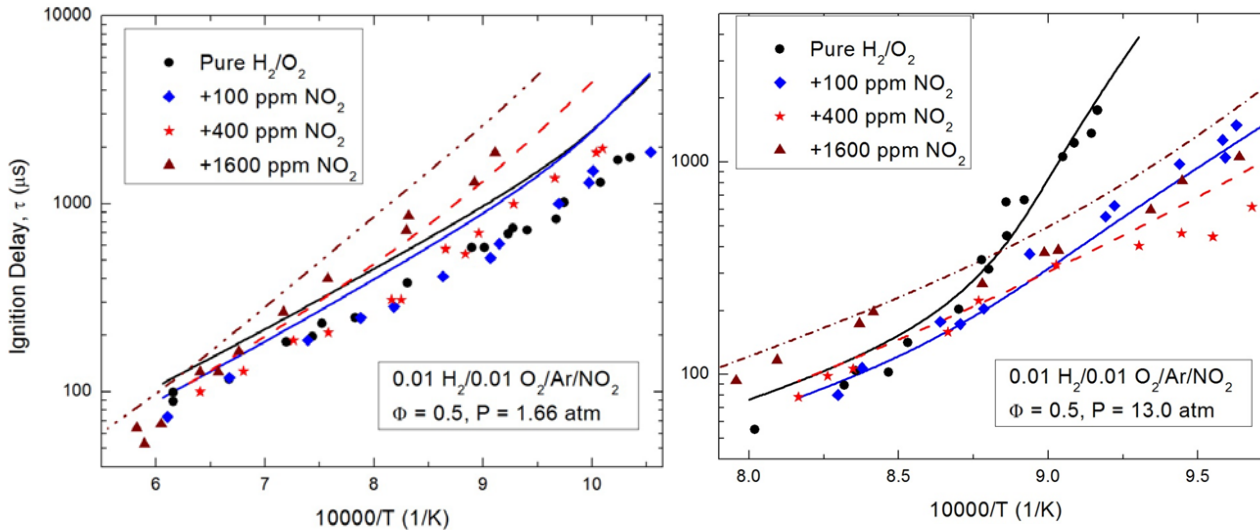


100 ppm → insignificant

400 ppm or higher → reactivity decreases

# Proposed Model Performance: Ignition Delay

## Dependence of $\tau_{ig}$ on initial $\text{NO}_2$ doping for $\text{H}_2/\text{O}_2$ system



**Pressure**



100 ppm  $\rightarrow$  insignificant

400 ppm or higher  $\rightarrow$  reactivity decreases

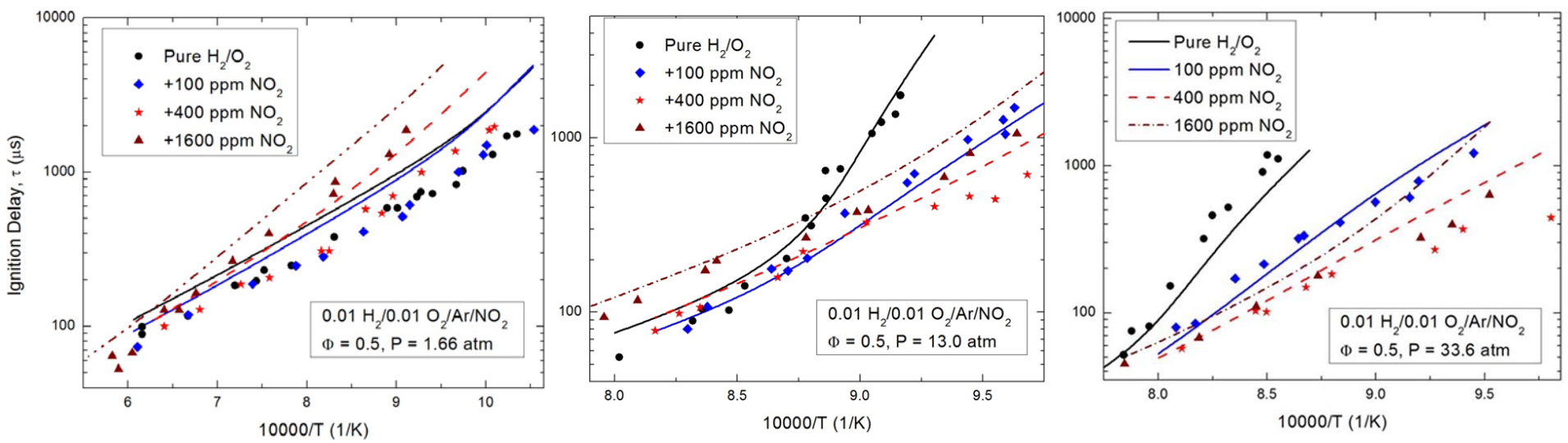
100 - 400 ppm  $\rightarrow$  reactivity increases

1600 ppm  $\rightarrow$  reactivity decreases

**High pressure non-monotonic behavior captured by the model**

# Proposed Model Performance: Ignition Delay

## Dependence of $\tau_{ig}$ on initial $\text{NO}_2$ doping for $\text{H}_2/\text{O}_2$ system



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100 ppm → insignificant  
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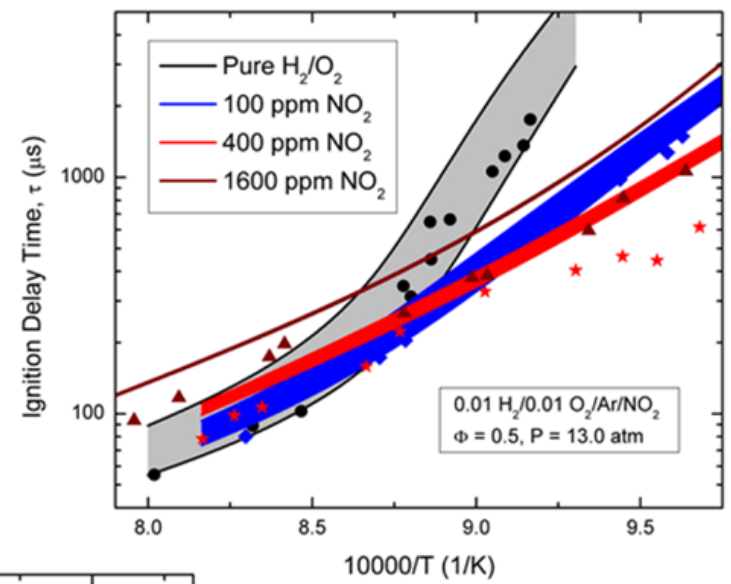
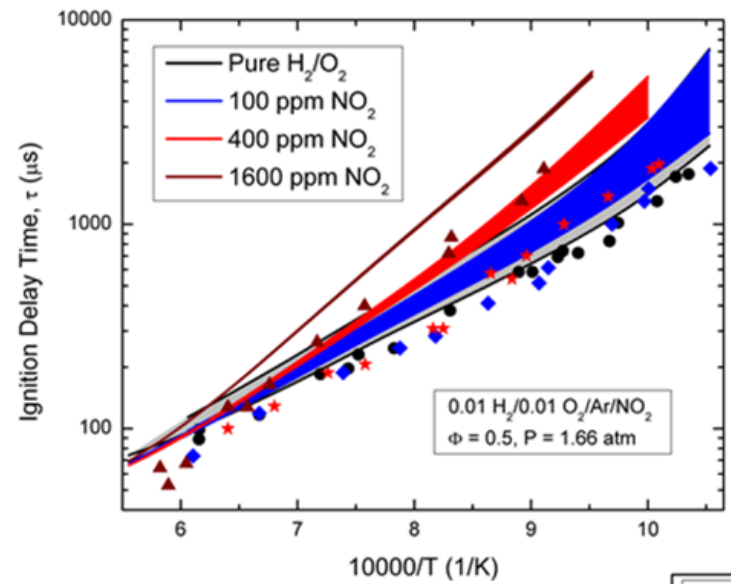
100 - 400 ppm → reactivity increases  
 1600 ppm → reactivity decreases

100 - 400 ppm → reactivity increases  
 1600 ppm → reactivity decreases

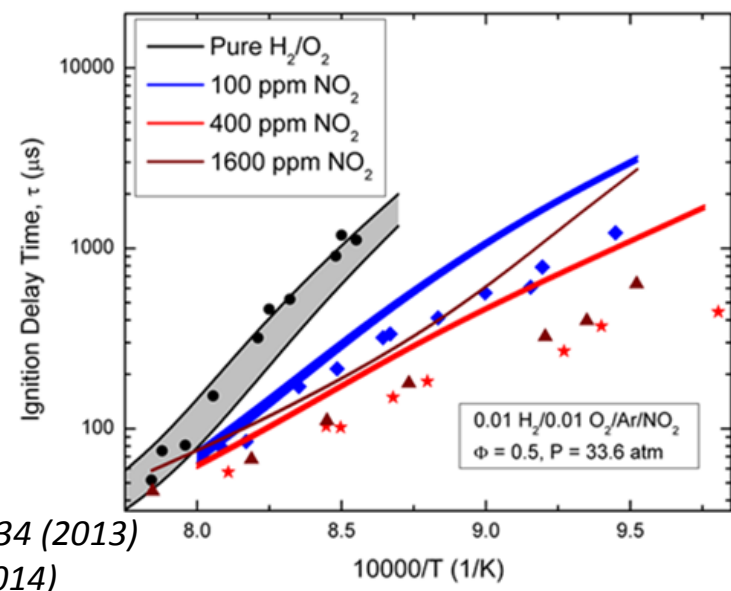
**High pressure non-monotonic behavior captured by the model**

# Proposed Model Performance: Ignition Delay

## Effect of initial H-atom impurities on the ignition delay of H<sub>2</sub>/O<sub>2</sub> system



350 ppb of H-impurity

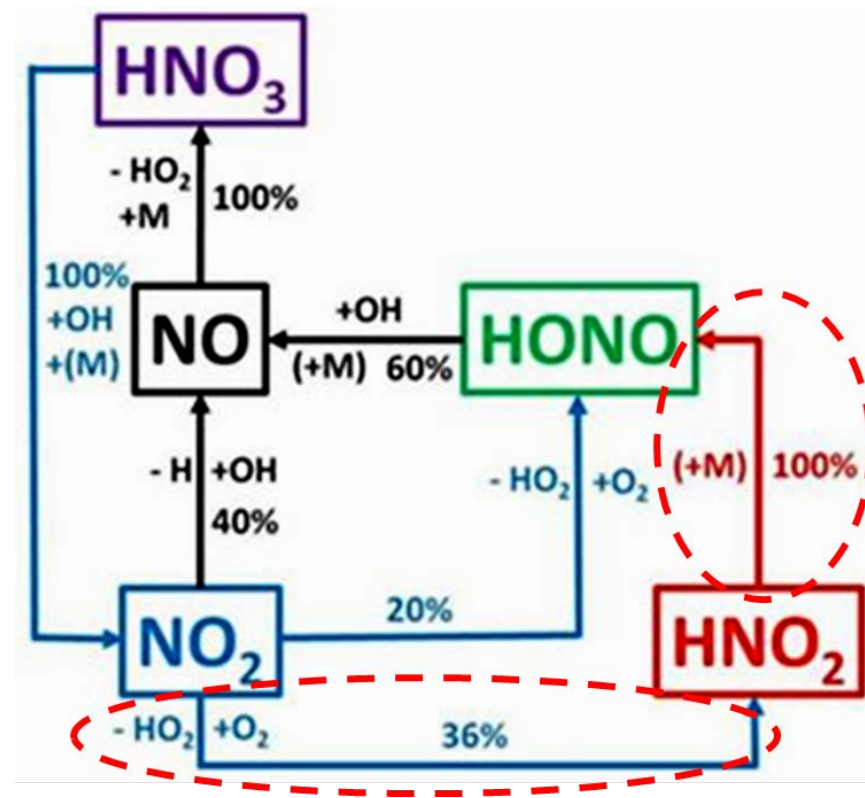
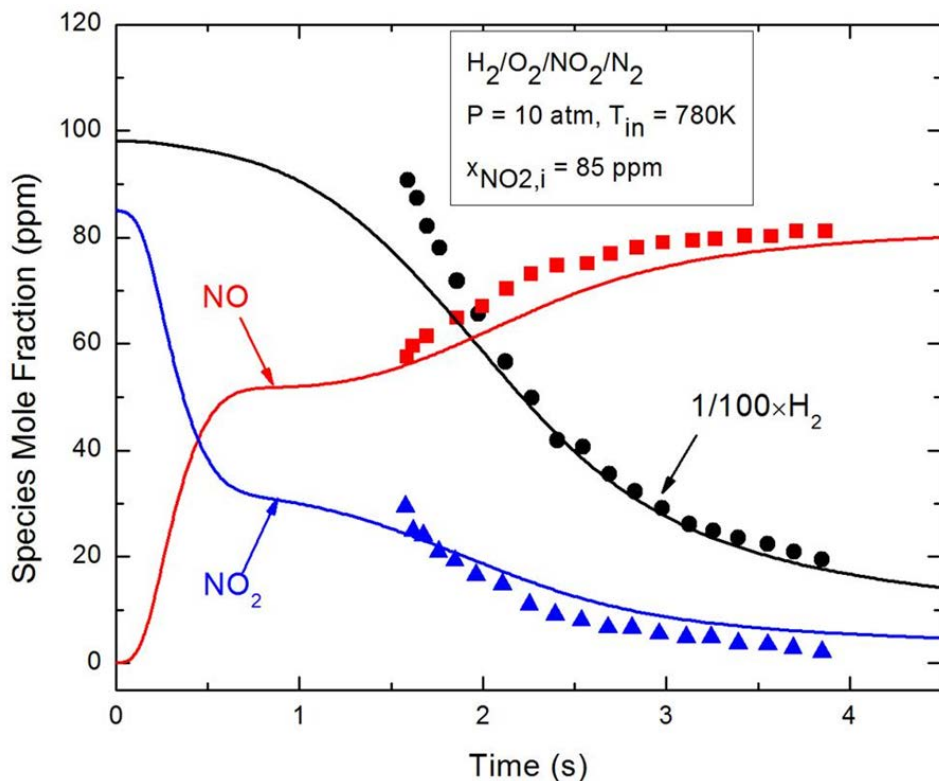


Impurity effects change with-

- ✓ pressure
- ✓ initial NO<sub>2</sub> doping

Mathieu et al., Proc. Combust. Inst. 34 (2013)  
 Urzay et al. Combust. Flame 161 (2014)

# Proposed Model Performance: PFR Speciation for $H_2/O_2/NO_2/N_2$ System

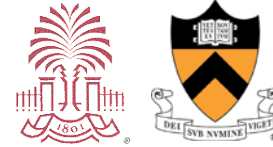


**Reasonable model prediction of fuel consumption and NO-NO<sub>2</sub> conversion**

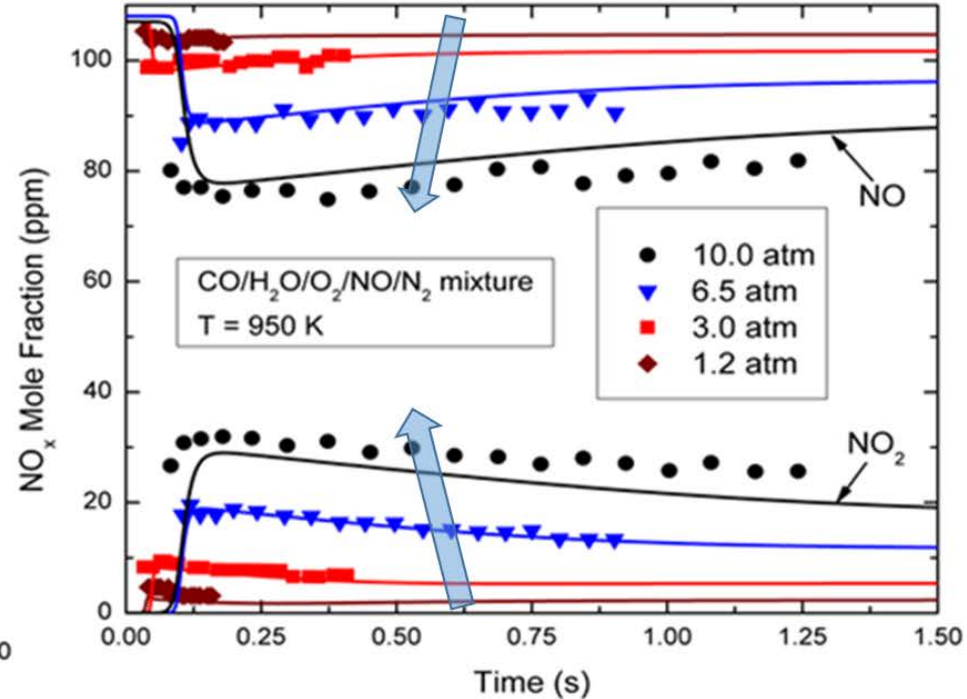
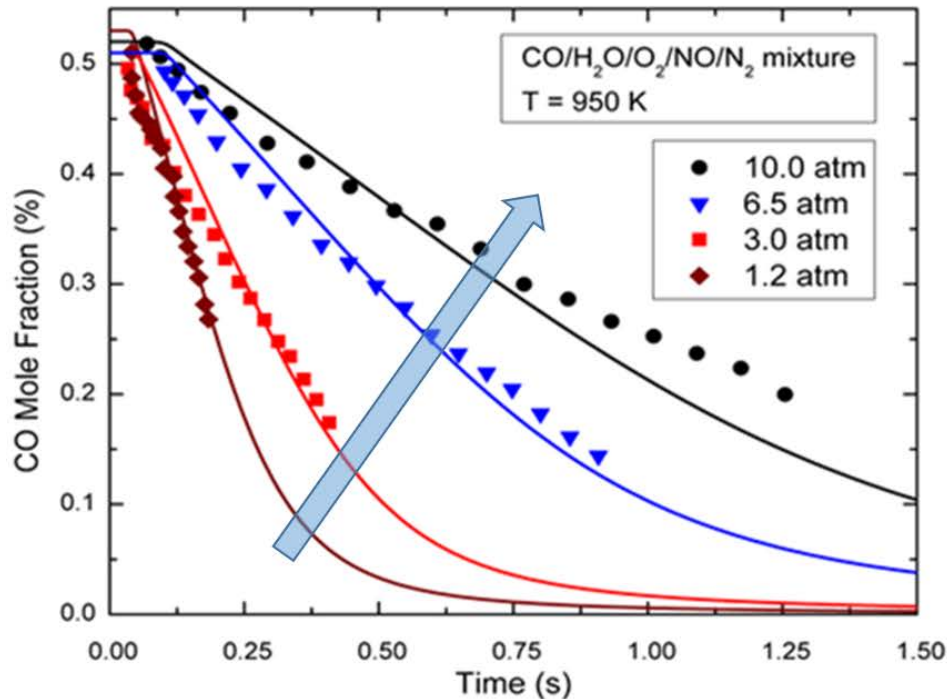
- NO → NO<sub>2</sub> conversion: through intermediate HNO<sub>3</sub>
- NO<sub>2</sub> → NO conversion: (i) direct  
(ii) through intermediate HONO  
(iii) through intermediate HNO<sub>2</sub>



# Proposed Model Performance: Variable Initial Conditions for CO/H<sub>2</sub>O/O<sub>2</sub>/NO System



## Variable Initial Pressure



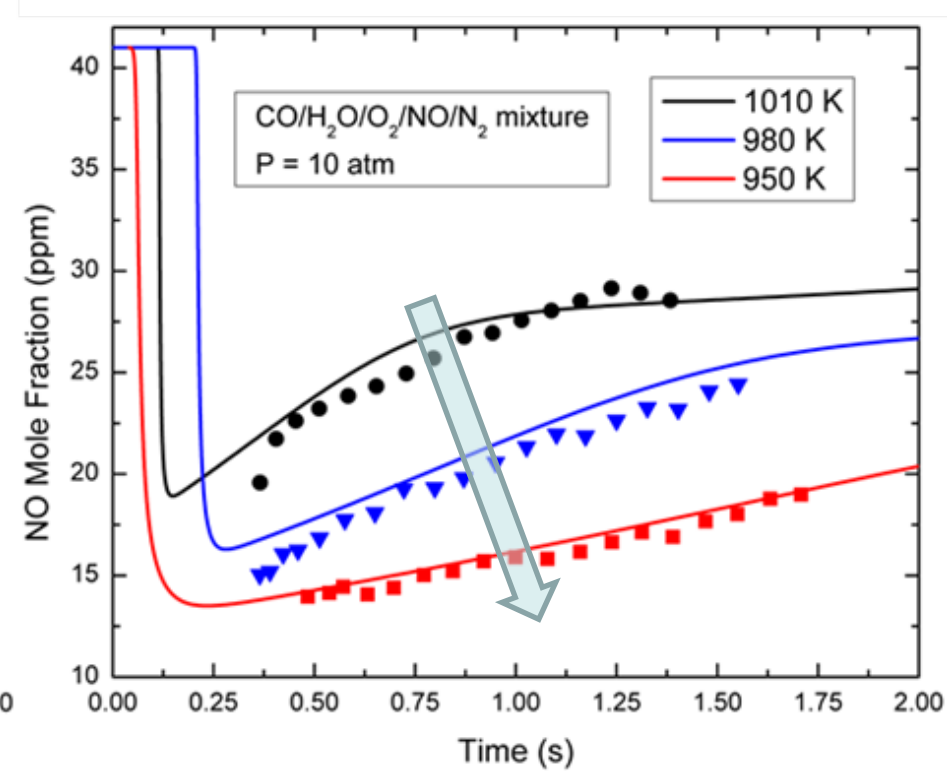
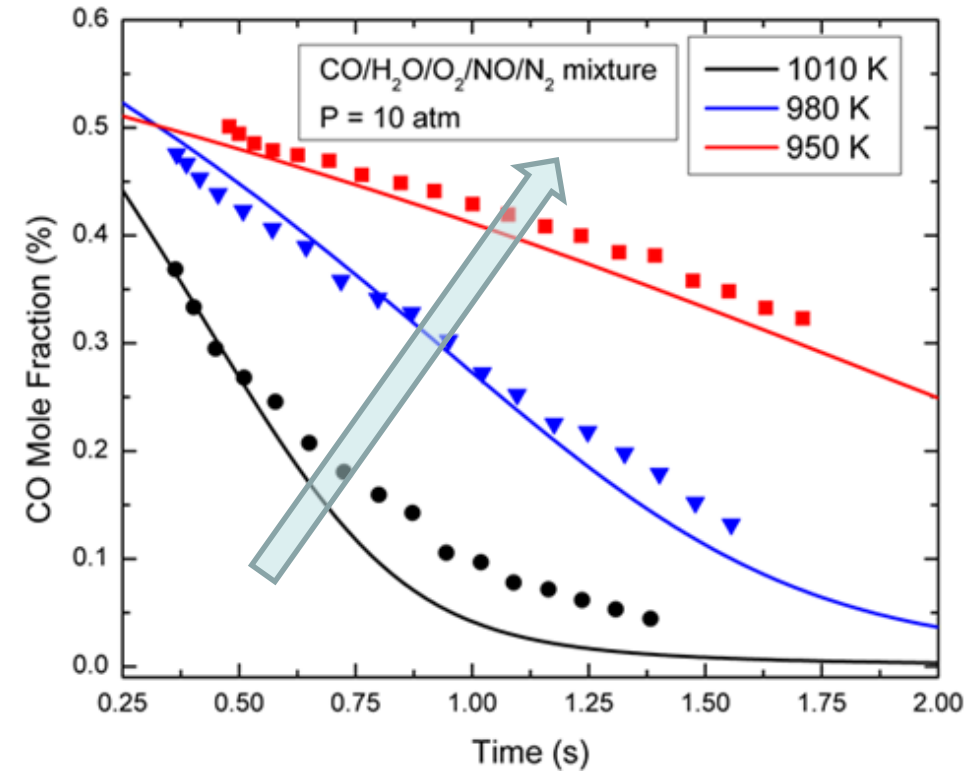
- ✓ Model reasonably predicts the experimental trends with variable initial pressure
- ✓ Complete NO-NO<sub>2</sub> interconversion without any formation of molecular nitrogen



# Proposed Model Performance: Variable Initial Conditions for CO/H<sub>2</sub>O/O<sub>2</sub>/NO System

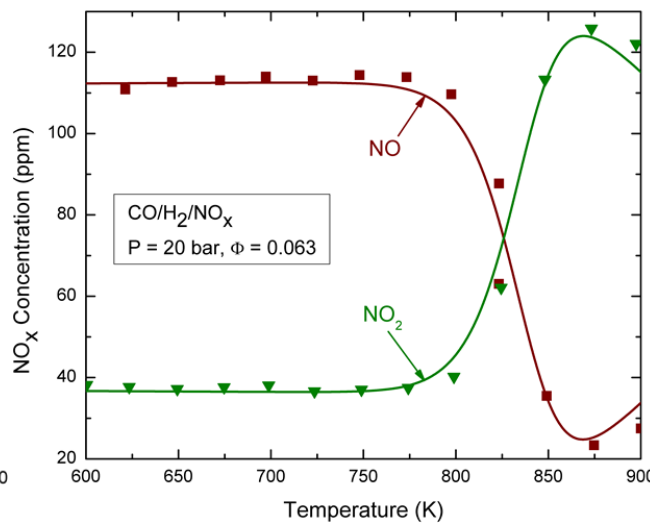
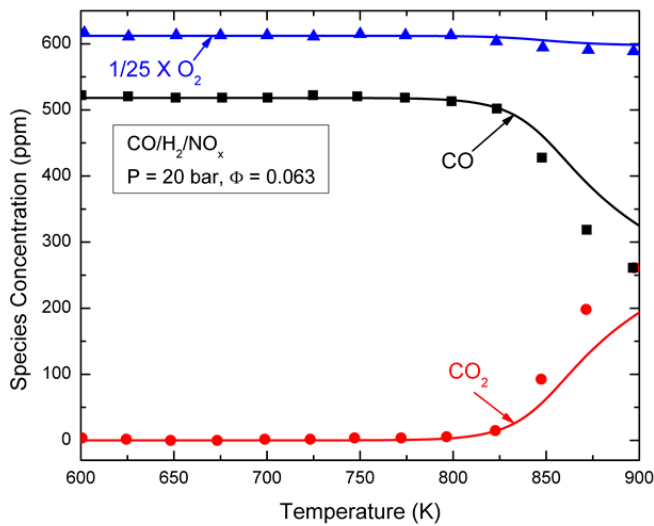
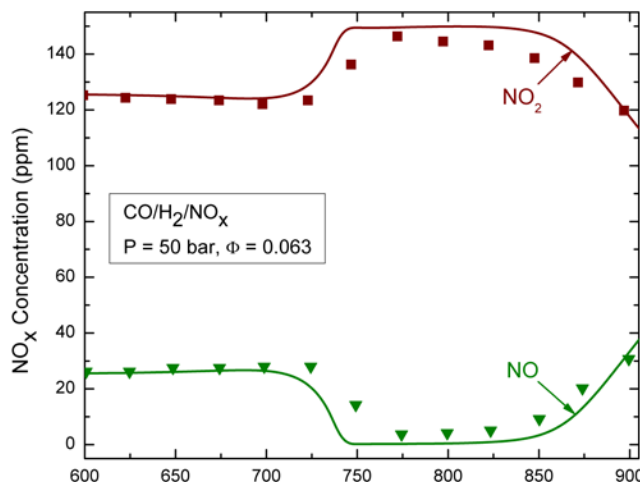
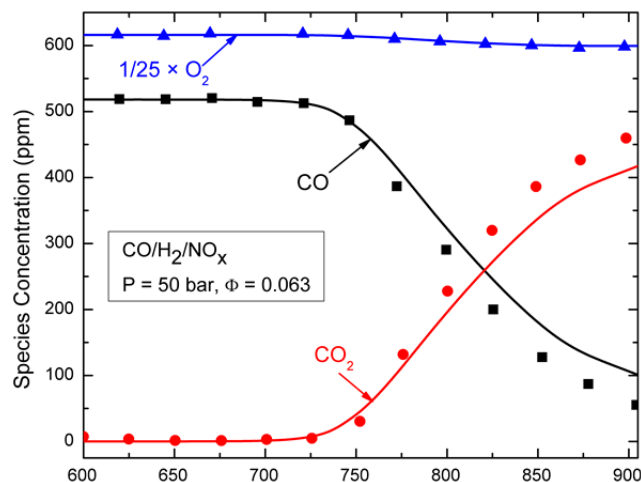


