



**Large Scale Screening of Low cost Ferritic Steel Designs for
Advanced Ultra-SuperCritical Boiler Using First Principles
Methods**

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2015 Crosscutting Technology Research Reviewing Meeting
Award # [DE-FE-0011549](#)
April 29, 2015



Outline

Background

Goal

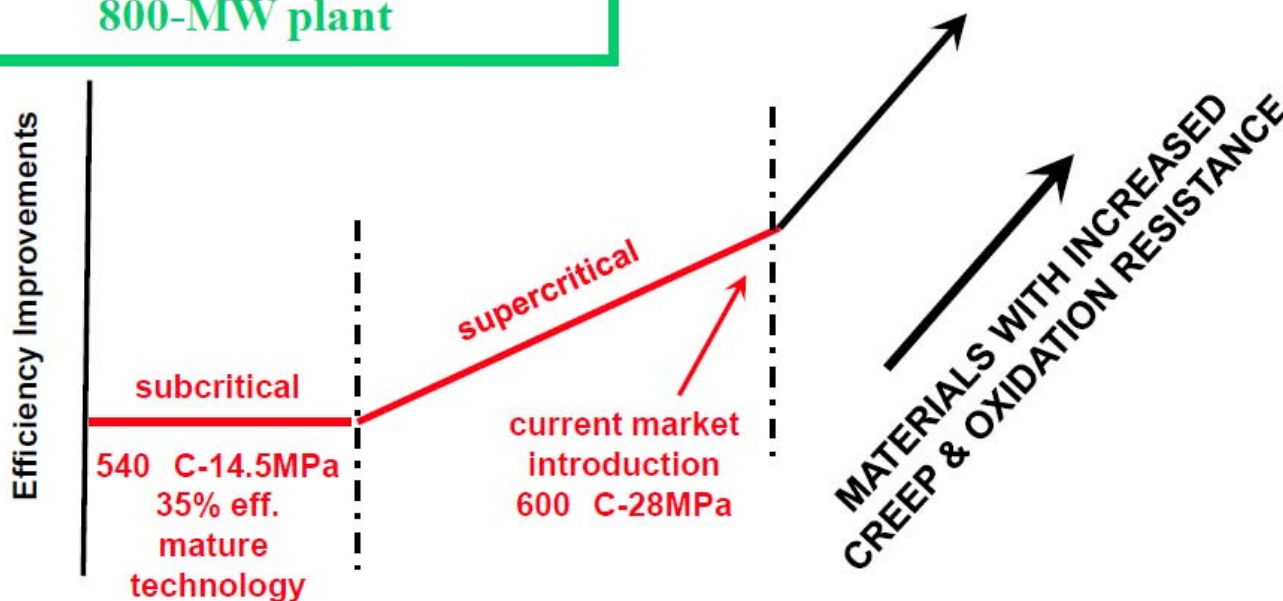
Approach

Project status

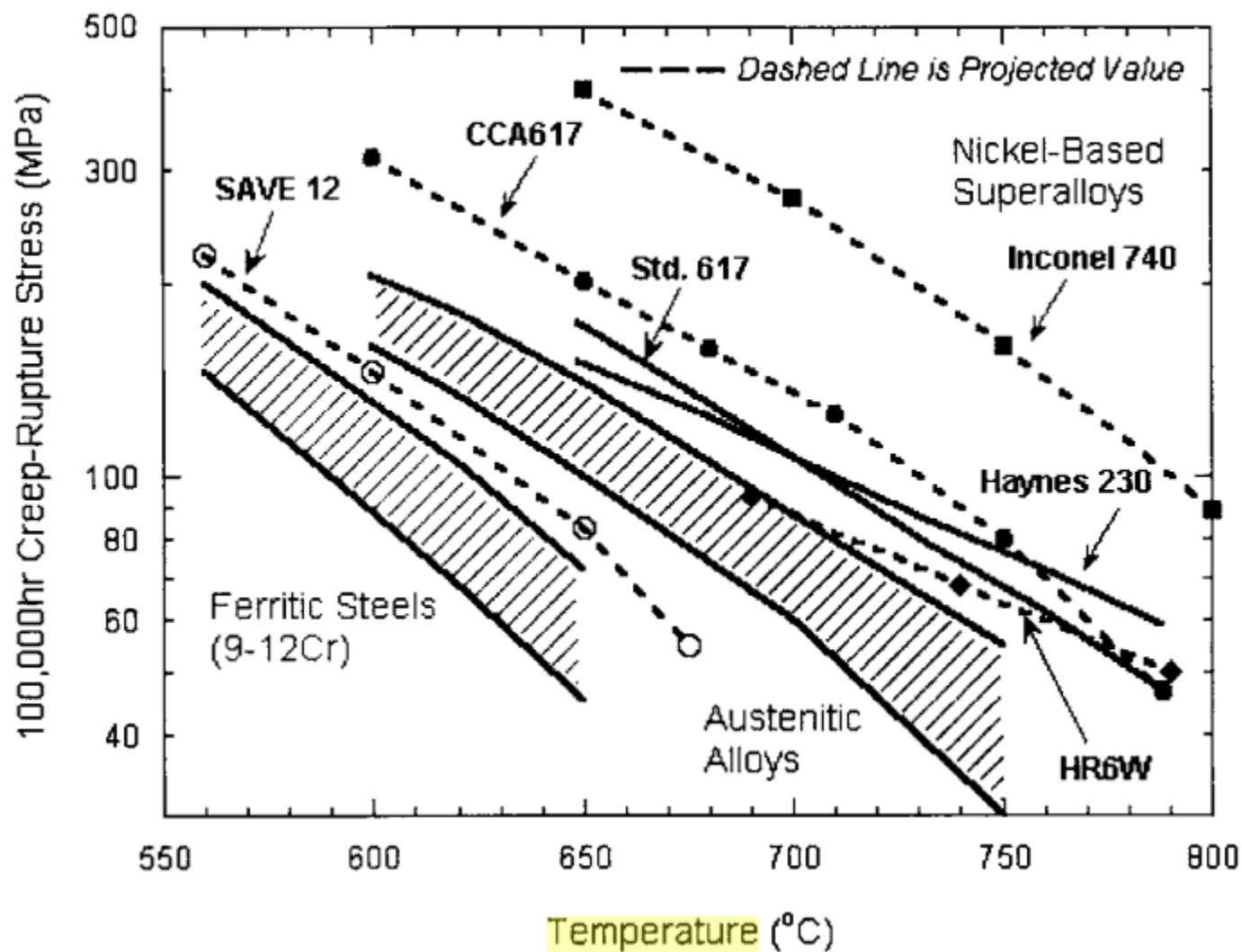
Increasing Efficiency

Each 1% increase in efficiency eliminates ~1,000,000 tons of CO₂ emissions over the lifetime of an 800-MW plant

US-DOE Advanced Power Systems:
46%-48% efficiency from coal generation
Steam condition: 760 C - 35MPa
~ 5ksi



100,000hr Creep-Rupture for USC Boiler Materials



❑ Material requirements for Advanced Ultra-SuperCritical (AUSC) boiler:

- **Low cost** metal
- Compatible thermal properties
- Sufficient high temperature performance
 - Sufficient mechanical strength
 - Creeping resistance
 - Corrosion resistance
- *Low temperature ductility*

□ Ferritic steel

- BCC matrix with low Ni content (low cost)
- Low temperature brittleness
- Weldability

□ New design of ferritic steel

- Composition modulation
- Microstructure engineering



Complexity of the Alloy Strategy

❑ Many structural factors:

➤ **Matrix**

➤ Precipitation

➤ Grain boundary

➤ Interphase

❑ Correlated problem

➤ Doping may solve a problem but bring in more problems

➤ Difficult to assess the effect of alloying

Known 9-12% Cr Ferritic Steels

Table 1. Precipitate Phases in Different Steel Phases. PT Represent for Prototype Structure and SG for Space Group Number.

Precipitate Phase	PT	SG	Steel Phases											
			P91	P92	E911	AXM	HCM12	P122	T122	NF1 2	FN5	TB12	VM12	X20
BCC_A2	W	229	X	x	x	x	x	x	x	x	x	x	x	x
M23C6	Cr23C6	225	X	x	x	x	x	x	x	x	x	x	x	x
LAVES	MgZn2	194	X	x	x		x	x	x	x	x	x	x	x
Z_PHASE	NaCl	225	X	x	x	x	x	x	x	x	x	x	x	x
NbNi₃	Al3Ti	139	X			x	x	x	x	x	x			
AlN	ZnO	194	X	x	x	x		x	x			x		
SIGMA	CrFe	136		x	x							x		
FCC_A1	Cu	225		x	x	x	x	x	x	x		x	x	x
HCP_A3	Mg	194		x	x							x		
M₂B_{Tetr}	Fe2B	140		x		x								
MU_PHASE	W6Fe7	166				x								
M6C	W3Fe3C	227				x								
Cr₂B_{Ortho}	Mg2Cu	70						x	x	x	x		x	
PI	Mo3Al2C	70										x	x	

Ferritic Steel Matrix

❑ BCC structure

❑ Composition of the BCC matrix in 9-12% Cr steels

Name	Fe	Cr	Ni	Mo	Si	Al
P91	0.9898	5.87E-4		8.42E-9	6.64E-3	2.77E-3
E911	0.9969	5.29E-4		1.13E-8	2.03E-3	5.75E-12
P92	0.9944	5.55E-4	6.10E-4	2.30E-8	3.83E-3	6.14E-4
AXM	0.9964	5.45E-4	5.96E-4	1.97E-7	1.31E-3	1.15E-3
HCM12	0.9977	5.36E-4	1.03E-5	1.19E-8	1.72E-3	
P122	0.9986	5.15E-4	6.22E-4	1.08E-11	2.99E-4	4.18E-11

- ❑ Screening ferritic steel design based on properties of the solid solution **matrix**
 - Elastic properties
 - Low temperature ductility

- ❑ Develop efficient parallel software for large scale screening calculations
 - first principles quality for solid solution system
 - Automated solid solution structure sampling
 - Automated properties calculations



Approach: Structure Modeling

- ❑ Dilute multi-component solid solution
 - requires huge atomic structure model
 - components of very low concentration considered as point defect

- ❑ Special quasi-random structures

□ Properties calculations

➤ *Supercell Approaches*

➤ *Ensemble Average of Supercells:* $F(\vec{\sigma}, T) \approx \sum_{i \in \vec{\sigma}} w_i(T) F_i(T)$

supercells are local snapshots in the infinite solid solution lattice $\vec{\sigma}$

➤ *Cluster Expansion Methods*

➤ *Weighted average of clusters:* $F(\vec{\sigma}, T) \cong \sum_{\alpha, s} K_{\alpha}^s(T) \Phi_{\alpha}^s$

α, s are cluster indices and cluster order indices

clusters are local structures in the infinite solid solution lattice $\vec{\sigma}$

➤ *Mathematically rigorous*

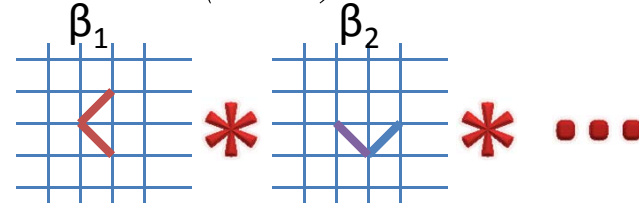
G(P,T) Module: UnitCell Expansion

Cluster Expansion Method for multi-component multi-sublattice systems:

P.D. Tepesch, et al PRL 74, 12 (1995)

$$F(\vec{\sigma}, T) \cong \sum_{\alpha, s} K_{\alpha}^s(T) \Phi_{\alpha}^s,$$

$$\Phi_{\alpha}^s = \prod_i \Phi_{\beta_i}^{s_i}; \alpha = \bigcup_i \beta_i$$



Challenge: number of cluster expansion terms n

$$n \sim (N-1)^{|\alpha|N_{\text{sublattice}}}$$

UnitCell Expansion Method for multi-component multi-sublattice systems:

$$F(\vec{\sigma}, T) \cong \sum_{\gamma, s} K_{\gamma}(T) \Phi_{\gamma}^s,$$



Rationale: Coarse grained cluster (CGC) expansion,

- Unitcells are treated as pseudo atom types
- Simplify lattice
- Expected must faster cluster interaction decaying over distance (*up to pair*)
- Much larger number of components (pseudo atoms) (*unitcell types*)