## Variable Initial Temperature



✓ Model reasonably predicts the experimental trends with variable initial Temperature

# Proposed Model Performance: PFR Species Evolution for CO/H<sub>2</sub>/NO<sub>x</sub> Oxidation System



- ✓ Flow reactor experiments at constant mass flow rate with temperature dependent residence time<sup>1</sup>

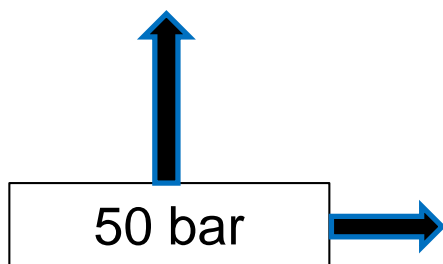
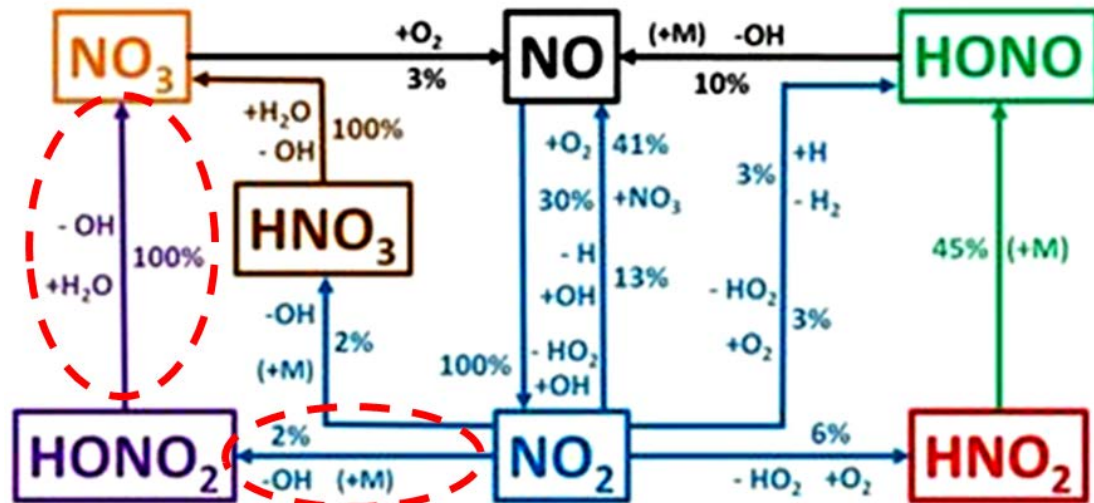
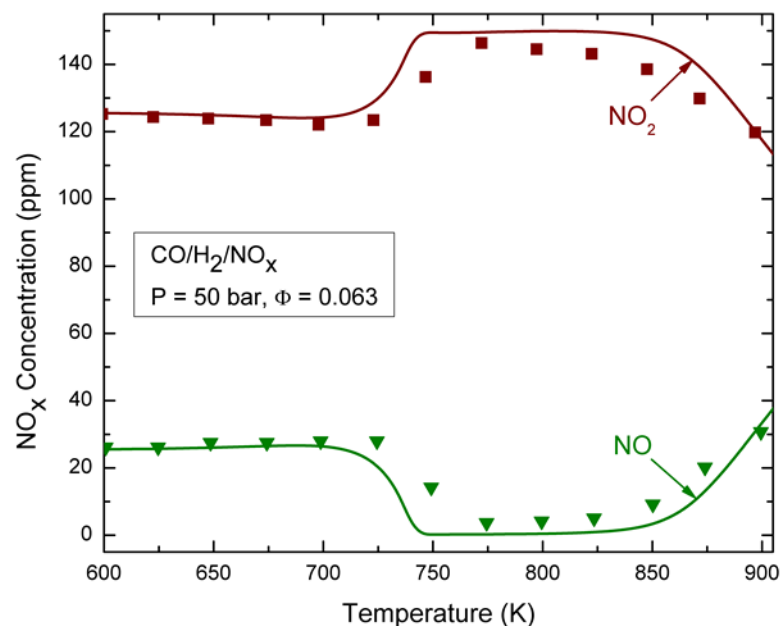
Pressure ↑

$$\tau_{20 \text{ bar}} = 2350/T$$

$$\tau_{50 \text{ bar}} = 6030/T$$

- ✓ Reasonable predictions for CO-CO<sub>2</sub> and NO-NO<sub>2</sub> conversion

# Proposed Model Performance: PFR Species Evolution for CO/H<sub>2</sub>/NO<sub>x</sub> Oxidation System



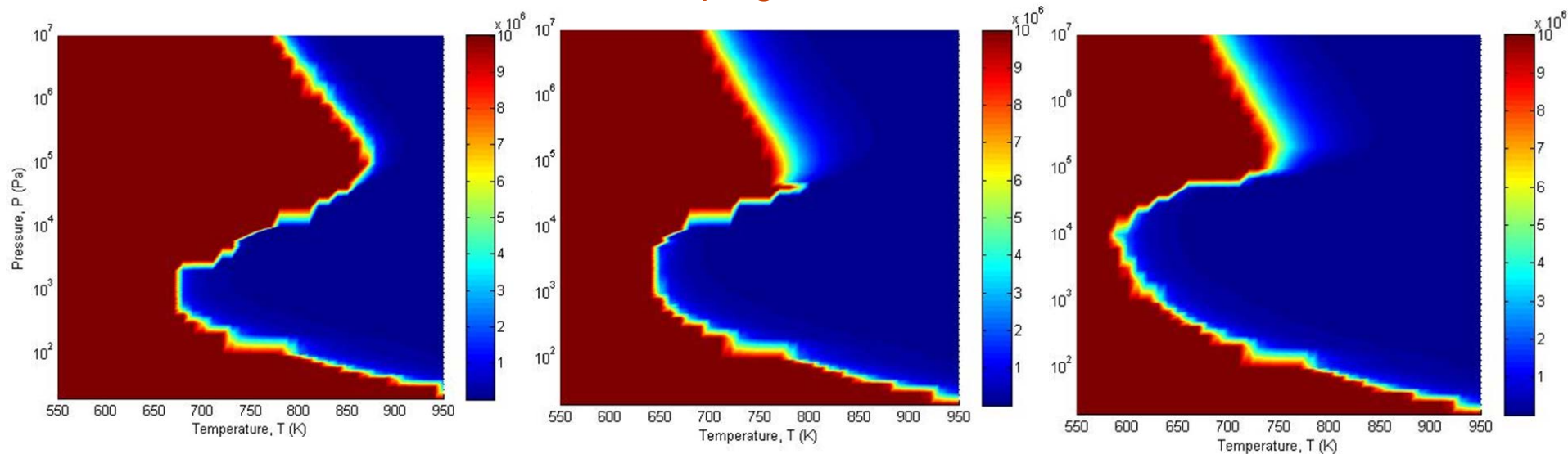
**Dominance of pressure-dependent reactions: two additional NO  $\leftrightarrow$  NO<sub>2</sub>**

# Effect of Physical and Chemical Perturbations on the Explosion limit and Ignition Delay Time of H<sub>2</sub>/O<sub>2</sub>



## Physical and chemical perturbation effects on the explosion limit as well as the ignition delay time of hydrogen

### Chemical Perturbation- initial NO doping



Base case

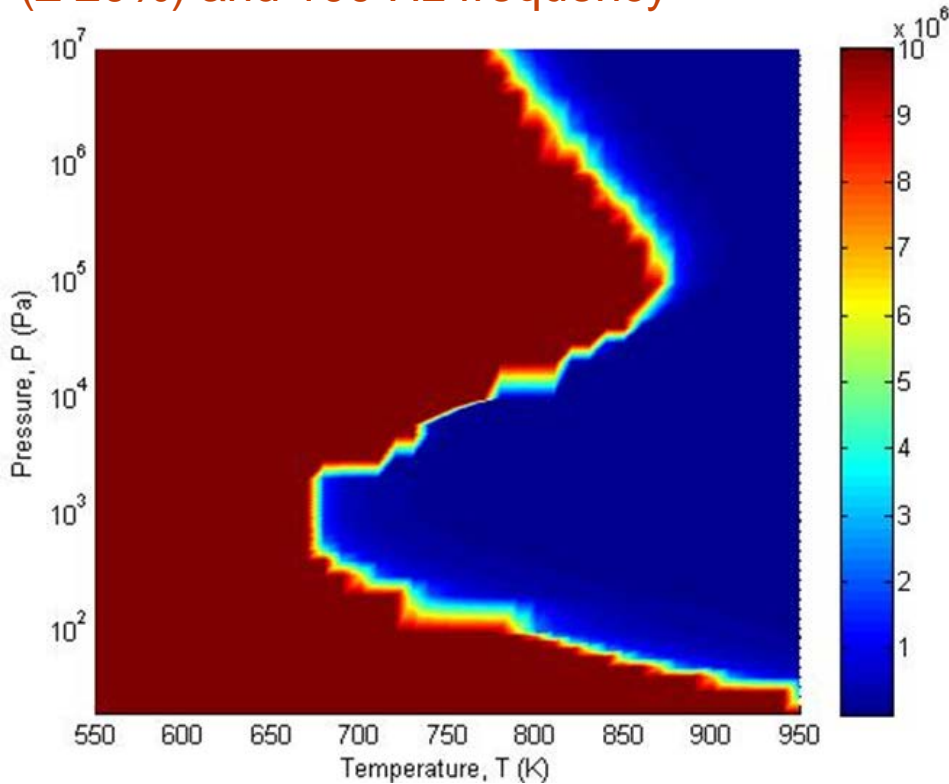
50 ppm NO

200 ppm NO

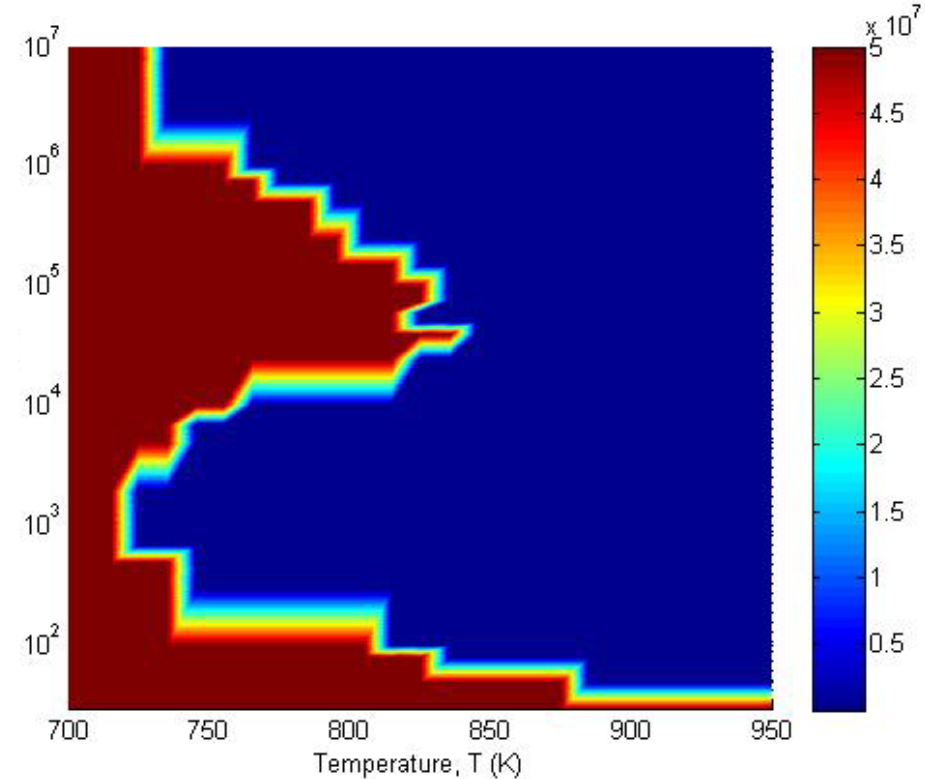
- ✓ With an increase in initial NO concentration, the initiation point of the second explosion limit moves towards higher pressures and lower temperatures
- ✓ The second explosion limit demarcation line becomes more and more flat with an increase in initial NO concentration
- ✓ The initiation point of the third explosion limit shifts toward lower pressures and higher temperatures with an increase in initial NO concentration

# Effect of Physical and Chemical Perturbations

Physical Perturbation- Fluctuating pressure with Gaussian random amplitude ( $\pm 20\%$ ) and 100 Hz frequency



Base case



Sinusoidal Pressure Perturbations

$$P = P_0 + A_{rand} * \sin(2\pi ft)$$

- ✓ With pressure perturbation, the initiation point of the second explosion limit moves towards higher temperatures and the initiation point of the third explosion limit moves towards lower temperatures
- ✓ The third explosion limit demarcation line becomes less steep with pressure perturbation

# Summary



- $C_0 - C_4/NO_x$  model has been assembled
- $H_2/CO/NO_x$  model has been validated
- Influence of trace impurities on combustion characteristics
- Chemical and physical perturbation effects on ignition delay and explosion limits for  $H_2/O_2$  systems
- Trace  $NO_x$  – emittents can alter the combustion behavior, global/optimized models can not capture intricate features



# Experimental Setup for Speciation Measurements

# Scope of Work



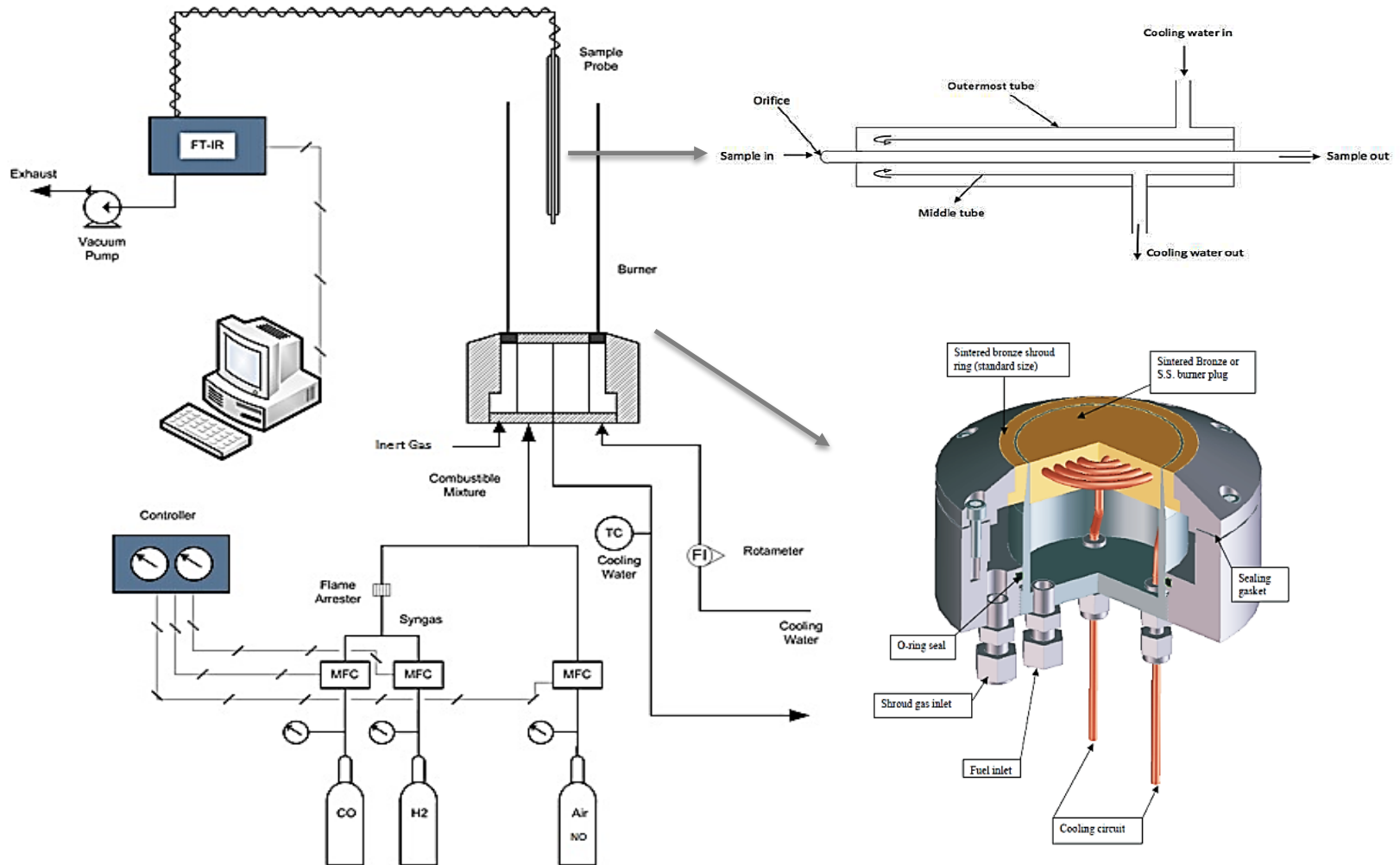
The presented work is focusing on  $\text{NO}_x$  formation in a syngas/air combustion system at atmospheric pressure.

Syngas tests were carried out with  $\Phi$ :0.5-1,  $\text{H}_2/\text{CO}$  from 1:1 to 1:4, total flow rate of 3-6 slpm.

The first set of experiments were conducted at atmospheric pressure and the second part is going to be done at elevated pressures.



# Schematic of Experimental Setup



# Experimental Plan

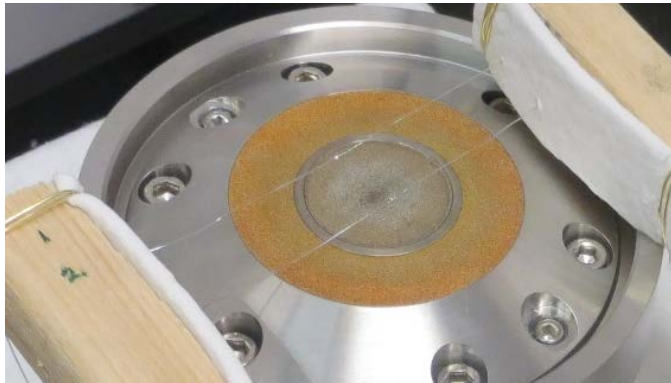


- Burner stability tests
- Temperature measurements
  - Flame temperatures
  - Radial temperature profile
  - Axial temperature profile
- Speciation data
  - NO, NO<sub>2</sub> and N<sub>2</sub>O concentration profiles
  - CO concentration profile

# Temperature Measurements

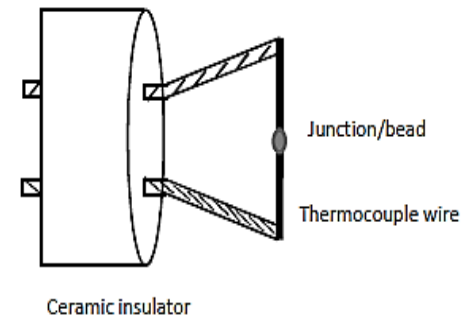
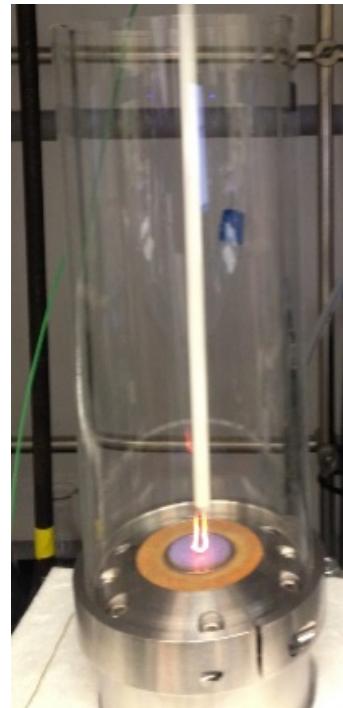


## Flame T measurements



- Radiation correction was applied to T measurements
- Using the R-type thermocouple, the radiation loss was % 8

## Radial and axial T profile measurements

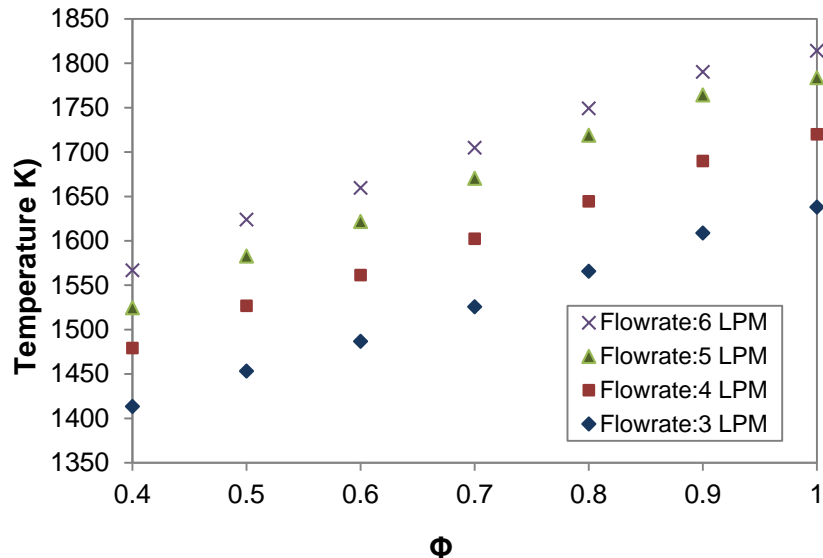


**Thermocouple diagram**

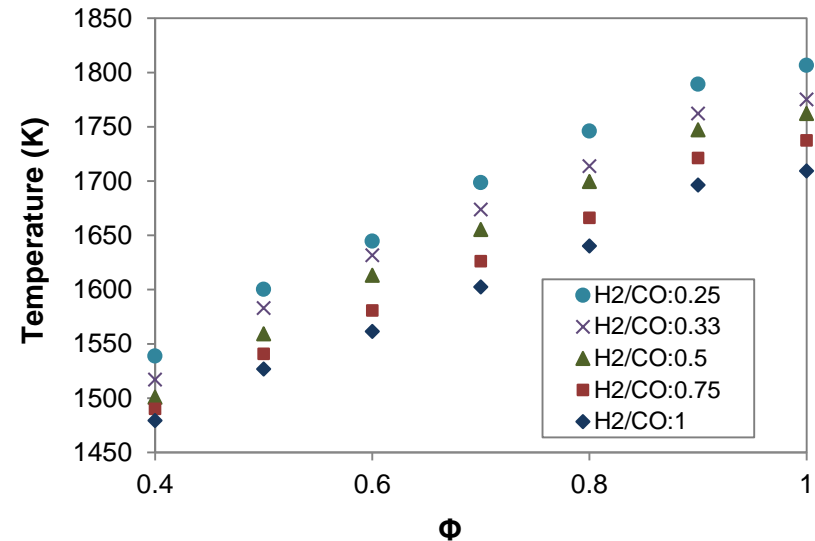
# Flame Temperature Measurements



## Different flow rates at $H_2/CO: 1$



## Different $H_2/CO$ ratios at 4 LPM

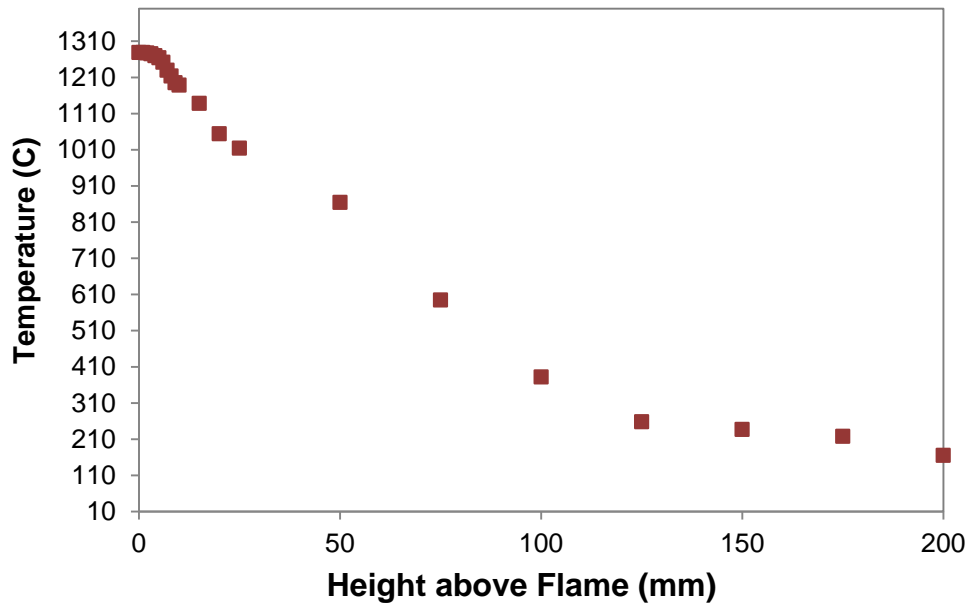


- With increasing the flow rate the distance between the burner plate and the reaction zone grows and heat transfer is reduced.
- Decreasing the  $H_2/CO$  ratio results in an increase in the flame temperature due to increased heat release by the  $CO+OH$  reaction.