Special Quasirandom Structure

- Poor man's approximation to cluster expansion method

$$F(\vec{\sigma}, T) \cong \sum_{\alpha, s} K_{\alpha}^s(T) \Phi_{\alpha}^s,$$

$$\langle F \rangle_{SQS} \cong \sum_{\alpha, s} K_{\alpha}^s(T) \langle \Phi_{\alpha}^s \rangle_{SQS},$$

$$\langle \Phi_{\alpha}^s \rangle_{SQS} \approx \langle \Phi_{\alpha}^s \rangle$$

□ At high temperature limit

- site occupation is complete random
- correlation function is known

$$\rho_{\alpha}(\sigma_{HT}) = \prod_{i \in \alpha} \left\langle \gamma_{\alpha_i, M_i}(\sigma_i) \right\rangle_{\alpha}$$

- match SQS correlation with the known correlation function
 - ✓ Exhaustive search
 - ✓ Genetic algorithm
 - ✓ Other global optimization approach may also be used

B. Application to 9-12Cr Ferritic Steels

□ B.1 Properties of known 9-12Cr ferritic steel

- Positive control using well characterized 9-12Cr ferritic steels
 - P91, E911, P92, AXM, HCM12, P122, T122, NF12, FN5, TB12, VM12 and X20
 - Formation energy and Elastic constants will be assessed initially.
 - Assess ductility using the ratio of bulk modulus and shear modulus.
 - Stacking fault energy and surface cleavage energy will be carried out to estimate the Rice-Thomson parameter which is widely used as ductility criterion.
 - Trend analysis of indicative parameter of ductility.

B. Application to 9-12Cr Ferritic Steels

□ B.2 Screening studies of Ferritic Steels

- Screening in a progressive manner with 4 components BCC solid solutions examined first.
- Precipitation effects to be assessed through homogenization
- Global optimization methods such as simulated annealing and genetic algorithm to locate the optimal ferritic design.

Challenges In Structure Modeling

❑ Incomplete structure information about the phases in the steel

- Missing information about site distribution
 - Phase compositions are known
 - Multiple non-equivalent solid solution sites

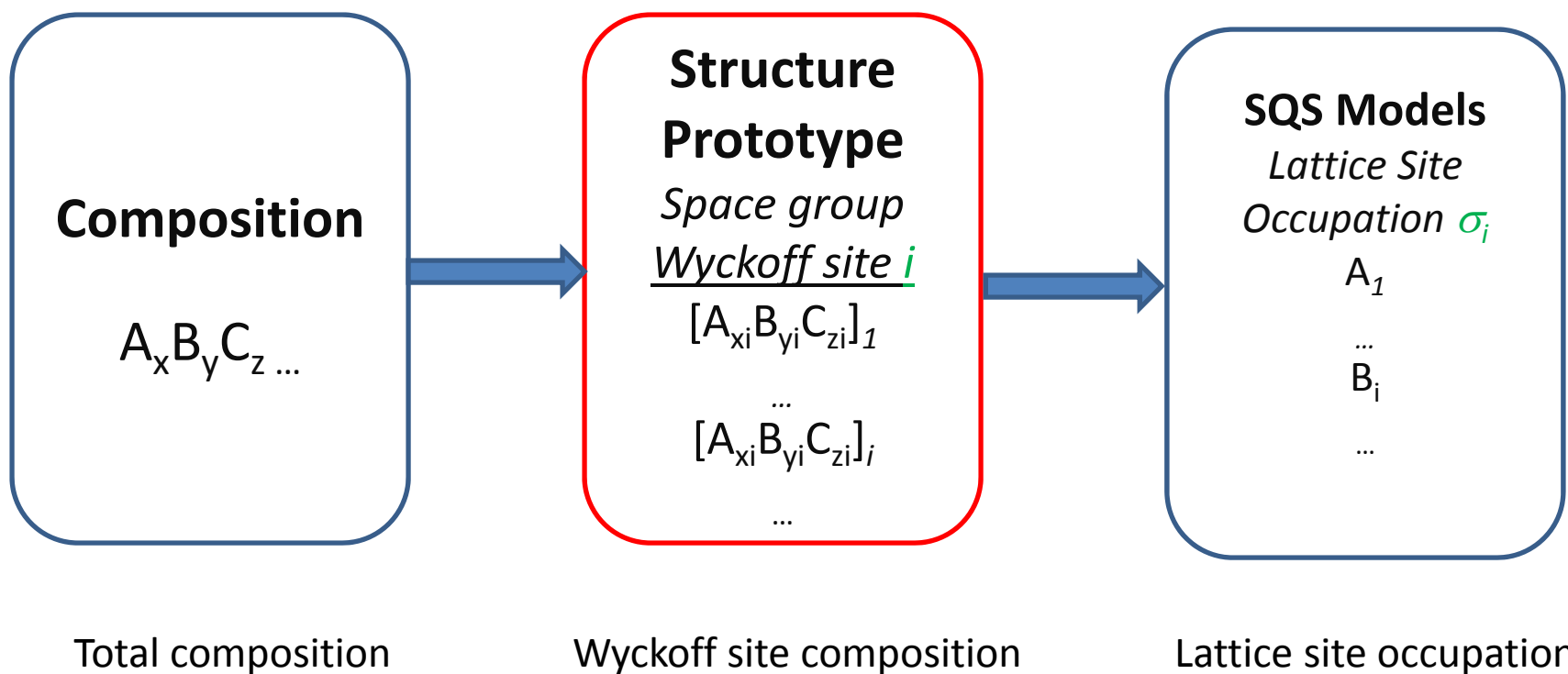
❑ Composition requires exceedingly large model

- Dopant concentration between 1000ppm to 1ppm
 - Need to assess the dopant-dopant interaction
 - Model requires > 1000 atoms
- Dilute dopant can be treated as point defect
- Using the scaling law to estimate the effect of dopant with intermediate concentration: $G \sim c^\alpha$

AXM Steel Facts

<u>Phase</u>	<u>Vol fract</u>	<u>Composition</u>	<u>Crystal</u>	<u>Microstructure</u>
BCC-A2#2	0.8464	$\text{Fe}_{0.996}\text{Si}_{0.002}\text{Al}_{0.001}$	cI2	Matrix phase
BCC-A2#1	0.1006	$\text{Cr}_{0.957}\text{Mn}_{0.043}$	cI2	Precipitation
M_{23}C_6	0.0203	$(\text{Cr}_{0.864}\text{Mn}_{0.130}\text{Fe}_{0.006})_{23}\text{C}_6$	cF116	Precipitation
μ -Phase	0.0112	$(\text{Fe}_{0.992}\text{Cr}_{0.008})_7(\text{W}_{0.650}\text{Mo}_{0.350})_6$	hR39	Precipitation
FCC-A1#1	0.0100	$\text{Ni}_{0.584}\text{Fe}_{0.370}\text{Si}_{0.046}$	cF4	Precipitation
M_6C	0.0037	$(\text{Mo}_{0.992}\text{W}_{0.008})\text{MoFe}_2\text{C}$	cF112	Precipitation
Z-Phase	0.0051	$(\text{Cr}_{0.898}\text{Fe}_{0.102})\text{VN}_{0.669}$	tP6	Precipitation
NbNi_3	0.0010	Ni_3Nb	oP8	Precipitation
AlN	0.0012	AlN	hP4	Precipitation
FCC-A1#3	0.0003	$\text{Cu}_{0.999}\text{Ni}_{0.001}$	cF4	Precipitation
M_2B	0.0003	$(\text{Mo}_{0.953}\text{Cr}_{0.047})_2\text{B}$	tI12	Precipitation

Structure Modeling



❑ Structure models generation

- Based on structure prototype
 - Limited to size < 250 atoms
 - Site-distribution based on prior knowledge

❑ Composition requires exceedingly large model

- Dopant concentration between 1000ppm to 1ppm
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Elastic Constants Calculations