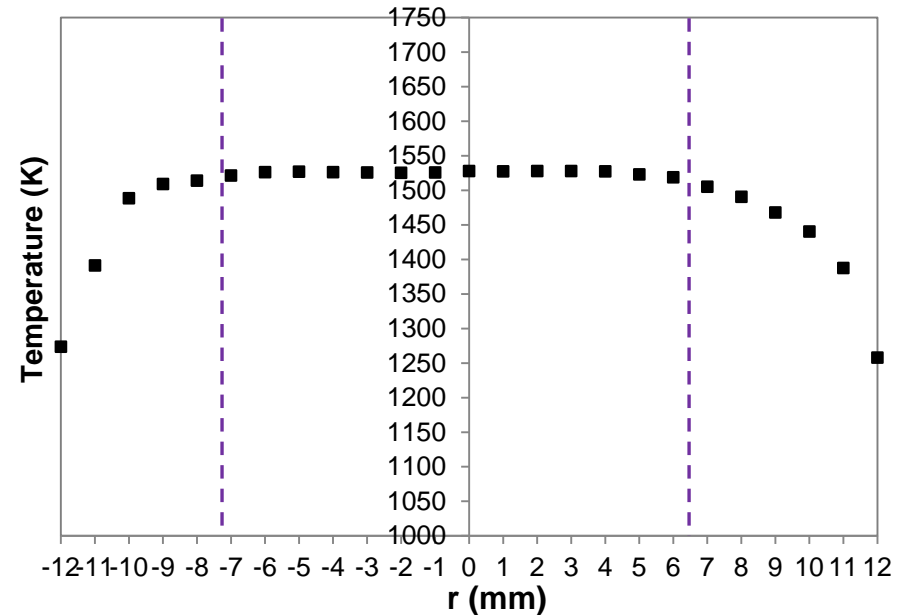
# Temperature Profiles

$H_2/CO:1$      $\Phi: 0.5$

Axial temperature profile



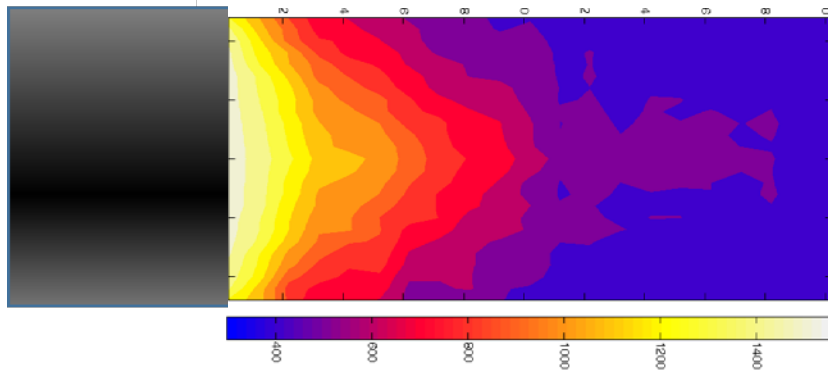
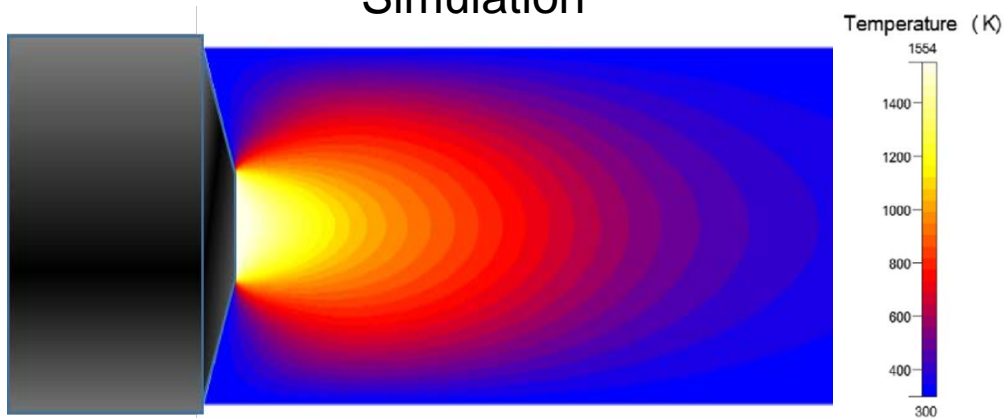
Radial temperature profile



- Temperature decreases as going away from the burner.
- A uniform temperature profile was obtained for a radius of 7mm.

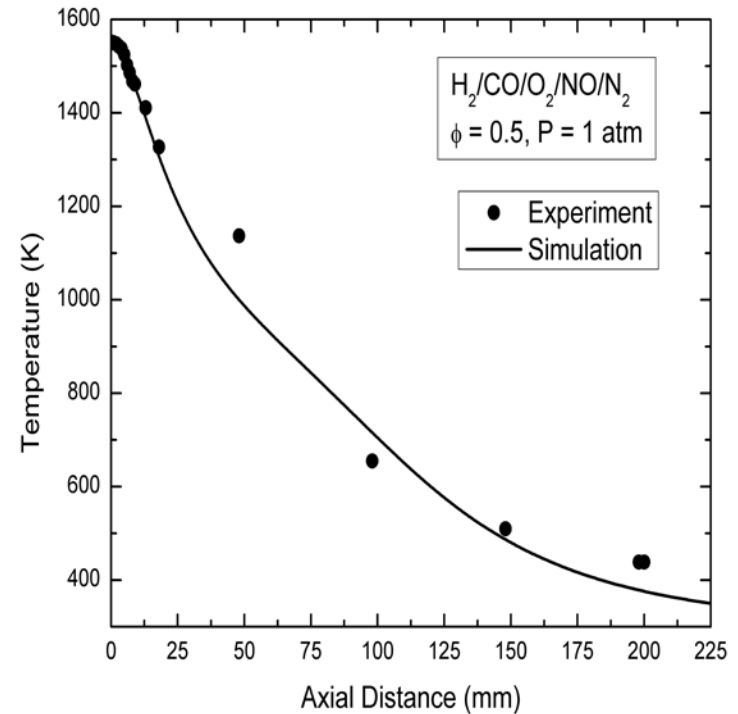
## 2-D Temperature Profile

Simulation



Experiment

## Centerline Temperature Profile

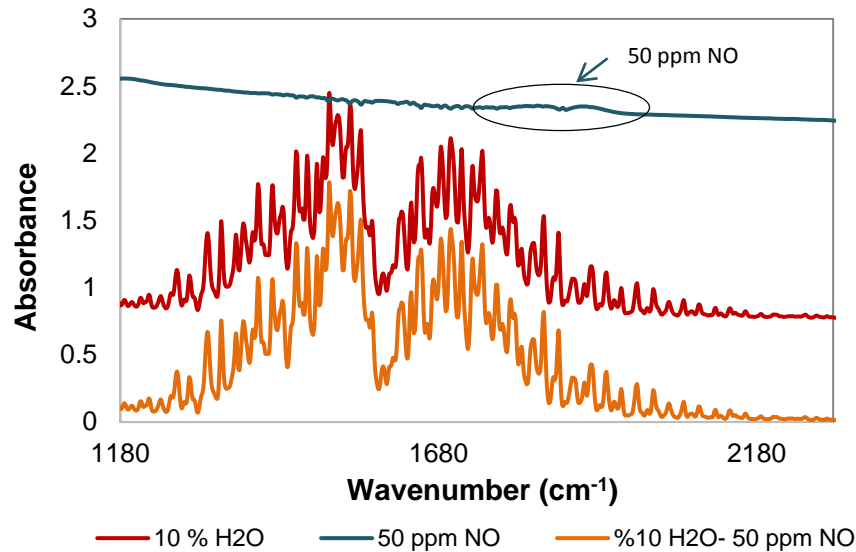


- CFD simulations reasonably predicts the experimental temperature distribution

# NO<sub>x</sub> Measurements with FTIR Spectroscopy



- FTIR spectroscopy is employed for speciation measurements.
- Overlapping peaks for the gases of interest.



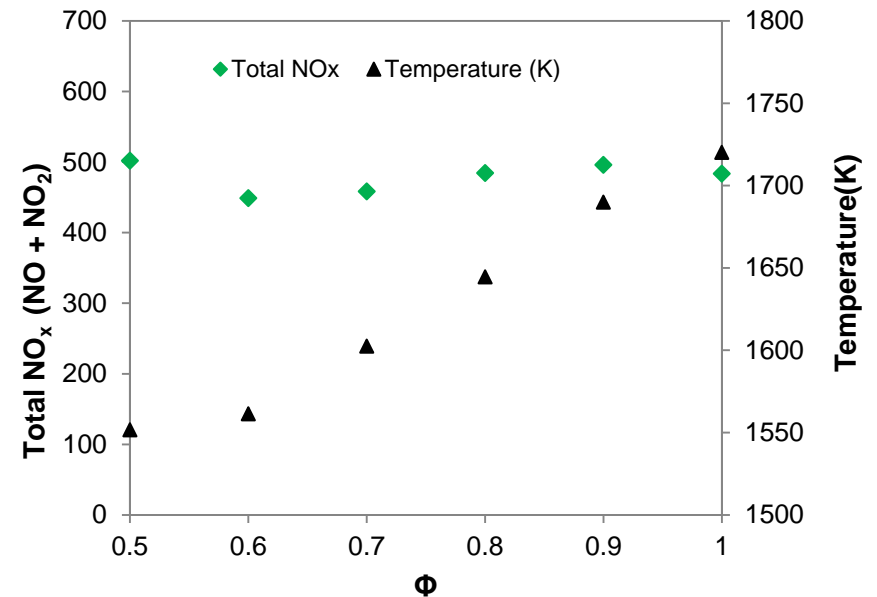
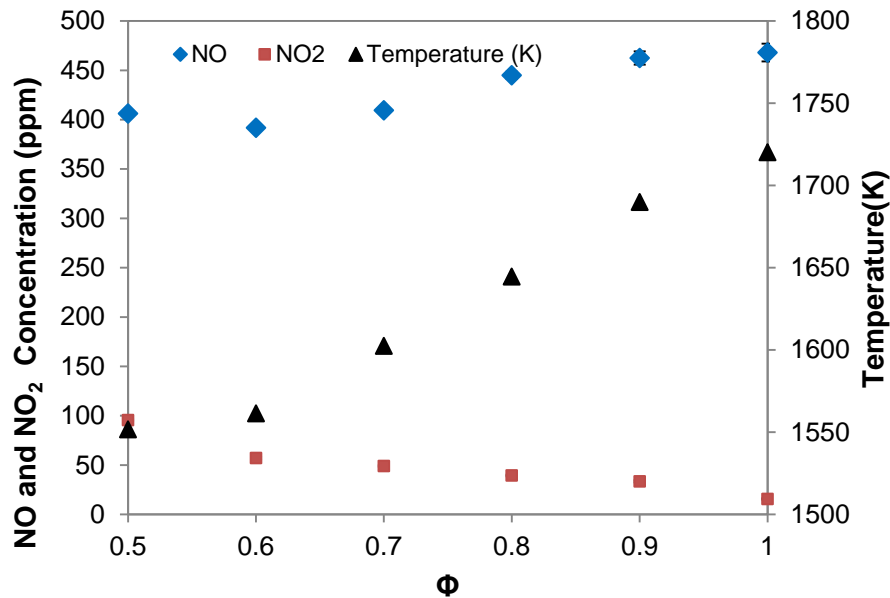
- To deconvolute the overlapping peaks, multivariate calibration was conducted.




Species	NO-H <sub>2</sub> O	NO <sub>2</sub> -H <sub>2</sub> O	N <sub>2</sub> O-H <sub>2</sub> O
Experimental sets	36	36	36

# NO<sub>x</sub> Speciation Data



NO<sub>x</sub> vs.  $\Phi$  with H<sub>2</sub>/CO:1 and 500 ppm NO in the feed



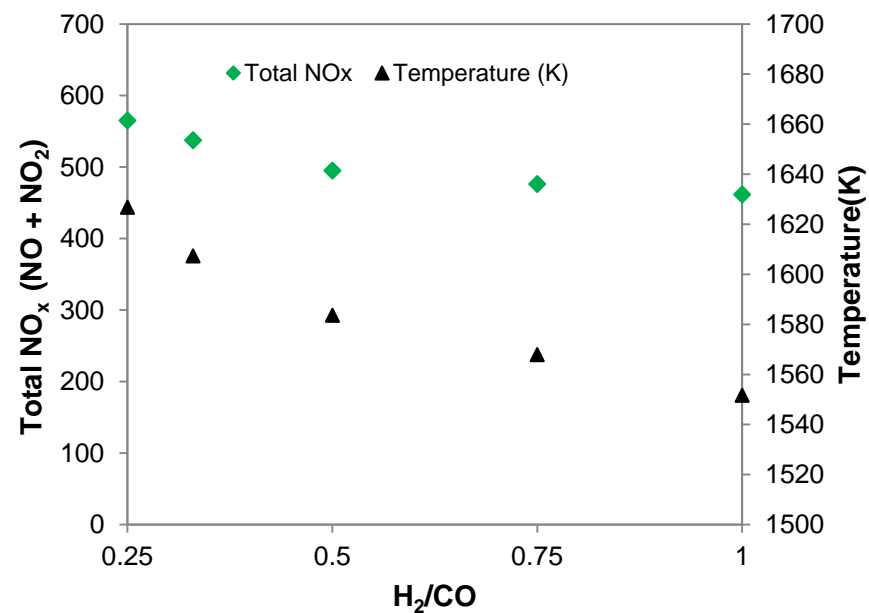
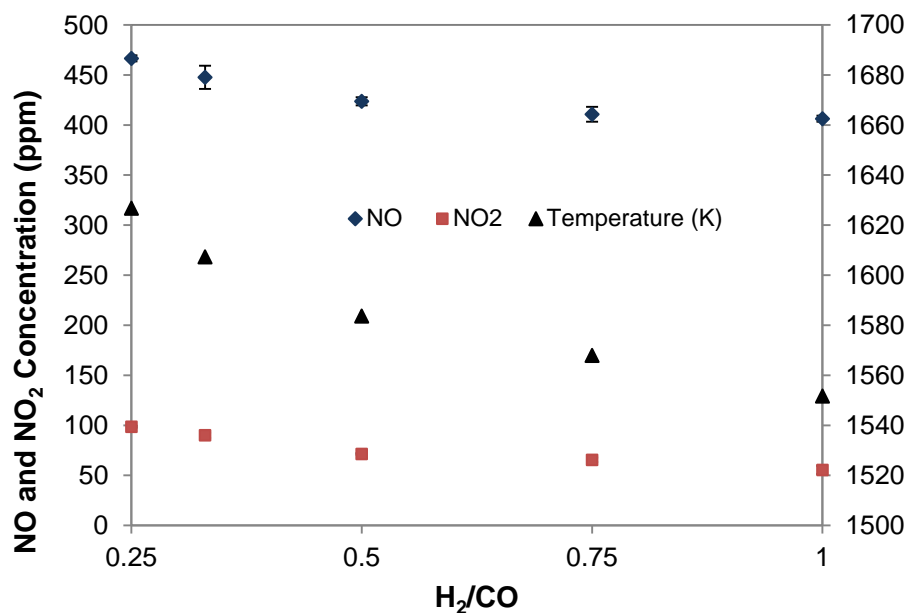
As  $\Phi$  increases  NO concentration   
NO<sub>2</sub> concentration   
Total NO<sub>x</sub> does not change much



# NO<sub>x</sub> Speciation Data



NO<sub>x</sub> vs. H<sub>2</sub>/CO with  $\Phi = 0.5$  and 500 ppm NO in the feed



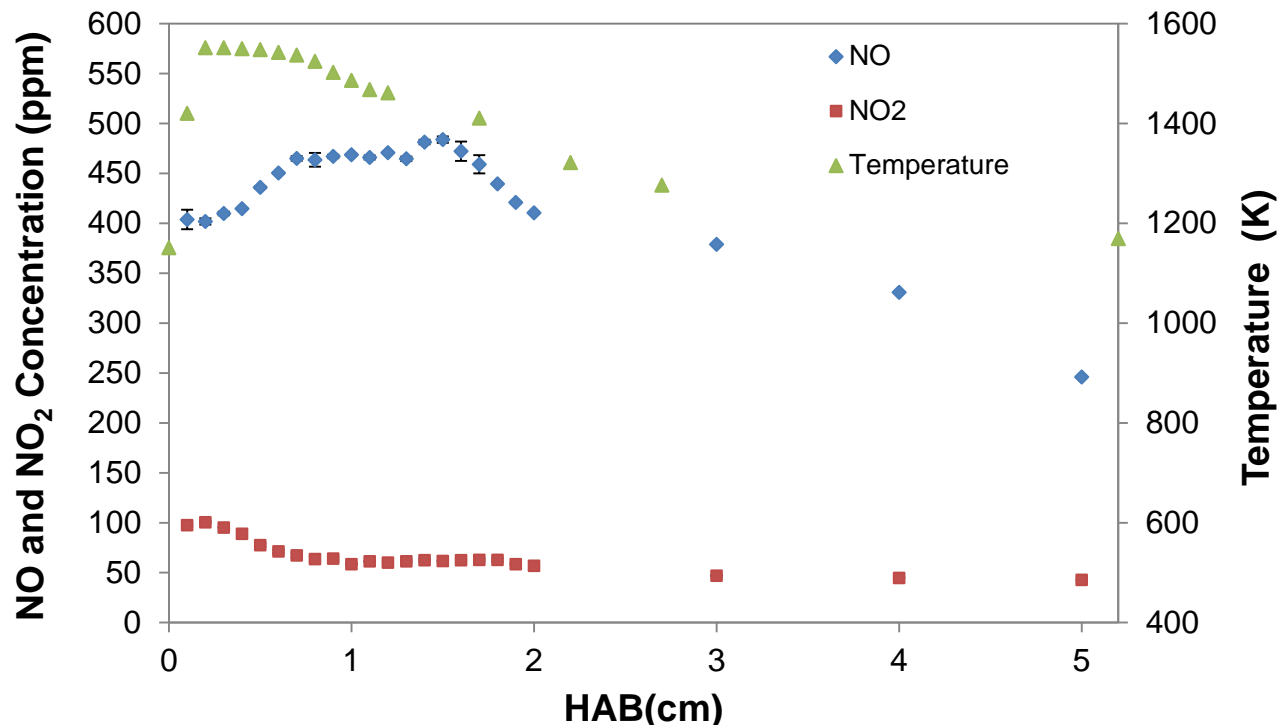
As H<sub>2</sub>/CO increases → NO concentration ↓  
NO<sub>2</sub> concentration ↓  
Total NO<sub>x</sub> ↓

# NO<sub>x</sub> Speciation Data



## NO, NO<sub>2</sub> profiles at different heights above burner (HAB)

H<sub>2</sub>/CO=1,  $\Phi=0.5$  and 500 ppm NO in the feed



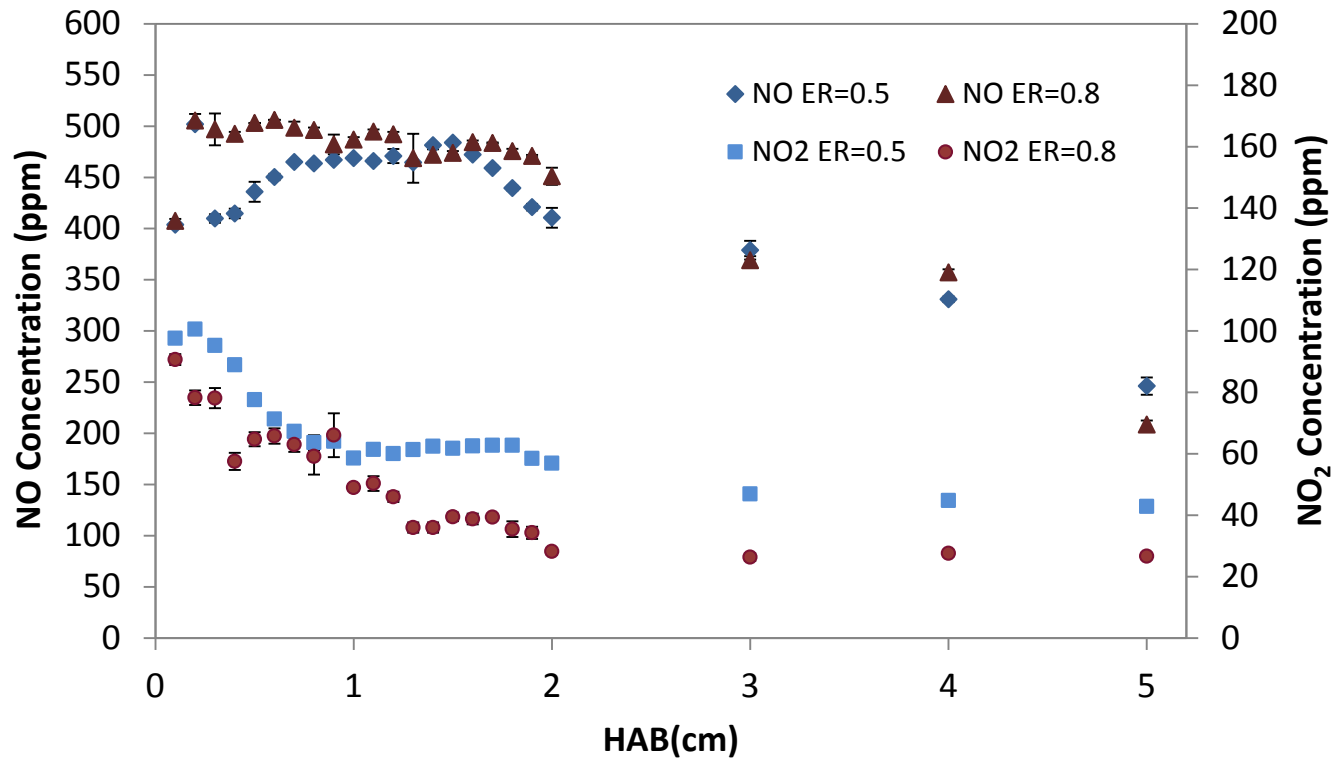
- Initially NO concentration increases due to NO<sub>2</sub> to NO conversion
- At lower T NO decreases due to NO to N<sub>2</sub> conversion
- No N<sub>2</sub>O was observed.




# NO<sub>x</sub> Speciation Data



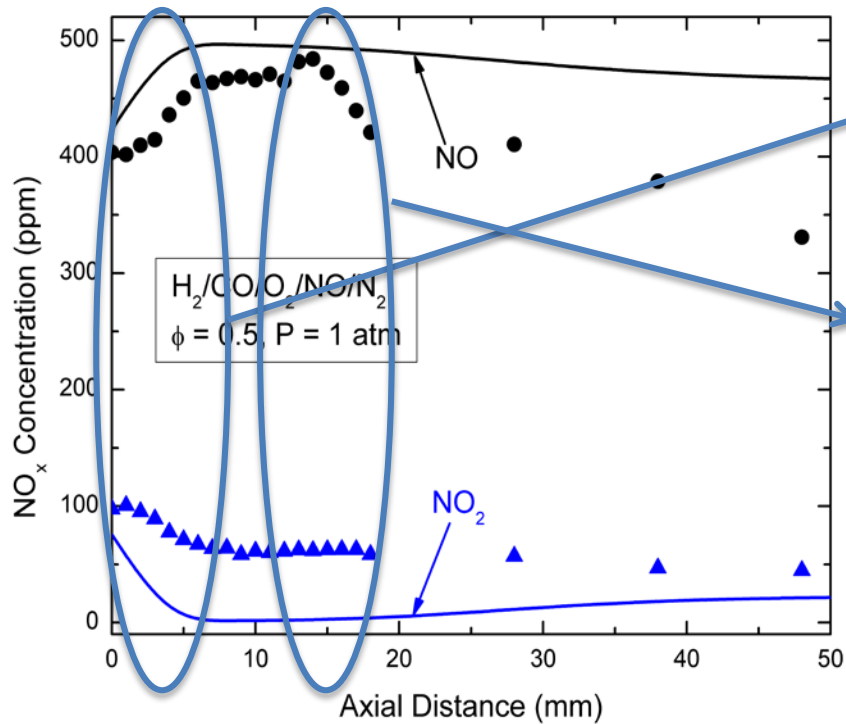
## NO, NO<sub>2</sub> profiles at different heights above the burner (HAB)

$\Phi=0.5$  and  $0.8$ ,  $H_2/CO=1$  and 500 ppm NO injection



As  $\Phi$  increases  NO concentration   
NO<sub>2</sub> concentration 

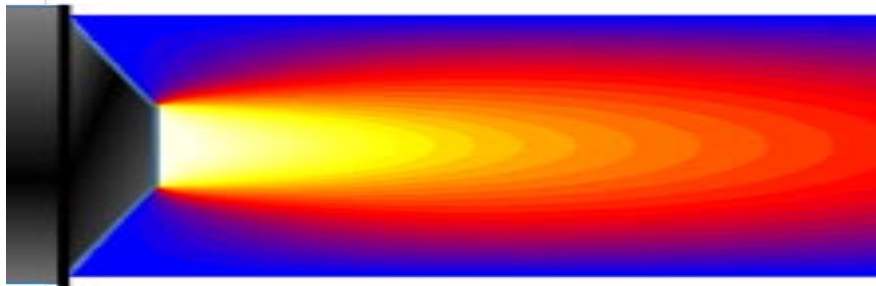
# NO<sub>x</sub> Speciation with CFD Modeling



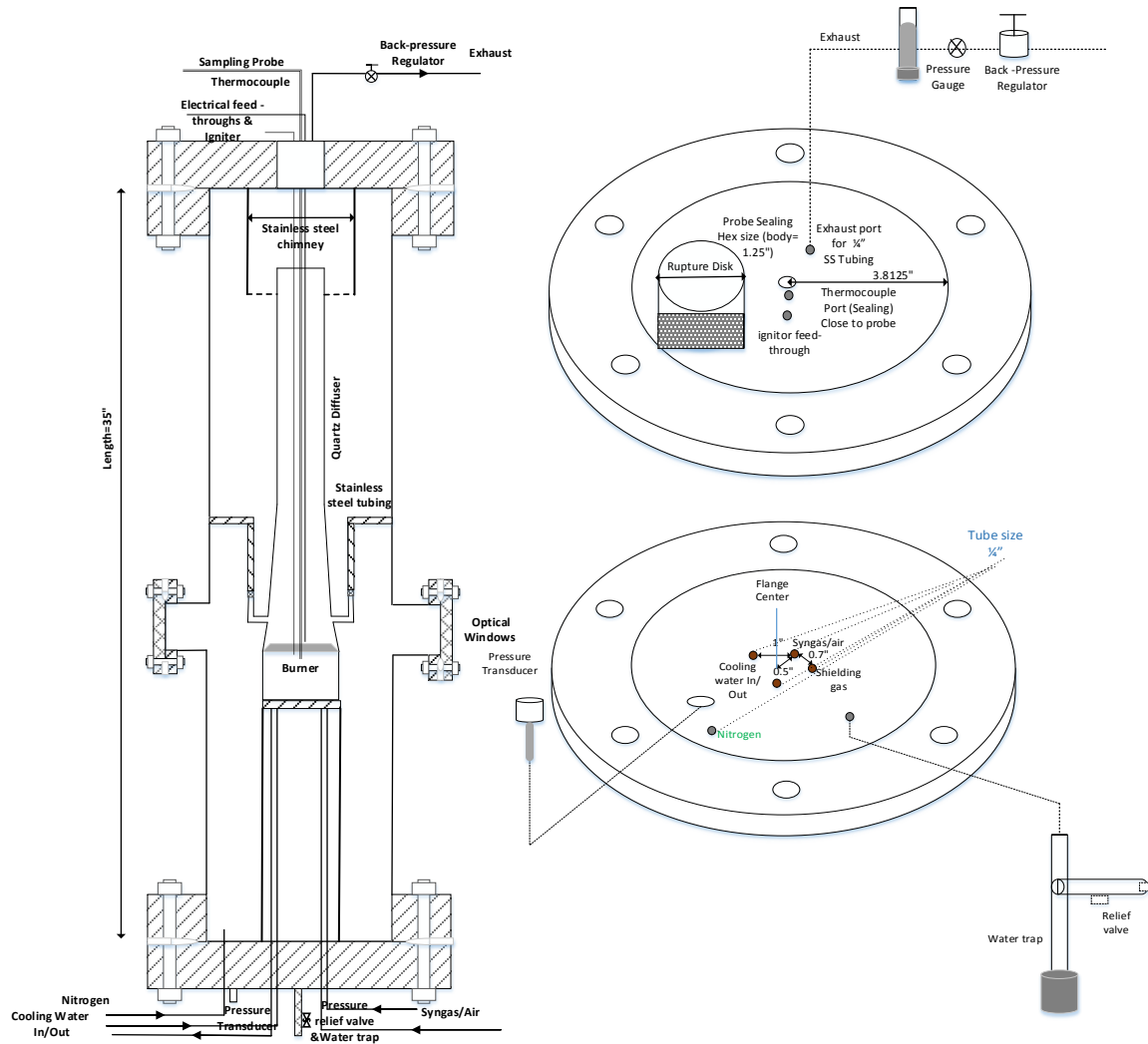
NO<sub>2</sub> to NO conversion  
**NO<sub>2</sub> + H = NO + OH (R1)**

NO to N<sub>2</sub> conversion  
**NO + N = N<sub>2</sub> + O (R2)**  
**NO + H = N + OH (R3)**

Temperature (K)



# High Pressure System



# Summary



- Axial and radial temperature profiles has been measured – temperature of the reacting zone.
- $\text{NO}_x$  speciation data at atmospheric pressure was collected at different conditions.
- There was a reasonable agreement between experimental data and simulations.

## Future Work

- $\text{NO}_x$ -CO speciation data will be collected at higher pressures (1-15atm), considering the effect of different parameters such as hydrocarbons and diluents.
- Effect of exhaust gas recirculation will be investigated.

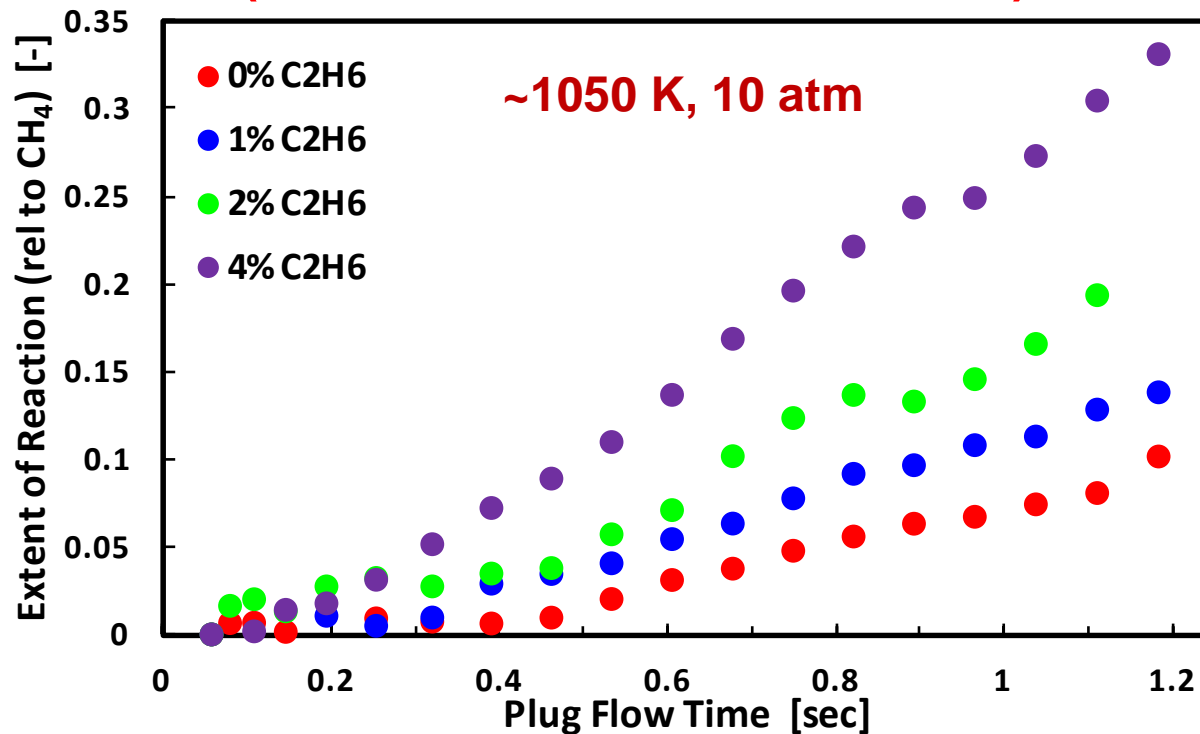


# Small Species Flow Reactor Pyrolysis/Oxidation Database

# NO<sub>x</sub>-perturbed CH<sub>4</sub> + 2% C<sub>2</sub>H<sub>6</sub> “natural gas” oxidation



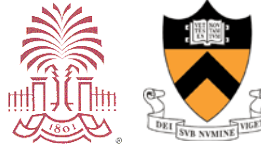
## Effect of increased C<sub>2</sub>H<sub>6</sub> doping in CH<sub>4</sub> (without NO<sub>x</sub> addition) (recap from last UTSR review meeting)



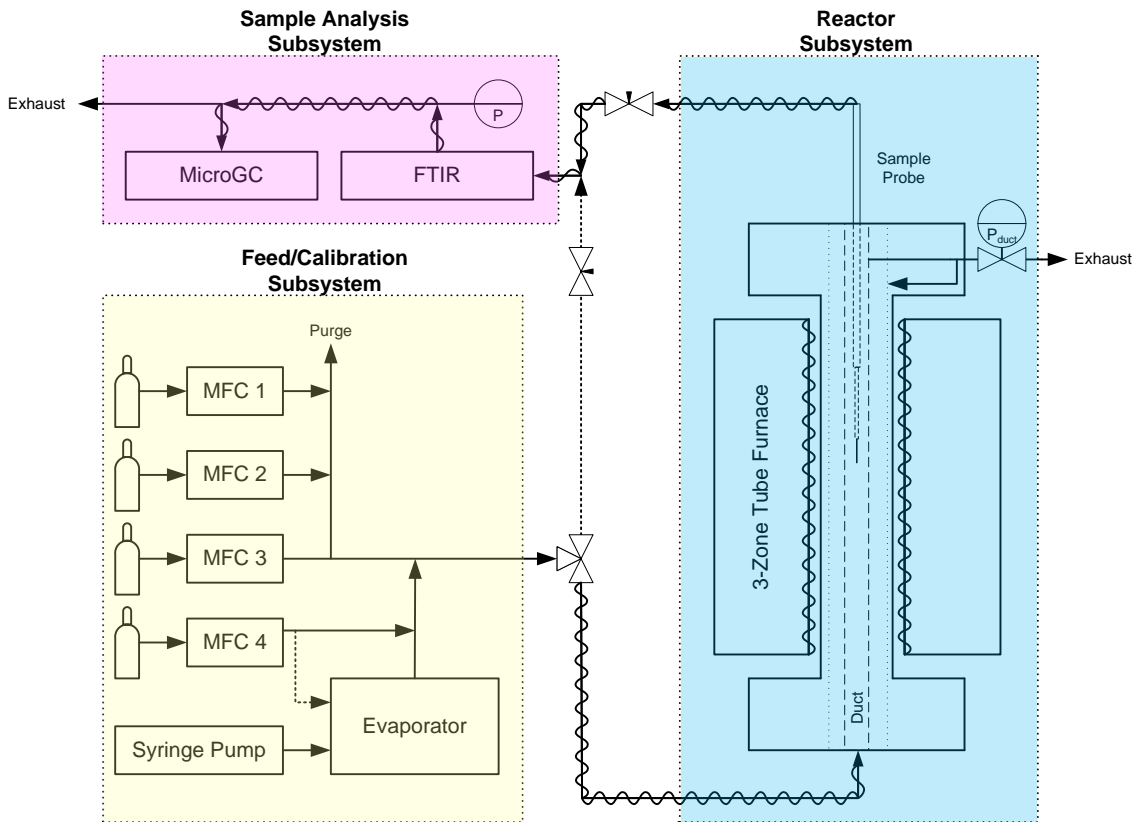
- Overall initial reactivity increases *threefold* for just 4% C<sub>2</sub>H<sub>6</sub> in CH<sub>4</sub>
- Additional reactivity expected with small (< 100 ppm) NO<sub>x</sub> addition
- NO<sub>x</sub> perturbed experiments use 2% C<sub>2</sub>H<sub>6</sub> in CH<sub>4</sub> as a representative “natural gas”



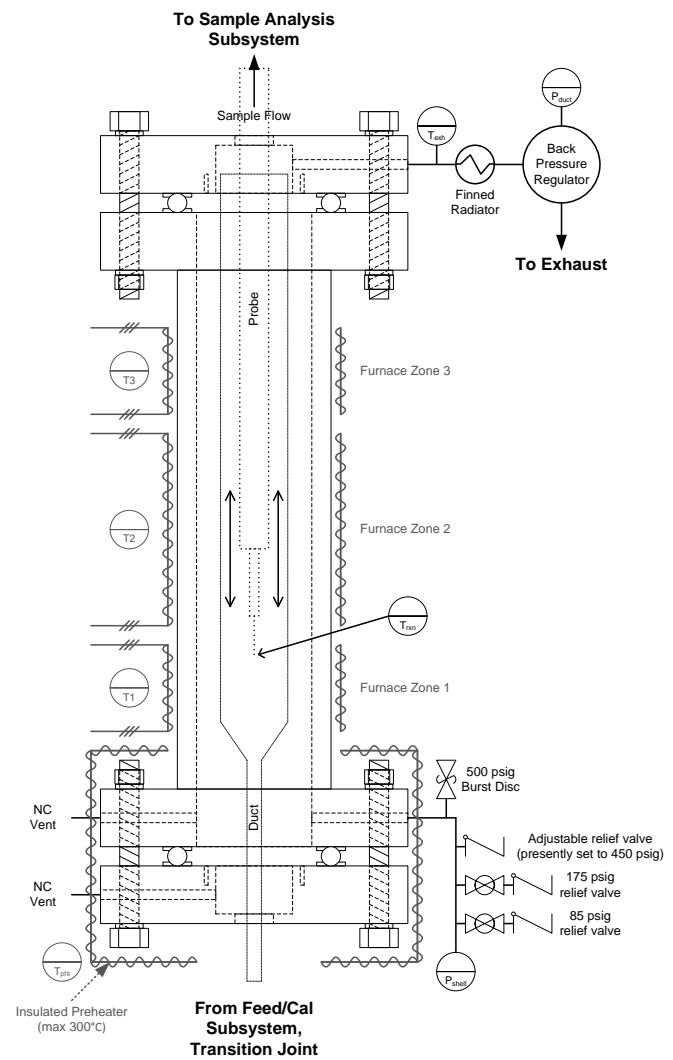
# Experimental Setup: HPLFR Schematics



## Facility Overview



## Reactor Subsystem Detail



# NO<sub>x</sub> Perturbed Methane/Ethane Blend Study in High Pressure Laminar Flow Reactor



- Exploration of intricate interactions between C<sub>1-2</sub> and NO<sub>x</sub> kinetics.
- Constrain/further validate the Fenimore NO<sub>x</sub> mechanism.
- NO<sub>x</sub> kinetics for “Shale Gas” (near-future potential as stationary power generation gas turbines).

## □ Non-Reacting Cases (Nominal Values, ppm)

CH <sub>4</sub>	=	9800	} %C ~ 1.02% Avoids excessive exothermicity
C <sub>2</sub> H <sub>6</sub>	=	200	
O <sub>2</sub>	=	20300 ( $\phi=1.0$ )	
NO	=	Nil	
Ar	=	Balance	

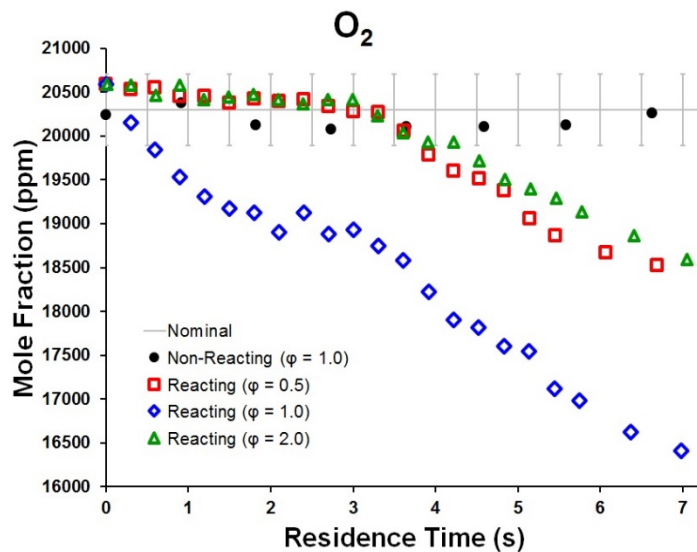
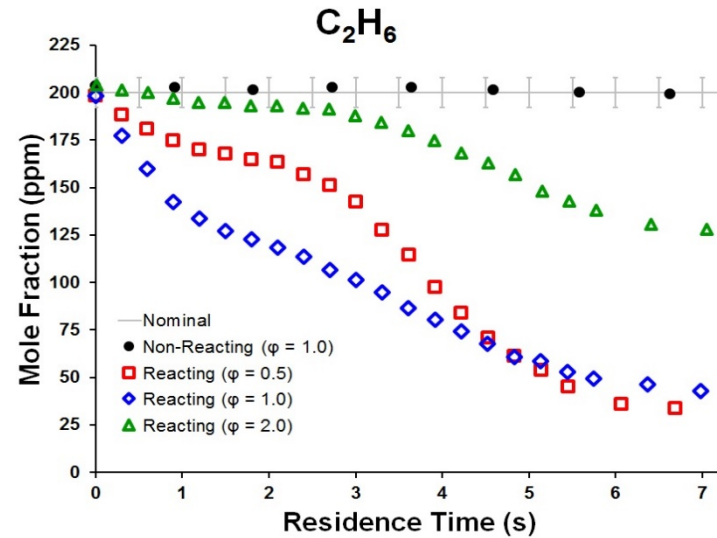
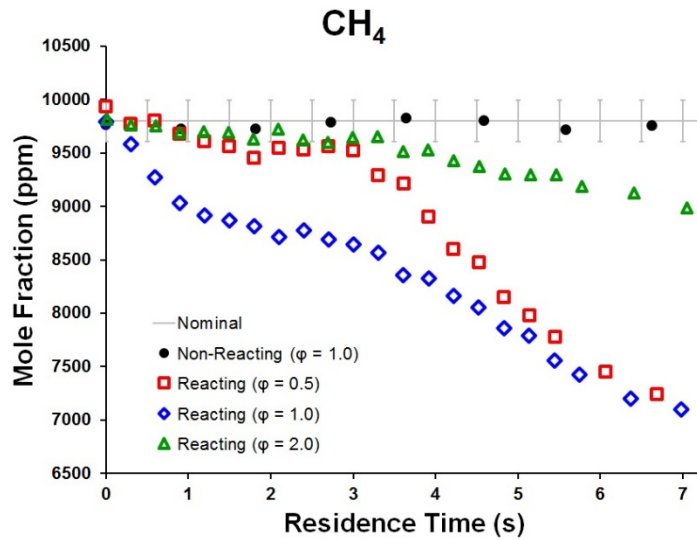
## □ Reacting Cases Run (Nominal Values, ppm)

CH <sub>4</sub>	=	9800
C <sub>2</sub> H <sub>6</sub>	=	200
O <sub>2</sub>	=	20300 ( $\phi=1.0$ ) / 40600 ( $\phi=0.5$ ) / 10150 ( $\phi=2.0$ )
NO	=	25
Ar	=	Balance

## □ P, T & Q<sub>blend</sub> (Nominal Values)

P	=	5 & 10 atm
T	=	820 K
Q <sub>blend</sub>	=	650 sccm & 1300 sccm

# HPLFR Experimental Measurements



## ❖ Measurement Uncertainty

CH<sub>4</sub> ~ 2%

C<sub>2</sub>H<sub>6</sub> ~ 4%

O<sub>2</sub> ~ 2%

## ❖ Illustration of O<sub>2</sub> measurement for rich & lean condition is scaled with respect to $\phi = 1.0$ case

## ❖ Quantification in progress for CO CO<sub>2</sub> C<sub>2</sub>H<sub>2</sub> H<sub>2</sub>O

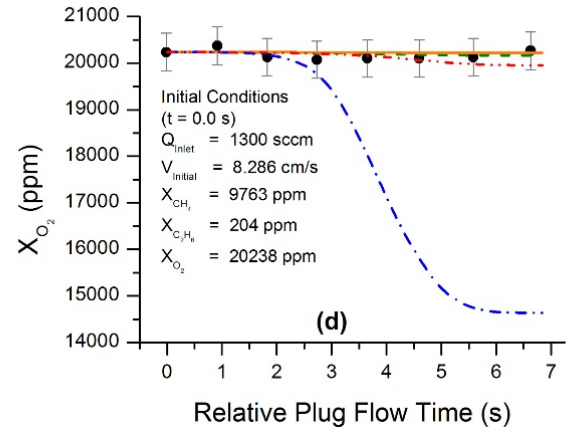
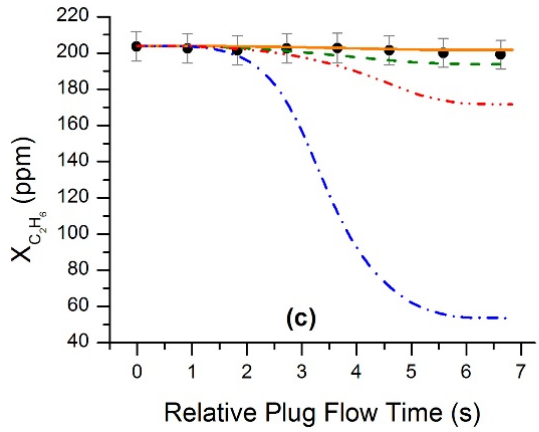
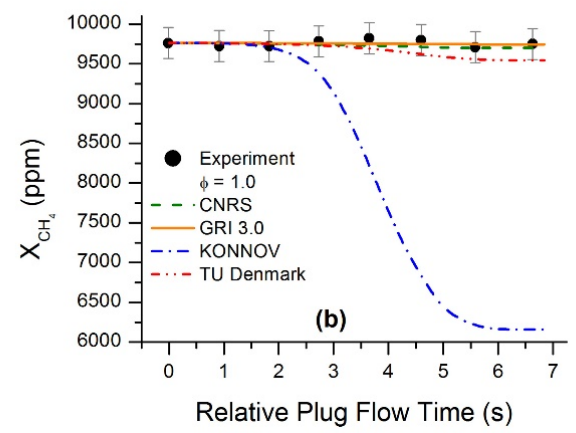
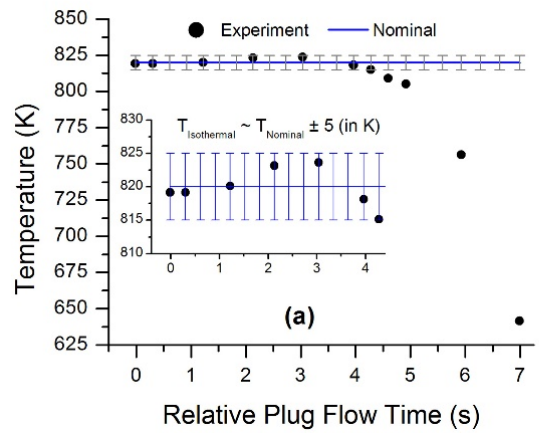
# Simulation # Non-Reacting Case

**P (Nominal) = 10 atm**  
**T (Nominal) = 820 K**  
 **$\Phi = 1.0$**

**NO<sub>x</sub> is not introduced**

**Fuel conversion is not observed.**

**Konnov et al. (2009) is particularly overly reactive under non-reacting condition !!!**



**GRI 3** # <http://combustion.berkeley.edu/gri-mech/>  
**CNRS** # R. Sivaramakrishnan et al, PCCP (2007)  
**KONNOV** # A.A. Konnov, C&F (2009)  
**TU Denmark** # S. Gersen et al, POCl (2011)

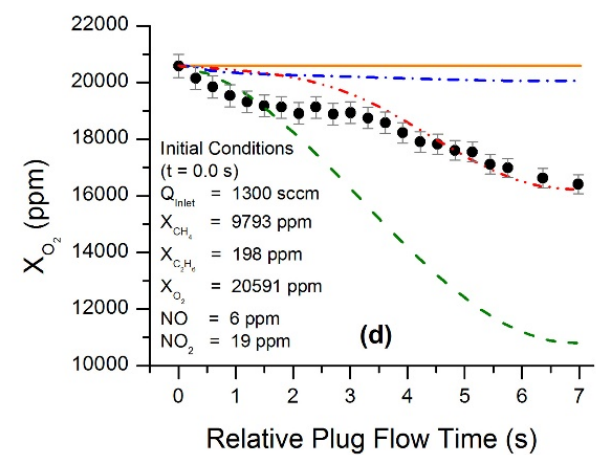
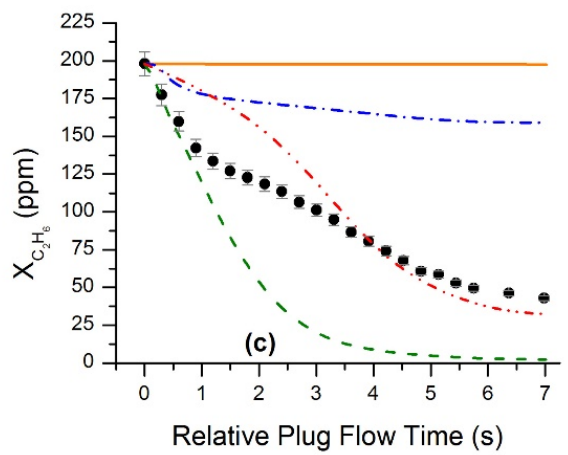
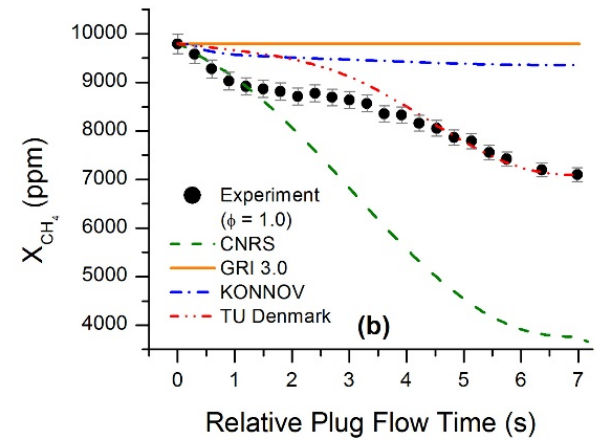
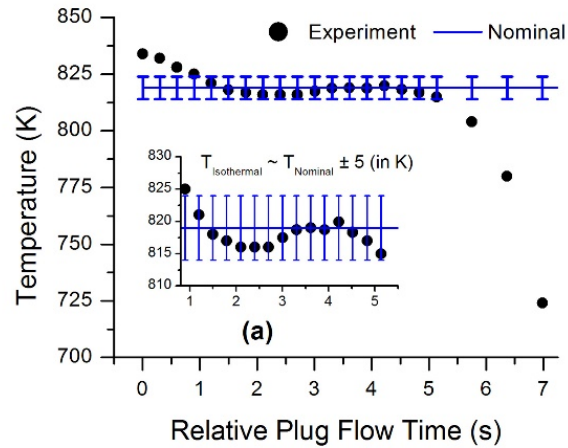
# Simulation # Reacting Case (with NO<sub>x</sub>)