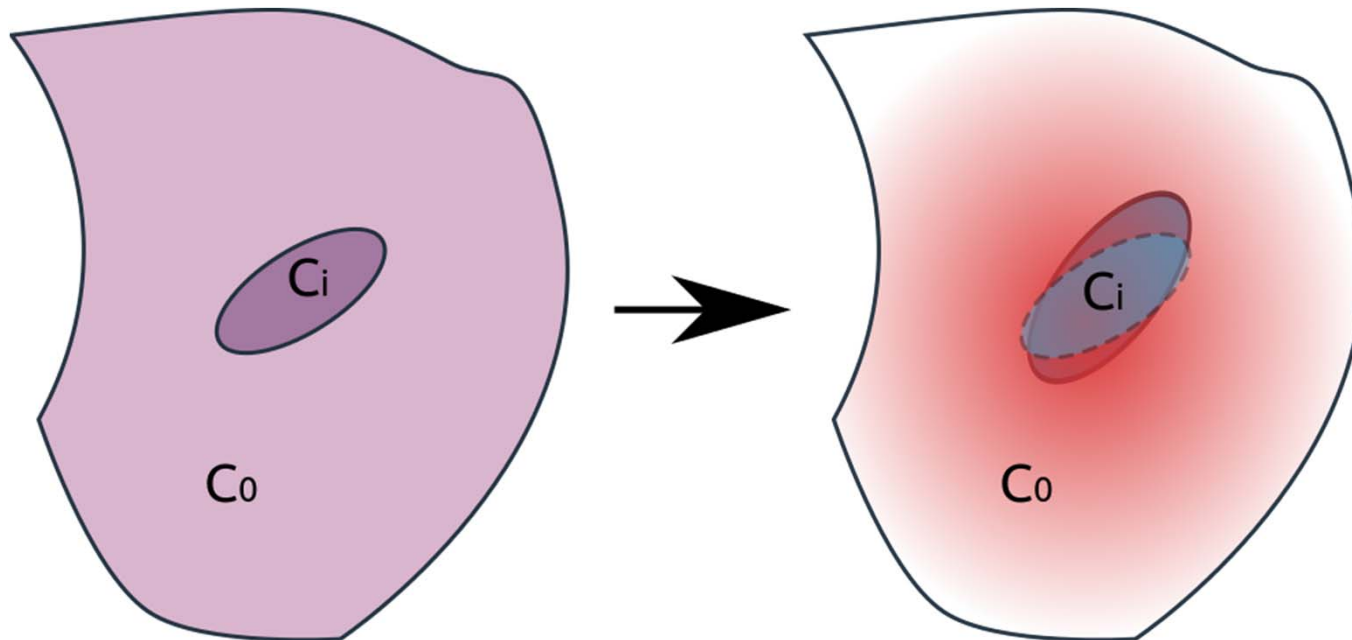
- ❑ Calculated use the in-home developed **G(p,T)** package
 - Employed VASP as the computing engine
 - Automate the calculation and fully taking advantages of symmetry
 - Both stress and energy based calculations are available
 - Accuracy setting:
 - Standard 400eV energy cutoff
 - Standard K-point sampling: metal (cutoff 35), others (cutoff 25)
 - Energy convergence 10^{-6} eV
 - Spin polarized calculation for selected phases

Elastic Constants Calculations

Phases	C_{11}, C_{22}, C_{33}	C_{44}, C_{55}, C_{66}	C_{12}, C_{13}, C_{23}	K	G	E	ν	G/K
BCC-A2#1	376 433	42 73	232 135	239	67	185	0.371	0.282
BCC-A2#2	330 estimated	110 estimated	171 estimated	224	97	253	0.311	0.433
AlN	377 356	113 125	129 99	196	122	304	0.241	0.622
FCC-A1#1	322	147	179	225	106	275	0.296	0.473
Cu	181	83	121	140	56	147	0.324	0.399
$M_{23}C_6$	459	111	216	297	115	306	0.328	0.388
M_2B	440 504	141 136	199 190	282	137	353	0.291	0.486
M_6C	442	115	203	282	117	308	0.318	0.413
μ -phase	442 426 406	92 94 94	245 225 217	293	95	256	0.354	0.323
NbNi ₃	290 305	113 111	178 153	206	91	238	0.307	0.442
Zphase	278 250	45 8	180 167	189	29	83	0.427	0.154