**P (Nominal) = 10 atm**  
**T (Nominal) = 819 K**  
**Φ = 1.0**  
**NO = 25 ± 1 ppm**

**Trace NO can enhance reactivity substantially !**

**CNRS is over-reactive whilst KONNOV mechanism is less reactive, even under reacting environment !!**

**TU Denmark predicts the best !!! Includes Nitro-methane/ethane chemistry.**

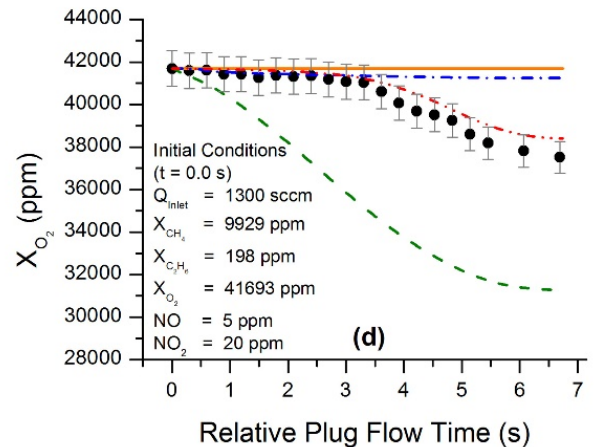
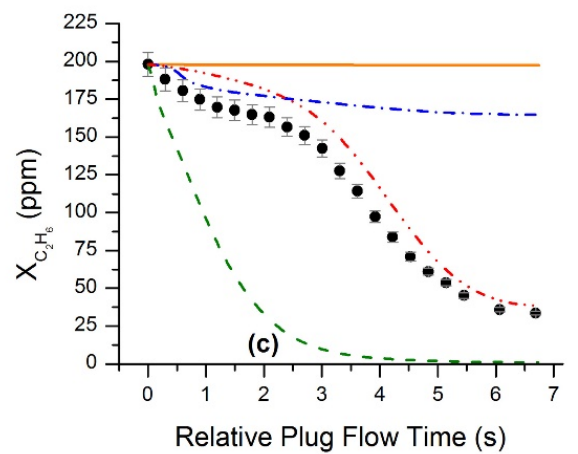
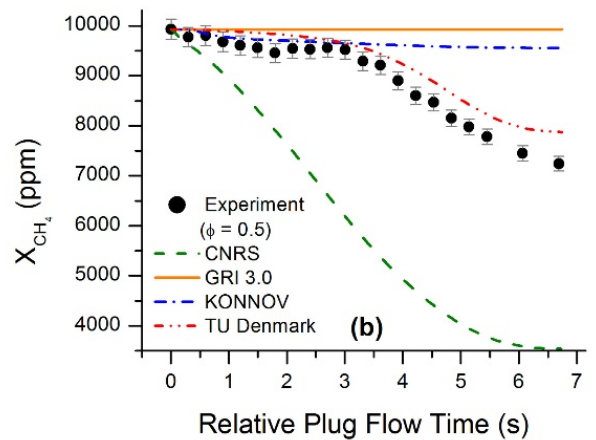
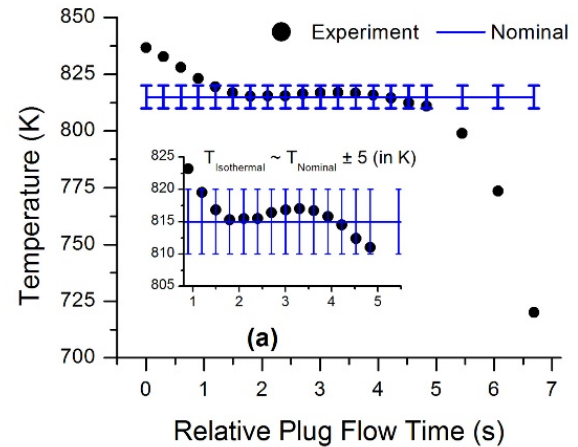


# Simulation # Reacting Case (with NO<sub>x</sub>)



**P (Nominal) = 10 atm**  
**T (Nominal) = 815 K**  
**Φ = 0.5**  
**NO = 25 ± 1 ppm**

**Chemkin-Pro based imposed temperature profile Plug flow reactor (PFR) Model is used to simulate all three reacting cases**

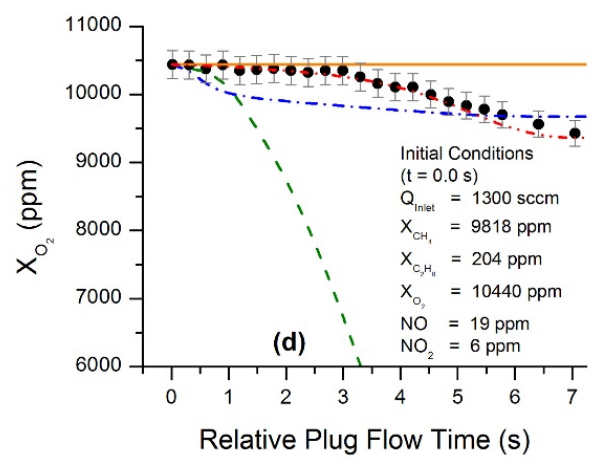
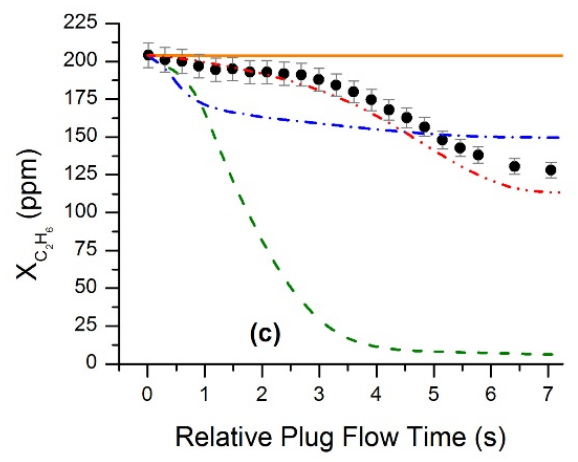
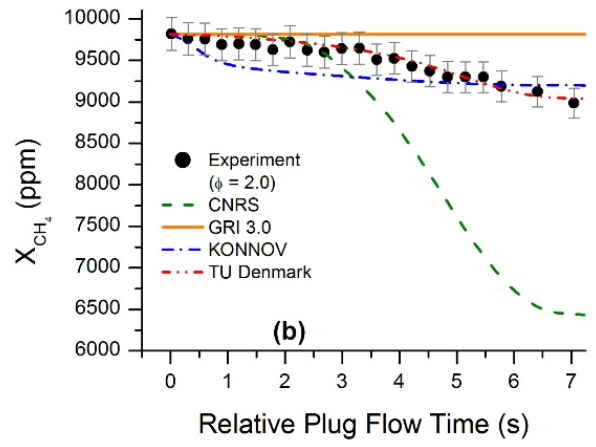
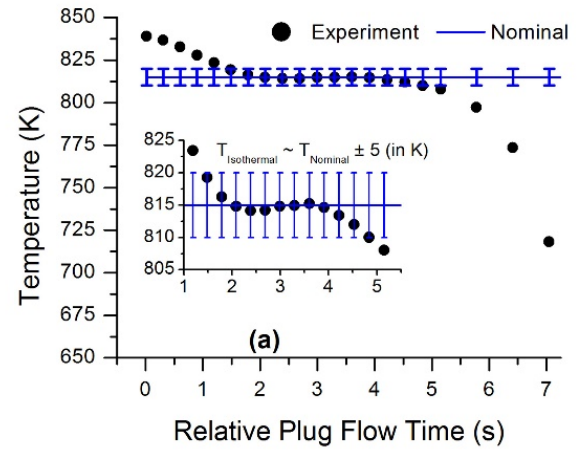




# Simulation # Reacting Case (with NO<sub>x</sub>)



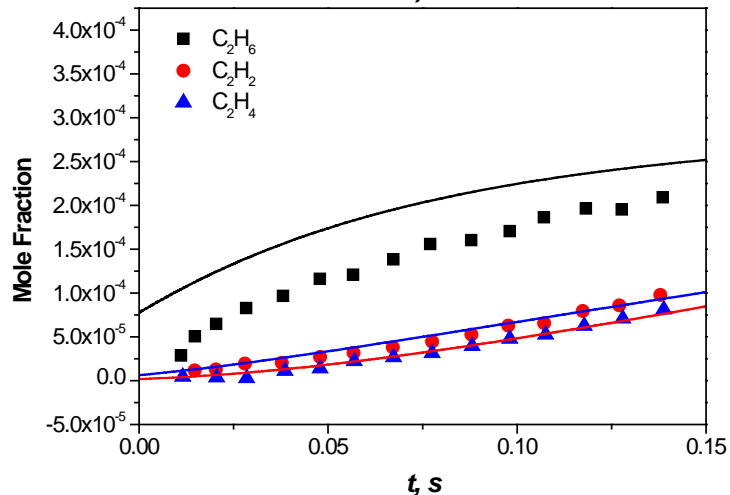
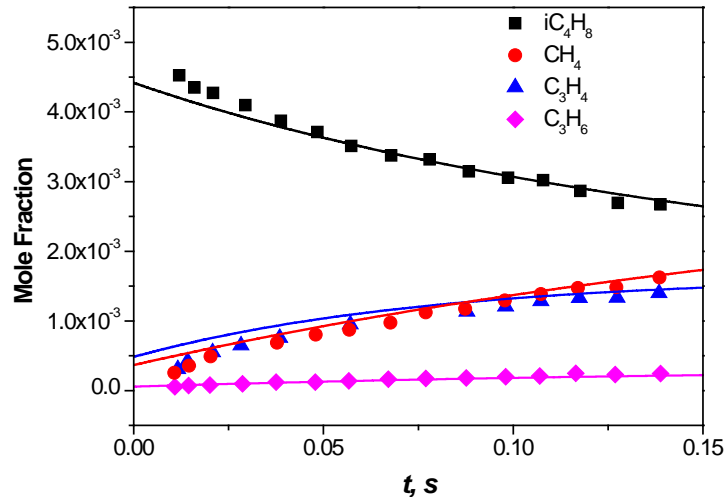
**P (Nominal) = 10 atm**  
**T (Nominal) = 815 K**  
 **$\Phi = 2.0$**   
**NO = 25 ± 1 ppm**





## Isobutene pyrolysis/oxidation near 1145 K

5000 ppm  $iC_4H_8$ ,  $\phi = \infty$

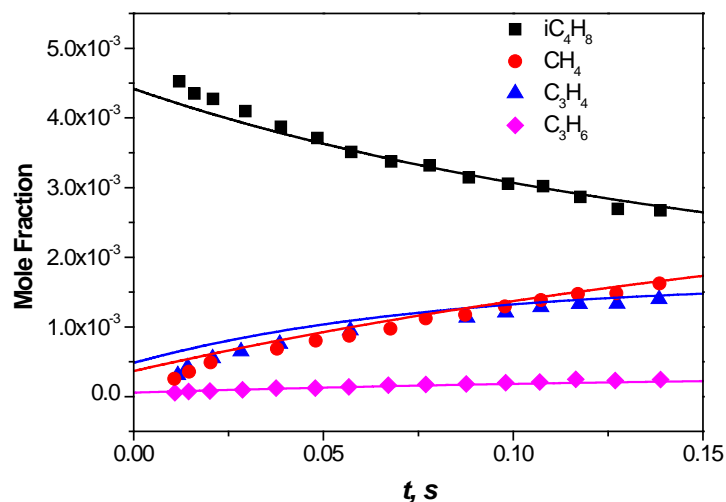


- Isobutene is a significant intermediate from isobutane oxidation
- Oxidation is relatively slow due to resonantly-stabilized isobutenyl radical
  - Pyrolytic pathways are competitive with oxidative ones
- Limited (reliable) pyrolysis data available in the literature
- Present flow reactor data motivated significant revisions to  $iC_4H_8$  pyrolysis kinetics of previous model iteration
- Major/minor species generally predicted well, with some over prediction of  $C_2H_6$  likely due to consumption pathways (i.e., not formation via  $CH_3$  recombination)

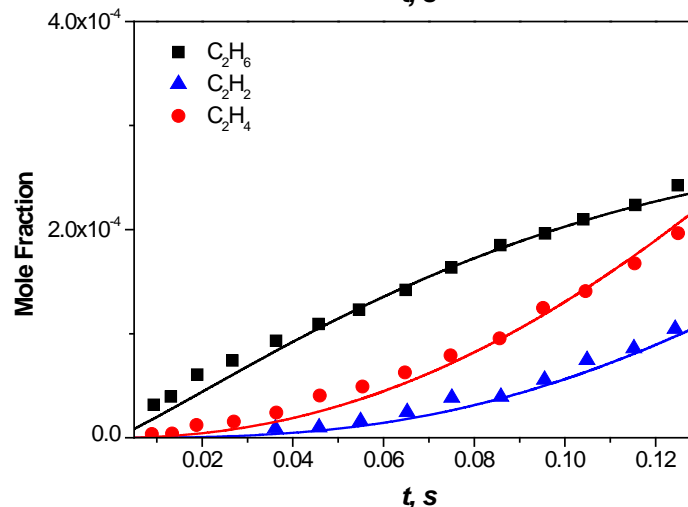
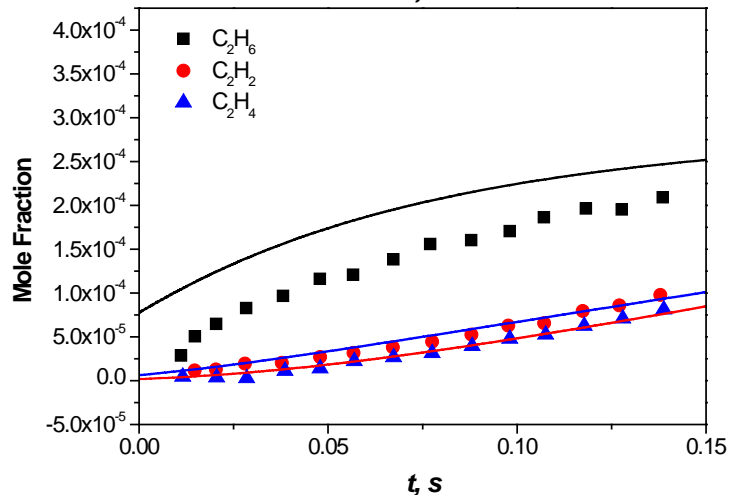
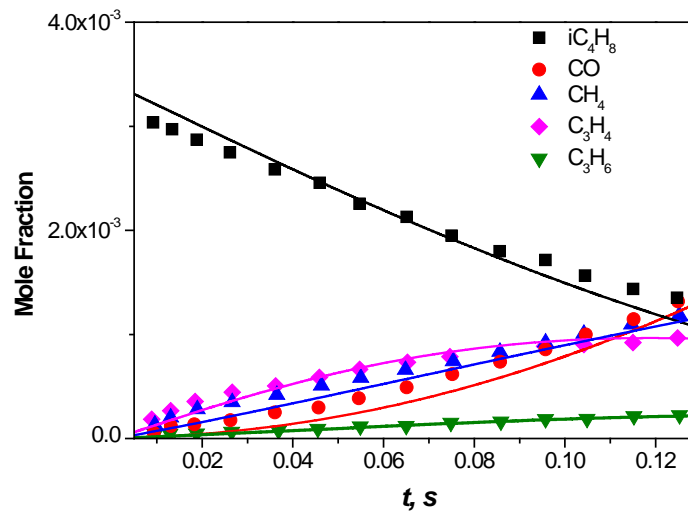
# Additional Small Species Database Efforts

## Isobutene pyrolysis/oxidation near 1145 K

5000 ppm  $iC_4H_8$ ,  $\phi = \infty$



3400 ppm  $iC_4H_8$ ,  $\phi = 0.91$



Also measurements for  $\sim 3400$  ppm  $iC_4H_8$  at  $\phi = 0.42$  and  $\phi = 1.29$

# Experimental Measurements with (In-Progress) Modeling



## Isobutane oxidation

- Six speciated oxidation experiments at temperatures similar to isobutene experiments discussed:

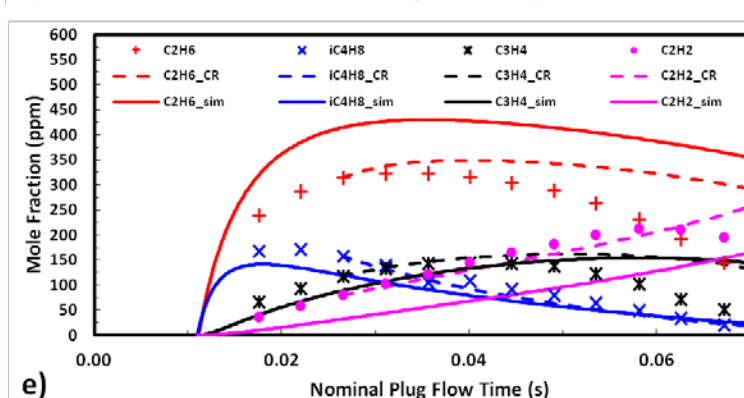
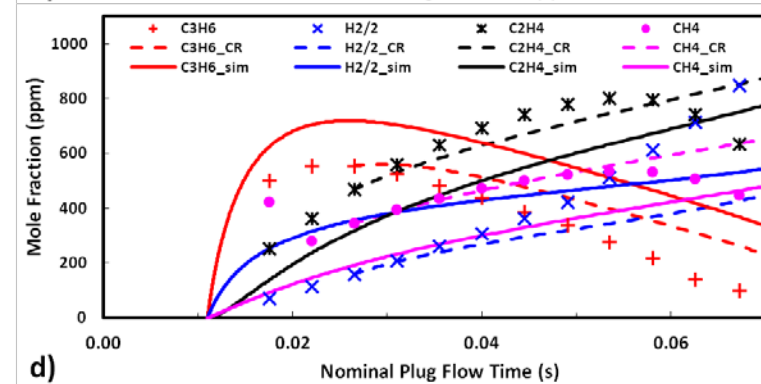
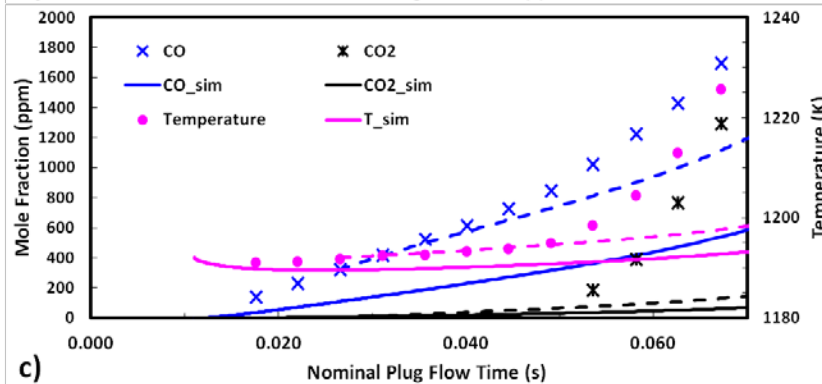
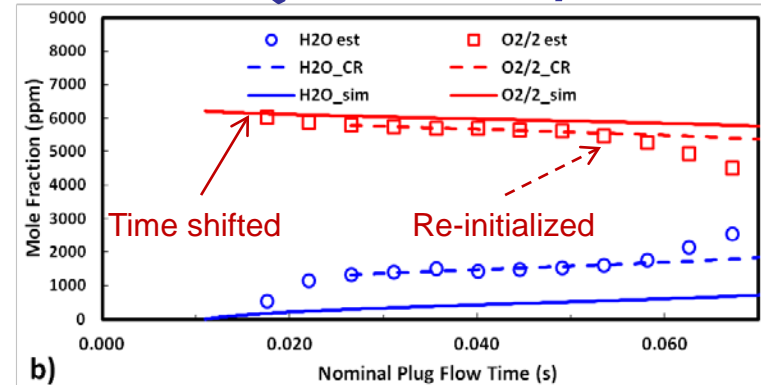
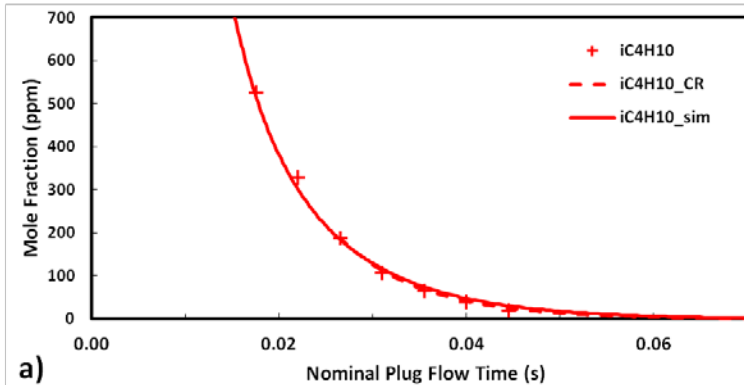
Experiment Reference	Nominal Initial Conditions			
	Temperature (K)	iC4H10 (ppm)	O2 (ppm)	Nominal $\phi$
IB1	1154	850	18100	0.3
IB2	1191	1500	12400	0.8
IB3	1184	2400	10400	1.5
IB4	1110	1100	23900	0.3
IB5	1152	1600	15100	0.7
IB6	1225	1500	6050	1.6

- Present modeling efforts focused on testing robustness of assumed initial conditions (ideal zero dimensional vs. time-shift vs. computational re-initialization vs. others)
- Updated kinetic sub-model for isobutene has yet to be tested against present flow reactor isobutane data

# Experimental Measurements with (In-Progress Modeling)

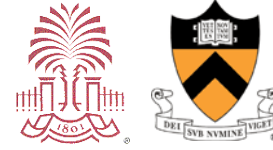


## Isobutane oxidation – Case IB2 (1191 K, 1 atm)



- Consumption of  $iC_4H_{10}$  and daughter  $iC_4H_8$  predicted well
- Discrepancies primarily due to under-predicted T evolution?
- Effect of updated  $iC_4H_8$  sub-model?

# Overall Summary

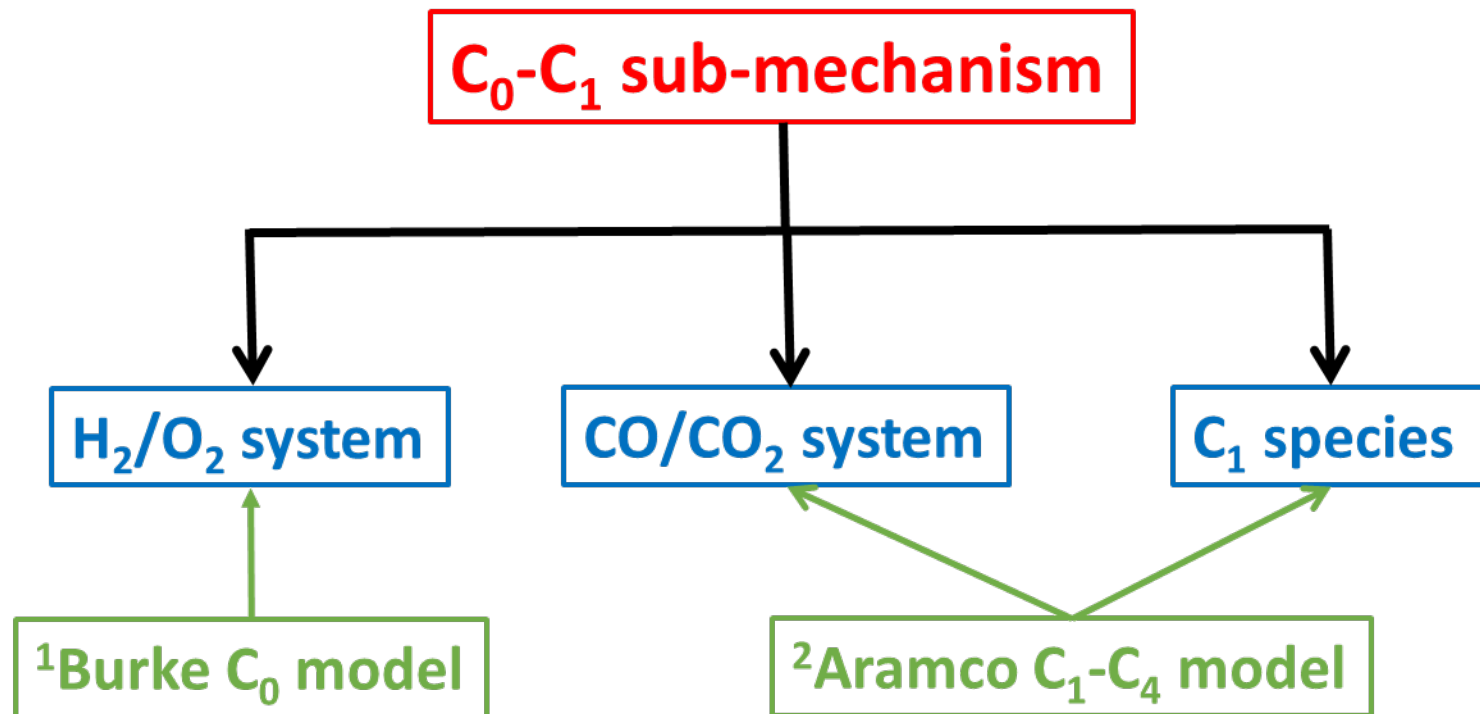
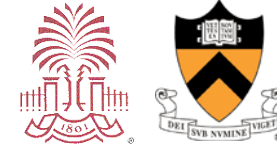


- $H_2/CO/NO_x$  model developed validated against a large dataset
- $C_0 - C_4 NO_x$  is being developed
- Chemical and physical perturbation effects on global combustion markers
- Atmospheric pressure burner experiments, flame- post flame speciation, temperature measurements
- Multi-dimensional CFD model with detailed chemical kinetics
- Species-resolved measurements from flow reactor oxidation of small hydrocarbon species ( $C_4$  and smaller) and  $H_2$  add to the database of experimental measurements relevant to improving the fidelity of high hydrogen content (HHC) fuels and natural gas combustion predictions for gas turbine applications
- Present database considers fuels composed of  $H_2$ ,  $CH_4$ ,  $C_2H_6$  (with significant  $C_2H_4$  daughter intermediates),  $C_3H_6$ ,  $iC_4H_8$ , and  $iC_4H_{10}$ . Oxidation may be in presence/absence of added trace  $NO_x$
- Modeling efforts are ongoing and are considering not only different available kinetic models, but also assumptions regarding initial conditions
- Detailed and reduced model constructs will be available



**Thank You**

# Model Elements: Proposed H<sub>2</sub>/CO/NO<sub>x</sub> Model

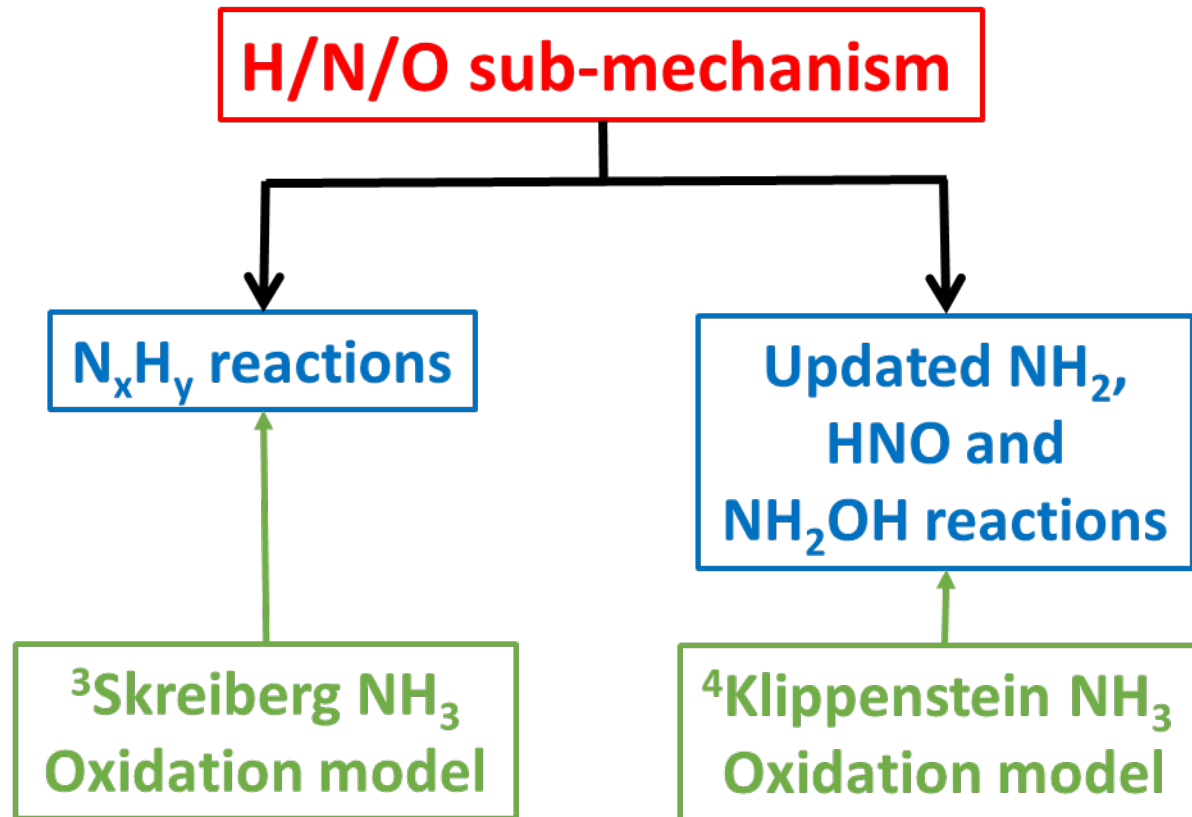


<sup>1</sup>Burke et al., Int. J. Chem. Kinet. 44 (2012)

<sup>2</sup>Metcalf et al., Int. J. Chem. Kinet. 45 (2013)

*No HOCO chemistry  
considered*

# Model Elements: Proposed H<sub>2</sub>/CO/NO<sub>x</sub> Model

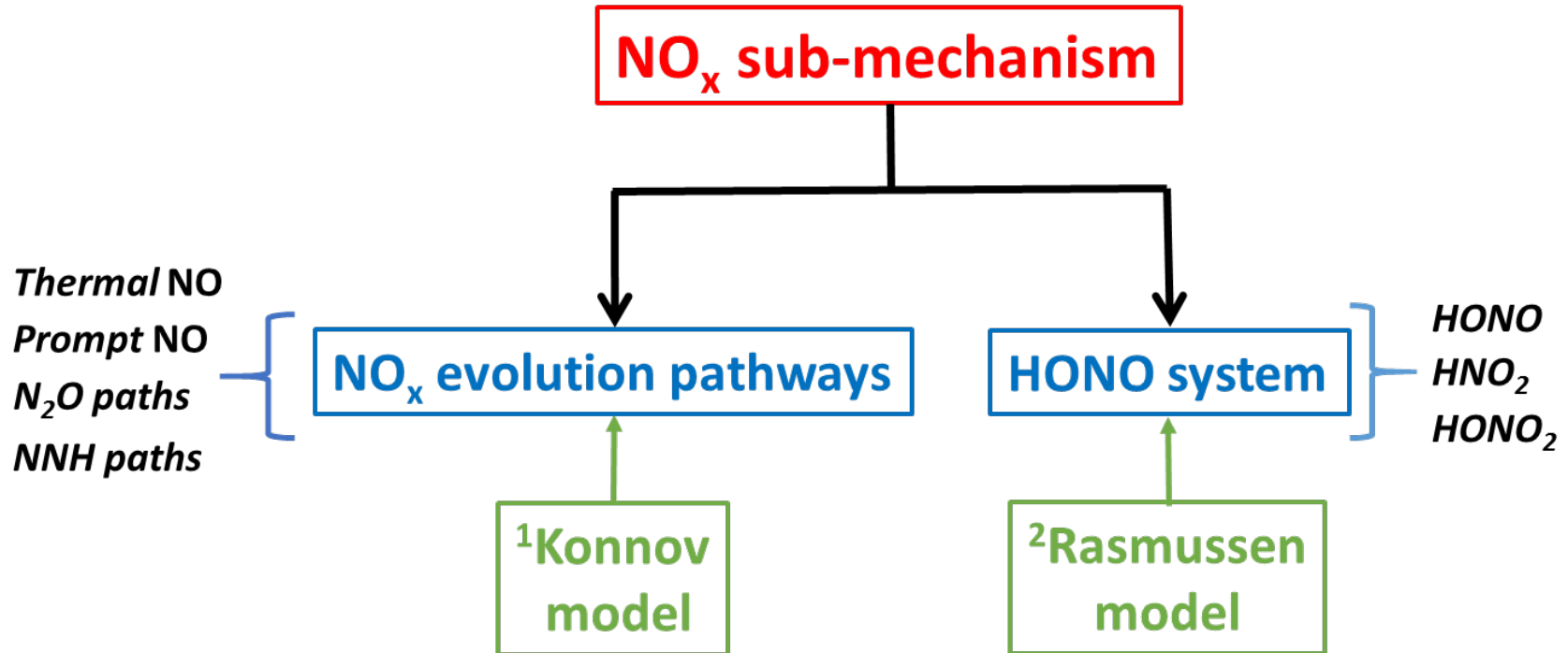


<sup>3</sup>Skreiberg et al., Combust. Flame 136 (2004)

<sup>4</sup>Klippenstein et al., Combust. Flame 158 (2011)



# Model Elements: Proposed H<sub>2</sub>/CO/NO<sub>x</sub> Model

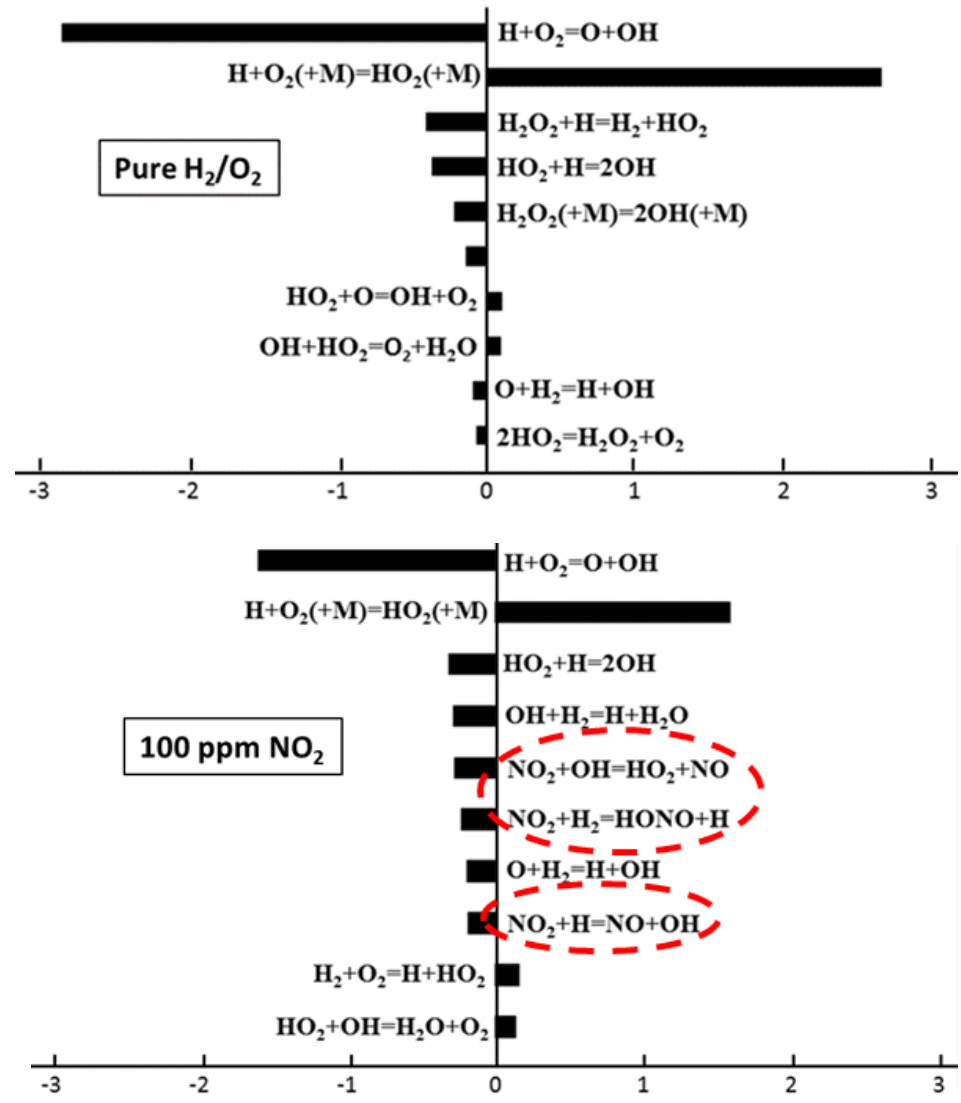
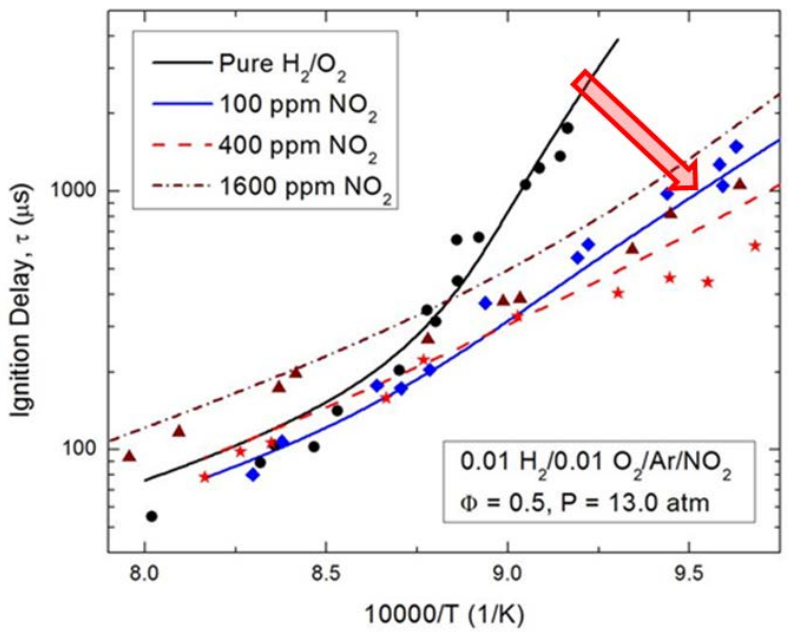


<sup>1</sup>Konnov et al., Combust. Flame 156 (2009)

<sup>2</sup>Rasmussen et al., Int. J. Chem. Kinet. 40 (2008)

# Proposed Model Performance: Ignition Delay

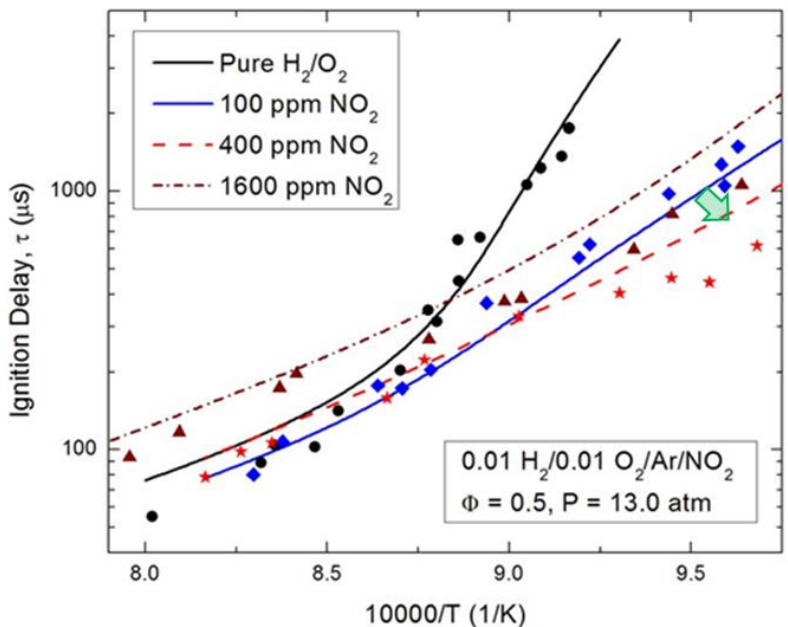
## Dependence of $\tau_{ig}$ on initial $\text{NO}_2$ doping for $\text{H}_2/\text{O}_2$ system



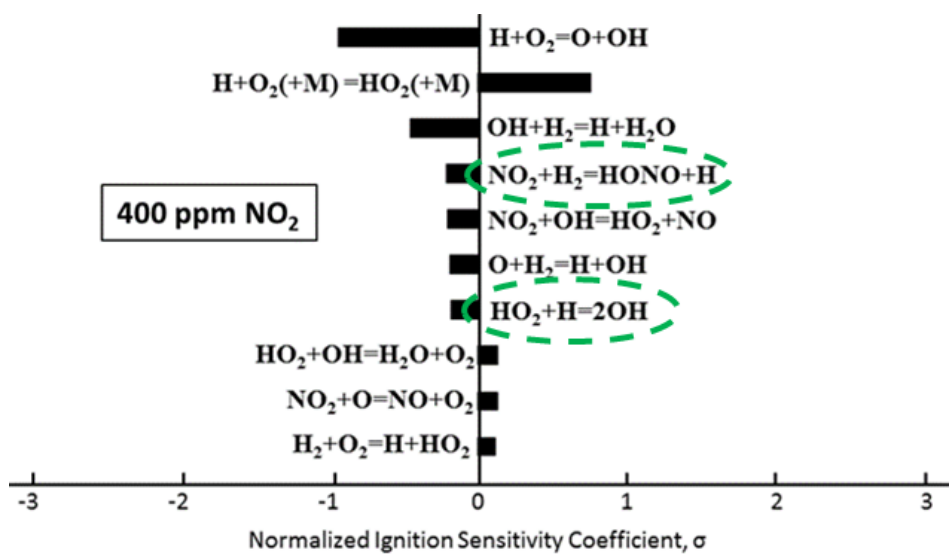
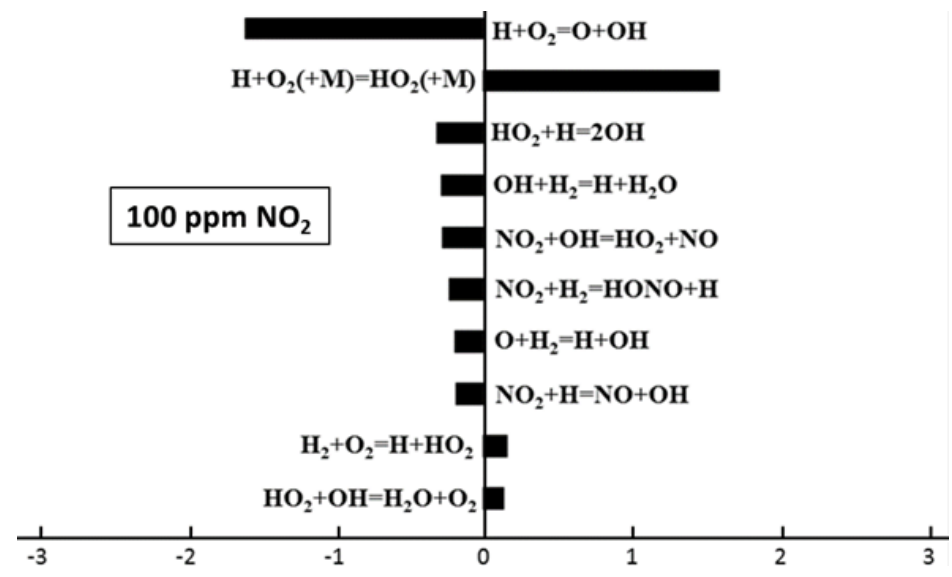
**High pressure non-monotonic behavior captured by the model**

# Proposed Model Performance: Ignition Delay

## Dependence of $\tau_{ig}$ on initial $\text{NO}_2$ doping for $\text{H}_2/\text{O}_2$ system

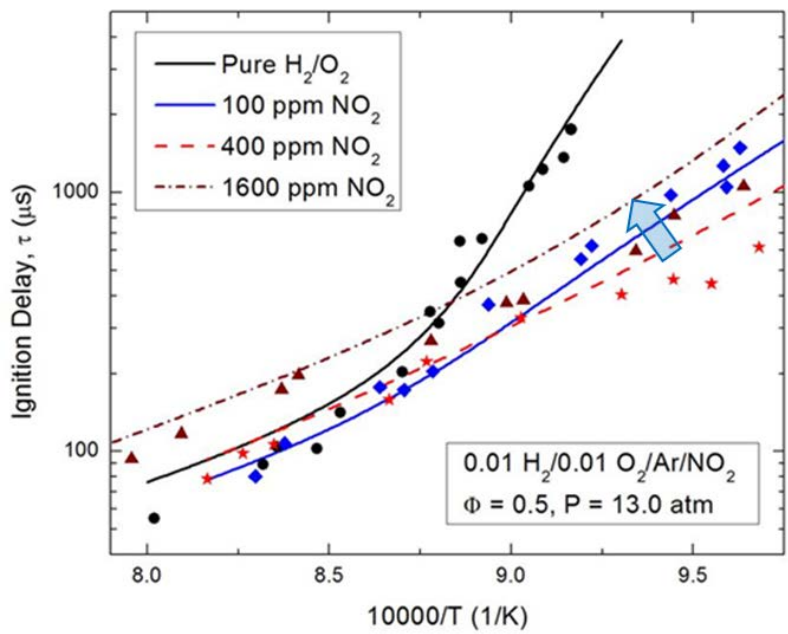


**High pressure non-monotonic behavior captured by the model**

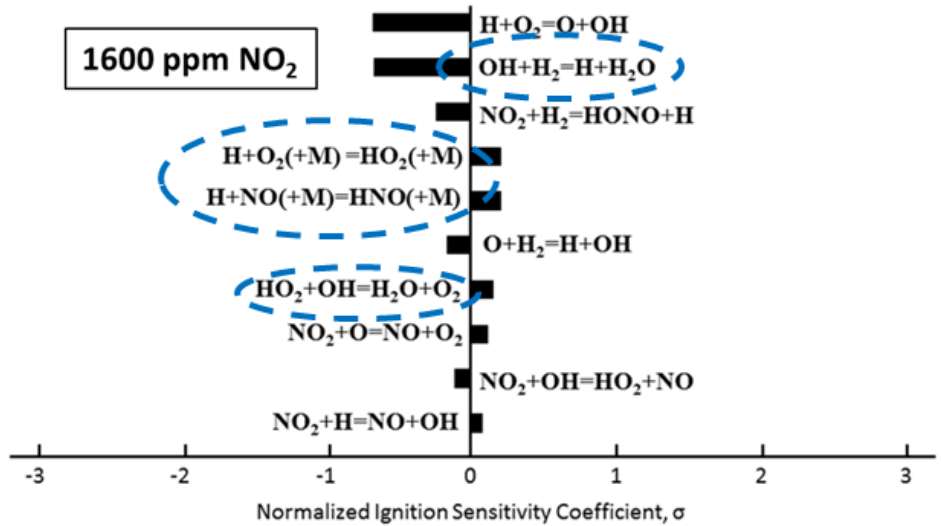
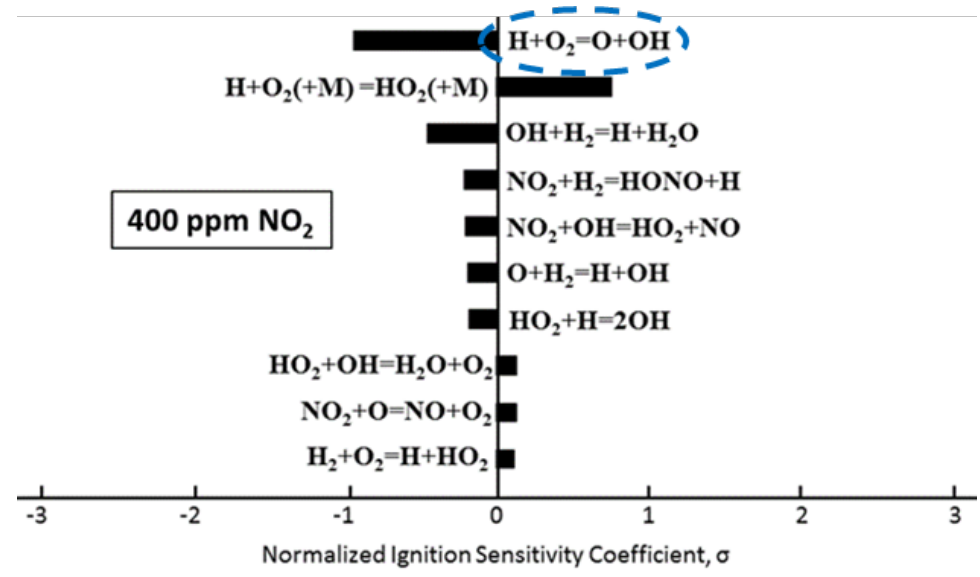


# Proposed Model Performance: Ignition Delay

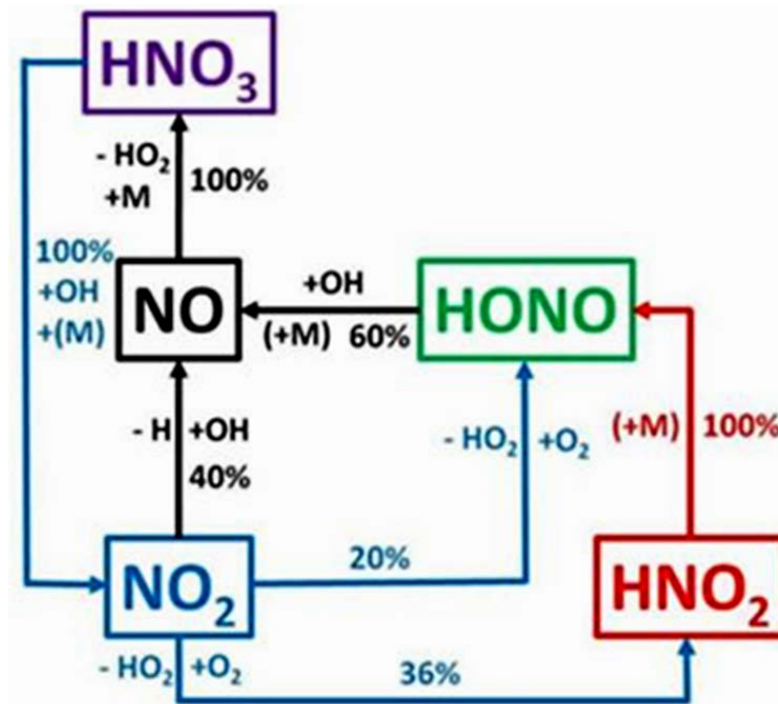
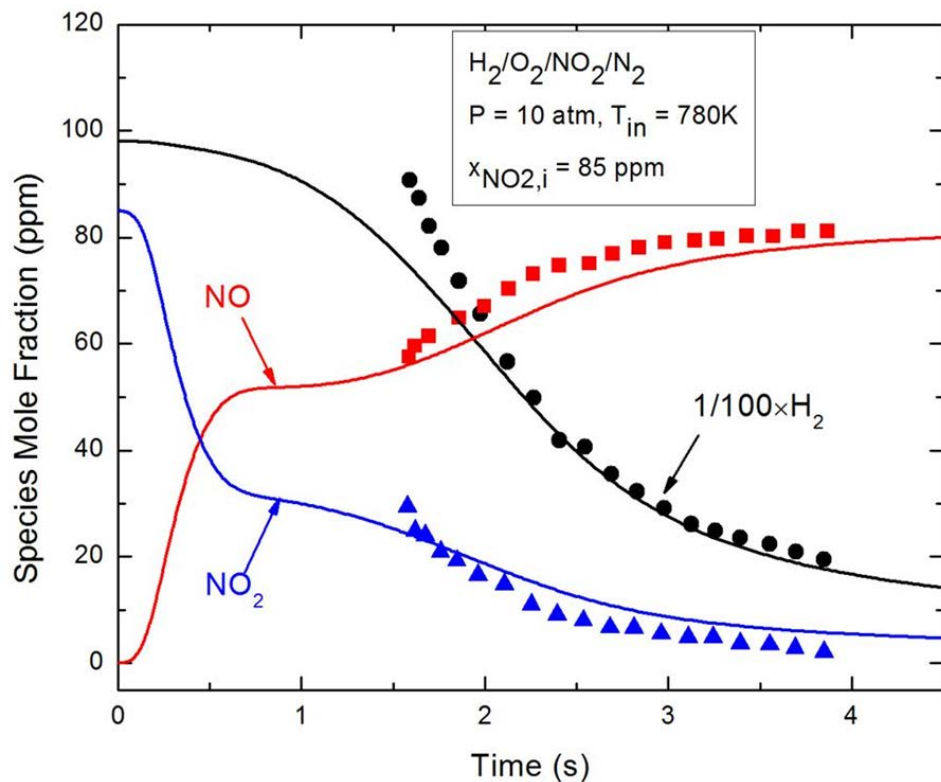
## Dependence of $\tau_{ig}$ on initial $\text{NO}_2$ doping for $\text{H}_2/\text{O}_2$ system