Precipitation Effects

- Homogenization scheme to assess the precipitation effects on elastic constants
 - Eshelby's inclusion theory



Effective Self Consistent Scheme

- ❑ Iterative scheme
- ❑ Multiple inclusion phases allowed
- ❑ Only volume fraction and bulk elastic constants used in the scheme

$$C^* = (H + C_M^{-1})^{-1}$$

$$H = \text{sum } (H_{l,i}^d (I - \Omega_{DI,i} H)^{-1})$$

$$H_{l,i}^d = c_i \{ (C_{l,i}^{-1} - C_M^{-1})^{-1} + C_M (I - S_{l,i}^M) \}^{-1}$$

$$\Omega_{DI,i} = C^* (I - S_{l,i}^*)$$



Elastic properties of AXM steel

□ Homogenized elastic modulus

Bulk modulus = 228 GPa,

Shear modulus = 94 GPa

Young's modulus = 249GPa

Poisson's ratio = 0.318



Inverse: Properties → Structure

- ❑ First principles method brings chemical accuracy for properties calculation with known structure
- ❑ The inverse process from properties to predict structure remains the greatest challenge to material science
- ❑ Two-step approach/Material genome approach
 - Properties -> Composition -> prototype library



❑ Ordered lattice structures:

- Crystal and Solid Solution
- Common description: $\{ \mathbf{L}_i \} \otimes \{ \mathbf{r}_j; \sigma_j \}$
where $\{ \mathbf{L}_i \}$ is the set of lattice symmetry operators
 $\{ \mathbf{r}_j \}$ is the set of lattice basis
 $\{ \sigma_j \}$ is the set of composition vector

❑ Composition vector σ

- $\sigma = \sum_i \eta_i \varepsilon_i$
- Each vector basis ε_i represents an element or a structure unit
- The component η_i represents the probability of the basis at the site
- Vacancy is also a basis

❑ Material Genome Approach

- The challenge is how to **traverse** the enormous configuration space
- Uniform structure indices are highly desired for data mining

❑ **LatMGA**: separate lattice from composition

- Structure = $\{ L_i \} \otimes \{ r_j; \sigma_j \} = [\{ L_i \} \otimes \{ r_j \}] \oplus [\{ L_i \} \otimes \{ \sigma_j \}]$
- Structure is indexed by lattice prototype and composition type
- Observation: **any lattice basis sets is a subset of a fine grid insider the unit cell**. For any stable structure at room temperature, **the grid needs not to be finer than the range of atomic vibration**. Therefore, any lattice may be a subset of supercell of a simple lattice such as simple cubic and hexagonal.

□ LatMGA:

➤ A systematic approach to index structure prototype

- ❖ { # lattice prototype
- ❖ { lattice unit type<fcc,hcp, etc.>,
supercell <n_xn_xn_x>,
space group }
- ❖ # composition space
- ❖ { mask vector,
composition vectors }
- ❖ }

➤ Three stage material configuration space exploration

{ lattice prototype discovery:

traverse the structure prototype indices; }

{ composition space discovery:

rules based selection of mask/composition vectors;