**High pressure non-monotonic behavior captured by the model**



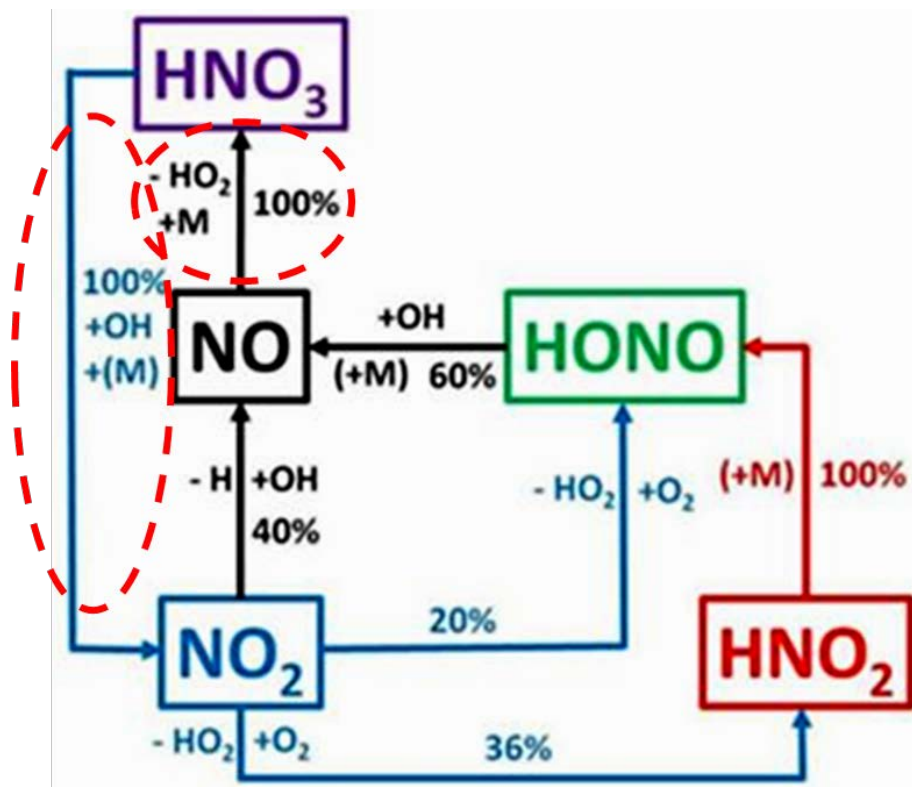
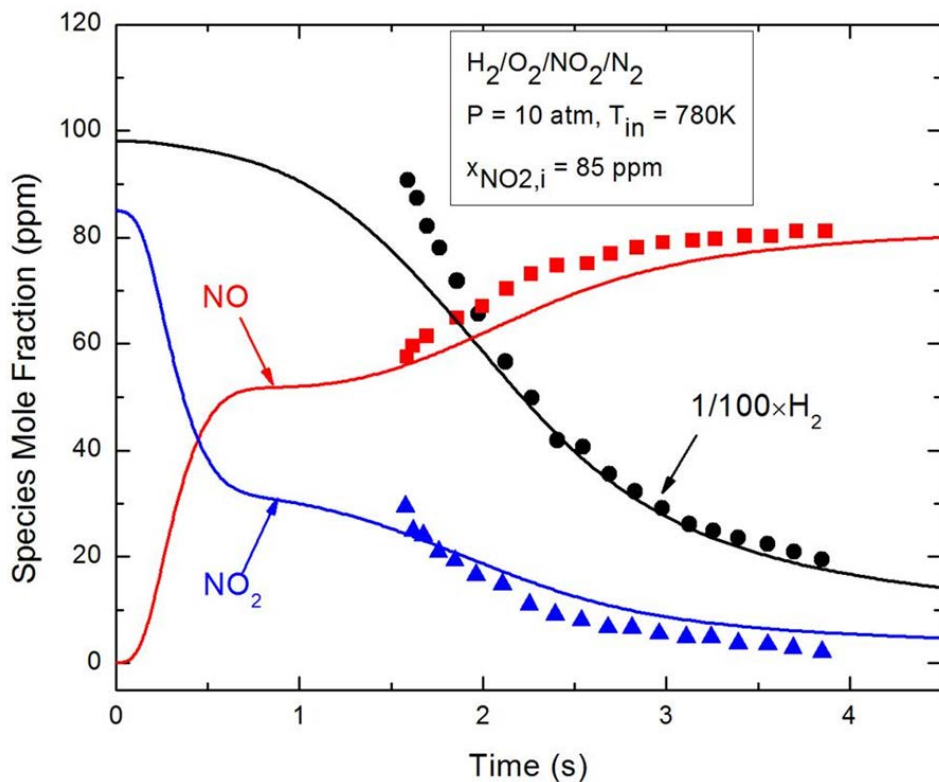
# Proposed Model Performance: PFR Speciation for $H_2/O_2/NO_2/N_2$ System



Major reaction pathways of NO-NO<sub>2</sub> recycling process

**Reasonable model prediction of fuel consumption and NO-NO<sub>2</sub> conversion**

# Proposed Model Performance: PFR Speciation for $\text{H}_2/\text{O}_2/\text{NO}_2/\text{N}_2$ System

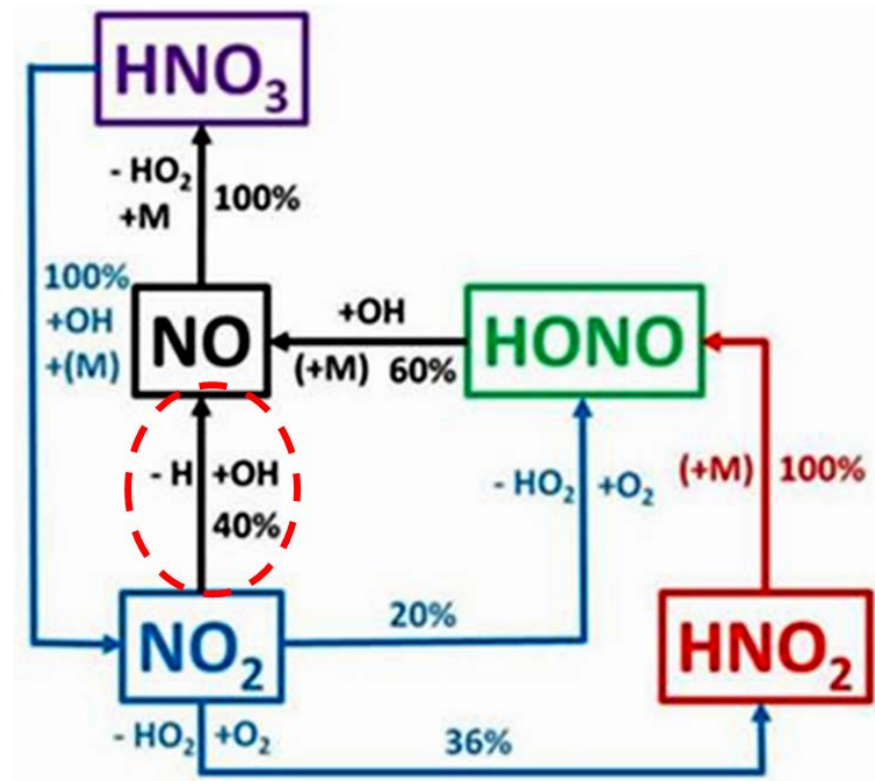
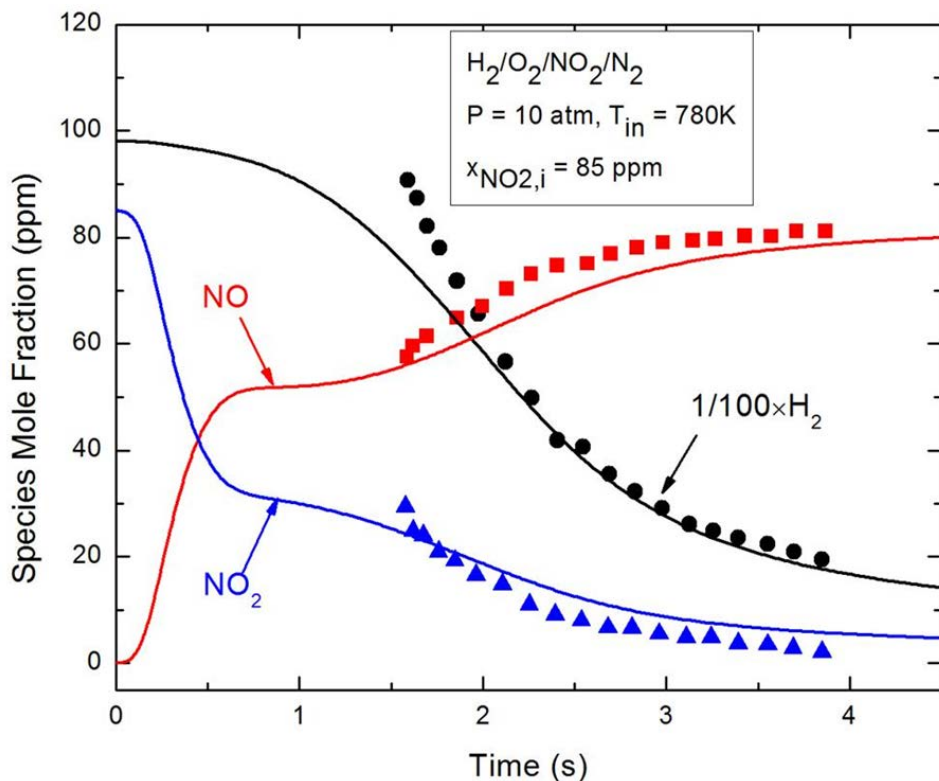


**Reasonable model prediction of fuel consumption and NO-NO<sub>2</sub> conversion**

NO → NO<sub>2</sub> conversion: through intermediate HNO<sub>3</sub>



# Proposed Model Performance: PFR Speciation for $\text{H}_2/\text{O}_2/\text{NO}_2/\text{N}_2$ System

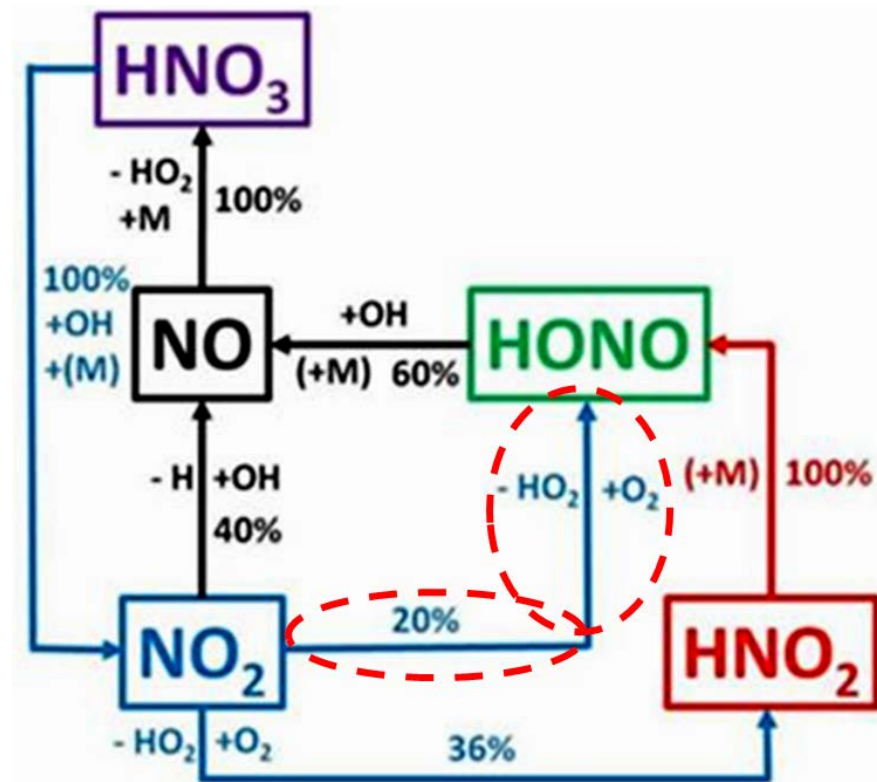
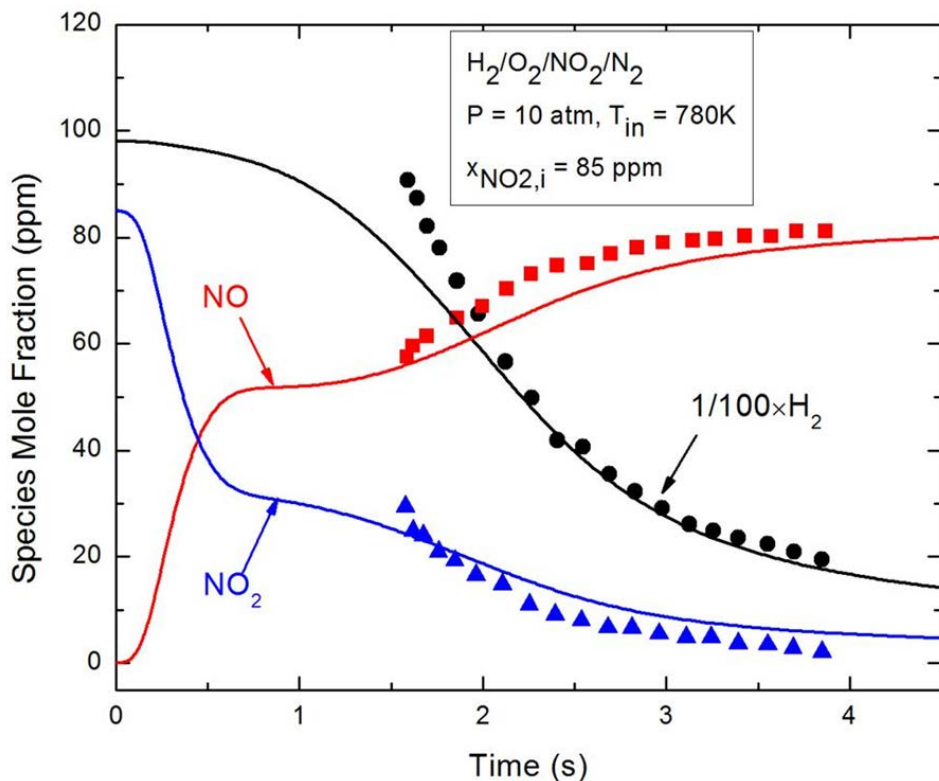


**Reasonable model prediction of fuel consumption and NO-NO<sub>2</sub> conversion**

NO → NO<sub>2</sub> conversion: through intermediate HNO<sub>3</sub>

NO<sub>2</sub> → NO conversion: (i) **direct**

# Proposed Model Performance: PFR Speciation for $\text{H}_2/\text{O}_2/\text{NO}_2/\text{N}_2$ System



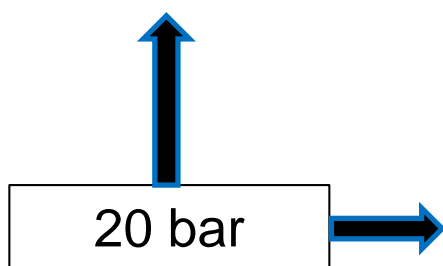
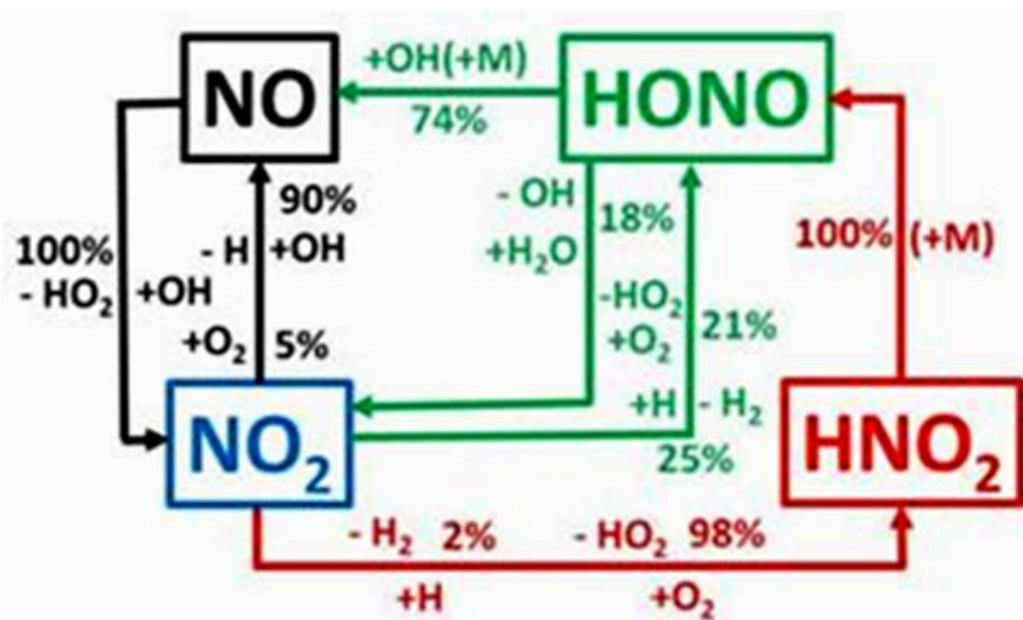
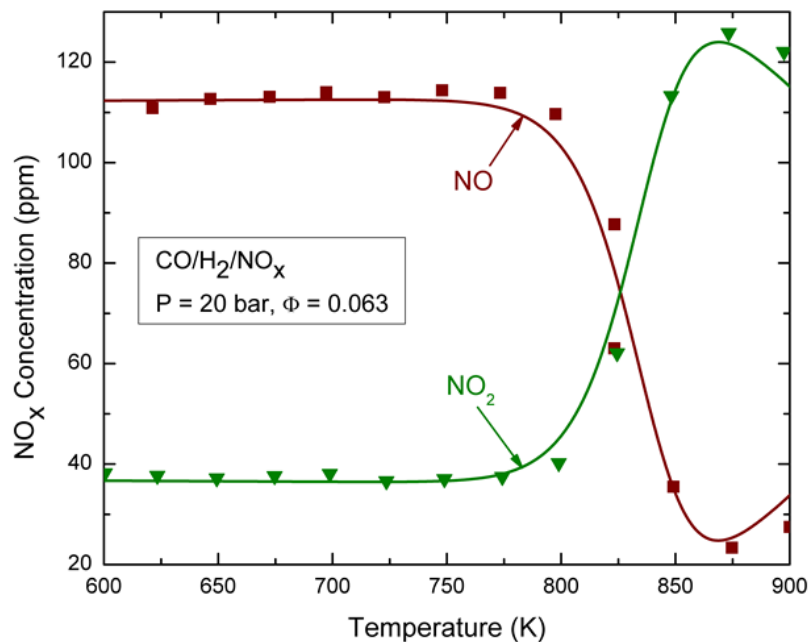
**Reasonable model prediction of fuel consumption and NO-NO<sub>2</sub> conversion**

NO → NO<sub>2</sub> conversion: through intermediate HNO<sub>3</sub>

NO<sub>2</sub> → NO conversion: (i) direct  
(ii) through intermediate HONO



# Proposed Model Performance: PFR Species Evolution for CO/H<sub>2</sub>/NO<sub>x</sub> Oxidation System

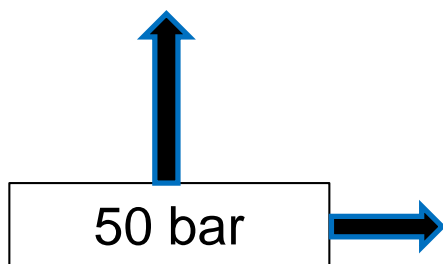
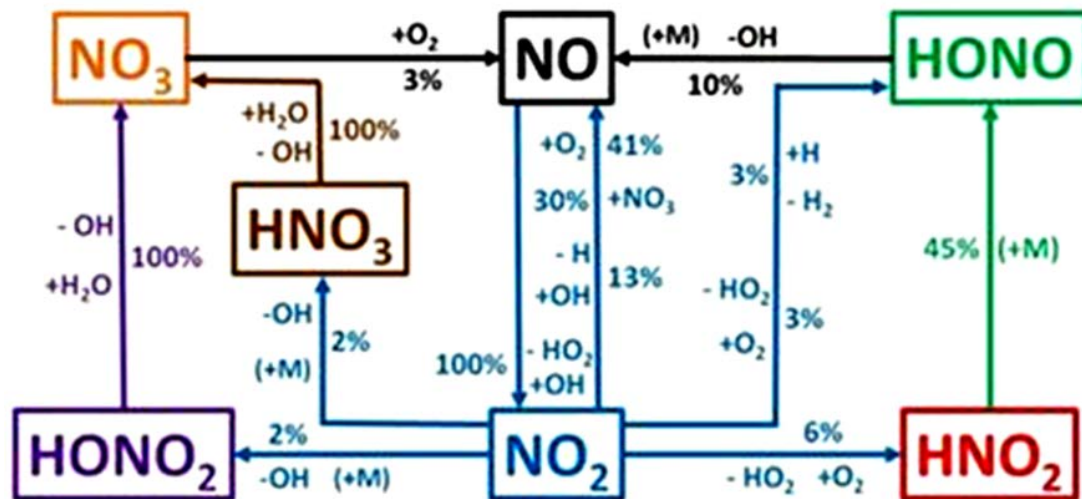
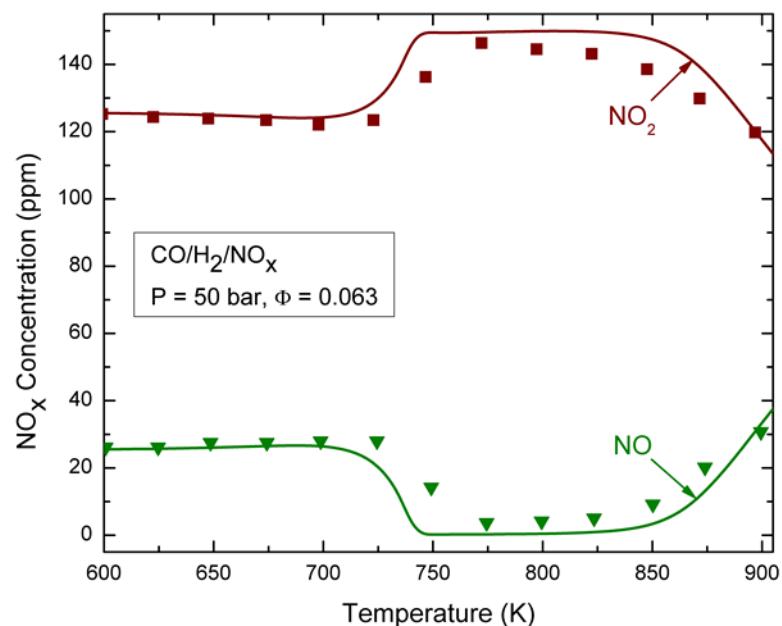


**NO**  $\leftrightarrow$  **NO<sub>2</sub>**: (i) direct

(ii) through intermediate **HONO**

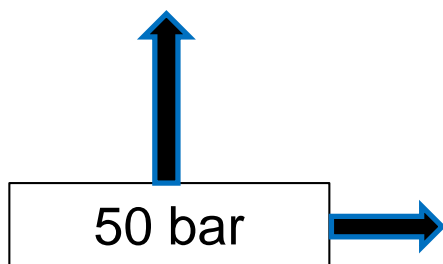
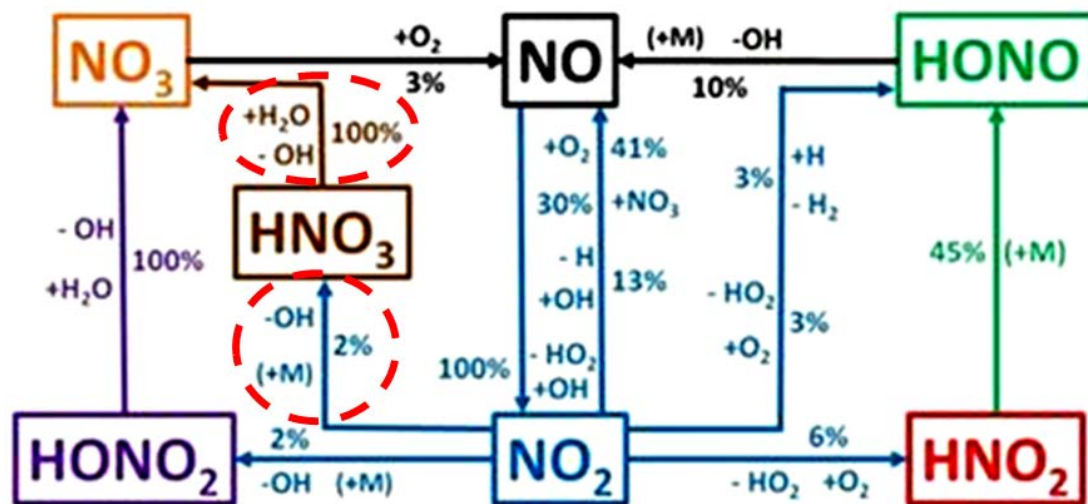
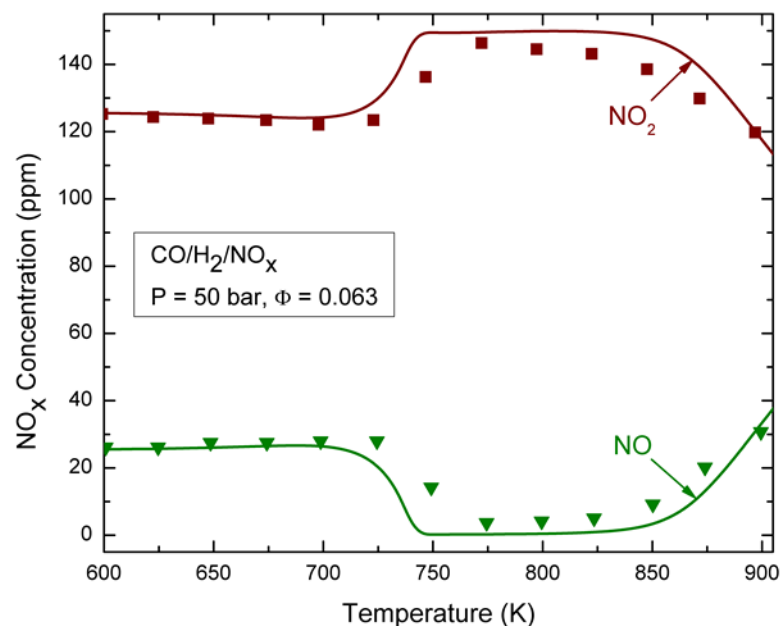
(iii) through intermediate **HNO<sub>2</sub>**

# Proposed Model Performance: PFR Species Evolution for CO/H<sub>2</sub>/NO<sub>x</sub> Oxidation System



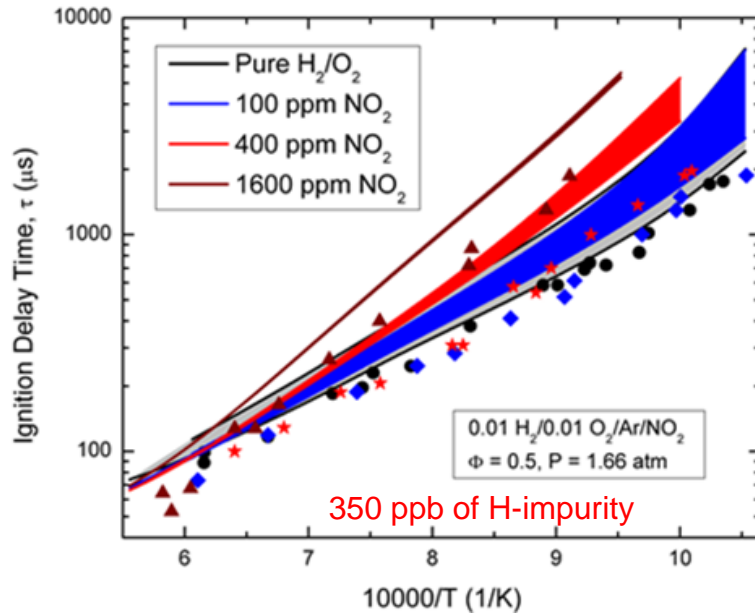
**Dominance of pressure-dependent reactions: two additional NO  $\leftrightarrow$  NO<sub>2</sub>**

# Proposed Model Performance: PFR Species Evolution for CO/H<sub>2</sub>/NO<sub>x</sub> Oxidation System

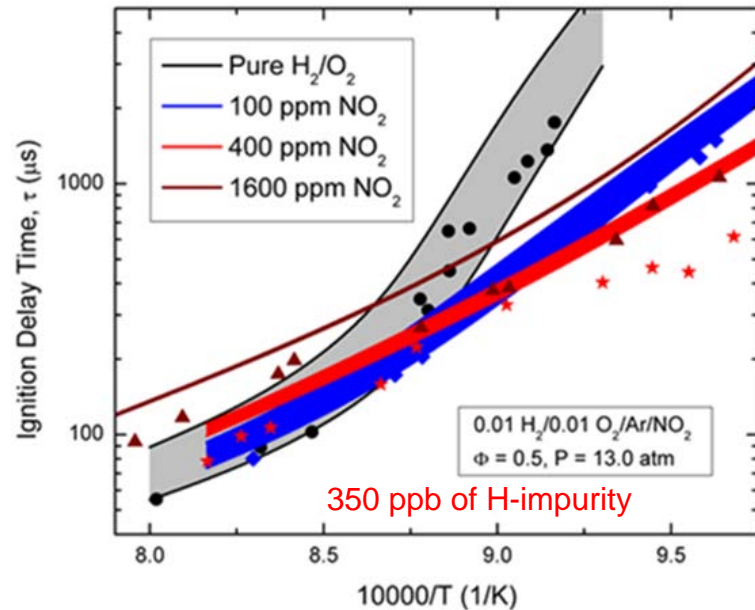


**Dominance of pressure-dependent reactions: two additional NO ↔ NO<sub>2</sub>**

# Effect of Physical and Chemical Perturbations on the Explosion limit and Ignition Delay Time of H<sub>2</sub>/O<sub>2</sub>



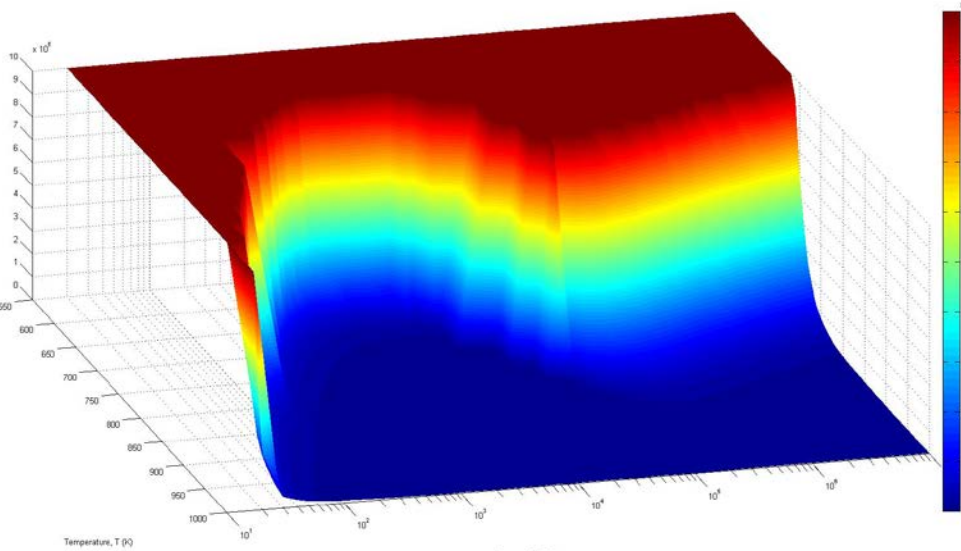
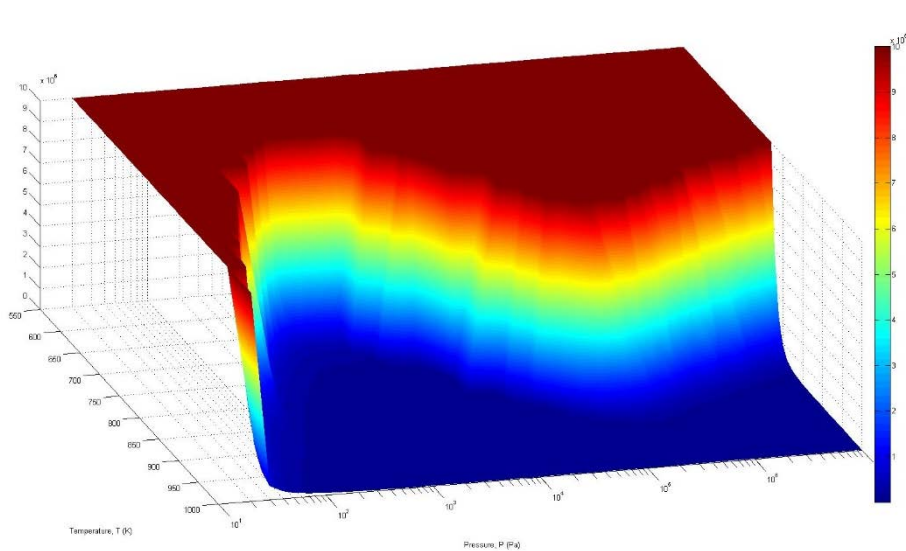
✓ Significant effects of impurities on the ignition delay time of H<sub>2</sub>-oxidation



✓ The nature of variation also changes with pressure.

# Effect of Physical and Chemical Perturbations on the Explosion limit and Ignition Delay Time of $H_2/O_2$

## Chemical Perturbation- initial NO doping

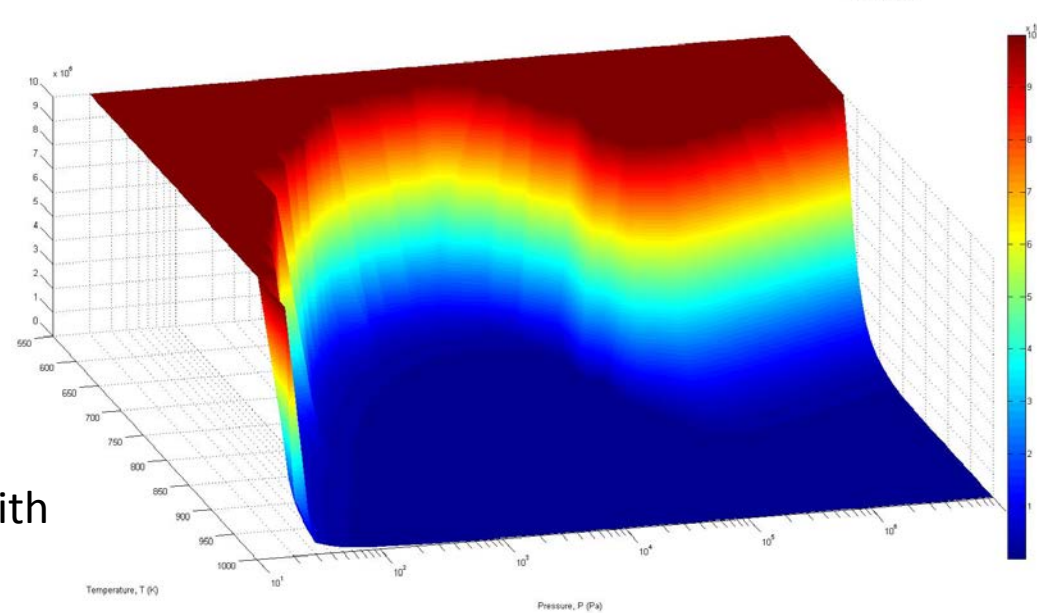


Base case

50 ppm NO

✓  $\tau$  changes more rapidly towards low T and high P along the 1<sup>st</sup> limit with a decrease in NO doping

✓ Change in  $\tau$  along the 2<sup>nd</sup> limit becomes more rapid with an increase in NO doping

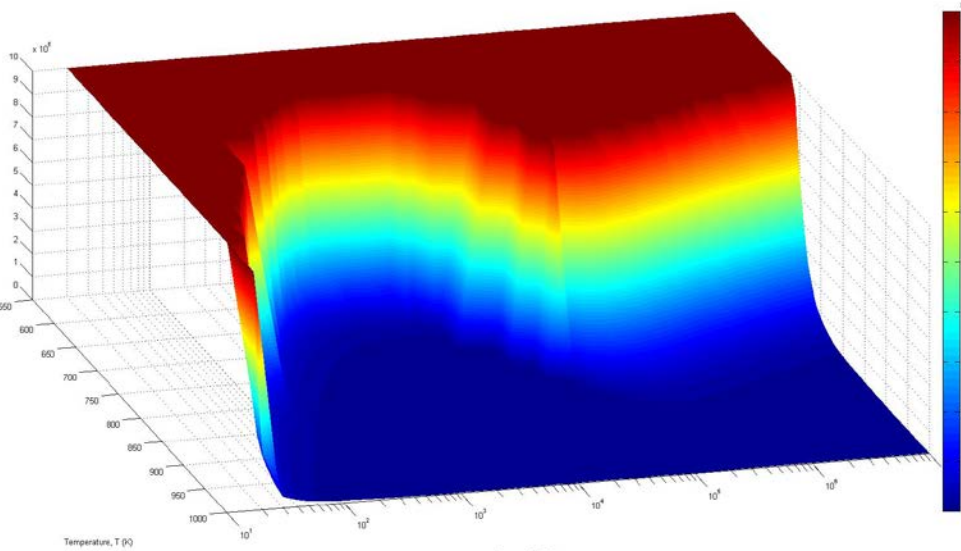
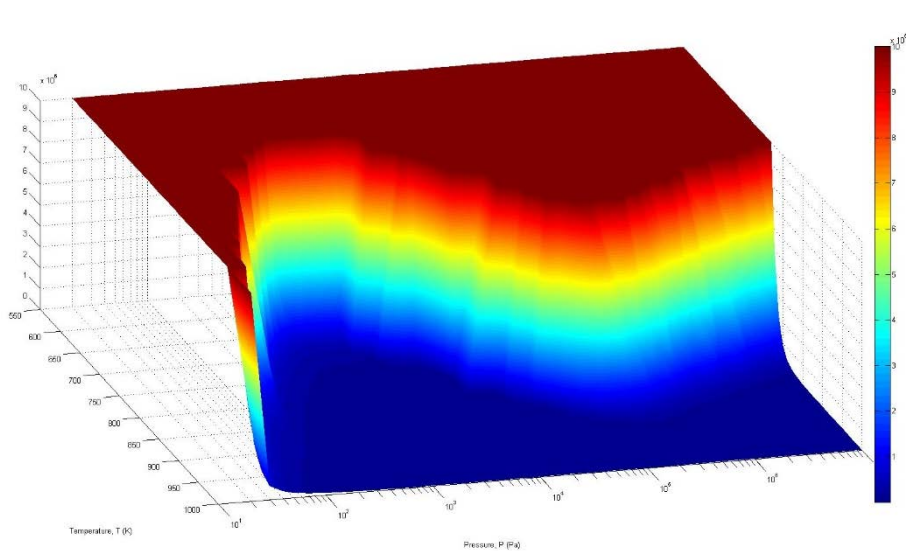


200 ppm NO



# Effect of Physical and Chemical Perturbations on the Explosion limit and Ignition Delay Time of H<sub>2</sub>/O<sub>2</sub>

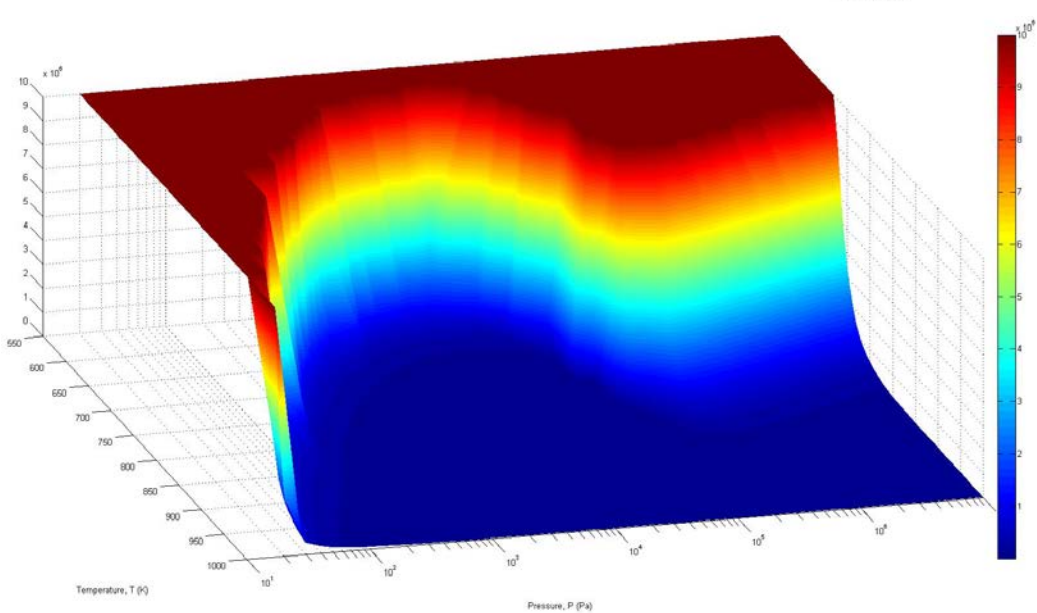
## Chemical Perturbation- initial NO doping



Base case

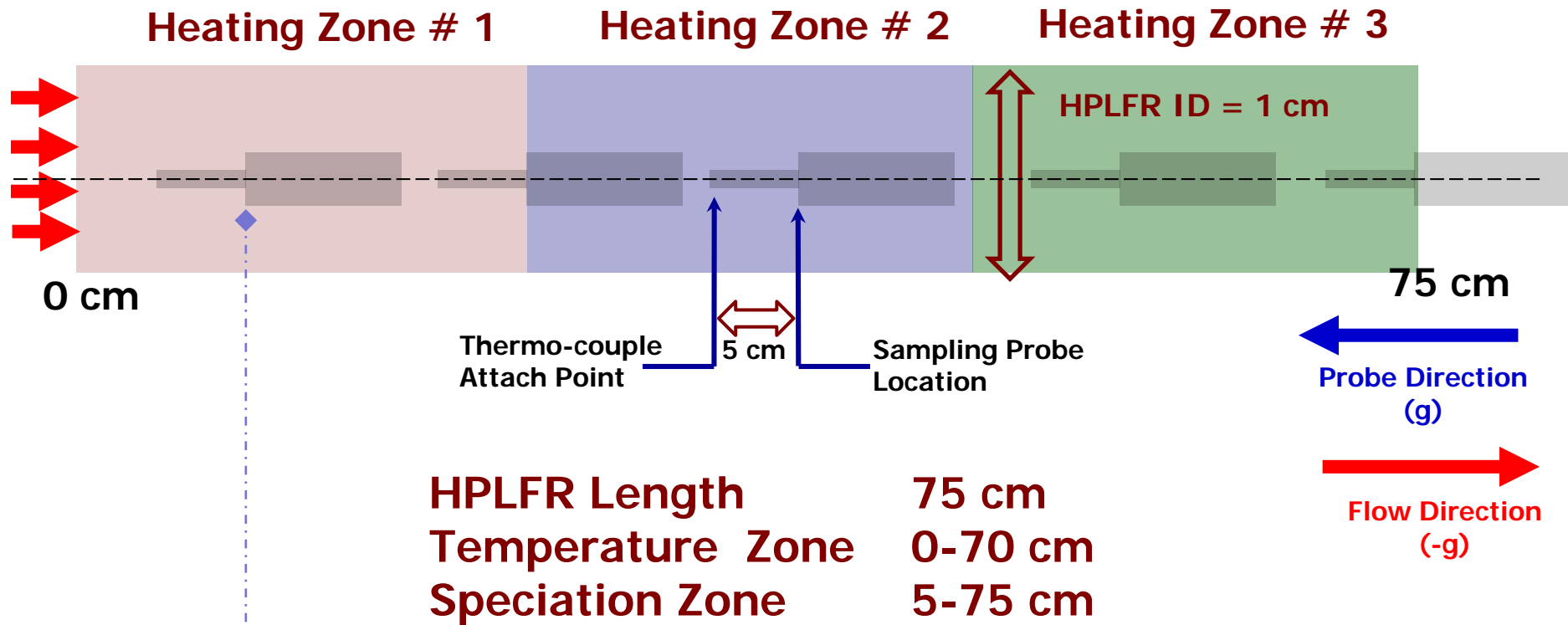
50 ppm NO

✓  $\tau$  changes more rapidly towards low T and high P along the 3<sup>rd</sup> limit with a decrease in NO doping



200 ppm NO

# Spatial → Temporal Coordinate Transformation



Last Speciation Data Point (probe moving top-to-bottom). Declare this position as  $X(\text{relative}) = 0.0$  cm

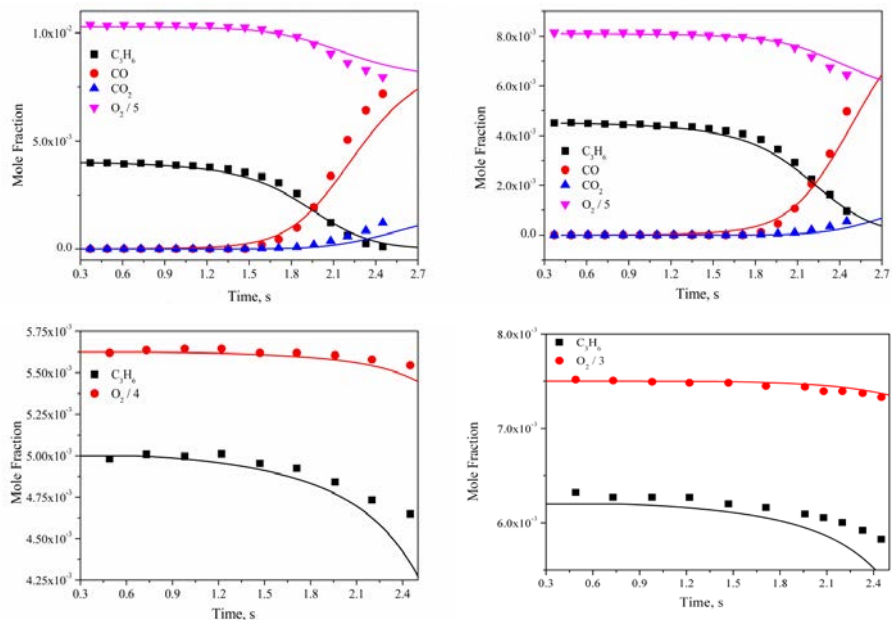
Match the corresponding "T" for each location upward already measured

Redo this until the first temperature location which is  $X(\text{end})$

Apply gas dynamics & Ideal Gas law. Get the velocity at particular location. and also get the "t"

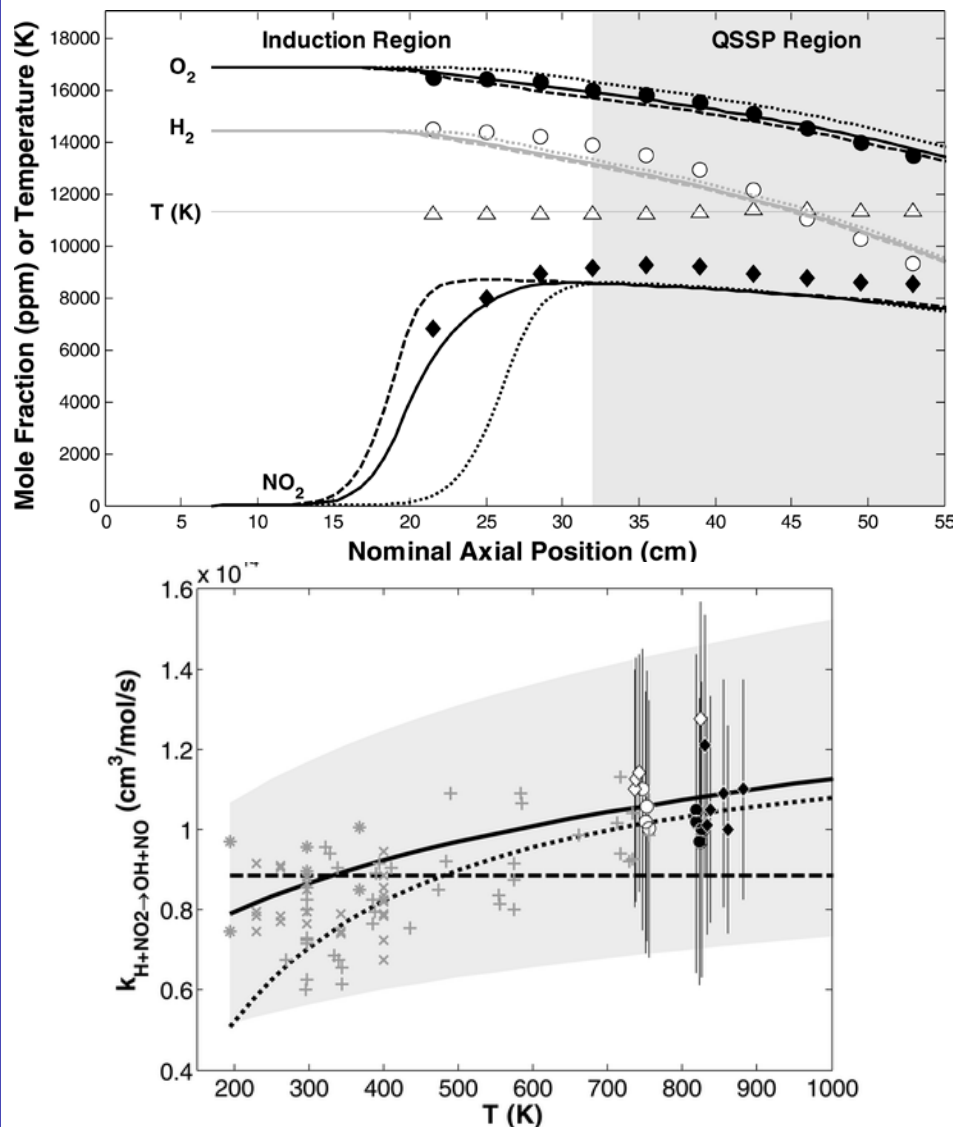
# Additional Small Species Database Efforts

## Propene oxidation<sup>1</sup>



- Recap of C<sub>3</sub>H<sub>6</sub> measurements/modeling presented at last UTSR review meeting
- Propene is an important intermediate in C<sub>3</sub>H<sub>8</sub> oxidation, as well as for kinetics of higher hydrocarbons fraction of natural gas
- Previous models predicted substantial reactivity at the relatively low reactivity ~800 K, 15 atm conditions shown

## NO<sub>x</sub>-perturbed H<sub>2</sub> oxidation<sup>2</sup>



Supported (in part) by  
Siemens Energy

1. Burke et al. *Combust Flame*. 161:2765 (2014)  
2. Haas & Dryer. *J Phys Chem A*. 119:7792 (2015)





1. Santner, J., Ahmed, S., **Farouk, T.**, Dryer, F., “Computational study of NO<sub>x</sub> formation at conditions relevant to gas turbine operation, part I” *Combustion and Flame (being submitted - November)*.
2. Ahmed, S., Santner, J., Dryer, F., Padak, B., **Farouk, T.**, “Computational study of NO<sub>x</sub> formations at conditions relevant to gas turbine operation part II: NO<sub>x</sub> in high hydrogen content fuel combustion at elevated pressure” *Combustion and Flame (being submitted - November)*.