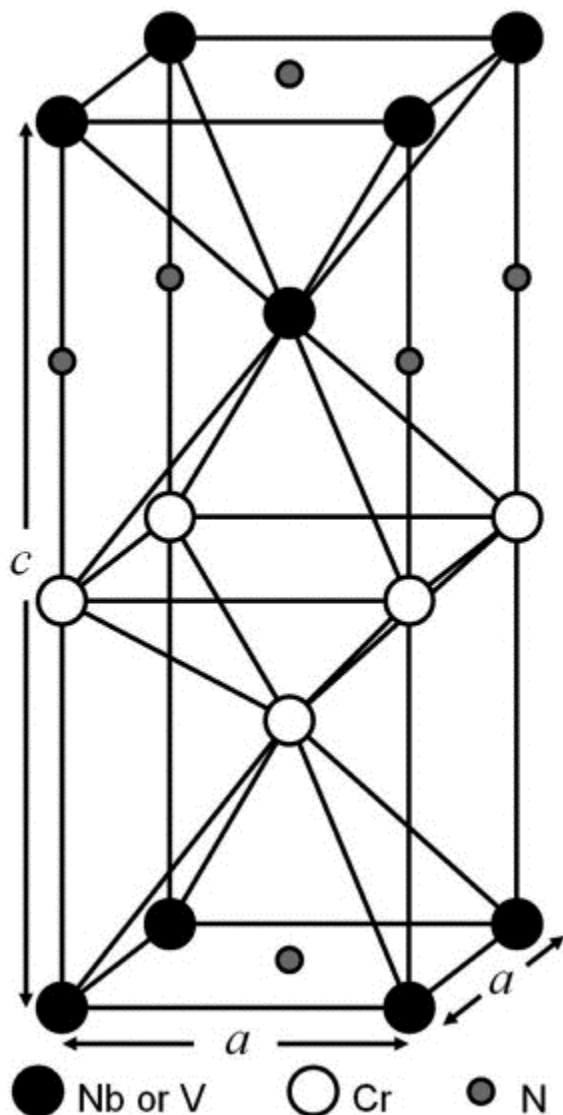
combine with lattice prototype to produce structure sample;

structure sample can be evaluated using first principles methods; }

{ material genome approach:

big data analysis on the high dimension structure indices space;

inverse map from properties to structure; }



Z-phase indices:

Lattice prototype:

space group: 129 (P4/nmm)

irreducible sites:

Site_1 2 c 1/4 1/4 7/8

Site_2 2 c 1/4 1/4 5/8

Site_3 2 c 1/4 1/4 1/8

** it is a subset of 2x2x8 **supercell** of
1 basis simple cubic lattice **casted**
into space group 129

Composition:

ε_1 =Nb, ε_2 =V ε_3 =Cr ε_4 =N ε_5 =Vac

Site_1 (0.5 0.5 0 0 0)

Site_2 (0 0 1 0 0)

Site_3 (0 0 0 1 0)

casted from scc-2-2-8 to 129 :: size= 2 2 8

space_group 129

origin 2

Aa1	0.75000	0.25000	0.00000	#	2 a Aa
Ab1	0.75000	0.25000	0.87500	#	4 f Ab
Ac1	0.75000	0.25000	0.75000	#	4 f Ac
Ad1	0.75000	0.25000	0.62500	#	4 f Ad
Ae1	0.75000	0.25000	0.50000	#	2 b Ae
Af1	0.25000	0.25000	0.00000	#	2 c Af
Ag1	0.25000	0.25000	0.12500	#	2 c Ag
Ah1	0.25000	0.25000	0.25000	#	2 c Ah
Ai1	0.25000	0.25000	0.37500	#	2 c Ai
Aj1	0.25000	0.25000	0.50000	#	2 c Aj
Ak1	0.25000	0.25000	0.62500	#	2 c Ak
Al1	0.25000	0.25000	0.75000	#	2 c Al
Am1	0.25000	0.25000	0.87500	#	2 c Am



Continue: LatMGA

Progress:

- Tested against all cubic phases found in the [Crystallography Open Database](#)
- Excluding wrongful data, all can be indexed using supercell of simple cubic casted into the specific space group and a mask to indicate the closely matched Wyckoff sites (for example, Ag1, Ak1, Am1 sites, a mask vector [0 0 0 0 0 0 1 0 0 0 1 0 1])
- We are now in the process of implementing programs to search for unexplored masks by combining with basis information of atoms such as atomic size, charge, etc.



Continue: LatMGA

Progress:

- ❑ All cubic phases with space group 225 (total 689 valid structures)
 - 304 mapped to SCC-2-2-2
 - 229 mapped to SCC-4-4-4
 - 10 mapped to SCC-6-6-6
 - 133 mapped to SCC-8-8-8
 - 13 mapped to SCC-12-12-12



Future Plan

- ❑ Study mechanical properties of all phases found in the 9-12% Cr ferritic steels;
- ❑ Search for steel composition with improved mechanical properties.
- ❑ Development of the LatMGA method for:
 - Prototype library generation based on composition
 - Automate structure model generation based on prototype library
 - Automate the properties calculation of structure models

 - Data mining to map properties to composition